DPIR Appendices Table of Contents

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Appendix B – Shadows Supporting Documentation

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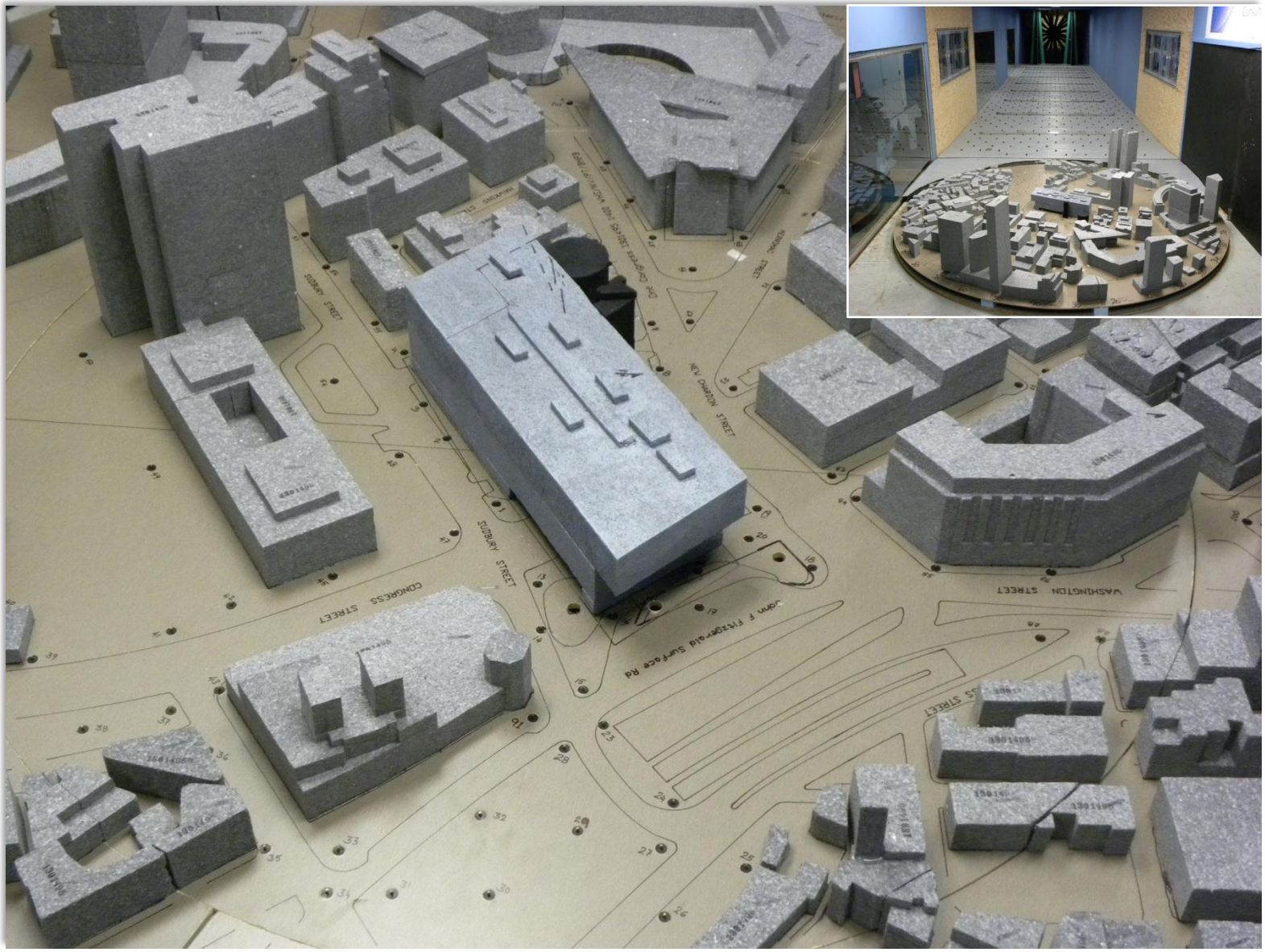
Appendix F – List of Property Owners

Appendix G – Metes and Bounds Description

Appendix H – Supplemental Graphics

Appendix A
Wind Supporting Documentation

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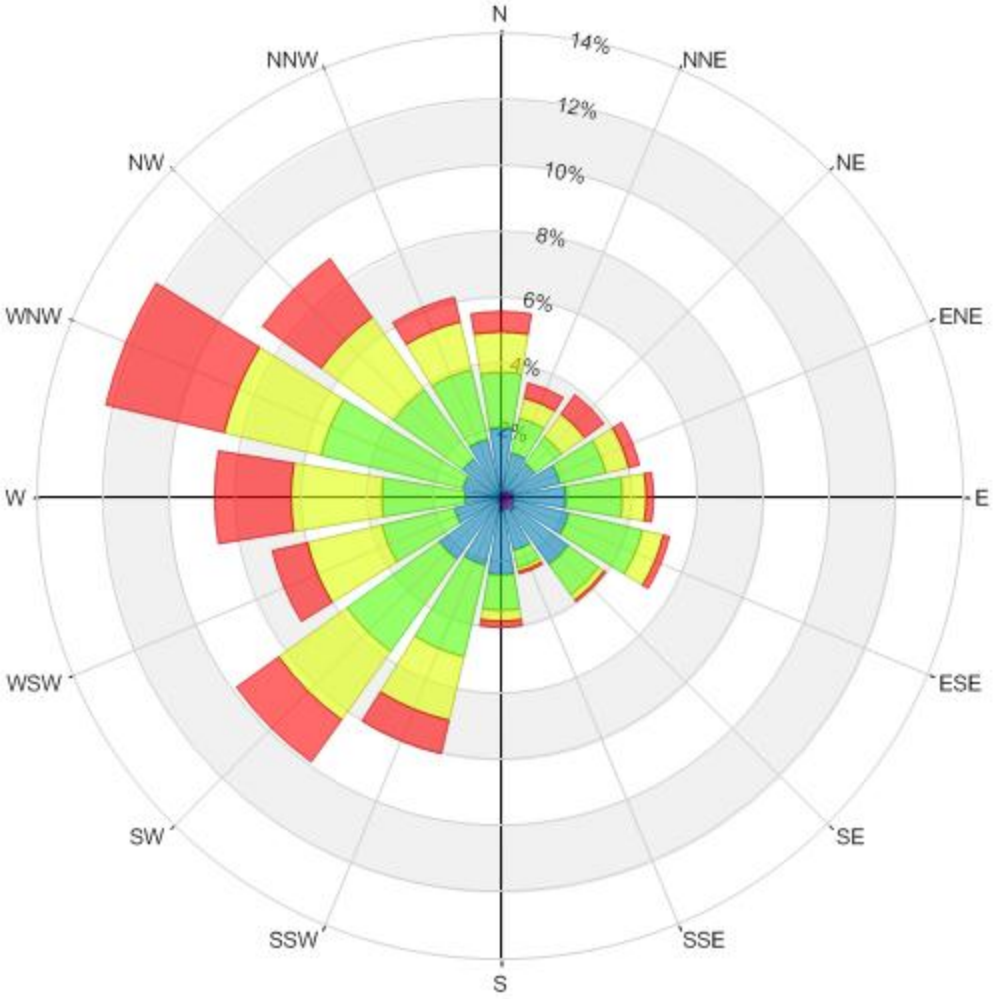
Wind Tunnel Study Model **No Build**	Figure No. 1a	RWDI
One Congress – Boston, MA Project #1301495	Date: August 19, 2013	



Wind Tunnel Study Model **Build – New Scheme**	Figure No. 1b	RWDI
One Congress – Boston, MA Project #1301495	Date: August 19, 2013	



Wind Tunnel Study Model **Mitigation – New Scheme**	Figure No. 1c	RWDI
One Congress – Boston, MA Project #1301495	Date: August 19, 2013	



Annual Winds

Wind Speed (mph)	Probability (%)
Calm	1.7
1-5	3.8
6-10	24.7
11-15	32.1
16-20	22.1
>20	15.5

Directional Distribution (%) of Winds (Blowing From)
Boston Logan International Airport (1981 - 2011)

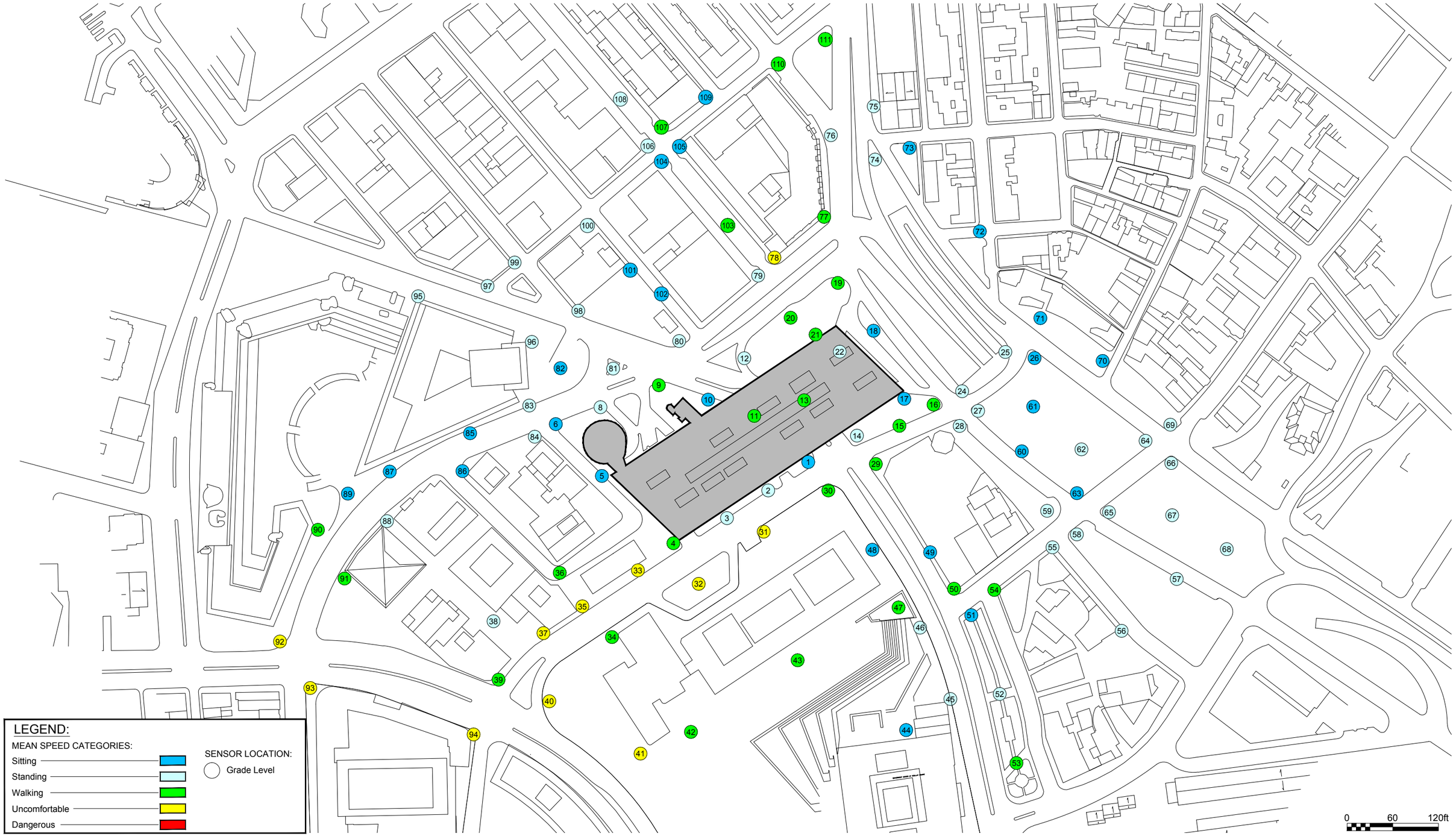
One Congress – Boston, MA

Project #1301495

Figure No. 2

Date: August 19, 2013

RWDI



Pedestrian Wind Conditions - Mean Speed -No Build

Annual (January to December, 1:00 to 24:00)

One Congress - Boston, MA

Project #1301495

True North

Drawn by:	SMR	Figure:	3a
Approx. Scale:			1"=120'
Date Revised:			Aug. 15, 2013

RWDI

LEGEND:

MEAN SPEED CATEGORIES:

- Sitting
- Standing
- Walking
- Uncomfortable
- Dangerous

SENSOR LOCATION:

- Grade Level

0 60 120ft

Pedestrian Wind Conditions - Mean Speed -Build (New Scheme)

Annual (January to December, 1:00 to 24:00)

True North

One Congress - Boston, MA

Project #1301495

Drawn by:	SMR	Figure:	3b
Approx. Scale:			1"=120'
Date Revised:			Aug. 15, 2013

RWDI

MITIGATION:

- Canopy
- Screen
- Trees

LEGEND:

MEAN SPEED CATEGORIES:

- Sitting
- Standing
- Walking
- Uncomfortable
- Dangerous

SENSOR LOCATION:

- Grade Level

0 60 120ft

Pedestrian Wind Conditions - Mean Speed - Mitigation (New Scheme)

Annual (January to December, 1:00 to 24:00)

True North

One Congress - Boston, MA

Project #1301495

Drawn by:	SMR	Figure:	3c
Approx. Scale:			1"=120'
Date Revised:			Aug. 15, 2013

RWDI

LEGEND:

EFFECTIVE GUST CATEGORIES:

Acceptable

Unacceptable

SENSOR LOCATION:

Grade Level

0 60 120ft

Pedestrian Wind Conditions - Effective Gust -No Build

Annual (January to December, 1:00 to 24:00)

True North

One Congress - Boston, MA

Project #1301495

Drawn by:	SMR	Figure:	4a
Approx. Scale:			1"=120'
Date Revised:			Aug. 15, 2013

RWDI

LEGEND:

EFFECTIVE GUST CATEGORIES:

Acceptable

Unacceptable

SENSOR LOCATION:

Grade Level

0 60 120ft

Pedestrian Wind Conditions - Effective Gust -Build (New Scheme)

Annual (January to December, 1:00 to 24:00)

True North

One Congress - Boston, MA

Project #1301495

Drawn by:	SMR	Figure:	4b
Approx. Scale:			1"=120'
Date Revised:			Aug. 15, 2013

RWDI

MITIGATION:

Canopy

Screen

Trees

LEGEND:

EFFECTIVE GUST CATEGORIES:

Acceptable

Unacceptable

SENSOR LOCATION:

Grade Level

0 60 120ft

Pedestrian Wind Conditions - Effective Gust -Mitigation (New Scheme)

Annual (January to December, 1:00 to 24:00)

True North

One Congress - Boston, MA

Project #1301495

Drawn by:	SMR	Figure:	4c
Approx. Scale:			1"=120'
Date Revised:			Aug. 15, 2013

RWDI

Appendix B
Shadows Supporting Documentation

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Note: ***The comprehensive shadow study contains a very large number of graphics and, therefore, was provided to select city agencies for review. This study can be made available on a CD-ROM upon request.***

Appendix C
Air Quality Supporting Documentation

■

MOBILE 6.2 Input Files

MOBILE 6.2 Output Files

MOBILE SOURCE ANALYSIS

- Microscale Input Files
  - Carbon Monoxide (CO)
  - Particulate Matter 10 (PM10)
  - Particulate Matter 2.5 (PM2.5)
- Microscale Output Files
  - Carbon Monoxide (CO)
  - Particulate Matter 10 (PM10)
  - Particulate Matter 2.5 (PM2.5)
- Microscale Results
  - Carbon Monoxide (CO)
  - Particulate Matter 10 (PM10)
  - Particulate Matter 2.5 (PM2.5)

STATIONARY SOURCE ANALYSIS

Mobile 6.2 Input Files

```
* Calendar Year 2013 Generic MOBILE6 input file for Mesoscale Build/No-Build
Analyses
* Filename MA13_ALL.INP created by Craig Woleader, MADEP 617-348-4046,
craig.woleader@state.ma.us and Marc Bennett, MADEP 617-292-5597,
marc.bennett@state.ma.us
* revised 12/2/05 to include actual diesel rebuild effects
* revised 12/17/08 to include new IM program program for 2013
*
***************     Header Section     ***************
MOBILE6 INPUT FILE
*
PARTICULATES       :
POLLUTANTS         : HC CO NOX CO2
DATABASE OUTPUT    :
WITH FIELDNAMES    :
AGGREGATED OUTPUT  :
SPREADSHEET        :
EMISSIONS TABLE    : MA13_WIN.tb1 REPLACE
REPORT FILE        : MA13_WIN.txt REPLACE
*
RUN DATA
***************     Run Section     ***************
> *** Mass. 2013 with LEV II Program ***

* Pollutant output format
EXPRESS HC AS VOC  :

* Mass. specific user inputs -- require external data file
REG DIST           : 2005_REG.D
I/M DESC FILE      : 09NEWIM.D

STAGE II REFUELING :
91 3 84. 84.

* Set Diesel Rebuild effects to 10% as per EPA
REBUILD EFFECTS    : 0.10

* Inputs for LEV II
94+ LDG IMP        : MA_LEV2.D
T2 EXH PHASE-IN    : LEV2EXH.D

T2 EVAP PHASE-IN   : LEV2EVAP.D

T2 CERT            : LEV2CERT.D


* Meteorological inputs

MIN/MAX TEMP       : 22.8 38.3


* Fuel inputs
FUEL RVP           : 13.5
FUEL PROGRAM       : 2 N


DIESEL FRACTIONS   :

0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000
0.003   0.003   0.002   0.002   0.002   0.002   0.001   0.001   0.001   0.000
0.001   0.001   0.003   0.001   0.002
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001   0.000   0.001   0.001   0.001   0.001
0.001   0.001   0.002   0.002   0.003
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001   0.000   0.001   0.001   0.001   0.001
```

```
0.001   0.001   0.002   0.002   0.003
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.006   0.005   0.012   0.012   0.017   0.015
0.014   0.016   0.017   0.014   0.018
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.006   0.005   0.012   0.012   0.017   0.015
0.014   0.016   0.017   0.014   0.018
0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176
0.170   0.207   0.202   0.206   0.243   0.176   0.285   0.267   0.212   0.255
0.295   0.249   0.251   0.188   0.175
0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385
0.407   0.433   0.467   0.464   0.480   0.375   0.472   0.480   0.366   0.400
0.344   0.285   0.333   0.314   0.253
0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674
0.634   0.664   0.719   0.717   0.744   0.715   0.565   0.810   0.803   0.644
0.654   0.605   0.525   0.389   0.356
0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830
0.845   0.860   0.840   0.819   0.813   0.610   0.686   0.570   0.733   0.607
0.729   0.685   0.725   0.631   0.350
0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884
0.840   0.887   0.931   0.917   0.914   0.923   0.901   0.908   0.898   0.903
0.876   0.804   0.844   0.782   0.702
0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977
0.972   0.953   0.993   0.992   0.992   0.990   0.981   0.976   0.975   0.959
0.982   0.965   0.963   0.945   0.902
0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972
0.955   0.984   0.995   0.992   0.991   0.995   0.993   0.993   0.995   0.992
0.986   0.995   0.981   0.993   0.971
1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000
1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000
1.000   1.000   1.000   1.000   1.000
0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786
0.917   0.884   0.925   0.968   0.961   0.972   0.985   0.971   0.941   0.905
0.965   0.940   0.907   0.964   0.609

***************     Scenario Section PM 2.5    ***************

****************** Freeway Scenarios ********************

SCENARIO RECORD    : MA Freeway 2.71 mph (= minimum allowed freeway speed)

CALENDAR YEAR      : 2013

EVALUATION MONTH   : 1

AVERAGE SPEED      : 2.71 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 3 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 3 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 4 mph
```

```
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 4 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 5 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 5 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 6 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 6 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 7 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 7 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 8 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 8 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 9 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 9 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 10 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 10 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
```

```
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 62 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 62 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 63 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 63 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 64 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 64 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 65 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 1
AVERAGE SPEED      : 65 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15

***************     End of This Run     ***************
END OF RUN
```

```
* Calendar Year 2013 Generic MOBILE6 input file for Mesoscale Build/No-Build
Analyses
* Filename MA13_ALL.INP created by Craig Woleader, MADEP 617-348-4046,
craig.woleader@state.ma.us and Marc Bennett, MADEP 617-292-5597,
marc.bennett@state.ma.us
* revised 12/2/05 to include actual diesel rebuild effects
* revised 12/17/08 to include new IM program program for 2013
*
***************     Header Section     ***************
MOBILE6 INPUT FILE
*
PARTICULATES       :
POLLUTANTS         : HC CO NOX CO2
DATABASE OUTPUT    :
WITH FIELDNAMES    :
AGGREGATED OUTPUT  :
SPREADSHEET        :
EMISSIONS TABLE    : MA13_SUM.tb1 REPLACE
REPORT FILE        : MA13_SUM.txt REPLACE
*
RUN DATA
***************     Run Section     ***************
> *** Mass. 2013 with LEV II Program ***

* Pollutant output format
EXPRESS HC AS VOC  :

* Mass. specific user inputs -- require external data file
REG DIST           : 2005_REG.D
I/M DESC FILE      : 09NEWIM.D

STAGE II REFUELING :
91 3 84. 84.

* Set Diesel Rebuild effects to 10% as per EPA
REBUILD EFFECTS    : 0.10

* Inputs for LEV II
94+ LDG IMP        : MA_LEV2.D
T2 EXH PHASE-IN    : LEV2EXH.D

T2 EVAP PHASE-IN   : LEV2EVAP.D

T2 CERT            : LEV2CERT.D


* Meteorological inputs
MIN/MAX TEMP       : 70.4 93.7

* Fuel inputs
FUEL RVP           : 6.8
FUEL PROGRAM       : 2 N


DIESEL FRACTIONS   :

0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000
0.003   0.003   0.002   0.002   0.002   0.002   0.001   0.001   0.001   0.000
0.001   0.001   0.003   0.001   0.002
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001   0.000   0.001   0.001   0.001   0.001
0.001   0.001   0.002   0.002   0.003
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
```

0.001 0.001 0.001 0.001 0.001 0.000 0.001 0.001 0.001 0.001
0.001 0.001 0.002 0.002 0.003
0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
0.005 0.005 0.005 0.005 0.006 0.005 0.012 0.012 0.017 0.015
0.014 0.016 0.017 0.014 0.018
0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005
0.005 0.005 0.005 0.005 0.006 0.005 0.012 0.012 0.017 0.015
0.014 0.016 0.017 0.014 0.018
0.176 0.176 0.176 0.176 0.176 0.176 0.176 0.176 0.176 0.176
0.170 0.207 0.202 0.206 0.243 0.176 0.285 0.267 0.212 0.255
0.295 0.249 0.251 0.188 0.175
0.385 0.385 0.385 0.385 0.385 0.385 0.385 0.385 0.385 0.385
0.407 0.433 0.467 0.464 0.480 0.375 0.472 0.480 0.366 0.400
0.344 0.285 0.333 0.314 0.253
0.674 0.674 0.674 0.674 0.674 0.674 0.674 0.674 0.674 0.674
0.634 0.664 0.719 0.717 0.744 0.715 0.565 0.810 0.803 0.644
0.654 0.605 0.525 0.389 0.356
0.830 0.830 0.830 0.830 0.830 0.830 0.830 0.830 0.830 0.830
0.845 0.860 0.840 0.819 0.813 0.610 0.686 0.570 0.733 0.607
0.729 0.685 0.725 0.631 0.350
0.884 0.884 0.884 0.884 0.884 0.884 0.884 0.884 0.884 0.884
0.840 0.887 0.931 0.917 0.914 0.923 0.901 0.908 0.898 0.903
0.876 0.804 0.844 0.782 0.702
0.977 0.977 0.977 0.977 0.977 0.977 0.977 0.977 0.977 0.977
0.972 0.953 0.993 0.992 0.992 0.990 0.981 0.976 0.975 0.959
0.982 0.965 0.963 0.945 0.902
0.972 0.972 0.972 0.972 0.972 0.972 0.972 0.972 0.972 0.972
0.955 0.984 0.995 0.992 0.991 0.995 0.993 0.993 0.995 0.992
0.986 0.995 0.981 0.993 0.971
1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000
1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000
1.000 1.000 1.000 1.000 1.000
0.786 0.786 0.786 0.786 0.786 0.786 0.786 0.786 0.786 0.786
0.917 0.884 0.925 0.968 0.961 0.972 0.985 0.971 0.941 0.905
0.965 0.940 0.907 0.964 0.609

********** Scenario Section PM 2.5 **********

********** Freeway Scenarios **********

SCENARIO RECORD : MA Freeway 2.71 mph (= minimum allowed freeway speed)

CALENDAR YEAR : 2013

EVALUATION MONTH : 7

AVERAGE SPEED : 2.71 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

SCENARIO RECORD : MA Freeway speed 3 mph
CALENDAR YEAR : 2013
EVALUATION MONTH : 7
AVERAGE SPEED : 3 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

```
SCENARIO RECORD    : MA Freeway speed 4 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 7
AVERAGE SPEED      : 4 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 5 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 7
AVERAGE SPEED      : 5 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 6 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 7
AVERAGE SPEED      : 6 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 7 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 7
AVERAGE SPEED      : 7 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 8 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 7
AVERAGE SPEED      : 8 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 9 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 7
AVERAGE SPEED      : 9 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 10 mph
```

```
AVERAGE SPEED      : 62 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 63 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 7
AVERAGE SPEED      : 63 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 64 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 7
AVERAGE SPEED      : 64 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 65 mph
CALENDAR YEAR      : 2013
EVALUATION MONTH   : 7
AVERAGE SPEED      : 65 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15

***************     End of This Run     ***************
END OF RUN
```

```
* Calendar Year 2028 Generic MOBILE6 input file for Mesoscale Build/No-Build
Analyses
* Filename MA28_ALL.INP created by Craig Woleader, MADEP 617-348-4046,
craig.woleader@state.ma.us and Marc Bennett, MADEP 617-292-5597,
marc.bennett@state.ma.us
* revised 12/2/05 to include actual diesel rebuild effects
* revised 12/17/08 to include new IM program program for 2028
*
***************     Header Section     ***************
MOBILE6 INPUT FILE
*
PARTICULATES       :
POLLUTANTS         : HC CO NOX CO2
DATABASE OUTPUT    :
WITH FIELDNAMES    :
AGGREGATED OUTPUT  :
SPREADSHEET        :
EMISSIONS TABLE    : MA28_WIN.tb1 REPLACE
REPORT FILE        : MA28_WIN.txt REPLACE
*
RUN DATA
***************     Run Section     ***************
> *** Mass. 2028 with LEV II Program ***

* Pollutant output format
EXPRESS HC AS VOC  :

* Mass. specific user inputs -- require external data file
REG DIST           : 2005_REG.D
I/M DESC FILE      : 09NEWIM.D

STAGE II REFUELING :
91 3 84. 84.

* Set Diesel Rebuild effects to 10% as per EPA
REBUILD EFFECTS    : 0.10

* Inputs for LEV II
94+ LDG IMP        : MA_LEV2.D
T2 EXH PHASE-IN    : LEV2EXH.D

T2 EVAP PHASE-IN   : LEV2EVAP.D

T2 CERT            : LEV2CERT.D


* Meteorological inputs

MIN/MAX TEMP       : 22.8 38.3


* Fuel inputs
FUEL RVP           : 13.5
FUEL PROGRAM       : 2 N


DIESEL FRACTIONS   :

0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000
0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000
0.000   0.000   0.000   0.000   0.000
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
```

```
0.001   0.001   0.001   0.001   0.001
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005
0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176
0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176
0.176   0.176   0.176   0.176   0.176
0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385
0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385
0.385   0.385   0.385   0.385   0.385
0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674
0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674
0.674   0.674   0.674   0.674   0.674
0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830
0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830
0.830   0.830   0.830   0.830   0.830
0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884
0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884
0.884   0.884   0.884   0.884   0.884
0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977
0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977
0.977   0.977   0.977   0.977   0.977
0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972
0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972
0.972   0.972   0.972   0.972   0.972
1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000
1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000
1.000   1.000   1.000   1.000   1.000
0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786
0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786
0.786   0.786   0.786   0.786   0.786
```

********** Scenario Section PM 2.5 **********

********** Freeway Scenarios **********

SCENARIO RECORD : MA Freeway 2.71 mph (= minimum allowed freeway speed)

CALENDAR YEAR : 2028

EVALUATION MONTH : 1

AVERAGE SPEED : 2.71 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV
PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

SCENARIO RECORD : MA Freeway speed 3 mph
CALENDAR YEAR : 2028
EVALUATION MONTH : 1
AVERAGE SPEED : 3 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV
PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

SCENARIO RECORD : MA Freeway speed 4 mph

```
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 4 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 5 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 5 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 6 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 6 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 7 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 7 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 8 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 8 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 9 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 9 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 10 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 10 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 2.5
```

```
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 62 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 62 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 63 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 63 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 64 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 64 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 65 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 1
AVERAGE SPEED      : 65 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV
PMDDR1.CSV  PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15

***************     End of This Run     ***************
END OF RUN
```

```
* Calendar Year 2028 Generic MOBILE6 input file for Mesoscale Build/No-Build
Analyses
* Filename MA28_ALL.INP created by Craig Woleader, MADEP 617-348-4046,
craig.woleader@state.ma.us and Marc Bennett, MADEP 617-292-5597,
marc.bennett@state.ma.us
* revised 12/2/05 to include actual diesel rebuild effects
* revised 12/17/08 to include new IM program program for 2028
*
***************     Header Section     ***************
MOBILE6 INPUT FILE
*
PARTICULATES       :
POLLUTANTS         : HC CO NOX CO2
DATABASE OUTPUT    :
WITH FIELDNAMES    :
AGGREGATED OUTPUT  :
SPREADSHEET        :
EMISSIONS TABLE    : MA28_SUM.tb1 REPLACE
REPORT FILE        : MA28_SUM.txt REPLACE
*
RUN DATA
***************     Run Section     ***************
> *** Mass. 2028 with LEV II Program ***

* Pollutant output format
EXPRESS HC AS VOC  :

* Mass. specific user inputs -- require external data file
REG DIST           : 2005_REG.D
I/M DESC FILE      : 09NEWIM.D

STAGE II REFUELING :
91 3 84. 84.

* Set Diesel Rebuild effects to 10% as per EPA
REBUILD EFFECTS    : 0.10

* Inputs for LEV II
94+ LDG IMP        : MA_LEV2.D
T2 EXH PHASE-IN    : LEV2EXH.D

T2 EVAP PHASE-IN   : LEV2EVAP.D

T2 CERT            : LEV2CERT.D


* Meteorological inputs
MIN/MAX TEMP       : 70.4 93.7


* Fuel inputs
FUEL RVP           : 6.8
FUEL PROGRAM       : 2 N


DIESEL FRACTIONS   :

0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000
0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000
0.000   0.000   0.000   0.000   0.000
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001
```

```
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001
0.001   0.001   0.001   0.001   0.001
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005   0.005
0.005   0.005   0.005   0.005   0.005
0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176
0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176   0.176
0.176   0.176   0.176   0.176   0.176
0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385
0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385   0.385
0.385   0.385   0.385   0.385   0.385
0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674
0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674   0.674
0.674   0.674   0.674   0.674   0.674
0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830
0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830   0.830
0.830   0.830   0.830   0.830   0.830
0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884
0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884   0.884
0.884   0.884   0.884   0.884   0.884
0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977
0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977   0.977
0.977   0.977   0.977   0.977   0.977
0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972
0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972   0.972
0.972   0.972   0.972   0.972   0.972
1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000
1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000   1.000
1.000   1.000   1.000   1.000   1.000
0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786
0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786   0.786
0.786   0.786   0.786   0.786   0.786

***************     Scenario Section PM 2.5    ***************

****************** Freeway Scenarios ******************


SCENARIO RECORD    : MA Freeway 2.71 mph (= minimum allowed freeway speed)

CALENDAR YEAR      : 2028

EVALUATION MONTH   : 7

AVERAGE SPEED      : 2.71 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 2.5
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Freeway speed 3 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 7
AVERAGE SPEED      : 3 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
```

PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

SCENARIO RECORD : MA Freeway speed 4 mph
CALENDAR YEAR : 2028
EVALUATION MONTH : 7
AVERAGE SPEED : 4 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

SCENARIO RECORD : MA Freeway speed 5 mph
CALENDAR YEAR : 2028
EVALUATION MONTH : 7
AVERAGE SPEED : 5 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

SCENARIO RECORD : MA Freeway speed 6 mph
CALENDAR YEAR : 2028
EVALUATION MONTH : 7
AVERAGE SPEED : 6 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

SCENARIO RECORD : MA Freeway speed 7 mph
CALENDAR YEAR : 2028
EVALUATION MONTH : 7
AVERAGE SPEED : 7 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

SCENARIO RECORD : MA Freeway speed 8 mph
CALENDAR YEAR : 2028
EVALUATION MONTH : 7
AVERAGE SPEED : 8 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

SCENARIO RECORD : MA Freeway speed 9 mph
CALENDAR YEAR : 2028
EVALUATION MONTH : 7
AVERAGE SPEED : 9 Freeway 92.0 0.0 0.0 8.0
PARTICULATE EF : PMGZML.CSV PMGDR1.CSV PMGDR2.CSV PMDZML.CSV PMDDR1.CSV PMDDR2.CSV
PARTICLE SIZE : 2.5
DIESEL SULFUR : 15

```
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 7
AVERAGE SPEED      : 62 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 63 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 7
AVERAGE SPEED      : 63 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 64 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 7
AVERAGE SPEED      : 64 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15


SCENARIO RECORD    : MA Arterial speed 65 mph
CALENDAR YEAR      : 2028
EVALUATION MONTH   : 7
AVERAGE SPEED      : 65 Arterial 0.0 100.0 0.0 0.0
PARTICULATE EF     : PMGZML.CSV  PMGDR1.CSV  PMGDR2.CSV  PMDZML.CSV  PMDDR1.CSV
PMDDR2.CSV
PARTICLE SIZE      : 10
DIESEL SULFUR      : 15

***************     End of This Run     ***************
END OF RUN
```

Mobile Source 6.2 Output Files

2013 Mobile Emission Rate

Arterial				Freeway			
Speed	Carbon Monoxide (CO)	Particulate Matter 10 (PM10)	Particulate Matter 2.5 (PM2.5)	Speed	Carbon Monoxide (CO)	Particulate Matter 10 (PM10)	Particulate Matter 2.5 (PM2.5)
2.5	21.7500	0.0335	0.0183	2.7	20.9700	0.0335	0.0183
3	19.6100	0.0335	0.0183	3	19.8300	0.0335	0.0183
4	16.9400	0.0335	0.0183	4	17.1600	0.0335	0.0183
5	15.3400	0.0335	0.0183	5	15.5600	0.0335	0.0183
6	14.2300	0.0335	0.0183	6	14.3800	0.0335	0.0183
7	13.4300	0.0335	0.0183	7	13.4900	0.0335	0.0183
8	12.8400	0.0335	0.0183	8	12.8200	0.0335	0.0183
9	12.3700	0.0335	0.0183	9	12.3000	0.0335	0.0183
10	12.0000	0.0335	0.0183	10	11.8900	0.0335	0.0183
11	11.6900	0.0335	0.0183	11	11.5500	0.0335	0.0183
12	11.4300	0.0335	0.0183	12	11.2800	0.0335	0.0183
13	11.2100	0.0335	0.0183	13	11.0400	0.0335	0.0183
14	11.0300	0.0335	0.0183	14	10.8500	0.0335	0.0183
15	10.8600	0.0335	0.0183	15	10.6700	0.0335	0.0183
16	10.7100	0.0335	0.0183	16	10.5400	0.0335	0.0183
17	10.5800	0.0335	0.0183	17	10.4800	0.0335	0.0183
18	10.4600	0.0335	0.0183	18	10.4200	0.0335	0.0183
19	10.3600	0.0335	0.0183	19	10.3600	0.0335	0.0183
20	10.2600	0.0335	0.0183	20	10.3100	0.0335	0.0183
21	10.1800	0.0335	0.0183	21	10.2700	0.0335	0.0183
22	10.1100	0.0335	0.0183	22	10.2300	0.0335	0.0183
23	10.0400	0.0335	0.0183	23	10.1900	0.0335	0.0183
24	9.9800	0.0335	0.0183	24	10.1600	0.0335	0.0183
25	9.9200	0.0335	0.0183	25	10.1300	0.0335	0.0183
26	9.8900	0.0335	0.0183	26	10.1000	0.0335	0.0183
27	9.8600	0.0335	0.0183	27	10.0700	0.0335	0.0183
28	9.8300	0.0335	0.0183	28	10.0500	0.0335	0.0183
29	9.8000	0.0335	0.0183	29	10.0300	0.0335	0.0183
30	9.7800	0.0335	0.0183	30	10.0100	0.0335	0.0183
31	9.7800	0.0335	0.0183	31	10.0000	0.0335	0.0183
32	9.7800	0.0335	0.0183	32	10.0000	0.0335	0.0183
33	9.7800	0.0335	0.0183	33	10.0100	0.0335	0.0183
34	9.7900	0.0335	0.0183	34	10.0100	0.0335	0.0183
35	9.7900	0.0335	0.0183	35	10.0100	0.0335	0.0183
36	9.8500	0.0335	0.0183	36	10.0700	0.0335	0.0183
37	9.9000	0.0335	0.0183	37	10.1300	0.0335	0.0183
38	9.9500	0.0335	0.0183	38	10.1800	0.0335	0.0183
39	10.0000	0.0335	0.0183	39	10.2300	0.0335	0.0183
40	10.0500	0.0335	0.0183	40	10.2900	0.0335	0.0183
41	10.1100	0.0335	0.0183	41	10.3500	0.0335	0.0183
42	10.1700	0.0335	0.0183	42	10.4100	0.0335	0.0183
43	10.2300	0.0335	0.0183	43	10.4600	0.0335	0.0183
44	10.2800	0.0335	0.0183	44	10.5200	0.0335	0.0183
45	10.3300	0.0335	0.0183	45	10.5800	0.0335	0.0183
46	10.4000	0.0335	0.0183	46	10.6500	0.0335	0.0183
47	10.4600	0.0335	0.0183	47	10.7100	0.0335	0.0183
48	10.5200	0.0335	0.0183	48	10.7700	0.0335	0.0183
49	10.5700	0.0335	0.0183	49	10.8400	0.0335	0.0183
50	10.6300	0.0335	0.0183	50	10.9100	0.0335	0.0183
51	10.6900	0.0335	0.0183	51	10.9700	0.0335	0.0183
52	10.7600	0.0335	0.0183	52	11.0400	0.0335	0.0183
53	10.8200	0.0335	0.0183	53	11.1100	0.0335	0.0183
54	10.8800	0.0335	0.0183	54	11.1900	0.0335	0.0183
55	10.9400	0.0335	0.0183	55	11.2700	0.0335	0.0183
56	11.0100	0.0335	0.0183	56	11.3400	0.0335	0.0183
57	11.0900	0.0335	0.0183	57	11.4200	0.0335	0.0183
58	11.1600	0.0335	0.0183	58	11.5100	0.0335	0.0183
59	11.2200	0.0335	0.0183	59	11.6000	0.0335	0.0183
60	11.2900	0.0335	0.0183	60	11.6800	0.0335	0.0183
61	11.3700	0.0335	0.0183	60.7	11.7400	0.0335	0.0183
62	11.4500	0.0335	0.0183	60.7	11.7400	0.0335	0.0183
63	11.5200	0.0335	0.0183	60.7	11.7400	0.0335	0.0183
64	11.5900	0.0335	0.0183	60.7	11.7400	0.0335	0.0183
65	11.6700	0.0335	0.0183	60.7	11.7400	0.0335	0.0183

2028 Mobile Emission Rate

Arterial				Freeway			
Speed	Carbon Monoxide (CO)	Particulate Matter 10 (PM10)	Particulate Matter 2.5 (PM2.5)	Speed	Carbon Monoxide (CO)	Particulate Matter 10 (PM10)	Particulate Matter 2.5 (PM2.5)
2.5	17.9900	0.0274	0.0127	2.7	17.3500	0.0274	0.0127
3	16.2700	0.0274	0.0127	3	16.4300	0.0274	0.0127
4	14.1100	0.0274	0.0127	4	14.2800	0.0274	0.0127
5	12.8200	0.0274	0.0127	5	12.9800	0.0274	0.0127
6	11.9200	0.0274	0.0127	6	12.0300	0.0274	0.0127
7	11.2800	0.0274	0.0127	7	11.3100	0.0274	0.0127
8	10.8000	0.0274	0.0127	8	10.7600	0.0274	0.0127
9	10.4200	0.0274	0.0127	9	10.3400	0.0274	0.0127
10	10.1200	0.0274	0.0127	10	10.0000	0.0274	0.0127
11	9.8700	0.0274	0.0127	11	9.7300	0.0274	0.0127
12	9.6600	0.0274	0.0127	12	9.5000	0.0274	0.0127
13	9.4800	0.0274	0.0127	13	9.3100	0.0274	0.0127
14	9.3300	0.0274	0.0127	14	9.1500	0.0274	0.0127
15	9.2000	0.0274	0.0127	15	9.0100	0.0274	0.0127
16	9.0800	0.0274	0.0127	16	8.9100	0.0274	0.0127
17	8.9700	0.0274	0.0127	17	8.8600	0.0274	0.0127
18	8.8800	0.0274	0.0127	18	8.8100	0.0274	0.0127
19	8.7900	0.0274	0.0127	19	8.7700	0.0274	0.0127
20	8.7200	0.0274	0.0127	20	8.7300	0.0274	0.0127
21	8.6500	0.0274	0.0127	21	8.7000	0.0274	0.0127
22	8.5900	0.0274	0.0127	22	8.6700	0.0274	0.0127
23	8.5300	0.0274	0.0127	23	8.6400	0.0274	0.0127
24	8.4800	0.0274	0.0127	24	8.6200	0.0274	0.0127
25	8.4400	0.0274	0.0127	25	8.5900	0.0274	0.0127
26	8.4100	0.0274	0.0127	26	8.5700	0.0274	0.0127
27	8.3900	0.0274	0.0127	27	8.5500	0.0274	0.0127
28	8.3700	0.0274	0.0127	28	8.5300	0.0274	0.0127
29	8.3500	0.0274	0.0127	29	8.5200	0.0274	0.0127
30	8.3300	0.0274	0.0127	30	8.5000	0.0274	0.0127
31	8.3300	0.0274	0.0127	31	8.5000	0.0274	0.0127
32	8.3300	0.0274	0.0127	32	8.5000	0.0274	0.0127
33	8.3300	0.0274	0.0127	33	8.5000	0.0274	0.0127
34	8.3400	0.0274	0.0127	34	8.5000	0.0274	0.0127
35	8.3400	0.0274	0.0127	35	8.5100	0.0274	0.0127
36	8.3900	0.0274	0.0127	36	8.5600	0.0274	0.0127
37	8.4400	0.0274	0.0127	37	8.6100	0.0274	0.0127
38	8.4800	0.0274	0.0127	38	8.6500	0.0274	0.0127
39	8.5200	0.0274	0.0127	39	8.6900	0.0274	0.0127
40	8.5700	0.0274	0.0127	40	8.7400	0.0274	0.0127
41	8.6200	0.0274	0.0127	41	8.8000	0.0274	0.0127
42	8.6700	0.0274	0.0127	42	8.8500	0.0274	0.0127
43	8.7200	0.0274	0.0127	43	8.8900	0.0274	0.0127
44	8.7600	0.0274	0.0127	44	8.9400	0.0274	0.0127
45	8.8100	0.0274	0.0127	45	9.0000	0.0274	0.0127
46	8.8600	0.0274	0.0127	46	9.0500	0.0274	0.0127
47	8.9100	0.0274	0.0127	47	9.1100	0.0274	0.0127
48	8.9600	0.0274	0.0127	48	9.1600	0.0274	0.0127
49	9.0100	0.0274	0.0127	49	9.2100	0.0274	0.0127
50	9.0600	0.0274	0.0127	50	9.2700	0.0274	0.0127
51	9.1200	0.0274	0.0127	51	9.3300	0.0274	0.0127
52	9.1700	0.0274	0.0127	52	9.3800	0.0274	0.0127
53	9.2200	0.0274	0.0127	53	9.4500	0.0274	0.0127
54	9.2700	0.0274	0.0127	54	9.5200	0.0274	0.0127
55	9.3200	0.0274	0.0127	55	9.5800	0.0274	0.0127
56	9.3900	0.0274	0.0127	56	9.6500	0.0274	0.0127
57	9.4500	0.0274	0.0127	57	9.7100	0.0274	0.0127
58	9.5100	0.0274	0.0127	58	9.7900	0.0274	0.0127
59	9.5700	0.0274	0.0127	59	9.8600	0.0274	0.0127
60	9.6200	0.0274	0.0127	60	9.9300	0.0274	0.0127
61	9.6900	0.0274	0.0127	60.7	9.9800	0.0274	0.0127
62	9.7600	0.0274	0.0127	60.7	9.9800	0.0274	0.0127
63	9.8200	0.0274	0.0127	60.7	9.9800	0.0274	0.0127
64	9.8800	0.0274	0.0127	60.7	9.9800	0.0274	0.0127
65	9.9400	0.0274	0.0127	60.7	9.9800	0.0274	0.0127

Mobile Source Analysis

Microscale (CAL3QHC) Input Files

- **2013 Existing**
- **2028 No-Build Condition**
- **2028 Build Condition**

2013 Existing Microscale Input Files (Carbon Monoxide (CO))

```
'Government Center Garage'   60   175   0   0   60   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Caus/Wash NE1'   6548.31   7035.9   6
'Caus/Wash NE2'   6581.41   6968.6   6
'Caus/Wash NE3'   6614.5   6901.3   6
'Caus/Wash NE4'   6669.75   6952.02   6
'Caus/Wash NE5'   6725   7002.74   6
'Caus/Wash SE1'   6753.58   6912.24   6
'Caus/Wash SE2'   6698.92   6862.05   6
'Caus/Wash SE3'   6643.09   6810.79   6
'Caus/Wash SE4'   6646.8   6736.4   6
'Caus/Wash SE5'   6649.95   6660.95   6
'Caus/Wash SW1'   6544.02   6561.02   6
'Caus/Wash SW2'   6540.9   6635.95   6
'Caus/Wash SW3'   6537.77   6710.89   6
'Caus/Wash SW4'   6476.83   6667.16   6
'Caus/Wash SW5'   6415.9   6623.44   6
'Caus/Wash NW1'   6407.38   6737.95   6
'Caus/Wash NW2'   6468.31   6781.67   6
'Caus/Wash NW3'   6529.25   6825.39   6
'Caus/Wash NW4'   6496.16   6892.69   6
'Caus/Wash NW5'   6463.06   6960   6
'Tha/Val NE1'   6667.28   6395.45   6
'Tha/Val NE2'   6668.3   6320.45   6
'Tha/Val NE3'   6669.31   6245.46   6
'Tha/Val NE4'   6744.31   6245.46   6
'Tha/Val NE5'   6819.25   6249.58   6
'Tha/Val SE1'   6822.27   6191.64   6
'Tha/Val SE2'   6747.3   6189.58   6
'Tha/Val SE3'   6672.33   6187.52   6
'Tha/Val SE4'   6671.6   6112.53   6
'Tha/Val SE5'   6670.88   6037.53   6
'Tha/Val SW1'   6560.17   5964.68   6
'Tha/Val SW2'   6560.89   6039.67   6
'Tha/Val SW3'   6561.62   6114.67   6
'Tha/Val SW4'   6502.18   6068.93   6
'Tha/Val SW5'   6442.74   6023.18   6
'Tha/Val NW1'   6440.95   6115.18   6
'Tha/Val NW2'   6500.39   6160.92   6
'Tha/Val NW3'   6559.82   6206.67   6
'Tha/Val NW4'   6558.81   6281.66   6
'Tha/Val NW5'   6557.8   6356.65   6
'Existing'   48   1   0   'C'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
90   70   3   223   54.3875   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
90   66   3   481   54.3875   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
90   68   3   527   54.3875   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
90   48   3   265   54.3875   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
90   70   3   142   54.3875   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
90   66   3   166   54.3875   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
90   68   3   265   54.3875   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
90   48   3   208   54.3875   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   56   3   2210   54.3875   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
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150   125   3   296   54.3875   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   73   3   216   54.3875   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
 1
150   108   3   693   54.3875   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   119   3   388   54.3875   1600   1   3
 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
100   34   3   1575   54.3875   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
100   66   3   253   54.3875   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
100   34   3   743   54.3875   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1528   54.3875   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   269   54.3875   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1797   54.3875   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   80   54.3875   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   374   54.3875   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   75   3   598   54.3875   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   916   54.3875   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   306   54.3875   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   16   54.3875   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1120   9.783   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1275   9.783   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   817   9.783   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1322   9.783   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3211   9.783   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1012   9.783   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2221   9.783   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1162   9.783   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2247   9.783   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   91   9.783   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2524   9.783   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   280   9.783   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   1841   9.783   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   269   9.783   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   80   9.783   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   811   9.783   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   374   9.783   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   650   9.783   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   406   9.783   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1226   9.783   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   978   9.783   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1420   9.783   1   98
 1
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'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   44   9.783   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   50   0.3048   1   0
'Bev/Was N1'   6561.96   6150.17   6
'Bev/Was N2'   6561.23   6075.17   6
'Bev/Was N3'   6560.51   6000.18   6
'Bev/Was N4'   6515.8   6060.39   6
'Bev/Was N5'   6471.09   6120.61   6
'Bev/Was SE1'   6670.99   6049.68   6
'Bev/Was SE2'   6670.19   5966.32   6
'Bev/Was SE3'   6624   5907.23   6
'Bev/Was SE4'   6626.07   5832.26   6
'Bev/Was SE5'   6628.13   5757.29   6
'Bev/Was SW1'   6541.84   5766.87   6
'Bev/Was SW2'   6540.09   5841.85   6
'Bev/Was SW3'   6537.71   5916.82   6
'Bev/Was SW4'   6493   5977.03   6
'Bev/Was SW5'   6448.29   6037.25   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Wash/Cong NE1'   6910.24   4571.18   6
'Wash/Cong NE2'   6925.8   4497.81   6
'Wash/Cong NE3'   6941.37   4424.45   6
'Wash/Cong NE4'   7012.01   4449.65   6
'Wash/Cong NE5'   7082.65   4474.85   6
'Wash/Cong SE1'   7095.42   4388.1   6
'Wash/Cong SE2'   7024.78   4362.9   6
'Wash/Cong SE3'   6954.14   4337.69   6
'Wash/Cong SE4'   6968.42   4264.06   6
'Wash/Cong SE5'   6982.69   4190.43   6
'Wash/Cong SW1'   6867.47   4164.74   6
'Wash/Cong SW2'   6853.27   4238.01   6
'Wash/Cong SW3'   6838.93   4312   6
'Wash/Cong SW4'   6765.63   4296.1   6
'Wash/Cong SW5'   6692.34   4280.2   6
'Wash/Cong NW1'   6682.41   4353.77   6
'Wash/Cong NW2'   6755.7   4369.67   6
'Wash/Cong NW3'   6828.9   4386.02   6
'Wash/Cong NW4'   6813.33   4459.38   6
'Wash/Cong NW5'   6797.76   4532.75   6
'Existing'   48   1   0   'C'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
90   70   3   223   54.3875   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
90   66   3   481   54.3875   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
90   68   3   527   54.3875   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
90   48   3   265   54.3875   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
90   70   3   142   54.3875   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
90   66   3   166   54.3875   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
90   68   3   265   54.3875   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
90   48   3   208   54.3875   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   56   3   2210   54.3875   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
150   125   3   296   54.3875   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   73   3   216   54.3875   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   108   3   693   54.3875   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   119   3   388   54.3875   1600   1   3
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 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
100   34   3   1575   54.3875   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
100   66   3   253   54.3875   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
100   34   3   743   54.3875   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1528   54.3875   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   269   54.3875   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1797   54.3875   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   80   54.3875   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   374   54.3875   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   75   3   598   54.3875   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   916   54.3875   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   306   54.3875   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   16   54.3875   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1120   9.783   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1275   9.783   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   817   9.783   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1322   9.783   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3211   9.783   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1012   9.783   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2221   9.783   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1162   9.783   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2247   9.783   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   91   9.783   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2524   9.783   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   280   9.783   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   1841   9.783   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   269   9.783   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   80   9.783   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   811   9.783   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   374   9.783   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   650   9.783   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   406   9.783   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1226   9.783   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   978   9.783   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1420   9.783   1   98
 1
'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   44   9.783   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   35   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Existing'   21   1   0   'C'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
100   79   3   208   54.3875   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
100   74   3   595   54.3875   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
100   71   3   332   54.3875   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
100   79   3   259   54.3875   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
100   79   3   66   54.3875   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
100   74   3   176   54.3875   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
100   71   3   371   54.3875   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
100   79   3   300   54.3875   1600   1   3
 2
'Char/93 SB_LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   62   3   1488   54.3875   1600   1   3
 2
'Char/93 WB_LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   60   3   298   54.3875   1600   1   3
 2
'Char/93 EB_TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   60   3   908   54.3875   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1289   9.783   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1112   9.783   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   999   9.783   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1207   9.783   1   78
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   1635   9.783   1   66
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   298   9.783   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   847   9.783   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   908   9.783   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   449   9.783   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   314   9.783   1   42
 1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2013EX'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   436   54.3875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   650   54.3875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   109   54.3875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   637   54.3875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   194   54.3875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   318   54.3875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   429   54.3875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   265   54.3875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   260   54.3875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   330   54.3875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   811   54.3875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   95   54.3875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   484   54.3875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   854   54.3875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   73   3   487   54.3875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   405   54.3875   1600   1   3
 2
```



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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   25   54.3875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   338   54.3875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   802   9.783   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1038   9.783   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1204   9.783   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   870   9.783   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   923   9.783   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1472   9.783   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   877   9.783   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1546   9.783   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   285   9.783   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   483   9.783   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   405   9.783   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   338   9.783   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   25   9.783   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1421   9.783   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1512   9.783   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   487   9.783   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2013EX'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   541   54.3875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   449   54.3875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   241   54.3875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   452   54.3875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   417   54.3875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   214   54.3875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   233   54.3875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   391   54.3875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   276   54.3875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   503   54.3875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   726   54.3875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   98   54.3875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   394   54.3875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   863   54.3875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   72   3   766   54.3875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   322   54.3875   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   35   54.3875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   853   54.3875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   818   9.783   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1226   9.783   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1219   9.783   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   859   9.783   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   796   9.783   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1264   9.783   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   954   9.783   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1198   9.783   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   805   9.783   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   405   9.783   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   322   9.783   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   853   9.783   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   35   9.783   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1185   9.783   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1465   9.783   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   766   9.783   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'   6492.55   5309.91   6
'Sud/Merr NE2'   6554.76   5268.01   6
'Sud/Merr NE3'   6616.16   5224.93   6
'Sud/Merr NE4'   6604.72   5255.31   6
'Sud/Merr NE5'   6753.29   5285.7   6
'Sud/Merr SE1'   6792.88   5222.3   6
'Sud/Merr SE2'   6724.31   5191.92   6
'Sud/Merr SE3'   6655.74   5161.53   6
'Sud/Merr SE4'   6695.46   5097.91   6
'Sud/Merr SE5'   6735.19   5034.29   6
'Sud/Merr SW1'   6638.58   4981.33   6
'Sud/Merr SW2'   6598.85   5044.95   6
'Sud/Merr SW3'   6559.13   5108.56   6
'Sud/Merr SW4'   6493.36   5072.52   6
'Sud/Merr SW5'   6427.59   5036.47   6
'Sud/Merr NW1'   6347.76   5104.47   6
'Sud/Merr NW2'   6413.53   5140.52   6
'Sud/Merr NW3'   6479.3   5176.56   6
'Sud/Merr NW4'   6417.09   5218.46   6
'Sud/Merr NW5'   6354.88   5260.35   6
'Sud/Sur NE1'   6755.94   5445.69   6
'Sud/Sur NE2'   6800.97   5385.71   6
'Sud/Sur NE3'   6845.99   5325.73   6
'Sud/Sur NE4'   6908.75   5366.8   6
'Sud/Sur NE5'   6971.5   5407.88   6
'Sud/Sur SE1'   7002.41   5368.35   6
'Sud/Sur SE2'   6939.66   5327.28   6
'Sud/Sur SE3'   6876.91   5286.2   6
'Sud/Sur SE4'   6931.69   5234.97   6
'Sud/Sur SE5'   6986.46   5183.75   6
'Sud/Sur SW1'   6932.3   5133.08   6
'Sud/Sur SE2'   6877.52   5184.31   6
'Sud/Sur SE3'   6822.74   5235.54   6
'Sud/Sur SE4'   6754.17   5205.15   6
'Sud/Sur SE5'   6685.61   5174.76   6
'Sud/Sur NW1'   6645.53   5237.94   6
'Sud/Sur NW2'   6714.1   5268.33   6
'Sud/Sur NW3'   6782.66   5298.72   6
'Sud/Sur NW4'   6709.54   5315.38   6
'Sud/Sur NW5'   6636.41   5332.03   6
'Sud/Sur N1'   6642.36   5493.71   6
'Sud/Sur N2'   6687.39   5433.73   6
'Sud/Sur N3'   6732.41   5373.75   6
'Sud/Sur N4'   6659.29   5390.41   6
'Sud/Sur N5'   6586.16   5407.07   6
'2013EX'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   436   54.3875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   650   54.3875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   109   54.3875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   637   54.3875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   194   54.3875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   318   54.3875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   429   54.3875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   265   54.3875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   260   54.3875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   330   54.3875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   811   54.3875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   95   54.3875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   484   54.3875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   854   54.3875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
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100   73   3   487   54.3875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   405   54.3875   1600   1   3
 2
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   25   54.3875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   338   54.3875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   802   9.783   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1038   9.783   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1204   9.783   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   870   9.783   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   923   9.783   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1472   9.783   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   877   9.783   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1546   9.783   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   285   9.783   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   483   9.783   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   405   9.783   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   338   9.783   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   25   9.783   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1421   9.783   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1512   9.783   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   487   9.783   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'   6492.55   5309.91   6
'Sud/Merr NE2'   6554.76   5268.01   6
'Sud/Merr NE3'   6616.16   5224.93   6
'Sud/Merr NE4'   6604.72   5255.31   6
'Sud/Merr NE5'   6753.29   5285.7   6
'Sud/Merr SE1'   6792.88   5222.3   6
'Sud/Merr SE2'   6724.31   5191.92   6
'Sud/Merr SE3'   6655.74   5161.53   6
'Sud/Merr SE4'   6695.46   5097.91   6
'Sud/Merr SE5'   6735.19   5034.29   6
'Sud/Merr SW1'   6638.58   4981.33   6
'Sud/Merr SW2'   6598.85   5044.95   6
'Sud/Merr SW3'   6559.13   5108.56   6
'Sud/Merr SW4'   6493.36   5072.52   6
'Sud/Merr SW5'   6427.59   5036.47   6
'Sud/Merr NW1'   6347.76   5104.47   6
'Sud/Merr NW2'   6413.53   5140.52   6
'Sud/Merr NW3'   6479.3   5176.56   6
'Sud/Merr NW4'   6417.09   5218.46   6
'Sud/Merr NW5'   6354.88   5260.35   6
'Sud/Sur NE1'   6755.94   5445.69   6
'Sud/Sur NE2'   6800.97   5385.71   6
'Sud/Sur NE3'   6845.99   5325.73   6
'Sud/Sur NE4'   6908.75   5366.8   6
'Sud/Sur NE5'   6971.5   5407.88   6
'Sud/Sur SE1'   7002.41   5368.35   6
'Sud/Sur SE2'   6939.66   5327.28   6
'Sud/Sur SE3'   6876.91   5286.2   6
'Sud/Sur SE4'   6931.69   5234.97   6
'Sud/Sur SE5'   6986.46   5183.75   6
'Sud/Sur SW1'   6932.3   5133.08   6
'Sud/Sur SE2'   6877.52   5184.31   6
'Sud/Sur SE3'   6822.74   5235.54   6
'Sud/Sur SE4'   6754.17   5205.15   6
'Sud/Sur SE5'   6685.61   5174.76   6
'Sud/Sur NW1'   6645.53   5237.94   6
'Sud/Sur NW2'   6714.1   5268.33   6
'Sud/Sur NW3'   6782.66   5298.72   6
'Sud/Sur NW4'   6709.54   5315.38   6
'Sud/Sur NW5'   6636.41   5332.03   6
'Sud/Sur N1'   6642.36   5493.71   6
'Sud/Sur N2'   6687.39   5433.73   6
'Sud/Sur N3'   6732.41   5373.75   6
'Sud/Sur N4'   6659.29   5390.41   6
'Sud/Sur N5'   6586.16   5407.07   6
'2013EX'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   541   54.3875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   449   54.3875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   241   54.3875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   452   54.3875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   417   54.3875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   214   54.3875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   233   54.3875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   391   54.3875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   276   54.3875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   503   54.3875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   726   54.3875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   98   54.3875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   394   54.3875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   863   54.3875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
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100   72   3   766   54.3875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   322   54.3875   1600   1   3
 2
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   35   54.3875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   853   54.3875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   818   9.783   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1226   9.783   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1219   9.783   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   859   9.783   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   796   9.783   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1264   9.783   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   954   9.783   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1198   9.783   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   805   9.783   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   405   9.783   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   322   9.783   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   853   9.783   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   35   9.783   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1185   9.783   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1465   9.783   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   766   9.783   1   78
1   0   4   1000   0   'Y'   10   0   36
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2028 No-Build Microscale Input Files (Carbon Monoxide (CO))

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'Government Center Garage'   60   175   0   0   60   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Caus/Wash NE1'   6548.31   7035.9   6
'Caus/Wash NE2'   6581.41   6968.6   6
'Caus/Wash NE3'   6614.5   6901.3   6
'Caus/Wash NE4'   6669.75   6952.02   6
'Caus/Wash NE5'   6725   7002.74   6
'Caus/Wash SE1'   6753.58   6912.24   6
'Caus/Wash SE2'   6698.92   6862.05   6
'Caus/Wash SE3'   6643.09   6810.79   6
'Caus/Wash SE4'   6646.8   6736.4   6
'Caus/Wash SE5'   6649.95   6660.95   6
'Caus/Wash SW1'   6544.02   6561.02   6
'Caus/Wash SW2'   6540.9   6635.95   6
'Caus/Wash SW3'   6537.77   6710.89   6
'Caus/Wash SW4'   6476.83   6667.16   6
'Caus/Wash SW5'   6415.9   6623.44   6
'Caus/Wash NW1'   6407.38   6737.95   6
'Caus/Wash NW2'   6468.31   6781.67   6
'Caus/Wash NW3'   6529.25   6825.39   6
'Caus/Wash NW4'   6496.16   6892.69   6
'Caus/Wash NW5'   6463.06   6960   6
'Tha/Val NE1'   6667.28   6395.45   6
'Tha/Val NE2'   6668.3   6320.45   6
'Tha/Val NE3'   6669.31   6245.46   6
'Tha/Val NE4'   6744.31   6245.46   6
'Tha/Val NE5'   6819.25   6249.58   6
'Tha/Val SE1'   6822.27   6191.64   6
'Tha/Val SE2'   6747.3   6189.58   6
'Tha/Val SE3'   6672.33   6187.52   6
'Tha/Val SE4'   6671.6   6112.53   6
'Tha/Val SE5'   6670.88   6037.53   6
'Tha/Val SW1'   6560.17   5964.68   6
'Tha/Val SW2'   6560.89   6039.67   6
'Tha/Val SW3'   6561.62   6114.67   6
'Tha/Val SW4'   6502.18   6068.93   6
'Tha/Val SW5'   6442.74   6023.18   6
'Tha/Val NW1'   6440.95   6115.18   6
'Tha/Val NW2'   6500.39   6160.92   6
'Tha/Val NW3'   6559.82   6206.67   6
'Tha/Val NW4'   6558.81   6281.66   6
'Tha/Val NW5'   6557.8   6356.65   6
'No Build'   48   1   0   'C'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   44.9875   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   531   44.9875   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   44.9875   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   44.9875   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   44.9875   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   194   44.9875   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   44.9875   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   44.9875   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2353   44.9875   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
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150   119   3   321   44.9875   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   44.9875   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
 1
150   120   3   741   44.9875   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   44.9875   1600   1   3
 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1678   44.9875   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   44.9875   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   737   44.9875   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1628   44.9875   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   44.9875   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1986   44.9875   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   515   44.9875   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   403   44.9875   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   647   44.9875   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   997   44.9875   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   332   44.9875   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   44.9875   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1396   8.334   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1568   8.334   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   899   8.334   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   8.334   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3419   8.334   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   8.334   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2371   8.334   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   8.334   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2397   8.334   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   8.334   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2837   8.334   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   8.334   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2324   8.334   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   8.334   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   515   8.334   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   8.334   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   403   8.334   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   702   8.334   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   8.334   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1343   8.334   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1063   8.334   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1529   8.334   1   98
 1
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'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   8.334   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   50   0.3048   1   0
'Bev/Was N1'   6561.96   6150.17   6
'Bev/Was N2'   6561.23   6075.17   6
'Bev/Was N3'   6560.51   6000.18   6
'Bev/Was N4'   6515.8   6060.39   6
'Bev/Was N5'   6471.09   6120.61   6
'Bev/Was SE1'   6670.99   6049.68   6
'Bev/Was SE2'   6670.19   5966.32   6
'Bev/Was SE3'   6624   5907.23   6
'Bev/Was SE4'   6626.07   5832.26   6
'Bev/Was SE5'   6628.13   5757.29   6
'Bev/Was SW1'   6541.84   5766.87   6
'Bev/Was SW2'   6540.09   5841.85   6
'Bev/Was SW3'   6537.71   5916.82   6
'Bev/Was SW4'   6493   5977.03   6
'Bev/Was SW5'   6448.29   6037.25   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Wash/Cong NE1'   6910.24   4571.18   6
'Wash/Cong NE2'   6925.8   4497.81   6
'Wash/Cong NE3'   6941.37   4424.45   6
'Wash/Cong NE4'   7012.01   4449.65   6
'Wash/Cong NE5'   7082.65   4474.85   6
'Wash/Cong SE1'   7095.42   4388.1   6
'Wash/Cong SE2'   7024.78   4362.9   6
'Wash/Cong SE3'   6954.14   4337.69   6
'Wash/Cong SE4'   6968.42   4264.06   6
'Wash/Cong SE5'   6982.69   4190.43   6
'Wash/Cong SW1'   6867.47   4164.74   6
'Wash/Cong SW2'   6853.27   4238.01   6
'Wash/Cong SW3'   6838.93   4312   6
'Wash/Cong SW4'   6765.63   4296.1   6
'Wash/Cong SW5'   6692.34   4280.2   6
'Wash/Cong NW1'   6682.41   4353.77   6
'Wash/Cong NW2'   6755.7   4369.67   6
'Wash/Cong NW3'   6828.9   4386.02   6
'Wash/Cong NW4'   6813.33   4459.38   6
'Wash/Cong NW5'   6797.76   4532.75   6
'No Build'   48   1   0   'C'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   44.9875   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   531   44.9875   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   44.9875   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   44.9875   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   44.9875   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   194   44.9875   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   44.9875   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   44.9875   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2353   44.9875   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
150   119   3   321   44.9875   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   44.9875   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   741   44.9875   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   44.9875   1600   1   3
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 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1678   44.9875   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   44.9875   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   737   44.9875   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1628   44.9875   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   44.9875   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1986   44.9875   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   515   44.9875   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   403   44.9875   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   647   44.9875   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   997   44.9875   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   332   44.9875   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   44.9875   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1396   8.334   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1568   8.334   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   899   8.334   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   8.334   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3419   8.334   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   8.334   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2371   8.334   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   8.334   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2397   8.334   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   8.334   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2837   8.334   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   8.334   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2324   8.334   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   8.334   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   515   8.334   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   8.334   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   403   8.334   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   702   8.334   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   8.334   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1343   8.334   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1063   8.334   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1529   8.334   1   98
 1
'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   8.334   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   35   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'No Build'   21   1   0   'C'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   79   3   304   44.9875   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   79   3   646   44.9875   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   71   3   412   44.9875   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   79   3   325   44.9875   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   93   3   70   44.9875   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   93   3   289   44.9875   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   439   44.9875   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   320   44.9875   1600   1   3
 2
'Char/93 SB_LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   62   3   1829   44.9875   1600   1   3
 2
'Char/93 WB_LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   60   3   321   44.9875   1600   1   3
 2
'Char/93 EB_TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   60   3   983   44.9875   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1623   8.334   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1414   8.334   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   1179   8.334   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1387   8.334   1   78
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2078   8.334   1   66
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   321   8.334   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   1059   8.334   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   983   8.334   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   488   8.334   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   414   8.334   1   42
 1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028NB'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   476   44.9875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   703   44.9875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   116   44.9875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   709   44.9875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   217   44.9875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   339   44.9875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   457   44.9875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   294   44.9875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   289   44.9875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   354   44.9875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   901   44.9875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   104   44.9875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   524   44.9875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   924   44.9875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   73   3   529   44.9875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   455   44.9875   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   26   44.9875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   373   44.9875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   877   8.334   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1122   8.334   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1326   8.334   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   939   8.334   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   849   8.334   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1614   8.334   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   950   8.334   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1709   8.334   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   318   8.334   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   536   8.334   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   455   8.334   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   373   8.334   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   26   8.334   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1555   8.334   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1648   8.334   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   529   8.334   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'   6492.55   5309.91   6
'Sud/Merr NE2'   6554.76   5268.01   6
'Sud/Merr NE3'   6616.16   5224.93   6
'Sud/Merr NE4'   6604.72   5255.31   6
'Sud/Merr NE5'   6753.29   5285.7   6
'Sud/Merr SE1'   6792.88   5222.3   6
'Sud/Merr SE2'   6724.31   5191.92   6
'Sud/Merr SE3'   6655.74   5161.53   6
'Sud/Merr SE4'   6695.46   5097.91   6
'Sud/Merr SE5'   6735.19   5034.29   6
'Sud/Merr SW1'   6638.58   4981.33   6
'Sud/Merr SW2'   6598.85   5044.95   6
'Sud/Merr SW3'   6559.13   5108.56   6
'Sud/Merr SW4'   6493.36   5072.52   6
'Sud/Merr SW5'   6427.59   5036.47   6
'Sud/Merr NW1'   6347.76   5104.47   6
'Sud/Merr NW2'   6413.53   5140.52   6
'Sud/Merr NW3'   6479.3   5176.56   6
'Sud/Merr NW4'   6417.09   5218.46   6
'Sud/Merr NW5'   6354.88   5260.35   6
'Sud/Sur NE1'   6755.94   5445.69   6
'Sud/Sur NE2'   6800.97   5385.71   6
'Sud/Sur NE3'   6845.99   5325.73   6
'Sud/Sur NE4'   6908.75   5366.8   6
'Sud/Sur NE5'   6971.5   5407.88   6
'Sud/Sur SE1'   7002.41   5368.35   6
'Sud/Sur SE2'   6939.66   5327.28   6
'Sud/Sur SE3'   6876.91   5286.2   6
'Sud/Sur SE4'   6931.69   5234.97   6
'Sud/Sur SE5'   6986.46   5183.75   6
'Sud/Sur SW1'   6932.3   5133.08   6
'Sud/Sur SE2'   6877.52   5184.31   6
'Sud/Sur SE3'   6822.74   5235.54   6
'Sud/Sur SE4'   6754.17   5205.15   6
'Sud/Sur SE5'   6685.61   5174.76   6
'Sud/Sur NW1'   6645.53   5237.94   6
'Sud/Sur NW2'   6714.1   5268.33   6
'Sud/Sur NW3'   6782.66   5298.72   6
'Sud/Sur NW4'   6709.54   5315.38   6
'Sud/Sur NW5'   6636.41   5332.03   6
'Sud/Sur N1'   6642.36   5493.71   6
'Sud/Sur N2'   6687.39   5433.73   6
'Sud/Sur N3'   6732.41   5373.75   6
'Sud/Sur N4'   6659.29   5390.41   6
'Sud/Sur N5'   6586.16   5407.07   6
'2028NB'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   476   44.9875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   703   44.9875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   116   44.9875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   709   44.9875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   217   44.9875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   339   44.9875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   457   44.9875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   294   44.9875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   289   44.9875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   354   44.9875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   901   44.9875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   104   44.9875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   524   44.9875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   924   44.9875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
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100   73   3   529   44.9875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   455   44.9875   1600   1   3
 2
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   26   44.9875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   373   44.9875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   877   8.334   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1122   8.334   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1326   8.334   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   939   8.334   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   849   8.334   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1614   8.334   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   950   8.334   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1709   8.334   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   318   8.334   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   536   8.334   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   455   8.334   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   373   8.334   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   26   8.334   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1555   8.334   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1648   8.334   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   529   8.334   1   78
1   0   4   1000   0   'Y'   10   0   36
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```
'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028NB'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   589   44.9875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   481   44.9875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   257   44.9875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   520   44.9875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   468   44.9875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   229   44.9875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   254   44.9875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   44.9875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   44.9875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   536   44.9875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   809   44.9875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   106   44.9875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   435   44.9875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   954   44.9875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   72   3   837   44.9875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   44.9875   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   44.9875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   928   44.9875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   921   8.334   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1336   8.334   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1354   8.334   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   940   8.334   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   863   8.334   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1593   8.334   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1023   8.334   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1636   8.334   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   901   8.334   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   488   8.334   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   8.334   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   928   8.334   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   8.334   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1317   8.334   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1611   8.334   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   837   8.334   1   78
1   0   4   1000   0   'Y'   10   0   36
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```
'Government Center Garage'   60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'   6492.55   5309.91   6
'Sud/Merr NE2'   6554.76   5268.01   6
'Sud/Merr NE3'   6616.16   5224.93   6
'Sud/Merr NE4'   6604.72   5255.31   6
'Sud/Merr NE5'   6753.29   5285.7   6
'Sud/Merr SE1'   6792.88   5222.3   6
'Sud/Merr SE2'   6724.31   5191.92   6
'Sud/Merr SE3'   6655.74   5161.53   6
'Sud/Merr SE4'   6695.46   5097.91   6
'Sud/Merr SE5'   6735.19   5034.29   6
'Sud/Merr SW1'   6638.58   4981.33   6
'Sud/Merr SW2'   6598.85   5044.95   6
'Sud/Merr SW3'   6559.13   5108.56   6
'Sud/Merr SW4'   6493.36   5072.52   6
'Sud/Merr SW5'   6427.59   5036.47   6
'Sud/Merr NW1'   6347.76   5104.47   6
'Sud/Merr NW2'   6413.53   5140.52   6
'Sud/Merr NW3'   6479.3   5176.56   6
'Sud/Merr NW4'   6417.09   5218.46   6
'Sud/Merr NW5'   6354.88   5260.35   6
'Sud/Sur NE1'   6755.94   5445.69   6
'Sud/Sur NE2'   6800.97   5385.71   6
'Sud/Sur NE3'   6845.99   5325.73   6
'Sud/Sur NE4'   6908.75   5366.8   6
'Sud/Sur NE5'   6971.5   5407.88   6
'Sud/Sur SE1'   7002.41   5368.35   6
'Sud/Sur SE2'   6939.66   5327.28   6
'Sud/Sur SE3'   6876.91   5286.2   6
'Sud/Sur SE4'   6931.69   5234.97   6
'Sud/Sur SE5'   6986.46   5183.75   6
'Sud/Sur SW1'   6932.3   5133.08   6
'Sud/Sur SE2'   6877.52   5184.31   6
'Sud/Sur SE3'   6822.74   5235.54   6
'Sud/Sur SE4'   6754.17   5205.15   6
'Sud/Sur SE5'   6685.61   5174.76   6
'Sud/Sur NW1'   6645.53   5237.94   6
'Sud/Sur NW2'   6714.1   5268.33   6
'Sud/Sur NW3'   6782.66   5298.72   6
'Sud/Sur NW4'   6709.54   5315.38   6
'Sud/Sur NW5'   6636.41   5332.03   6
'Sud/Sur N1'   6642.36   5493.71   6
'Sud/Sur N2'   6687.39   5433.73   6
'Sud/Sur N3'   6732.41   5373.75   6
'Sud/Sur N4'   6659.29   5390.41   6
'Sud/Sur N5'   6586.16   5407.07   6
'2028NB'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   589   44.9875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   481   44.9875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   257   44.9875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   520   44.9875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   468   44.9875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   229   44.9875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   254   44.9875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   44.9875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   44.9875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   536   44.9875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   809   44.9875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   106   44.9875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   435   44.9875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   954   44.9875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
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100   72   3   837   44.9875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   44.9875   1600   1   3
 2
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   44.9875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   928   44.9875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   921   8.334   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1336   8.334   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1354   8.334   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   940   8.334   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   863   8.334   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1593   8.334   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1023   8.334   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1636   8.334   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   901   8.334   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   488   8.334   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   8.334   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   928   8.334   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   8.334   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1317   8.334   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1611   8.334   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   837   8.334   1   78
1   0   4   1000   0   'Y'   10   0   36
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2028 Build
Microscale Input Files
(Carbon Monoxide (CO))

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'Government Center Garage'   60   175   0   0   60   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Caus/Wash NE1'   6548.31   7035.9   6
'Caus/Wash NE2'   6581.41   6968.6   6
'Caus/Wash NE3'   6614.5   6901.3   6
'Caus/Wash NE4'   6669.75   6952.02   6
'Caus/Wash NE5'   6725   7002.74   6
'Caus/Wash SE1'   6753.58   6912.24   6
'Caus/Wash SE2'   6698.92   6862.05   6
'Caus/Wash SE3'   6643.09   6810.79   6
'Caus/Wash SE4'   6646.8   6736.4   6
'Caus/Wash SE5'   6649.95   6660.95   6
'Caus/Wash SW1'   6544.02   6561.02   6
'Caus/Wash SW2'   6540.9   6635.95   6
'Caus/Wash SW3'   6537.77   6710.89   6
'Caus/Wash SW4'   6476.83   6667.16   6
'Caus/Wash SW5'   6415.9   6623.44   6
'Caus/Wash NW1'   6407.38   6737.95   6
'Caus/Wash NW2'   6468.31   6781.67   6
'Caus/Wash NW3'   6529.25   6825.39   6
'Caus/Wash NW4'   6496.16   6892.69   6
'Caus/Wash NW5'   6463.06   6960   6
'Tha/Val NE1'   6667.28   6395.45   6
'Tha/Val NE2'   6668.3   6320.45   6
'Tha/Val NE3'   6669.31   6245.46   6
'Tha/Val NE4'   6744.31   6245.46   6
'Tha/Val NE5'   6819.25   6249.58   6
'Tha/Val SE1'   6822.27   6191.64   6
'Tha/Val SE2'   6747.3   6189.58   6
'Tha/Val SE3'   6672.33   6187.52   6
'Tha/Val SE4'   6671.6   6112.53   6
'Tha/Val SE5'   6670.88   6037.53   6
'Tha/Val SW1'   6560.17   5964.68   6
'Tha/Val SW2'   6560.89   6039.67   6
'Tha/Val SW3'   6561.62   6114.67   6
'Tha/Val SW4'   6502.18   6068.93   6
'Tha/Val SW5'   6442.74   6023.18   6
'Tha/Val NW1'   6440.95   6115.18   6
'Tha/Val NW2'   6500.39   6160.92   6
'Tha/Val NW3'   6559.82   6206.67   6
'Tha/Val NW4'   6558.81   6281.66   6
'Tha/Val NW5'   6557.8   6356.65   6
'Build'   48   1   0   'C'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   44.9875   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   585   44.9875   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   44.9875   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   44.9875   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   44.9875   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   208   44.9875   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   44.9875   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   44.9875   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2380   44.9875   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
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150   119   3   321   44.9875   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   44.9875   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   748   44.9875   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   44.9875   1600   1   3
 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1705   44.9875   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   44.9875   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   744   44.9875   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1655   44.9875   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   44.9875   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   2013   44.9875   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   542   44.9875   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   459   44.9875   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   636   44.9875   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   1267   44.9875   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   345   44.9875   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   44.9875   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1464   8.334   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1588   8.334   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   967   8.334   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   8.334   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3453   8.334   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   8.334   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2405   8.334   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   8.334   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2431   8.334   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   8.334   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2871   8.334   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   8.334   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2351   8.334   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   8.334   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   542   8.334   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   8.334   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   459   8.334   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   729   8.334   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   8.334   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1629   8.334   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1333   8.334   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1545   8.334   1   98
 1
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'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   8.334   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   50   0.3048   1   0
'Bev/Was N1'   6561.96   6150.17   6
'Bev/Was N2'   6561.23   6075.17   6
'Bev/Was N3'   6560.51   6000.18   6
'Bev/Was N4'   6515.8   6060.39   6
'Bev/Was N5'   6471.09   6120.61   6
'Bev/Was SE1'   6670.99   6049.68   6
'Bev/Was SE2'   6670.19   5966.32   6
'Bev/Was SE3'   6624   5907.23   6
'Bev/Was SE4'   6626.07   5832.26   6
'Bev/Was SE5'   6628.13   5757.29   6
'Bev/Was SW1'   6541.84   5766.87   6
'Bev/Was SW2'   6540.09   5841.85   6
'Bev/Was SW3'   6537.71   5916.82   6
'Bev/Was SW4'   6493   5977.03   6
'Bev/Was SW5'   6448.29   6037.25   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Wash/Cong NE1'   6910.24   4571.18   6
'Wash/Cong NE2'   6925.8   4497.81   6
'Wash/Cong NE3'   6941.37   4424.45   6
'Wash/Cong NE4'   7012.01   4449.65   6
'Wash/Cong NE5'   7082.65   4474.85   6
'Wash/Cong SE1'   7095.42   4388.1   6
'Wash/Cong SE2'   7024.78   4362.9   6
'Wash/Cong SE3'   6954.14   4337.69   6
'Wash/Cong SE4'   6968.42   4264.06   6
'Wash/Cong SE5'   6982.69   4190.43   6
'Wash/Cong SW1'   6867.47   4164.74   6
'Wash/Cong SW2'   6853.27   4238.01   6
'Wash/Cong SW3'   6838.93   4312   6
'Wash/Cong SW4'   6765.63   4296.1   6
'Wash/Cong SW5'   6692.34   4280.2   6
'Wash/Cong NW1'   6682.41   4353.77   6
'Wash/Cong NW2'   6755.7   4369.67   6
'Wash/Cong NW3'   6828.9   4386.02   6
'Wash/Cong NW4'   6813.33   4459.38   6
'Wash/Cong NW5'   6797.76   4532.75   6
'Build'   48   1   0   'C'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   44.9875   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   585   44.9875   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   44.9875   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   44.9875   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   44.9875   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   208   44.9875   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   44.9875   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   44.9875   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2380   44.9875   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
150   119   3   321   44.9875   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   44.9875   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   748   44.9875   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   44.9875   1600   1   3
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 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1705   44.9875   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   44.9875   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   744   44.9875   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1655   44.9875   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   44.9875   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   2013   44.9875   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   542   44.9875   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   459   44.9875   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   636   44.9875   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   1267   44.9875   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   345   44.9875   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   44.9875   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1464   8.334   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1588   8.334   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   967   8.334   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   8.334   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3453   8.334   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   8.334   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2405   8.334   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   8.334   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2431   8.334   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   8.334   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2871   8.334   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   8.334   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2351   8.334   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   8.334   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   542   8.334   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   8.334   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   459   8.334   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   729   8.334   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   8.334   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1629   8.334   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1333   8.334   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1545   8.334   1   98
 1
'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   8.334   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   35   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Build'   21   1   0   'C'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   79   3   304   44.9875   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   79   3   672   44.9875   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   71   3   412   44.9875   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   79   3   325   44.9875   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   93   3   70   44.9875   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   93   3   331   44.9875   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   439   44.9875   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   320   44.9875   1600   1   3
 2
'Char/93 SB_LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   62   3   1842   44.9875   1600   1   3
 2
'Char/93 WB_LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   60   3   334   44.9875   1600   1   3
 2
'Char/93 EB_TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   60   3   1159   44.9875   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1691   8.334   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1414   8.334   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   1247   8.334   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1387   8.334   1   78
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2091   8.334   1   66
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   334   8.334   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   1059   8.334   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   1159   8.334   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   499   8.334   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   414   8.334   1   42
 1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028BD'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   530   44.9875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   74   3   757   44.9875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   44   3   116   44.9875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   70   3   1002   44.9875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   80   3   281   44.9875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   340   44.9875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   472   44.9875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   294   44.9875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   289   44.9875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   367   44.9875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   937   44.9875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   89   3   104   44.9875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   41   3   524   44.9875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   52   3   1232   44.9875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   76   3   579   44.9875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   455   44.9875   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   26   44.9875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   420   44.9875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   945   8.334   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1232   8.334   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1619   8.334   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   1565   8.334   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   1016   8.334   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1651   8.334   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   964   8.334   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1759   8.334   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   360   8.334   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   541   8.334   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   455   8.334   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   420   8.334   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   26   8.334   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1848   8.334   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1944   8.334   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   579   8.334   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028BD'   34   1   0   'C'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   615   44.9875   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   79   3   517   44.9875   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   52   3   257   44.9875   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   73   3   660   44.9875   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   72   3   679   44.9875   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   233   44.9875   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   301   44.9875   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   44.9875   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   44.9875   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   543   44.9875   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   827   44.9875   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   88   3   106   44.9875   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   52   3   435   44.9875   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   64   3   1094   44.9875   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   65   3   992   44.9875   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   44.9875   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   44.9875   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   1075   44.9875   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   989   8.334   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1538   8.334   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1494   8.334   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   1409   8.334   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   921   8.334   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1615   8.334   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1034   8.334   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1697   8.334   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   1032   8.334   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   504   8.334   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   8.334   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   1075   8.334   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   8.334   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1457   8.334   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1759   8.334   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   992   8.334   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55   5309.91   6
'Sud/Merr NE2'    6554.76   5268.01   6
'Sud/Merr NE3'    6616.16   5224.93   6
'Sud/Merr NE4'    6604.72   5255.31   6
'Sud/Merr NE5'    6753.29   5285.7    6
'Sud/Merr SE1'    6792.88   5222.3    6
'Sud/Merr SE2'    6724.31   5191.92   6
'Sud/Merr SE3'    6655.74   5161.53   6
'Sud/Merr SE4'    6695.46   5097.91   6
'Sud/Merr SE5'    6735.19   5034.29   6
'Sud/Merr SW1'    6638.58   4981.33   6
'Sud/Merr SW2'    6598.85   5044.95   6
'Sud/Merr SW3'    6559.13   5108.56   6
'Sud/Merr SW4'    6493.36   5072.52   6
'Sud/Merr SW5'    6427.59   5036.47   6
'Sud/Merr NW1'    6347.76   5104.47   6
'Sud/Merr NW2'    6413.53   5140.52   6
'Sud/Merr NW3'    6479.3    5176.56   6
'Sud/Merr NW4'    6417.09   5218.46   6
'Sud/Merr NW5'    6354.88   5260.35   6
'Sud/Sur NE1'    6755.94    5445.69    6
'Sud/Sur NE2'    6800.97    5385.71    6
'Sud/Sur NE3'    6845.99    5325.73    6
'Sud/Sur NE4'    6908.75    5366.8     6
'Sud/Sur NE5'    6971.5     5407.88    6
'Sud/Sur SE1'    7002.41    5368.35    6
'Sud/Sur SE2'    6939.66    5327.28    6
'Sud/Sur SE3'    6876.91    5286.2     6
'Sud/Sur SE4'    6931.69    5234.97    6
'Sud/Sur SE5'    6986.46    5183.75    6
'Sud/Sur SW1'    6932.3     5133.08    6
'Sud/Sur SE2'    6877.52    5184.31    6
'Sud/Sur SE3'    6822.74    5235.54    6
'Sud/Sur SE4'    6754.17    5205.15    6
'Sud/Sur SE5'    6685.61    5174.76    6
'Sud/Sur NW1'    6645.53    5237.94    6
'Sud/Sur NW2'    6714.1     5268.33    6
'Sud/Sur NW3'    6782.66    5298.72    6
'Sud/Sur NW4'    6709.54    5315.38    6
'Sud/Sur NW5'    6636.41    5332.03    6
'Sud/Sur N1'    6642.36    5493.71    6
'Sud/Sur N2'    6687.39    5433.73    6
'Sud/Sur N3'    6732.41    5373.75    6
'Sud/Sur N4'    6659.29    5390.41    6
'Sud/Sur N5'    6586.16    5407.07    6
'2028BD'    34   1   0   'C'
 2
'Char/Merr SB'    'AG'    6111.61    5425.13    5935.42    5488.8    1   30   3
100   76   3   530   44.9875   1600   1   3
 2
'Char/Merr WB'    'AG'    6250.42    5435.24    6385.37    5541.98    1   30   3
100   74   3   757   44.9875   1600   1   3
 2
'Char/Merr NB R'    'AG'    6291.66    5369.7    6396.62    5298.54    1   10   1
100   44   3   116   44.9875   1600   1   3
 2
'Char/Merr NB LTT'    'AG'    6280.41    5347.23    6376    5279.81    1   20   2
100   70   3   1002   44.9875   1600   1   3
 2
'Char/Merr EB'    'AG'    6104.22    5362.21    5928.03    5296.67    1   20   2
100   80   3   281   44.9875   1600   1   3
 2
'Char/Cam SB L'    'AG'    5384.06    4834.19    5405.87    4921.31    1   10   1
90   58   3   340   44.9875   1600   1   3
 2
'Char/Cam SB TR'    'AG'    5360.81    4833.46    5388.43    4922.76    1   20   2
90   71   3   472   44.9875   1600   1   3
 2
'Char/Cam WB LTTR'    'AG'    5410.95    4793.53    5564.29    4757.95    1   20   2
90   54   3   294   44.9875   1600   1   3
 2
'Char/Cam NB L'    'AG'    5362.99    4722.37    5360.81    4625.08    1   10   1
90   58   3   289   44.9875   1600   1   3
 2
'Char/Cam NB TR'    'AG'    5383.34    4723.83    5384.79    4624.36    1   20   2
90   71   3   367   44.9875   1600   1   3
 2
'Char/Cam EB TTTR'    'AG'    5302.67    4739.8    5163.87    4741.25    1   30   3
90   54   3   937   44.9875   1600   1   3
 2
'Sud/Merr SB L'    'AG'    6532.74    5210.31    6469.76    5255.15    1   10   1
100   89   3   104   44.9875   1600   1   3
 2
'Sud/Merr SB TTT'    'AG'    6518.26    5190.78    6450.94    5229.84    1   30   3
100   41   3   524   44.9875   1600   1   3
 2
'Sud/Merr NB TTTR'    'AG'    6621.05    5161.13    6684.76    5049.03    1   30   3
100   52   3   1232   44.9875   1600   1   3
 2
'Sud/Merr EB LTTR'    'AG'    6523.33    5145.94    6435.74    5093.15    1   40   4
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100   76   3   579   44.9875   1600   1   3
 2
'Sud/Sur SB LTT'    'AG'    6777.46    5369.67    6709.4    5455.47    1   20   2
100   53   3   455   44.9875   1600   1   3
 2
'Sud/Sur SEB'    'AG'    6757.21    5330.01    6705.35    5342.96    1   10   1
100   70   3   26   44.9875   1600   1   3
 2
'Sud/Sur EB TTR'    'AG'    6794.47    5259.59    6672.95    5211.83    1   30   3
100   77   3   420   44.9875   1600   1   3
 1
'Char/Merr N'    'AG'    6202.34    5403.71    5845.34    5537.04    945    8.334    1   84
 1
'Char/Merr E'    'AG'    6201.86    5389.77    6552.37    5635.08    1232    8.334    1   90
 1
'Char/Merr S'    'AG'    6214.99    5412.24    6411.79    5262.43    1619    8.334    1   98
 1
'Char/Merr W'    'AG'    6198.12    5397.26    5806.38    5264.31    1565    8.334    1   98
 1
'Char/Camb N'    'AG'    5352.47    4779.69    5466.46    5028.93    1016    8.334    1   78
 1
'Char/Camb E'    'AG'    5334.74    4787.8    5780.86    4671.3    1651    8.334    1   102
 1
'Char/Camb S'    'AG'    5359.22    4760.44    5362.39    4406.78    964    8.334    1   78
 1
'Char/Camb W'    'AG'    5364.5    4766.77    5009.45    4767.83    1759    8.334    1   90
 1
'Sur/Sud E'    'AG'    6831.79    5286.55    6967.42    5375.33    360    8.334    1   30
 1
'Sur/Sud S'    'AG'    6823.37    5285.61    7028.22    5094.04    541    8.334    1   54
 1
'Sur/Sud N'    'AG'    6816.26    5313.7    6641.09    5547.04    455    8.334    1   42
 1
'Sur/Sud W'    'AG'    6584.37    5170.37    6806.25    5268.7    420    8.334    1   54
 1
'Sur/Sud NW'    'AG'    6797.91    5327.04    6702.82    5348.7    26    8.334    1   42
 1
'Merr/Sud N'    'AG'    6569.36    5187.04    6420.88    5287.04    1848    8.334    1   98
 1
'Merr/Sud S'    'AG'    6567.69    5198.7    6786.23    4848.7    1944    8.334    1   90
 1
'Merr/Sud W'    'AG'    6576.03    5173.7    6284.09    5013.7    579    8.334    1   78
1   0   4   1000   0   'Y'   10   0   36
```

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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55   5309.91   6
'Sud/Merr NE2'    6554.76   5268.01   6
'Sud/Merr NE3'    6616.16   5224.93   6
'Sud/Merr NE4'    6604.72   5255.31   6
'Sud/Merr NE5'    6753.29   5285.7    6
'Sud/Merr SE1'    6792.88   5222.3    6
'Sud/Merr SE2'    6724.31   5191.92   6
'Sud/Merr SE3'    6655.74   5161.53   6
'Sud/Merr SE4'    6695.46   5097.91   6
'Sud/Merr SE5'    6735.19   5034.29   6
'Sud/Merr SW1'    6638.58   4981.33   6
'Sud/Merr SW2'    6598.85   5044.95   6
'Sud/Merr SW3'    6559.13   5108.56   6
'Sud/Merr SW4'    6493.36   5072.52   6
'Sud/Merr SW5'    6427.59   5036.47   6
'Sud/Merr NW1'    6347.76   5104.47   6
'Sud/Merr NW2'    6413.53   5140.52   6
'Sud/Merr NW3'    6479.3    5176.56   6
'Sud/Merr NW4'    6417.09   5218.46   6
'Sud/Merr NW5'    6354.88   5260.35   6
'Sud/Sur NE1'    6755.94    5445.69    6
'Sud/Sur NE2'    6800.97    5385.71    6
'Sud/Sur NE3'    6845.99    5325.73    6
'Sud/Sur NE4'    6908.75    5366.8     6
'Sud/Sur NE5'    6971.5     5407.88    6
'Sud/Sur SE1'    7002.41    5368.35    6
'Sud/Sur SE2'    6939.66    5327.28    6
'Sud/Sur SE3'    6876.91    5286.2     6
'Sud/Sur SE4'    6931.69    5234.97    6
'Sud/Sur SE5'    6986.46    5183.75    6
'Sud/Sur SW1'    6932.3     5133.08    6
'Sud/Sur SE2'    6877.52    5184.31    6
'Sud/Sur SE3'    6822.74    5235.54    6
'Sud/Sur SE4'    6754.17    5205.15    6
'Sud/Sur SE5'    6685.61    5174.76    6
'Sud/Sur NW1'    6645.53    5237.94    6
'Sud/Sur NW2'    6714.1     5268.33    6
'Sud/Sur NW3'    6782.66    5298.72    6
'Sud/Sur NW4'    6709.54    5315.38    6
'Sud/Sur NW5'    6636.41    5332.03    6
'Sud/Sur N1'    6642.36    5493.71    6
'Sud/Sur N2'    6687.39    5433.73    6
'Sud/Sur N3'    6732.41    5373.75    6
'Sud/Sur N4'    6659.29    5390.41    6
'Sud/Sur N5'    6586.16    5407.07    6
'2028BD'    34   1   0   'C'
 2
'Char/Merr SB'    'AG'    6111.61    5425.13    5935.42    5488.8    1   30   3
100   76   3   615   44.9875   1600   1   3
 2
'Char/Merr WB'    'AG'    6250.42    5435.24    6385.37    5541.98    1   30   3
100   79   3   517   44.9875   1600   1   3
 2
'Char/Merr NB R'    'AG'    6291.66    5369.7    6396.62    5298.54    1   10   1
100   52   3   257   44.9875   1600   1   3
 2
'Char/Merr NB LTT'    'AG'    6280.41    5347.23    6376    5279.81    1   20   2
100   73   3   660   44.9875   1600   1   3
 2
'Char/Merr EB'    'AG'    6104.22    5362.21    5928.03    5296.67    1   20   2
100   72   3   679   44.9875   1600   1   3
 2
'Char/Cam SB L'    'AG'    5384.06    4834.19    5405.87    4921.31    1   10   1
100   60   3   233   44.9875   1600   1   3
 2
'Char/Cam SB TR'    'AG'    5360.81    4833.46    5388.43    4922.76    1   20   2
100   72   3   301   44.9875   1600   1   3
 2
'Char/Cam WB LTTR'    'AG'    5410.95    4793.53    5564.29    4757.95    1   20   2
100   62   3   435   44.9875   1600   1   3
 2
'Char/Cam NB L'    'AG'    5362.99    4722.37    5360.81    4625.08    1   10   1
100   60   3   299   44.9875   1600   1   3
 2
'Char/Cam NB TR'    'AG'    5383.34    4723.83    5384.79    4624.36    1   20   2
100   72   3   543   44.9875   1600   1   3
 2
'Char/Cam EB TTTR'    'AG'    5302.67    4739.8    5163.87    4741.25    1   30   3
100   62   3   827   44.9875   1600   1   3
 2
'Sud/Merr SB L'    'AG'    6532.74    5210.31    6469.76    5255.15    1   10   1
100   88   3   106   44.9875   1600   1   3
 2
'Sud/Merr SB TTT'    'AG'    6518.26    5190.78    6450.94    5229.84    1   30   3
100   52   3   435   44.9875   1600   1   3
 2
'Sud/Merr NB TTTR'    'AG'    6621.05    5161.13    6684.76    5049.03    1   30   3
100   64   3   1094   44.9875   1600   1   3
 2
'Sud/Merr EB LTTR'    'AG'    6523.33    5145.94    6435.74    5093.15    1   40   4
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100   65   3   992   44.9875   1600   1   3
 2
'Sud/Sur SB LTT'    'AG'    6777.46    5369.67    6709.4    5455.47    1   20   2
100   70   3   424   44.9875   1600   1   3
 2
'Sud/Sur SEB'    'AG'    6757.21    5330.01    6705.35    5342.96    1   10   1
100   80   3   37   44.9875   1600   1   3
 2
'Sud/Sur EB TTR'    'AG'    6794.47    5259.59    6672.95    5211.83    1   30   3
100   50   3   1075   44.9875   1600   1   3
 1
'Char/Merr N'    'AG'    6202.34    5403.71    5845.34    5537.04    989    8.334    1   84
 1
'Char/Merr E'    'AG'    6201.86    5389.77    6552.37    5635.08    1538    8.334    1   90
 1
'Char/Merr S'    'AG'    6214.99    5412.24    6411.79    5262.43    1494    8.334    1   98
 1
'Char/Merr W'    'AG'    6198.12    5397.26    5806.38    5264.31    1409    8.334    1   98
 1
'Char/Camb N'    'AG'    5352.47    4779.69    5466.46    5028.93    921    8.334    1   78
 1
'Char/Camb E'    'AG'    5334.74    4787.8    5780.86    4671.3    1615    8.334    1   102
 1
'Char/Camb S'    'AG'    5359.22    4760.44    5362.39    4406.78    1034    8.334    1   78
 1
'Char/Camb W'    'AG'    5364.5    4766.77    5009.45    4767.83    1697    8.334    1   90
 1
'Sur/Sud E'    'AG'    6831.79    5286.55    6967.42    5375.33    1032    8.334    1   30
 1
'Sur/Sud S'    'AG'    6823.37    5285.61    7028.22    5094.04    504    8.334    1   54
 1
'Sur/Sud N'    'AG'    6816.26    5313.7    6641.09    5547.04    424    8.334    1   42
 1
'Sur/Sud W'    'AG'    6584.37    5170.37    6806.25    5268.7    1075    8.334    1   54
 1
'Sur/Sud NW'    'AG'    6797.91    5327.04    6702.82    5348.7    37    8.334    1   42
 1
'Merr/Sud N'    'AG'    6569.36    5187.04    6420.88    5287.04    1457    8.334    1   98
 1
'Merr/Sud S'    'AG'    6567.69    5198.7    6786.23    4848.7    1759    8.334    1   90
 1
'Merr/Sud W'    'AG'    6576.03    5173.7    6284.09    5013.7    992    8.334    1   78
1   0   4   1000   0   'Y'   10   0   36
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2013 Existing Microscale Input Files (Particulate Matter 10 (PM10))

```
'Government Center Garage'   60   175   0   0   60   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Caus/Wash NE1'   6548.31   7035.9   6
'Caus/Wash NE2'   6581.41   6968.6   6
'Caus/Wash NE3'   6614.5   6901.3   6
'Caus/Wash NE4'   6669.75   6952.02   6
'Caus/Wash NE5'   6725   7002.74   6
'Caus/Wash SE1'   6753.58   6912.24   6
'Caus/Wash SE2'   6698.92   6862.05   6
'Caus/Wash SE3'   6643.09   6810.79   6
'Caus/Wash SE4'   6646.8   6736.4   6
'Caus/Wash SE5'   6649.95   6660.95   6
'Caus/Wash SW1'   6544.02   6561.02   6
'Caus/Wash SW2'   6540.9   6635.95   6
'Caus/Wash SW3'   6537.77   6710.89   6
'Caus/Wash SW4'   6476.83   6667.16   6
'Caus/Wash SW5'   6415.9   6623.44   6
'Caus/Wash NW1'   6407.38   6737.95   6
'Caus/Wash NW2'   6468.31   6781.67   6
'Caus/Wash NW3'   6529.25   6825.39   6
'Caus/Wash NW4'   6496.16   6892.69   6
'Caus/Wash NW5'   6463.06   6960   6
'Tha/Val NE1'   6667.28   6395.45   6
'Tha/Val NE2'   6668.3   6320.45   6
'Tha/Val NE3'   6669.31   6245.46   6
'Tha/Val NE4'   6744.31   6245.46   6
'Tha/Val NE5'   6819.25   6249.58   6
'Tha/Val SE1'   6822.27   6191.64   6
'Tha/Val SE2'   6747.3   6189.58   6
'Tha/Val SE3'   6672.33   6187.52   6
'Tha/Val SE4'   6671.6   6112.53   6
'Tha/Val SE5'   6670.88   6037.53   6
'Tha/Val SW1'   6560.17   5964.68   6
'Tha/Val SW2'   6560.89   6039.67   6
'Tha/Val SW3'   6561.62   6114.67   6
'Tha/Val SW4'   6502.18   6068.93   6
'Tha/Val SW5'   6442.74   6023.18   6
'Tha/Val NW1'   6440.95   6115.18   6
'Tha/Val NW2'   6500.39   6160.92   6
'Tha/Val NW3'   6559.82   6206.67   6
'Tha/Val NW4'   6558.81   6281.66   6
'Tha/Val NW5'   6557.8   6356.65   6
'Existing'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
90   70   3   223   0.08375   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
90   66   3   481   0.08375   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
90   68   3   527   0.08375   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
90   48   3   265   0.08375   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
90   70   3   142   0.08375   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
90   66   3   166   0.08375   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
90   68   3   265   0.08375   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
90   48   3   208   0.08375   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   56   3   2210   0.08375   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
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150   125   3   296   0.08375   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   73   3   216   0.08375   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
 1
150   108   3   693   0.08375   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   119   3   388   0.08375   1600   1   3
 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
100   34   3   1575   0.08375   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
100   66   3   253   0.08375   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
100   34   3   743   0.08375   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1528   0.08375   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   269   0.08375   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1797   0.08375   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   80   0.08375   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   374   0.08375   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   75   3   598   0.08375   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   916   0.08375   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   306   0.08375   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   16   0.08375   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1120   0.0335   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1275   0.0335   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   817   0.0335   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1322   0.0335   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3211   0.0335   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1012   0.0335   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2221   0.0335   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1162   0.0335   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2247   0.0335   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   91   0.0335   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2524   0.0335   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   280   0.0335   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   1841   0.0335   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   269   0.0335   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   80   0.0335   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   811   0.0335   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   374   0.0335   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   650   0.0335   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   406   0.0335   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1226   0.0335   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   978   0.0335   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1420   0.0335   1   98
 1
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'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   44   0.0335   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   50   0.3048   1   0
'Bev/Was N1'   6561.96   6150.17   6
'Bev/Was N2'   6561.23   6075.17   6
'Bev/Was N3'   6560.51   6000.18   6
'Bev/Was N4'   6515.8   6060.39   6
'Bev/Was N5'   6471.09   6120.61   6
'Bev/Was SE1'   6670.99   6049.68   6
'Bev/Was SE2'   6670.19   5966.32   6
'Bev/Was SE3'   6624   5907.23   6
'Bev/Was SE4'   6626.07   5832.26   6
'Bev/Was SE5'   6628.13   5757.29   6
'Bev/Was SW1'   6541.84   5766.87   6
'Bev/Was SW2'   6540.09   5841.85   6
'Bev/Was SW3'   6537.71   5916.82   6
'Bev/Was SW4'   6493   5977.03   6
'Bev/Was SW5'   6448.29   6037.25   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Wash/Cong NE1'   6910.24   4571.18   6
'Wash/Cong NE2'   6925.8   4497.81   6
'Wash/Cong NE3'   6941.37   4424.45   6
'Wash/Cong NE4'   7012.01   4449.65   6
'Wash/Cong NE5'   7082.65   4474.85   6
'Wash/Cong SE1'   7095.42   4388.1   6
'Wash/Cong SE2'   7024.78   4362.9   6
'Wash/Cong SE3'   6954.14   4337.69   6
'Wash/Cong SE4'   6968.42   4264.06   6
'Wash/Cong SE5'   6982.69   4190.43   6
'Wash/Cong SW1'   6867.47   4164.74   6
'Wash/Cong SW2'   6853.27   4238.01   6
'Wash/Cong SW3'   6838.93   4312   6
'Wash/Cong SW4'   6765.63   4296.1   6
'Wash/Cong SW5'   6692.34   4280.2   6
'Wash/Cong NW1'   6682.41   4353.77   6
'Wash/Cong NW2'   6755.7   4369.67   6
'Wash/Cong NW3'   6828.9   4386.02   6
'Wash/Cong NW4'   6813.33   4459.38   6
'Wash/Cong NW5'   6797.76   4532.75   6
'Existing'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
90   70   3   223   0.08375   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
90   66   3   481   0.08375   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
90   68   3   527   0.08375   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
90   48   3   265   0.08375   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
90   70   3   142   0.08375   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
90   66   3   166   0.08375   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
90   68   3   265   0.08375   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
90   48   3   208   0.08375   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   56   3   2210   0.08375   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
150   125   3   296   0.08375   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   73   3   216   0.08375   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   108   3   693   0.08375   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   119   3   388   0.08375   1600   1   3
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 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
100   34   3   1575   0.08375   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
100   66   3   253   0.08375   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
100   34   3   743   0.08375   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1528   0.08375   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   269   0.08375   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1797   0.08375   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   80   0.08375   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   374   0.08375   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   75   3   598   0.08375   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   916   0.08375   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   306   0.08375   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   16   0.08375   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1120   0.0335   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1275   0.0335   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   817   0.0335   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1322   0.0335   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3211   0.0335   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1012   0.0335   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2221   0.0335   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1162   0.0335   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2247   0.0335   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   91   0.0335   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2524   0.0335   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   280   0.0335   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   1841   0.0335   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   269   0.0335   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   80   0.0335   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   811   0.0335   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   374   0.0335   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   650   0.0335   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   406   0.0335   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1226   0.0335   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   978   0.0335   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1420   0.0335   1   98
 1
'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   44   0.0335   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   35   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Existing'   21   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
100   79   3   208   0.08375   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
100   74   3   595   0.08375   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
100   71   3   332   0.08375   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
100   79   3   259   0.08375   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
100   79   3   66   0.08375   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
100   74   3   176   0.08375   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
100   71   3   371   0.08375   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
100   79   3   300   0.08375   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   62   3   1488   0.08375   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   60   3   298   0.08375   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   60   3   908   0.08375   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1289   0.0335   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1112   0.0335   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   999   0.0335   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1207   0.0335   1   78
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   1635   0.0335   1   66
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   298   0.0335   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   847   0.0335   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   908   0.0335   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   449   0.0335   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   314   0.0335   1   42
 1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2013EX'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   436   0.08375   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   650   0.08375   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   109   0.08375   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   637   0.08375   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   194   0.08375   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   318   0.08375   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   429   0.08375   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   265   0.08375   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   260   0.08375   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   330   0.08375   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   811   0.08375   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   95   0.08375   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   484   0.08375   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   854   0.08375   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   73   3   487   0.08375   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   405   0.08375   1600   1   3
 2
```



```
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   25   0.08375   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   338   0.08375   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   802   0.0335   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1038   0.0335   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1204   0.0335   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   870   0.0335   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   923   0.0335   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1472   0.0335   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   877   0.0335   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1546   0.0335   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   285   0.0335   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   483   0.0335   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   405   0.0335   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   338   0.0335   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   25   0.0335   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1421   0.0335   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1512   0.0335   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   487   0.0335   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2013EX'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   541   0.08375   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   449   0.08375   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   241   0.08375   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   452   0.08375   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   417   0.08375   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   214   0.08375   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   233   0.08375   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   391   0.08375   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   276   0.08375   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   503   0.08375   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   726   0.08375   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   98   0.08375   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   394   0.08375   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   863   0.08375   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   72   3   766   0.08375   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   322   0.08375   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   35   0.08375   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   853   0.08375   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   818   0.0335   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1226   0.0335   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1219   0.0335   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   859   0.0335   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   796   0.0335   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1264   0.0335   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   954   0.0335   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1198   0.0335   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   805   0.0335   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   405   0.0335   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   322   0.0335   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   853   0.0335   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   35   0.0335   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1185   0.0335   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1465   0.0335   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   766   0.0335   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'   6492.55   5309.91   6
'Sud/Merr NE2'   6554.76   5268.01   6
'Sud/Merr NE3'   6616.16   5224.93   6
'Sud/Merr NE4'   6604.72   5255.31   6
'Sud/Merr NE5'   6753.29   5285.7   6
'Sud/Merr SE1'   6792.88   5222.3   6
'Sud/Merr SE2'   6724.31   5191.92   6
'Sud/Merr SE3'   6655.74   5161.53   6
'Sud/Merr SE4'   6695.46   5097.91   6
'Sud/Merr SE5'   6735.19   5034.29   6
'Sud/Merr SW1'   6638.58   4981.33   6
'Sud/Merr SW2'   6598.85   5044.95   6
'Sud/Merr SW3'   6559.13   5108.56   6
'Sud/Merr SW4'   6493.36   5072.52   6
'Sud/Merr SW5'   6427.59   5036.47   6
'Sud/Merr NW1'   6347.76   5104.47   6
'Sud/Merr NW2'   6413.53   5140.52   6
'Sud/Merr NW3'   6479.3   5176.56   6
'Sud/Merr NW4'   6417.09   5218.46   6
'Sud/Merr NW5'   6354.88   5260.35   6
'Sud/Sur NE1'   6755.94   5445.69   6
'Sud/Sur NE2'   6800.97   5385.71   6
'Sud/Sur NE3'   6845.99   5325.73   6
'Sud/Sur NE4'   6908.75   5366.8   6
'Sud/Sur NE5'   6971.5   5407.88   6
'Sud/Sur SE1'   7002.41   5368.35   6
'Sud/Sur SE2'   6939.66   5327.28   6
'Sud/Sur SE3'   6876.91   5286.2   6
'Sud/Sur SE4'   6931.69   5234.97   6
'Sud/Sur SE5'   6986.46   5183.75   6
'Sud/Sur SW1'   6932.3   5133.08   6
'Sud/Sur SE2'   6877.52   5184.31   6
'Sud/Sur SE3'   6822.74   5235.54   6
'Sud/Sur SE4'   6754.17   5205.15   6
'Sud/Sur SE5'   6685.61   5174.76   6
'Sud/Sur NW1'   6645.53   5237.94   6
'Sud/Sur NW2'   6714.1   5268.33   6
'Sud/Sur NW3'   6782.66   5298.72   6
'Sud/Sur NW4'   6709.54   5315.38   6
'Sud/Sur NW5'   6636.41   5332.03   6
'Sud/Sur N1'   6642.36   5493.71   6
'Sud/Sur N2'   6687.39   5433.73   6
'Sud/Sur N3'   6732.41   5373.75   6
'Sud/Sur N4'   6659.29   5390.41   6
'Sud/Sur N5'   6586.16   5407.07   6
'2013EX'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   436   0.08375   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   650   0.08375   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   109   0.08375   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   637   0.08375   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   194   0.08375   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   318   0.08375   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   429   0.08375   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   265   0.08375   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   260   0.08375   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   330   0.08375   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   811   0.08375   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   95   0.08375   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   484   0.08375   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   854   0.08375   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
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100   73   3   487   0.08375   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   405   0.08375   1600   1   3
 2
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   25   0.08375   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   338   0.08375   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   802   0.0335   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1038   0.0335   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1204   0.0335   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   870   0.0335   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   923   0.0335   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1472   0.0335   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   877   0.0335   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1546   0.0335   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   285   0.0335   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   483   0.0335   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   405   0.0335   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   338   0.0335   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   25   0.0335   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1421   0.0335   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1512   0.0335   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   487   0.0335   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'   6492.55   5309.91   6
'Sud/Merr NE2'   6554.76   5268.01   6
'Sud/Merr NE3'   6616.16   5224.93   6
'Sud/Merr NE4'   6604.72   5255.31   6
'Sud/Merr NE5'   6753.29   5285.7   6
'Sud/Merr SE1'   6792.88   5222.3   6
'Sud/Merr SE2'   6724.31   5191.92   6
'Sud/Merr SE3'   6655.74   5161.53   6
'Sud/Merr SE4'   6695.46   5097.91   6
'Sud/Merr SE5'   6735.19   5034.29   6
'Sud/Merr SW1'   6638.58   4981.33   6
'Sud/Merr SW2'   6598.85   5044.95   6
'Sud/Merr SW3'   6559.13   5108.56   6
'Sud/Merr SW4'   6493.36   5072.52   6
'Sud/Merr SW5'   6427.59   5036.47   6
'Sud/Merr NW1'   6347.76   5104.47   6
'Sud/Merr NW2'   6413.53   5140.52   6
'Sud/Merr NW3'   6479.3   5176.56   6
'Sud/Merr NW4'   6417.09   5218.46   6
'Sud/Merr NW5'   6354.88   5260.35   6
'Sud/Sur NE1'   6755.94   5445.69   6
'Sud/Sur NE2'   6800.97   5385.71   6
'Sud/Sur NE3'   6845.99   5325.73   6
'Sud/Sur NE4'   6908.75   5366.8   6
'Sud/Sur NE5'   6971.5   5407.88   6
'Sud/Sur SE1'   7002.41   5368.35   6
'Sud/Sur SE2'   6939.66   5327.28   6
'Sud/Sur SE3'   6876.91   5286.2   6
'Sud/Sur SE4'   6931.69   5234.97   6
'Sud/Sur SE5'   6986.46   5183.75   6
'Sud/Sur SW1'   6932.3   5133.08   6
'Sud/Sur SE2'   6877.52   5184.31   6
'Sud/Sur SE3'   6822.74   5235.54   6
'Sud/Sur SE4'   6754.17   5205.15   6
'Sud/Sur SE5'   6685.61   5174.76   6
'Sud/Sur NW1'   6645.53   5237.94   6
'Sud/Sur NW2'   6714.1   5268.33   6
'Sud/Sur NW3'   6782.66   5298.72   6
'Sud/Sur NW4'   6709.54   5315.38   6
'Sud/Sur NW5'   6636.41   5332.03   6
'Sud/Sur N1'   6642.36   5493.71   6
'Sud/Sur N2'   6687.39   5433.73   6
'Sud/Sur N3'   6732.41   5373.75   6
'Sud/Sur N4'   6659.29   5390.41   6
'Sud/Sur N5'   6586.16   5407.07   6
'2013EX'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   541   0.08375   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   449   0.08375   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   241   0.08375   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   452   0.08375   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   417   0.08375   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   214   0.08375   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   233   0.08375   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   391   0.08375   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   276   0.08375   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   503   0.08375   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   726   0.08375   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   98   0.08375   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   394   0.08375   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   863   0.08375   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
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100   72   3   766   0.08375   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   322   0.08375   1600   1   3
 2
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   35   0.08375   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   853   0.08375   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   818   0.0335   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1226   0.0335   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1219   0.0335   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   859   0.0335   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   796   0.0335   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1264   0.0335   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   954   0.0335   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1198   0.0335   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   805   0.0335   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   405   0.0335   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   322   0.0335   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   853   0.0335   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   35   0.0335   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1185   0.0335   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1465   0.0335   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   766   0.0335   1   78
1   0   4   1000   0   'Y'   10   0   36
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2028 No-Build
Microscale Input Files
(Particulate Matter 10 (PM10))

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'Government Center Garage'   60   175   0   0   60   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Caus/Wash NE1'   6548.31   7035.9   6
'Caus/Wash NE2'   6581.41   6968.6   6
'Caus/Wash NE3'   6614.5   6901.3   6
'Caus/Wash NE4'   6669.75   6952.02   6
'Caus/Wash NE5'   6725   7002.74   6
'Caus/Wash SE1'   6753.58   6912.24   6
'Caus/Wash SE2'   6698.92   6862.05   6
'Caus/Wash SE3'   6643.09   6810.79   6
'Caus/Wash SE4'   6646.8   6736.4   6
'Caus/Wash SE5'   6649.95   6660.95   6
'Caus/Wash SW1'   6544.02   6561.02   6
'Caus/Wash SW2'   6540.9   6635.95   6
'Caus/Wash SW3'   6537.77   6710.89   6
'Caus/Wash SW4'   6476.83   6667.16   6
'Caus/Wash SW5'   6415.9   6623.44   6
'Caus/Wash NW1'   6407.38   6737.95   6
'Caus/Wash NW2'   6468.31   6781.67   6
'Caus/Wash NW3'   6529.25   6825.39   6
'Caus/Wash NW4'   6496.16   6892.69   6
'Caus/Wash NW5'   6463.06   6960   6
'Tha/Val NE1'   6667.28   6395.45   6
'Tha/Val NE2'   6668.3   6320.45   6
'Tha/Val NE3'   6669.31   6245.46   6
'Tha/Val NE4'   6744.31   6245.46   6
'Tha/Val NE5'   6819.25   6249.58   6
'Tha/Val SE1'   6822.27   6191.64   6
'Tha/Val SE2'   6747.3   6189.58   6
'Tha/Val SE3'   6672.33   6187.52   6
'Tha/Val SE4'   6671.6   6112.53   6
'Tha/Val SE5'   6670.88   6037.53   6
'Tha/Val SW1'   6560.17   5964.68   6
'Tha/Val SW2'   6560.89   6039.67   6
'Tha/Val SW3'   6561.62   6114.67   6
'Tha/Val SW4'   6502.18   6068.93   6
'Tha/Val SW5'   6442.74   6023.18   6
'Tha/Val NW1'   6440.95   6115.18   6
'Tha/Val NW2'   6500.39   6160.92   6
'Tha/Val NW3'   6559.82   6206.67   6
'Tha/Val NW4'   6558.81   6281.66   6
'Tha/Val NW5'   6557.8   6356.65   6
'No Build'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   0.0685   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   531   0.0685   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   0.0685   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   0.0685   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   0.0685   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   194   0.0685   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   0.0685   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   0.0685   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2353   0.0685   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
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150   119   3   321   0.0685   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   0.0685   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   741   0.0685   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   0.0685   1600   1   3
 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1678   0.0685   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   0.0685   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   737   0.0685   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1628   0.0685   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   0.0685   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1986   0.0685   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   515   0.0685   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   403   0.0685   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   647   0.0685   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   997   0.0685   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   332   0.0685   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   0.0685   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1396   0.0274   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1568   0.0274   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   899   0.0274   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   0.0274   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3419   0.0274   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   0.0274   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2371   0.0274   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   0.0274   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2397   0.0274   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   0.0274   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2837   0.0274   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   0.0274   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2324   0.0274   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   0.0274   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   515   0.0274   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   0.0274   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   403   0.0274   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   702   0.0274   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   0.0274   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1343   0.0274   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1063   0.0274   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1529   0.0274   1   98
 1
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'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   0.0274   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   50   0.3048   1   0
'Bev/Was N1'   6561.96   6150.17   6
'Bev/Was N2'   6561.23   6075.17   6
'Bev/Was N3'   6560.51   6000.18   6
'Bev/Was N4'   6515.8   6060.39   6
'Bev/Was N5'   6471.09   6120.61   6
'Bev/Was SE1'   6670.99   6049.68   6
'Bev/Was SE2'   6670.19   5966.32   6
'Bev/Was SE3'   6624   5907.23   6
'Bev/Was SE4'   6626.07   5832.26   6
'Bev/Was SE5'   6628.13   5757.29   6
'Bev/Was SW1'   6541.84   5766.87   6
'Bev/Was SW2'   6540.09   5841.85   6
'Bev/Was SW3'   6537.71   5916.82   6
'Bev/Was SW4'   6493   5977.03   6
'Bev/Was SW5'   6448.29   6037.25   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Wash/Cong NE1'   6910.24   4571.18   6
'Wash/Cong NE2'   6925.8   4497.81   6
'Wash/Cong NE3'   6941.37   4424.45   6
'Wash/Cong NE4'   7012.01   4449.65   6
'Wash/Cong NE5'   7082.65   4474.85   6
'Wash/Cong SE1'   7095.42   4388.1   6
'Wash/Cong SE2'   7024.78   4362.9   6
'Wash/Cong SE3'   6954.14   4337.69   6
'Wash/Cong SE4'   6968.42   4264.06   6
'Wash/Cong SE5'   6982.69   4190.43   6
'Wash/Cong SW1'   6867.47   4164.74   6
'Wash/Cong SW2'   6853.27   4238.01   6
'Wash/Cong SW3'   6838.93   4312   6
'Wash/Cong SW4'   6765.63   4296.1   6
'Wash/Cong SW5'   6692.34   4280.2   6
'Wash/Cong NW1'   6682.41   4353.77   6
'Wash/Cong NW2'   6755.7   4369.67   6
'Wash/Cong NW3'   6828.9   4386.02   6
'Wash/Cong NW4'   6813.33   4459.38   6
'Wash/Cong NW5'   6797.76   4532.75   6
'No Build'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   0.0685   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   531   0.0685   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   0.0685   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   0.0685   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   0.0685   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   194   0.0685   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   0.0685   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   0.0685   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2353   0.0685   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
150   119   3   321   0.0685   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   0.0685   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   741   0.0685   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   0.0685   1600   1   3
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 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1678   0.0685   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   0.0685   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   737   0.0685   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1628   0.0685   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   0.0685   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1986   0.0685   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   515   0.0685   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   403   0.0685   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   647   0.0685   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   997   0.0685   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   332   0.0685   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   0.0685   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1396   0.0274   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1568   0.0274   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   899   0.0274   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   0.0274   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3419   0.0274   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   0.0274   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2371   0.0274   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   0.0274   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2397   0.0274   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   0.0274   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2837   0.0274   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   0.0274   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2324   0.0274   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   0.0274   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   515   0.0274   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   0.0274   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   403   0.0274   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   702   0.0274   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   0.0274   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1343   0.0274   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1063   0.0274   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1529   0.0274   1   98
 1
'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   0.0274   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   35   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'No Build'   21   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   79   3   304   0.0685   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   79   3   646   0.0685   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   71   3   412   0.0685   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   79   3   325   0.0685   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   93   3   70   0.0685   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   93   3   289   0.0685   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   439   0.0685   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   320   0.0685   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   62   3   1829   0.0685   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   60   3   321   0.0685   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   60   3   983   0.0685   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1623   0.0274   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1414   0.0274   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   1179   0.0274   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1387   0.0274   1   78
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2078   0.0274   1   66
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   321   0.0274   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   1059   0.0274   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   983   0.0274   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   488   0.0274   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   414   0.0274   1   42
 1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028NB'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   476   0.0685   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   703   0.0685   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   116   0.0685   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   709   0.0685   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   217   0.0685   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   339   0.0685   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   457   0.0685   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   294   0.0685   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   289   0.0685   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   354   0.0685   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   901   0.0685   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   104   0.0685   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   524   0.0685   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   924   0.0685   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   73   3   529   0.0685   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   455   0.0685   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   26   0.0685   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   373   0.0685   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   877   0.0274   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1122   0.0274   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1326   0.0274   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   939   0.0274   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   849   0.0274   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1614   0.0274   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   950   0.0274   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1709   0.0274   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   318   0.0274   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   536   0.0274   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   455   0.0274   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   373   0.0274   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   26   0.0274   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1555   0.0274   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1648   0.0274   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   529   0.0274   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028NB'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   589   0.0685   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   481   0.0685   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   257   0.0685   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   520   0.0685   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   468   0.0685   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   229   0.0685   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   254   0.0685   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   0.0685   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   0.0685   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   536   0.0685   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   809   0.0685   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   106   0.0685   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   435   0.0685   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   954   0.0685   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   72   3   837   0.0685   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   0.0685   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   0.0685   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   928   0.0685   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   921   0.0274   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1336   0.0274   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1354   0.0274   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   940   0.0274   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   863   0.0274   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1593   0.0274   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1023   0.0274   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1636   0.0274   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   901   0.0274   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   488   0.0274   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   0.0274   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   928   0.0274   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   0.0274   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1317   0.0274   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1611   0.0274   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   837   0.0274   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55   5309.91   6
'Sud/Merr NE2'    6554.76   5268.01   6
'Sud/Merr NE3'    6616.16   5224.93   6
'Sud/Merr NE4'    6604.72   5255.31   6
'Sud/Merr NE5'    6753.29   5285.7    6
'Sud/Merr SE1'    6792.88   5222.3    6
'Sud/Merr SE2'    6724.31   5191.92   6
'Sud/Merr SE3'    6655.74   5161.53   6
'Sud/Merr SE4'    6695.46   5097.91   6
'Sud/Merr SE5'    6735.19   5034.29   6
'Sud/Merr SW1'    6638.58   4981.33   6
'Sud/Merr SW2'    6598.85   5044.95   6
'Sud/Merr SW3'    6559.13   5108.56   6
'Sud/Merr SW4'    6493.36   5072.52   6
'Sud/Merr SW5'    6427.59   5036.47   6
'Sud/Merr NW1'    6347.76   5104.47   6
'Sud/Merr NW2'    6413.53   5140.52   6
'Sud/Merr NW3'    6479.3    5176.56   6
'Sud/Merr NW4'    6417.09   5218.46   6
'Sud/Merr NW5'    6354.88   5260.35   6
'Sud/Sur NE1'    6755.94    5445.69    6
'Sud/Sur NE2'    6800.97    5385.71    6
'Sud/Sur NE3'    6845.99    5325.73    6
'Sud/Sur NE4'    6908.75    5366.8     6
'Sud/Sur NE5'    6971.5     5407.88    6
'Sud/Sur SE1'    7002.41    5368.35    6
'Sud/Sur SE2'    6939.66    5327.28    6
'Sud/Sur SE3'    6876.91    5286.2     6
'Sud/Sur SE4'    6931.69    5234.97    6
'Sud/Sur SE5'    6986.46    5183.75    6
'Sud/Sur SW1'    6932.3     5133.08    6
'Sud/Sur SE2'    6877.52    5184.31    6
'Sud/Sur SE3'    6822.74    5235.54    6
'Sud/Sur SE4'    6754.17    5205.15    6
'Sud/Sur SE5'    6685.61    5174.76    6
'Sud/Sur NW1'    6645.53    5237.94    6
'Sud/Sur NW2'    6714.1     5268.33    6
'Sud/Sur NW3'    6782.66    5298.72    6
'Sud/Sur NW4'    6709.54    5315.38    6
'Sud/Sur NW5'    6636.41    5332.03    6
'Sud/Sur N1'    6642.36    5493.71    6
'Sud/Sur N2'    6687.39    5433.73    6
'Sud/Sur N3'    6732.41    5373.75    6
'Sud/Sur N4'    6659.29    5390.41    6
'Sud/Sur N5'    6586.16    5407.07    6
'2028NB'    34   1   0   'P'
 2
'Char/Merr SB'    'AG'    6111.61    5425.13    5935.42    5488.8    1   30   3
100   76   3   476   0.0685   1600   1   3
 2
'Char/Merr WB'    'AG'    6250.42    5435.24    6385.37    5541.98    1   30   3
100   76   3   703   0.0685   1600   1   3
 2
'Char/Merr NB R'    'AG'    6291.66    5369.7    6396.62    5298.54    1   10   1
100   45   3   116   0.0685   1600   1   3
 2
'Char/Merr NB LTT'    'AG'    6280.41    5347.23    6376    5279.81    1   20   2
100   71   3   709   0.0685   1600   1   3
 2
'Char/Merr EB'    'AG'    6104.22    5362.21    5928.03    5296.67    1   20   2
100   79   3   217   0.0685   1600   1   3
 2
'Char/Cam SB L'    'AG'    5384.06    4834.19    5405.87    4921.31    1   10   1
90   58   3   339   0.0685   1600   1   3
 2
'Char/Cam SB TR'    'AG'    5360.81    4833.46    5388.43    4922.76    1   20   2
90   71   3   457   0.0685   1600   1   3
 2
'Char/Cam WB LTTR'    'AG'    5410.95    4793.53    5564.29    4757.95    1   20   2
90   54   3   294   0.0685   1600   1   3
 2
'Char/Cam NB L'    'AG'    5362.99    4722.37    5360.81    4625.08    1   10   1
90   58   3   289   0.0685   1600   1   3
 2
'Char/Cam NB TR'    'AG'    5383.34    4723.83    5384.79    4624.36    1   20   2
90   71   3   354   0.0685   1600   1   3
 2
'Char/Cam EB TTTR'    'AG'    5302.67    4739.8    5163.87    4741.25    1   30   3
90   54   3   901   0.0685   1600   1   3
 2
'Sud/Merr SB L'    'AG'    6532.74    5210.31    6469.76    5255.15    1   10   1
100   86   3   104   0.0685   1600   1   3
 2
'Sud/Merr SB TTT'    'AG'    6518.26    5190.78    6450.94    5229.84    1   30   3
100   49   3   524   0.0685   1600   1   3
 2
'Sud/Merr NB TTTR'    'AG'    6621.05    5161.13    6684.76    5049.03    1   30   3
100   63   3   924   0.0685   1600   1   3
 2
'Sud/Merr EB LTTR'    'AG'    6523.33    5145.94    6435.74    5093.15    1   40   4
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100   73   3   529   0.0685   1600   1   3
 2
'Sud/Sur SB LTT'    'AG'    6777.46    5369.67    6709.4    5455.47    1   20   2
100   53   3   455   0.0685   1600   1   3
 2
'Sud/Sur SEB'    'AG'    6757.21    5330.01    6705.35    5342.96    1   10   1
100   70   3   26   0.0685   1600   1   3
 2
'Sud/Sur EB TTR'    'AG'    6794.47    5259.59    6672.95    5211.83    1   30   3
100   77   3   373   0.0685   1600   1   3
 1
'Char/Merr N'    'AG'    6202.34    5403.71    5845.34    5537.04    877    0.0274    1   84
 1
'Char/Merr E'    'AG'    6201.86    5389.77    6552.37    5635.08    1122    0.0274    1   90
 1
'Char/Merr S'    'AG'    6214.99    5412.24    6411.79    5262.43    1326    0.0274    1   98
 1
'Char/Merr W'    'AG'    6198.12    5397.26    5806.38    5264.31    939    0.0274    1   98
 1
'Char/Camb N'    'AG'    5352.47    4779.69    5466.46    5028.93    849    0.0274    1   78
 1
'Char/Camb E'    'AG'    5334.74    4787.8    5780.86    4671.3    1614    0.0274    1   102
 1
'Char/Camb S'    'AG'    5359.22    4760.44    5362.39    4406.78    950    0.0274    1   78
 1
'Char/Camb W'    'AG'    5364.5    4766.77    5009.45    4767.83    1709    0.0274    1   90
 1
'Sur/Sud E'    'AG'    6831.79    5286.55    6967.42    5375.33    318    0.0274    1   30
 1
'Sur/Sud S'    'AG'    6823.37    5285.61    7028.22    5094.04    536    0.0274    1   54
 1
'Sur/Sud N'    'AG'    6816.26    5313.7    6641.09    5547.04    455    0.0274    1   42
 1
'Sur/Sud W'    'AG'    6584.37    5170.37    6806.25    5268.7    373    0.0274    1   54
 1
'Sur/Sud NW'    'AG'    6797.91    5327.04    6702.82    5348.7    26    0.0274    1   42
 1
'Merr/Sud N'    'AG'    6569.36    5187.04    6420.88    5287.04    1555    0.0274    1   98
 1
'Merr/Sud S'    'AG'    6567.69    5198.7    6786.23    4848.7    1648    0.0274    1   90
 1
'Merr/Sud W'    'AG'    6576.03    5173.7    6284.09    5013.7    529    0.0274    1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55   5309.91   6
'Sud/Merr NE2'    6554.76   5268.01   6
'Sud/Merr NE3'    6616.16   5224.93   6
'Sud/Merr NE4'    6604.72   5255.31   6
'Sud/Merr NE5'    6753.29   5285.7    6
'Sud/Merr SE1'    6792.88   5222.3    6
'Sud/Merr SE2'    6724.31   5191.92   6
'Sud/Merr SE3'    6655.74   5161.53   6
'Sud/Merr SE4'    6695.46   5097.91   6
'Sud/Merr SE5'    6735.19   5034.29   6
'Sud/Merr SW1'    6638.58   4981.33   6
'Sud/Merr SW2'    6598.85   5044.95   6
'Sud/Merr SW3'    6559.13   5108.56   6
'Sud/Merr SW4'    6493.36   5072.52   6
'Sud/Merr SW5'    6427.59   5036.47   6
'Sud/Merr NW1'    6347.76   5104.47   6
'Sud/Merr NW2'    6413.53   5140.52   6
'Sud/Merr NW3'    6479.3    5176.56   6
'Sud/Merr NW4'    6417.09   5218.46   6
'Sud/Merr NW5'    6354.88   5260.35   6
'Sud/Sur NE1'    6755.94   5445.69   6
'Sud/Sur NE2'    6800.97   5385.71   6
'Sud/Sur NE3'    6845.99   5325.73   6
'Sud/Sur NE4'    6908.75   5366.8    6
'Sud/Sur NE5'    6971.5    5407.88   6
'Sud/Sur SE1'    7002.41   5368.35   6
'Sud/Sur SE2'    6939.66   5327.28   6
'Sud/Sur SE3'    6876.91   5286.2    6
'Sud/Sur SE4'    6931.69   5234.97   6
'Sud/Sur SE5'    6986.46   5183.75   6
'Sud/Sur SW1'    6932.3    5133.08   6
'Sud/Sur SE2'    6877.52   5184.31   6
'Sud/Sur SE3'    6822.74   5235.54   6
'Sud/Sur SE4'    6754.17   5205.15   6
'Sud/Sur SE5'    6685.61   5174.76   6
'Sud/Sur NW1'    6645.53   5237.94   6
'Sud/Sur NW2'    6714.1    5268.33   6
'Sud/Sur NW3'    6782.66   5298.72   6
'Sud/Sur NW4'    6709.54   5315.38   6
'Sud/Sur NW5'    6636.41   5332.03   6
'Sud/Sur N1'    6642.36   5493.71   6
'Sud/Sur N2'    6687.39   5433.73   6
'Sud/Sur N3'    6732.41   5373.75   6
'Sud/Sur N4'    6659.29   5390.41   6
'Sud/Sur N5'    6586.16   5407.07   6
'2028NB'    34   1   0   'P'
 2
'Char/Merr SB'    'AG'    6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   589   0.0685   1600   1   3
 2
'Char/Merr WB'    'AG'    6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   481   0.0685   1600   1   3
 2
'Char/Merr NB R'    'AG'    6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   257   0.0685   1600   1   3
 2
'Char/Merr NB LTT'    'AG'    6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   520   0.0685   1600   1   3
 2
'Char/Merr EB'    'AG'    6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   468   0.0685   1600   1   3
 2
'Char/Cam SB L'    'AG'    5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   229   0.0685   1600   1   3
 2
'Char/Cam SB TR'    'AG'    5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   254   0.0685   1600   1   3
 2
'Char/Cam WB LTTR'    'AG'    5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   0.0685   1600   1   3
 2
'Char/Cam NB L'    'AG'    5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   0.0685   1600   1   3
 2
'Char/Cam NB TR'    'AG'    5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   536   0.0685   1600   1   3
 2
'Char/Cam EB TTTR'    'AG'    5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   809   0.0685   1600   1   3
 2
'Sud/Merr SB L'    'AG'    6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   106   0.0685   1600   1   3
 2
'Sud/Merr SB TTT'    'AG'    6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   435   0.0685   1600   1   3
 2
'Sud/Merr NB TTTR'    'AG'    6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   954   0.0685   1600   1   3
 2
'Sud/Merr EB LTTR'    'AG'    6523.33   5145.94   6435.74   5093.15   1   40   4
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100   72   3   837   0.0685   1600   1   3
 2
'Sud/Sur SB LTT'    'AG'    6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   0.0685   1600   1   3
 2
'Sud/Sur SEB'    'AG'    6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   0.0685   1600   1   3
 2
'Sud/Sur EB TTR'    'AG'    6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   928   0.0685   1600   1   3
 1
'Char/Merr N'    'AG'    6202.34   5403.71   5845.34   5537.04   921   0.0274   1   84
 1
'Char/Merr E'    'AG'    6201.86   5389.77   6552.37   5635.08   1336   0.0274   1   90
 1
'Char/Merr S'    'AG'    6214.99   5412.24   6411.79   5262.43   1354   0.0274   1   98
 1
'Char/Merr W'    'AG'    6198.12   5397.26   5806.38   5264.31   940   0.0274   1   98
 1
'Char/Camb N'    'AG'    5352.47   4779.69   5466.46   5028.93   863   0.0274   1   78
 1
'Char/Camb E'    'AG'    5334.74   4787.8   5780.86   4671.3   1593   0.0274   1   102
 1
'Char/Camb S'    'AG'    5359.22   4760.44   5362.39   4406.78   1023   0.0274   1   78
 1
'Char/Camb W'    'AG'    5364.5   4766.77   5009.45   4767.83   1636   0.0274   1   90
 1
'Sur/Sud E'    'AG'    6831.79   5286.55   6967.42   5375.33   901   0.0274   1   30
 1
'Sur/Sud S'    'AG'    6823.37   5285.61   7028.22   5094.04   488   0.0274   1   54
 1
'Sur/Sud N'    'AG'    6816.26   5313.7   6641.09   5547.04   424   0.0274   1   42
 1
'Sur/Sud W'    'AG'    6584.37   5170.37   6806.25   5268.7   928   0.0274   1   54
 1
'Sur/Sud NW'    'AG'    6797.91   5327.04   6702.82   5348.7   37   0.0274   1   42
 1
'Merr/Sud N'    'AG'    6569.36   5187.04   6420.88   5287.04   1317   0.0274   1   98
 1
'Merr/Sud S'    'AG'    6567.69   5198.7   6786.23   4848.7   1611   0.0274   1   90
 1
'Merr/Sud W'    'AG'    6576.03   5173.7   6284.09   5013.7   837   0.0274   1   78
1   0   4   1000   0   'Y'   10   0   36
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2028 Build
Microscale Input Files
(Particulate Matter 10 (PM10))

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'Government Center Garage'   60   175   0   0   60   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Caus/Wash NE1'   6548.31   7035.9   6
'Caus/Wash NE2'   6581.41   6968.6   6
'Caus/Wash NE3'   6614.5   6901.3   6
'Caus/Wash NE4'   6669.75   6952.02   6
'Caus/Wash NE5'   6725   7002.74   6
'Caus/Wash SE1'   6753.58   6912.24   6
'Caus/Wash SE2'   6698.92   6862.05   6
'Caus/Wash SE3'   6643.09   6810.79   6
'Caus/Wash SE4'   6646.8   6736.4   6
'Caus/Wash SE5'   6649.95   6660.95   6
'Caus/Wash SW1'   6544.02   6561.02   6
'Caus/Wash SW2'   6540.9   6635.95   6
'Caus/Wash SW3'   6537.77   6710.89   6
'Caus/Wash SW4'   6476.83   6667.16   6
'Caus/Wash SW5'   6415.9   6623.44   6
'Caus/Wash NW1'   6407.38   6737.95   6
'Caus/Wash NW2'   6468.31   6781.67   6
'Caus/Wash NW3'   6529.25   6825.39   6
'Caus/Wash NW4'   6496.16   6892.69   6
'Caus/Wash NW5'   6463.06   6960   6
'Tha/Val NE1'   6667.28   6395.45   6
'Tha/Val NE2'   6668.3   6320.45   6
'Tha/Val NE3'   6669.31   6245.46   6
'Tha/Val NE4'   6744.31   6245.46   6
'Tha/Val NE5'   6819.25   6249.58   6
'Tha/Val SE1'   6822.27   6191.64   6
'Tha/Val SE2'   6747.3   6189.58   6
'Tha/Val SE3'   6672.33   6187.52   6
'Tha/Val SE4'   6671.6   6112.53   6
'Tha/Val SE5'   6670.88   6037.53   6
'Tha/Val SW1'   6560.17   5964.68   6
'Tha/Val SW2'   6560.89   6039.67   6
'Tha/Val SW3'   6561.62   6114.67   6
'Tha/Val SW4'   6502.18   6068.93   6
'Tha/Val SW5'   6442.74   6023.18   6
'Tha/Val NW1'   6440.95   6115.18   6
'Tha/Val NW2'   6500.39   6160.92   6
'Tha/Val NW3'   6559.82   6206.67   6
'Tha/Val NW4'   6558.81   6281.66   6
'Tha/Val NW5'   6557.8   6356.65   6
'Build'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   0.0685   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   585   0.0685   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   0.0685   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   0.0685   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   0.0685   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   208   0.0685   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   0.0685   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   0.0685   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2380   0.0685   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
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150   119   3   321   0.0685   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   0.0685   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   748   0.0685   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   0.0685   1600   1   3
 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1705   0.0685   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   0.0685   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   744   0.0685   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1655   0.0685   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   0.0685   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   2013   0.0685   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   542   0.0685   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   459   0.0685   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   636   0.0685   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   1267   0.0685   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   345   0.0685   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   0.0685   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1464   0.0274   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1588   0.0274   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   967   0.0274   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   0.0274   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3453   0.0274   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   0.0274   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2405   0.0274   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   0.0274   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2431   0.0274   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   0.0274   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2871   0.0274   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   0.0274   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2351   0.0274   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   0.0274   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   542   0.0274   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   0.0274   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   459   0.0274   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   729   0.0274   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   0.0274   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1629   0.0274   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1333   0.0274   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1545   0.0274   1   98
 1
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'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   0.0274   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   50   0.3048   1   0
'Bev/Was N1'   6561.96   6150.17   6
'Bev/Was N2'   6561.23   6075.17   6
'Bev/Was N3'   6560.51   6000.18   6
'Bev/Was N4'   6515.8   6060.39   6
'Bev/Was N5'   6471.09   6120.61   6
'Bev/Was SE1'   6670.99   6049.68   6
'Bev/Was SE2'   6670.19   5966.32   6
'Bev/Was SE3'   6624   5907.23   6
'Bev/Was SE4'   6626.07   5832.26   6
'Bev/Was SE5'   6628.13   5757.29   6
'Bev/Was SW1'   6541.84   5766.87   6
'Bev/Was SW2'   6540.09   5841.85   6
'Bev/Was SW3'   6537.71   5916.82   6
'Bev/Was SW4'   6493   5977.03   6
'Bev/Was SW5'   6448.29   6037.25   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Wash/Cong NE1'   6910.24   4571.18   6
'Wash/Cong NE2'   6925.8   4497.81   6
'Wash/Cong NE3'   6941.37   4424.45   6
'Wash/Cong NE4'   7012.01   4449.65   6
'Wash/Cong NE5'   7082.65   4474.85   6
'Wash/Cong SE1'   7095.42   4388.1   6
'Wash/Cong SE2'   7024.78   4362.9   6
'Wash/Cong SE3'   6954.14   4337.69   6
'Wash/Cong SE4'   6968.42   4264.06   6
'Wash/Cong SE5'   6982.69   4190.43   6
'Wash/Cong SW1'   6867.47   4164.74   6
'Wash/Cong SW2'   6853.27   4238.01   6
'Wash/Cong SW3'   6838.93   4312   6
'Wash/Cong SW4'   6765.63   4296.1   6
'Wash/Cong SW5'   6692.34   4280.2   6
'Wash/Cong NW1'   6682.41   4353.77   6
'Wash/Cong NW2'   6755.7   4369.67   6
'Wash/Cong NW3'   6828.9   4386.02   6
'Wash/Cong NW4'   6813.33   4459.38   6
'Wash/Cong NW5'   6797.76   4532.75   6
'Build'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   0.0685   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   585   0.0685   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   0.0685   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   0.0685   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   0.0685   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   208   0.0685   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   0.0685   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   0.0685   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2380   0.0685   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
150   119   3   321   0.0685   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   0.0685   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   748   0.0685   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   0.0685   1600   1   3
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 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1705   0.0685   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   0.0685   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   744   0.0685   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1655   0.0685   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   0.0685   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   2013   0.0685   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   542   0.0685   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   459   0.0685   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   636   0.0685   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   1267   0.0685   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   345   0.0685   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   0.0685   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1464   0.0274   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1588   0.0274   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   967   0.0274   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   0.0274   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3453   0.0274   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   0.0274   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2405   0.0274   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   0.0274   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2431   0.0274   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   0.0274   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2871   0.0274   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   0.0274   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2351   0.0274   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   0.0274   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   542   0.0274   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   0.0274   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   459   0.0274   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   729   0.0274   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   0.0274   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1629   0.0274   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1333   0.0274   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1545   0.0274   1   98
 1
'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   0.0274   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   35   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Build'   21   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   79   3   304   0.0685   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   79   3   672   0.0685   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   71   3   412   0.0685   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   79   3   325   0.0685   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   93   3   70   0.0685   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   93   3   331   0.0685   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   439   0.0685   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   320   0.0685   1600   1   3
 2
'Char/93 SB_LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   62   3   1842   0.0685   1600   1   3
 2
'Char/93 WB_LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   60   3   334   0.0685   1600   1   3
 2
'Char/93 EB_TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   60   3   1159   0.0685   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1691   0.0274   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1414   0.0274   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   1247   0.0274   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1387   0.0274   1   78
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2091   0.0274   1   66
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   334   0.0274   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   1059   0.0274   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   1159   0.0274   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   499   0.0274   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   414   0.0274   1   42
 1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028BD'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   530   0.0685   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   74   3   757   0.0685   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   44   3   116   0.0685   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   70   3   1002   0.0685   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   80   3   281   0.0685   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   340   0.0685   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   472   0.0685   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   294   0.0685   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   289   0.0685   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   367   0.0685   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   937   0.0685   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   89   3   104   0.0685   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   41   3   524   0.0685   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   52   3   1232   0.0685   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   76   3   579   0.0685   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   455   0.0685   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   26   0.0685   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   420   0.0685   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   945   0.0274   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1232   0.0274   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1619   0.0274   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   1565   0.0274   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   1016   0.0274   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1651   0.0274   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   964   0.0274   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1759   0.0274   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   360   0.0274   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   541   0.0274   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   455   0.0274   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   420   0.0274   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   26   0.0274   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1848   0.0274   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1944   0.0274   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   579   0.0274   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028BD'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   615   0.0685   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   79   3   517   0.0685   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   52   3   257   0.0685   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   73   3   660   0.0685   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   72   3   679   0.0685   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   233   0.0685   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   301   0.0685   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   0.0685   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   0.0685   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   543   0.0685   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   827   0.0685   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   88   3   106   0.0685   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   52   3   435   0.0685   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   64   3   1094   0.0685   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   65   3   992   0.0685   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   0.0685   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   0.0685   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   1075   0.0685   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   989   0.0274   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1538   0.0274   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1494   0.0274   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   1409   0.0274   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   921   0.0274   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1615   0.0274   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1034   0.0274   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1697   0.0274   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   1032   0.0274   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   504   0.0274   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   0.0274   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   1075   0.0274   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   0.0274   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1457   0.0274   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1759   0.0274   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   992   0.0274   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55   5309.91   6
'Sud/Merr NE2'    6554.76   5268.01   6
'Sud/Merr NE3'    6616.16   5224.93   6
'Sud/Merr NE4'    6604.72   5255.31   6
'Sud/Merr NE5'    6753.29   5285.7    6
'Sud/Merr SE1'    6792.88   5222.3    6
'Sud/Merr SE2'    6724.31   5191.92   6
'Sud/Merr SE3'    6655.74   5161.53   6
'Sud/Merr SE4'    6695.46   5097.91   6
'Sud/Merr SE5'    6735.19   5034.29   6
'Sud/Merr SW1'    6638.58   4981.33   6
'Sud/Merr SW2'    6598.85   5044.95   6
'Sud/Merr SW3'    6559.13   5108.56   6
'Sud/Merr SW4'    6493.36   5072.52   6
'Sud/Merr SW5'    6427.59   5036.47   6
'Sud/Merr NW1'    6347.76   5104.47   6
'Sud/Merr NW2'    6413.53   5140.52   6
'Sud/Merr NW3'    6479.3    5176.56   6
'Sud/Merr NW4'    6417.09   5218.46   6
'Sud/Merr NW5'    6354.88   5260.35   6
'Sud/Sur NE1'    6755.94   5445.69   6
'Sud/Sur NE2'    6800.97   5385.71   6
'Sud/Sur NE3'    6845.99   5325.73   6
'Sud/Sur NE4'    6908.75   5366.8    6
'Sud/Sur NE5'    6971.5    5407.88   6
'Sud/Sur SE1'    7002.41   5368.35   6
'Sud/Sur SE2'    6939.66   5327.28   6
'Sud/Sur SE3'    6876.91   5286.2    6
'Sud/Sur SE4'    6931.69   5234.97   6
'Sud/Sur SE5'    6986.46   5183.75   6
'Sud/Sur SW1'    6932.3    5133.08   6
'Sud/Sur SE2'    6877.52   5184.31   6
'Sud/Sur SE3'    6822.74   5235.54   6
'Sud/Sur SE4'    6754.17   5205.15   6
'Sud/Sur SE5'    6685.61   5174.76   6
'Sud/Sur NW1'    6645.53   5237.94   6
'Sud/Sur NW2'    6714.1    5268.33   6
'Sud/Sur NW3'    6782.66   5298.72   6
'Sud/Sur NW4'    6709.54   5315.38   6
'Sud/Sur NW5'    6636.41   5332.03   6
'Sud/Sur N1'    6642.36   5493.71   6
'Sud/Sur N2'    6687.39   5433.73   6
'Sud/Sur N3'    6732.41   5373.75   6
'Sud/Sur N4'    6659.29   5390.41   6
'Sud/Sur N5'    6586.16   5407.07   6
'2028BD'    34   1   0   'P'
 2
'Char/Merr SB'    'AG'    6111.61    5425.13    5935.42    5488.8    1   30   3
100   76   3   530   0.0685   1600   1   3
 2
'Char/Merr WB'    'AG'    6250.42    5435.24    6385.37    5541.98    1   30   3
100   74   3   757   0.0685   1600   1   3
 2
'Char/Merr NB R'    'AG'    6291.66    5369.7    6396.62    5298.54    1   10   1
100   44   3   116   0.0685   1600   1   3
 2
'Char/Merr NB LTT'    'AG'    6280.41    5347.23    6376    5279.81    1   20   2
100   70   3   1002   0.0685   1600   1   3
 2
'Char/Merr EB'    'AG'    6104.22    5362.21    5928.03    5296.67    1   20   2
100   80   3   281   0.0685   1600   1   3
 2
'Char/Cam SB L'    'AG'    5384.06    4834.19    5405.87    4921.31    1   10   1
90   58   3   340   0.0685   1600   1   3
 2
'Char/Cam SB TR'    'AG'    5360.81    4833.46    5388.43    4922.76    1   20   2
90   71   3   472   0.0685   1600   1   3
 2
'Char/Cam WB LTTR'    'AG'    5410.95    4793.53    5564.29    4757.95    1   20   2
90   54   3   294   0.0685   1600   1   3
 2
'Char/Cam NB L'    'AG'    5362.99    4722.37    5360.81    4625.08    1   10   1
90   58   3   289   0.0685   1600   1   3
 2
'Char/Cam NB TR'    'AG'    5383.34    4723.83    5384.79    4624.36    1   20   2
90   71   3   367   0.0685   1600   1   3
 2
'Char/Cam EB TTTR'    'AG'    5302.67    4739.8    5163.87    4741.25    1   30   3
90   54   3   937   0.0685   1600   1   3
 2
'Sud/Merr SB L'    'AG'    6532.74    5210.31    6469.76    5255.15    1   10   1
100   89   3   104   0.0685   1600   1   3
 2
'Sud/Merr SB TTT'    'AG'    6518.26    5190.78    6450.94    5229.84    1   30   3
100   41   3   524   0.0685   1600   1   3
 2
'Sud/Merr NB TTTR'    'AG'    6621.05    5161.13    6684.76    5049.03    1   30   3
100   52   3   1232   0.0685   1600   1   3
 2
'Sud/Merr EB LTTR'    'AG'    6523.33    5145.94    6435.74    5093.15    1   40   4
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100   76   3   579   0.0685   1600   1   3
 2
'Sud/Sur SB LTT'    'AG'    6777.46    5369.67    6709.4    5455.47    1   20   2
100   53   3   455   0.0685   1600   1   3
 2
'Sud/Sur SEB'    'AG'    6757.21    5330.01    6705.35    5342.96    1   10   1
100   70   3   26   0.0685   1600   1   3
 2
'Sud/Sur EB TTR'    'AG'    6794.47    5259.59    6672.95    5211.83    1   30   3
100   77   3   420   0.0685   1600   1   3
 1
'Char/Merr N'    'AG'    6202.34    5403.71    5845.34    5537.04    945   0.0274   1   84
 1
'Char/Merr E'    'AG'    6201.86    5389.77    6552.37    5635.08    1232   0.0274   1   90
 1
'Char/Merr S'    'AG'    6214.99    5412.24    6411.79    5262.43    1619   0.0274   1   98
 1
'Char/Merr W'    'AG'    6198.12    5397.26    5806.38    5264.31    1565   0.0274   1   98
 1
'Char/Camb N'    'AG'    5352.47    4779.69    5466.46    5028.93    1016   0.0274   1   78
 1
'Char/Camb E'    'AG'    5334.74    4787.8    5780.86    4671.3    1651   0.0274   1   102
 1
'Char/Camb S'    'AG'    5359.22    4760.44    5362.39    4406.78    964   0.0274   1   78
 1
'Char/Camb W'    'AG'    5364.5    4766.77    5009.45    4767.83    1759   0.0274   1   90
 1
'Sur/Sud E'    'AG'    6831.79    5286.55    6967.42    5375.33    360   0.0274   1   30
 1
'Sur/Sud S'    'AG'    6823.37    5285.61    7028.22    5094.04    541   0.0274   1   54
 1
'Sur/Sud N'    'AG'    6816.26    5313.7    6641.09    5547.04    455   0.0274   1   42
 1
'Sur/Sud W'    'AG'    6584.37    5170.37    6806.25    5268.7    420   0.0274   1   54
 1
'Sur/Sud NW'    'AG'    6797.91    5327.04    6702.82    5348.7    26   0.0274   1   42
 1
'Merr/Sud N'    'AG'    6569.36    5187.04    6420.88    5287.04    1848   0.0274   1   98
 1
'Merr/Sud S'    'AG'    6567.69    5198.7    6786.23    4848.7    1944   0.0274   1   90
 1
'Merr/Sud W'    'AG'    6576.03    5173.7    6284.09    5013.7    579   0.0274   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'   6492.55   5309.91   6
'Sud/Merr NE2'   6554.76   5268.01   6
'Sud/Merr NE3'   6616.16   5224.93   6
'Sud/Merr NE4'   6604.72   5255.31   6
'Sud/Merr NE5'   6753.29   5285.7   6
'Sud/Merr SE1'   6792.88   5222.3   6
'Sud/Merr SE2'   6724.31   5191.92   6
'Sud/Merr SE3'   6655.74   5161.53   6
'Sud/Merr SE4'   6695.46   5097.91   6
'Sud/Merr SE5'   6735.19   5034.29   6
'Sud/Merr SW1'   6638.58   4981.33   6
'Sud/Merr SW2'   6598.85   5044.95   6
'Sud/Merr SW3'   6559.13   5108.56   6
'Sud/Merr SW4'   6493.36   5072.52   6
'Sud/Merr SW5'   6427.59   5036.47   6
'Sud/Merr NW1'   6347.76   5104.47   6
'Sud/Merr NW2'   6413.53   5140.52   6
'Sud/Merr NW3'   6479.3   5176.56   6
'Sud/Merr NW4'   6417.09   5218.46   6
'Sud/Merr NW5'   6354.88   5260.35   6
'Sud/Sur NE1'   6755.94   5445.69   6
'Sud/Sur NE2'   6800.97   5385.71   6
'Sud/Sur NE3'   6845.99   5325.73   6
'Sud/Sur NE4'   6908.75   5366.8   6
'Sud/Sur NE5'   6971.5   5407.88   6
'Sud/Sur SE1'   7002.41   5368.35   6
'Sud/Sur SE2'   6939.66   5327.28   6
'Sud/Sur SE3'   6876.91   5286.2   6
'Sud/Sur SE4'   6931.69   5234.97   6
'Sud/Sur SE5'   6986.46   5183.75   6
'Sud/Sur SW1'   6932.3   5133.08   6
'Sud/Sur SE2'   6877.52   5184.31   6
'Sud/Sur SE3'   6822.74   5235.54   6
'Sud/Sur SE4'   6754.17   5205.15   6
'Sud/Sur SE5'   6685.61   5174.76   6
'Sud/Sur NW1'   6645.53   5237.94   6
'Sud/Sur NW2'   6714.1   5268.33   6
'Sud/Sur NW3'   6782.66   5298.72   6
'Sud/Sur NW4'   6709.54   5315.38   6
'Sud/Sur NW5'   6636.41   5332.03   6
'Sud/Sur N1'   6642.36   5493.71   6
'Sud/Sur N2'   6687.39   5433.73   6
'Sud/Sur N3'   6732.41   5373.75   6
'Sud/Sur N4'   6659.29   5390.41   6
'Sud/Sur N5'   6586.16   5407.07   6
'2028BD'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   615   0.0685   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   79   3   517   0.0685   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   52   3   257   0.0685   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   73   3   660   0.0685   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   72   3   679   0.0685   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   233   0.0685   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   301   0.0685   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   0.0685   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   0.0685   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   543   0.0685   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   827   0.0685   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   88   3   106   0.0685   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   52   3   435   0.0685   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   64   3   1094   0.0685   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
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100   65   3   992   0.0685   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   0.0685   1600   1   3
 2
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   0.0685   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   1075   0.0685   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   989   0.0274   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1538   0.0274   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1494   0.0274   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   1409   0.0274   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   921   0.0274   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1615   0.0274   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1034   0.0274   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1697   0.0274   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   1032   0.0274   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   504   0.0274   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   0.0274   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   1075   0.0274   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   0.0274   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1457   0.0274   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1759   0.0274   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   992   0.0274   1   78
1   0   4   1000   0   'Y'   10   0   36
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2013 Existing Microscale Input Files (Particulate Matter 2.5 (PM2.5))

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'Government Center Garage'   60   175   0   0   60   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Caus/Wash NE1'   6548.31   7035.9   6
'Caus/Wash NE2'   6581.41   6968.6   6
'Caus/Wash NE3'   6614.5   6901.3   6
'Caus/Wash NE4'   6669.75   6952.02   6
'Caus/Wash NE5'   6725   7002.74   6
'Caus/Wash SE1'   6753.58   6912.24   6
'Caus/Wash SE2'   6698.92   6862.05   6
'Caus/Wash SE3'   6643.09   6810.79   6
'Caus/Wash SE4'   6646.8   6736.4   6
'Caus/Wash SE5'   6649.95   6660.95   6
'Caus/Wash SW1'   6544.02   6561.02   6
'Caus/Wash SW2'   6540.9   6635.95   6
'Caus/Wash SW3'   6537.77   6710.89   6
'Caus/Wash SW4'   6476.83   6667.16   6
'Caus/Wash SW5'   6415.9   6623.44   6
'Caus/Wash NW1'   6407.38   6737.95   6
'Caus/Wash NW2'   6468.31   6781.67   6
'Caus/Wash NW3'   6529.25   6825.39   6
'Caus/Wash NW4'   6496.16   6892.69   6
'Caus/Wash NW5'   6463.06   6960   6
'Tha/Val NE1'   6667.28   6395.45   6
'Tha/Val NE2'   6668.3   6320.45   6
'Tha/Val NE3'   6669.31   6245.46   6
'Tha/Val NE4'   6744.31   6245.46   6
'Tha/Val NE5'   6819.25   6249.58   6
'Tha/Val SE1'   6822.27   6191.64   6
'Tha/Val SE2'   6747.3   6189.58   6
'Tha/Val SE3'   6672.33   6187.52   6
'Tha/Val SE4'   6671.6   6112.53   6
'Tha/Val SE5'   6670.88   6037.53   6
'Tha/Val SW1'   6560.17   5964.68   6
'Tha/Val SW2'   6560.89   6039.67   6
'Tha/Val SW3'   6561.62   6114.67   6
'Tha/Val SW4'   6502.18   6068.93   6
'Tha/Val SW5'   6442.74   6023.18   6
'Tha/Val NW1'   6440.95   6115.18   6
'Tha/Val NW2'   6500.39   6160.92   6
'Tha/Val NW3'   6559.82   6206.67   6
'Tha/Val NW4'   6558.81   6281.66   6
'Tha/Val NW5'   6557.8   6356.65   6
'Existing'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
90   70   3   223   0.04575   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
90   66   3   481   0.04575   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
90   68   3   527   0.04575   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
90   48   3   265   0.04575   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
90   70   3   142   0.04575   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
90   66   3   166   0.04575   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
90   68   3   265   0.04575   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
90   48   3   208   0.04575   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   56   3   2210   0.04575   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
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150   125   3   296   0.04575   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   73   3   216   0.04575   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
 1
150   108   3   693   0.04575   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   119   3   388   0.04575   1600   1   3
 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
100   34   3   1575   0.04575   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
100   66   3   253   0.04575   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
100   34   3   743   0.04575   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1528   0.04575   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   269   0.04575   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1797   0.04575   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   80   0.04575   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   374   0.04575   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   75   3   598   0.04575   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   916   0.04575   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   306   0.04575   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   16   0.04575   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1120   0.0183   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1275   0.0183   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   817   0.0183   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1322   0.0183   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3211   0.0183   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1012   0.0183   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2221   0.0183   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1162   0.0183   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2247   0.0183   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   91   0.0183   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2524   0.0183   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   280   0.0183   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   1841   0.0183   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   269   0.0183   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   80   0.0183   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   811   0.0183   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   374   0.0183   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   650   0.0183   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   406   0.0183   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1226   0.0183   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   978   0.0183   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1420   0.0183   1   98
 1
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'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   44   0.0183   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   50   0.3048   1   0
'Bev/Was N1'   6561.96   6150.17   6
'Bev/Was N2'   6561.23   6075.17   6
'Bev/Was N3'   6560.51   6000.18   6
'Bev/Was N4'   6515.8   6060.39   6
'Bev/Was N5'   6471.09   6120.61   6
'Bev/Was SE1'   6670.99   6049.68   6
'Bev/Was SE2'   6670.19   5966.32   6
'Bev/Was SE3'   6624   5907.23   6
'Bev/Was SE4'   6626.07   5832.26   6
'Bev/Was SE5'   6628.13   5757.29   6
'Bev/Was SW1'   6541.84   5766.87   6
'Bev/Was SW2'   6540.09   5841.85   6
'Bev/Was SW3'   6537.71   5916.82   6
'Bev/Was SW4'   6493   5977.03   6
'Bev/Was SW5'   6448.29   6037.25   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Wash/Cong NE1'   6910.24   4571.18   6
'Wash/Cong NE2'   6925.8   4497.81   6
'Wash/Cong NE3'   6941.37   4424.45   6
'Wash/Cong NE4'   7012.01   4449.65   6
'Wash/Cong NE5'   7082.65   4474.85   6
'Wash/Cong SE1'   7095.42   4388.1   6
'Wash/Cong SE2'   7024.78   4362.9   6
'Wash/Cong SE3'   6954.14   4337.69   6
'Wash/Cong SE4'   6968.42   4264.06   6
'Wash/Cong SE5'   6982.69   4190.43   6
'Wash/Cong SW1'   6867.47   4164.74   6
'Wash/Cong SW2'   6853.27   4238.01   6
'Wash/Cong SW3'   6838.93   4312   6
'Wash/Cong SW4'   6765.63   4296.1   6
'Wash/Cong SW5'   6692.34   4280.2   6
'Wash/Cong NW1'   6682.41   4353.77   6
'Wash/Cong NW2'   6755.7   4369.67   6
'Wash/Cong NW3'   6828.9   4386.02   6
'Wash/Cong NW4'   6813.33   4459.38   6
'Wash/Cong NW5'   6797.76   4532.75   6
'Existing'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
90   70   3   223   0.04575   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
90   66   3   481   0.04575   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
90   68   3   527   0.04575   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
90   48   3   265   0.04575   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
90   70   3   142   0.04575   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
90   66   3   166   0.04575   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
90   68   3   265   0.04575   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
90   48   3   208   0.04575   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   56   3   2210   0.04575   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
150   125   3   296   0.04575   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   73   3   216   0.04575   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   108   3   693   0.04575   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   119   3   388   0.04575   1600   1   3
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 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
100   34   3   1575   0.04575   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
100   66   3   253   0.04575   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
100   34   3   743   0.04575   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1528   0.04575   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   269   0.04575   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1797   0.04575   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   80   0.04575   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   374   0.04575   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   75   3   598   0.04575   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   916   0.04575   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   306   0.04575   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   16   0.04575   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1120   0.0183   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1275   0.0183   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   817   0.0183   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1322   0.0183   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3211   0.0183   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1012   0.0183   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2221   0.0183   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1162   0.0183   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2247   0.0183   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   91   0.0183   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2524   0.0183   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   280   0.0183   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   1841   0.0183   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   269   0.0183   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   80   0.0183   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   811   0.0183   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   374   0.0183   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   650   0.0183   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   406   0.0183   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1226   0.0183   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   978   0.0183   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1420   0.0183   1   98
 1
'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   44   0.0183   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   35   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Existing'   21   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
100   79   3   208   0.04575   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
100   74   3   595   0.04575   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
100   71   3   332   0.04575   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
100   79   3   259   0.04575   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
100   79   3   66   0.04575   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
100   74   3   176   0.04575   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
100   71   3   371   0.04575   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
100   79   3   300   0.04575   1600   1   3
 2
'Char/93 SB_LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   62   3   1488   0.04575   1600   1   3
 2
'Char/93 WB_LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   60   3   298   0.04575   1600   1   3
 2
'Char/93 EB_TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   60   3   908   0.04575   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1289   0.0183   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1112   0.0183   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   999   0.0183   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1207   0.0183   1   78
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   1635   0.0183   1   66
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   298   0.0183   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   847   0.0183   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   908   0.0183   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   449   0.0183   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   314   0.0183   1   42
 1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2013EX'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   436   0.04575   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   650   0.04575   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   109   0.04575   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   637   0.04575   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   194   0.04575   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   318   0.04575   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   429   0.04575   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   265   0.04575   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   260   0.04575   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   330   0.04575   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   811   0.04575   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   95   0.04575   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   484   0.04575   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   854   0.04575   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   73   3   487   0.04575   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   405   0.04575   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   25   0.04575   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   338   0.04575   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   802   0.0183   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1038   0.0183   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1204   0.0183   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   870   0.0183   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   923   0.0183   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1472   0.0183   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   877   0.0183   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1546   0.0183   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   285   0.0183   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   483   0.0183   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   405   0.0183   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   338   0.0183   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   25   0.0183   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1421   0.0183   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1512   0.0183   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   487   0.0183   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2013EX'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   541   0.04575   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   449   0.04575   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   241   0.04575   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   452   0.04575   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   417   0.04575   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   214   0.04575   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   233   0.04575   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   391   0.04575   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   276   0.04575   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   503   0.04575   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   726   0.04575   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   98   0.04575   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   394   0.04575   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   863   0.04575   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   72   3   766   0.04575   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   322   0.04575   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   35   0.04575   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   853   0.04575   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   818   0.0183   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1226   0.0183   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1219   0.0183   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   859   0.0183   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   796   0.0183   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1264   0.0183   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   954   0.0183   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1198   0.0183   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   805   0.0183   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   405   0.0183   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   322   0.0183   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   853   0.0183   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   35   0.0183   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1185   0.0183   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1465   0.0183   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   766   0.0183   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55   5309.91   6
'Sud/Merr NE2'    6554.76   5268.01   6
'Sud/Merr NE3'    6616.16   5224.93   6
'Sud/Merr NE4'    6604.72   5255.31   6
'Sud/Merr NE5'    6753.29   5285.7    6
'Sud/Merr SE1'    6792.88   5222.3    6
'Sud/Merr SE2'    6724.31   5191.92   6
'Sud/Merr SE3'    6655.74   5161.53   6
'Sud/Merr SE4'    6695.46   5097.91   6
'Sud/Merr SE5'    6735.19   5034.29   6
'Sud/Merr SW1'    6638.58   4981.33   6
'Sud/Merr SW2'    6598.85   5044.95   6
'Sud/Merr SW3'    6559.13   5108.56   6
'Sud/Merr SW4'    6493.36   5072.52   6
'Sud/Merr SW5'    6427.59   5036.47   6
'Sud/Merr NW1'    6347.76   5104.47   6
'Sud/Merr NW2'    6413.53   5140.52   6
'Sud/Merr NW3'    6479.3    5176.56   6
'Sud/Merr NW4'    6417.09   5218.46   6
'Sud/Merr NW5'    6354.88   5260.35   6
'Sud/Sur NE1'    6755.94   5445.69   6
'Sud/Sur NE2'    6800.97   5385.71   6
'Sud/Sur NE3'    6845.99   5325.73   6
'Sud/Sur NE4'    6908.75   5366.8    6
'Sud/Sur NE5'    6971.5    5407.88   6
'Sud/Sur SE1'    7002.41   5368.35   6
'Sud/Sur SE2'    6939.66   5327.28   6
'Sud/Sur SE3'    6876.91   5286.2    6
'Sud/Sur SE4'    6931.69   5234.97   6
'Sud/Sur SE5'    6986.46   5183.75   6
'Sud/Sur SW1'    6932.3    5133.08   6
'Sud/Sur SE2'    6877.52   5184.31   6
'Sud/Sur SE3'    6822.74   5235.54   6
'Sud/Sur SE4'    6754.17   5205.15   6
'Sud/Sur SE5'    6685.61   5174.76   6
'Sud/Sur NW1'    6645.53   5237.94   6
'Sud/Sur NW2'    6714.1    5268.33   6
'Sud/Sur NW3'    6782.66   5298.72   6
'Sud/Sur NW4'    6709.54   5315.38   6
'Sud/Sur NW5'    6636.41   5332.03   6
'Sud/Sur N1'    6642.36   5493.71   6
'Sud/Sur N2'    6687.39   5433.73   6
'Sud/Sur N3'    6732.41   5373.75   6
'Sud/Sur N4'    6659.29   5390.41   6
'Sud/Sur N5'    6586.16   5407.07   6
'2013EX'    34   1   0   'P'
 2
'Char/Merr SB'    'AG'    6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   436   0.04575   1600   1   3
 2
'Char/Merr WB'    'AG'    6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   650   0.04575   1600   1   3
 2
'Char/Merr NB R'    'AG'    6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   109   0.04575   1600   1   3
 2
'Char/Merr NB LTT'    'AG'    6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   637   0.04575   1600   1   3
 2
'Char/Merr EB'    'AG'    6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   194   0.04575   1600   1   3
 2
'Char/Cam SB L'    'AG'    5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   318   0.04575   1600   1   3
 2
'Char/Cam SB TR'    'AG'    5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   429   0.04575   1600   1   3
 2
'Char/Cam WB LTTR'    'AG'    5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   265   0.04575   1600   1   3
 2
'Char/Cam NB L'    'AG'    5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   260   0.04575   1600   1   3
 2
'Char/Cam NB TR'    'AG'    5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   330   0.04575   1600   1   3
 2
'Char/Cam EB TTTR'    'AG'    5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   811   0.04575   1600   1   3
 2
'Sud/Merr SB L'    'AG'    6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   95   0.04575   1600   1   3
 2
'Sud/Merr SB TTT'    'AG'    6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   484   0.04575   1600   1   3
 2
'Sud/Merr NB TTTR'    'AG'    6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   854   0.04575   1600   1   3
 2
'Sud/Merr EB LTTR'    'AG'    6523.33   5145.94   6435.74   5093.15   1   40   4
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100   73   3   487   0.04575   1600   1   3
 2
'Sud/Sur SB LTT'    'AG'    6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   405   0.04575   1600   1   3
 2
'Sud/Sur SEB'    'AG'    6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   25   0.04575   1600   1   3
 2
'Sud/Sur EB TTR'    'AG'    6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   338   0.04575   1600   1   3
 1
'Char/Merr N'    'AG'    6202.34   5403.71   5845.34   5537.04   802   0.0183   1   84
 1
'Char/Merr E'    'AG'    6201.86   5389.77   6552.37   5635.08   1038   0.0183   1   90
 1
'Char/Merr S'    'AG'    6214.99   5412.24   6411.79   5262.43   1204   0.0183   1   98
 1
'Char/Merr W'    'AG'    6198.12   5397.26   5806.38   5264.31   870   0.0183   1   98
 1
'Char/Camb N'    'AG'    5352.47   4779.69   5466.46   5028.93   923   0.0183   1   78
 1
'Char/Camb E'    'AG'    5334.74   4787.8   5780.86   4671.3   1472   0.0183   1   102
 1
'Char/Camb S'    'AG'    5359.22   4760.44   5362.39   4406.78   877   0.0183   1   78
 1
'Char/Camb W'    'AG'    5364.5   4766.77   5009.45   4767.83   1546   0.0183   1   90
 1
'Sur/Sud E'    'AG'    6831.79   5286.55   6967.42   5375.33   285   0.0183   1   30
 1
'Sur/Sud S'    'AG'    6823.37   5285.61   7028.22   5094.04   483   0.0183   1   54
 1
'Sur/Sud N'    'AG'    6816.26   5313.7   6641.09   5547.04   405   0.0183   1   42
 1
'Sur/Sud W'    'AG'    6584.37   5170.37   6806.25   5268.7   338   0.0183   1   54
 1
'Sur/Sud NW'    'AG'    6797.91   5327.04   6702.82   5348.7   25   0.0183   1   42
 1
'Merr/Sud N'    'AG'    6569.36   5187.04   6420.88   5287.04   1421   0.0183   1   98
 1
'Merr/Sud S'    'AG'    6567.69   5198.7   6786.23   4848.7   1512   0.0183   1   90
 1
'Merr/Sud W'    'AG'    6576.03   5173.7   6284.09   5013.7   487   0.0183   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55    5309.91    6
'Sud/Merr NE2'    6554.76    5268.01    6
'Sud/Merr NE3'    6616.16    5224.93    6
'Sud/Merr NE4'    6604.72    5255.31    6
'Sud/Merr NE5'    6753.29    5285.7    6
'Sud/Merr SE1'    6792.88    5222.3    6
'Sud/Merr SE2'    6724.31    5191.92    6
'Sud/Merr SE3'    6655.74    5161.53    6
'Sud/Merr SE4'    6695.46    5097.91    6
'Sud/Merr SE5'    6735.19    5034.29    6
'Sud/Merr SW1'    6638.58    4981.33    6
'Sud/Merr SW2'    6598.85    5044.95    6
'Sud/Merr SW3'    6559.13    5108.56    6
'Sud/Merr SW4'    6493.36    5072.52    6
'Sud/Merr SW5'    6427.59    5036.47    6
'Sud/Merr NW1'    6347.76    5104.47    6
'Sud/Merr NW2'    6413.53    5140.52    6
'Sud/Merr NW3'    6479.3    5176.56    6
'Sud/Merr NW4'    6417.09    5218.46    6
'Sud/Merr NW5'    6354.88    5260.35    6
'Sud/Sur NE1'    6755.94    5445.69    6
'Sud/Sur NE2'    6800.97    5385.71    6
'Sud/Sur NE3'    6845.99    5325.73    6
'Sud/Sur NE4'    6908.75    5366.8    6
'Sud/Sur NE5'    6971.5    5407.88    6
'Sud/Sur SE1'    7002.41    5368.35    6
'Sud/Sur SE2'    6939.66    5327.28    6
'Sud/Sur SE3'    6876.91    5286.2    6
'Sud/Sur SE4'    6931.69    5234.97    6
'Sud/Sur SE5'    6986.46    5183.75    6
'Sud/Sur SW1'    6932.3    5133.08    6
'Sud/Sur SE2'    6877.52    5184.31    6
'Sud/Sur SE3'    6822.74    5235.54    6
'Sud/Sur SE4'    6754.17    5205.15    6
'Sud/Sur SE5'    6685.61    5174.76    6
'Sud/Sur NW1'    6645.53    5237.94    6
'Sud/Sur NW2'    6714.1    5268.33    6
'Sud/Sur NW3'    6782.66    5298.72    6
'Sud/Sur NW4'    6709.54    5315.38    6
'Sud/Sur NW5'    6636.41    5332.03    6
'Sud/Sur N1'    6642.36    5493.71    6
'Sud/Sur N2'    6687.39    5433.73    6
'Sud/Sur N3'    6732.41    5373.75    6
'Sud/Sur N4'    6659.29    5390.41    6
'Sud/Sur N5'    6586.16    5407.07    6
'2013EX'    34   1   0   'P'
 2
'Char/Merr SB'    'AG'    6111.61    5425.13    5935.42    5488.8    1   30   3
100   75   3   541   0.04575   1600   1   3
 2
'Char/Merr WB'    'AG'    6250.42    5435.24    6385.37    5541.98    1   30   3
100   78   3   449   0.04575   1600   1   3
 2
'Char/Merr NB R'    'AG'    6291.66    5369.7    6396.62    5298.54    1   10   1
100   46   3   241   0.04575   1600   1   3
 2
'Char/Merr NB LTT'    'AG'    6280.41    5347.23    6376    5279.81    1   20   2
100   68   3   452   0.04575   1600   1   3
 2
'Char/Merr EB'    'AG'    6104.22    5362.21    5928.03    5296.67    1   20   2
100   79   3   417   0.04575   1600   1   3
 2
'Char/Cam SB L'    'AG'    5384.06    4834.19    5405.87    4921.31    1   10   1
100   60   3   214   0.04575   1600   1   3
 2
'Char/Cam SB TR'    'AG'    5360.81    4833.46    5388.43    4922.76    1   20   2
100   72   3   233   0.04575   1600   1   3
 2
'Char/Cam WB LTTR'    'AG'    5410.95    4793.53    5564.29    4757.95    1   20   2
100   62   3   391   0.04575   1600   1   3
 2
'Char/Cam NB L'    'AG'    5362.99    4722.37    5360.81    4625.08    1   10   1
100   60   3   276   0.04575   1600   1   3
 2
'Char/Cam NB TR'    'AG'    5383.34    4723.83    5384.79    4624.36    1   20   2
100   72   3   503   0.04575   1600   1   3
 2
'Char/Cam EB TTTR'    'AG'    5302.67    4739.8    5163.87    4741.25    1   30   3
100   62   3   726   0.04575   1600   1   3
 2
'Sud/Merr SB L'    'AG'    6532.74    5210.31    6469.76    5255.15    1   10   1
100   84   3   98   0.04575   1600   1   3
 2
'Sud/Merr SB TTT'    'AG'    6518.26    5190.78    6450.94    5229.84    1   30   3
100   50   3   394   0.04575   1600   1   3
 2
'Sud/Merr NB TTTR'    'AG'    6621.05    5161.13    6684.76    5049.03    1   30   3
100   66   3   863   0.04575   1600   1   3
 2
'Sud/Merr EB LTTR'    'AG'    6523.33    5145.94    6435.74    5093.15    1   40   4
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100   72   3   766   0.04575   1600   1   3
 2
'Sud/Sur SB LTT'    'AG'    6777.46    5369.67    6709.4    5455.47    1   20   2
100   70   3   322   0.04575   1600   1   3
 2
'Sud/Sur SEB'    'AG'    6757.21    5330.01    6705.35    5342.96    1   10   1
100   80   3   35   0.04575   1600   1   3
 2
'Sud/Sur EB TTR'    'AG'    6794.47    5259.59    6672.95    5211.83    1   30   3
100   50   3   853   0.04575   1600   1   3
 1
'Char/Merr N'    'AG'    6202.34    5403.71    5845.34    5537.04    818    0.0183    1   84
 1
'Char/Merr E'    'AG'    6201.86    5389.77    6552.37    5635.08    1226    0.0183    1   90
 1
'Char/Merr S'    'AG'    6214.99    5412.24    6411.79    5262.43    1219    0.0183    1   98
 1
'Char/Merr W'    'AG'    6198.12    5397.26    5806.38    5264.31    859    0.0183    1   98
 1
'Char/Camb N'    'AG'    5352.47    4779.69    5466.46    5028.93    796    0.0183    1   78
 1
'Char/Camb E'    'AG'    5334.74    4787.8    5780.86    4671.3    1264    0.0183    1   102
 1
'Char/Camb S'    'AG'    5359.22    4760.44    5362.39    4406.78    954    0.0183    1   78
 1
'Char/Camb W'    'AG'    5364.5    4766.77    5009.45    4767.83    1198    0.0183    1   90
 1
'Sur/Sud E'    'AG'    6831.79    5286.55    6967.42    5375.33    805    0.0183    1   30
 1
'Sur/Sud S'    'AG'    6823.37    5285.61    7028.22    5094.04    405    0.0183    1   54
 1
'Sur/Sud N'    'AG'    6816.26    5313.7    6641.09    5547.04    322    0.0183    1   42
 1
'Sur/Sud W'    'AG'    6584.37    5170.37    6806.25    5268.7    853    0.0183    1   54
 1
'Sur/Sud NW'    'AG'    6797.91    5327.04    6702.82    5348.7    35    0.0183    1   42
 1
'Merr/Sud N'    'AG'    6569.36    5187.04    6420.88    5287.04    1185    0.0183    1   98
 1
'Merr/Sud S'    'AG'    6567.69    5198.7    6786.23    4848.7    1465    0.0183    1   90
 1
'Merr/Sud W'    'AG'    6576.03    5173.7    6284.09    5013.7    766    0.0183    1   78
1   0   4   1000   0   'Y'   10   0   36
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2028 No-Build
Microscale Input Files
(Particulate Matter 2.5 (PM2.5))

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'Government Center Garage'   60   175   0   0   60   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Caus/Wash NE1'   6548.31   7035.9   6
'Caus/Wash NE2'   6581.41   6968.6   6
'Caus/Wash NE3'   6614.5   6901.3   6
'Caus/Wash NE4'   6669.75   6952.02   6
'Caus/Wash NE5'   6725   7002.74   6
'Caus/Wash SE1'   6753.58   6912.24   6
'Caus/Wash SE2'   6698.92   6862.05   6
'Caus/Wash SE3'   6643.09   6810.79   6
'Caus/Wash SE4'   6646.8   6736.4   6
'Caus/Wash SE5'   6649.95   6660.95   6
'Caus/Wash SW1'   6544.02   6561.02   6
'Caus/Wash SW2'   6540.9   6635.95   6
'Caus/Wash SW3'   6537.77   6710.89   6
'Caus/Wash SW4'   6476.83   6667.16   6
'Caus/Wash SW5'   6415.9   6623.44   6
'Caus/Wash NW1'   6407.38   6737.95   6
'Caus/Wash NW2'   6468.31   6781.67   6
'Caus/Wash NW3'   6529.25   6825.39   6
'Caus/Wash NW4'   6496.16   6892.69   6
'Caus/Wash NW5'   6463.06   6960   6
'Tha/Val NE1'   6667.28   6395.45   6
'Tha/Val NE2'   6668.3   6320.45   6
'Tha/Val NE3'   6669.31   6245.46   6
'Tha/Val NE4'   6744.31   6245.46   6
'Tha/Val NE5'   6819.25   6249.58   6
'Tha/Val SE1'   6822.27   6191.64   6
'Tha/Val SE2'   6747.3   6189.58   6
'Tha/Val SE3'   6672.33   6187.52   6
'Tha/Val SE4'   6671.6   6112.53   6
'Tha/Val SE5'   6670.88   6037.53   6
'Tha/Val SW1'   6560.17   5964.68   6
'Tha/Val SW2'   6560.89   6039.67   6
'Tha/Val SW3'   6561.62   6114.67   6
'Tha/Val SW4'   6502.18   6068.93   6
'Tha/Val SW5'   6442.74   6023.18   6
'Tha/Val NW1'   6440.95   6115.18   6
'Tha/Val NW2'   6500.39   6160.92   6
'Tha/Val NW3'   6559.82   6206.67   6
'Tha/Val NW4'   6558.81   6281.66   6
'Tha/Val NW5'   6557.8   6356.65   6
'No Build'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   0.03175   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   531   0.03175   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   0.03175   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   0.03175   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   0.03175   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   194   0.03175   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   0.03175   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   0.03175   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2353   0.03175   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
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150   119   3   321   0.03175   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   0.03175   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   741   0.03175   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   0.03175   1600   1   3
 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1678   0.03175   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   0.03175   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   737   0.03175   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1628   0.03175   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   0.03175   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1986   0.03175   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   515   0.03175   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   403   0.03175   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   647   0.03175   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   997   0.03175   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   332   0.03175   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   0.03175   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1396   0.0127   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1568   0.0127   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   899   0.0127   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   0.0127   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3419   0.0127   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   0.0127   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2371   0.0127   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   0.0127   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2397   0.0127   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   0.0127   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2837   0.0127   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   0.0127   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2324   0.0127   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   0.0127   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   515   0.0127   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   0.0127   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   403   0.0127   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   702   0.0127   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   0.0127   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1343   0.0127   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1063   0.0127   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1529   0.0127   1   98
 1
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'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   0.0127   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   50   0.3048   1   0
'Bev/Was N1'   6561.96   6150.17   6
'Bev/Was N2'   6561.23   6075.17   6
'Bev/Was N3'   6560.51   6000.18   6
'Bev/Was N4'   6515.8   6060.39   6
'Bev/Was N5'   6471.09   6120.61   6
'Bev/Was SE1'   6670.99   6049.68   6
'Bev/Was SE2'   6670.19   5966.32   6
'Bev/Was SE3'   6624   5907.23   6
'Bev/Was SE4'   6626.07   5832.26   6
'Bev/Was SE5'   6628.13   5757.29   6
'Bev/Was SW1'   6541.84   5766.87   6
'Bev/Was SW2'   6540.09   5841.85   6
'Bev/Was SW3'   6537.71   5916.82   6
'Bev/Was SW4'   6493   5977.03   6
'Bev/Was SW5'   6448.29   6037.25   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Wash/Cong NE1'   6910.24   4571.18   6
'Wash/Cong NE2'   6925.8   4497.81   6
'Wash/Cong NE3'   6941.37   4424.45   6
'Wash/Cong NE4'   7012.01   4449.65   6
'Wash/Cong NE5'   7082.65   4474.85   6
'Wash/Cong SE1'   7095.42   4388.1   6
'Wash/Cong SE2'   7024.78   4362.9   6
'Wash/Cong SE3'   6954.14   4337.69   6
'Wash/Cong SE4'   6968.42   4264.06   6
'Wash/Cong SE5'   6982.69   4190.43   6
'Wash/Cong SW1'   6867.47   4164.74   6
'Wash/Cong SW2'   6853.27   4238.01   6
'Wash/Cong SW3'   6838.93   4312   6
'Wash/Cong SW4'   6765.63   4296.1   6
'Wash/Cong SW5'   6692.34   4280.2   6
'Wash/Cong NW1'   6682.41   4353.77   6
'Wash/Cong NW2'   6755.7   4369.67   6
'Wash/Cong NW3'   6828.9   4386.02   6
'Wash/Cong NW4'   6813.33   4459.38   6
'Wash/Cong NW5'   6797.76   4532.75   6
'No Build'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   0.03175   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   531   0.03175   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   0.03175   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   0.03175   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   0.03175   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   194   0.03175   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   0.03175   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   0.03175   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2353   0.03175   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
150   119   3   321   0.03175   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   0.03175   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   741   0.03175   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   0.03175   1600   1   3
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 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1678   0.03175   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   0.03175   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   737   0.03175   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1628   0.03175   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   0.03175   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   1986   0.03175   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   515   0.03175   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   403   0.03175   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   647   0.03175   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   997   0.03175   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   332   0.03175   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   0.03175   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1396   0.0127   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1568   0.0127   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   899   0.0127   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   0.0127   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3419   0.0127   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   0.0127   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2371   0.0127   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   0.0127   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2397   0.0127   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   0.0127   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2837   0.0127   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   0.0127   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2324   0.0127   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   0.0127   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   515   0.0127   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   0.0127   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   403   0.0127   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   702   0.0127   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   0.0127   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1343   0.0127   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1063   0.0127   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1529   0.0127   1   98
 1
'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   0.0127   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   35   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'No Build'   21   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   79   3   304   0.03175   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   79   3   646   0.03175   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   71   3   412   0.03175   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   79   3   325   0.03175   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   93   3   70   0.03175   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   93   3   289   0.03175   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   439   0.03175   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   320   0.03175   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   62   3   1829   0.03175   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   60   3   321   0.03175   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   60   3   983   0.03175   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1623   0.0127   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1414   0.0127   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   1179   0.0127   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1387   0.0127   1   78
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2078   0.0127   1   66
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   321   0.0127   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   1059   0.0127   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   983   0.0127   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   488   0.0127   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   414   0.0127   1   42
 1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028NB'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   476   0.03175   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   703   0.03175   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   116   0.03175   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   709   0.03175   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   217   0.03175   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   339   0.03175   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   457   0.03175   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   294   0.03175   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   289   0.03175   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   354   0.03175   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   901   0.03175   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   104   0.03175   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   524   0.03175   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   924   0.03175   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   73   3   529   0.03175   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   455   0.03175   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   26   0.03175   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   373   0.03175   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   877   0.0127   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1122   0.0127   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1326   0.0127   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   939   0.0127   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   849   0.0127   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1614   0.0127   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   950   0.0127   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1709   0.0127   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   318   0.0127   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   536   0.0127   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   455   0.0127   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   373   0.0127   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   26   0.0127   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1555   0.0127   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1648   0.0127   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   529   0.0127   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028NB'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   589   0.03175   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   481   0.03175   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   257   0.03175   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   520   0.03175   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   468   0.03175   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   229   0.03175   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   254   0.03175   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   0.03175   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   0.03175   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   536   0.03175   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   809   0.03175   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   106   0.03175   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   435   0.03175   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   954   0.03175   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   72   3   837   0.03175   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   0.03175   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   0.03175   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   928   0.03175   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   921   0.0127   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1336   0.0127   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1354   0.0127   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   940   0.0127   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   863   0.0127   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1593   0.0127   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1023   0.0127   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1636   0.0127   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   901   0.0127   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   488   0.0127   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   0.0127   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   928   0.0127   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   0.0127   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1317   0.0127   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1611   0.0127   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   837   0.0127   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55   5309.91   6
'Sud/Merr NE2'    6554.76   5268.01   6
'Sud/Merr NE3'    6616.16   5224.93   6
'Sud/Merr NE4'    6604.72   5255.31   6
'Sud/Merr NE5'    6753.29   5285.7    6
'Sud/Merr SE1'    6792.88   5222.3    6
'Sud/Merr SE2'    6724.31   5191.92   6
'Sud/Merr SE3'    6655.74   5161.53   6
'Sud/Merr SE4'    6695.46   5097.91   6
'Sud/Merr SE5'    6735.19   5034.29   6
'Sud/Merr SW1'    6638.58   4981.33   6
'Sud/Merr SW2'    6598.85   5044.95   6
'Sud/Merr SW3'    6559.13   5108.56   6
'Sud/Merr SW4'    6493.36   5072.52   6
'Sud/Merr SW5'    6427.59   5036.47   6
'Sud/Merr NW1'    6347.76   5104.47   6
'Sud/Merr NW2'    6413.53   5140.52   6
'Sud/Merr NW3'    6479.3    5176.56   6
'Sud/Merr NW4'    6417.09   5218.46   6
'Sud/Merr NW5'    6354.88   5260.35   6
'Sud/Sur NE1'    6755.94   5445.69   6
'Sud/Sur NE2'    6800.97   5385.71   6
'Sud/Sur NE3'    6845.99   5325.73   6
'Sud/Sur NE4'    6908.75   5366.8    6
'Sud/Sur NE5'    6971.5    5407.88   6
'Sud/Sur SE1'    7002.41   5368.35   6
'Sud/Sur SE2'    6939.66   5327.28   6
'Sud/Sur SE3'    6876.91   5286.2    6
'Sud/Sur SE4'    6931.69   5234.97   6
'Sud/Sur SE5'    6986.46   5183.75   6
'Sud/Sur SW1'    6932.3    5133.08   6
'Sud/Sur SE2'    6877.52   5184.31   6
'Sud/Sur SE3'    6822.74   5235.54   6
'Sud/Sur SE4'    6754.17   5205.15   6
'Sud/Sur SE5'    6685.61   5174.76   6
'Sud/Sur NW1'    6645.53   5237.94   6
'Sud/Sur NW2'    6714.1    5268.33   6
'Sud/Sur NW3'    6782.66   5298.72   6
'Sud/Sur NW4'    6709.54   5315.38   6
'Sud/Sur NW5'    6636.41   5332.03   6
'Sud/Sur N1'    6642.36   5493.71   6
'Sud/Sur N2'    6687.39   5433.73   6
'Sud/Sur N3'    6732.41   5373.75   6
'Sud/Sur N4'    6659.29   5390.41   6
'Sud/Sur N5'    6586.16   5407.07   6
'2028NB'    34   1   0   'P'
 2
'Char/Merr SB'    'AG'    6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   476   0.03175   1600   1   3
 2
'Char/Merr WB'    'AG'    6250.42   5435.24   6385.37   5541.98   1   30   3
100   76   3   703   0.03175   1600   1   3
 2
'Char/Merr NB R'    'AG'    6291.66   5369.7   6396.62   5298.54   1   10   1
100   45   3   116   0.03175   1600   1   3
 2
'Char/Merr NB LTT'    'AG'    6280.41   5347.23   6376   5279.81   1   20   2
100   71   3   709   0.03175   1600   1   3
 2
'Char/Merr EB'    'AG'    6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   217   0.03175   1600   1   3
 2
'Char/Cam SB L'    'AG'    5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   339   0.03175   1600   1   3
 2
'Char/Cam SB TR'    'AG'    5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   457   0.03175   1600   1   3
 2
'Char/Cam WB LTTR'    'AG'    5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   294   0.03175   1600   1   3
 2
'Char/Cam NB L'    'AG'    5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   289   0.03175   1600   1   3
 2
'Char/Cam NB TR'    'AG'    5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   354   0.03175   1600   1   3
 2
'Char/Cam EB TTTR'    'AG'    5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   901   0.03175   1600   1   3
 2
'Sud/Merr SB L'    'AG'    6532.74   5210.31   6469.76   5255.15   1   10   1
100   86   3   104   0.03175   1600   1   3
 2
'Sud/Merr SB TTT'    'AG'    6518.26   5190.78   6450.94   5229.84   1   30   3
100   49   3   524   0.03175   1600   1   3
 2
'Sud/Merr NB TTTR'    'AG'    6621.05   5161.13   6684.76   5049.03   1   30   3
100   63   3   924   0.03175   1600   1   3
 2
'Sud/Merr EB LTTR'    'AG'    6523.33   5145.94   6435.74   5093.15   1   40   4
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100   73   3   529   0.03175   1600   1   3
 2
'Sud/Sur SB LTT'    'AG'    6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   455   0.03175   1600   1   3
 2
'Sud/Sur SEB'    'AG'    6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   26   0.03175   1600   1   3
 2
'Sud/Sur EB TTR'    'AG'    6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   373   0.03175   1600   1   3
 1
'Char/Merr N'    'AG'    6202.34   5403.71   5845.34   5537.04   877   0.0127   1   84
 1
'Char/Merr E'    'AG'    6201.86   5389.77   6552.37   5635.08   1122   0.0127   1   90
 1
'Char/Merr S'    'AG'    6214.99   5412.24   6411.79   5262.43   1326   0.0127   1   98
 1
'Char/Merr W'    'AG'    6198.12   5397.26   5806.38   5264.31   939   0.0127   1   98
 1
'Char/Camb N'    'AG'    5352.47   4779.69   5466.46   5028.93   849   0.0127   1   78
 1
'Char/Camb E'    'AG'    5334.74   4787.8   5780.86   4671.3   1614   0.0127   1   102
 1
'Char/Camb S'    'AG'    5359.22   4760.44   5362.39   4406.78   950   0.0127   1   78
 1
'Char/Camb W'    'AG'    5364.5   4766.77   5009.45   4767.83   1709   0.0127   1   90
 1
'Sur/Sud E'    'AG'    6831.79   5286.55   6967.42   5375.33   318   0.0127   1   30
 1
'Sur/Sud S'    'AG'    6823.37   5285.61   7028.22   5094.04   536   0.0127   1   54
 1
'Sur/Sud N'    'AG'    6816.26   5313.7   6641.09   5547.04   455   0.0127   1   42
 1
'Sur/Sud W'    'AG'    6584.37   5170.37   6806.25   5268.7   373   0.0127   1   54
 1
'Sur/Sud NW'    'AG'    6797.91   5327.04   6702.82   5348.7   26   0.0127   1   42
 1
'Merr/Sud N'    'AG'    6569.36   5187.04   6420.88   5287.04   1555   0.0127   1   98
 1
'Merr/Sud S'    'AG'    6567.69   5198.7   6786.23   4848.7   1648   0.0127   1   90
 1
'Merr/Sud W'    'AG'    6576.03   5173.7   6284.09   5013.7   529   0.0127   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'   6492.55   5309.91   6
'Sud/Merr NE2'   6554.76   5268.01   6
'Sud/Merr NE3'   6616.16   5224.93   6
'Sud/Merr NE4'   6604.72   5255.31   6
'Sud/Merr NE5'   6753.29   5285.7   6
'Sud/Merr SE1'   6792.88   5222.3   6
'Sud/Merr SE2'   6724.31   5191.92   6
'Sud/Merr SE3'   6655.74   5161.53   6
'Sud/Merr SE4'   6695.46   5097.91   6
'Sud/Merr SE5'   6735.19   5034.29   6
'Sud/Merr SW1'   6638.58   4981.33   6
'Sud/Merr SW2'   6598.85   5044.95   6
'Sud/Merr SW3'   6559.13   5108.56   6
'Sud/Merr SW4'   6493.36   5072.52   6
'Sud/Merr SW5'   6427.59   5036.47   6
'Sud/Merr NW1'   6347.76   5104.47   6
'Sud/Merr NW2'   6413.53   5140.52   6
'Sud/Merr NW3'   6479.3   5176.56   6
'Sud/Merr NW4'   6417.09   5218.46   6
'Sud/Merr NW5'   6354.88   5260.35   6
'Sud/Sur NE1'   6755.94   5445.69   6
'Sud/Sur NE2'   6800.97   5385.71   6
'Sud/Sur NE3'   6845.99   5325.73   6
'Sud/Sur NE4'   6908.75   5366.8   6
'Sud/Sur NE5'   6971.5   5407.88   6
'Sud/Sur SE1'   7002.41   5368.35   6
'Sud/Sur SE2'   6939.66   5327.28   6
'Sud/Sur SE3'   6876.91   5286.2   6
'Sud/Sur SE4'   6931.69   5234.97   6
'Sud/Sur SE5'   6986.46   5183.75   6
'Sud/Sur SW1'   6932.3   5133.08   6
'Sud/Sur SE2'   6877.52   5184.31   6
'Sud/Sur SE3'   6822.74   5235.54   6
'Sud/Sur SE4'   6754.17   5205.15   6
'Sud/Sur SE5'   6685.61   5174.76   6
'Sud/Sur NW1'   6645.53   5237.94   6
'Sud/Sur NW2'   6714.1   5268.33   6
'Sud/Sur NW3'   6782.66   5298.72   6
'Sud/Sur NW4'   6709.54   5315.38   6
'Sud/Sur NW5'   6636.41   5332.03   6
'Sud/Sur N1'   6642.36   5493.71   6
'Sud/Sur N2'   6687.39   5433.73   6
'Sud/Sur N3'   6732.41   5373.75   6
'Sud/Sur N4'   6659.29   5390.41   6
'Sud/Sur N5'   6586.16   5407.07   6
'2028NB'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   75   3   589   0.03175   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   78   3   481   0.03175   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   46   3   257   0.03175   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   68   3   520   0.03175   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   79   3   468   0.03175   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   229   0.03175   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   254   0.03175   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   0.03175   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   0.03175   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   536   0.03175   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   809   0.03175   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   84   3   106   0.03175   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   50   3   435   0.03175   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   66   3   954   0.03175   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
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100   72   3   837   0.03175   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   0.03175   1600   1   3
 2
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   0.03175   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   928   0.03175   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   921   0.0127   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1336   0.0127   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1354   0.0127   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   940   0.0127   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   863   0.0127   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1593   0.0127   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1023   0.0127   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1636   0.0127   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   901   0.0127   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   488   0.0127   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   0.0127   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   928   0.0127   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   0.0127   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1317   0.0127   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1611   0.0127   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   837   0.0127   1   78
1   0   4   1000   0   'Y'   10   0   36
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2028 Build
Microscale Input Files
(Particulate Matter 2.5 (PM2.5))

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'Government Center Garage'   60   175   0   0   60   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Caus/Wash NE1'   6548.31   7035.9   6
'Caus/Wash NE2'   6581.41   6968.6   6
'Caus/Wash NE3'   6614.5   6901.3   6
'Caus/Wash NE4'   6669.75   6952.02   6
'Caus/Wash NE5'   6725   7002.74   6
'Caus/Wash SE1'   6753.58   6912.24   6
'Caus/Wash SE2'   6698.92   6862.05   6
'Caus/Wash SE3'   6643.09   6810.79   6
'Caus/Wash SE4'   6646.8   6736.4   6
'Caus/Wash SE5'   6649.95   6660.95   6
'Caus/Wash SW1'   6544.02   6561.02   6
'Caus/Wash SW2'   6540.9   6635.95   6
'Caus/Wash SW3'   6537.77   6710.89   6
'Caus/Wash SW4'   6476.83   6667.16   6
'Caus/Wash SW5'   6415.9   6623.44   6
'Caus/Wash NW1'   6407.38   6737.95   6
'Caus/Wash NW2'   6468.31   6781.67   6
'Caus/Wash NW3'   6529.25   6825.39   6
'Caus/Wash NW4'   6496.16   6892.69   6
'Caus/Wash NW5'   6463.06   6960   6
'Tha/Val NE1'   6667.28   6395.45   6
'Tha/Val NE2'   6668.3   6320.45   6
'Tha/Val NE3'   6669.31   6245.46   6
'Tha/Val NE4'   6744.31   6245.46   6
'Tha/Val NE5'   6819.25   6249.58   6
'Tha/Val SE1'   6822.27   6191.64   6
'Tha/Val SE2'   6747.3   6189.58   6
'Tha/Val SE3'   6672.33   6187.52   6
'Tha/Val SE4'   6671.6   6112.53   6
'Tha/Val SE5'   6670.88   6037.53   6
'Tha/Val SW1'   6560.17   5964.68   6
'Tha/Val SW2'   6560.89   6039.67   6
'Tha/Val SW3'   6561.62   6114.67   6
'Tha/Val SW4'   6502.18   6068.93   6
'Tha/Val SW5'   6442.74   6023.18   6
'Tha/Val NW1'   6440.95   6115.18   6
'Tha/Val NW2'   6500.39   6160.92   6
'Tha/Val NW3'   6559.82   6206.67   6
'Tha/Val NW4'   6558.81   6281.66   6
'Tha/Val NW5'   6557.8   6356.65   6
'Build'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   0.03175   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   585   0.03175   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   0.03175   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   0.03175   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   0.03175   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   208   0.03175   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   0.03175   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   0.03175   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2380   0.03175   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
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150   119   3   321   0.03175   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   0.03175   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   748   0.03175   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   0.03175   1600   1   3
 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1705   0.03175   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   0.03175   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   744   0.03175   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1655   0.03175   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   0.03175   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   2013   0.03175   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   542   0.03175   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   459   0.03175   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   636   0.03175   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   1267   0.03175   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   345   0.03175   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   0.03175   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1464   0.0127   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1588   0.0127   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   967   0.0127   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   0.0127   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3453   0.0127   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   0.0127   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2405   0.0127   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   0.0127   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2431   0.0127   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   0.0127   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2871   0.0127   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   0.0127   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2351   0.0127   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   0.0127   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   542   0.0127   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   0.0127   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   459   0.0127   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   729   0.0127   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   0.0127   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1629   0.0127   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1333   0.0127   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1545   0.0127   1   98
 1
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'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   0.0127   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   50   0.3048   1   0
'Bev/Was N1'   6561.96   6150.17   6
'Bev/Was N2'   6561.23   6075.17   6
'Bev/Was N3'   6560.51   6000.18   6
'Bev/Was N4'   6515.8   6060.39   6
'Bev/Was N5'   6471.09   6120.61   6
'Bev/Was SE1'   6670.99   6049.68   6
'Bev/Was SE2'   6670.19   5966.32   6
'Bev/Was SE3'   6624   5907.23   6
'Bev/Was SE4'   6626.07   5832.26   6
'Bev/Was SE5'   6628.13   5757.29   6
'Bev/Was SW1'   6541.84   5766.87   6
'Bev/Was SW2'   6540.09   5841.85   6
'Bev/Was SW3'   6537.71   5916.82   6
'Bev/Was SW4'   6493   5977.03   6
'Bev/Was SW5'   6448.29   6037.25   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Wash/Cong NE1'   6910.24   4571.18   6
'Wash/Cong NE2'   6925.8   4497.81   6
'Wash/Cong NE3'   6941.37   4424.45   6
'Wash/Cong NE4'   7012.01   4449.65   6
'Wash/Cong NE5'   7082.65   4474.85   6
'Wash/Cong SE1'   7095.42   4388.1   6
'Wash/Cong SE2'   7024.78   4362.9   6
'Wash/Cong SE3'   6954.14   4337.69   6
'Wash/Cong SE4'   6968.42   4264.06   6
'Wash/Cong SE5'   6982.69   4190.43   6
'Wash/Cong SW1'   6867.47   4164.74   6
'Wash/Cong SW2'   6853.27   4238.01   6
'Wash/Cong SW3'   6838.93   4312   6
'Wash/Cong SW4'   6765.63   4296.1   6
'Wash/Cong SW5'   6692.34   4280.2   6
'Wash/Cong NW1'   6682.41   4353.77   6
'Wash/Cong NW2'   6755.7   4369.67   6
'Wash/Cong NW3'   6828.9   4386.02   6
'Wash/Cong NW4'   6813.33   4459.38   6
'Wash/Cong NW5'   6797.76   4532.75   6
'Build'   48   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   75   3   376   0.03175   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   75   3   585   0.03175   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   91   3   588   0.03175   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   75   3   308   0.03175   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   97   3   152   0.03175   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   97   3   208   0.03175   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   324   0.03175   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   222   0.03175   1600   1   3
 2
'Caus/Wash SB LTTRR'   'AG'   6548.55   6868.7   6476.41   7018.59   1   40   4
150   94   3   2380   0.03175   1600   1   3
 2
'Caus/Wash WB LLTT'   'AG'   6635.88   6867.75   6716.57   6937.95   1   20   2
150   119   3   321   0.03175   1600   1   3
 2
'Caus/Wash WB R'   'AG'   6624.28   6883.3   6698.77   6952.62   1   10   1
150   104   3   230   0.03175   1600   1   3
 2
'Caus/Wash NB TTR'   'AG'   6603.51   6751.87   6608.73   6635.76   1   20   2
150   120   3   748   0.03175   1600   1   3
 2
'Caus/Wash EB LLTTR'   'AG'   6538.72   6754.84   6450.1   6693.07   1   30   3
150   117   3   422   0.03175   1600   1   3
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 2
'Tha/Val SB LTTR'   'AG'   6598.97   6223.96   6594.55   6338.74   1   20   2
104   30   3   1705   0.03175   1600   1   3
 2
'Tha/Val NB L'   'AG'   6631   6138.62   6630.19   6045.65   1   10   1
104   74   3   472   0.03175   1600   1   3
 2
'Tha/Val NB TR'   'AG'   6645.56   6138.62   6647.18   6045.65   1   10   1
104   30   3   744   0.03175   1600   1   3
 2
'Bev/Was SB TTT'   'AG'   6592.87   5963.93   6593.51   6055.9   1   30   3
100   45   3   1655   0.03175   1600   1   3
 2
'Bev/Was EB RRR'   'AG'   6545.89   5954.26   6500.2   6018.96   1   30   3
100   55   3   356   0.03175   1600   1   3
 2
'Char/93 SB LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   53   3   2013   0.03175   1600   1   3
 2
'Char/93 WB LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   69   3   542   0.03175   1600   1   3
 2
'Char/93 EB TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   69   3   459   0.03175   1600   1   3
 2
'North/Congress SB LT'   'AG'   6876.61   4408.92   6837.72   4601.49   1   30   3
100   90   3   636   0.03175   1600   1   3
 2
'North/Con WB LLTR'   'AG'   6920.59   4378.33   7035.87   4419.12   1   20   2
100   60   3   1267   0.03175   1600   1   3
 2
'Nor/Con NB LTTTR'   'AG'   6914.92   4333.42   6934.22   4190.46   1   30   3
100   74   3   345   0.03175   1600   1   3
 2
'Nor/Con EB LTR'   'AG'   6869.69   4342.19   6796.45   4323.47   1   10   1
100   60   3   17   0.03175   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1464   0.0127   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1588   0.0127   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   967   0.0127   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1486   0.0127   1   78
 1
'Wash/Caus N'   'AG'   6596.92   6812.42   6408.25   7196.09   3453   0.0127   1   90
 1
'Wash/Caus E'   'AG'   6592   6822.26   6793.8   7007.54   1091   0.0127   1   66
 1
'Wash/Caus S'   'AG'   6588.72   6809.14   6603.49   6454.98   2405   0.0127   1   90
 1
'Wash/Caus W'   'AG'   6583.8   6804.22   6263.88   6574.68   1253   0.0127   1   78
 1
'Wash/Tha/Val N'   'AG'   6615.36   6167.26   6611.69   6439.12   2431   0.0127   1   90
 1
'Wash/Tha/Val E'   'AG'   6617.2   6215.02   6951.72   6224.2   39   0.0127   1   38
 1
'Wash/Tha/Val S'   'AG'   6617.42   6197.49   6614.71   5917.32   2871   0.0127   1   90
 1
'Wash/Tha/Val W'   'AG'   6609.85   6198.48   6449.94   6075.41   501   0.0127   1   54
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2351   0.0127   1   66
 1
'Wash/Bev W'   'AG'   6569.64   5930.84   6486.71   6042.54   356   0.0127   1   48
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   542   0.0127   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   903   0.0127   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   459   0.0127   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   729   0.0127   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   457   0.0127   1   42
 1
'North/Congress N'   'AG'   6888.89   4387.54   6808.23   4767.65   1629   0.0127   1   98
 1
'North/Congress East'   'AG'   6893.46   4361.69   7106.52   4437.72   1333   0.0127   1   66
 1
'North/Congress South'   'AG'   6884.56   4386.62   6960.42   3995.27   1545   0.0127   1   98
 1
'North/Congress West'   'AG'   6893.46   4361.69   6745.17   4329.52   47   0.0127   1   54
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   35   0.3048   1   0
'Stan/Lom NE1'   5177.02   6071.23   6
'Stan/Lom NE2'   5219.4   6009.36   6
'Stan/Lom NE3'   5261.78   5947.48   6
'Stan/Lom NE4'   5321.14   5893.32   6
'Stan/Lom NE5'   5380.5   6039.16   6
'Stan/Lom SE1'   5380.37   5915.24   6
'Stan/Lom SE2'   5321.01   5869.4   6
'Stan/Lom SE3'   5261.66   5823.56   6
'Stan/Lom SE4'   5330   5792.67   6
'Stan/Lom SE5'   5400.32   5766.35   6
'Stan/Lom SW1'   5405.83   5659.65   6
'Stan/Lom SW2'   5335.59   5685.94   6
'Stan/Lom SW3'   5265.35   5712.23   6
'Stan/Lom SW4'   5243.19   5640.58   6
'Stan/Lom SW5'   5221.04   5568.92   6
'Stan/Lom NW1'   5144.04   5651.66   6
'Stan/Lom NW2'   5166.2   5723.31   6
'Stan/Lom NW3'   5188.35   5794.97   6
'Stan/Lom NW4'   5181.74   5869.68   6
'Stan/Lom NW5'   5136.51   5935.72   6
'Char/93 NE1'   6625   5871.08   6
'Char/93 NE2'   6627.06   5796.11   6
'Char/93 NE3'   6629.13   5721.14   6
'Char/93 NE4'   6699.75   5695.89   6
'Char/93 NE5'   6750.61   5633.15   6
'Char/93 S1'   6657.79   5466.02   6
'Char/93 S2'   6614.72   5527.42   6
'Char/93 S3'   6571.66   5588.82   6
'Char/93 S4'   6512.89   5542.23   6
'Char/93 S5'   6454.12   5495.63   6
'Char/93 NW1'   6424.08   5632.48   6
'Char/93 NW2'   6483.55   5678.17   6
'Char/93 NW3'   6543.02   5723.87   6
'Char/93 NW4'   6540.96   5798.84   6
'Char/93 NW5'   6538.89   5873.81   6
'Build'   21   1   0   'P'
 2
'Stan/Lom SB L'   'AG'   5194.38   5948.04   5096.76   6092.73   1   10   1
120   79   3   304   0.03175   1600   1   3
 2
'Stan/Lom SB TRR'   'AG'   5173.54   5937.08   5074.83   6078.48   1   20   2
120   79   3   672   0.03175   1600   1   3
 2
'Stan/Lom WB LTT'   'AG'   5306.81   5930.31   5378.66   5989.27   1   20   2
120   71   3   412   0.03175   1600   1   3
 2
'Stan/Lom WB R'   'AG'   5292.44   5947.7   5364.29   6002.87   1   10   1
120   79   3   325   0.03175   1600   1   3
 2
'Stan/Lom NB L'   'AG'   5307.57   5737.36   5403.62   5707.88   1   10   1
120   93   3   70   0.03175   1600   1   3
 2
'Stan/Lom NB TRR'   'AG'   5314.37   5765.33   5412.69   5732.07   1   20   2
120   93   3   331   0.03175   1600   1   3
 2
'Stan/Lom EB LLT'   'AG'   5214.53   5705.34   5182.01   5593.47   1   20   2
120   97   3   439   0.03175   1600   1   3
 2
'Stan/Lom EB R'   'AG'   5236.47   5698.54   5204.7   5586.67   1   10   1
120   97   3   320   0.03175   1600   1   3
 2
'Char/93 SB_LLTTRR'   'AG'   6587.8   5740.03   6583.99   5839.61   1   40   4
100   62   3   1842   0.03175   1600   1   3
 2
'Char/93 WB_LTT'   'AG'   6702.79   5647.77   6767.76   5566.6   1   20   2
100   60   3   334   0.03175   1600   1   3
 2
'Char/93 EB_TTR'   'AG'   6560.75   5622.5   6479.99   5563.39   1   30   3
100   60   3   1159   0.03175   1600   1   3
 1
'Merr/Stan/Cau/Loma N'   'AG'   5250.48   5866.65   4995.32   6239.2   1691   0.0127   1   90
 1
'Merr/Stan/Cau/Loma E'   'AG'   5239.62   5868.45   5518.3   6083.67   1414   0.0127   1   78
 1
'Merr/Stan/Cau/Loma S'   'AG'   5248.67   5770.79   5717.36   5595.37   1247   0.0127   1   78
 1
'Merr/Stan/Cau/Loma W'   'AG'   5232.21   5770.94   5117.19   5398.94   1387   0.0127   1   78
 1
'Wash/Bev S'   'AG'   6585.87   5729.95   6580.46   5926.33   2091   0.0127   1   66
 1
'Char/93 Sumner '   'AG'   6646.79   5711.98   6863.63   5444.55   334   0.0127   1   42
 1
'Char/93 S'   'AG'   6584.18   5677.44   6839.86   5392.52   1059   0.0127   1   48
 1
'Char/93 W EB'   'AG'   6579.66   5642.39   6409.96   5507.84   1159   0.0127   1   54
 1
'Char/93 W WB'   'AG'   6568.34   5696.66   6372.62   5546.28   499   0.0127   1   54
 1
'Char/93 S SW'   'AG'   6596.52   5607.36   6730.38   5416.5   414   0.0127   1   42
 1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028BD'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   530   0.03175   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   74   3   757   0.03175   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   44   3   116   0.03175   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   70   3   1002   0.03175   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   80   3   281   0.03175   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   340   0.03175   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   472   0.03175   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   294   0.03175   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   289   0.03175   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   367   0.03175   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   937   0.03175   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   89   3   104   0.03175   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   41   3   524   0.03175   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   52   3   1232   0.03175   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   76   3   579   0.03175   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   455   0.03175   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   26   0.03175   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   420   0.03175   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   945   0.0127   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1232   0.0127   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1619   0.0127   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   1565   0.0127   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   1016   0.0127   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1651   0.0127   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   964   0.0127   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1759   0.0127   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   360   0.0127   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   541   0.0127   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   455   0.0127   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   420   0.0127   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   26   0.0127   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1848   0.0127   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1944   0.0127   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   579   0.0127   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'   60   175   0   0   40   0.3048   1   0
'Char/Merr NE1'   6063.67   5511.01   6
'Char/Merr NE2'   6133.93   5484.77   6
'Char/Merr NE3'   6204.18   5458.53   6
'Char/Merr NE4'   6265.63   5501.53   6
'Char/Merr NE5'   6327.08   5544.54   6
'Char/Merr SE1'   6443.67   5491.87   6
'Char/Merr SE2'   6382.22   5448.87   6
'Char/Merr SE3'   6320.78   5405.86   6
'Char/Merr SE4'   6380.45   5360.44   6
'Char/Merr SE5'   6440.13   5315.01   6
'Char/Merr SW1'   6331.99   5249.03   6
'Char/Merr SW2'   6272.31   5294.45   6
'Char/Merr SW3'   6212.64   5339.88   6
'Char/Merr SW4'   6141.62   5315.78   6
'Char/Merr SW5'   6070.6   5291.67   6
'Char/Merr NW1'   5902.07   5359.09   6
'Char/Merr NW2'   5973.09   5383.19   6
'Char/Merr NW3'   6044.11   5407.3   6
'Char/Merr NW4'   5973.85   5433.54   6
'Char/Merr NW5'   5903.59   5459.78   6
'Char/Cam NE1'   5490.17   4962.96   6
'Char/Cam NE2'   5458.98   4894.75   6
'Char/Cam NE3'   5427.78   4826.55   6
'Char/Cam NE4'   5500.35   4807.6   6
'Char/Cam NE5'   5572.92   4788.65   6
'Char/Cam SE1'   5553.85   4667.54   6
'Char/Cam SE2'   5481.28   4686.49   6
'Char/Cam SE3'   5408.72   4705.44   6
'Char/Cam SE4'   5409.39   4630.44   6
'Char/Cam SE5'   5410.06   4555.44   6
'Char/Cam SW1'   5312   4561.94   6
'Char/Cam SW2'   5310.65   4636.93   6
'Char/Cam SW3'   5310.65   4711.93   6
'Char/Cam SW4'   5235.65   4712.15   6
'Char/Cam SW5'   5160.65   4711.93   6
'Char/Cam NW1'   5167.9   4822.36   6
'Char/Cam NW2'   5242.9   4822.13   6
'Char/Cam NW3'   5317.9   4821.91   6
'Char/Cam NW4'   5349.09   4890.11   6
'Char/Cam NW5'   5380.28   4958.32   6
'2028BD'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   615   0.03175   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   79   3   517   0.03175   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   52   3   257   0.03175   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   73   3   660   0.03175   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   72   3   679   0.03175   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   233   0.03175   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   301   0.03175   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   0.03175   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   0.03175   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   543   0.03175   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   827   0.03175   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   88   3   106   0.03175   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   52   3   435   0.03175   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   64   3   1094   0.03175   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
100   65   3   992   0.03175   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   0.03175   1600   1   3
 2
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'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   0.03175   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   1075   0.03175   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   989   0.0127   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1538   0.0127   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1494   0.0127   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   1409   0.0127   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   921   0.0127   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1615   0.0127   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1034   0.0127   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1697   0.0127   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   1032   0.0127   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   504   0.0127   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   0.0127   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   1075   0.0127   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   0.0127   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1457   0.0127   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1759   0.0127   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   992   0.0127   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55   5309.91   6
'Sud/Merr NE2'    6554.76   5268.01   6
'Sud/Merr NE3'    6616.16   5224.93   6
'Sud/Merr NE4'    6604.72   5255.31   6
'Sud/Merr NE5'    6753.29   5285.7    6
'Sud/Merr SE1'    6792.88   5222.3    6
'Sud/Merr SE2'    6724.31   5191.92   6
'Sud/Merr SE3'    6655.74   5161.53   6
'Sud/Merr SE4'    6695.46   5097.91   6
'Sud/Merr SE5'    6735.19   5034.29   6
'Sud/Merr SW1'    6638.58   4981.33   6
'Sud/Merr SW2'    6598.85   5044.95   6
'Sud/Merr SW3'    6559.13   5108.56   6
'Sud/Merr SW4'    6493.36   5072.52   6
'Sud/Merr SW5'    6427.59   5036.47   6
'Sud/Merr NW1'    6347.76   5104.47   6
'Sud/Merr NW2'    6413.53   5140.52   6
'Sud/Merr NW3'    6479.3    5176.56   6
'Sud/Merr NW4'    6417.09   5218.46   6
'Sud/Merr NW5'    6354.88   5260.35   6
'Sud/Sur NE1'    6755.94   5445.69   6
'Sud/Sur NE2'    6800.97   5385.71   6
'Sud/Sur NE3'    6845.99   5325.73   6
'Sud/Sur NE4'    6908.75   5366.8    6
'Sud/Sur NE5'    6971.5    5407.88   6
'Sud/Sur SE1'    7002.41   5368.35   6
'Sud/Sur SE2'    6939.66   5327.28   6
'Sud/Sur SE3'    6876.91   5286.2    6
'Sud/Sur SE4'    6931.69   5234.97   6
'Sud/Sur SE5'    6986.46   5183.75   6
'Sud/Sur SW1'    6932.3    5133.08   6
'Sud/Sur SE2'    6877.52   5184.31   6
'Sud/Sur SE3'    6822.74   5235.54   6
'Sud/Sur SE4'    6754.17   5205.15   6
'Sud/Sur SE5'    6685.61   5174.76   6
'Sud/Sur NW1'    6645.53   5237.94   6
'Sud/Sur NW2'    6714.1    5268.33   6
'Sud/Sur NW3'    6782.66   5298.72   6
'Sud/Sur NW4'    6709.54   5315.38   6
'Sud/Sur NW5'    6636.41   5332.03   6
'Sud/Sur N1'    6642.36   5493.71   6
'Sud/Sur N2'    6687.39   5433.73   6
'Sud/Sur N3'    6732.41   5373.75   6
'Sud/Sur N4'    6659.29   5390.41   6
'Sud/Sur N5'    6586.16   5407.07   6
'2028BD'    34   1   0   'P'
 2
'Char/Merr SB'    'AG'    6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   530   0.03175   1600   1   3
 2
'Char/Merr WB'    'AG'    6250.42   5435.24   6385.37   5541.98   1   30   3
100   74   3   757   0.03175   1600   1   3
 2
'Char/Merr NB R'    'AG'    6291.66   5369.7   6396.62   5298.54   1   10   1
100   44   3   116   0.03175   1600   1   3
 2
'Char/Merr NB LTT'    'AG'    6280.41   5347.23   6376   5279.81   1   20   2
100   70   3   1002   0.03175   1600   1   3
 2
'Char/Merr EB'    'AG'    6104.22   5362.21   5928.03   5296.67   1   20   2
100   80   3   281   0.03175   1600   1   3
 2
'Char/Cam SB L'    'AG'    5384.06   4834.19   5405.87   4921.31   1   10   1
90   58   3   340   0.03175   1600   1   3
 2
'Char/Cam SB TR'    'AG'    5360.81   4833.46   5388.43   4922.76   1   20   2
90   71   3   472   0.03175   1600   1   3
 2
'Char/Cam WB LTTR'    'AG'    5410.95   4793.53   5564.29   4757.95   1   20   2
90   54   3   294   0.03175   1600   1   3
 2
'Char/Cam NB L'    'AG'    5362.99   4722.37   5360.81   4625.08   1   10   1
90   58   3   289   0.03175   1600   1   3
 2
'Char/Cam NB TR'    'AG'    5383.34   4723.83   5384.79   4624.36   1   20   2
90   71   3   367   0.03175   1600   1   3
 2
'Char/Cam EB TTTR'    'AG'    5302.67   4739.8   5163.87   4741.25   1   30   3
90   54   3   937   0.03175   1600   1   3
 2
'Sud/Merr SB L'    'AG'    6532.74   5210.31   6469.76   5255.15   1   10   1
100   89   3   104   0.03175   1600   1   3
 2
'Sud/Merr SB TTT'    'AG'    6518.26   5190.78   6450.94   5229.84   1   30   3
100   41   3   524   0.03175   1600   1   3
 2
'Sud/Merr NB TTTR'    'AG'    6621.05   5161.13   6684.76   5049.03   1   30   3
100   52   3   1232   0.03175   1600   1   3
 2
'Sud/Merr EB LTTR'    'AG'    6523.33   5145.94   6435.74   5093.15   1   40   4
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100   76   3   579   0.03175   1600   1   3
 2
'Sud/Sur SB LTT'    'AG'    6777.46   5369.67   6709.4   5455.47   1   20   2
100   53   3   455   0.03175   1600   1   3
 2
'Sud/Sur SEB'    'AG'    6757.21   5330.01   6705.35   5342.96   1   10   1
100   70   3   26   0.03175   1600   1   3
 2
'Sud/Sur EB TTR'    'AG'    6794.47   5259.59   6672.95   5211.83   1   30   3
100   77   3   420   0.03175   1600   1   3
 1
'Char/Merr N'    'AG'    6202.34   5403.71   5845.34   5537.04   945   0.0127   1   84
 1
'Char/Merr E'    'AG'    6201.86   5389.77   6552.37   5635.08   1232   0.0127   1   90
 1
'Char/Merr S'    'AG'    6214.99   5412.24   6411.79   5262.43   1619   0.0127   1   98
 1
'Char/Merr W'    'AG'    6198.12   5397.26   5806.38   5264.31   1565   0.0127   1   98
 1
'Char/Camb N'    'AG'    5352.47   4779.69   5466.46   5028.93   1016   0.0127   1   78
 1
'Char/Camb E'    'AG'    5334.74   4787.8   5780.86   4671.3   1651   0.0127   1   102
 1
'Char/Camb S'    'AG'    5359.22   4760.44   5362.39   4406.78   964   0.0127   1   78
 1
'Char/Camb W'    'AG'    5364.5   4766.77   5009.45   4767.83   1759   0.0127   1   90
 1
'Sur/Sud E'    'AG'    6831.79   5286.55   6967.42   5375.33   360   0.0127   1   30
 1
'Sur/Sud S'    'AG'    6823.37   5285.61   7028.22   5094.04   541   0.0127   1   54
 1
'Sur/Sud N'    'AG'    6816.26   5313.7   6641.09   5547.04   455   0.0127   1   42
 1
'Sur/Sud W'    'AG'    6584.37   5170.37   6806.25   5268.7   420   0.0127   1   54
 1
'Sur/Sud NW'    'AG'    6797.91   5327.04   6702.82   5348.7   26   0.0127   1   42
 1
'Merr/Sud N'    'AG'    6569.36   5187.04   6420.88   5287.04   1848   0.0127   1   98
 1
'Merr/Sud S'    'AG'    6567.69   5198.7   6786.23   4848.7   1944   0.0127   1   90
 1
'Merr/Sud W'    'AG'    6576.03   5173.7   6284.09   5013.7   579   0.0127   1   78
1   0   4   1000   0   'Y'   10   0   36
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'Government Center Garage'    60   175   0   0   45   0.3048   1   0
'Sud/Merr NE1'    6492.55   5309.91   6
'Sud/Merr NE2'    6554.76   5268.01   6
'Sud/Merr NE3'    6616.16   5224.93   6
'Sud/Merr NE4'    6604.72   5255.31   6
'Sud/Merr NE5'    6753.29   5285.7   6
'Sud/Merr SE1'    6792.88   5222.3   6
'Sud/Merr SE2'    6724.31   5191.92   6
'Sud/Merr SE3'    6655.74   5161.53   6
'Sud/Merr SE4'    6695.46   5097.91   6
'Sud/Merr SE5'    6735.19   5034.29   6
'Sud/Merr SW1'    6638.58   4981.33   6
'Sud/Merr SW2'    6598.85   5044.95   6
'Sud/Merr SW3'    6559.13   5108.56   6
'Sud/Merr SW4'    6493.36   5072.52   6
'Sud/Merr SW5'    6427.59   5036.47   6
'Sud/Merr NW1'    6347.76   5104.47   6
'Sud/Merr NW2'    6413.53   5140.52   6
'Sud/Merr NW3'    6479.3   5176.56   6
'Sud/Merr NW4'    6417.09   5218.46   6
'Sud/Merr NW5'    6354.88   5260.35   6
'Sud/Sur NE1'   6755.94   5445.69   6
'Sud/Sur NE2'   6800.97   5385.71   6
'Sud/Sur NE3'   6845.99   5325.73   6
'Sud/Sur NE4'   6908.75   5366.8   6
'Sud/Sur NE5'   6971.5   5407.88   6
'Sud/Sur SE1'   7002.41   5368.35   6
'Sud/Sur SE2'   6939.66   5327.28   6
'Sud/Sur SE3'   6876.91   5286.2   6
'Sud/Sur SE4'   6931.69   5234.97   6
'Sud/Sur SE5'   6986.46   5183.75   6
'Sud/Sur SW1'   6932.3   5133.08   6
'Sud/Sur SE2'   6877.52   5184.31   6
'Sud/Sur SE3'   6822.74   5235.54   6
'Sud/Sur SE4'   6754.17   5205.15   6
'Sud/Sur SE5'   6685.61   5174.76   6
'Sud/Sur NW1'   6645.53   5237.94   6
'Sud/Sur NW2'   6714.1   5268.33   6
'Sud/Sur NW3'   6782.66   5298.72   6
'Sud/Sur NW4'   6709.54   5315.38   6
'Sud/Sur NW5'   6636.41   5332.03   6
'Sud/Sur N1'   6642.36   5493.71   6
'Sud/Sur N2'   6687.39   5433.73   6
'Sud/Sur N3'   6732.41   5373.75   6
'Sud/Sur N4'   6659.29   5390.41   6
'Sud/Sur N5'   6586.16   5407.07   6
'2028BD'   34   1   0   'P'
 2
'Char/Merr SB'   'AG'   6111.61   5425.13   5935.42   5488.8   1   30   3
100   76   3   615   0.03175   1600   1   3
 2
'Char/Merr WB'   'AG'   6250.42   5435.24   6385.37   5541.98   1   30   3
100   79   3   517   0.03175   1600   1   3
 2
'Char/Merr NB R'   'AG'   6291.66   5369.7   6396.62   5298.54   1   10   1
100   52   3   257   0.03175   1600   1   3
 2
'Char/Merr NB LTT'   'AG'   6280.41   5347.23   6376   5279.81   1   20   2
100   73   3   660   0.03175   1600   1   3
 2
'Char/Merr EB'   'AG'   6104.22   5362.21   5928.03   5296.67   1   20   2
100   72   3   679   0.03175   1600   1   3
 2
'Char/Cam SB L'   'AG'   5384.06   4834.19   5405.87   4921.31   1   10   1
100   60   3   233   0.03175   1600   1   3
 2
'Char/Cam SB TR'   'AG'   5360.81   4833.46   5388.43   4922.76   1   20   2
100   72   3   301   0.03175   1600   1   3
 2
'Char/Cam WB LTTR'   'AG'   5410.95   4793.53   5564.29   4757.95   1   20   2
100   62   3   435   0.03175   1600   1   3
 2
'Char/Cam NB L'   'AG'   5362.99   4722.37   5360.81   4625.08   1   10   1
100   60   3   299   0.03175   1600   1   3
 2
'Char/Cam NB TR'   'AG'   5383.34   4723.83   5384.79   4624.36   1   20   2
100   72   3   543   0.03175   1600   1   3
 2
'Char/Cam EB TTTR'   'AG'   5302.67   4739.8   5163.87   4741.25   1   30   3
100   62   3   827   0.03175   1600   1   3
 2
'Sud/Merr SB L'   'AG'   6532.74   5210.31   6469.76   5255.15   1   10   1
100   88   3   106   0.03175   1600   1   3
 2
'Sud/Merr SB TTT'   'AG'   6518.26   5190.78   6450.94   5229.84   1   30   3
100   52   3   435   0.03175   1600   1   3
 2
'Sud/Merr NB TTTR'   'AG'   6621.05   5161.13   6684.76   5049.03   1   30   3
100   64   3   1094   0.03175   1600   1   3
 2
'Sud/Merr EB LTTR'   'AG'   6523.33   5145.94   6435.74   5093.15   1   40   4
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100   65   3   992   0.03175   1600   1   3
 2
'Sud/Sur SB LTT'   'AG'   6777.46   5369.67   6709.4   5455.47   1   20   2
100   70   3   424   0.03175   1600   1   3
 2
'Sud/Sur SEB'   'AG'   6757.21   5330.01   6705.35   5342.96   1   10   1
100   80   3   37   0.03175   1600   1   3
 2
'Sud/Sur EB TTR'   'AG'   6794.47   5259.59   6672.95   5211.83   1   30   3
100   50   3   1075   0.03175   1600   1   3
 1
'Char/Merr N'   'AG'   6202.34   5403.71   5845.34   5537.04   989   0.0127   1   84
 1
'Char/Merr E'   'AG'   6201.86   5389.77   6552.37   5635.08   1538   0.0127   1   90
 1
'Char/Merr S'   'AG'   6214.99   5412.24   6411.79   5262.43   1494   0.0127   1   98
 1
'Char/Merr W'   'AG'   6198.12   5397.26   5806.38   5264.31   1409   0.0127   1   98
 1
'Char/Camb N'   'AG'   5352.47   4779.69   5466.46   5028.93   921   0.0127   1   78
 1
'Char/Camb E'   'AG'   5334.74   4787.8   5780.86   4671.3   1615   0.0127   1   102
 1
'Char/Camb S'   'AG'   5359.22   4760.44   5362.39   4406.78   1034   0.0127   1   78
 1
'Char/Camb W'   'AG'   5364.5   4766.77   5009.45   4767.83   1697   0.0127   1   90
 1
'Sur/Sud E'   'AG'   6831.79   5286.55   6967.42   5375.33   1032   0.0127   1   30
 1
'Sur/Sud S'   'AG'   6823.37   5285.61   7028.22   5094.04   504   0.0127   1   54
 1
'Sur/Sud N'   'AG'   6816.26   5313.7   6641.09   5547.04   424   0.0127   1   42
 1
'Sur/Sud W'   'AG'   6584.37   5170.37   6806.25   5268.7   1075   0.0127   1   54
 1
'Sur/Sud NW'   'AG'   6797.91   5327.04   6702.82   5348.7   37   0.0127   1   42
 1
'Merr/Sud N'   'AG'   6569.36   5187.04   6420.88   5287.04   1457   0.0127   1   98
 1
'Merr/Sud S'   'AG'   6567.69   5198.7   6786.23   4848.7   1759   0.0127   1   90
 1
'Merr/Sud W'   'AG'   6576.03   5173.7   6284.09   5013.7   992   0.0127   1   78
1   0   4   1000   0   'Y'   10   0   36
```

Microscale (CAL3QHC) Output Files

- **2013 Existing**
- **2028 No-Build Condition**
- **2028 Build Condition**

2013 Existing Microscale Output Files (Carbon Monoxide (CO))

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:39:25

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT)				*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
		X1	Y1	X2	Y2										
1. Stan/Lom SB L	*	5194.4	5948.0	5135.6	6035.2	*	105.	326.	AG	113.	100.0	1.0	10.0	0.84	5.3
2. Stan/Lom SB TRR	*	5173.5	5937.1	5122.0	6010.9	*	90.	325.	AG	214.	100.0	1.0	20.0	0.71	4.6
3. Stan/Lom WB LTT	*	5306.8	5930.3	5403.5	6009.6	*	125.	51.	AG	220.	100.0	1.0	20.0	0.87	6.4
4. Stan/Lom WB R	*	5292.4	5947.7	5347.6	5990.1	*	70.	52.	AG	78.	100.0	1.0	10.0	0.40	3.5
5. Stan/Lom NB L	*	5307.6	5737.4	5359.5	5721.4	*	54.	107.	AG	113.	100.0	1.0	10.0	0.53	2.8
6. Stan/Lom NB TRR	*	5314.4	5765.3	5342.7	5755.7	*	30.	109.	AG	214.	100.0	1.0	20.0	0.25	1.5
7. Stan/Lom EB LLT	*	5214.5	5705.3	5200.8	5658.2	*	49.	196.	AG	220.	100.0	1.0	20.0	0.44	2.5
8. Stan/Lom EB R	*	5236.5	5698.5	5221.6	5646.0	*	55.	196.	AG	78.	100.0	1.0	10.0	0.32	2.8
9. Caus/Wash SB LTTRR	*	6548.6	6868.7	6475.2	7021.0	*	169.	334.	AG	218.	100.0	1.0	40.0	0.58	8.6
10. Caus/Wash WB LLTT	*	6635.9	6867.8	6714.6	6936.2	*	104.	49.	AG	243.	100.0	1.0	20.0	0.69	5.3
11. Caus/Wash WB R	*	6624.3	6883.3	6687.4	6942.0	*	86.	47.	AG	71.	100.0	1.0	10.0	0.28	4.4
12. Caus/Wash NB TTR	*	6603.5	6751.9	6613.9	6519.8	*	232.	177.	AG	210.	100.0	1.0	20.0	0.88	11.8
13. Caus/Wash EB LLTTR	*	6538.7	6754.8	6469.9	6706.8	*	84.	235.	AG	347.	100.0	1.0	30.0	0.47	4.3
14. Tha/Val SB LTTR	*	6599.0	6224.0	6593.3	6370.2	*	146.	358.	AG	99.	100.0	1.0	20.0	0.81	7.4
15. Tha/Val NB L	*	6631.0	6138.6	6630.2	6047.3	*	91.	180.	AG	96.	100.0	1.0	10.0	0.55	4.6
16. Tha/Val NB TR	*	6645.6	6138.6	6648.0	6000.5	*	138.	179.	AG	50.	100.0	1.0	10.0	0.76	7.0
17. Bev/Was SB TTT	*	6592.9	5963.9	6593.7	6089.2	*	125.	0.	AG	197.	100.0	1.0	30.0	0.64	6.4
18. Bev/Was EB RRR	*	6545.9	5954.3	6530.5	5976.1	*	27.	325.	AG	241.	100.0	1.0	30.0	0.14	1.4
19. Char/93 SB LLTTRR	*	6587.8	5740.0	6582.8	5870.1	*	130.	358.	AG	309.	100.0	1.0	40.0	0.67	6.6
20. Char/93 WB LTT	*	6702.8	5647.8	6712.2	5636.0	*	15.	141.	AG	201.	100.0	1.0	20.0	0.10	0.8
21. Char/93 EB TTR	*	6560.8	5622.5	6523.0	5594.9	*	47.	234.	AG	302.	100.0	1.0	30.0	0.30	2.4
22. North/Congress SB LT	*	6876.6	4408.9	6860.5	4488.9	*	82.	349.	AG	328.	100.0	1.0	30.0	0.62	4.1
23. North/Con WB LLTR	*	6920.6	4378.3	7073.6	4432.5	*	162.	71.	AG	175.	100.0	1.0	20.0	0.82	8.2
24. Nor/Con NB LTTTR	*	6914.9	4333.4	6920.4	4292.5	*	41.	172.	AG	324.	100.0	1.0	30.0	0.30	2.1
25. Nor/Con EB LTR	*	6869.7	4342.2	6864.6	4340.9	*	5.	256.	AG	88.	100.0	1.0	10.0	0.03	0.3
26. Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1120.	9.8	1.0	90.0		
27. Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1275.	9.8	1.0	78.0		
28. Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	817.	9.8	1.0	78.0		
29. Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1322.	9.8	1.0	78.0		
30. Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3211.	9.8	1.0	90.0		
31. Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1012.	9.8	1.0	66.0		
32. Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2221.	9.8	1.0	90.0		
33. Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1162.	9.8	1.0	78.0		
34. Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2247.	9.8	1.0	90.0		
35. Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	91.	9.8	1.0	38.0		
36. Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2524.	9.8	1.0	90.0		
37. Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	280.	9.8	1.0	54.0		
38. Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	1841.	9.8	1.0	66.0		
39. Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	269.	9.8	1.0	48.0		
40. Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	80.	9.8	1.0	42.0		
41. Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	811.	9.8	1.0	48.0		
42. Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	374.	9.8	1.0	54.0		
43. Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	650.	9.8	1.0	54.0		

44. Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	406.	9.8	1.0	42.0		

JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:39:25

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT)				*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
		X1	Y1	X2	Y2										
45. North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1226.	9.8	1.0	98.0		
46. North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	978.	9.8	1.0	66.0		
47. North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1420.	9.8	1.0	98.0		
48. North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	44.	9.8	1.0	54.0		

JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:39:25

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. Stan/Lom SB L	*	90	70	3.0	223	1600	54.39	1	3
2. Stan/Lom SB TRR	*	90	66	3.0	481	1600	54.39	1	3
3. Stan/Lom WB LTT	*	90	68	3.0	527	1600	54.39	1	3
4. Stan/Lom WB R	*	90	48	3.0	265	1600	54.39	1	3
5. Stan/Lom NB L	*	90	70	3.0	142	1600	54.39	1	3
6. Stan/Lom NB TRR	*	90	66	3.0	166	1600	54.39	1	3
7. Stan/Lom EB LLT	*	90	68	3.0	265	1600	54.39	1	3
8. Stan/Lom EB R	*	90	48	3.0	208	1600	54.39	1	3
9. Caus/Wash SB LTTRR	*	150	56	3.0	2210	1600	54.39	1	3
10. Caus/Wash WB LLTT	*	150	125	3.0	296	1600	54.39	1	3
11. Caus/Wash WB R	*	150	73	3.0	216	1600	54.39	1	3
12. Caus/Wash NB TTR	*	150	108	3.0	693	1600	54.39	1	3
13. Caus/Wash EB LLTTR	*	150	119	3.0	388	1600	54.39	1	3
14. Tha/Val SB LTTR	*	100	34	3.0	1575	1600	54.39	1	3
15. Tha/Val NB L	*	100	66	3.0	253	1600	54.39	1	3
16. Tha/Val NB TR	*	100	34	3.0	743	1600	54.39	1	3
17. Bev/Was SB TTT	*	100	45	3.0	1528	1600	54.39	1	3
18. Bev/Was EB RRR	*	100	55	3.0	269	1600	54.39	1	3
19. Char/93 SB LLTTRR	*	100	53	3.0	1797	1600	54.39	1	3
20. Char/93 WB LTT	*	100	69	3.0	80	1600	54.39	1	3
21. Char/93 EB TTR	*	100	69	3.0	374	1600	54.39	1	3
22. North/Congress SB LT	*	100	75	3.0	598	1600	54.39	1	3
23. North/Con WB LLTR	*	100	60	3.0	916	1600	54.39	1	3
24. Nor/Con NB LTTTR	*	100	74	3.0	306	1600	54.39	1	3
25. Nor/Con EB LTR	*	100	60	3.0	16	1600	54.39	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2. Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3. Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4. Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5. Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6. Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7. Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8. Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9. Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10. Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11. Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12. Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13. Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14. Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15. Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16. Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17. Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18. Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19. Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20. Stan/Lom NW5	*	5136.5	5935.7	6.0	*

JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:39:25

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
21. Caus/Wash NE1	6548.3	7035.9	6.0
22. Caus/Wash NE2	6581.4	6968.6	6.0
23. Caus/Wash NE3	6614.5	6901.3	6.0
24. Caus/Wash NE4	6669.8	6952.0	6.0
25. Caus/Wash NE5	6725.0	7002.7	6.0
26. Caus/Wash SE1	6753.6	6912.2	6.0
27. Caus/Wash SE2	6698.9	6862.0	6.0
28. Caus/Wash SE3	6643.1	6810.8	6.0
29. Caus/Wash SE4	6646.8	6736.4	6.0
30. Caus/Wash SE5	6650.0	6661.0	6.0
31. Caus/Wash SW1	6544.0	6561.0	6.0
32. Caus/Wash SW2	6540.9	6636.0	6.0
33. Caus/Wash SW3	6537.8	6710.9	6.0
34. Caus/Wash SW4	6476.8	6667.2	6.0
35. Caus/Wash SW5	6415.9	6623.4	6.0
36. Caus/Wash NW1	6407.4	6738.0	6.0
37. Caus/Wash NW2	6468.3	6781.7	6.0
38. Caus/Wash NW3	6529.3	6825.4	6.0
39. Caus/Wash NW4	6496.2	6892.7	6.0
40. Caus/Wash NW5	6463.1	6960.0	6.0
41. Tha/Val NE1	6667.3	6395.5	6.0
42. Tha/Val NE2	6668.3	6320.5	6.0
43. Tha/Val NE3	6669.3	6245.5	6.0
44. Tha/Val NE4	6744.3	6245.5	6.0
45. Tha/Val NE5	6819.2	6249.6	6.0
46. Tha/Val SE1	6822.3	6191.6	6.0
47. Tha/Val SE2	6747.3	6189.6	6.0
48. Tha/Val SE3	6672.3	6187.5	6.0
49. Tha/Val SE4	6671.6	6112.5	6.0
50. Tha/Val SE5	6670.9	6037.5	6.0
51. Tha/Val SW1	6560.2	5964.7	6.0
52. Tha/Val SW2	6560.9	6039.7	6.0
53. Tha/Val SW3	6561.6	6114.7	6.0
54. Tha/Val SW4	6502.2	6068.9	6.0
55. Tha/Val SW5	6442.7	6023.2	6.0
56. Tha/Val NW1	6441.0	6115.2	6.0
57. Tha/Val NW2	6500.4	6160.9	6.0
58. Tha/Val NW3	6559.8	6206.7	6.0
59. Tha/Val NW4	6558.8	6281.7	6.0
60. Tha/Val NW5	6557.8	6356.7	6.0

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.0	0.0	0.0	0.0	0.0	0.6	0.7	0.5	0.4	0.2	0.4	0.7	0.5	0.7	0.7	0.2	0.2	0.4	0.6	0.8
10.	0.0	0.0	0.0	0.0	0.0	0.6	0.7	0.5	0.4	0.1	0.3	0.6	0.6	0.5	0.5	0.2	0.1	0.2	0.5	0.9
20.	0.0	0.0	0.0	0.0	0.0	0.5	0.7	0.6	0.3	0.1	0.2	0.5	0.5	0.4	0.4	0.4	0.3	0.3	0.3	0.9
30.	0.0	0.0	0.0	0.0	0.0	0.5	0.6	0.6	0.2	0.0	0.2	0.4	0.5	0.3	0.3	0.5	0.5	0.4	0.3	0.9
40.	0.0	0.0	0.1	0.1	0.0	0.3	0.5	0.6	0.1	0.0	0.2	0.3	0.4	0.2	0.1	0.6	0.5	0.5	0.5	0.9
50.	0.0	0.0	0.4	0.1	0.1	0.2	0.3	0.4	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.8	0.4	0.5	0.7	0.9
60.	0.0	0.0	0.6	0.4	0.2	0.1	0.1	0.1	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.7	0.5	0.3	0.9	0.9
70.	0.0	0.1	0.8	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.8	0.4	0.1	0.7	1.0
80.	0.0	0.2	0.9	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.1	0.1	0.7	0.5	0.1	0.6	1.0
90.	0.1	0.3	0.9	0.9	0.4	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.1	0.0	0.5	0.5	0.1	0.4	0.8
100.	0.2	0.4	0.8	0.9	0.3	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.1	0.0	0.5	0.6	0.3	0.2	0.7
110.	0.2	0.5	0.5	0.8	0.3	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.0	0.0	0.3	0.6	0.5	0.3	0.5
120.	0.2	0.4	0.4	0.9	0.3	0.0	0.1	0.3	0.3	0.2	0.1	0.1	0.1	0.0	0.0	0.3	0.7	0.4	0.3	0.4
130.	0.2	0.4	0.5	0.9	0.4	0.0	0.1	0.4	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.7	0.3	0.3	0.4

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
140.	0.4	0.5	0.4	1.0	0.5	0.1	0.1	0.4	0.4	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.6	0.4	0.2	0.2
150.	0.4	0.4	0.5	1.0	0.7	0.1	0.1	0.4	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.4	0.2	0.2
160.	0.4	0.4	0.5	1.0	0.8	0.1	0.2	0.2	0.6	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.5	0.5	0.2	0.1
170.	0.6	0.5	0.5	1.0	0.8	0.1	0.2	0.3	0.6	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.5	0.5	0.3	0.2
180.	0.6	0.5	0.7	1.0	0.9	0.1	0.2	0.3	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.3	0.1
190.	0.7	0.4	0.7	1.1	1.1	0.1	0.3	0.5	0.7	0.2	0.0	0.0	0.1	0.1	0.1	0.3	0.4	0.5	0.2	0.1
200.	0.6	0.6	0.6	0.9	1.0	0.2	0.3	0.6	0.7	0.2	0.0	0.0	0.3	0.3	0.2	0.2	0.2	0.2	0.1	0.0
210.	0.6	0.5	0.5	0.7	1.0	0.2	0.4	0.5	0.6	0.3	0.0	0.1	0.6	0.4	0.3	0.1	0.1	0.1	0.0	0.0
220.	0.5	0.6	0.4	0.5	0.8	0.2	0.2	0.2	0.7	0.4	0.0	0.1	0.6	0.4	0.4	0.0	0.0	0.0	0.0	0.0
230.	0.5	0.6	0.4	0.3	0.5	0.2	0.1	0.1	0.6	0.5	0.1	0.2	0.7	0.4	0.4	0.0	0.0	0.0	0.0	0.0
240.	0.3	0.7	0.3	0.3	0.2	0.2	0.1	0.1	0.5	0.7	0.1	0.2	0.8	0.4	0.4	0.0	0.0	0.0	0.0	0.0
250.	0.3	0.6	0.4	0.3	0.2	0.4	0.1	0.0	0.4	0.6	0.1	0.3	0.8	0.4	0.4	0.0	0.0	0.0	0.0	0.0
260.	0.3	0.6	0.4	0.4	0.2	0.4	0.3	0.0	0.2	0.6	0.1	0.3	0.5	0.3	0.3	0.0	0.0	0.0	0.0	0.0
270.	0.3	0.6	0.6	0.4	0.1	0.7	0.3	0.0	0.2	0.5	0.2	0.3	0.4	0.3	0.3	0.0	0.0	0.0	0.0	0.0
280.	0.3	0.5	0.6	0.4	0.1	0.8	0.5	0.0	0.1	0.3	0.2	0.3	0.4	0.5	0.3	0.0	0.0	0.0	0.0	0.0
290.	0.3	0.4	0.6	0.2	0.1	0.8	0.6	0.1	0.0	0.2	0.2	0.3	0.3	0.6	0.3	0.0	0.0	0.0	0.0	0.0
300.	0.3	0.3	0.6	0.1	0.1	0.9	0.7	0.1	0.1	0.2	0.4	0.2	0.3	0.7	0.3	0.0	0.0	0.0	0.0	0.0
310.	0.3	0.3	0.5	0.1	0.0	0.8	0.8	0.3	0.4	0.4	0.5	0.3	0.3	0.7	0.3	0.0	0.0	0.0	0.0	0.0
320.	0.2	0.3	0.3	0.0	0.0	0.8	0.5	0.5	0.4	0.2	0.5	0.3	0.5	0.8	0.3	0.0	0.0	0.0	0.2	0.1
330.	0.1	0.1	0.1	0.0	0.0	0.6	0.5	0.7	0.4	0.3	0.6	0.7	0.5	1.0	0.5	0.0	0.0	0.2	0.5	0.3
340.	0.0	0.0	0.1	0.0	0.0	0.6	0.4	0.6	0.4	0.2	0.5	0.6	0.6	0.9	0.6	0.0	0.1	0.3	0.8	0.5
350.	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.5	0.3	0.2	0.4	0.7	0.4	0.6	0.6	0.1	0.2	0.4	0.8	0.7
360.	0.0	0.0	0.0	0.0	0.0	0.6	0.7	0.5	0.4	0.2	0.4	0.7	0.5	0.7	0.7	0.2	0.2	0.4	0.6	0.8
MAX	0.7	0.7	0.9	1.1	1.1	0.9	0.8	0.7	0.7	0.7	0.6	0.7	0.8	1.0	0.7	0.8	0.7	0.5	0.9	1.0
DEGR.	190	240	80	190	190	300	310	330	200	240	330	0	240	330	0	50	120	40	60	70

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.0	0.1	0.1	0.0	0.0	0.3	0.7	0.8	0.7	0.6	1.0	1.2	1.8	1.3	0.6	0.2	0.6	1.5	1.6	1.1
10.	0.0	0.0	0.0	0.0	0.0	0.3	0.6	0.8	0.5	0.3	1.3	1.2	1.5	1.5	0.8	0.4	0.7	1.4	1.5	1.3
20.	0.0	0.0	0.0	0.0	0.0	0.2	0.5	0.7	0.2	0.2	1.1	1.2	1.6	1.7	1.0	0.4	0.8	1.2	1.5	1.4
30.	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.6	0.2	0.0	1.0	1.1	1.3	1.6	1.1	0.5	0.7	1.0	1.4	1.3
40.	0.0	0.0	0.1	0.1	0.0	0.1	0.2	0.4	0.0	0.0	0.9	1.0	1.2	1.4	1.1	0.4	0.8	1.0	1.3	1.2
50.	0.0	0.0	0.4	0.1	0.0	0.1	0.1	0.2	0.0	0.0	0.9	0.9	1.0	1.1	1.0	0.7	0.8	1.0	1.2	1.2
60.	0.0	0.0	0.6	0.2	0.1	0.0	0.0	0.1	0.0	0.0	0.8	0.8	0.7	0.6	0.5	0.7	0.8	1.3	1.5	1.3
70.	0.0	0.0	0.8	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.7	0.5	0.3	0.9	0.8	1.2	1.5	1.3

```
  80.  *   0.0   0.1   0.9   0.3   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   0.9   0.8   1.1
1.4   1.3
  90.  *   0.0   0.1   1.0   0.4   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   1.1   0.8   1.0
1.5   1.5
 100.  *   0.1   0.2   1.0   0.4   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   1.1   0.9   0.9
1.5   1.6
 110.  *   0.1   0.3   1.0   0.5   0.2   0.0   0.0   0.0   0.0   0.0   0.7   0.8   0.8   0.5   0.3   1.0   1.0   1.0
1.4   1.7
 120.  *   0.2   0.4   0.7   0.6   0.2   0.0   0.0   0.0   0.0   0.0   0.7   0.8   0.8   0.5   0.3   0.8   1.2   1.0
1.2   1.7
 130.  *   0.3   0.4   0.8   0.8   0.3   0.0   0.0   0.0   0.0   0.0   0.7   0.9   0.9   0.4   0.3   0.7   1.3   1.1
1.2   1.6
 140.  *   0.3   0.5   0.7   0.8   0.3   0.0   0.0   0.0   0.0   0.0   0.6   0.8   0.9   0.5   0.3   0.7   1.4   1.2
1.1   1.5
 150.  *   0.6   0.5   0.7   0.9   0.3   0.0   0.0   0.0   0.0   0.0   0.7   0.9   1.1   0.3   0.3   0.5   1.4   1.3
1.1   1.2
 160.  *   1.1   1.0   0.8   0.9   0.3   0.0   0.0   0.1   0.1   0.1   0.8   0.9   1.0   0.4   0.2   0.5   1.3   1.3
1.1   1.0
 170.  *   1.4   1.3   1.2   1.1   0.4   0.0   0.0   0.4   0.4   0.3   0.8   0.7   0.9   0.2   0.1   0.5   1.0   1.3
1.1   0.8
 180.  *   1.7   1.8   1.5   1.5   0.6   0.0   0.3   0.9   0.8   0.7   0.4   0.4   0.5   0.1   0.0   0.3   0.6   1.3
0.6   0.3
 190.  *   1.5   1.5   1.7   1.5   1.0   0.3   0.5   1.3   1.1   1.0   0.2   0.2   0.1   0.0   0.0   0.3   0.5   0.9
0.4   0.2
 200.  *   1.5   1.4   1.4   1.6   1.0   0.4   0.6   1.2   1.2   1.0   0.0   0.0   0.0   0.0   0.0   0.3   0.5   0.8
0.3   0.1
 210.  *   1.3   1.3   1.4   1.4   1.3   0.3   0.6   1.0   1.2   1.0   0.0   0.0   0.0   0.0   0.0   0.3   0.4   0.7
0.1   0.1
 220.  *   1.1   1.1   1.3   1.2   1.0   0.6   0.6   1.0   1.0   1.0   0.0   0.0   0.1   0.0   0.0   0.3   0.4   0.5
0.1   0.0
 230.  *   1.1   1.1   1.1   0.8   0.8   0.9   0.9   1.1   1.0   1.0   0.0   0.0   0.1   0.1   0.1   0.2   0.3   0.3
0.0   0.0
 240.  *   1.1   1.2   1.0   0.6   0.4   1.0   0.9   1.1   1.0   0.9   0.0   0.0   0.4   0.2   0.2   0.1   0.1   0.1
0.0   0.0
 250.  *   1.1   1.2   1.0   0.7   0.5   1.0   0.9   1.1   1.2   1.0   0.0   0.1   0.6   0.3   0.3   0.0   0.0   0.1
0.0   0.0
 260.  *   0.9   1.1   1.0   0.7   0.4   1.2   1.0   1.1   1.4   1.0   0.0   0.1   0.8   0.4   0.3   0.0   0.0   0.0
0.0   0.0
 270.  *   0.8   1.1   1.1   0.7   0.4   1.3   1.1   1.0   1.3   1.1   0.1   0.2   1.0   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 280.  *   0.8   1.1   1.2   0.7   0.4   1.2   1.3   0.8   1.2   1.1   0.1   0.2   1.1   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 290.  *   0.9   1.2   1.3   0.6   0.3   1.1   1.4   1.1   1.1   1.2   0.1   0.2   1.1   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 300.  *   0.9   1.1   1.3   0.6   0.2   0.8   1.4   1.3   1.0   1.2   0.1   0.3   1.1   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 310.  *   0.9   1.1   1.3   0.4   0.1   0.6   1.4   1.6   1.1   1.4   0.1   0.4   1.1   0.3   0.3   0.0   0.0   0.1
0.1   0.1
 320.  *   0.8   0.9   1.1   0.2   0.0   0.5   1.1   1.7   1.3   1.5   0.2   0.5   1.1   0.3   0.3   0.0   0.0   0.3
0.1   0.1
 330.  *   0.5   0.6   0.7   0.1   0.0   0.3   1.0   1.5   1.4   1.5   0.2   0.7   1.2   0.4   0.3   0.0   0.0   0.6
0.5   0.3
 340.  *   0.2   0.3   0.3   0.0   0.0   0.2   0.7   1.2   1.2   1.5   0.5   0.9   1.4   0.6   0.3   0.0   0.1   1.2
0.9   0.6
 350.  *   0.1   0.1   0.1   0.0   0.0   0.3   0.7   0.8   0.8   1.1   0.9   1.1   1.7   1.0   0.4   0.1   0.4   1.5
1.4   1.0
 360.  *   0.0   0.1   0.1   0.0   0.0   0.3   0.7   0.8   0.7   0.6   1.0   1.2   1.8   1.3   0.6   0.2   0.6   1.5
1.6   1.1

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX   *   1.7   1.8   1.7   1.6   1.3   1.3   1.4   1.7   1.4   1.5   1.3   1.2   1.8   1.7   1.1   1.1   1.4   1.5
1.6   1.7
 DEGR. *  180   180   190   200   210   270   290   320   260   320    10     0     0    20    40    90   140     0
0   110
```


JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52 REC53 REC54 REC55 REC56 REC57 REC58
REC59 REC60

------*-------------------------------------------------------------------------------------------------------------
-------
   0.  *   0.4   0.6   0.7   0.0   0.0   0.0   0.1   0.6   0.8   0.7   0.8   0.8   0.9   0.4   0.2   0.3   0.2   0.8
0.7   1.0
  10.  *   0.1   0.2   0.2   0.0   0.0   0.0   0.0   0.2   0.2   0.2   1.2   1.1   1.3   0.6   0.3   0.2   0.5   1.0
1.0   0.9
  20.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.5   1.1   1.1   0.6   0.3   0.3   0.5   1.0
```



```
0.9   0.8
  30.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.4   1.2   0.9   0.6   0.4   0.3   0.5   0.8
0.9   0.7
  40.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.4   1.3   0.8   0.5   0.4   0.3   0.5   0.8
0.8   0.6
  50.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.2   1.3   0.8   0.4   0.3   0.2   0.4   0.8
0.8   0.5
  60.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1   1.2   0.7   0.5   0.5   0.4   0.4   0.6
0.7   0.6
  70.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0   1.2   0.6   0.6   0.4   0.4   0.6   0.6
0.7   0.6
  80.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0   1.2   0.7   0.6   0.5   0.4   0.6   0.6
0.7   0.6
  90.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9   1.1   0.7   0.7   0.6   0.4   0.5   0.7
0.8   0.8
 100.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8   1.1   0.7   0.6   0.5   0.5   0.6   0.8
0.7   0.7
 110.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   1.1   0.8   0.6   0.5   0.5   0.5   0.9
0.7   0.7
 120.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   1.1   0.9   0.6   0.6   0.6   0.7   1.0
0.7   0.7
 130.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.6   1.1   1.1   0.6   0.4   0.4   0.6   1.0
0.9   0.8
 140.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.8   1.1   1.1   0.5   0.4   0.6   0.7   1.0
0.8   0.9
 150.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9   1.2   1.2   0.7   0.4   0.4   0.8   1.2
0.9   1.0
 160.  *   0.1   0.0   0.0   0.0   0.0   0.0   0.0   0.1   0.0   0.0   1.2   1.1   1.4   0.7   0.2   0.2   0.6   1.1
0.9   1.1
 170.  *   0.2   0.2   0.2   0.0   0.0   0.0   0.0   0.1   0.1   0.1   1.2   1.1   1.2   0.5   0.0   0.2   0.4   1.2
1.0   1.1
 180.  *   0.5   0.5   0.7   0.0   0.0   0.0   0.0   0.6   0.5   0.4   1.0   0.8   0.9   0.3   0.0   0.0   0.3   0.8
0.8   0.8
 190.  *   1.1   1.1   1.2   0.3   0.0   0.0   0.2   1.1   0.8   0.7   0.7   0.6   0.5   0.1   0.0   0.0   0.1   0.5
0.2   0.2
 200.  *   1.0   1.0   1.3   0.5   0.3   0.1   0.4   1.4   1.1   0.9   0.5   0.4   0.1   0.1   0.0   0.0   0.1   0.1
0.0   0.0
 210.  *   0.8   0.9   1.0   0.6   0.3   0.3   0.6   1.3   1.3   1.1   0.3   0.2   0.0   0.0   0.0   0.0   0.1   0.1
0.0   0.0
 220.  *   0.7   0.8   0.8   0.5   0.3   0.5   0.5   1.0   1.2   1.0   0.3   0.2   0.0   0.0   0.0   0.0   0.0   0.1
0.0   0.0
 230.  *   0.7   0.7   0.9   0.5   0.3   0.3   0.6   0.8   1.2   1.0   0.4   0.1   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 240.  *   0.6   0.6   0.8   0.4   0.3   0.3   0.5   0.8   1.0   1.0   0.6   0.1   0.0   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 250.  *   0.6   0.6   0.7   0.4   0.3   0.3   0.4   0.9   1.0   1.1   0.7   0.0   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 260.  *   0.5   0.6   0.6   0.4   0.3   0.3   0.5   1.0   0.9   1.0   0.7   0.0   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 270.  *   0.5   0.7   0.7   0.4   0.2   0.3   0.4   1.0   0.8   1.0   0.8   0.0   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 280.  *   0.5   0.6   0.6   0.4   0.3   0.3   0.4   0.8   0.8   1.1   0.7   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 290.  *   0.6   0.6   0.6   0.4   0.2   0.2   0.4   0.7   0.8   1.0   0.7   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 300.  *   0.6   0.6   0.6   0.4   0.2   0.2   0.4   0.7   0.9   1.0   0.6   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 310.  *   0.6   0.6   0.7   0.3   0.2   0.2   0.4   0.8   1.0   1.0   0.5   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 320.  *   0.8   0.8   0.7   0.4   0.3   0.2   0.4   0.8   0.8   1.0   0.4   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.1
 330.  *   1.0   1.0   0.9   0.6   0.4   0.5   0.4   0.8   0.9   1.1   0.3   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1
 340.  *   1.3   1.1   1.0   0.5   0.3   0.3   0.5   1.1   1.2   1.4   0.3   0.0   0.1   0.1   0.0   0.0   0.0   0.2
0.2   0.3
 350.  *   0.9   0.9   0.9   0.3   0.1   0.2   0.3   0.9   1.2   1.2   0.4   0.4   0.5   0.2   0.0   0.0   0.2   0.4
0.5   0.7
 360.  *   0.4   0.6   0.7   0.0   0.0   0.0   0.1   0.6   0.8   0.7   0.8   0.8   0.9   0.4   0.2   0.3   0.2   0.8
0.7   1.0

------*-------------------------------------------------------------------------------------------------------------
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 MAX   *   1.3   1.1   1.3   0.6   0.4   0.5   0.6   1.4   1.3   1.4   1.5   1.3   1.4   0.7   0.6   0.6   0.8   1.2
1.0   1.1
 DEGR. *  340   190   200   210   330   220   210   200   210   340    20    40   160    90    90   120   150   150
10   160
```

THE HIGHEST CONCENTRATION OF 1.80 PPM OCCURRED AT RECEPTOR REC22.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:40:13

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1. Stan/Lom SB L	*	5194.4	5948.0	5135.6	6035.2	*	105.	326.	AG	113.	100.0	1.0	10.0	0.84 5.3
2. Stan/Lom SB TRR	*	5173.5	5937.1	5122.0	6010.9	*	90.	325.	AG	214.	100.0	1.0	20.0	0.71 4.6
3. Stan/Lom WB LTT	*	5306.8	5930.3	5403.5	6009.6	*	125.	51.	AG	220.	100.0	1.0	20.0	0.87 6.4
4. Stan/Lom WB R	*	5292.4	5947.7	5347.6	5990.1	*	70.	52.	AG	78.	100.0	1.0	10.0	0.40 3.5
5. Stan/Lom NB L	*	5307.6	5737.4	5359.5	5721.4	*	54.	107.	AG	113.	100.0	1.0	10.0	0.53 2.8
6. Stan/Lom NB TRR	*	5314.4	5765.3	5342.7	5755.7	*	30.	109.	AG	214.	100.0	1.0	20.0	0.25 1.5
7. Stan/Lom EB LLT	*	5214.5	5705.3	5200.8	5658.2	*	49.	196.	AG	220.	100.0	1.0	20.0	0.44 2.5
8. Stan/Lom EB R	*	5236.5	5698.5	5221.6	5646.0	*	55.	196.	AG	78.	100.0	1.0	10.0	0.32 2.8
9. Caus/Wash SB LTTRR	*	6548.6	6868.7	6475.2	7021.0	*	169.	334.	AG	218.	100.0	1.0	40.0	0.58 8.6
10. Caus/Wash WB LLTT	*	6635.9	6867.8	6714.6	6936.2	*	104.	49.	AG	243.	100.0	1.0	20.0	0.69 5.3
11. Caus/Wash WB R	*	6624.3	6883.3	6687.4	6942.0	*	86.	47.	AG	71.	100.0	1.0	10.0	0.28 4.4
12. Caus/Wash NB TTR	*	6603.5	6751.9	6613.9	6519.8	*	232.	177.	AG	210.	100.0	1.0	20.0	0.88 11.8
13. Caus/Wash EB LLTTR	*	6538.7	6754.8	6469.9	6706.8	*	84.	235.	AG	347.	100.0	1.0	30.0	0.47 4.3
14. Tha/Val SB LTTR	*	6599.0	6224.0	6593.3	6370.2	*	146.	358.	AG	99.	100.0	1.0	20.0	0.81 7.4
15. Tha/Val NB L	*	6631.0	6138.6	6630.2	6047.3	*	91.	180.	AG	96.	100.0	1.0	10.0	0.55 4.6
16. Tha/Val NB TR	*	6645.6	6138.6	6648.0	6000.5	*	138.	179.	AG	50.	100.0	1.0	10.0	0.76 7.0
17. Bev/Was SB TTT	*	6592.9	5963.9	6593.7	6089.2	*	125.	0.	AG	197.	100.0	1.0	30.0	0.64 6.4
18. Bev/Was EB RRR	*	6545.9	5954.3	6530.5	5976.1	*	27.	325.	AG	241.	100.0	1.0	30.0	0.14 1.4
19. Char/93 SB LLTTRR	*	6587.8	5740.0	6582.8	5870.1	*	130.	358.	AG	309.	100.0	1.0	40.0	0.67 6.6
20. Char/93 WB LTT	*	6702.8	5647.8	6712.2	5636.0	*	15.	141.	AG	201.	100.0	1.0	20.0	0.10 0.8
21. Char/93 EB TTR	*	6560.8	5622.5	6523.0	5594.9	*	47.	234.	AG	302.	100.0	1.0	30.0	0.30 2.4
22. North/Congress SB LT	*	6876.6	4408.9	6860.5	4488.9	*	82.	349.	AG	328.	100.0	1.0	30.0	0.62 4.1
23. North/Con WB LLTR	*	6920.6	4378.3	7073.6	4432.5	*	162.	71.	AG	175.	100.0	1.0	20.0	0.82 8.2
24. Nor/Con NB LTTTR	*	6914.9	4333.4	6920.4	4292.5	*	41.	172.	AG	324.	100.0	1.0	30.0	0.30 2.1
25. Nor/Con EB LTR	*	6869.7	4342.2	6864.6	4340.9	*	5.	256.	AG	88.	100.0	1.0	10.0	0.03 0.3
26. Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1120.	9.8	1.0	90.0	
27. Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1275.	9.8	1.0	78.0	
28. Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	817.	9.8	1.0	78.0	
29. Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1322.	9.8	1.0	78.0	
30. Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3211.	9.8	1.0	90.0	
31. Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1012.	9.8	1.0	66.0	
32. Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2221.	9.8	1.0	90.0	
33. Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1162.	9.8	1.0	78.0	
34. Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2247.	9.8	1.0	90.0	
35. Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	91.	9.8	1.0	38.0	
36. Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2524.	9.8	1.0	90.0	
37. Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	280.	9.8	1.0	54.0	
38. Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	1841.	9.8	1.0	66.0	
39. Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	269.	9.8	1.0	48.0	
40. Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	80.	9.8	1.0	42.0	
41. Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	811.	9.8	1.0	48.0	
42. Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	374.	9.8	1.0	54.0	
43. Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	650.	9.8	1.0	54.0	

44. Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	406.	9.8	1.0	42.0	

JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:40:13

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45. North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1226.	9.8	1.0	98.0	
46. North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	978.	9.8	1.0	66.0	
47. North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1420.	9.8	1.0	98.0	
48. North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	44.	9.8	1.0	54.0	

JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:40:13

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. Stan/Lom SB L	*	90	70	3.0	223	1600	54.39	1	3
2. Stan/Lom SB TRR	*	90	66	3.0	481	1600	54.39	1	3
3. Stan/Lom WB LTT	*	90	68	3.0	527	1600	54.39	1	3
4. Stan/Lom WB R	*	90	48	3.0	265	1600	54.39	1	3
5. Stan/Lom NB L	*	90	70	3.0	142	1600	54.39	1	3
6. Stan/Lom NB TRR	*	90	66	3.0	166	1600	54.39	1	3
7. Stan/Lom EB LLT	*	90	68	3.0	265	1600	54.39	1	3
8. Stan/Lom EB R	*	90	48	3.0	208	1600	54.39	1	3
9. Caus/Wash SB LTTRR	*	150	56	3.0	2210	1600	54.39	1	3
10. Caus/Wash WB LLTT	*	150	125	3.0	296	1600	54.39	1	3
11. Caus/Wash WB R	*	150	73	3.0	216	1600	54.39	1	3
12. Caus/Wash NB TTR	*	150	108	3.0	693	1600	54.39	1	3
13. Caus/Wash EB LLTTR	*	150	119	3.0	388	1600	54.39	1	3
14. Tha/Val SB LTTR	*	100	34	3.0	1575	1600	54.39	1	3
15. Tha/Val NB L	*	100	66	3.0	253	1600	54.39	1	3
16. Tha/Val NB TR	*	100	34	3.0	743	1600	54.39	1	3
17. Bev/Was SB TTT	*	100	45	3.0	1528	1600	54.39	1	3
18. Bev/Was EB RRR	*	100	55	3.0	269	1600	54.39	1	3
19. Char/93 SB LLTTRR	*	100	53	3.0	1797	1600	54.39	1	3
20. Char/93 WB LTT	*	100	69	3.0	80	1600	54.39	1	3
21. Char/93 EB TTR	*	100	69	3.0	374	1600	54.39	1	3
22. North/Congress SB LT	*	100	75	3.0	598	1600	54.39	1	3
23. North/Con WB LLTR	*	100	60	3.0	916	1600	54.39	1	3
24. Nor/Con NB LTTTR	*	100	74	3.0	306	1600	54.39	1	3
25. Nor/Con EB LTR	*	100	60	3.0	16	1600	54.39	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Bev/Was N1	*	6562.0	6150.2	6.0	*
2. Bev/Was N2	*	6561.2	6075.2	6.0	*
3. Bev/Was N3	*	6560.5	6000.2	6.0	*
4. Bev/Was N4	*	6515.8	6060.4	6.0	*
5. Bev/Was N5	*	6471.1	6120.6	6.0	*
6. Bev/Was SE1	*	6671.0	6049.7	6.0	*
7. Bev/Was SE2	*	6670.2	5966.3	6.0	*
8. Bev/Was SE3	*	6624.0	5907.2	6.0	*
9. Bev/Was SE4	*	6626.1	5832.3	6.0	*
10. Bev/Was SE5	*	6628.1	5757.3	6.0	*
11. Bev/Was SW1	*	6541.8	5766.9	6.0	*
12. Bev/Was SW2	*	6540.1	5841.9	6.0	*
13. Bev/Was SW3	*	6537.7	5916.8	6.0	*
14. Bev/Was SW4	*	6493.0	5977.0	6.0	*
15. Bev/Was SW5	*	6448.3	6037.3	6.0	*
16. Char/93 NE1	*	6625.0	5871.1	6.0	*
17. Char/93 NE2	*	6627.1	5796.1	6.0	*
18. Char/93 NE3	*	6629.1	5721.1	6.0	*
19. Char/93 NE4	*	6699.8	5695.9	6.0	*
20. Char/93 NE5	*	6750.6	5633.2	6.0	*

JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:40:13

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
21. Char/93 S1	6657.8	5466.0	6.0
22. Char/93 S2	6614.7	5527.4	6.0
23. Char/93 S3	6571.7	5588.8	6.0
24. Char/93 S4	6512.9	5542.2	6.0
25. Char/93 S5	6454.1	5495.6	6.0
26. Char/93 NW1	6424.1	5632.5	6.0
27. Char/93 NW2	6483.6	5678.2	6.0
28. Char/93 NW3	6543.0	5723.9	6.0
29. Char/93 NW4	6541.0	5798.8	6.0
30. Char/93 NW5	6538.9	5873.8	6.0
31. Wash/Cong NE1	6910.2	4571.2	6.0
32. Wash/Cong NE2	6925.8	4497.8	6.0
33. Wash/Cong NE3	6941.4	4424.5	6.0
34. Wash/Cong NE4	7012.0	4449.6	6.0
35. Wash/Cong NE5	7082.7	4474.9	6.0
36. Wash/Cong SE1	7095.4	4388.1	6.0
37. Wash/Cong SE2	7024.8	4362.9	6.0
38. Wash/Cong SE3	6954.1	4337.7	6.0
39. Wash/Cong SE4	6968.4	4264.1	6.0
40. Wash/Cong SE5	6982.7	4190.4	6.0
41. Wash/Cong SW1	6867.5	4164.7	6.0
42. Wash/Cong SW2	6853.3	4238.0	6.0
43. Wash/Cong SW3	6838.9	4312.0	6.0
44. Wash/Cong SW4	6765.6	4296.1	6.0
45. Wash/Cong SW5	6692.3	4280.2	6.0
46. Wash/Cong NW1	6682.4	4353.8	6.0
47. Wash/Cong NW2	6755.7	4369.7	6.0
48. Wash/Cong NW3	6828.9	4386.0	6.0
49. Wash/Cong NW4	6813.3	4459.4	6.0
50. Wash/Cong NW5	6797.8	4532.8	6.0

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	1.0	1.0	0.8	0.4	0.2	0.8	0.9	1.6	1.0	1.0	1.0	0.8	0.9	0.4	0.2	1.4	1.0	1.1	0.3	0.1
10.	1.3	1.2	1.1	0.6	0.4	0.2	0.2	1.2	0.6	0.4	1.3	1.2	1.2	0.4	0.4	0.8	0.6	0.4	0.0	0.0
20.	1.1	1.1	1.3	0.7	0.4	0.0	0.1	0.8	0.2	0.1	1.5	1.2	1.2	0.5	0.3	0.4	0.1	0.1	0.0	0.0
30.	1.0	0.9	1.4	0.6	0.4	0.0	0.0	0.5	0.1	0.0	1.4	1.0	1.2	0.6	0.4	0.2	0.0	0.0	0.0	0.0
40.	0.9	0.9	1.3	0.5	0.5	0.0	0.0	0.3	0.0	0.0	1.3	1.1	1.1	0.6	0.4	0.1	0.0	0.0	0.0	0.0
50.	1.0	0.9	1.3	0.5	0.5	0.0	0.0	0.2	0.0	0.0	1.2	1.0	0.9	0.7	0.4	0.0	0.0	0.0	0.0	0.0
60.	1.0	0.9	1.1	0.6	0.5	0.0	0.0	0.2	0.0	0.0	1.2	1.0	0.7	0.7	0.4	0.0	0.0	0.0	0.0	0.0
70.	0.9	1.0	1.1	0.6	0.5	0.0	0.0	0.1	0.0	0.0	1.2	1.0	0.6	0.8	0.4	0.0	0.0	0.0	0.0	0.0
80.	0.9	1.1	1.1	0.7	0.5	0.0	0.0	0.1	0.0	0.0	1.2	1.2	0.6	0.9	0.4	0.0	0.0	0.0	0.0	0.0
90.	0.7	1.1	1.1	0.8	0.4	0.0	0.0	0.0	0.0	0.0	1.2	1.2	0.6	1.0	0.5	0.0	0.0	0.0	0.0	0.0
100.	0.7	1.2	1.1	0.7	0.5	0.0	0.0	0.0	0.0	0.0	1.1	1.2	0.5	0.8	0.6	0.0	0.0	0.0	0.0	0.0
110.	0.7	1.2	1.1	0.7	0.5	0.0	0.0	0.1	0.0	0.0	0.9	1.1	0.5	0.7	0.5	0.0	0.0	0.0	0.0	0.0
120.	0.7	1.1	1.0	0.7	0.6	0.0	0.0	0.1	0.0	0.0	0.8	1.2	0.6	0.6	0.6	0.0	0.0	0.0	0.0	0.0
130.	0.9	1.1	1.0	0.6	0.6	0.0	0.0	0.1	0.0	0.0	0.7	1.3	0.8	0.6	0.5	0.0	0.0	0.0	0.0	0.0
140.	0.9	1.3	0.9	0.6	0.5	0.0	0.0	0.0	0.0	0.0	0.5	1.3	1.0	0.6	0.5	0.0	0.0	0.1	0.0	0.0
150.	1.0	1.3	0.9	0.7	0.5	0.0	0.0	0.0	0.0	0.1	0.5	1.2	1.3	0.7	0.4	0.0	0.1	0.1	0.2	0.0
160.	1.2	1.2	1.1	0.7	0.5	0.0	0.0	0.1	0.1	0.1	0.4	0.9	1.3	0.5	0.2	0.1	0.1	0.2	0.2	0.1
170.	1.1	1.2	1.2	0.6	0.3	0.1	0.1	0.3	0.2	0.1	0.4	0.7	0.8	0.2	0.1	0.3	0.1	0.3	0.2	0.1
180.	0.8	0.9	0.9	0.4	0.1	0.4	0.2	0.7	0.4	0.1	0.2	0.4	0.4	0.0	0.0	0.5	0.2	0.3	0.2	0.1
190.	0.5	0.4	0.7	0.1	0.1	0.6	0.3	1.0	0.8	0.1	0.2	0.3	0.2	0.0	0.0	0.8	0.5	0.2	0.2	0.1
200.	0.2	0.1	0.5	0.1	0.1	1.0	0.7	1.1	1.1	0.3	0.2	0.1	0.0	0.0	0.0	1.3	0.7	0.2	0.1	0.1
210.	0.1	0.1	0.5	0.1	0.1	1.1	0.9	1.3	1.4	0.4	0.1	0.1	0.0	0.0	0.0	1.4	0.9	0.3	0.1	0.1
220.	0.1	0.0	0.4	0.1	0.1	1.1	0.8	1.1	1.4	0.5	0.1	0.0	0.0	0.0	0.0	1.4	1.1	0.5	0.1	0.1
230.	0.1	0.0	0.4	0.0	0.1	1.1	0.7	0.9	1.3	0.5	0.0	0.0	0.0	0.0	0.0	1.3	1.2	0.4	0.2	0.1
240.	0.1	0.0	0.3	0.0	0.0	1.1	0.8	0.8	1.3	0.7	0.0	0.0	0.0	0.0	0.0	1.2	1.1	0.2	0.4	0.1
250.	0.1	0.0	0.2	0.0	0.0	1.0	0.6	0.7	1.1	0.9	0.0	0.0	0.0	0.0	0.0	1.0	1.1	0.1	0.3	0.2
260.	0.1	0.0	0.1	0.0	0.0	1.0	0.9	0.6	1.2	1.0	0.0	0.0	0.0	0.0	0.0	1.0	1.2	0.1	0.2	0.3
270.	0.1	0.0	0.1	0.0	0.0	1.1	0.9	0.6	1.2	1.2	0.0	0.0	0.0	0.0	0.0	0.8	1.2	0.1	0.1	0.4
280.	0.1	0.0	0.1	0.0	0.0	1.1	0.9	0.5	1.2	1.2	0.0	0.0	0.0	0.0	0.0	0.7	1.2	0.4	0.2	0.4
290.	0.1	0.1	0.1	0.0	0.0	1.0	0.9	0.6	1.1	1.3	0.0	0.0	0.0	0.0	0.0	0.5	1.1	0.6	0.4	0.3
300.	0.1	0.1	0.1	0.1	0.0	0.9	0.9	0.7	1.1	1.3	0.0	0.0	0.0	0.0	0.0	0.4	1.3	0.9	0.5	0.3
310.	0.1	0.1	0.0	0.1	0.0	0.9	1.0	0.9	1.0	1.3	0.0	0.0	0.0	0.0	0.0	0.6	1.3	1.0	0.5	0.4
320.	0.1	0.1	0.0	0.1	0.0	1.0	0.9	0.8	1.0	1.3	0.0	0.0	0.0	0.0	0.0	0.6	1.2	1.2	0.5	0.4
330.	0.1	0.1	0.0	0.1	0.0	1.0	1.2	1.1	1.0	1.4	0.0	0.0	0.2	0.0	0.0	0.9	1.1	1.2	0.5	0.3
340.	0.2	0.1	0.1	0.1	0.0	1.4	1.4	1.3	0.9	1.3	0.0	0.0	0.3	0.0	0.0	1.0	1.1	1.3	0.6	0.5
350.	0.6	0.5	0.4	0.2	0.2	1.2	1.2	1.7	1.3	1.4	0.2	0.4	0.5	0.2	0.0	1.3	1.2	1.3	0.6	0.4
360.	1.0	1.0	0.8	0.4	0.2	0.8	0.9	1.6	1.0	1.0	1.0	0.8	0.9	0.4	0.2	1.4	1.0	1.1	0.3	0.1
MAX	1.3	1.3	1.4	0.8	0.6	1.4	1.4	1.7	1.4	1.4	1.5	1.3	1.3	1.0	0.6	1.4	1.3	1.3	0.6	0.5
DEGR.	10	150	30	90	120	340	340	350	210	330	20	140	150	90	100	0	300	340	340	340

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.6	0.7	1.3	0.9	0.2	0.1	0.3	1.1	0.9	0.9	0.1	0.1	0.1	0.0	0.0	0.2	0.5	0.6	0.4	0.3
10.	0.3	0.5	1.0	1.0	0.6	0.3	0.6	1.5	1.1	1.0	0.0	0.0	0.0	0.0	0.0	0.2	0.6	0.6	0.3	0.2
20.	0.2	0.2	0.4	1.0	0.6	0.4	0.8	1.6	1.4	1.1	0.0	0.0	0.0	0.0	0.0	0.1	0.6	0.6	0.2	0.2
30.	0.2	0.2	0.1	0.8	0.6	0.3	0.6	1.4	1.4	1.1	0.0	0.0	0.0	0.0	0.0	0.1	0.5	0.6	0.2	0.0
40.	0.2	0.2	0.1	0.5	0.3	0.5	0.7	1.3	1.3	0.8	0.0	0.0	0.0	0.0	0.0	0.1	0.4	0.6	0.2	0.0
50.	0.2	0.2	0.1	0.2	0.3	0.4	0.5	1.1	1.3	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.0	0.0
60.	0.2	0.2	0.2	0.1	0.1	0.3	0.5	0.9	1.2	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.0	0.0
70.	0.2	0.2	0.2	0.1	0.1	0.2	0.3	0.7	1.1	0.5	0.0	0.0	0.2	0.1	0.0	0.0	0.1	0.1	0.0	0.0
80.	0.2	0.2	0.3	0.2	0.1	0.4	0.2	0.4	1.2	0.7	0.0	0.0	0.4	0.1	0.0	0.0	0.0	0.1	0.0	0.0
90.	0.2	0.2	0.3	0.2	0.1	0.4	0.3	0.3	1.2	0.8	0.0	0.0	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.0
100.	0.2	0.2	0.3	0.2	0.1	0.6	0.3	0.1	1.2	0.9	0.0	0.0	0.7	0.4	0.0	0.0	0.0	0.0	0.0	0.0
110.	0.2	0.2	0.3	0.1	0.0	0.6	0.4	0.1	1.1	1.1	0.0	0.2	0.7	0.6	0.0	0.0	0.0	0.0	0.0	0.0
120.	0.1	0.2	0.3	0.0	0.0	0.5	0.4	0.1	1.2	1.2	0.0	0.2	0.7	0.6	0.0	0.0	0.0	0.0	0.0	0.0

130.	*	0.1	0.2	0.2	0.0	0.0	0.3	0.7	0.3	1.0	1.2	0.2	0.3	0.7	0.5	0.1	0.0	0.0	0.0
0.0	0.0																		
140.	*	0.0	0.1	0.1	0.0	0.0	0.3	0.6	0.3	1.0	1.3	0.2	0.3	0.6	0.5	0.1	0.0	0.0	0.0
0.0	0.0																		
150.	*	0.0	0.0	0.1	0.0	0.0	0.3	0.5	0.4	0.7	1.3	0.2	0.3	0.6	0.6	0.1	0.0	0.0	0.0
0.0	0.0																		
160.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.3	0.6	1.1	0.4	0.4	0.7	0.6	0.2	0.0	0.0	0.1
0.1	0.1																		
170.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.4	0.6	0.8	0.5	0.6	0.8	0.6	0.2	0.0	0.0	0.2
0.2	0.2																		
180.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.5	0.3	0.5	0.8	0.8	0.9	0.6	0.3	0.0	0.1	0.4
0.3	0.3																		
190.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.5	0.2	0.2	0.7	0.8	1.1	0.9	0.6	0.0	0.1	0.5
0.4	0.3																		
200.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.7	0.7	1.0	1.0	0.6	0.1	0.2	0.6
0.4	0.4																		
210.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1	0.0	0.6	0.7	0.9	1.0	0.7	0.1	0.2	0.7
0.4	0.4																		
220.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.0	0.0	0.5	0.7	0.6	1.0	0.9	0.1	0.3	0.9
0.4	0.4																		
230.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.4	0.8	0.4	0.9	0.9	0.1	0.3	0.9
0.3	0.3																		
240.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.1	0.0	0.0	0.3	0.8	0.5	0.7	0.7	0.3	0.4	0.9
0.3	0.3																		
250.	*	0.0	0.0	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.7	0.6	0.5	0.6	0.4	0.5	0.8
0.3	0.3																		
260.	*	0.0	0.0	0.4	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.6	0.6	0.3	0.3	0.5	0.5	0.8
0.3	0.3																		
270.	*	0.0	0.0	0.6	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.7	0.4	0.2	0.8	0.5	0.7
0.3	0.3																		
280.	*	0.0	0.1	0.7	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.8	0.4	0.2	0.8	0.8	0.5
0.4	0.3																		
290.	*	0.0	0.1	0.8	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.8	0.3	0.1	0.8	1.0	0.6
0.5	0.3																		
300.	*	0.0	0.3	0.9	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.7	0.2	0.1	0.8	1.0	0.6
0.6	0.4																		
310.	*	0.2	0.4	0.9	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.2	0.1	0.7	0.9	0.9
1.0	0.5																		
320.	*	0.1	0.3	0.9	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.6	0.2	0.1	0.5	0.8	1.0
1.0	0.6																		
330.	*	0.2	0.3	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.5	0.1	0.0	0.4	0.6	1.1
1.1	0.7																		
340.	*	0.4	0.5	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.3	0.0	0.0	0.4	0.7	1.1
0.8	0.8																		
350.	*	0.5	0.6	0.9	0.3	0.2	0.0	0.0	0.3	0.2	0.2	0.1	0.2	0.2	0.0	0.0	0.2	0.5	0.7
0.5	0.7																		
360.	*	0.6	0.7	1.3	0.9	0.2	0.1	0.3	1.1	0.9	0.9	0.1	0.1	0.1	0.0	0.0	0.2	0.5	0.6
0.4	0.3																		
------	*	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------
-------																			
MAX	*	0.6	0.7	1.3	1.0	0.6	0.6	0.8	1.6	1.4	1.3	0.8	0.8	1.1	1.0	0.9	0.8	1.0	1.1
1.1	0.8																		
DEGR.	*	0	0	0	10	10	100	20	20	30	150	180	180	190	200	220	270	290	330
330	340																		

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50
0.	* 0.6	0.6	0.6	0.1	0.0	0.0	0.1	0.5	0.3	0.3
10.	* 0.8	0.6	0.7	0.1	0.1	0.0	0.1	0.7	0.4	0.3
20.	* 0.7	0.8	0.7	0.3	0.1	0.1	0.2	0.9	0.4	0.3
30.	* 0.7	0.8	0.7	0.4	0.2	0.1	0.3	0.9	0.3	0.3
40.	* 0.6	0.7	0.7	0.3	0.2	0.1	0.4	0.8	0.4	0.3
50.	* 0.3	0.7	0.8	0.5	0.2	0.2	0.4	0.8	0.5	0.3
60.	* 0.3	0.5	0.8	0.4	0.5	0.2	0.4	0.8	0.6	0.3
70.	* 0.3	0.4	0.8	0.5	0.3	0.4	0.5	0.6	0.8	0.3
80.	* 0.3	0.3	0.8	0.5	0.4	0.5	0.5	0.8	0.9	0.3
90.	* 0.3	0.3	0.6	0.3	0.2	0.4	0.4	0.7	1.1	0.3
100.	* 0.3	0.3	0.6	0.3	0.1	0.2	0.5	0.6	1.1	0.3
110.	* 0.3	0.3	0.5	0.2	0.1	0.2	0.3	0.7	1.2	0.6
120.	* 0.4	0.4	0.5	0.2	0.1	0.2	0.3	0.6	1.1	0.7
130.	* 0.4	0.4	0.4	0.2	0.1	0.1	0.2	0.6	0.9	0.9
140.	* 0.4	0.4	0.4	0.2	0.1	0.1	0.2	0.6	0.8	1.0
150.	* 0.3	0.4	0.4	0.1	0.0	0.1	0.2	0.6	0.7	0.9
160.	* 0.3	0.3	0.4	0.0	0.0	0.0	0.1	0.4	0.5	0.7
170.	* 0.1	0.2	0.2	0.0	0.0	0.0	0.0	0.3	0.3	0.4

180.	*	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.1	0.1
190.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
200.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
210.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
220.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
230.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
240.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
250.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
260.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
270.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
280.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
290.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
300.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
310.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
320.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
330.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
340.	*	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.1	0.1	0.1
350.	*	0.4	0.3	0.4	0.0	0.0	0.0	0.0	0.2	0.2	0.2
360.	*	0.6	0.6	0.6	0.1	0.0	0.0	0.1	0.5	0.3	0.3
------	*	------	------	------	------	------	------	------	------	------	------
MAX	*	0.8	0.8	0.8	0.5	0.5	0.5	0.5	0.9	1.2	1.0
DEGR.	*	10	20	50	50	60	80	70	30	110	140

THE HIGHEST CONCENTRATION OF 1.70 PPM OCCURRED AT RECEPTOR REC8 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:37:50

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH (VEH)	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE
1.	Stan/Lom SB L	*	5194.4	5948.0	5135.6	6035.1	*	105.	326.	AG	115.	100.0	1.0	10.0	0.81	5.3
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5086.9	6061.1	*	151.	325.	AG	216.	100.0	1.0	20.0	0.88	7.7
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5356.6	5971.2	*	64.	51.	AG	207.	100.0	1.0	20.0	0.43	3.3
4.	Stan/Lom WB R	*	5292.4	5947.7	5467.2	6081.9	*	220.	52.	AG	115.	100.0	1.0	10.0	1.01	11.2
5.	Stan/Lom NB L	*	5307.6	5737.4	5334.8	5729.0	*	29.	107.	AG	115.	100.0	1.0	10.0	0.26	1.4
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5348.1	5753.9	*	36.	109.	AG	216.	100.0	1.0	20.0	0.26	1.8
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5194.5	5636.4	*	72.	196.	AG	207.	100.0	1.0	20.0	0.48	3.6
8.	Stan/Lom EB R	*	5236.5	5698.5	5057.8	5069.3	*	654.	196.	AG	115.	100.0	1.0	10.0	1.17	33.2
9.	Char/93 SB LLTTRR	*	6587.8	5740.0	6583.0	5866.1	*	126.	358.	AG	362.	100.0	1.0	40.0	0.70	6.4
10.	Char/93 WB LTT	*	6702.8	5647.8	6733.3	5609.6	*	49.	141.	AG	175.	100.0	1.0	20.0	0.27	2.5
11.	Char/93 EB TTR	*	6560.8	5622.5	6480.8	5564.0	*	99.	234.	AG	263.	100.0	1.0	30.0	0.54	5.0
12.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1289.	9.8	1.0	90.0		
13.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1112.	9.8	1.0	78.0		
14.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	999.	9.8	1.0	78.0		
15.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1207.	9.8	1.0	78.0		
16.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	1635.	9.8	1.0	66.0		
17.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	298.	9.8	1.0	42.0		
18.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	847.	9.8	1.0	48.0		
19.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	908.	9.8	1.0	54.0		
20.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	449.	9.8	1.0	54.0		
21.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	314.	9.8	1.0	42.0		

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JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:37:50

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Stan/Lom SB L	*	100	79	3.0	208	1600	54.39	1	3
2.	Stan/Lom SB TRR	*	100	74	3.0	595	1600	54.39	1	3
3.	Stan/Lom WB LTT	*	100	71	3.0	332	1600	54.39	1	3
4.	Stan/Lom WB R	*	100	79	3.0	259	1600	54.39	1	3
5.	Stan/Lom NB L	*	100	79	3.0	66	1600	54.39	1	3
6.	Stan/Lom NB TRR	*	100	74	3.0	176	1600	54.39	1	3
7.	Stan/Lom EB LLT	*	100	71	3.0	371	1600	54.39	1	3
8.	Stan/Lom EB R	*	100	79	3.0	300	1600	54.39	1	3
9.	Char/93 SB LLTTRR	*	100	62	3.0	1488	1600	54.39	1	3
10.	Char/93 WB LTT	*	100	60	3.0	298	1600	54.39	1	3
11.	Char/93 EB TTR	*	100	60	3.0	908	1600	54.39	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*

8.	Stan/Lom SE3	*	5261.7	5823.6	6.0 *
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0 *
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0 *
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0 *
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0 *
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0 *
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0 *
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0 *
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0 *
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0 *
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0 *
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0 *
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0 *
21.	Char/93 NE1	*	6625.0	5871.1	6.0 *
22.	Char/93 NE2	*	6627.1	5796.1	6.0 *
23.	Char/93 NE3	*	6629.1	5721.1	6.0 *
24.	Char/93 NE4	*	6699.8	5695.9	6.0 *
25.	Char/93 NE5	*	6750.6	5633.2	6.0 *
26.	Char/93 S1	*	6657.8	5466.0	6.0 *
27.	Char/93 S2	*	6614.7	5527.4	6.0 *
28.	Char/93 S3	*	6571.7	5588.8	6.0 *
29.	Char/93 S4	*	6512.9	5542.2	6.0 *
30.	Char/93 S5	*	6454.1	5495.6	6.0 *
31.	Char/93 NW1	*	6424.1	5632.5	6.0 *
32.	Char/93 NW2	*	6483.6	5678.2	6.0 *
33.	Char/93 NW3	*	6543.0	5723.9	6.0 *
34.	Char/93 NW4	*	6541.0	5798.8	6.0 *

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JOB: Government Center Garage RUN: Existing

DATE : 7/ 9/13
TIME : 8:37:50

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
35.	Char/93 NW5	*	6538.9	5873.8	6.0	*

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JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* 0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.4	0.4	0.2	0.3	0.6	0.5	0.6	0.9	0.2	0.3	0.5	0.7	1.0
10.	* 0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.6	0.4	0.1	0.3	0.4	0.5	0.6	0.8	0.3	0.3	0.2	0.5	1.0
20.	* 0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.6	0.3	0.1	0.3	0.5	0.6	0.3	0.4	0.4	0.3	0.3	0.3	0.9
30.	* 0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.6	0.1	0.0	0.2	0.2	0.4	0.3	0.2	0.3	0.3	0.5	0.3	0.9
40.	* 0.0	0.0	0.2	0.1	0.0	0.3	0.4	0.5	0.1	0.0	0.2	0.2	0.4	0.2	0.1	0.6	0.4	0.5	0.5	0.9
50.	* 0.0	0.0	0.4	0.3	0.2	0.2	0.2	0.2	0.0	0.0	0.3	0.3	0.5	0.1	0.1	0.7	0.4	0.5	0.7	0.9
60.	* 0.0	0.0	0.7	0.5	0.4	0.1	0.1	0.1	0.0	0.0	0.3	0.3	0.5	0.1	0.1	0.8	0.3	0.2	0.8	1.0
70.	* 0.0	0.2	0.9	0.6	0.5	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.2	0.1	0.8	0.4	0.1	0.8	1.0
80.	* 0.0	0.2	0.9	0.6	0.6	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.8	0.6	0.1	0.4	1.1
90.	* 0.1	0.3	0.8	0.6	0.6	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.1	0.1	0.8	0.5	0.1	0.4	0.8
100.	* 0.2	0.4	0.7	0.6	0.6	0.0	0.0	0.1	0.1	0.1	0.3	0.3	0.3	0.1	0.0	0.7	0.6	0.3	0.3	0.6
110.	* 0.2	0.4	0.5	0.7	0.6	0.0	0.0	0.2	0.2	0.2	0.2	0.2	0.2	0.0	0.0	0.5	0.7	0.5	0.3	0.5
120.	* 0.3	0.4	0.4	0.8	0.6	0.0	0.1	0.4	0.3	0.3	0.1	0.1	0.1	0.0	0.0	0.5	0.6	0.5	0.3	0.5
130.	* 0.2	0.5	0.5	0.9	0.6	0.1	0.1	0.4	0.4	0.3	0.0	0.0	0.0	0.0	0.0	0.4	0.7	0.4	0.3	0.4
140.	* 0.4	0.5	0.4	1.0	0.6	0.1	0.2	0.4	0.4	0.3	0.0	0.0	0.0	0.0	0.0	0.4	0.7	0.3	0.1	0.3
150.	* 0.4	0.4	0.5	1.1	0.7	0.1	0.2	0.4	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.4	0.7	0.5		

0.2	0.3																		
160.	*	0.5	0.4	0.5	1.1	0.7	0.1	0.3	0.2	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.5	0.7	0.5
0.4	0.2																		
170.	*	0.7	0.6	0.5	1.1	0.7	0.1	0.2	0.3	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.5	0.7	0.7
0.4	0.3																		
180.	*	0.8	0.6	0.7	1.0	0.8	0.1	0.2	0.5	0.7	0.2	0.0	0.0	0.1	0.1	0.1	0.5	0.6	0.7
0.4	0.2																		
190.	*	0.7	0.5	0.8	1.2	0.8	0.2	0.4	0.7	0.8	0.2	0.0	0.0	0.3	0.3	0.3	0.4	0.4	0.5
0.3	0.1																		
200.	*	0.7	0.6	0.7	1.0	1.1	0.4	0.5	0.7	0.9	0.3	0.0	0.1	0.6	0.5	0.5	0.2	0.2	0.3
0.1	0.0																		
210.	*	0.7	0.5	0.5	0.8	0.9	0.3	0.5	0.5	0.8	0.4	0.1	0.2	0.8	0.7	0.7	0.1	0.1	0.1
0.0	0.0																		
220.	*	0.7	0.6	0.4	0.4	0.9	0.2	0.4	0.2	0.7	0.4	0.1	0.2	0.9	0.7	0.6	0.0	0.0	0.0
0.0	0.0																		
230.	*	0.7	0.6	0.4	0.4	0.6	0.2	0.1	0.1	0.7	0.4	0.2	0.3	0.9	0.7	0.7	0.0	0.0	0.0
0.0	0.0																		
240.	*	0.6	0.7	0.3	0.3	0.4	0.2	0.1	0.1	0.5	0.7	0.2	0.3	0.8	0.6	0.6	0.0	0.0	0.0
0.0	0.0																		
250.	*	0.5	0.7	0.4	0.3	0.2	0.4	0.1	0.0	0.3	0.7	0.2	0.4	0.7	0.7	0.6	0.0	0.0	0.0
0.0	0.0																		
260.	*	0.5	0.7	0.4	0.4	0.2	0.4	0.3	0.0	0.3	0.6	0.3	0.4	0.6	0.6	0.6	0.0	0.0	0.0
0.0	0.0																		
270.	*	0.4	0.7	0.6	0.5	0.2	0.7	0.4	0.0	0.2	0.5	0.3	0.4	0.4	0.7	0.5	0.0	0.0	0.0
0.0	0.0																		
280.	*	0.3	0.6	0.6	0.4	0.1	0.8	0.4	0.0	0.1	0.3	0.2	0.3	0.4	0.8	0.5	0.0	0.0	0.0
0.0	0.0																		
290.	*	0.4	0.7	0.8	0.3	0.1	0.9	0.7	0.1	0.1	0.3	0.2	0.3	0.3	0.8	0.5	0.0	0.0	0.0
0.0	0.0																		
300.	*	0.4	0.5	0.7	0.2	0.1	1.0	0.7	0.1	0.2	0.3	0.3	0.2	0.3	0.9	0.5	0.0	0.0	0.0
0.0	0.0																		
310.	*	0.3	0.4	0.6	0.1	0.0	0.8	0.8	0.4	0.4	0.4	0.5	0.4	0.4	0.9	0.5	0.0	0.0	0.0
0.1	0.1																		
320.	*	0.3	0.3	0.3	0.0	0.0	0.8	0.7	0.7	0.5	0.4	0.6	0.4	0.4	0.8	0.7	0.0	0.0	0.0
0.3	0.2																		
330.	*	0.1	0.2	0.2	0.0	0.0	0.6	0.4	0.8	0.4	0.3	0.6	0.8	0.6	0.9	0.7	0.0	0.0	0.2
0.6	0.5																		
340.	*	0.0	0.1	0.1	0.0	0.0	0.5	0.5	0.7	0.3	0.2	0.5	0.7	0.6	0.9	1.0	0.1	0.2	0.4
0.9	0.8																		
350.	*	0.0	0.0	0.0	0.0	0.0	0.5	0.6	0.5	0.3	0.3	0.4	0.7	0.7	0.8	1.1	0.2	0.3	0.6
0.8	0.9																		
360.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.4	0.4	0.2	0.3	0.6	0.5	0.6	0.9	0.2	0.3	0.5
0.7	1.0																		
------	*	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------
-------																			
MAX	*	0.8	0.7	0.9	1.2	1.1	1.0	0.8	0.8	0.9	0.7	0.6	0.8	0.9	0.9	1.1	0.8	0.7	0.7
0.9	1.1																		
DEGR.	*	180	240	70	190	200	300	310	330	200	240	320	330	220	300	350	60	110	170
340	80																		

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35
0.	*	0.1	0.1	0.4	0.0	0.0	0.4	0.5	0.9	1.2	0.5	0.0	0.0	0.5	0.2	0.1
10.	*	0.0	0.1	0.2	0.0	0.0	0.2	0.4	0.9	1.3	0.8	0.0	0.2	0.9	0.4	0.1
20.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.2	0.5	1.2	0.9	0.2	0.4	1.2	0.7	0.2
30.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.9	0.9	0.2	0.5	1.3	1.0	0.2
40.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.2	0.6	0.7	0.3	0.6	1.3	1.2	0.3
50.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.2	0.3	0.5	0.3	0.5	1.1	1.3	0.3
60.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.1	0.3	0.3	0.4	1.0	1.2	0.4
70.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.2	0.3	0.7	1.2	0.4
80.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.4	0.1	0.4	1.2	0.5
90.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.1	0.5	0.2	0.2	1.2	0.6
100.	*	0.0	0.0	0.1	0.0	0.0	0.2	0.3	0.3	0.1	0.1	0.6	0.2	0.1	1.2	0.8
110.	*	0.0	0.0	0.1	0.0	0.0	0.2	0.2	0.3	0.1	0.0	0.6	0.4	0.1	1.2	1.0
120.	*	0.0	0.0	0.2	0.0	0.0	0.2	0.2	0.3	0.0	0.0	0.6	0.5	0.2	1.2	1.1
130.	*	0.0	0.0	0.2	0.0	0.0	0.1	0.2	0.2	0.0	0.0	0.5	0.5	0.2	1.2	1.3
140.	*	0.0	0.0	0.3	0.2	0.1	0.0	0.1	0.1	0.0	0.0	0.4	0.5	0.3	1.1	1.4
150.	*	0.0	0.3	0.4	0.4	0.1	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.4	0.8	1.4
160.	*	0.1	0.2	0.3	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.2	0.5	0.4	0.5	1.1
170.	*	0.3	0.1	0.2	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.2	0.5	0.4	0.6	0.9
180.	*	0.5	0.2	0.2	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.4	0.4	0.5
190.	*	0.9	0.5	0.2	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.6	0.3	0.3
200.	*	1.4	0.8	0.4	0.2	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.5	0.3	0.0
210.	*	1.6	1.1	0.4	0.2	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.4	0.1	0.0
220.	*	1.4	1.4	0.6	0.3	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.0

230.	*	1.4	1.3	0.5	0.4	0.5	0.0	0.0	0.2	0.1	0.0	0.0	0.1	0.1	0.0	0.0
240.	*	1.2	1.2	0.3	0.5	0.6	0.0	0.0	0.4	0.1	0.0	0.0	0.0	0.0	0.0	0.0
250.	*	1.1	1.2	0.1	0.5	0.8	0.0	0.0	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.0
260.	*	0.9	1.2	0.1	0.5	0.8	0.0	0.1	1.0	0.3	0.1	0.0	0.0	0.0	0.0	0.0
270.	*	0.7	1.3	0.2	0.1	0.8	0.0	0.2	1.1	0.3	0.1	0.0	0.0	0.0	0.0	0.0
280.	*	0.5	1.2	0.4	0.3	0.6	0.0	0.2	1.1	0.5	0.1	0.0	0.0	0.0	0.0	0.0
290.	*	0.4	1.3	0.7	0.4	0.5	0.2	0.3	1.1	0.4	0.2	0.0	0.0	0.0	0.0	0.0
300.	*	0.4	1.3	0.8	0.5	0.4	0.2	0.4	1.0	0.6	0.2	0.0	0.0	0.0	0.0	0.0
310.	*	0.4	1.4	1.1	0.6	0.5	0.3	0.4	0.9	0.7	0.2	0.0	0.0	0.0	0.0	0.0
320.	*	0.3	1.3	1.2	0.5	0.3	0.2	0.3	0.9	0.8	0.3	0.0	0.0	0.0	0.0	0.0
330.	*	0.2	1.1	1.4	0.4	0.2	0.4	0.3	0.8	0.9	0.3	0.0	0.0	0.0	0.0	0.0
340.	*	0.2	0.7	1.2	0.2	0.1	0.4	0.6	0.9	0.9	0.3	0.0	0.0	0.0	0.0	0.0
350.	*	0.1	0.4	0.9	0.0	0.0	0.4	0.5	0.8	0.9	0.3	0.0	0.0	0.2	0.1	0.0
360.	*	0.1	0.1	0.4	0.0	0.0	0.4	0.5	0.9	1.2	0.5	0.0	0.0	0.5	0.2	0.1
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MAX	*	1.6	1.4	1.4	0.6	0.8	0.4	0.6	1.1	1.3	0.9	0.6	0.6	1.3	1.3	1.4
DEGR.	*	210	220	330	310	250	0	340	270	10	20	100	40	30	50	140

THE HIGHEST CONCENTRATION OF 1.60 PPM OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
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The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6054.9	5445.6	*	60.	290.	AG	333.	100.0	1.0	30.0	0.48	3.1
2.	Char/Merr WB	*	6250.4	5435.2	6323.7	5493.2	*	93.	52.	AG	333.	100.0	1.0	30.0	0.71	4.7
3.	Char/Merr NB R	*	6291.7	5369.7	6313.9	5354.6	*	27.	124.	AG	66.	100.0	1.0	10.0	0.14	1.4
4.	Char/Merr NB LTT	*	6280.4	5347.2	6395.2	5266.3	*	140.	125.	AG	207.	100.0	1.0	20.0	0.83	7.1
5.	Char/Merr EB	*	6104.2	5362.2	6064.9	5347.6	*	42.	250.	AG	230.	100.0	1.0	20.0	0.38	2.1
6.	Char/Cam SB L	*	5384.1	4834.2	5408.6	4932.0	*	101.	14.	AG	94.	100.0	1.0	10.0	0.66	5.1
7.	Char/Cam SB TR	*	5360.8	4833.5	5392.6	4936.4	*	108.	17.	AG	230.	100.0	1.0	20.0	0.86	5.5
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5448.9	4784.7	*	39.	103.	AG	175.	100.0	1.0	20.0	0.24	2.0
9.	Char/Cam NB L	*	5363.0	4722.4	5361.1	4639.9	*	82.	181.	AG	94.	100.0	1.0	10.0	0.54	4.2
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.3	4657.5	*	66.	179.	AG	230.	100.0	1.0	20.0	0.67	3.4
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5222.9	4740.6	*	80.	271.	AG	263.	100.0	1.0	30.0	0.49	4.1
12.	Sud/Merr SB L	*	6532.7	5210.3	6493.6	5238.2	*	48.	305.	AG	125.	100.0	1.0	10.0	0.66	2.4
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6480.9	5212.4	*	43.	300.	AG	214.	100.0	1.0	30.0	0.22	2.2
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6669.4	5076.1	*	98.	150.	AG	276.	100.0	1.0	30.0	0.55	5.0
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6482.0	5121.0	*	48.	239.	AG	426.	100.0	1.0	40.0	0.34	2.5
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6741.1	5415.5	*	59.	322.	AG	155.	100.0	1.0	20.0	0.30	3.0
17.	Sud/Sur SEB	*	6757.2	5330.0	6747.9	5332.3	*	10.	284.	AG	102.	100.0	1.0	10.0	0.06	0.5
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6750.6	5242.3	*	47.	249.	AG	337.	100.0	1.0	30.0	0.39	2.4
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	802.	9.8	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1038.	9.8	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1204.	9.8	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	870.	9.8	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	923.	9.8	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1472.	9.8	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	877.	9.8	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1546.	9.8	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	285.	9.8	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	483.	9.8	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	405.	9.8	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	338.	9.8	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	25.	9.8	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1421.	9.8	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1512.	9.8	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	487.	9.8	1.0	78.0		

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JOB: Government Center Garage RUN: 2013EX

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ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Char/Merr SB	*	100	76	3.0	436	1600	54.39	1	3
2.	Char/Merr WB	*	100	76	3.0	650	1600	54.39	1	3
3.	Char/Merr NB R	*	100	45	3.0	109	1600	54.39	1	3
4.	Char/Merr NB LTT	*	100	71	3.0	637	1600	54.39	1	3

5.	Char/Merr EB	*	100	79	3.0	194	1600	54.39	1	3
6.	Char/Cam SB L	*	90	58	3.0	318	1600	54.39	1	3
7.	Char/Cam SB TR	*	90	71	3.0	429	1600	54.39	1	3
8.	Char/Cam WB LTTR	*	90	54	3.0	265	1600	54.39	1	3
9.	Char/Cam NB L	*	90	58	3.0	260	1600	54.39	1	3
10.	Char/Cam NB TR	*	90	71	3.0	330	1600	54.39	1	3
11.	Char/Cam EB TTTR	*	90	54	3.0	811	1600	54.39	1	3
12.	Sud/Merr SB L	*	100	86	3.0	95	1600	54.39	1	3
13.	Sud/Merr SB TTT	*	100	49	3.0	484	1600	54.39	1	3
14.	Sud/Merr NB TTTR	*	100	63	3.0	854	1600	54.39	1	3
15.	Sud/Merr EB LTTR	*	100	73	3.0	487	1600	54.39	1	3
16.	Sud/Sur SB LTT	*	100	53	3.0	405	1600	54.39	1	3
17.	Sud/Sur SEB	*	100	70	3.0	25	1600	54.39	1	3
18.	Sud/Sur EB TTR	*	100	77	3.0	338	1600	54.39	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Char/Merr NE1	*	6063.7	5511.0	6.0	*
2.	Char/Merr NE2	*	6133.9	5484.8	6.0	*
3.	Char/Merr NE3	*	6204.2	5458.5	6.0	*
4.	Char/Merr NE4	*	6265.6	5501.5	6.0	*
5.	Char/Merr NE5	*	6327.1	5544.5	6.0	*
6.	Char/Merr SE1	*	6443.7	5491.9	6.0	*
7.	Char/Merr SE2	*	6382.2	5448.9	6.0	*
8.	Char/Merr SE3	*	6320.8	5405.9	6.0	*
9.	Char/Merr SE4	*	6380.5	5360.4	6.0	*
10.	Char/Merr SE5	*	6440.1	5315.0	6.0	*
11.	Char/Merr SW1	*	6332.0	5249.0	6.0	*
12.	Char/Merr SW2	*	6272.3	5294.5	6.0	*
13.	Char/Merr SW3	*	6212.6	5339.9	6.0	*
14.	Char/Merr SW4	*	6141.6	5315.8	6.0	*
15.	Char/Merr SW5	*	6070.6	5291.7	6.0	*
16.	Char/Merr NW1	*	5902.1	5359.1	6.0	*
17.	Char/Merr NW2	*	5973.1	5383.2	6.0	*
18.	Char/Merr NW3	*	6044.1	5407.3	6.0	*
19.	Char/Merr NW4	*	5973.9	5433.5	6.0	*
20.	Char/Merr NW5	*	5903.6	5459.8	6.0	*
21.	Char/Cam NE1	*	5490.2	4963.0	6.0	*
22.	Char/Cam NE2	*	5459.0	4894.8	6.0	*
23.	Char/Cam NE3	*	5427.8	4826.6	6.0	*
24.	Char/Cam NE4	*	5500.4	4807.6	6.0	*
25.	Char/Cam NE5	*	5572.9	4788.7	6.0	*
26.	Char/Cam SE1	*	5553.9	4667.5	6.0	*
27.	Char/Cam SE2	*	5481.3	4686.5	6.0	*

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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
28.	Char/Cam SE3	*	5408.7	4705.4	6.0	*
29.	Char/Cam SE4	*	5409.4	4630.4	6.0	*
30.	Char/Cam SE5	*	5410.1	4555.4	6.0	*
31.	Char/Cam SW1	*	5312.0	4561.9	6.0	*
32.	Char/Cam SW2	*	5310.7	4636.9	6.0	*
33.	Char/Cam SW3	*	5310.7	4711.9	6.0	*
34.	Char/Cam SW4	*	5235.6	4712.1	6.0	*
35.	Char/Cam SW5	*	5160.6	4711.9	6.0	*
36.	Char/Cam NW1	*	5167.9	4822.4	6.0	*
37.	Char/Cam NW2	*	5242.9	4822.1	6.0	*
38.	Char/Cam NW3	*	5317.9	4821.9	6.0	*
39.	Char/Cam NW4	*	5349.1	4890.1	6.0	*
40.	Char/Cam NW5	*	5380.3	4958.3	6.0	*

PAGE 4

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) *	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

0. *	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.1	0.1	0.9	0.8	0.6	0.4	0.7	0.1	0.1	0.3	0.2 0.2
10. *	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.2	0.1	0.8	0.9	0.5	0.3	0.7	0.1	0.1	0.5	0.2 0.2
20. *	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.1	0.1	0.7	0.9	0.8	0.4	0.6	0.1	0.1	0.6	0.2 0.2
30. *	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.1	0.0	0.7	0.9	0.9	0.6	0.6	0.1	0.1	0.8	0.2 0.2
40. *	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.0	0.6	0.7	0.9	0.6	0.6	0.1	0.2	0.9	0.2 0.2
50. *	0.0	0.0	0.2	0.1	0.1	0.2	0.2	0.2	0.0	0.0	0.6	0.7	0.7	0.6	0.7	0.2	0.3	0.9	0.2 0.2
60. *	0.0	0.1	0.5	0.2	0.2	0.1	0.1	0.1	0.0	0.1	0.7	0.7	0.5	0.6	0.6	0.3	0.4	1.1	0.3 0.2
70. *	0.1	0.1	0.7	0.3	0.3	0.0	0.0	0.0	0.0	0.1	0.6	0.7	0.5	0.4	0.4	0.5	0.6	1.1	0.6 0.2
80. *	0.1	0.3	0.9	0.4	0.3	0.0	0.0	0.0	0.0	0.1	0.5	0.8	0.5	0.3	0.2	0.7	0.8	1.1	0.7 0.5
90. *	0.2	0.4	0.9	0.6	0.3	0.0	0.0	0.0	0.0	0.1	0.4	0.7	0.6	0.5	0.3	0.5	0.8	0.9	0.9 0.6
100. *	0.3	0.5	1.0	0.7	0.3	0.0	0.0	0.0	0.0	0.2	0.5	0.8	0.7	0.3	0.3	0.5	0.5	0.7	0.8 0.7
110. *	0.4	0.6	0.8	0.9	0.3	0.0	0.0	0.0	0.1	0.3	0.7	0.7	0.8	0.4	0.1	0.3	0.6	0.7	0.6 0.4
120. *	0.6	0.9	1.0	0.9	0.2	0.0	0.0	0.3	0.3	0.6	0.6	0.7	0.7	0.1	0.1	0.2	0.4	0.6	0.4 0.3
130. *	0.8	0.7	1.0	1.1	0.2	0.0	0.1	0.4	0.5	0.8	0.2	0.3	0.4	0.1	0.0	0.2	0.2	0.4	0.2 0.1
140. *	0.6	0.7	1.0	1.4	0.5	0.1	0.3	0.6	0.8	1.1	0.3	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.2 0.1
150. *	0.6	0.5	0.7	1.5	0.5	0.3	0.3	0.8	0.7	1.0	0.1	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1 0.1
160. *	0.8	0.3	0.5	1.2	0.6	0.2	0.4	0.5	0.5	0.7	0.1	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1 0.1
170. *	0.8	0.3	0.5	1.2	0.6	0.3	0.3	0.6	0.5	0.5	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.1 0.1
180. *	0.8	0.4	0.5	1.2	0.8	0.1	0.2	0.6	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1 0.1
190. *	0.5	0.6	0.4	1.0	1.0	0.3	0.4	0.6	0.6	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1 0.1
200. *	0.4	0.8	0.5	0.6	1.0	0.2	0.4	0.6	0.6	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1 0.1
210. *	0.3	0.9	0.5	0.6	1.0	0.2	0.4	0.6	0.6	0.5	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.2	0.1 0.1
220. *	0.3	0.9	0.6	0.5	0.8	0.2	0.3	0.4	0.6	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2 0.0
230. *	0.3	0.8	0.6	0.5	0.6	0.3	0.4	0.3	0.6	0.5	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1 0.0
240. *	0.2	0.7	0.6	0.4	0.5	0.5	0.5	0.5	0.6	0.7	0.0	0.0	0.1	0.1	0.0	0.1	0.2	0.2	0.0 0.0
250. *	0.2	0.4	0.6	0.3	0.3	0.7	0.5	0.6	0.6	0.7	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.0 0.0
260. *	0.2	0.3	0.7	0.2	0.1	0.9	1.0	0.8	0.6	0.8	0.0	0.1	0.3	0.2	0.2	0.0	0.0	0.1	0.0 0.0
270. *	0.2	0.3	0.5	0.1	0.1	0.6	1.1	0.7	0.7	0.8	0.1	0.1	0.4	0.3	0.2	0.0	0.0	0.0	0.0 0.0
280. *	0.2	0.2	0.3	0.1	0.0	0.4	0.9	0.9	0.7	0.7	0.1	0.1	0.4	0.4	0.2	0.0	0.0	0.0	0.0 0.0
290. *	0.1	0.1	0.2	0.0	0.0	0.3	0.7	0.8	0.7	0.8	0.1	0.3	0.5	0.4	0.2	0.0	0.0	0.1	0.1 0.0
300. *	0.0	0.1	0.1	0.0	0.0	0.2	0.5	0.8	0.6	0.5	0.4	0.3	0.6	0.5	0.2	0.0	0.0	0.2	0.1 0.1
310. *	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.8	0.4	0.4	0.5	0.4	0.6	0.6	0.2	0.0	0.0	0.2	0.2 0.1
320. *	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.8	0.4	0.4	0.6	0.6	0.6	0.7	0.3	0.0	0.1	0.2	0.2 0.1
330. *	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.8	0.3	0.2	0.7	0.4	0.6	0.6	0.3	0.0	0.1	0.2	0.2 0.2
340. *	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.7	0.2	0.1	0.8	0.5	0.4	0.5	0.5	0.1	0.1	0.2	0.2 0.2
350. *	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.6	0.3	0.1	0.9	0.8	0.4	0.4	0.5	0.1	0.1	0.2	0.2 0.2
360. *	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.1	0.1	0.9	0.8	0.6	0.4	0.7	0.1	0.1	0.3	0.2 0.2
MAX *	0.8	0.9	1.0	1.5	1.0	0.9	1.1	0.9	0.8	1.1	0.9	0.9	0.9	0.7	0.7	0.7	0.8	1.1	0.9 0.7
DEGR. *	130	120	100	150	190	260	270	280	140	140	0	10	30	320	0	80	80	60	90 100

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM)	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	*	0.1	0.2	0.3	0.0	0.0	0.3	0.4	0.8	0.7	0.5	0.3	0.6	0.7	1.0	0.4	0.0	0.0	0.0	0.0	0.0
10.	*	0.1	0.2	0.2	0.0	0.0	0.3	0.3	0.6	0.5	0.3	0.7	0.7	0.8	1.1	0.4	0.0	0.0	0.0	0.0	0.0
20.	*	0.0	0.1	0.2	0.0	0.0	0.3	0.3	0.5	0.2	0.2	0.8	0.6	1.0	1.0	0.3	0.0	0.0	0.2	0.2	0.0
30.	*	0.0	0.1	0.1	0.0	0.0	0.3	0.3	0.4	0.2	0.2	0.6	0.9	0.9	1.3	0.4	0.0	0.0	0.5	0.4	0.1
40.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.1	0.5	0.7	1.0	1.5	0.6	0.0	0.2	0.8	0.5	0.2
50.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.4	0.7	0.9	1.4	0.7	0.0	0.2	0.9	0.8	0.2
60.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.7	0.8	1.4	1.0	0.2	0.3	0.8	0.9	0.2
70.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.7	0.7	1.1	0.9	0.2	0.3	0.8	0.9	0.2
80.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.6	0.9	1.0	0.9	0.4	0.4	0.7	0.8	0.2
90.	*	0.0	0.0	0.1	0.1	0.0	0.3	0.4	0.4	0.1	0.0	0.2	0.4	0.8	0.6	0.8	0.6	0.5	0.7	0.8	0.2
100.	*	0.0	0.0	0.2	0.2	0.1	0.2	0.3	0.3	0.0	0.0	0.2	0.2	0.8	0.5	0.5	0.6	0.6	0.9	0.8	0.2
110.	*	0.0	0.0	0.3	0.3	0.3	0.1	0.1	0.2	0.0	0.0	0.2	0.2	0.7	0.4	0.1	0.7	0.7	0.9	0.9	0.2
120.	*	0.0	0.1	0.4	0.4	0.4	0.0	0.1	0.1	0.0	0.0	0.2	0.2	0.5	0.1	0.1	0.9	0.8	0.9	1.0	0.3
130.	*	0.1	0.2	0.4	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.7	0.8	0.9	1.2	0.5
140.	*	0.1	0.2	0.5	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.1	0.1	0.7	0.9	0.8	1.2	0.7
150.	*	0.1	0.2	0.6	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.4	0.1	0.0	0.6	0.8	1.0	1.2	0.9
160.	*	0.1	0.2	0.7	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.0	0.4	0.7	1.0	1.0	1.2
170.	*	0.1	0.2	0.6	0.3	0.3	0.0	0.0	0.1	0.1	0.0	0.2	0.2	0.2	0.0	0.0	0.4	0.8	0.9	1.0	1.4
180.	*	0.2	0.3	0.8	0.3	0.3	0.0	0.0	0.3	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.4	0.7	0.8	1.1	1.5
190.	*	0.2	0.5	0.9	0.3	0.3	0.0	0.0	0.4	0.2	0.2	0.0	0.0	0.1	0.0	0.0	0.4	0.6	0.7	0.7	1.2
200.	*	0.3	0.6	0.8	0.4	0.3	0.0	0.1	0.6	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.7	0.5	0.8
210.	*	0.6	0.7	1.0	0.5	0.4	0.0	0.1	0.8	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.5	0.7	0.4	0.5
220.	*	0.8	0.7	0.8	0.5	0.4	0.1	0.1	0.9	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.7	0.3	0.3
230.	*	0.8	0.8	0.8	0.6	0.6	0.1	0.1	0.9	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.3	0.2
240.	*	0.7	1.0	0.9	0.9	0.6	0.1	0.1	0.9	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.2	0.1
250.	*	0.6	0.9	0.8	1.0	0.7	0.1	0.2	0.9	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.2	0.1
260.	*	0.3	0.7	0.9	1.0	0.8	0.2	0.4	1.1	0.2	0.2	0.0	0.0	0.2	0.1	0.1	0.3	0.4	0.4	0.1	0.0
270.	*	0.2	0.6	0.7	0.7	0.9	0.4	0.6	1.2	0.2	0.2	0.0	0.0	0.4	0.2	0.1	0.2	0.2	0.3	0.0	0.0
280.	*	0.2	0.6	0.7	0.6	0.6	0.6	0.7	1.4	0.4	0.2	0.0	0.1	0.8	0.3	0.3	0.1	0.1	0.1	0.0	0.0
290.	*	0.2	0.5	0.6	0.3	0.3	0.8	0.7	1.5	0.6	0.3	0.0	0.1	1.1	0.4	0.3	0.0	0.0	0.0	0.0	0.0
300.	*	0.2	0.5	0.6	0.4	0.2	0.5	0.8	1.2	0.7	0.3	0.1	0.2	1.2	0.4	0.4	0.0	0.0	0.0	0.0	0.0
310.	*	0.2	0.3	0.6	0.4	0.2	0.7	0.5	1.0	0.8	0.4	0.1	0.3	1.1	0.5	0.4	0.0	0.0	0.0	0.0	0.0
320.	*	0.2	0.2	0.6	0.2	0.1	0.6	0.8	0.9	1.0	0.6	0.2	0.4	1.0	0.6	0.4	0.0	0.0	0.0	0.0	0.0
330.	*	0.2	0.2	0.6	0.2	0.1	0.6	0.7	0.8	1.0	0.7	0.3	0.4	0.9	0.7	0.4	0.0	0.0	0.0	0.0	0.0
340.	*	0.2	0.3	0.6	0.1	0.0	0.5	0.6	0.7	1.1	0.7	0.3	0.4	0.8	0.7	0.3	0.0	0.0	0.0	0.0	0.0
350.	*	0.1	0.2	0.5	0.1	0.0	0.3	0.5	0.8	0.9	0.8	0.3	0.4	0.7	1.0	0.4	0.0	0.0	0.0	0.0	0.0
360.	*	0.1	0.2	0.3	0.0	0.0	0.3	0.4	0.8	0.7	0.5	0.3	0.6	0.7	1.0	0.4	0.0	0.0	0.0	0.0	0.0
MAX	*	0.8	1.0	1.0	1.0	0.9	0.8	0.8	1.5	1.1	0.8	0.8	0.9	1.2	1.5	1.0	0.9	0.9	1.0	1.2	1.5

DEGR. * 220 240 210 250 270 290 320 290 340 350 20 30 300 40 60 120 140 150
130 180

THE HIGHEST CONCENTRATION OF 1.50 PPM OCCURRED AT RECEPTOR REC4 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17: 7:40

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6042.2	5450.2	*	74.	290.	AG	328.	100.0	1.0	30.0	0.56	3.8
2.	Char/Merr WB	*	6250.4	5435.2	6300.3	5474.7	*	64.	52.	AG	341.	100.0	1.0	30.0	0.55	3.2
3.	Char/Merr NB R	*	6291.7	5369.7	6341.8	5335.7	*	61.	124.	AG	67.	100.0	1.0	10.0	0.31	3.1
4.	Char/Merr NB LTT	*	6280.4	5347.2	6349.1	5298.8	*	84.	125.	AG	198.	100.0	1.0	20.0	0.52	4.3
5.	Char/Merr EB	*	6104.2	5362.2	6005.8	5325.6	*	105.	250.	AG	230.	100.0	1.0	20.0	0.81	5.3
6.	Char/Cam SB L	*	5384.1	4834.2	5401.1	4902.3	*	70.	14.	AG	88.	100.0	1.0	10.0	0.38	3.6
7.	Char/Cam SB TR	*	5360.8	4833.5	5374.3	4877.1	*	46.	17.	AG	210.	100.0	1.0	20.0	0.32	2.3
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5475.3	4778.6	*	66.	103.	AG	181.	100.0	1.0	20.0	0.37	3.4
9.	Char/Cam NB L	*	5363.0	4722.4	5361.0	4631.8	*	91.	181.	AG	88.	100.0	1.0	10.0	0.49	4.6
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.8	4624.7	*	99.	179.	AG	210.	100.0	1.0	20.0	0.68	5.0
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5220.6	4740.7	*	82.	271.	AG	271.	100.0	1.0	30.0	0.46	4.2
12.	Sud/Merr SB L	*	6532.7	5210.3	6496.1	5236.4	*	45.	305.	AG	123.	100.0	1.0	10.0	0.56	2.3
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6487.3	5208.8	*	36.	300.	AG	219.	100.0	1.0	30.0	0.18	1.8
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6672.2	5071.1	*	104.	150.	AG	289.	100.0	1.0	30.0	0.62	5.3
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6458.9	5107.1	*	75.	239.	AG	420.	100.0	1.0	40.0	0.52	3.8
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6739.2	5418.0	*	62.	322.	AG	204.	100.0	1.0	20.0	0.40	3.1
17.	Sud/Sur SEB	*	6757.2	5330.0	6742.4	5333.7	*	15.	284.	AG	117.	100.0	1.0	10.0	0.15	0.8
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6722.2	5231.2	*	78.	249.	AG	219.	100.0	1.0	30.0	0.39	3.9
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	818.	9.8	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1226.	9.8	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1219.	9.8	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	859.	9.8	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	796.	9.8	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1264.	9.8	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	954.	9.8	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1198.	9.8	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	805.	9.8	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	405.	9.8	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	322.	9.8	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	853.	9.8	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	35.	9.8	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1185.	9.8	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1465.	9.8	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	766.	9.8	1.0	78.0		

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17: 7:40

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Char/Merr SB	*	100	75	3.0	541	1600	54.39	1	3
2.	Char/Merr WB	*	100	78	3.0	449	1600	54.39	1	3
3.	Char/Merr NB R	*	100	46	3.0	241	1600	54.39	1	3
4.	Char/Merr NB LTT	*	100	68	3.0	452	1600	54.39	1	3
5.	Char/Merr EB	*	100	79	3.0	417	1600	54.39	1	3
6.	Char/Cam SB L	*	100	60	3.0	214	1600	54.39	1	3
7.	Char/Cam SB TR	*	100	72	3.0	233	1600	54.39	1	3
8.	Char/Cam WB LTTR	*	100	62	3.0	391	1600	54.39	1	3
9.	Char/Cam NB L	*	100	60	3.0	276	1600	54.39	1	3
10.	Char/Cam NB TR	*	100	72	3.0	503	1600	54.39	1	3
11.	Char/Cam EB TTTR	*	100	62	3.0	726	1600	54.39	1	3
12.	Sud/Merr SB L	*	100	84	3.0	98	1600	54.39	1	3
13.	Sud/Merr SB TTT	*	100	50	3.0	394	1600	54.39	1	3
14.	Sud/Merr NB TTTR	*	100	66	3.0	863	1600	54.39	1	3
15.	Sud/Merr EB LTTR	*	100	72	3.0	766	1600	54.39	1	3
16.	Sud/Sur SB LTT	*	100	70	3.0	322	1600	54.39	1	3
17.	Sud/Sur SEB	*	100	80	3.0	35	1600	54.39	1	3
18.	Sud/Sur EB TTR	*	100	50	3.0	853	1600	54.39	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Char/Merr NE1	*	6063.7	5511.0	6.0
2.	Char/Merr NE2	*	6133.9	5484.8	6.0
3.	Char/Merr NE3	*	6204.2	5458.5	6.0
4.	Char/Merr NE4	*	6265.6	5501.5	6.0
5.	Char/Merr NE5	*	6327.1	5544.5	6.0
6.	Char/Merr SE1	*	6443.7	5491.9	6.0
7.	Char/Merr SE2	*	6382.2	5448.9	6.0
8.	Char/Merr SE3	*	6320.8	5405.9	6.0
9.	Char/Merr SE4	*	6380.5	5360.4	6.0
10.	Char/Merr SE5	*	6440.1	5315.0	6.0
11.	Char/Merr SW1	*	6332.0	5249.0	6.0
12.	Char/Merr SW2	*	6272.3	5294.5	6.0
13.	Char/Merr SW3	*	6212.6	5339.9	6.0
14.	Char/Merr SW4	*	6141.6	5315.8	6.0
15.	Char/Merr SW5	*	6070.6	5291.7	6.0
16.	Char/Merr NW1	*	5902.1	5359.1	6.0
17.	Char/Merr NW2	*	5973.1	5383.2	6.0
18.	Char/Merr NW3	*	6044.1	5407.3	6.0
19.	Char/Merr NW4	*	5973.9	5433.5	6.0
20.	Char/Merr NW5	*	5903.6	5459.8	6.0
21.	Char/Cam NE1	*	5490.2	4963.0	6.0
22.	Char/Cam NE2	*	5459.0	4894.8	6.0
23.	Char/Cam NE3	*	5427.8	4826.6	6.0
24.	Char/Cam NE4	*	5500.4	4807.6	6.0
25.	Char/Cam NE5	*	5572.9	4788.7	6.0
26.	Char/Cam SE1	*	5553.9	4667.5	6.0
27.	Char/Cam SE2	*	5481.3	4686.5	6.0

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17: 7:40

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
28.	Char/Cam SE3	*	5408.7	4705.4	6.0
29.	Char/Cam SE4	*	5409.4	4630.4	6.0
30.	Char/Cam SE5	*	5410.1	4555.4	6.0
31.	Char/Cam SW1	*	5312.0	4561.9	6.0
32.	Char/Cam SW2	*	5310.7	4636.9	6.0
33.	Char/Cam SW3	*	5310.7	4711.9	6.0
34.	Char/Cam SW4	*	5235.6	4712.1	6.0
35.	Char/Cam SW5	*	5160.6	4711.9	6.0
36.	Char/Cam NW1	*	5167.9	4822.4	6.0
37.	Char/Cam NW2	*	5242.9	4822.1	6.0
38.	Char/Cam NW3	*	5317.9	4821.9	6.0
39.	Char/Cam NW4	*	5349.1	4890.1	6.0
40.	Char/Cam NW5	*	5380.3	4958.3	6.0

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

0.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.8	0.8	0.6	0.4	0.8	0.1	0.1	0.6	0.2	0.2
10.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.1	0.6	0.9	0.6	0.3	0.8	0.1	0.1	0.8	0.2	0.2
20.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.4	0.2	0.1	0.5	0.9	0.7	0.4	0.7	0.1	0.1	0.9	0.2	0.2
30.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.4	0.1	0.0	0.5	0.9	1.0	0.6	0.6	0.1	0.2	0.9	0.2	0.2
40.	*	0.0	0.0	0.1	0.1	0.0	0.3	0.3	0.4	0.1	0.0	0.3	0.8	0.9	0.5	0.6	0.1	0.3	0.9	0.2	0.2
50.	*	0.0	0.0	0.2	0.1	0.1	0.2	0.2	0.3	0.0	0.0	0.3	0.7	0.8	0.6	0.7	0.2	0.4	0.9	0.2	0.2
60.	*	0.0	0.1	0.4	0.3	0.2	0.1	0.1	0.1	0.0	0.0	0.4	0.6	0.5	0.6	0.5	0.4	0.5	1.0	0.3	0.2
70.	*	0.1	0.1	0.6	0.4	0.3	0.0	0.0	0.1	0.0	0.1	0.3	0.6	0.5	0.4	0.3	0.5	0.7	1.2	0.6	0.3
80.	*	0.1	0.3	0.8	0.4	0.4	0.0	0.0	0.0	0.0	0.1	0.4	0.7	0.4	0.3	0.2	0.7	0.8	1.1	0.8	0.5
90.	*	0.2	0.4	0.9	0.4	0.3	0.0	0.0	0.0	0.0	0.1	0.5	0.6	0.5	0.3	0.2	0.6	0.7	0.9	1.0	0.7
100.	*	0.2	0.4	0.9	0.3	0.3	0.0	0.0	0.0	0.0	0.3	0.7	0.5	0.6	0.3	0.2	0.5	0.5	0.7	0.8	0.7
110.	*	0.4	0.6	0.8	0.4	0.3	0.0	0.0	0.0	0.2	0.3	0.7	0.6	0.7	0.4	0.2	0.3	0.6	0.6	0.6	0.5
120.	*	0.5	0.7	1.0	0.5	0.3	0.0	0.0	0.3	0.3	0.6	0.7	0.7	0.6	0.2	0.2	0.3	0.6	0.5	0.4	0.4
130.	*	0.7	0.7	1.2	0.9	0.3	0.0	0.1	0.4	0.5	0.8	0.4	0.4	0.3	0.2	0.0	0.2	0.5	0.4	0.3	0.2
140.	*	0.6	0.7	1.0	1.3	0.4	0.1	0.3	0.5	0.7	1.0	0.3	0.2	0.2	0.0	0.0	0.2	0.4	0.5	0.3	0.2
150.	*	0.6	0.5	0.7	1.6	0.6	0.3	0.3	0.7	0.7	1.0	0.2	0.1	0.1	0.0	0.0	0.2	0.4	0.5	0.3	0.2
160.	*	0.8	0.3	0.6	1.3	0.6	0.3	0.4	0.6	0.5	0.9	0.1	0.1	0.0	0.0	0.0	0.2	0.3	0.5	0.2	0.1
170.	*	0.9	0.3	0.5	1.3	0.5	0.3	0.3	0.6	0.5	0.6	0.1	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.2	0.1
180.	*	0.9	0.4	0.5	1.2	0.6	0.2	0.1	0.6	0.4	0.5	0.1	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.1
190.	*	0.8	0.5	0.4	1.0	0.7	0.1	0.3	0.6	0.3	0.5	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.1
200.	*	0.7	0.9	0.5	0.7	0.7	0.1	0.3	0.6	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1
210.	*	0.4	1.0	0.6	0.8	0.8	0.2	0.3	0.6	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.1	0.1
220.	*	0.4	1.0	0.6	0.6	0.8	0.2	0.3	0.4	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.1	0.0
230.	*	0.3	0.9	0.7	0.5	0.7	0.3	0.4	0.4	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1	0.0
240.	*	0.2	0.7	0.6	0.5	0.6	0.5	0.5	0.5	0.7	0.4	0.0	0.0	0.1	0.1	0.0	0.1	0.2	0.2	0.0	0.0
250.	*	0.2	0.5	0.7	0.4	0.3	0.7	0.7	0.7	0.7	0.5	0.0	0.0	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0
260.	*	0.2	0.5	0.7	0.2	0.2	0.9	1.0	1.0	0.8	0.6	0.0	0.1	0.3	0.3	0.2	0.0	0.0	0.1	0.0	0.0
270.	*	0.2	0.4	0.5	0.2	0.1	0.6	1.0	0.9	0.9	0.6	0.1	0.2	0.5	0.5	0.2	0.0	0.0	0.0	0.0	0.0
280.	*	0.2	0.2	0.3	0.1	0.0	0.4	0.8	1.0	0.7	0.7	0.2	0.2	0.5	0.6	0.3	0.0	0.0	0.0	0.0	0.0
290.	*	0.1	0.1	0.2	0.0	0.0	0.3	0.5	1.0	0.7	0.8	0.2	0.4	0.5	0.5	0.3	0.0	0.0	0.1	0.1	0.0
300.	*	0.0	0.1	0.1	0.0	0.0	0.3	0.4	0.9	0.7	0.5	0.5	0.4	0.6	0.6	0.4	0.0	0.0	0.2	0.2	0.1
310.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.9	0.5	0.3	0.5	0.4	0.6	0.7	0.5	0.0	0.0	0.2	0.2	0.1
320.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.8	0.4	0.3	0.6	0.6	0.6	0.7	0.6	0.0	0.1	0.2	0.2	0.1
330.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.7	0.3	0.1	0.7	0.4	0.6	0.6	0.7	0.0	0.1	0.3	0.2	0.2
340.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.2	0.1	0.8	0.6	0.4	0.5	0.8	0.1	0.1	0.3	0.2	0.2
350.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.2	0.1	0.8	0.6	0.5	0.5	0.9	0.1	0.1	0.5	0.2	0.2
360.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.8	0.8	0.6	0.4	0.8	0.1	0.1	0.6	0.2	0.2
MAX	*	0.9	1.0	1.2	1.6	0.8	0.9	1.0	1.0	0.9	1.0	0.8	0.9	1.0	0.7	0.9	0.7	0.8	1.2	1.0	0.7
DEGR.	*	170	210	130	150	210	260	260	260	270	140	0	10	30	310	350	80	80	70	90	90

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	*	0.1	0.2	0.2	0.0	0.0	0.3	0.5	0.5	0.7	0.5	0.3	0.4	0.4	1.0	0.3	0.0	0.0	0.0	0.0	0.0
10.	*	0.1	0.2	0.2	0.0	0.0	0.3	0.3	0.5	0.4	0.5	0.6	0.6	0.7	1.0	0.3	0.0	0.0	0.0	0.0	0.0
20.	*	0.0	0.1	0.1	0.0	0.0	0.3	0.3	0.6	0.3	0.1	0.7	0.5	0.8	1.0	0.3	0.0	0.0	0.1	0.1	0.0
30.	*	0.0	0.0	0.1	0.0	0.0	0.3	0.3	0.5	0.2	0.1	0.7	0.8	0.8	1.2	0.3	0.0	0.0	0.3	0.1	0.1
40.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.6	0.9	0.6	1.4	0.4	0.0	0.0	0.4	0.2	0.1
50.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.5	0.9	0.8	1.4	0.6	0.0	0.1	0.6	0.2	0.2
60.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.1	0.4	0.8	0.7	1.2	0.8	0.1	0.2	0.6	0.2	0.2
70.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.4	0.2	0.1	0.3	0.8	0.8	1.1	0.9	0.1	0.2	0.6	0.2	0.2
80.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.4	0.1	0.0	0.3	0.6	0.8	0.9	1.0	0.4	0.3	0.5	0.3	0.2
90.	*	0.0	0.0	0.1	0.1	0.0	0.3	0.3	0.4	0.1	0.0	0.2	0.6	0.8	0.6	0.7	0.3	0.6	0.7	0.3	0.2
100.	*	0.0	0.0	0.2	0.1	0.1	0.2	0.2	0.3	0.0	0.0	0.2	0.3	0.7	0.4	0.5	0.4	0.7	0.8	0.4	0.2
110.	*	0.0	0.0	0.3	0.3	0.2	0.1	0.1	0.1	0.0	0.0	0.2	0.3	0.7	0.3	0.2	0.7	0.7	0.9	0.6	0.2
120.	*	0.0	0.1	0.5	0.4	0.3	0.0	0.0	0.1	0.0	0.0	0.2	0.2	0.6	0.2	0.1	0.8	0.7	0.8	0.9	0.3
130.	*	0.1	0.2	0.6	0.4	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.1	0.1	0.8	0.7	0.7	1.0	0.3
140.	*	0.1	0.2	0.7	0.4	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.1	0.1	0.6	0.8	0.8	1.0	0.3
150.	*	0.1	0.2	0.6	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.1	0.0	0.6	0.8	0.9	1.0	0.5
160.	*	0.1	0.2	0.7	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.0	0.4	0.7	1.1	1.0	0.5
170.	*	0.1	0.3	0.7	0.3	0.3	0.0	0.0	0.1	0.1	0.0	0.2	0.2	0.3	0.0	0.0	0.3	0.8	0.7	1.0	0.8
180.	*	0.1	0.3	0.8	0.3	0.3	0.0	0.0	0.3	0.1	0.1	0.1	0.1	0.2	0.0	0.0	0.3	0.6	0.7	0.9	0.7
190.	*	0.3	0.5	1.0	0.3	0.3	0.0	0.0	0.6	0.2	0.2	0.0	0.1	0.1	0.0	0.0	0.3	0.5	0.6	0.7	0.7
200.	*	0.5	0.6	0.9	0.4	0.3	0.0	0.1	0.7	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.6	0.5	0.6
210.	*	0.5	0.7	1.0	0.6	0.4	0.0	0.1	0.9	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.6	0.4	0.3
220.	*	0.6	0.6	0.8	0.7	0.4	0.1	0.1	1.0	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.3	0.2
230.	*	0.5	0.7	0.8	0.8	0.5	0.1	0.2	0.9	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.3	0.1
240.	*	0.4	0.8	0.8	1.0	0.5	0.1	0.2	0.8	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.2	0.1
250.	*	0.3	0.5	0.8	0.9	0.8	0.2	0.3	0.8	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.1	0.0
260.	*	0.2	0.5	0.7	1.0	0.7	0.2	0.4	1.0	0.5	0.2	0.0	0.0	0.2	0.1	0.0	0.2	0.3	0.3	0.1	0.0
270.	*	0.2	0.4	0.6	0.8	0.6	0.3	0.6	1.1	0.7	0.2	0.0	0.0	0.4	0.2	0.1	0.1	0.2	0.2	0.0	0.0
280.	*	0.2	0.2	0.7	0.6	0.5	0.5	0.7	1.3	0.9	0.2	0.0	0.0	0.7	0.3	0.2	0.1	0.1	0.1	0.0	0.0
290.	*	0.2	0.2	0.5	0.3	0.2	0.6	0.7	1.3	1.0	0.2	0.0	0.1	1.0	0.3	0.3	0.0	0.0	0.0	0.0	0.0
300.	*	0.2	0.2	0.5	0.2	0.1	0.4	0.7	1.1	1.1	0.3	0.1	0.1	1.1	0.4	0.3	0.0	0.0	0.0	0.0	0.0
310.	*	0.2	0.2	0.5	0.1	0.1	0.5	0.5	0.9	1.4	0.5	0.1	0.3	1.0	0.4	0.3	0.0	0.0	0.0	0.0	0.0
320.	*	0.2	0.2	0.4	0.1	0.1	0.5	0.5	0.9	1.3	0.6	0.1	0.4	1.0	0.5	0.3	0.0	0.0	0.0	0.0	0.0
330.	*	0.2	0.2	0.3	0.1	0.1	0.5	0.6	0.7	1.2	0.8	0.2	0.5	0.9	0.6	0.3	0.0	0.0	0.0	0.0	0.0
340.	*	0.1	0.2	0.3	0.1	0.0	0.4	0.6	0.7	1.0	0.8	0.2	0.5	0.7	0.8	0.3	0.0	0.0	0.0	0.0	0.0
350.	*	0.1	0.2	0.2	0.1	0.0	0.3	0.5	0.6	0.8	0.8	0.3	0.4	0.6	0.9	0.3	0.0	0.0	0.0	0.0	0.0
360.	*	0.1	0.2	0.2	0.0	0.0	0.3	0.5	0.5	0.7	0.5	0.3	0.4	0.4	1.0	0.3	0.0	0.0	0.0	0.0	0.0
MAX	*	0.6	0.8	1.0	1.0	0.8	0.6	0.7	1.3	1.4	0.8	0.7	0.9	1.1	1.4	1.0	0.8	0.8	1.1	1.0	0.8

DEGR. * 220 240 190 240 250 290 300 280 310 330 20 40 300 40 80 120 140 160
130 170

THE HIGHEST CONCENTRATION OF 1.60 PPM OCCURRED AT RECEPTOR REC4 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17:10:30

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6054.9	5445.6	*	60.	290.	AG	333.	100.0	1.0	30.0	0.48
2.	Char/Merr WB	*	6250.4	5435.2	6323.7	5493.2	*	93.	52.	AG	333.	100.0	1.0	30.0	0.71
3.	Char/Merr NB R	*	6291.7	5369.7	6313.9	5354.6	*	27.	124.	AG	66.	100.0	1.0	10.0	0.14
4.	Char/Merr NB LTT	*	6280.4	5347.2	6395.2	5266.3	*	140.	125.	AG	207.	100.0	1.0	20.0	0.83
5.	Char/Merr EB	*	6104.2	5362.2	6064.9	5347.6	*	42.	250.	AG	230.	100.0	1.0	20.0	0.38
6.	Char/Cam SB L	*	5384.1	4834.2	5408.6	4932.0	*	101.	14.	AG	94.	100.0	1.0	10.0	0.66
7.	Char/Cam SB TR	*	5360.8	4833.5	5392.6	4936.4	*	108.	17.	AG	230.	100.0	1.0	20.0	0.86
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5448.9	4784.7	*	39.	103.	AG	175.	100.0	1.0	20.0	0.24
9.	Char/Cam NB L	*	5363.0	4722.4	5361.1	4639.9	*	82.	181.	AG	94.	100.0	1.0	10.0	0.54
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.3	4657.5	*	66.	179.	AG	230.	100.0	1.0	20.0	0.67
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5222.9	4740.6	*	80.	271.	AG	263.	100.0	1.0	30.0	0.49
12.	Sud/Merr SB L	*	6532.7	5210.3	6493.6	5238.2	*	48.	305.	AG	125.	100.0	1.0	10.0	0.66
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6480.9	5212.4	*	43.	300.	AG	214.	100.0	1.0	30.0	0.22
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6669.4	5076.1	*	98.	150.	AG	276.	100.0	1.0	30.0	0.55
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6482.0	5121.0	*	48.	239.	AG	426.	100.0	1.0	40.0	0.34
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6741.1	5415.5	*	59.	322.	AG	155.	100.0	1.0	20.0	0.30
17.	Sud/Sur SEB	*	6757.2	5330.0	6747.9	5332.3	*	10.	284.	AG	102.	100.0	1.0	10.0	0.06
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6750.6	5242.3	*	47.	249.	AG	337.	100.0	1.0	30.0	0.39
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	802.	9.8	1.0	84.0	
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1038.	9.8	1.0	90.0	
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1204.	9.8	1.0	98.0	
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	870.	9.8	1.0	98.0	
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	923.	9.8	1.0	78.0	
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1472.	9.8	1.0	****	
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	877.	9.8	1.0	78.0	
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1546.	9.8	1.0	90.0	
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	285.	9.8	1.0	30.0	
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	483.	9.8	1.0	54.0	
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	405.	9.8	1.0	42.0	
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	338.	9.8	1.0	54.0	
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	25.	9.8	1.0	42.0	
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1421.	9.8	1.0	98.0	
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1512.	9.8	1.0	90.0	
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	487.	9.8	1.0	78.0	

DATE : 8/ 7/13
TIME : 17:10:30

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Char/Merr SB	*	100	76	3.0	436	1600	54.39	1	3
2.	Char/Merr WB	*	100	76	3.0	650	1600	54.39	1	3
3.	Char/Merr NB R	*	100	45	3.0	109	1600	54.39	1	3
4.	Char/Merr NB LTT	*	100	71	3.0	637	1600	54.39	1	3

5.	Char/Merr EB	*	100	79	3.0	194	1600	54.39	1	3
6.	Char/Cam SB L	*	90	58	3.0	318	1600	54.39	1	3
7.	Char/Cam SB TR	*	90	71	3.0	429	1600	54.39	1	3
8.	Char/Cam WB LTTR	*	90	54	3.0	265	1600	54.39	1	3
9.	Char/Cam NB L	*	90	58	3.0	260	1600	54.39	1	3
10.	Char/Cam NB TR	*	90	71	3.0	330	1600	54.39	1	3
11.	Char/Cam EB TTTR	*	90	54	3.0	811	1600	54.39	1	3
12.	Sud/Merr SB L	*	100	86	3.0	95	1600	54.39	1	3
13.	Sud/Merr SB TTT	*	100	49	3.0	484	1600	54.39	1	3
14.	Sud/Merr NB TTTR	*	100	63	3.0	854	1600	54.39	1	3
15.	Sud/Merr EB LTTR	*	100	73	3.0	487	1600	54.39	1	3
16.	Sud/Sur SB LTT	*	100	53	3.0	405	1600	54.39	1	3
17.	Sud/Sur SEB	*	100	70	3.0	25	1600	54.39	1	3
18.	Sud/Sur EB TTR	*	100	77	3.0	338	1600	54.39	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Sud/Merr NE1	*	6492.5	5309.9	6.0	*
2.	Sud/Merr NE2	*	6554.8	5268.0	6.0	*
3.	Sud/Merr NE3	*	6616.2	5224.9	6.0	*
4.	Sud/Merr NE4	*	6684.7	5255.3	6.0	*
5.	Sud/Merr NE5	*	6753.3	5285.7	6.0	*
6.	Sud/Merr SE1	*	6792.9	5222.3	6.0	*
7.	Sud/Merr SE2	*	6724.3	5191.9	6.0	*
8.	Sud/Merr SE3	*	6655.7	5161.5	6.0	*
9.	Sud/Merr SE4	*	6695.5	5097.9	6.0	*
10.	Sud/Merr SE5	*	6735.2	5034.3	6.0	*
11.	Sud/Merr SW1	*	6638.6	4981.3	6.0	*
12.	Sud/Merr SW2	*	6598.9	5045.0	6.0	*
13.	Sud/Merr SW3	*	6559.1	5108.6	6.0	*
14.	Sud/Merr SW4	*	6493.4	5072.5	6.0	*
15.	Sud/Merr SW5	*	6427.6	5036.5	6.0	*
16.	Sud/Merr NW1	*	6347.8	5104.5	6.0	*
17.	Sud/Merr NW2	*	6413.5	5140.5	6.0	*
18.	Sud/Merr NW3	*	6479.3	5176.6	6.0	*
19.	Sud/Merr NW4	*	6417.1	5218.5	6.0	*
20.	Sud/Merr NW5	*	6354.9	5260.4	6.0	*
21.	Sud/Sur NE1	*	6755.9	5445.7	6.0	*
22.	Sud/Sur NE2	*	6801.0	5385.7	6.0	*
23.	Sud/Sur NE3	*	6846.0	5325.7	6.0	*
24.	Sud/Sur NE4	*	6908.8	5366.8	6.0	*
25.	Sud/Sur NE5	*	6971.5	5407.9	6.0	*
26.	Sud/Sur SE1	*	7002.4	5368.4	6.0	*
27.	Sud/Sur SE2	*	6939.7	5327.3	6.0	*

DATE : 8/ 7/13
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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
28.	Sud/Sur SE3	*	6876.9	5286.2	6.0	*
29.	Sud/Sur SE4	*	6931.7	5235.0	6.0	*
30.	Sud/Sur SE5	*	6986.5	5183.8	6.0	*
31.	Sud/Sur SW1	*	6932.3	5133.1	6.0	*
32.	Sud/Sur SE2	*	6877.5	5184.3	6.0	*
33.	Sud/Sur SE3	*	6822.7	5235.5	6.0	*
34.	Sud/Sur SE4	*	6754.2	5205.1	6.0	*
35.	Sud/Sur SE5	*	6685.6	5174.8	6.0	*
36.	Sud/Sur NW1	*	6645.5	5237.9	6.0	*
37.	Sud/Sur NW2	*	6714.1	5268.3	6.0	*
38.	Sud/Sur NW3	*	6782.7	5298.7	6.0	*
39.	Sud/Sur NW4	*	6709.5	5315.4	6.0	*
40.	Sud/Sur NW5	*	6636.4	5332.0	6.0	*
41.	Sud/Sur N1	*	6642.4	5493.7	6.0	*
42.	Sud/Sur N2	*	6687.4	5433.7	6.0	*
43.	Sud/Sur N3	*	6732.4	5373.8	6.0	*
44.	Sud/Sur N4	*	6659.3	5390.4	6.0	*
45.	Sud/Sur N5	*	6586.2	5407.1	6.0	*

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.1	0.0	0.0	0.0	0.2	0.7	0.1	0.1	0.0	0.1	0.7	0.6	0.5	1.1	0.4	0.4	0.4	0.7	0.5	1.0
10.	*	0.1	0.0	0.0	0.0	0.2	0.4	0.2	0.1	0.1	0.1	0.7	0.6	0.5	1.1	0.3	0.3	0.3	0.8	0.4	0.9
20.	*	0.0	0.0	0.0	0.1	0.2	0.3	0.3	0.1	0.1	0.1	0.6	0.7	0.5	1.1	0.5	0.3	0.2	0.9	0.3	0.9
30.	*	0.0	0.0	0.0	0.1	0.1	0.2	0.5	0.2	0.1	0.0	0.6	0.9	0.5	0.7	0.6	0.1	0.3	0.9	0.3	0.9
40.	*	0.0	0.0	0.0	0.1	0.1	0.1	0.5	0.2	0.1	0.0	0.3	0.8	0.5	0.6	0.6	0.1	0.3	0.9	0.3	0.8
50.	*	0.0	0.0	0.0	0.0	0.1	0.1	0.4	0.3	0.0	0.0	0.4	0.8	0.8	0.5	0.5	0.2	0.3	0.9	0.3	0.9
60.	*	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.0	0.0	0.4	0.7	0.9	0.4	0.4	0.4	0.4	0.8	0.3	0.8
70.	*	0.0	0.0	0.2	0.1	0.0	0.1	0.2	0.1	0.0	0.0	0.3	0.5	0.7	0.4	0.3	0.5	0.6	0.9	0.4	0.9
80.	*	0.0	0.1	0.2	0.4	0.0	0.1	0.1	0.0	0.0	0.0	0.3	0.4	0.7	0.4	0.3	0.5	0.7	0.9	0.6	0.8
90.	*	0.0	0.1	0.2	0.5	0.1	0.1	0.1	0.0	0.0	0.0	0.4	0.4	0.8	0.3	0.2	0.5	0.8	0.7	0.7	0.7
100.	*	0.1	0.1	0.2	0.5	0.3	0.1	0.1	0.0	0.0	0.0	0.4	0.4	0.7	0.3	0.2	0.4	0.8	1.0	0.8	0.8
110.	*	0.1	0.1	0.1	0.4	0.4	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.2	0.1	0.2	0.7	0.9	1.0	0.9
120.	*	0.2	0.0	0.1	0.2	0.6	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.2	0.1	0.2	0.5	1.1	0.9	0.9
130.	*	0.4	0.3	0.2	0.1	0.7	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.1	0.0	0.1	0.3	1.1	0.8	0.6
140.	*	0.5	0.6	0.3	0.1	0.7	0.0	0.0	0.1	0.1	0.1	0.3	0.4	0.4	0.1	0.0	0.1	0.1	1.0	0.5	0.4
150.	*	0.8	0.7	0.7	0.1	0.8	0.0	0.0	0.4	0.3	0.2	0.2	0.2	0.2	0.0	0.0	0.1	0.1	1.0	0.3	0.3
160.	*	0.9	0.8	1.0	0.2	0.8	0.0	0.1	0.7	0.4	0.3	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.9	0.2	0.2
170.	*	0.9	0.6	1.0	0.4	0.8	0.0	0.1	1.0	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.7	0.1	0.1
180.	*	0.8	0.7	0.9	0.5	0.6	0.1	0.2	1.2	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.5	0.1	0.0
190.	*	0.6	0.7	0.7	0.5	0.6	0.1	0.3	1.2	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.4	0.1	0.0
200.	*	0.5	0.8	0.6	0.5	0.6	0.1	0.3	1.2	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.1	0.0
210.	*	0.3	0.9	0.6	0.5	0.6	0.2	0.4	1.1	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.1	0.0
220.	*	0.3	0.8	0.8	0.5	0.3	0.3	0.5	1.0	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.0
230.	*	0.4	0.7	0.8	0.6	0.4	0.4	0.5	1.1	0.7	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0
240.	*	0.5	0.5	0.8	0.5	0.5	0.3	0.6	1.3	0.9	0.4	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.0	0.1
250.	*	0.5	0.4	0.7	0.6	0.3	0.5	0.7	1.3	0.9	0.3	0.0	0.0	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0
260.	*	0.6	0.5	0.6	0.3	0.1	0.5	0.7	1.2	1.2	0.3	0.0	0.0	0.4	0.1	0.1	0.0	0.0	0.0	0.0	0.1
270.	*	0.6	0.5	0.6	0.4	0.3	0.4	0.4	1.3	1.3	0.4	0.0	0.1	0.5	0.1	0.1	0.0	0.0	0.0	0.0	0.2
280.	*	0.7	0.7	0.6	0.3	0.1	0.6	0.6	1.1	1.3	0.6	0.0	0.1	0.6	0.1	0.1	0.0	0.0	0.0	0.2	0.2
290.	*	0.7	0.6	0.5	0.2	0.1	0.7	0.4	1.0	1.4	0.7	0.0	0.2	0.8	0.1	0.1	0.0	0.1	0.2	0.4	0.4
300.	*	0.3	0.4	0.6	0.2	0.1	0.8	0.3	0.8	1.6	1.0	0.1	0.3	1.1	0.1	0.1	0.1	0.1	0.4	0.7	0.7
310.	*	0.2	0.3	0.3	0.1	0.1	0.9	0.2	0.8	1.0	1.0	0.2	0.7	1.1	0.2	0.1	0.1	0.3	0.6	0.7	0.9
320.	*	0.2	0.2	0.1	0.1	0.1	0.9	0.2	0.4	0.7	0.7	0.5	0.8	1.2	0.3	0.1	0.2	0.2	0.8	1.0	1.1
330.	*	0.1	0.1	0.1	0.1	0.0	0.9	0.1	0.3	0.2	0.4	0.4	0.8	1.0	0.7	0.3	0.1	0.6	0.7	1.0	1.1
340.	*	0.1	0.1	0.1	0.0	0.1	1.0	0.1	0.1	0.1	0.2	0.6	0.6	0.9	0.8	0.5	0.4	0.6	0.6	0.8	1.2
350.	*	0.1	0.1	0.0	0.0	0.2	0.9	0.1	0.1	0.0	0.0	0.7	0.4	0.6	1.0	0.4	0.4	0.5	0.6	0.6	1.1
360.	*	0.1	0.0	0.0	0.0	0.2	0.7	0.1	0.1	0.0	0.1	0.7	0.6	0.5	1.1	0.4	0.4	0.4	0.7	0.5	1.0
MAX	*	0.9	0.9	1.0	0.6	0.8	1.0	0.7	1.3	1.6	1.0	0.7	0.9	1.2	1.1	0.6	0.5	0.8	1.1	1.0	1.2
DEGR.	*	170	210	160	230	170	340	250	240	300	300	0	30	320	0	30	70	90	120	110	340

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.8	0.1	0.0	0.1	0.2	0.1	0.0
10.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.7	0.1	0.0	0.2	0.2	0.2	0.0
20.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.2	0.7	0.1	0.0	0.2	0.1	0.2	0.0
30.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.2	0.7	0.2	0.0	0.2	0.1	0.2	0.0
40.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.2	0.5	0.3	0.1	0.0	0.1	0.2	0.0
50.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.4	0.3	0.0	0.0	0.1	0.2	0.1
60.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.1	0.0	0.1	0.2	0.1
70.	*	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.2	0.1	0.1	0.1	0.1
80.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.3	0.3	0.1	0.0	0.0
90.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.1	0.0	0.3	0.6	0.1	0.0	0.0
100.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.1	0.0	0.2	0.7	0.1	0.0	0.1
110.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.1	0.0	0.1	0.7	0.1	0.2	0.1
120.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.0	0.1	0.6	0.2	0.3	0.1
130.	*	0.0	0.0	0.2	0.1	0.0	0.0	0.0	0.1	0.1	0.0	0.1	0.1	0.1	0.0	0.0	0.1	0.4	0.2	0.4	0.1
140.	*	0.0	0.1	0.2	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.2	0.4	0.1
150.	*	0.3	0.1	0.2	0.1	0.0	0.0	0.0	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.4	0.3	0.1
160.	*	0.4	0.2	0.2	0.1	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.2	0.4	0.2	0.4	0.2	0.2
170.	*	0.5	0.2	0.2	0.2	0.0	0.0	0.1	0.2	0.2	0.1	0.0	0.0	0.0	0.1	0.4	0.7	0.2	0.6	0.2	0.3
180.	*	0.6	0.3	0.2	0.2	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.5	0.7	0.4	0.8	0.4	0.4
190.	*	0.7	0.4	0.3	0.2	0.0	0.0	0.1	0.2	0.1	0.1	0.0	0.1	0.1	0.2	0.6	0.7	0.4	0.8	0.4	0.3
200.	*	0.5	0.4	0.4	0.3	0.2	0.0	0.2	0.2	0.2	0.1	0.0	0.1	0.1	0.3	0.7	0.6	0.5	0.9	0.5	0.3
210.	*	0.4	0.4	0.5	0.3	0.2	0.1	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.3	0.7	0.5	0.5	0.7	0.3	0.4
220.	*	0.4	0.4	0.6	0.4	0.3	0.1	0.2	0.3	0.2	0.2	0.1	0.1	0.2	0.4	0.8	0.6	0.4	0.6	0.3	0.4
230.	*	0.2	0.5	0.5	0.4	0.4	0.1	0.4	0.4	0.2	0.2	0.1	0.1	0.2	0.4	0.7	0.7	0.6	0.5	0.4	0.4
240.	*	0.2	0.4	0.6	0.2	0.2	0.3	0.4	0.6	0.3	0.2	0.1	0.2	0.2	0.5	0.9	0.8	0.5	0.4	0.2	0.2
250.	*	0.2	0.5	0.3	0.1	0.0	0.2	0.3	0.7	0.3	0.3	0.1	0.2	0.5	0.7	0.8	0.6	0.3	0.2	0.1	0.2
260.	*	0.2	0.5	0.2	0.0	0.0	0.1	0.3	0.5	0.4	0.3	0.2	0.3	0.7	0.6	1.0	0.3	0.1	0.1	0.3	0.3
270.	*	0.3	0.5	0.2	0.2	0.0	0.1	0.1	0.4	0.3	0.4	0.2	0.3	0.6	0.3	0.8	0.5	0.3	0.2	0.3	0.3
280.	*	0.2	0.6	0.1	0.3	0.1	0.0	0.1	0.2	0.2	0.3	0.3	0.2	0.9	0.4	0.7	0.4	0.3	0.1	0.1	0.3
290.	*	0.2	0.5	0.3	0.3	0.0	0.0	0.3	0.3	0.2	0.3	0.2	0.1	0.7	0.3	0.6	0.3	0.3	0.1	0.2	0.2
300.	*	0.2	0.4	0.3	0.0	0.0	0.0	0.1	0.4	0.1	0.2	0.1	0.2	0.8	0.1	0.6	0.4	0.1	0.1	0.1	0.2
310.	*	0.1	0.2	0.2	0.0	0.0	0.0	0.1	0.3	0.2	0.1	0.2	0.2	0.5	0.2	0.3	0.2	0.1	0.1	0.1	0.1
320.	*	0.1	0.1	0.2	0.0	0.0	0.0	0.1	0.3	0.0	0.0	0.2	0.2	0.4	0.2	0.2	0.1	0.1	0.1	0.1	0.1
330.	*	0.0	0.0	0.1	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.2	0.4	0.2	0.2	0.1	0.0	0.2	0.0	0.1
340.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.1	0.2	0.3	0.1	0.0	0.0	0.2	0.0	0.1
350.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.1	0.2	0.4	0.1	0.0	0.0	0.2	0.1	0.0
360.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.8	0.1	0.0	0.1	0.2	0.1	0.0

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------*-------------------------------------------------------------------------------------------------------------
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 MAX   *   0.7   0.6   0.6   0.4   0.4   0.3   0.4   0.7   0.4   0.4   0.3   0.3   0.9   0.8   1.0   0.8   0.7   0.9
0.5   0.4
 DEGR. *  190   280   220   220   230   240   230   250   260   270   280   260   280     0   260   240   100   200
200   180
```


JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45
0.	0.1	0.1	0.2	0.1	0.0
10.	0.1	0.1	0.3	0.1	0.0
20.	0.1	0.1	0.3	0.1	0.0
30.	0.1	0.1	0.4	0.1	0.0
40.	0.1	0.1	0.4	0.1	0.0
50.	0.1	0.1	0.4	0.1	0.0
60.	0.1	0.1	0.4	0.1	0.0
70.	0.1	0.1	0.4	0.2	0.0
80.	0.1	0.1	0.4	0.2	0.0
90.	0.1	0.2	0.3	0.2	0.1
100.	0.1	0.2	0.3	0.2	0.1
110.	0.1	0.3	0.2	0.2	0.0
120.	0.3	0.3	0.1	0.0	0.1
130.	0.2	0.3	0.2	0.1	0.1
140.	0.2	0.3	0.2	0.1	0.1
150.	0.1	0.1	0.1	0.1	0.1
160.	0.2	0.1	0.2	0.2	0.2
170.	0.2	0.2	0.3	0.2	0.3
180.	0.2	0.2	0.2	0.3	0.3
190.	0.1	0.2	0.2	0.3	0.3
200.	0.2	0.2	0.2	0.4	0.2
210.	0.1	0.3	0.2	0.3	0.2
220.	0.1	0.1	0.3	0.2	0.1
230.	0.2	0.1	0.2	0.1	0.3
240.	0.2	0.1	0.1	0.1	0.3
250.	0.1	0.2	0.1	0.3	0.2
260.	0.2	0.1	0.2	0.2	0.3
270.	0.2	0.2	0.1	0.3	0.4
280.	0.1	0.2	0.2	0.2	0.2
290.	0.1	0.1	0.1	0.2	0.2
300.	0.1	0.1	0.1	0.1	0.1
310.	0.1	0.1	0.1	0.1	0.1
320.	0.1	0.1	0.2	0.1	0.1
330.	0.1	0.1	0.1	0.1	0.1
340.	0.0	0.1	0.1	0.0	0.1
350.	0.1	0.1	0.1	0.0	0.1
360.	0.1	0.1	0.2	0.1	0.0
MAX	0.3	0.3	0.4	0.4	0.4
DEGR.	120	110	30	200	270

THE HIGHEST CONCENTRATION OF 1.60 PPM OCCURRED AT RECEPTOR REC9 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17:10:38

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6042.2	5450.2	*	74.	290.	AG	328.	100.0	1.0	30.0	0.56
2.	Char/Merr WB	*	6250.4	5435.2	6300.3	5474.7	*	64.	52.	AG	341.	100.0	1.0	30.0	0.55
3.	Char/Merr NB R	*	6291.7	5369.7	6341.8	5335.7	*	61.	124.	AG	67.	100.0	1.0	10.0	0.31
4.	Char/Merr NB LTT	*	6280.4	5347.2	6349.1	5298.8	*	84.	125.	AG	198.	100.0	1.0	20.0	0.52
5.	Char/Merr EB	*	6104.2	5362.2	6005.8	5325.6	*	105.	250.	AG	230.	100.0	1.0	20.0	0.81
6.	Char/Cam SB L	*	5384.1	4834.2	5401.1	4902.3	*	70.	14.	AG	88.	100.0	1.0	10.0	0.38
7.	Char/Cam SB TR	*	5360.8	4833.5	5374.3	4877.1	*	46.	17.	AG	210.	100.0	1.0	20.0	0.32
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5475.3	4778.6	*	66.	103.	AG	181.	100.0	1.0	20.0	0.37
9.	Char/Cam NB L	*	5363.0	4722.4	5361.0	4631.8	*	91.	181.	AG	88.	100.0	1.0	10.0	0.49
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.8	4624.7	*	99.	179.	AG	210.	100.0	1.0	20.0	0.68
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5220.6	4740.7	*	82.	271.	AG	271.	100.0	1.0	30.0	0.46
12.	Sud/Merr SB L	*	6532.7	5210.3	6496.1	5236.4	*	45.	305.	AG	123.	100.0	1.0	10.0	0.56
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6487.3	5208.8	*	36.	300.	AG	219.	100.0	1.0	30.0	0.18
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6672.2	5071.1	*	104.	150.	AG	289.	100.0	1.0	30.0	0.62
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6458.9	5107.1	*	75.	239.	AG	420.	100.0	1.0	40.0	0.52
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6739.2	5418.0	*	62.	322.	AG	204.	100.0	1.0	20.0	0.40
17.	Sud/Sur SEB	*	6757.2	5330.0	6742.4	5333.7	*	15.	284.	AG	117.	100.0	1.0	10.0	0.15
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6722.2	5231.2	*	78.	249.	AG	219.	100.0	1.0	30.0	0.39
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	818.	9.8	1.0	84.0	
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1226.	9.8	1.0	90.0	
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1219.	9.8	1.0	98.0	
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	859.	9.8	1.0	98.0	
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	796.	9.8	1.0	78.0	
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1264.	9.8	1.0	****	
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	954.	9.8	1.0	78.0	
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1198.	9.8	1.0	90.0	
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	805.	9.8	1.0	30.0	
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	405.	9.8	1.0	54.0	
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	322.	9.8	1.0	42.0	
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	853.	9.8	1.0	54.0	
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	35.	9.8	1.0	42.0	
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1185.	9.8	1.0	98.0	
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1465.	9.8	1.0	90.0	
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	766.	9.8	1.0	78.0	

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17:10:38

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Char/Merr SB	*	100	75	3.0	541	1600	54.39	1	3
2.	Char/Merr WB	*	100	78	3.0	449	1600	54.39	1	3
3.	Char/Merr NB R	*	100	46	3.0	241	1600	54.39	1	3
4.	Char/Merr NB LTT	*	100	68	3.0	452	1600	54.39	1	3

5.	Char/Merr EB	*	100	79	3.0	417	1600	54.39	1	3
6.	Char/Cam SB L	*	100	60	3.0	214	1600	54.39	1	3
7.	Char/Cam SB TR	*	100	72	3.0	233	1600	54.39	1	3
8.	Char/Cam WB LTTR	*	100	62	3.0	391	1600	54.39	1	3
9.	Char/Cam NB L	*	100	60	3.0	276	1600	54.39	1	3
10.	Char/Cam NB TR	*	100	72	3.0	503	1600	54.39	1	3
11.	Char/Cam EB TTTR	*	100	62	3.0	726	1600	54.39	1	3
12.	Sud/Merr SB L	*	100	84	3.0	98	1600	54.39	1	3
13.	Sud/Merr SB TTT	*	100	50	3.0	394	1600	54.39	1	3
14.	Sud/Merr NB TTTR	*	100	66	3.0	863	1600	54.39	1	3
15.	Sud/Merr EB LTTR	*	100	72	3.0	766	1600	54.39	1	3
16.	Sud/Sur SB LTT	*	100	70	3.0	322	1600	54.39	1	3
17.	Sud/Sur SEB	*	100	80	3.0	35	1600	54.39	1	3
18.	Sud/Sur EB TTR	*	100	50	3.0	853	1600	54.39	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Sud/Merr NE1	*	6492.5	5309.9	6.0
2.	Sud/Merr NE2	*	6554.8	5268.0	6.0
3.	Sud/Merr NE3	*	6616.2	5224.9	6.0
4.	Sud/Merr NE4	*	6684.7	5255.3	6.0
5.	Sud/Merr NE5	*	6753.3	5285.7	6.0
6.	Sud/Merr SE1	*	6792.9	5222.3	6.0
7.	Sud/Merr SE2	*	6724.3	5191.9	6.0
8.	Sud/Merr SE3	*	6655.7	5161.5	6.0
9.	Sud/Merr SE4	*	6695.5	5097.9	6.0
10.	Sud/Merr SE5	*	6735.2	5034.3	6.0
11.	Sud/Merr SW1	*	6638.6	4981.3	6.0
12.	Sud/Merr SW2	*	6598.9	5045.0	6.0
13.	Sud/Merr SW3	*	6559.1	5108.6	6.0
14.	Sud/Merr SW4	*	6493.4	5072.5	6.0
15.	Sud/Merr SW5	*	6427.6	5036.5	6.0
16.	Sud/Merr NW1	*	6347.8	5104.5	6.0
17.	Sud/Merr NW2	*	6413.5	5140.5	6.0
18.	Sud/Merr NW3	*	6479.3	5176.6	6.0
19.	Sud/Merr NW4	*	6417.1	5218.5	6.0
20.	Sud/Merr NW5	*	6354.9	5260.4	6.0
21.	Sud/Sur NE1	*	6755.9	5445.7	6.0
22.	Sud/Sur NE2	*	6801.0	5385.7	6.0
23.	Sud/Sur NE3	*	6846.0	5325.7	6.0
24.	Sud/Sur NE4	*	6908.8	5366.8	6.0
25.	Sud/Sur NE5	*	6971.5	5407.9	6.0
26.	Sud/Sur SE1	*	7002.4	5368.4	6.0
27.	Sud/Sur SE2	*	6939.7	5327.3	6.0

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
28.	Sud/Sur SE3	*	6876.9	5286.2	6.0
29.	Sud/Sur SE4	*	6931.7	5235.0	6.0
30.	Sud/Sur SE5	*	6986.5	5183.8	6.0
31.	Sud/Sur SW1	*	6932.3	5133.1	6.0
32.	Sud/Sur SE2	*	6877.5	5184.3	6.0
33.	Sud/Sur SE3	*	6822.7	5235.5	6.0
34.	Sud/Sur SE4	*	6754.2	5205.1	6.0
35.	Sud/Sur SE5	*	6685.6	5174.8	6.0
36.	Sud/Sur NW1	*	6645.5	5237.9	6.0
37.	Sud/Sur NW2	*	6714.1	5268.3	6.0
38.	Sud/Sur NW3	*	6782.7	5298.7	6.0
39.	Sud/Sur NW4	*	6709.5	5315.4	6.0
40.	Sud/Sur NW5	*	6636.4	5332.0	6.0
41.	Sud/Sur N1	*	6642.4	5493.7	6.0
42.	Sud/Sur N2	*	6687.4	5433.7	6.0
43.	Sud/Sur N3	*	6732.4	5373.8	6.0
44.	Sud/Sur N4	*	6659.3	5390.4	6.0
45.	Sud/Sur N5	*	6586.2	5407.1	6.0

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
	(PPM)																			
0.	0.1	0.0	0.0	0.0	0.4	0.6	0.6	0.2	0.2	0.2	0.8	0.6	0.6	1.5	0.6	0.3	0.3	0.5	0.4	0.6
10.	0.1	0.0	0.0	0.0	0.3	0.4	0.7	0.2	0.2	0.2	0.8	0.7	0.6	1.3	0.5	0.2	0.3	0.6	0.4	0.5
20.	0.0	0.0	0.0	0.1	0.2	0.3	0.8	0.3	0.2	0.1	0.8	0.8	0.6	1.2	0.8	0.3	0.2	0.8	0.3	0.4
30.	0.0	0.0	0.0	0.1	0.2	0.3	0.8	0.4	0.2	0.0	0.5	0.9	0.5	0.8	0.9	0.1	0.2	0.8	0.3	0.4
40.	0.0	0.0	0.1	0.1	0.1	0.3	0.7	0.5	0.1	0.0	0.3	0.9	0.7	0.8	0.9	0.1	0.3	0.9	0.3	0.3
50.	0.0	0.0	0.0	0.0	0.0	0.2	0.6	0.5	0.0	0.0	0.3	0.8	0.9	0.6	0.8	0.1	0.3	0.9	0.3	0.3
60.	0.0	0.1	0.2	0.1	0.1	0.2	0.4	0.4	0.0	0.0	0.4	0.7	0.9	0.7	0.6	0.4	0.5	0.9	0.3	0.4
70.	0.0	0.0	0.3	0.3	0.1	0.1	0.2	0.2	0.0	0.0	0.3	0.5	0.8	0.5	0.2	0.8	0.7	0.9	0.3	0.5
80.	0.0	0.1	0.5	0.5	0.2	0.1	0.0	0.0	0.0	0.0	0.3	0.4	0.7	0.4	0.2	0.8	1.0	0.9	0.6	0.5
90.	0.0	0.2	0.5	0.6	0.2	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.8	0.3	0.2	0.7	1.2	0.8	0.7	0.5
100.	0.2	0.2	0.4	0.8	0.3	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.7	0.3	0.1	0.6	1.2	1.1	0.9	0.7
110.	0.2	0.2	0.3	0.7	0.5	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.2	0.1	0.4	1.2	1.0	0.9	0.8
120.	0.3	0.1	0.2	0.5	0.6	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.2	0.1	0.3	1.0	1.2	0.8	0.9
130.	0.4	0.4	0.2	0.4	0.6	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.1	0.0	0.2	0.7	1.2	0.8	0.8
140.	0.6	0.7	0.4	0.3	0.6	0.0	0.0	0.1	0.1	0.1	0.3	0.3	0.4	0.1	0.0	0.2	0.4	1.1	0.6	0.6
150.	0.7	0.8	0.8	0.2	0.7	0.0	0.0	0.5	0.2	0.2	0.1	0.2	0.2	0.0	0.0	0.2	0.3	1.1	0.5	0.3
160.	1.0	0.8	1.1	0.3	0.7	0.0	0.1	0.7	0.4	0.3	0.1	0.1	0.1	0.0	0.0	0.2	0.2	1.1	0.3	0.3
170.	0.9	0.7	1.2	0.5	0.8	0.0	0.1	1.1	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	1.1	0.2	0.1
180.	0.8	0.6	0.9	0.6	0.8	0.1	0.2	1.1	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	1.0	0.1	0.1
190.	0.7	0.6	0.8	0.7	0.9	0.1	0.3	1.2	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.9	0.1	0.1
200.	0.5	0.9	0.8	0.8	1.0	0.1	0.4	1.2	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.7	0.1	0.0
210.	0.4	1.0	0.7	0.7	0.9	0.2	0.4	1.1	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.0
220.	0.3	0.9	0.9	0.8	0.8	0.2	0.5	1.1	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.0	0.0
230.	0.4	0.7	1.0	0.7	0.8	0.3	0.5	1.0	0.8	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.0	0.0
240.	0.3	0.5	1.1	0.6	0.6	0.6	0.8	1.3	1.0	0.4	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.1
250.	0.4	0.3	0.7	0.6	0.5	0.6	0.8	1.4	1.0	0.3	0.0	0.0	0.4	0.2	0.1	0.0	0.0	0.1	0.0	0.0
260.	0.4	0.4	0.7	0.1	0.1	0.9	0.9	1.4	1.2	0.3	0.0	0.1	0.6	0.2	0.2	0.0	0.0	0.0	0.0	0.1
270.	0.5	0.4	0.6	0.2	0.2	0.8	0.7	1.3	1.4	0.5	0.0	0.1	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.2
280.	0.6	0.6	0.5	0.2	0.1	0.9	0.6	1.2	1.4	0.7	0.1	0.2	0.9	0.2	0.2	0.0	0.0	0.0	0.2	0.3
290.	0.7	0.7	0.3	0.2	0.1	0.9	0.5	1.2	1.5	0.8	0.1	0.3	1.0	0.3	0.2	0.0	0.1	0.2	0.4	0.5
300.	0.3	0.4	0.4	0.1	0.1	0.8	0.5	0.8	1.6	1.1	0.2	0.4	1.0	0.4	0.2	0.1	0.1	0.4	0.7	0.7
310.	0.2	0.3	0.2	0.1	0.1	0.8	0.3	0.7	1.1	1.1	0.4	0.6	1.1	0.7	0.2	0.2	0.3	0.6	0.6	0.9
320.	0.1	0.1	0.1	0.1	0.1	0.8	0.3	0.5	0.8	1.0	0.6	0.7	1.1	0.9	0.2	0.2	0.2	0.7	0.8	1.0
330.	0.1	0.1	0.1	0.1	0.0	0.7	0.3	0.4	0.4	0.5	0.6	0.8	1.0	1.1	0.3	0.1	0.5	0.5	0.7	1.0
340.	0.1	0.1	0.1	0.0	0.1	0.8	0.3	0.3	0.1	0.3	0.5	0.7	0.9	1.3	0.4	0.3	0.5	0.5	0.6	1.0
350.	0.1	0.1	0.0	0.0	0.3	0.8	0.4	0.2	0.1	0.2	0.7	0.5	0.8	1.4	0.4	0.4	0.2	0.5	0.4	0.9
360.	0.1	0.0	0.0	0.0	0.4	0.6	0.6	0.2	0.2	0.2	0.8	0.6	0.6	1.5	0.6	0.3	0.3	0.5	0.4	0.6
MAX	1.0	1.0	1.2	0.8	1.0	0.9	0.9	1.4	1.6	1.1	0.8	0.9	1.1	1.5	0.9	0.8	1.2	1.2	0.9	1.0
DEGR.	160	210	170	100	200	260	260	250	300	300	0	30	310	0	30	70	90	120	100	320

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
	CONCENTRATION (PPM)																			
0.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.2	0.2	0.2	0.8	0.2	0.0	0.1	0.2	0.1	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.1	0.0	0.1	0.2	0.2	0.8	0.2	0.0	0.1	0.2	0.2	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.0	0.0	0.1	0.2	0.2	0.7	0.5	0.0	0.1	0.1	0.2	0.0
30.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.0	0.0	0.1	0.1	0.3	0.6	0.5	0.1	0.1	0.1	0.2	0.0
40.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.0	0.0	0.1	0.1	0.3	0.6	0.6	0.1	0.1	0.1	0.2	0.0
50.	0.0	0.0	0.1	0.0	0.0	0.0	0.1	0.2	0.0	0.0	0.1	0.1	0.2	0.4	0.6	0.0	0.0	0.1	0.1	0.1
60.	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.2	0.4	0.5	0.2	0.1	0.2	0.2	0.1
70.	0.0	0.0	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.4	0.2	0.2	0.1	0.1
80.	0.0	0.0	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.4	0.3	0.2	0.2	0.1
90.	0.0	0.0	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.5	0.5	0.2	0.1	0.1
100.	0.0	0.1	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.5	0.7	0.2	0.1	0.0
110.	0.0	0.1	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.4	0.8	0.2	0.3	0.2
120.	0.1	0.1	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.2	0.7	0.1	0.3	0.2
130.	0.1	0.1	0.2	0.2	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.7	0.2	0.3	0.2
140.	0.1	0.2	0.3	0.2	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.2	0.7	0.2	0.4	0.2
150.	0.2	0.2	0.3	0.2	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.4	0.6	0.3	0.4	0.2
160.	0.4	0.3	0.3	0.2	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.2	0.6	0.6	0.4	0.3	0.3
170.	0.7	0.1	0.3	0.3	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.4	0.8	0.5	0.5	0.4	0.4
180.	0.8	0.4	0.3	0.3	0.1	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.5	0.9	0.6	0.7	0.4	0.5
190.	0.9	0.4	0.4	0.4	0.1	0.0	0.1	0.2	0.1	0.1	0.0	0.1	0.1	0.2	0.6	0.8	0.6	0.8	0.4	0.4
200.	0.7	0.6	0.6	0.5	0.2	0.0	0.2	0.2	0.2	0.1	0.0	0.1	0.1	0.3	0.7	0.7	0.7	1.0	0.5	0.6
210.	0.7	0.5	0.5	0.4	0.3	0.1	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.3	0.8	0.8	0.7	0.9	0.3	0.4
220.	0.5	0.7	0.7	0.6	0.3	0.1	0.2	0.3	0.2	0.2	0.1	0.1	0.2	0.4	0.8	0.7	0.8	0.8	0.5	0.4
230.	0.4	0.7	0.7	0.6	0.6	0.3	0.6	0.5	0.2	0.2	0.1	0.1	0.2	0.4	0.8	0.9	0.6	0.9	0.5	0.4
240.	0.2	0.6	0.8	0.5	0.3	0.6	0.6	0.8	0.3	0.2	0.1	0.2	0.4	0.7	0.9	0.8	0.6	0.6	0.3	0.1
250.	0.2	0.6	0.4	0.1	0.0	0.4	0.5	1.0	0.5	0.3	0.2	0.3	0.7	0.8	1.0	0.6	0.5	0.4	0.1	0.2
260.	0.2	0.6	0.2	0.0	0.1	0.2	0.5	0.7	0.6	0.4	0.3	0.4	1.0	0.7	1.0	0.3	0.1	0.1	0.2	0.2
270.	0.2	0.7	0.2	0.1	0.1	0.2	0.3	0.6	0.3	0.4	0.3	0.5	0.8	0.6	0.8	0.3	0.2	0.2	0.2	0.1
280.	0.2	0.7	0.2	0.2	0.1	0.3	0.5	0.3	0.3	0.3	0.3	0.3	1.0	0.5	0.9	0.3	0.2	0.1	0.2	0.2
290.	0.2	0.6	0.3	0.2	0.1	0.2	0.4	0.3	0.3	0.3	0.2	0.3	0.8	0.6	0.7	0.2	0.2	0.1	0.1	0.2
300.	0.2	0.5	0.4	0.1	0.0	0.0	0.4	0.5	0.3	0.1	0.2	0.4	0.7	0.5	0.5	0.3	0.1	0.1	0.1	0.1
310.	0.2	0.4	0.3	0.0	0.0	0.0	0.2	0.4	0.3	0.1	0.2	0.3	0.6	0.6	0.4	0.1	0.1	0.2	0.1	0.1
320.	0.1	0.2	0.2	0.0	0.0	0.0	0.2	0.4	0.1	0.1	0.2	0.3	0.4	0.7	0.3	0.1	0.1	0.2	0.1	0.1
330.	0.0	0.0	0.1	0.0	0.0	0.0	0.2	0.2	0.1	0.1	0.1	0.2	0.4	0.7	0.3	0.1	0.1	0.2	0.1	0.1
340.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.1	0.2	0.2	0.3	0.7	0.2	0.1	0.0	0.3	0.0	0.1
350.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.2	0.2	0.3	0.8	0.2	0.0	0.0	0.3	0.0	0.0
360.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.2	0.2	0.2	0.8	0.2	0.0	0.1	0.2	0.1	0.0

```
------*-------------------------------------------------------------------------------------------------------------
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 MAX   *   0.9   0.7   0.8   0.6   0.6   0.6   0.6   1.0   0.6   0.4   0.3   0.5   1.0   0.8   1.0   0.9   0.8   1.0
0.5   0.6
 DEGR. *  190   220   240   220   230   240   230   250   260   260   260   270   260     0   250   180   110   200
200   200
```


JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45
0.	0.1	0.1	0.3	0.0	0.0
10.	0.1	0.1	0.4	0.0	0.0
20.	0.1	0.1	0.4	0.0	0.0
30.	0.1	0.1	0.5	0.1	0.0
40.	0.1	0.1	0.5	0.1	0.0
50.	0.1	0.1	0.5	0.1	0.0
60.	0.1	0.1	0.5	0.2	0.0
70.	0.1	0.1	0.5	0.2	0.0
80.	0.1	0.1	0.5	0.3	0.1
90.	0.1	0.2	0.5	0.3	0.1
100.	0.1	0.3	0.4	0.2	0.1
110.	0.1	0.3	0.3	0.1	0.0
120.	0.2	0.4	0.2	0.0	0.1
130.	0.2	0.3	0.2	0.1	0.2
140.	0.2	0.2	0.1	0.2	0.2
150.	0.1	0.2	0.3	0.2	0.2
160.	0.3	0.2	0.4	0.3	0.3
170.	0.3	0.3	0.5	0.3	0.4
180.	0.3	0.3	0.3	0.4	0.3
190.	0.2	0.3	0.4	0.3	0.4
200.	0.2	0.3	0.3	0.3	0.3
210.	0.3	0.4	0.4	0.4	0.3
220.	0.1	0.3	0.4	0.3	0.1
230.	0.1	0.1	0.3	0.1	0.2
240.	0.1	0.2	0.1	0.1	0.1
250.	0.2	0.1	0.1	0.2	0.2
260.	0.2	0.1	0.1	0.1	0.2
270.	0.1	0.1	0.1	0.2	0.4
280.	0.2	0.1	0.1	0.2	0.2
290.	0.1	0.1	0.1	0.1	0.1
300.	0.1	0.1	0.1	0.1	0.1
310.	0.1	0.1	0.1	0.1	0.1
320.	0.1	0.1	0.1	0.1	0.1
330.	0.1	0.1	0.1	0.1	0.1
340.	0.0	0.1	0.1	0.0	0.1
350.	0.1	0.1	0.2	0.0	0.1
360.	0.1	0.1	0.3	0.0	0.0
MAX	0.3	0.4	0.5	0.4	0.4
DEGR.	160	120	30	180	170

THE HIGHEST CONCENTRATION OF 1.60 PPM OCCURRED AT RECEPTOR REC9 .

2028 No-Build Microscale Output Files (Carbon Monoxide (CO))

JOB: Government Center Garage RUN: No Build

DATE : 7/10/13
TIME : 15:35:33

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	75.	100.0	1.0	10.0	0.71	7.8
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5111.3	6026.2	*	109.	325.	AG	151.	100.0	1.0	20.0	0.50	5.5
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	183.	100.0	1.0	20.0	0.92	9.6
4.	Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	75.	100.0	1.0	10.0	0.58	6.4
5.	Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	98.	100.0	1.0	10.0	0.64	4.1
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5363.1	5748.8	*	51.	109.	AG	195.	100.0	1.0	20.0	0.41	2.6
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	195.	100.0	1.0	20.0	0.68	4.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	98.	100.0	1.0	10.0	0.93	8.1
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6176.7	7641.4	*	857.	334.	AG	302.	100.0	1.0	40.0	1.08	43.6
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	191.	100.0	1.0	20.0	0.58	5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	84.	100.0	1.0	10.0	0.53	6.6
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6665.3	5376.7	*	1377.	177.	AG	193.	100.0	1.0	20.0	1.39	69.9
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	282.	100.0	1.0	30.0	0.47	4.6
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.7	6361.5	*	138.	358.	AG	70.	100.0	1.0	20.0	0.79	7.0
15.	Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	86.	100.0	1.0	10.0	1.23	59.7
16.	Tha/Val NB TR	*	6645.6	6138.6	6647.7	6017.7	*	121.	179.	AG	35.	100.0	1.0	10.0	0.69	6.1
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6097.3	*	133.	0.	AG	163.	100.0	1.0	30.0	0.68	6.8
18.	Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	199.	100.0	1.0	30.0	0.18	1.8
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.3	5883.7	*	144.	358.	AG	256.	100.0	1.0	40.0	0.74	7.3
20.	Char/93 WB LTT	*	6702.8	5647.8	6763.4	5572.1	*	97.	141.	AG	167.	100.0	1.0	20.0	0.62	4.9
21.	Char/93 EB TTR	*	6560.8	5622.5	6520.0	5592.6	*	51.	234.	AG	250.	100.0	1.0	30.0	0.32	2.6
22.	North/Congress SB LT	*	6876.6	4408.9	6569.4	5930.4	*	1552.	349.	AG	326.	100.0	1.0	30.0	2.69	78.8
23.	North/Con WB LLTR	*	6920.6	4378.3	7106.5	4444.1	*	197.	71.	AG	145.	100.0	1.0	20.0	0.89	10.0
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6920.9	4289.3	*	45.	172.	AG	268.	100.0	1.0	30.0	0.33	2.3
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	72.	100.0	1.0	10.0	0.03	0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1396.	8.3	1.0	90.0		
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1568.	8.3	1.0	78.0		
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	899.	8.3	1.0	78.0		
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	8.3	1.0	78.0		
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3419.	8.3	1.0	90.0		
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	8.3	1.0	66.0		
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2371.	8.3	1.0	90.0		
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	8.3	1.0	78.0		
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2397.	8.3	1.0	90.0		
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	8.3	1.0	38.0		
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2837.	8.3	1.0	90.0		
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	8.3	1.0	54.0		
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2324.	8.3	1.0	66.0		
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	8.3	1.0	48.0		
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	515.	8.3	1.0	42.0		
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	8.3	1.0	48.0		
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	403.	8.3	1.0	54.0		
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	702.	8.3	1.0	54.0		

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	8.3	1.0	42.0		
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1343.	8.3	1.0	98.0		
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1063.	8.3	1.0	66.0		
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1529.	8.3	1.0	98.0		
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	8.3	1.0	54.0		

JOB: Government Center Garage RUN: No Build

DATE : 7/10/13
TIME : 15:35:33

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Stan/Lom SB L	*	120	75	3.0	376	1600	44.99	1	3
2.	Stan/Lom SB TRR	*	120	75	3.0	531	1600	44.99	1	3
3.	Stan/Lom WB LTT	*	120	91	3.0	588	1600	44.99	1	3
4.	Stan/Lom WB R	*	120	75	3.0	308	1600	44.99	1	3
5.	Stan/Lom NB L	*	120	97	3.0	152	1600	44.99	1	3
6.	Stan/Lom NB TRR	*	120	97	3.0	194	1600	44.99	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	324	1600	44.99	1	3
8.	Stan/Lom EB R	*	120	97	3.0	222	1600	44.99	1	3
9.	Caus/Wash SB LTTRR	*	150	94	3.0	2353	1600	44.99	1	3
10.	Caus/Wash WB LLTT	*	150	119	3.0	321	1600	44.99	1	3
11.	Caus/Wash WB R	*	150	104	3.0	230	1600	44.99	1	3
12.	Caus/Wash NB TTR	*	150	120	3.0	741	1600	44.99	1	3
13.	Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	44.99	1	3
14.	Tha/Val SB LTTR	*	104	30	3.0	1678	1600	44.99	1	3
15.	Tha/Val NB L	*	104	74	3.0	472	1600	44.99	1	3
16.	Tha/Val NB TR	*	104	30	3.0	737	1600	44.99	1	3
17.	Bev/Was SB TTT	*	100	45	3.0	1628	1600	44.99	1	3
18.	Bev/Was EB RRR	*	100	55	3.0	356	1600	44.99	1	3
19.	Char/93 SB LLTTRR	*	100	53	3.0	1986	1600	44.99	1	3
20.	Char/93 WB LTT	*	100	69	3.0	515	1600	44.99	1	3
21.	Char/93 EB TTR	*	100	69	3.0	403	1600	44.99	1	3
22.	North/Congress SB LT	*	100	90	3.0	647	1600	44.99	1	3
23.	North/Con WB LLTR	*	100	60	3.0	997	1600	44.99	1	3
24.	Nor/Con NB LTTTR	*	100	74	3.0	332	1600	44.99	1	3
25.	Nor/Con EB LTR	*	100	60	3.0	17	1600	44.99	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.0	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8.	Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0	*

JOB: Government Center Garage RUN: No Build

DATE : 7/10/13
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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
21. Caus/Wash NE1	6548.3	7035.9	6.0
22. Caus/Wash NE2	6581.4	6968.6	6.0
23. Caus/Wash NE3	6614.5	6901.3	6.0
24. Caus/Wash NE4	6669.8	6952.0	6.0
25. Caus/Wash NE5	6725.0	7002.7	6.0
26. Caus/Wash SE1	6753.6	6912.2	6.0
27. Caus/Wash SE2	6698.9	6862.0	6.0
28. Caus/Wash SE3	6643.1	6810.8	6.0
29. Caus/Wash SE4	6646.8	6736.4	6.0
30. Caus/Wash SE5	6650.0	6661.0	6.0
31. Caus/Wash SW1	6544.0	6561.0	6.0
32. Caus/Wash SW2	6540.9	6636.0	6.0
33. Caus/Wash SW3	6537.8	6710.9	6.0
34. Caus/Wash SW4	6476.8	6667.2	6.0
35. Caus/Wash SW5	6415.9	6623.4	6.0
36. Caus/Wash NW1	6407.4	6738.0	6.0
37. Caus/Wash NW2	6468.3	6781.7	6.0
38. Caus/Wash NW3	6529.3	6825.4	6.0
39. Caus/Wash NW4	6496.2	6892.7	6.0
40. Caus/Wash NW5	6463.1	6960.0	6.0
41. Tha/Val NE1	6667.3	6395.5	6.0
42. Tha/Val NE2	6668.3	6320.5	6.0
43. Tha/Val NE3	6669.3	6245.5	6.0
44. Tha/Val NE4	6744.3	6245.5	6.0
45. Tha/Val NE5	6819.2	6249.6	6.0
46. Tha/Val SE1	6822.3	6191.6	6.0
47. Tha/Val SE2	6747.3	6189.6	6.0
48. Tha/Val SE3	6672.3	6187.5	6.0
49. Tha/Val SE4	6671.6	6112.5	6.0
50. Tha/Val SE5	6670.9	6037.5	6.0
51. Tha/Val SW1	6560.2	5964.7	6.0
52. Tha/Val SW2	6560.9	6039.7	6.0
53. Tha/Val SW3	6561.6	6114.7	6.0
54. Tha/Val SW4	6502.2	6068.9	6.0
55. Tha/Val SW5	6442.7	6023.2	6.0
56. Tha/Val NW1	6441.0	6115.2	6.0
57. Tha/Val NW2	6500.4	6160.9	6.0
58. Tha/Val NW3	6559.8	6206.7	6.0
59. Tha/Val NW4	6558.8	6281.7	6.0
60. Tha/Val NW5	6557.8	6356.7	6.0

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.0	0.0	0.0	0.0	0.0	0.8	0.7	0.5	0.3	0.2	0.4	0.7	0.5	0.6	0.8	0.1	0.3	0.3	0.6	0.8
10.	0.0	0.0	0.0	0.0	0.0	0.7	0.8	0.5	0.4	0.2	0.3	0.7	0.6	0.5	0.7	0.2	0.1	0.2	0.5	0.8
20.	0.0	0.0	0.0	0.0	0.0	0.7	0.8	0.6	0.3	0.1	0.2	0.7	0.5	0.4	0.5	0.4	0.3	0.3	0.3	0.7
30.	0.0	0.0	0.0	0.0	0.0	0.6	0.7	0.6	0.3	0.1	0.3	0.5	0.5	0.4	0.3	0.5	0.5	0.5	0.3	0.7
40.	0.0	0.1	0.2	0.2	0.1	0.5	0.7	0.6	0.1	0.0	0.2	0.3	0.4	0.2	0.1	0.6	0.5	0.5	0.5	0.7
50.	0.0	0.0	0.4	0.3	0.1	0.2	0.4	0.4	0.0	0.0	0.2	0.3	0.4	0.3	0.1	0.8	0.4	0.5	0.7	0.7
60.	0.0	0.0	0.6	0.6	0.2	0.1	0.1	0.1	0.0	0.0	0.2	0.3	0.5	0.1	0.1	0.7	0.5	0.3	0.9	0.9
70.	0.0	0.2	1.0	0.9	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.8	0.5	0.1	0.8	0.9
80.	0.0	0.2	0.9	1.0	0.6	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.8	0.5	0.1	0.6	0.8
90.	0.2	0.5	0.8	1.0	0.7	0.0	0.0	0.0	0.1	0.1	0.4	0.4	0.5	0.2	0.1	0.9	0.7	0.2	0.4	0.8
100.	0.2	0.6	0.9	1.1	0.9	0.1	0.1	0.2	0.2	0.2	0.3	0.3	0.5	0.2	0.1	0.8	0.6	0.4	0.3	0.8
110.	0.3	0.6	0.6	1.0	0.8	0.1	0.1	0.3	0.3	0.2	0.2	0.3	0.3	0.1	0.1	0.8	0.8	0.5	0.4	0.5
120.	0.3	0.5	0.5	1.0	0.8	0.1	0.2	0.4	0.4	0.3	0.2	0.2	0.2	0.1	0.1	0.7	0.7	0.5	0.4	0.6
130.	0.3	0.4	0.5	1.0	0.8	0.1	0.2	0.6	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.5	0.7	0.3	0.3	0.4

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
140.	0.4	0.5	0.4	0.9	0.8	0.1	0.1	0.4	0.5	0.2	0.0	0.0	0.0	0.0	0.0	0.5	0.7	0.4	0.1	0.2
150.	0.4	0.4	0.5	0.9	0.8	0.1	0.2	0.4	0.6	0.2	0.0	0.0	0.0	0.0	0.0	0.5	0.8	0.4	0.2	0.2
160.	0.4	0.4	0.6	0.9	0.9	0.1	0.2	0.2	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.8	0.5	0.3	0.2
170.	0.6	0.5	0.5	0.9	1.0	0.1	0.3	0.3	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.7	0.7	0.4	0.2
180.	0.6	0.5	0.7	1.0	1.1	0.1	0.2	0.4	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.5	0.7	0.3	0.1
190.	0.7	0.4	0.8	0.9	1.2	0.2	0.3	0.6	0.7	0.2	0.0	0.0	0.2	0.1	0.1	0.3	0.3	0.5	0.2	0.1
200.	0.6	0.4	0.6	1.0	1.1	0.3	0.4	0.7	0.7	0.3	0.0	0.0	0.4	0.3	0.2	0.2	0.2	0.2	0.1	0.0
210.	0.6	0.5	0.6	0.7	1.0	0.2	0.4	0.4	0.8	0.4	0.0	0.1	0.7	0.6	0.3	0.1	0.1	0.1	0.0	0.0
220.	0.6	0.5	0.4	0.5	0.9	0.1	0.3	0.3	0.7	0.4	0.0	0.1	0.8	0.6	0.5	0.0	0.0	0.0	0.0	0.0
230.	0.5	0.6	0.4	0.4	0.5	0.2	0.1	0.1	0.6	0.7	0.1	0.3	0.9	0.6	0.5	0.0	0.0	0.0	0.0	0.0
240.	0.5	0.6	0.3	0.3	0.3	0.2	0.1	0.1	0.5	0.8	0.1	0.4	0.8	0.7	0.6	0.0	0.0	0.0	0.0	0.0
250.	0.4	0.6	0.3	0.3	0.2	0.4	0.2	0.0	0.3	0.8	0.1	0.4	0.7	0.7	0.5	0.0	0.0	0.0	0.0	0.0
260.	0.4	0.6	0.4	0.3	0.2	0.5	0.3	0.0	0.2	0.6	0.3	0.4	0.5	0.8	0.5	0.0	0.0	0.0	0.0	0.0
270.	0.4	0.5	0.4	0.4	0.1	0.6	0.4	0.0	0.2	0.6	0.2	0.4	0.4	0.8	0.5	0.0	0.0	0.0	0.0	0.0
280.	0.3	0.5	0.6	0.3	0.1	0.8	0.5	0.0	0.1	0.3	0.2	0.3	0.3	0.8	0.5	0.0	0.0	0.0	0.0	0.0
290.	0.3	0.4	0.6	0.2	0.1	0.8	0.6	0.1	0.1	0.3	0.2	0.3	0.3	0.8	0.5	0.0	0.0	0.0	0.0	0.0
300.	0.3	0.5	0.6	0.2	0.1	0.8	0.7	0.1	0.2	0.2	0.4	0.2	0.3	0.8	0.5	0.0	0.0	0.0	0.0	0.0
310.	0.3	0.4	0.5	0.1	0.0	0.8	0.7	0.3	0.4	0.3	0.5	0.3	0.3	0.8	0.5	0.0	0.0	0.0	0.1	0.0
320.	0.2	0.3	0.3	0.0	0.0	0.8	0.6	0.6	0.5	0.3	0.5	0.3	0.4	0.8	0.6	0.0	0.0	0.0	0.2	0.1
330.	0.1	0.1	0.2	0.0	0.0	0.7	0.4	0.7	0.4	0.3	0.6	0.7	0.5	0.9	0.8	0.0	0.0	0.1	0.5	0.4
340.	0.0	0.1	0.1	0.0	0.0	0.7	0.4	0.6	0.3	0.2	0.6	0.6	0.6	0.8	1.1	0.1	0.1	0.3	0.7	0.6
350.	0.0	0.0	0.0	0.0	0.0	0.7	0.6	0.5	0.3	0.2	0.4	0.7	0.5	0.7	1.1	0.1	0.2	0.3	0.7	0.8
360.	0.0	0.0	0.0	0.0	0.0	0.8	0.7	0.5	0.3	0.2	0.4	0.7	0.5	0.6	0.8	0.1	0.3	0.3	0.6	0.8
MAX	0.7	0.6	1.0	1.1	1.2	0.8	0.8	0.7	0.8	0.8	0.6	0.7	0.9	0.9	1.1	0.9	0.8	0.7	0.9	0.9
DEGR.	190	100	70	100	190	0	10	200	210	240	330	0	230	330	340	90	110	170	60	60

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.0	0.0	0.0	0.0	0.0	0.3	0.7	0.7	0.4	0.5	1.0	1.3	1.8	1.4	0.8	0.5	0.9	1.8	2.0	1.8
10.	0.0	0.0	0.0	0.0	0.0	0.2	0.6	0.7	0.3	0.3	1.2	1.1	1.6	1.5	0.9	0.6	0.8	1.5	1.8	1.7
20.	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.7	0.2	0.1	1.0	1.1	1.3	1.4	0.9	0.6	0.8	1.3	1.7	1.7
30.	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.5	0.2	0.0	1.0	1.1	1.1	1.4	0.9	0.6	0.7	1.0	1.5	1.5
40.	0.0	0.0	0.2	0.0	0.0	0.1	0.2	0.3	0.0	0.0	0.9	0.8	1.0	1.3	1.0	0.5	0.6	1.0	1.5	1.5
50.	0.0	0.0	0.3	0.1	0.0	0.1	0.1	0.1	0.0	0.0	0.8	0.8	1.0	1.0	0.8	0.6	0.8	1.2	1.5	1.5
60.	0.0	0.0	0.6	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.7	0.6	0.5	0.7	0.7	1.2	1.5	1.5
70.	0.0	0.0	0.7	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.8	0.7	0.6	0.4	0.3	0.7	0.8	1.0	1.7	1.5

```
  80.  *   0.0   0.1   0.8   0.5   0.1   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.7   0.5   0.3   0.9   0.7   1.0
1.6   1.4
  90.  *   0.0   0.1   0.9   0.6   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   1.0   0.7   0.8
1.6   1.7
 100.  *   0.1   0.3   0.9   0.6   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   1.0   0.8   0.8
1.6   1.7
 110.  *   0.1   0.3   0.8   0.6   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   0.9   0.9   0.7
1.4   1.8
 120.  *   0.2   0.4   0.7   0.7   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   0.8   1.2   0.8
1.3   1.8
 130.  *   0.3   0.4   0.7   0.7   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.4   0.7   1.2   0.9
1.3   1.8
 140.  *   0.3   0.5   0.5   0.7   0.2   0.0   0.0   0.0   0.0   0.0   0.9   0.9   0.9   0.6   0.4   0.9   1.3   1.1
1.0   1.5
 150.  *   0.6   0.4   0.6   0.8   0.2   0.0   0.0   0.0   0.0   0.0   0.9   0.9   1.0   0.5   0.5   0.7   1.4   1.2
1.0   1.1
 160.  *   1.0   0.8   0.8   0.8   0.2   0.0   0.0   0.1   0.1   0.1   1.2   1.3   1.2   0.7   0.5   0.7   1.4   1.6
1.1   1.1
 170.  *   1.6   1.4   1.3   1.1   0.4   0.1   0.2   0.6   0.6   0.6   1.2   1.2   1.3   0.6   0.4   0.8   1.4   1.6
1.2   0.9
 180.  *   1.9   1.9   1.7   1.6   0.8   0.2   0.6   1.2   1.2   1.2   0.8   0.8   0.8   0.3   0.1   0.4   0.8   1.3
0.8   0.5
 190.  *   1.7   1.6   1.7   1.7   1.1   0.6   0.8   1.4   1.3   1.4   0.3   0.3   0.3   0.0   0.0   0.3   0.5   0.9
0.3   0.1
 200.  *   1.5   1.4   1.4   1.6   1.3   0.5   0.7   1.0   1.2   1.1   0.0   0.0   0.0   0.0   0.0   0.3   0.4   0.7
0.3   0.1
 210.  *   1.3   1.3   1.2   1.3   1.3   0.4   0.5   0.9   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.3   0.3   0.7
0.1   0.1
 220.  *   1.2   1.3   1.2   1.1   1.1   0.5   0.6   0.8   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.3   0.3   0.5
0.1   0.0
 230.  *   1.2   1.2   1.1   0.8   0.8   0.9   0.8   1.0   0.9   0.9   0.0   0.0   0.1   0.1   0.1   0.2   0.2   0.3
0.0   0.0
 240.  *   1.2   1.2   1.0   0.7   0.5   0.8   0.9   0.9   1.0   0.9   0.0   0.0   0.4   0.2   0.2   0.1   0.1   0.1
0.0   0.0
 250.  *   1.2   1.2   1.0   0.7   0.5   1.1   0.9   1.1   1.1   0.8   0.0   0.1   0.5   0.3   0.2   0.0   0.0   0.0
0.0   0.0
 260.  *   1.2   1.2   1.1   0.7   0.5   1.1   1.0   0.9   1.2   1.0   0.0   0.1   0.7   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 270.  *   1.2   1.2   1.2   0.7   0.5   1.3   1.0   0.9   1.2   1.1   0.1   0.2   0.8   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 280.  *   1.2   1.2   1.2   0.7   0.6   1.3   1.2   0.9   1.2   1.1   0.1   0.2   0.9   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 290.  *   1.4   1.4   1.4   0.8   0.6   1.2   1.4   1.0   1.1   1.2   0.1   0.2   1.0   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 300.  *   1.4   1.5   1.5   0.8   0.5   1.1   1.5   1.3   0.9   1.2   0.1   0.3   1.0   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 310.  *   1.4   1.5   1.5   0.7   0.4   0.9   1.4   1.6   1.0   1.3   0.1   0.4   1.0   0.3   0.3   0.0   0.0   0.1
0.1   0.1
 320.  *   1.3   1.4   1.5   0.5   0.2   0.6   1.3   1.9   1.5   1.4   0.2   0.4   1.0   0.4   0.3   0.0   0.0   0.4
0.3   0.3
 330.  *   0.9   1.0   1.0   0.3   0.1   0.3   0.9   1.6   1.6   1.7   0.3   0.7   1.2   0.6   0.3   0.0   0.1   1.0
0.9   0.8
 340.  *   0.4   0.5   0.5   0.0   0.0   0.2   0.7   1.2   1.3   1.5   0.7   1.0   1.5   0.8   0.3   0.1   0.4   1.8
1.6   1.5
 350.  *   0.1   0.1   0.1   0.0   0.0   0.2   0.6   1.0   0.8   1.0   1.0   1.3   1.9   1.2   0.6   0.4   0.7   2.0
2.0   1.9
 360.  *   0.0   0.0   0.0   0.0   0.0   0.3   0.7   0.7   0.4   0.5   1.0   1.3   1.8   1.4   0.8   0.5   0.9   1.8
2.0   1.8

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 MAX   *   1.9   1.9   1.7   1.7   1.3   1.3   1.5   1.9   1.6   1.7   1.2   1.3   1.9   1.5   1.0   1.0   1.4   2.0
2.0   1.9
 DEGR. *  180   180   180   190   200   270   300   320   330   330    10     0   350    10    40    90   160   350
0   350
```


JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

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 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52 REC53 REC54 REC55 REC56 REC57 REC58
REC59 REC60

------*-----------------------------------------------------------------------------------------------------------------
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   0.  *   0.5   0.8   0.8   0.0   0.0   0.0   0.0   0.7   1.0   1.1   1.1   1.0   1.0   0.6   0.2   0.2   0.4   0.9
0.8   0.8
  10.  *   0.1   0.3   0.3   0.0   0.0   0.0   0.0   0.2   0.3   0.3   1.4   1.3   1.3   0.6   0.6   0.4   0.6   1.2
1.1   1.1
  20.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.7   1.4   1.4   0.6   0.4   0.3   0.5   1.1
```



```
1.1   0.9
  30.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.7   1.4   1.2   0.7   0.5   0.5   0.7   1.0
1.0   0.8
  40.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.6   1.6   1.2   0.7   0.6   0.4   0.6   1.0
1.0   0.8
  50.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.4   1.4   1.0   0.7   0.5   0.4   0.6   0.9
0.9   0.7
  60.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.3   1.4   0.9   0.7   0.6   0.5   0.7   0.9
0.9   0.8
  70.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.3   1.2   0.8   0.7   0.5   0.5   0.8   0.9
0.9   0.8
  80.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.2   1.3   1.0   0.8   0.6   0.5   0.8   0.9
0.9   0.9
  90.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1   1.3   1.0   0.9   0.6   0.5   0.7   1.1
0.9   0.9
 100.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0   1.3   1.1   0.9   0.7   0.6   0.7   1.2
0.9   0.9
 110.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9   1.3   1.0   0.9   0.7   0.6   0.7   1.2
0.9   0.9
 120.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9   1.4   1.2   0.9   0.8   0.7   0.9   1.2
0.9   0.9
 130.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.2   1.4   1.3   0.8   1.1   0.8   0.9   1.2
1.0   1.0
 140.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.6   1.4   1.5   1.0   1.2   1.1   1.0   1.3
1.1   1.2
 150.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   2.1   1.8   1.6   1.5   1.1   1.2   1.2   1.6
1.1   1.4
 160.  *   0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.2   0.1   0.1   3.0   2.1   1.9   1.6   0.9   1.0   1.3   1.8
1.6   1.5
 170.  *   0.6   0.6   0.7   0.1   0.1   0.1   0.1   0.6   0.6   0.6   3.1   2.1   2.1   1.3   0.3   0.7   1.1   2.0
1.8   1.7
 180.  *   1.2   1.4   1.5   0.3   0.2   0.2   0.3   1.5   1.4   1.3   2.3   1.8   1.6   0.6   0.1   0.1   0.5   1.3
1.5   1.3
 190.  *   1.8   1.9   1.9   0.9   0.3   0.3   0.8   1.9   1.8   1.8   1.2   1.0   0.7   0.2   0.0   0.0   0.2   0.7
0.5   0.4
 200.  *   1.4   1.7   2.0   0.9   0.8   0.4   1.0   1.9   2.1   2.0   0.7   0.5   0.3   0.1   0.0   0.0   0.1   0.1
0.1   0.0
 210.  *   1.2   1.1   1.4   1.0   0.8   0.8   1.1   1.7   2.1   1.9   0.4   0.3   0.0   0.0   0.0   0.0   0.1   0.1
0.0   0.0
 220.  *   1.1   1.2   1.3   0.7   0.8   0.8   0.9   1.4   1.7   1.8   0.3   0.2   0.0   0.0   0.0   0.0   0.1   0.1
0.0   0.0
 230.  *   1.0   1.0   1.2   0.7   0.4   0.6   0.7   1.2   1.4   1.5   0.4   0.1   0.0   0.0   0.0   0.0   0.0   0.1
0.0   0.0
 240.  *   0.9   0.9   1.2   0.6   0.4   0.4   0.6   1.3   1.4   1.5   0.5   0.1   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 250.  *   0.8   0.9   0.9   0.6   0.4   0.3   0.6   1.1   1.3   1.4   0.6   0.1   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 260.  *   0.8   0.9   1.0   0.6   0.4   0.4   0.7   1.3   1.3   1.4   0.6   0.0   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 270.  *   0.8   0.9   1.0   0.5   0.3   0.3   0.6   1.2   1.4   1.4   0.7   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 280.  *   0.8   0.9   1.0   0.6   0.3   0.4   0.6   1.1   1.3   1.4   0.7   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 290.  *   0.7   0.9   1.0   0.6   0.3   0.3   0.5   1.0   1.2   1.3   0.7   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 300.  *   0.8   0.9   1.0   0.5   0.3   0.3   0.5   1.1   1.3   1.4   0.6   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 310.  *   1.0   0.9   1.0   0.5   0.3   0.3   0.5   1.1   1.2   1.3   0.5   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 320.  *   1.0   1.1   1.1   0.5   0.4   0.4   0.6   1.2   1.2   1.6   0.4   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.1
 330.  *   1.4   1.4   1.4   0.7   0.5   0.5   0.7   1.4   1.4   1.5   0.3   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1
 340.  *   1.6   1.4   1.4   0.8   0.4   0.4   0.7   1.4   1.7   2.0   0.4   0.2   0.2   0.1   0.0   0.0   0.1   0.2
0.3   0.4
 350.  *   1.2   1.1   1.2   0.4   0.2   0.2   0.4   1.2   1.4   1.5   0.6   0.7   0.6   0.3   0.1   0.1   0.3   0.6
0.7   0.7
 360.  *   0.5   0.8   0.8   0.0   0.0   0.0   0.0   0.7   1.0   1.1   1.1   1.0   1.0   0.6   0.2   0.2   0.4   0.9
0.8   0.8

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 MAX   *   1.8   1.9   2.0   1.0   0.8   0.8   1.1   1.9   2.1   2.0   3.1   2.1   2.1   1.6   1.2   1.2   1.3   2.0
1.8   1.7
 DEGR. *  190   190   200   210   200   210   210   190   200   200   170   160   170   160   140   150   160   170
170   170
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THE HIGHEST CONCENTRATION OF   3.10 PPM OCCURRED AT RECEPTOR REC51.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: No Build

DATE : 7/10/13
TIME : 15:35:38

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1. Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	75.	100.0	1.0	10.0	0.71
2. Stan/Lom SB TRR	*	5173.5	5937.1	5111.3	6026.2	*	109.	325.	AG	151.	100.0	1.0	20.0	0.50
3. Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	183.	100.0	1.0	20.0	0.92
4. Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	75.	100.0	1.0	10.0	0.58
5. Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	98.	100.0	1.0	10.0	0.64
6. Stan/Lom NB TRR	*	5314.4	5765.3	5363.1	5748.8	*	51.	109.	AG	195.	100.0	1.0	20.0	0.41
7. Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	195.	100.0	1.0	20.0	0.68
8. Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	98.	100.0	1.0	10.0	0.93
9. Caus/Wash SB LTTRR	*	6548.6	6868.7	6176.7	7641.4	*	857.	334.	AG	302.	100.0	1.0	40.0	1.08
10. Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	191.	100.0	1.0	20.0	0.58
11. Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	84.	100.0	1.0	10.0	0.53
12. Caus/Wash NB TTR	*	6603.5	6751.9	6665.3	5376.7	*	1377.	177.	AG	193.	100.0	1.0	20.0	1.39
13. Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	282.	100.0	1.0	30.0	0.47
14. Tha/Val SB LTTR	*	6599.0	6224.0	6593.7	6361.5	*	138.	358.	AG	70.	100.0	1.0	20.0	0.79
15. Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	86.	100.0	1.0	10.0	1.23
16. Tha/Val NB TR	*	6645.6	6138.6	6647.7	6017.7	*	121.	179.	AG	35.	100.0	1.0	10.0	0.69
17. Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6097.3	*	133.	0.	AG	163.	100.0	1.0	30.0	0.68
18. Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	199.	100.0	1.0	30.0	0.18
19. Char/93 SB LLTTRR	*	6587.8	5740.0	6582.3	5883.7	*	144.	358.	AG	256.	100.0	1.0	40.0	0.74
20. Char/93 WB LTT	*	6702.8	5647.8	6763.4	5572.1	*	97.	141.	AG	167.	100.0	1.0	20.0	0.62
21. Char/93 EB TTR	*	6560.8	5622.5	6520.0	5592.6	*	51.	234.	AG	250.	100.0	1.0	30.0	0.32
22. North/Congress SB LT	*	6876.6	4408.9	6569.4	5930.4	*	1552.	349.	AG	326.	100.0	1.0	30.0	2.69
23. North/Con WB LLTR	*	6920.6	4378.3	7106.5	4444.1	*	197.	71.	AG	145.	100.0	1.0	20.0	0.89
24. Nor/Con NB LTTTR	*	6914.9	4333.4	6920.9	4289.3	*	45.	172.	AG	268.	100.0	1.0	30.0	0.33
25. Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	72.	100.0	1.0	10.0	0.03
26. Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1396.	8.3	1.0	90.0	
27. Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1568.	8.3	1.0	78.0	
28. Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	899.	8.3	1.0	78.0	
29. Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	8.3	1.0	78.0	
30. Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3419.	8.3	1.0	90.0	
31. Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	8.3	1.0	66.0	
32. Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2371.	8.3	1.0	90.0	
33. Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	8.3	1.0	78.0	
34. Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2397.	8.3	1.0	90.0	
35. Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	8.3	1.0	38.0	
36. Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2837.	8.3	1.0	90.0	
37. Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	8.3	1.0	54.0	
38. Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2324.	8.3	1.0	66.0	
39. Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	8.3	1.0	48.0	
40. Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	515.	8.3	1.0	42.0	
41. Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	8.3	1.0	48.0	
42. Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	403.	8.3	1.0	54.0	
43. Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	702.	8.3	1.0	54.0	

44. Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	8.3	1.0	42.0	

JOB: Government Center Garage RUN: No Build

DATE : 7/10/13
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LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45. North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1343.	8.3	1.0	98.0	
46. North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1063.	8.3	1.0	66.0	
47. North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1529.	8.3	1.0	98.0	
48. North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	8.3	1.0	54.0	

JOB: Government Center Garage RUN: No Build

DATE : 7/10/13
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ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. Stan/Lom SB L	*	120	75	3.0	376	1600	44.99	1	3
2. Stan/Lom SB TRR	*	120	75	3.0	531	1600	44.99	1	3
3. Stan/Lom WB LTT	*	120	91	3.0	588	1600	44.99	1	3
4. Stan/Lom WB R	*	120	75	3.0	308	1600	44.99	1	3
5. Stan/Lom NB L	*	120	97	3.0	152	1600	44.99	1	3
6. Stan/Lom NB TRR	*	120	97	3.0	194	1600	44.99	1	3
7. Stan/Lom EB LLT	*	120	97	3.0	324	1600	44.99	1	3
8. Stan/Lom EB R	*	120	97	3.0	222	1600	44.99	1	3
9. Caus/Wash SB LTTRR	*	150	94	3.0	2353	1600	44.99	1	3
10. Caus/Wash WB LLTT	*	150	119	3.0	321	1600	44.99	1	3
11. Caus/Wash WB R	*	150	104	3.0	230	1600	44.99	1	3
12. Caus/Wash NB TTR	*	150	120	3.0	741	1600	44.99	1	3
13. Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	44.99	1	3
14. Tha/Val SB LTTR	*	104	30	3.0	1678	1600	44.99	1	3
15. Tha/Val NB L	*	104	74	3.0	472	1600	44.99	1	3
16. Tha/Val NB TR	*	104	30	3.0	737	1600	44.99	1	3
17. Bev/Was SB TTT	*	100	45	3.0	1628	1600	44.99	1	3
18. Bev/Was EB RRR	*	100	55	3.0	356	1600	44.99	1	3
19. Char/93 SB LLTTRR	*	100	53	3.0	1986	1600	44.99	1	3
20. Char/93 WB LTT	*	100	69	3.0	515	1600	44.99	1	3
21. Char/93 EB TTR	*	100	69	3.0	403	1600	44.99	1	3
22. North/Congress SB LT	*	100	90	3.0	647	1600	44.99	1	3
23. North/Con WB LLTR	*	100	60	3.0	997	1600	44.99	1	3
24. Nor/Con NB LTTTR	*	100	74	3.0	332	1600	44.99	1	3
25. Nor/Con EB LTR	*	100	60	3.0	17	1600	44.99	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Bev/Was N1	*	6562.0	6150.2	6.0	*
2. Bev/Was N2	*	6561.2	6075.2	6.0	*
3. Bev/Was N3	*	6560.5	6000.2	6.0	*
4. Bev/Was N4	*	6515.8	6060.4	6.0	*
5. Bev/Was N5	*	6471.1	6120.6	6.0	*
6. Bev/Was SE1	*	6671.0	6049.7	6.0	*
7. Bev/Was SE2	*	6670.2	5966.3	6.0	*
8. Bev/Was SE3	*	6624.0	5907.2	6.0	*
9. Bev/Was SE4	*	6626.1	5832.3	6.0	*
10. Bev/Was SE5	*	6628.1	5757.3	6.0	*
11. Bev/Was SW1	*	6541.8	5766.9	6.0	*
12. Bev/Was SW2	*	6540.1	5841.9	6.0	*
13. Bev/Was SW3	*	6537.7	5916.8	6.0	*
14. Bev/Was SW4	*	6493.0	5977.0	6.0	*
15. Bev/Was SW5	*	6448.3	6037.3	6.0	*
16. Char/93 NE1	*	6625.0	5871.1	6.0	*
17. Char/93 NE2	*	6627.1	5796.1	6.0	*
18. Char/93 NE3	*	6629.1	5721.1	6.0	*
19. Char/93 NE4	*	6699.8	5695.9	6.0	*
20. Char/93 NE5	*	6750.6	5633.2	6.0	*

JOB: Government Center Garage RUN: No Build

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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
21. Char/93 S1	6657.8	5466.0	6.0
22. Char/93 S2	6614.7	5527.4	6.0
23. Char/93 S3	6571.7	5588.8	6.0
24. Char/93 S4	6512.9	5542.2	6.0
25. Char/93 S5	6454.1	5495.6	6.0
26. Char/93 NW1	6424.1	5632.5	6.0
27. Char/93 NW2	6483.6	5678.2	6.0
28. Char/93 NW3	6543.0	5723.9	6.0
29. Char/93 NW4	6541.0	5798.8	6.0
30. Char/93 NW5	6538.9	5873.8	6.0
31. Wash/Cong NE1	6910.2	4571.2	6.0
32. Wash/Cong NE2	6925.8	4497.8	6.0
33. Wash/Cong NE3	6941.4	4424.5	6.0
34. Wash/Cong NE4	7012.0	4449.6	6.0
35. Wash/Cong NE5	7082.7	4474.9	6.0
36. Wash/Cong SE1	7095.4	4388.1	6.0
37. Wash/Cong SE2	7024.8	4362.9	6.0
38. Wash/Cong SE3	6954.1	4337.7	6.0
39. Wash/Cong SE4	6968.4	4264.1	6.0
40. Wash/Cong SE5	6982.7	4190.4	6.0
41. Wash/Cong SW1	6867.5	4164.7	6.0
42. Wash/Cong SW2	6853.3	4238.0	6.0
43. Wash/Cong SW3	6838.9	4312.0	6.0
44. Wash/Cong SW4	6765.6	4296.1	6.0
45. Wash/Cong SW5	6692.3	4280.2	6.0
46. Wash/Cong NW1	6682.4	4353.8	6.0
47. Wash/Cong NW2	6755.7	4369.7	6.0
48. Wash/Cong NW3	6828.9	4386.0	6.0
49. Wash/Cong NW4	6813.3	4459.4	6.0
50. Wash/Cong NW5	6797.8	4532.8	6.0

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	1.1	1.0	1.1	0.6	0.3	1.0	1.2	3.1	2.6	2.9	1.4	1.2	1.1	0.7	0.4	2.8	2.8	3.3	0.4	0.2
10.	1.3	1.3	1.3	0.7	0.5	0.3	0.3	2.6	2.3	2.0	2.1	1.5	1.3	0.6	0.6	2.4	2.2	2.2	0.1	0.0
20.	1.5	1.3	1.4	0.8	0.4	0.0	0.1	2.2	1.7	1.5	2.4	2.0	1.4	0.8	0.4	1.9	1.5	1.5	0.0	0.0
30.	1.3	1.2	1.6	0.8	0.5	0.0	0.0	1.8	1.3	1.1	2.3	2.1	1.4	0.8	0.5	1.5	1.2	1.1	0.0	0.0
40.	1.3	1.1	1.5	0.8	0.6	0.0	0.0	1.4	1.1	0.9	2.2	2.0	1.3	0.8	0.6	1.2	1.0	0.9	0.0	0.0
50.	1.3	1.3	1.4	0.7	0.6	0.0	0.0	1.2	0.9	0.8	2.1	2.1	1.3	1.0	0.5	1.0	0.9	0.7	0.0	0.0
60.	1.1	1.3	1.4	0.7	0.7	0.0	0.0	1.1	0.9	0.8	2.0	2.1	1.4	1.1	0.5	0.9	0.8	0.6	0.0	0.0
70.	1.2	1.1	1.2	0.9	0.7	0.0	0.0	1.0	0.9	0.7	2.0	2.0	1.4	1.2	0.5	0.9	0.8	0.6	0.0	0.0
80.	1.2	1.4	1.3	0.9	0.8	0.0	0.0	1.0	0.9	0.7	2.0	2.1	1.5	1.2	0.5	0.9	0.7	0.6	0.0	0.0
90.	1.1	1.4	1.3	0.9	0.7	0.0	0.0	0.9	0.8	0.6	2.0	2.1	1.6	1.1	0.7	0.9	0.7	0.6	0.0	0.0
100.	1.0	1.3	1.3	0.9	0.7	0.0	0.0	0.9	0.9	0.7	1.9	2.1	1.6	1.2	0.7	0.9	0.8	0.7	0.0	0.0
110.	1.0	1.3	1.3	0.9	0.8	0.0	0.0	1.0	0.9	0.7	1.7	2.1	1.8	1.1	0.8	0.9	0.8	0.7	0.0	0.0
120.	1.0	1.4	1.3	0.9	0.9	0.0	0.0	1.0	0.9	0.8	1.8	2.1	1.9	1.4	0.9	0.9	0.8	1.1	0.0	0.0
130.	1.1	1.4	1.2	0.9	0.9	0.0	0.0	1.2	0.9	1.0	1.8	2.3	2.2	1.3	1.0	1.1	0.9	1.1	0.0	0.0
140.	1.3	1.6	1.3	0.9	0.9	0.0	0.0	1.1	1.1	1.2	1.7	2.6	2.4	1.5	1.3	1.1	1.2	1.5	0.2	0.1
150.	1.5	1.6	1.7	1.5	1.2	0.0	0.0	1.4	1.6	1.6	1.6	2.3	2.8	1.7	1.2	1.4	1.6	1.8	0.4	0.2
160.	1.9	2.0	2.1	1.7	1.4	0.1	0.2	1.9	2.2	2.3	1.3	2.1	2.6	1.4	0.9	2.1	2.2	2.6	0.7	0.6
170.	2.0	2.0	2.5	1.4	0.9	0.6	0.5	2.5	2.7	2.9	1.1	1.4	1.8	0.8	0.4	2.5	2.7	3.6	1.1	0.8
180.	1.4	1.7	2.0	0.7	0.3	1.3	1.1	2.7	2.8	3.1	0.5	0.8	0.8	0.1	0.1	2.7	2.8	3.5	1.3	1.0

190.	0.8	0.7	1.1	0.3	0.1	1.9	1.6	2.5	2.6	2.6	0.2	0.2	0.2	0.0	0.0	2.5	2.5	3.0	1.3	1.2
200.	0.2	0.2	0.6	0.1	0.1	2.0	1.9	2.3	2.4	2.3	0.1	0.1	0.0	0.0	0.0	2.3	2.3	2.4	1.3	1.3
210.	0.1	0.2	0.4	0.1	0.1	2.0	1.9	2.0	2.2	2.0	0.1	0.0	0.0	0.0	0.0	2.3	2.2	2.0	1.2	1.3
220.	0.2	0.0	0.5	0.1	0.1	1.7	1.8	1.9	2.2	1.9	0.1	0.0	0.0	0.0	0.0	2.1	2.1	2.0	1.2	1.3
230.	0.2	0.0	0.4	0.1	0.1	1.7	1.8	1.7	2.0	1.6	0.0	0.0	0.0	0.0	0.0	2.0	2.3	1.8	1.2	1.3
240.	0.2	0.0	0.4	0.0	0.1	1.5	1.6	1.5	2.0	1.8	0.0	0.0	0.0	0.0	0.0	1.8	2.1	1.4	1.2	1.2
250.	0.2	0.0	0.3	0.0	0.0	1.3	1.3	1.4	2.0	1.9	0.0	0.0	0.0	0.0	0.0	1.8	2.0	1.4	1.3	1.3
260.	0.2	0.0	0.2	0.0	0.0	1.4	1.5	1.3	2.0	2.2	0.0	0.0	0.0	0.0	0.0	1.8	2.0	1.4	1.2	1.4
270.	0.1	0.1	0.1	0.0	0.0	1.4	1.3	1.2	2.0	2.2	0.0	0.0	0.0	0.0	0.0	1.7	2.0	1.3	1.1	1.5
280.	0.1	0.1	0.1	0.1	0.0	1.4	1.4	1.0	2.0	2.2	0.0	0.0	0.0	0.0	0.0	1.6	2.1	1.5	1.2	1.2
290.	0.1	0.1	0.1	0.1	0.0	1.3	1.2	1.0	2.0	2.3	0.0	0.0	0.0	0.0	0.0	1.5	2.1	1.9	1.3	1.1
300.	0.1	0.1	0.1	0.1	0.0	1.3	1.3	1.0	2.0	2.4	0.0	0.0	0.0	0.0	0.0	1.3	2.2	2.3	1.4	1.1
310.	0.1	0.1	0.1	0.1	0.0	1.3	1.4	0.9	1.9	2.7	0.0	0.0	0.0	0.0	0.0	1.3	2.4	2.7	1.6	1.3
320.	0.1	0.1	0.0	0.1	0.0	1.4	1.5	0.9	2.0	2.9	0.0	0.0	0.0	0.0	0.0	1.2	2.4	3.0	1.6	1.2
330.	0.1	0.1	0.1	0.1	0.0	1.5	1.6	1.1	2.0	3.0	0.0	0.0	0.2	0.0	0.0	1.2	2.4	3.4	1.3	0.9
340.	0.2	0.2	0.2	0.2	0.0	1.9	1.8	1.7	1.8	3.1	0.0	0.0	0.3	0.0	0.0	1.7	2.4	3.6	1.5	1.0
350.	0.6	0.7	0.7	0.3	0.2	1.5	1.8	2.5	2.4	3.1	0.4	0.4	0.6	0.2	0.1	2.4	2.9	3.9	1.3	0.6
360.	1.1	1.0	1.1	0.6	0.3	1.0	1.2	3.1	2.6	2.9	1.4	1.2	1.1	0.7	0.4	2.8	2.8	3.3	0.4	0.2
MAX	2.0	2.0	2.5	1.7	1.4	2.0	1.9	3.1	2.8	3.1	2.4	2.6	2.8	1.7	1.3	2.8	2.9	3.9	1.6	1.5
DEGR.	170	160	170	160	160	200	200	0	180	340	20	140	150	150	140	0	350	350	310	270

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	4.8	2.3	1.7	1.0	0.4	0.1	0.4	1.5	1.4	1.1	0.1	0.2	0.2	0.0	0.0	0.4	0.4	0.7	0.5	0.4
10.	4.1	2.4	1.9	1.5	0.8	0.3	0.7	2.0	1.8	1.3	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.4	0.2	0.2
20.	3.1	2.1	1.4	1.5	1.0	0.6	1.2	2.3	2.3	1.8	0.0	0.0	0.0	0.0	0.0	0.2	0.5	0.6	0.2	0.2
30.	2.5	1.9	1.1	1.3	1.2	0.6	1.2	2.2	2.4	1.8	0.0	0.0	0.0	0.0	0.0	0.1	0.5	0.6	0.2	0.0
40.	2.0	1.8	1.1	1.1	0.8	0.9	1.3	2.1	2.3	1.8	0.0	0.0	0.0	0.0	0.0	0.1	0.4	0.6	0.2	0.0
50.	1.7	1.8	0.9	0.8	0.8	1.0	1.0	1.8	2.2	1.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.0	0.0
60.	1.7	1.8	1.0	0.7	0.6	0.7	1.1	1.6	2.0	1.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.0	0.0
70.	1.6	1.7	1.1	0.8	0.6	0.6	0.9	1.4	2.0	1.8	0.0	0.0	0.2	0.1	0.0	0.0	0.1	0.2	0.0	0.0
80.	1.6	1.6	1.1	0.8	0.6	0.8	0.6	1.3	2.0	1.9	0.0	0.0	0.4	0.2	0.0	0.0	0.0	0.1	0.0	0.0
90.	1.6	1.5	1.2	0.8	0.6	0.8	0.8	1.1	2.0	2.0	0.0	0.0	0.6	0.4	0.0	0.0	0.0	0.0	0.0	0.0
100.	1.6	1.6	1.2	0.8	0.5	0.9	0.9	0.9	2.0	2.0	0.0	0.1	0.6	0.4	0.0	0.0	0.0	0.0	0.0	0.0
110.	1.8	1.7	1.1	0.7	0.5	1.0	1.1	1.0	2.0	2.1	0.0	0.2	0.6	0.5	0.0	0.0	0.0	0.0	0.0	0.0
120.	1.8	1.8	1.1	0.7	0.5	0.9	1.1	1.2	2.1	2.2	0.0	0.2	0.6	0.5	0.0	0.0	0.0	0.0	0.0	0.0

130.	*	2.1	1.7	1.2	0.6	0.4	0.8	1.3	1.4	2.2	2.3	0.2	0.2	0.5	0.5	0.2	0.0	0.0	0.0
0.0	0.0																		
140.	*	2.5	1.8	1.1	0.6	0.4	0.8	1.1	1.3	2.2	2.5	0.2	0.2	0.5	0.5	0.2	0.0	0.0	0.0
0.0	0.0																		
150.	*	3.2	1.8	1.1	0.5	0.4	0.7	1.1	1.4	1.9	2.6	0.2	0.2	0.5	0.5	0.3	0.0	0.0	0.0
0.0	0.0																		
160.	*	3.8	1.8	0.9	0.4	0.2	0.5	0.8	1.2	1.6	2.3	0.4	0.3	0.6	0.5	0.4	0.0	0.0	0.1
0.1	0.1																		
170.	*	4.0	1.3	0.6	0.3	0.1	0.3	0.6	0.9	1.2	1.6	0.4	0.6	0.8	0.5	0.5	0.0	0.0	0.2
0.2	0.2																		
180.	*	3.4	0.7	0.2	0.0	0.0	0.2	0.3	0.7	0.6	0.8	0.8	0.6	0.9	0.6	0.5	0.0	0.1	0.4
0.3	0.3																		
190.	*	2.5	0.3	0.0	0.0	0.0	0.2	0.3	0.4	0.2	0.3	0.7	0.7	0.9	0.6	0.6	0.0	0.1	0.5
0.4	0.3																		
200.	*	1.7	0.1	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.9	0.6	0.9	0.9	0.7	0.1	0.2	0.6
0.4	0.3																		
210.	*	1.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.1	0.0	0.8	0.6	0.8	0.9	0.7	0.1	0.2	0.7
0.4	0.3																		
220.	*	0.9	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.0	0.0	0.9	0.7	0.6	0.9	0.8	0.1	0.2	0.7
0.3	0.3																		
230.	*	0.9	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.8	0.8	0.4	0.6	0.8	0.1	0.3	0.8
0.3	0.3																		
240.	*	0.6	0.0	0.1	0.1	0.0	0.0	0.0	0.1	0.0	0.0	0.7	0.7	0.5	0.6	0.5	0.3	0.4	0.8
0.3	0.3																		
250.	*	0.6	0.0	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.5	0.5	0.5	0.3	0.5	0.8
0.3	0.3																		
260.	*	0.7	0.0	0.4	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.6	0.3	0.4	0.5	0.5	0.7
0.3	0.3																		
270.	*	0.6	0.0	0.5	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.7	0.5	0.3	0.8	0.4	0.6
0.3	0.3																		
280.	*	0.6	0.0	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.8	0.8	0.5	0.3	0.9	0.8	0.5
0.4	0.3																		
290.	*	0.7	0.1	0.8	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.8	0.5	0.4	0.9	0.8	0.6
0.5	0.3																		
300.	*	0.8	0.2	0.8	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.9	0.9	0.9	0.6	0.4	1.0	0.9	0.6
0.6	0.3																		
310.	*	1.2	0.3	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.9	0.9	0.9	0.6	0.4	0.9	1.0	1.0
0.7	0.4																		
320.	*	1.6	0.3	0.7	0.2	0.2	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	0.5	0.4	0.8	1.0	1.2
1.0	0.6																		
330.	*	2.5	0.3	0.7	0.2	0.2	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.1	0.5	0.3	0.7	0.9	1.5
1.2	0.8																		
340.	*	3.8	0.9	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.1	1.0	1.1	1.1	0.4	0.3	0.7	1.0	1.5
1.3	1.1																		
350.	*	4.8	1.7	1.2	0.4	0.2	0.1	0.1	0.5	0.4	0.4	0.6	0.6	0.7	0.3	0.2	0.6	0.7	1.2
0.9	1.0																		
360.	*	4.8	2.3	1.7	1.0	0.4	0.1	0.4	1.5	1.4	1.1	0.1	0.2	0.2	0.0	0.0	0.4	0.4	0.7
0.5	0.4																		
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MAX	*	4.8	2.4	1.9	1.5	1.2	1.0	1.3	2.3	2.4	2.6	1.0	1.1	1.1	0.9	0.8	1.0	1.0	1.5
1.3	1.1																		
DEGR.	*	0	10	10	10	30	110	130	20	30	150	320	340	330	200	220	300	310	330
340	340																		

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50
0.	* 0.8	1.0	1.1	0.6	0.4	0.4	0.6	1.3	1.3	1.2
10.	* 0.8	0.8	0.9	0.5	0.4	0.3	0.6	1.2	1.1	1.1
20.	* 0.8	0.8	0.8	0.6	0.4	0.4	0.6	1.1	1.1	1.1
30.	* 0.7	0.7	0.6	0.4	0.4	0.4	0.6	1.0	1.0	1.0
40.	* 0.5	0.7	0.6	0.3	0.3	0.4	0.6	0.9	0.9	0.9
50.	* 0.3	0.7	0.8	0.5	0.3	0.4	0.5	0.8	0.9	0.9
60.	* 0.3	0.5	0.8	0.5	0.5	0.3	0.5	0.6	0.8	0.8
70.	* 0.3	0.4	0.8	0.5	0.3	0.5	0.5	0.6	0.9	0.9
80.	* 0.3	0.3	0.7	0.5	0.3	0.5	0.5	0.8	0.9	0.9
90.	* 0.3	0.3	0.6	0.3	0.2	0.3	0.3	0.7	1.1	0.9
100.	* 0.3	0.3	0.5	0.3	0.1	0.2	0.4	0.6	1.1	0.8
110.	* 0.3	0.3	0.5	0.2	0.1	0.1	0.3	0.6	1.1	1.1
120.	* 0.3	0.3	0.4	0.2	0.1	0.1	0.3	0.5	1.0	1.1
130.	* 0.3	0.4	0.4	0.2	0.1	0.1	0.2	0.5	0.9	1.1
140.	* 0.3	0.4	0.4	0.2	0.1	0.1	0.2	0.5	0.8	1.1
150.	* 0.3	0.4	0.4	0.1	0.0	0.0	0.1	0.5	0.6	0.9
160.	* 0.2	0.3	0.3	0.0	0.0	0.0	0.1	0.4	0.5	0.6
170.	* 0.1	0.2	0.2	0.0	0.0	0.0	0.0	0.3	0.3	0.3

180.	*	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.1	0.1
190.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
200.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
210.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
220.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
230.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
240.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
250.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
260.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
270.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
280.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
290.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
300.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
310.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
320.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
330.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1
340.	*	0.3	0.4	0.4	0.1	0.0	0.0	0.1	0.4	0.4	0.4
350.	*	0.8	0.8	1.0	0.3	0.1	0.1	0.4	1.0	0.9	0.9
360.	*	0.8	1.0	1.1	0.6	0.4	0.4	0.6	1.3	1.3	1.2
------	*	----	----	----	----	----	----	----	----	----	----
MAX	*	0.8	1.0	1.1	0.6	0.5	0.5	0.6	1.3	1.3	1.2
DEGR.	*	0	0	0	0	60	70	0	0	0	0

THE HIGHEST CONCENTRATION OF 4.80 PPM OCCURRED AT RECEPTOR REC21.

♀ CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: No Build

DATE : 7/10/13
TIME : 15:35:44

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Stan/Lom SB L	*	5194.4	5948.0	5120.9	6056.9	*	131.	326.	AG	79.	100.0	1.0	10.0	0.63	6.7
2. Stan/Lom SB TRR	*	5173.5	5937.1	5093.7	6051.5	*	140.	325.	AG	159.	100.0	1.0	20.0	0.67	7.1
3. Stan/Lom WB LTT	*	5306.8	5930.3	5368.6	5981.0	*	80.	51.	AG	143.	100.0	1.0	20.0	0.35	4.1
4. Stan/Lom WB R	*	5292.4	5947.7	5403.8	6033.2	*	140.	52.	AG	79.	100.0	1.0	10.0	0.68	7.1
5. Stan/Lom NB L	*	5307.6	5737.4	5341.6	5726.9	*	36.	107.	AG	94.	100.0	1.0	10.0	0.24	1.8
6. Stan/Lom NB TRR	*	5314.4	5765.3	5383.7	5741.9	*	73.	109.	AG	187.	100.0	1.0	20.0	0.49	3.7
7. Stan/Lom EB LLT	*	5214.5	5705.3	5171.4	5556.9	*	155.	196.	AG	195.	100.0	1.0	20.0	0.92	7.9
8. Stan/Lom EB R	*	5236.5	5698.5	4944.8	4671.4	*	1068.	196.	AG	98.	100.0	1.0	10.0	1.34	54.2
9. Char/93 SB LLTTRR	*	6587.8	5740.0	6580.9	5920.1	*	180.	358.	AG	299.	100.0	1.0	40.0	0.87	9.2
10. Char/93 WB LTT	*	6702.8	5647.8	6735.6	5606.8	*	52.	141.	AG	145.	100.0	1.0	20.0	0.29	2.7
11. Char/93 EB TTR	*	6560.8	5622.5	6474.2	5559.1	*	107.	234.	AG	217.	100.0	1.0	30.0	0.58	5.5
12. Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1623.	8.3	1.0	90.0		
13. Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1414.	8.3	1.0	78.0		
14. Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	1179.	8.3	1.0	78.0		
15. Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1387.	8.3	1.0	78.0		
16. Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2078.	8.3	1.0	66.0		
17. Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	321.	8.3	1.0	42.0		
18. Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	1059.	8.3	1.0	48.0		
19. Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	983.	8.3	1.0	54.0		
20. Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	488.	8.3	1.0	54.0		
21. Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	414.	8.3	1.0	42.0		

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JOB: Government Center Garage RUN: No Build

DATE : 7/10/13
TIME : 15:35:44

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. Stan/Lom SB L	*	120	79	3.0	304	1600	44.99	1	3
2. Stan/Lom SB TRR	*	120	79	3.0	646	1600	44.99	1	3
3. Stan/Lom WB LTT	*	120	71	3.0	412	1600	44.99	1	3
4. Stan/Lom WB R	*	120	79	3.0	325	1600	44.99	1	3
5. Stan/Lom NB L	*	120	93	3.0	70	1600	44.99	1	3
6. Stan/Lom NB TRR	*	120	93	3.0	289	1600	44.99	1	3
7. Stan/Lom EB LLT	*	120	97	3.0	439	1600	44.99	1	3
8. Stan/Lom EB R	*	120	97	3.0	320	1600	44.99	1	3
9. Char/93 SB LLTTRR	*	100	62	3.0	1829	1600	44.99	1	3
10. Char/93 WB LTT	*	100	60	3.0	321	1600	44.99	1	3
11. Char/93 EB TTR	*	100	60	3.0	983	1600	44.99	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2. Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3. Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4. Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5. Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6. Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7. Stan/Lom SE2	*	5321.0	5869.4	6.0	*

8. Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9. Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10. Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11. Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12. Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13. Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14. Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15. Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16. Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17. Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18. Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19. Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20. Stan/Lom NW5	*	5136.5	5935.7	6.0	*
21. Char/93 NE1	*	6625.0	5871.1	6.0	*
22. Char/93 NE2	*	6627.1	5796.1	6.0	*
23. Char/93 NE3	*	6629.1	5721.1	6.0	*
24. Char/93 NE4	*	6699.8	5695.9	6.0	*
25. Char/93 NE5	*	6750.6	5633.2	6.0	*
26. Char/93 S1	*	6657.8	5466.0	6.0	*
27. Char/93 S2	*	6614.7	5527.4	6.0	*
28. Char/93 S3	*	6571.7	5588.8	6.0	*
29. Char/93 S4	*	6512.9	5542.2	6.0	*
30. Char/93 S5	*	6454.1	5495.6	6.0	*
31. Char/93 NW1	*	6424.1	5632.5	6.0	*
32. Char/93 NW2	*	6483.6	5678.2	6.0	*
33. Char/93 NW3	*	6543.0	5723.9	6.0	*
34. Char/93 NW4	*	6541.0	5798.8	6.0	*

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JOB: Government Center Garage RUN: No Build

DATE : 7/10/13
TIME : 15:35:44

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
35. Char/93 NW5	*	6538.9	5873.8	6.0	*

♀ PAGE 4

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE * CONCENTRATION (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	0.0	0.0	0.0	0.0	0.0	0.5	0.6	0.5	0.3	0.1	0.3	0.6	0.5	0.6	0.8	0.2	0.3	0.4	0.6	0.9
10. *	0.0	0.0	0.0	0.0	0.0	0.3	0.6	0.4	0.3	0.1	0.3	0.6	0.4	0.5	0.8	0.2	0.2	0.2	0.6	0.9
20. *	0.0	0.0	0.0	0.0	0.0	0.4	0.7	0.6	0.2	0.1	0.3	0.6	0.5	0.3	0.4	0.3	0.3	0.3	0.4	0.8
30. *	0.0	0.0	0.0	0.0	0.0	0.4	0.5	0.6	0.1	0.0	0.2	0.5	0.4	0.3	0.3	0.4	0.3	0.4	0.3	0.8
40. *	0.0	0.0	0.1	0.1	0.0	0.3	0.4	0.5	0.1	0.0	0.2	0.3	0.4	0.2	0.2	0.6	0.4	0.5	0.4	0.8
50. *	0.0	0.0	0.3	0.2	0.1	0.2	0.2	0.3	0.0	0.0	0.3	0.4	0.5	0.2	0.1	0.7	0.4	0.5	0.8	0.7
60. *	0.0	0.0	0.6	0.4	0.2	0.1	0.1	0.1	0.0	0.0	0.3	0.3	0.6	0.2	0.1	0.7	0.3	0.2	0.7	0.8
70. *	0.0	0.1	0.8	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.2	0.1	0.9	0.5	0.1	0.7	0.8
80. *	0.0	0.1	0.8	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.2	0.1	0.8	0.6	0.1	0.6	0.8
90. *	0.1	0.3	0.7	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.1	0.1	0.8	0.6	0.2	0.4	0.8
100. *	0.1	0.4	0.6	0.6	0.4	0.0	0.0	0.1	0.1	0.1	0.3	0.3	0.3	0.1	0.0	0.8	0.6	0.4	0.3	0.6
110. *	0.1	0.4	0.4	0.7	0.4	0.0	0.0	0.3	0.2	0.2	0.2	0.2	0.2	0.0	0.0	0.7	0.7	0.5	0.3	0.5
120. *	0.2	0.4	0.4	0.7	0.4	0.0	0.1	0.5	0.4	0.3	0.1	0.1	0.1	0.0	0.0	0.7	0.6	0.5	0.4	0.5
130. *	0.2	0.4	0.4	0.8	0.5	0.1	0.1	0.5	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.4	0.4	0.4
140. *	0.3	0.4	0.4	0.9	0.5	0.1	0.2	0.5	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.3	0.1	0.3
150. *	0.4	0.5	0.6	0.9	0.6	0.1	0.3	0.4	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.4		

0.2	0.3																		
160.	*	0.5	0.5	0.6	0.9	0.6	0.1	0.3	0.2	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.7	0.8	0.5
0.3	0.2																		
170.	*	0.7	0.6	0.6	1.0	0.6	0.1	0.2	0.3	0.8	0.3	0.0	0.0	0.0	0.0	0.0	0.6	0.8	0.7
0.4	0.3																		
180.	*	0.9	0.8	0.9	0.9	0.7	0.2	0.2	0.6	0.7	0.2	0.0	0.0	0.1	0.1	0.1	0.6	0.7	0.7
0.4	0.3																		
190.	*	0.9	0.7	0.8	1.1	0.7	0.2	0.4	0.6	0.8	0.2	0.0	0.0	0.3	0.3	0.3	0.4	0.5	0.6
0.4	0.2																		
200.	*	0.6	0.4	0.8	1.0	1.1	0.4	0.5	0.8	0.9	0.5	0.0	0.1	0.7	0.5	0.5	0.2	0.3	0.4
0.1	0.0																		
210.	*	0.6	0.5	0.6	0.7	0.9	0.4	0.5	0.5	0.8	0.6	0.1	0.2	0.9	0.7	0.6	0.1	0.1	0.1
0.0	0.0																		
220.	*	0.6	0.5	0.4	0.4	0.7	0.3	0.4	0.3	0.8	0.8	0.1	0.2	0.9	0.9	0.6	0.0	0.0	0.0
0.0	0.0																		
230.	*	0.6	0.6	0.4	0.3	0.5	0.2	0.1	0.1	0.7	0.8	0.2	0.4	1.0	1.0	0.6	0.0	0.0	0.0
0.0	0.0																		
240.	*	0.6	0.6	0.3	0.3	0.3	0.2	0.1	0.1	0.5	1.1	0.2	0.5	0.7	0.9	0.6	0.0	0.0	0.0
0.0	0.0																		
250.	*	0.5	0.6	0.3	0.3	0.2	0.4	0.2	0.0	0.3	1.0	0.3	0.5	0.7	0.9	0.6	0.0	0.0	0.0
0.0	0.0																		
260.	*	0.4	0.6	0.4	0.3	0.2	0.4	0.3	0.0	0.3	0.8	0.3	0.5	0.5	0.8	0.7	0.0	0.0	0.0
0.0	0.0																		
270.	*	0.3	0.6	0.5	0.4	0.2	0.6	0.4	0.0	0.2	0.6	0.2	0.4	0.4	0.8	0.8	0.0	0.0	0.0
0.0	0.0																		
280.	*	0.4	0.7	0.7	0.3	0.1	0.7	0.5	0.0	0.1	0.4	0.2	0.3	0.3	0.8	0.8	0.0	0.0	0.0
0.0	0.0																		
290.	*	0.4	0.6	0.7	0.3	0.1	0.8	0.7	0.1	0.2	0.3	0.2	0.3	0.3	0.8	0.8	0.0	0.0	0.0
0.0	0.0																		
300.	*	0.4	0.5	0.6	0.2	0.1	0.9	0.7	0.2	0.1	0.2	0.3	0.2	0.3	0.8	0.8	0.0	0.0	0.0
0.0	0.0																		
310.	*	0.4	0.4	0.6	0.1	0.0	0.7	0.8	0.4	0.4	0.4	0.5	0.4	0.4	0.8	0.9	0.0	0.0	0.0
0.1	0.1																		
320.	*	0.3	0.3	0.3	0.0	0.0	0.7	0.6	0.6	0.5	0.3	0.5	0.3	0.4	0.8	0.9	0.0	0.0	0.0
0.3	0.2																		
330.	*	0.1	0.2	0.2	0.0	0.0	0.6	0.5	0.7	0.4	0.2	0.7	0.8	0.6	0.9	0.9	0.0	0.0	0.2
0.5	0.5																		
340.	*	0.1	0.1	0.1	0.0	0.0	0.6	0.4	0.7	0.3	0.2	0.6	0.8	0.6	0.9	1.1	0.1	0.1	0.3
0.8	0.7																		
350.	*	0.0	0.0	0.0	0.0	0.0	0.5	0.5	0.5	0.3	0.2	0.5	0.7	0.6	0.8	1.0	0.1	0.3	0.4
0.7	0.9																		
360.	*	0.0	0.0	0.0	0.0	0.0	0.5	0.6	0.5	0.3	0.1	0.3	0.6	0.5	0.6	0.8	0.2	0.3	0.4
0.6	0.9																		

MAX	*	0.9	0.8	0.9	1.1	1.1	0.9	0.8	0.8	0.9	1.1	0.7	0.8	1.0	1.0	1.1	0.9	0.8	0.7
0.8	0.9																		
DEGR.	*	180	180	180	190	200	300	310	200	200	240	330	330	230	230	340	70	160	170
50	0																		

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35
0.	* 0.1	0.3	0.4	0.0	0.0	0.4	0.5	0.9	1.0	0.4	0.0	0.0	0.6	0.3	0.1
10.	* 0.0	0.1	0.2	0.0	0.0	0.2	0.4	0.7	1.2	0.8	0.0	0.2	1.0	0.7	0.1
20.	* 0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	1.1	1.0	0.2	0.4	1.2	1.0	0.3
30.	* 0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.4	0.9	0.8	0.3	0.5	1.2	1.2	0.6
40.	* 0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.3	0.5	0.6	0.4	0.6	1.2	1.2	0.7
50.	* 0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.2	0.3	0.4	0.3	0.5	1.0	1.2	0.9
60.	* 0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.3	0.3	0.3	0.9	1.2	1.0
70.	* 0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.4	0.1	0.1	0.1	0.3	0.7	1.1	1.0
80.	* 0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.4	0.1	0.1	0.4	0.1	0.4	1.1	1.2
90.	* 0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.1	0.4	0.2	0.2	1.2	1.2
100.	* 0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.1	0.5	0.2	0.1	1.1	1.1
110.	* 0.0	0.0	0.1	0.0	0.0	0.2	0.3	0.3	0.1	0.0	0.6	0.4	0.1	1.1	1.1
120.	* 0.0	0.0	0.1	0.0	0.0	0.2	0.2	0.3	0.0	0.0	0.6	0.5	0.1	1.1	1.2
130.	* 0.0	0.0	0.2	0.0	0.0	0.1	0.2	0.2	0.0	0.0	0.4	0.5	0.2	1.1	1.3
140.	* 0.0	0.0	0.3	0.2	0.0	0.0	0.1	0.1	0.0	0.0	0.4	0.5	0.4	1.0	1.4
150.	* 0.0	0.2	0.4	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.3	0.8	1.3
160.	* 0.1	0.2	0.3	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.2	0.5	0.4	0.5	1.1
170.	* 0.3	0.1	0.2	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.3	0.5	0.8
180.	* 0.5	0.2	0.2	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.4	0.4	0.5
190.	* 1.0	0.5	0.2	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.4	0.3	0.3
200.	* 1.3	0.8	0.4	0.2	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.4	0.3	0.0
210.	* 1.5	1.0	0.4	0.2	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.1	0.0
220.	* 1.3	1.3	0.6	0.2	0.4	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.0	

230.	*	1.2	1.2	0.5	0.4	0.5	0.0	0.0	0.2	0.1	0.0	0.0	0.1	0.1	0.0	0.0
240.	*	1.2	1.1	0.3	0.4	0.5	0.0	0.0	0.4	0.1	0.0	0.0	0.0	0.0	0.0	0.0
250.	*	1.1	1.1	0.1	0.5	0.7	0.0	0.0	0.6	0.2	0.0	0.0	0.0	0.0	0.0	0.0
260.	*	1.1	1.1	0.1	0.4	0.7	0.0	0.1	0.8	0.2	0.1	0.0	0.0	0.0	0.0	0.0
270.	*	1.2	1.2	0.1	0.1	0.7	0.0	0.2	1.0	0.4	0.1	0.0	0.0	0.0	0.0	0.0
280.	*	1.1	1.1	0.4	0.3	0.5	0.0	0.2	1.0	0.4	0.1	0.0	0.0	0.0	0.0	0.0
290.	*	1.1	1.1	0.6	0.4	0.5	0.2	0.3	0.9	0.5	0.1	0.0	0.0	0.0	0.0	0.0
300.	*	1.1	1.2	0.8	0.5	0.4	0.2	0.3	0.8	0.6	0.2	0.0	0.0	0.0	0.0	0.0
310.	*	1.0	1.3	1.0	0.5	0.4	0.2	0.3	0.8	0.7	0.2	0.0	0.0	0.0	0.0	0.0
320.	*	0.7	1.3	1.2	0.6	0.4	0.2	0.3	0.8	0.8	0.3	0.0	0.0	0.0	0.0	0.0
330.	*	0.6	1.2	1.3	0.5	0.3	0.4	0.2	0.7	0.8	0.3	0.0	0.0	0.0	0.0	0.0
340.	*	0.3	0.9	1.2	0.2	0.2	0.4	0.6	0.8	0.8	0.3	0.0	0.0	0.0	0.0	0.0
350.	*	0.1	0.6	0.9	0.0	0.0	0.5	0.5	0.7	0.8	0.3	0.0	0.0	0.2	0.1	0.0
360.	*	0.1	0.3	0.4	0.0	0.0	0.4	0.5	0.9	1.0	0.4	0.0	0.0	0.6	0.3	0.1

MAX	*	1.5	1.3	1.3	0.6	0.7	0.5	0.6	1.0	1.2	1.0	0.6	0.6	1.2	1.2	1.4
DEGR.	*	210	220	330	320	250	350	340	270	10	20	110	40	20	30	140

THE HIGHEST CONCENTRATION OF 1.50 PPM OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:13:52

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6049.9	5447.4	*	66.	290.	AG	275.	100.0	1.0	30.0	0.52	3.3
2.	Char/Merr WB	*	6250.4	5435.2	6333.8	5501.2	*	106.	52.	AG	275.	100.0	1.0	30.0	0.77	5.4
3.	Char/Merr NB R	*	6291.7	5369.7	6315.3	5353.7	*	29.	124.	AG	54.	100.0	1.0	10.0	0.14	1.5
4.	Char/Merr NB LTT	*	6280.4	5347.2	6430.5	5241.4	*	184.	125.	AG	171.	100.0	1.0	20.0	0.92	9.3
5.	Char/Merr EB	*	6104.2	5362.2	6060.5	5345.9	*	47.	250.	AG	191.	100.0	1.0	20.0	0.42	2.4
6.	Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.5	*	108.	14.	AG	78.	100.0	1.0	10.0	0.71	5.5
7.	Char/Cam SB TR	*	5360.8	4833.5	5398.9	4956.5	*	129.	17.	AG	190.	100.0	1.0	20.0	0.92	6.5
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	145.	100.0	1.0	20.0	0.27	2.2
9.	Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	78.	100.0	1.0	10.0	0.60	4.7
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.4	4650.0	*	74.	179.	AG	190.	100.0	1.0	20.0	0.71	3.7
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5214.1	4740.7	*	89.	271.	AG	217.	100.0	1.0	30.0	0.54	4.5
12.	Sud/Merr SB L	*	6532.7	5210.3	6487.5	5242.5	*	56.	305.	AG	104.	100.0	1.0	10.0	0.72	2.8
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6477.9	5214.2	*	47.	300.	AG	177.	100.0	1.0	30.0	0.24	2.4
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6673.5	5068.9	*	106.	150.	AG	228.	100.0	1.0	30.0	0.60	5.4
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6478.2	5118.7	*	53.	239.	AG	352.	100.0	1.0	40.0	0.38	2.7
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	128.	100.0	1.0	20.0	0.34	3.3
17.	Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	84.	100.0	1.0	10.0	0.06	0.5
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6745.9	5240.5	*	52.	249.	AG	279.	100.0	1.0	30.0	0.43	2.7
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	877.	8.3	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1122.	8.3	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1326.	8.3	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	939.	8.3	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	849.	8.3	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1614.	8.3	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	950.	8.3	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1709.	8.3	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	318.	8.3	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	536.	8.3	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	8.3	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	373.	8.3	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	8.3	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1555.	8.3	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1648.	8.3	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	529.	8.3	1.0	78.0		

JOB: Government Center Garage RUN: 2028NB

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ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Char/Merr SB	*	100	76	3.0	476	1600	44.99	1	3
2.	Char/Merr WB	*	100	76	3.0	703	1600	44.99	1	3
3.	Char/Merr NB R	*	100	45	3.0	116	1600	44.99	1	3
4.	Char/Merr NB LTT	*	100	71	3.0	709	1600	44.99	1	3

5. Char/Merr EB	*	100	79	3.0	217	1600	44.99	1	3
6. Char/Cam SB L	*	90	58	3.0	339	1600	44.99	1	3
7. Char/Cam SB TR	*	90	71	3.0	457	1600	44.99	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	294	1600	44.99	1	3
9. Char/Cam NB L	*	90	58	3.0	289	1600	44.99	1	3
10. Char/Cam NB TR	*	90	71	3.0	354	1600	44.99	1	3
11. Char/Cam EB TTTR	*	90	54	3.0	901	1600	44.99	1	3
12. Sud/Merr SB L	*	100	86	3.0	104	1600	44.99	1	3
13. Sud/Merr SB TTT	*	100	49	3.0	524	1600	44.99	1	3
14. Sud/Merr NB TTTR	*	100	63	3.0	924	1600	44.99	1	3
15. Sud/Merr EB LTTR	*	100	73	3.0	529	1600	44.99	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	455	1600	44.99	1	3
17. Sud/Sur SEB	*	100	70	3.0	26	1600	44.99	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	373	1600	44.99	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Char/Merr NE1	*	6063.7	5511.0	6.0
2.	Char/Merr NE2	*	6133.9	5484.8	6.0
3.	Char/Merr NE3	*	6204.2	5458.5	6.0
4.	Char/Merr NE4	*	6265.6	5501.5	6.0
5.	Char/Merr NE5	*	6327.1	5544.5	6.0
6.	Char/Merr SE1	*	6443.7	5491.9	6.0
7.	Char/Merr SE2	*	6382.2	5448.9	6.0
8.	Char/Merr SE3	*	6320.8	5405.9	6.0
9.	Char/Merr SE4	*	6380.5	5360.4	6.0
10.	Char/Merr SE5	*	6440.1	5315.0	6.0
11.	Char/Merr SW1	*	6332.0	5249.0	6.0
12.	Char/Merr SW2	*	6272.3	5294.5	6.0
13.	Char/Merr SW3	*	6212.6	5339.9	6.0
14.	Char/Merr SW4	*	6141.6	5315.8	6.0
15.	Char/Merr SW5	*	6070.6	5291.7	6.0
16.	Char/Merr NW1	*	5902.1	5359.1	6.0
17.	Char/Merr NW2	*	5973.1	5383.2	6.0
18.	Char/Merr NW3	*	6044.1	5407.3	6.0
19.	Char/Merr NW4	*	5973.9	5433.5	6.0
20.	Char/Merr NW5	*	5903.6	5459.8	6.0
21.	Char/Cam NE1	*	5490.2	4963.0	6.0
22.	Char/Cam NE2	*	5459.0	4894.8	6.0
23.	Char/Cam NE3	*	5427.8	4826.6	6.0
24.	Char/Cam NE4	*	5500.4	4807.6	6.0
25.	Char/Cam NE5	*	5572.9	4788.7	6.0
26.	Char/Cam SE1	*	5553.9	4667.5	6.0
27.	Char/Cam SE2	*	5481.3	4686.5	6.0

JOB: Government Center Garage RUN: 2028NB

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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
28.	Char/Cam SE3	*	5408.7	4705.4	6.0
29.	Char/Cam SE4	*	5409.4	4630.4	6.0
30.	Char/Cam SE5	*	5410.1	4555.4	6.0
31.	Char/Cam SW1	*	5312.0	4561.9	6.0
32.	Char/Cam SW2	*	5310.7	4636.9	6.0
33.	Char/Cam SW3	*	5310.7	4711.9	6.0
34.	Char/Cam SW4	*	5235.6	4712.1	6.0
35.	Char/Cam SW5	*	5160.6	4711.9	6.0
36.	Char/Cam NW1	*	5167.9	4822.4	6.0
37.	Char/Cam NW2	*	5242.9	4822.1	6.0
38.	Char/Cam NW3	*	5317.9	4821.9	6.0
39.	Char/Cam NW4	*	5349.1	4890.1	6.0
40.	Char/Cam NW5	*	5380.3	4958.3	6.0

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) *	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

0.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.1	0.8	0.7	0.5	0.4	0.7	0.1	0.1	0.4	0.2	0.2
10.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.1	0.1	0.8	0.9	0.5	0.3	0.7	0.1	0.1	0.5	0.2	0.2
20.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.1	0.1	0.6	0.7	0.6	0.4	0.6	0.1	0.1	0.7	0.2	0.2
30.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.0	0.7	0.8	0.9	0.5	0.4	0.1	0.1	0.7	0.2	0.2
40.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.0	0.6	0.7	0.8	0.6	0.6	0.1	0.2	0.8	0.2	0.2
50.	*	0.0	0.0	0.2	0.1	0.1	0.1	0.2	0.2	0.0	0.0	0.6	0.5	0.7	0.6	0.5	0.2	0.3	0.8	0.2	0.2
60.	*	0.0	0.0	0.4	0.2	0.2	0.1	0.1	0.1	0.0	0.0	0.6	0.5	0.5	0.6	0.4	0.2	0.4	1.0	0.3	0.2
70.	*	0.0	0.2	0.7	0.4	0.3	0.0	0.0	0.0	0.0	0.1	0.6	0.6	0.5	0.4	0.3	0.5	0.6	1.0	0.6	0.2
80.	*	0.1	0.2	0.8	0.5	0.3	0.0	0.0	0.0	0.0	0.1	0.7	0.7	0.4	0.3	0.2	0.6	0.7	0.9	0.7	0.5
90.	*	0.2	0.4	0.8	0.7	0.3	0.0	0.0	0.0	0.0	0.1	0.5	0.7	0.5	0.3	0.2	0.4	0.7	0.9	0.9	0.5
100.	*	0.2	0.4	0.9	0.8	0.3	0.0	0.0	0.0	0.0	0.1	0.6	0.6	0.7	0.3	0.3	0.5	0.5	0.7	0.7	0.6
110.	*	0.4	0.4	0.6	0.8	0.2	0.0	0.0	0.0	0.1	0.2	0.7	0.6	0.8	0.4	0.1	0.2	0.5	0.6	0.6	0.4
120.	*	0.5	0.7	0.8	0.8	0.2	0.0	0.0	0.3	0.3	0.6	0.5	0.5	0.6	0.1	0.1	0.2	0.4	0.6	0.4	0.2
130.	*	0.8	0.7	0.9	1.0	0.2	0.0	0.1	0.3	0.5	0.7	0.2	0.3	0.4	0.0	0.0	0.2	0.2	0.4	0.2	0.1
140.	*	0.5	0.6	0.9	1.2	0.4	0.1	0.3	0.6	0.7	0.9	0.2	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.2	0.1
150.	*	0.6	0.5	0.6	1.2	0.5	0.2	0.2	0.8	0.7	0.9	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1
160.	*	0.6	0.3	0.5	1.1	0.7	0.2	0.5	0.5	0.6	0.7	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1
170.	*	0.8	0.3	0.5	1.1	0.7	0.3	0.3	0.5	0.5	0.5	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.1	0.1
180.	*	0.7	0.3	0.4	1.0	0.8	0.1	0.2	0.5	0.4	0.5	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1	0.1
190.	*	0.6	0.5	0.4	0.8	1.1	0.3	0.3	0.5	0.4	0.5	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1	0.1
200.	*	0.4	0.6	0.4	0.6	1.0	0.2	0.3	0.4	0.4	0.5	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1	0.1
210.	*	0.4	0.7	0.5	0.5	0.9	0.2	0.3	0.4	0.5	0.5	0.0	0.0	0.0	0.0	0.0	0.3	0.2	0.2	0.1	0.0
220.	*	0.3	0.7	0.6	0.4	0.8	0.2	0.3	0.4	0.5	0.5	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.1	0.0
230.	*	0.3	0.7	0.5	0.3	0.6	0.3	0.4	0.3	0.5	0.5	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.1	0.0
240.	*	0.2	0.6	0.6	0.3	0.5	0.5	0.4	0.4	0.4	0.5	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.0	0.0
250.	*	0.2	0.4	0.6	0.3	0.3	0.7	0.5	0.4	0.5	0.6	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0
260.	*	0.2	0.3	0.5	0.2	0.1	0.8	0.9	0.7	0.5	0.7	0.0	0.1	0.3	0.2	0.2	0.0	0.0	0.1	0.0	0.0
270.	*	0.2	0.2	0.4	0.1	0.1	0.6	0.9	0.7	0.5	0.7	0.1	0.1	0.4	0.2	0.2	0.0	0.0	0.0	0.0	0.0
280.	*	0.2	0.2	0.3	0.1	0.0	0.5	0.8	0.8	0.7	0.7	0.1	0.1	0.3	0.3	0.2	0.0	0.0	0.0	0.0	0.0
290.	*	0.1	0.1	0.1	0.0	0.0	0.3	0.6	0.7	0.6	0.6	0.1	0.3	0.5	0.4	0.2	0.0	0.0	0.1	0.1	0.0
300.	*	0.0	0.1	0.1	0.0	0.0	0.2	0.6	0.7	0.5	0.5	0.4	0.3	0.5	0.5	0.2	0.0	0.0	0.2	0.1	0.1
310.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.5	0.6	0.4	0.3	0.5	0.4	0.6	0.6	0.2	0.0	0.0	0.2	0.2	0.1
320.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.6	0.3	0.2	0.5	0.6	0.6	0.5	0.3	0.0	0.1	0.2	0.2	0.1
330.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.6	0.3	0.2	0.7	0.4	0.4	0.6	0.3	0.0	0.1	0.2	0.2	0.2
340.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.6	0.3	0.1	0.7	0.4	0.4	0.5	0.5	0.0	0.1	0.2	0.2	0.2
350.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.6	0.2	0.1	0.8	0.5	0.4	0.4	0.6	0.1	0.1	0.3	0.2	0.2
360.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.1	0.8	0.7	0.5	0.4	0.7	0.1	0.1	0.4	0.2	0.2
MAX	*	0.8	0.7	0.9	1.2	1.1	0.8	0.9	0.8	0.7	0.9	0.8	0.9	0.9	0.6	0.7	0.6	0.7	1.0	0.9	0.6
DEGR.	*	130	120	130	140	190	260	260	150	140	140	0	10	30	40	0	80	80	60	90	100

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	*	0.1	0.2	0.3	0.0	0.0	0.3	0.3	0.6	0.6	0.5	0.3	0.5	0.6	1.0	0.4	0.0	0.0	0.0	0.0	0.0
10.	*	0.1	0.1	0.2	0.0	0.0	0.3	0.3	0.6	0.3	0.2	0.6	0.6	0.6	0.9	0.3	0.0	0.0	0.0	0.0	0.0
20.	*	0.0	0.1	0.1	0.0	0.0	0.3	0.3	0.5	0.2	0.1	0.8	0.6	0.8	0.9	0.3	0.0	0.0	0.2	0.2	0.0
30.	*	0.0	0.0	0.1	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.5	0.9	0.9	1.1	0.3	0.0	0.0	0.5	0.3	0.1
40.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.1	0.4	0.6	0.7	1.3	0.6	0.0	0.1	0.7	0.6	0.1
50.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.1	0.4	0.7	0.8	1.3	0.8	0.0	0.2	0.7	0.8	0.2
60.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.7	0.8	1.1	1.0	0.2	0.3	0.6	0.8	0.2
70.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.7	0.7	1.0	0.8	0.2	0.3	0.6	0.8	0.3
80.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.6	0.8	0.8	0.8	0.4	0.3	0.5	0.8	0.3
90.	*	0.0	0.0	0.1	0.1	0.0	0.3	0.4	0.4	0.1	0.0	0.2	0.5	0.8	0.6	0.8	0.5	0.5	0.6	0.8	0.4
100.	*	0.0	0.0	0.2	0.1	0.1	0.2	0.3	0.3	0.0	0.0	0.2	0.2	0.7	0.4	0.5	0.5	0.6	0.8	0.7	0.5
110.	*	0.0	0.0	0.3	0.3	0.2	0.1	0.1	0.2	0.0	0.0	0.2	0.2	0.6	0.2	0.1	0.7	0.7	0.9	0.8	0.6
120.	*	0.0	0.1	0.4	0.4	0.3	0.0	0.0	0.1	0.0	0.0	0.2	0.2	0.5	0.1	0.1	0.9	0.7	0.9	0.9	0.9
130.	*	0.1	0.2	0.4	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.7	0.8	0.8	1.2	0.9
140.	*	0.1	0.2	0.5	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.7	0.8	0.8	1.1	1.1
150.	*	0.1	0.2	0.6	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.0	0.6	0.6	0.8	1.0	1.1
160.	*	0.1	0.2	0.5	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.1	0.0	0.4	0.7	0.9	1.0	1.2
170.	*	0.1	0.2	0.6	0.3	0.3	0.0	0.0	0.1	0.1	0.0	0.2	0.2	0.2	0.0	0.0	0.3	0.7	0.7	1.0	1.3
180.	*	0.1	0.3	0.8	0.3	0.3	0.0	0.0	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.4	0.7	0.8	0.8	1.4
190.	*	0.2	0.5	0.7	0.3	0.3	0.0	0.0	0.4	0.2	0.2	0.0	0.0	0.1	0.0	0.0	0.3	0.5	0.5	0.7	1.0
200.	*	0.3	0.6	0.8	0.4	0.3	0.0	0.1	0.6	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.5	0.4	0.7
210.	*	0.4	0.7	0.8	0.5	0.4	0.0	0.1	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.7	0.3	0.4
220.	*	0.7	0.6	0.7	0.5	0.4	0.1	0.1	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.7	0.3	0.3
230.	*	0.7	0.8	0.8	0.6	0.5	0.1	0.1	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.3	0.1
240.	*	0.6	0.9	0.8	0.8	0.6	0.1	0.2	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.2	0.1
250.	*	0.5	0.7	0.8	0.9	0.7	0.1	0.2	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.4	0.1	0.1
260.	*	0.3	0.6	0.8	0.8	0.7	0.2	0.3	1.0	0.2	0.2	0.0	0.0	0.2	0.1	0.1	0.3	0.3	0.4	0.1	0.0
270.	*	0.3	0.5	0.6	0.7	0.6	0.3	0.6	1.1	0.2	0.2	0.0	0.0	0.4	0.2	0.1	0.2	0.2	0.2	0.0	0.0
280.	*	0.2	0.5	0.7	0.5	0.5	0.5	0.7	1.3	0.4	0.2	0.0	0.0	0.8	0.3	0.2	0.1	0.1	0.1	0.0	0.0
290.	*	0.2	0.5	0.5	0.3	0.3	0.7	0.7	1.4	0.6	0.2	0.0	0.1	1.0	0.5	0.3	0.0	0.0	0.0	0.0	0.0
300.	*	0.2	0.5	0.5	0.3	0.2	0.4	0.8	1.1	0.8	0.3	0.1	0.2	1.0	0.5	0.4	0.0	0.0	0.0	0.0	0.0
310.	*	0.2	0.5	0.6	0.3	0.2	0.7	0.5	0.9	0.9	0.4	0.1	0.3	1.0	0.6	0.4	0.0	0.0	0.0	0.0	0.0
320.	*	0.2	0.3	0.6	0.2	0.1	0.6	0.7	0.7	1.0	0.4	0.1	0.4	0.9	0.7	0.4	0.0	0.0	0.0	0.0	0.0
330.	*	0.1	0.2	0.6	0.2	0.1	0.6	0.6	0.8	0.9	0.6	0.2	0.4	0.9	0.7	0.3	0.0	0.0	0.0	0.0	0.0
340.	*	0.1	0.2	0.5	0.1	0.0	0.4	0.6	0.7	1.0	0.6	0.2	0.4	0.6	0.8	0.3	0.0	0.0	0.0	0.0	0.0
350.	*	0.1	0.2	0.4	0.1	0.0	0.3	0.6	0.6	0.9	0.7	0.2	0.4	0.5	0.8	0.3	0.0	0.0	0.0	0.0	0.0
360.	*	0.1	0.2	0.3	0.0	0.0	0.3	0.3	0.6	0.6	0.5	0.3	0.5	0.6	1.0	0.4	0.0	0.0	0.0	0.0	0.0
MAX	*	0.7	0.9	0.8	0.9	0.7	0.7	0.8	1.4	1.0	0.7	0.8	0.9	1.0	1.3	1.0	0.9	0.8	0.9	1.2	1.4

NB_3a

DEGR. * 220 240 180 250 250 310 300 290 320 350 20 30 290 40 60 120 130 110
130 180

THE HIGHEST CONCENTRATION OF 1.40 PPM OCCURRED AT RECEPTOR REC40.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:13:46

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6036.0	5452.4	*	80.	290.	AG	272.	100.0	1.0	30.0	0.61
2. Char/Merr WB	*	6250.4	5435.2	6303.9	5477.6	*	68.	52.	AG	282.	100.0	1.0	30.0	0.59
3. Char/Merr NB R	*	6291.7	5369.7	6345.2	5333.4	*	65.	124.	AG	56.	100.0	1.0	10.0	0.33
4. Char/Merr NB LTT	*	6280.4	5347.2	6359.4	5291.5	*	97.	125.	AG	164.	100.0	1.0	20.0	0.60
5. Char/Merr EB	*	6104.2	5362.2	5973.2	5313.5	*	140.	250.	AG	191.	100.0	1.0	20.0	0.91
6. Char/Cam SB L	*	5384.1	4834.2	5402.3	4907.1	*	75.	14.	AG	72.	100.0	1.0	10.0	0.41
7. Char/Cam SB TR	*	5360.8	4833.5	5375.6	4881.2	*	50.	17.	AG	174.	100.0	1.0	20.0	0.35
8. Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	150.	100.0	1.0	20.0	0.41
9. Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	72.	100.0	1.0	10.0	0.53
10. Char/Cam NB TR	*	5383.3	4723.8	5384.9	4614.7	*	109.	179.	AG	174.	100.0	1.0	20.0	0.73
11. Char/Cam EB TTTR	*	5302.7	4739.8	5211.5	4740.8	*	91.	271.	AG	224.	100.0	1.0	30.0	0.51
12. Sud/Merr SB L	*	6532.7	5210.3	6492.2	5239.1	*	50.	305.	AG	101.	100.0	1.0	10.0	0.60
13. Sud/Merr SB TTT	*	6518.3	5190.8	6484.0	5210.7	*	40.	300.	AG	181.	100.0	1.0	30.0	0.20
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6677.8	5061.4	*	115.	150.	AG	239.	100.0	1.0	30.0	0.69
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6452.9	5103.5	*	82.	239.	AG	348.	100.0	1.0	40.0	0.57
16. Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	169.	100.0	1.0	20.0	0.53
17. Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	97.	100.0	1.0	10.0	0.15
18. Sud/Sur EB TTR	*	6794.5	5259.6	6715.8	5228.7	*	84.	249.	AG	181.	100.0	1.0	30.0	0.43
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	921.	8.3	1.0	84.0	
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1336.	8.3	1.0	90.0	
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1354.	8.3	1.0	98.0	
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	940.	8.3	1.0	98.0	
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	863.	8.3	1.0	78.0	
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1593.	8.3	1.0	****	
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1023.	8.3	1.0	78.0	
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1636.	8.3	1.0	90.0	
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	901.	8.3	1.0	30.0	
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	488.	8.3	1.0	54.0	
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	8.3	1.0	42.0	
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	928.	8.3	1.0	54.0	
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	8.3	1.0	42.0	
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1317.	8.3	1.0	98.0	
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1611.	8.3	1.0	90.0	
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	837.	8.3	1.0	78.0	

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:13:46

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. Char/Merr SB	*	100	75	3.0	589	1600	44.99	1	3
2. Char/Merr WB	*	100	78	3.0	481	1600	44.99	1	3
3. Char/Merr NB R	*	100	46	3.0	257	1600	44.99	1	3
4. Char/Merr NB LTT	*	100	68	3.0	520	1600	44.99	1	3
5. Char/Merr EB	*	100	79	3.0	468	1600	44.99	1	3
6. Char/Cam SB L	*	100	60	3.0	229	1600	44.99	1	3
7. Char/Cam SB TR	*	100	72	3.0	254	1600	44.99	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	435	1600	44.99	1	3
9. Char/Cam NB L	*	100	60	3.0	299	1600	44.99	1	3
10. Char/Cam NB TR	*	100	72	3.0	536	1600	44.99	1	3
11. Char/Cam EB TTTR	*	100	62	3.0	809	1600	44.99	1	3
12. Sud/Merr SB L	*	100	84	3.0	106	1600	44.99	1	3
13. Sud/Merr SB TTT	*	100	50	3.0	435	1600	44.99	1	3
14. Sud/Merr NB TTTR	*	100	66	3.0	954	1600	44.99	1	3
15. Sud/Merr EB LTTR	*	100	72	3.0	837	1600	44.99	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	424	1600	44.99	1	3
17. Sud/Sur SEB	*	100	80	3.0	37	1600	44.99	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	928	1600	44.99	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Char/Merr NE1	*	6063.7	5511.0	6.0	*
2. Char/Merr NE2	*	6133.9	5484.8	6.0	*
3. Char/Merr NE3	*	6204.2	5458.5	6.0	*
4. Char/Merr NE4	*	6265.6	5501.5	6.0	*
5. Char/Merr NE5	*	6327.1	5544.5	6.0	*
6. Char/Merr SE1	*	6443.7	5491.9	6.0	*
7. Char/Merr SE2	*	6382.2	5448.9	6.0	*
8. Char/Merr SE3	*	6320.8	5405.9	6.0	*
9. Char/Merr SE4	*	6380.5	5360.4	6.0	*
10. Char/Merr SE5	*	6440.1	5315.0	6.0	*
11. Char/Merr SW1	*	6332.0	5249.0	6.0	*
12. Char/Merr SW2	*	6272.3	5294.5	6.0	*
13. Char/Merr SW3	*	6212.6	5339.9	6.0	*
14. Char/Merr SW4	*	6141.6	5315.8	6.0	*
15. Char/Merr SW5	*	6070.6	5291.7	6.0	*
16. Char/Merr NW1	*	5902.1	5359.1	6.0	*
17. Char/Merr NW2	*	5973.1	5383.2	6.0	*
18. Char/Merr NW3	*	6044.1	5407.3	6.0	*
19. Char/Merr NW4	*	5973.9	5433.5	6.0	*
20. Char/Merr NW5	*	5903.6	5459.8	6.0	*
21. Char/Cam NE1	*	5490.2	4963.0	6.0	*
22. Char/Cam NE2	*	5459.0	4894.8	6.0	*
23. Char/Cam NE3	*	5427.8	4826.6	6.0	*
24. Char/Cam NE4	*	5500.4	4807.6	6.0	*
25. Char/Cam NE5	*	5572.9	4788.7	6.0	*
26. Char/Cam SE1	*	5553.9	4667.5	6.0	*
27. Char/Cam SE2	*	5481.3	4686.5	6.0	*

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:13:46

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
28. Char/Cam SE3	*	5408.7	4705.4	6.0	*
29. Char/Cam SE4	*	5409.4	4630.4	6.0	*
30. Char/Cam SE5	*	5410.1	4555.4	6.0	*
31. Char/Cam SW1	*	5312.0	4561.9	6.0	*
32. Char/Cam SW2	*	5310.7	4636.9	6.0	*
33. Char/Cam SW3	*	5310.7	4711.9	6.0	*
34. Char/Cam SW4	*	5235.6	4712.1	6.0	*
35. Char/Cam SW5	*	5160.6	4711.9	6.0	*
36. Char/Cam NW1	*	5167.9	4822.4	6.0	*
37. Char/Cam NW2	*	5242.9	4822.1	6.0	*
38. Char/Cam NW3	*	5317.9	4821.9	6.0	*
39. Char/Cam NW4	*	5349.1	4890.1	6.0	*
40. Char/Cam NW5	*	5380.3	4958.3	6.0	*

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) *	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

0.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.8	0.8	0.5	0.4	0.8	0.1	0.1	0.6	0.2	0.2
10.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.1	0.7	0.8	0.5	0.3	0.8	0.1	0.1	0.7	0.2	0.2
20.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.1	0.6	0.7	0.7	0.4	0.6	0.1	0.1	0.8	0.2	0.2
30.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.1	0.0	0.6	0.8	0.8	0.5	0.4	0.1	0.2	0.8	0.2	0.2
40.	*	0.0	0.0	0.1	0.0	0.0	0.3	0.3	0.3	0.1	0.0	0.4	0.8	0.9	0.5	0.6	0.1	0.3	0.8	0.2	0.2
50.	*	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.0	0.0	0.3	0.7	0.7	0.6	0.7	0.2	0.3	0.8	0.3	0.2
60.	*	0.0	0.1	0.4	0.3	0.2	0.1	0.1	0.1	0.0	0.0	0.3	0.6	0.5	0.6	0.5	0.3	0.5	0.9	0.3	0.2
70.	*	0.1	0.1	0.6	0.3	0.3	0.0	0.0	0.0	0.0	0.1	0.3	0.6	0.5	0.4	0.3	0.4	0.6	1.1	0.6	0.2
80.	*	0.1	0.3	0.8	0.4	0.3	0.0	0.0	0.0	0.0	0.1	0.4	0.5	0.4	0.3	0.2	0.6	0.7	1.0	0.8	0.4
90.	*	0.2	0.3	0.8	0.3	0.3	0.0	0.0	0.0	0.0	0.1	0.3	0.6	0.5	0.3	0.2	0.6	0.7	0.9	1.0	0.5
100.	*	0.2	0.4	0.8	0.4	0.3	0.0	0.0	0.0	0.0	0.2	0.6	0.4	0.6	0.3	0.1	0.5	0.5	0.6	0.8	0.7
110.	*	0.4	0.6	0.7	0.5	0.3	0.0	0.0	0.0	0.1	0.3	0.6	0.5	0.7	0.4	0.2	0.4	0.5	0.5	0.5	0.5
120.	*	0.5	0.6	0.8	0.6	0.3	0.0	0.0	0.3	0.2	0.6	0.7	0.6	0.6	0.2	0.1	0.4	0.6	0.5	0.4	0.3
130.	*	0.7	0.6	1.0	0.9	0.3	0.0	0.1	0.4	0.5	0.7	0.4	0.4	0.3	0.0	0.0	0.3	0.5	0.4	0.3	0.2
140.	*	0.5	0.7	0.9	1.1	0.4	0.1	0.3	0.5	0.6	0.9	0.3	0.2	0.1	0.0	0.0	0.2	0.5	0.4	0.3	0.2
150.	*	0.6	0.5	0.7	1.3	0.5	0.2	0.3	0.7	0.7	0.9	0.2	0.1	0.0	0.0	0.0	0.2	0.5	0.5	0.3	0.2
160.	*	0.8	0.3	0.4	1.2	0.6	0.2	0.4	0.5	0.5	0.8	0.1	0.1	0.0	0.0	0.0	0.2	0.4	0.5	0.3	0.2
170.	*	0.8	0.3	0.5	1.2	0.5	0.3	0.3	0.6	0.5	0.6	0.1	0.0	0.0	0.0	0.0	0.2	0.4	0.5	0.2	0.1
180.	*	0.8	0.3	0.5	1.1	0.6	0.2	0.1	0.6	0.3	0.5	0.1	0.0	0.0	0.0	0.0	0.2	0.3	0.5	0.2	0.1
190.	*	0.8	0.5	0.4	0.9	0.7	0.1	0.3	0.6	0.4	0.5	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.5	0.1	0.1
200.	*	0.7	0.6	0.4	0.7	0.7	0.1	0.3	0.6	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.1
210.	*	0.6	0.8	0.5	0.6	0.7	0.2	0.3	0.5	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.3	0.2	0.4	0.1	0.0
220.	*	0.4	0.8	0.6	0.5	0.8	0.2	0.3	0.4	0.5	0.3	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.3	0.1	0.0
230.	*	0.3	0.8	0.6	0.4	0.6	0.2	0.4	0.4	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.1	0.0
240.	*	0.2	0.7	0.6	0.5	0.5	0.5	0.4	0.5	0.6	0.3	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.0	0.0
250.	*	0.2	0.5	0.7	0.3	0.3	0.6	0.7	0.7	0.6	0.5	0.0	0.0	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0
260.	*	0.2	0.4	0.6	0.2	0.2	0.8	1.0	0.8	0.7	0.6	0.0	0.1	0.3	0.3	0.2	0.0	0.0	0.1	0.0	0.0
270.	*	0.2	0.3	0.5	0.2	0.1	0.5	0.9	0.9	0.9	0.7	0.1	0.2	0.5	0.4	0.3	0.0	0.0	0.0	0.0	0.0
280.	*	0.2	0.2	0.3	0.1	0.0	0.4	0.7	1.0	0.7	0.7	0.2	0.2	0.4	0.5	0.4	0.0	0.0	0.0	0.0	0.0
290.	*	0.1	0.1	0.2	0.0	0.0	0.3	0.5	0.8	0.6	0.7	0.2	0.4	0.5	0.5	0.4	0.0	0.0	0.1	0.1	0.0
300.	*	0.0	0.1	0.1	0.0	0.0	0.3	0.4	0.8	0.6	0.5	0.5	0.4	0.6	0.6	0.5	0.0	0.0	0.2	0.1	0.1
310.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.8	0.5	0.3	0.5	0.4	0.6	0.6	0.5	0.0	0.0	0.2	0.2	0.1
320.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.7	0.4	0.2	0.5	0.6	0.6	0.6	0.6	0.0	0.1	0.2	0.2	0.1
330.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.7	0.3	0.1	0.7	0.4	0.4	0.6	0.6	0.0	0.1	0.3	0.2	0.2
340.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.2	0.1	0.7	0.4	0.4	0.5	0.7	0.0	0.1	0.4	0.2	0.2
350.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.2	0.1	0.8	0.6	0.5	0.4	0.8	0.1	0.1	0.5	0.2	0.2
360.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.8	0.8	0.5	0.4	0.8	0.1	0.1	0.6	0.2	0.2
MAX	*	0.8	0.8	1.0	1.3	0.8	0.8	1.0	1.0	0.9	0.9	0.8	0.8	0.9	0.6	0.8	0.6	0.7	1.1	1.0	0.7
DEGR.	*	160	210	130	150	220	260	260	280	270	140	0	0	40	50	0	80	80	70	90	100

angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	*	0.1	0.2	0.2	0.0	0.0	0.3	0.4	0.5	0.6	0.5	0.3	0.4	0.4	0.9	0.3	0.0	0.0	0.0	0.0	0.0
10.	*	0.1	0.1	0.2	0.0	0.0	0.3	0.3	0.5	0.4	0.2	0.6	0.5	0.7	0.9	0.3	0.0	0.0	0.0	0.0	0.0
20.	*	0.0	0.1	0.1	0.0	0.0	0.3	0.3	0.6	0.3	0.1	0.6	0.5	0.7	0.9	0.3	0.0	0.0	0.1	0.1	0.0
30.	*	0.0	0.0	0.1	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.7	0.8	0.9	1.0	0.3	0.0	0.0	0.3	0.1	0.1
40.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.6	0.7	0.6	1.3	0.5	0.0	0.0	0.4	0.2	0.1
50.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.1	0.4	0.8	0.9	1.2	0.7	0.0	0.1	0.5	0.2	0.2
60.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.4	0.7	0.8	1.2	0.9	0.1	0.2	0.6	0.2	0.2
70.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.7	0.8	1.1	0.9	0.1	0.2	0.6	0.2	0.2
80.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.7	0.7	0.8	0.9	0.3	0.3	0.5	0.3	0.2
90.	*	0.0	0.0	0.1	0.1	0.0	0.3	0.4	0.4	0.1	0.0	0.2	0.6	0.8	0.6	0.8	0.4	0.5	0.7	0.4	0.2
100.	*	0.0	0.0	0.2	0.1	0.1	0.2	0.3	0.3	0.0	0.0	0.2	0.4	0.7	0.3	0.5	0.5	0.7	0.8	0.4	0.2
110.	*	0.0	0.0	0.3	0.3	0.2	0.1	0.1	0.1	0.0	0.0	0.2	0.3	0.6	0.2	0.2	0.7	0.7	0.9	0.6	0.2
120.	*	0.0	0.1	0.5	0.4	0.3	0.0	0.0	0.1	0.0	0.0	0.2	0.2	0.5	0.2	0.1	0.9	0.7	0.9	0.9	0.3
130.	*	0.1	0.2	0.6	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.1	0.8	0.7	0.8	1.1	0.3
140.	*	0.1	0.2	0.7	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.6	0.1	0.1	0.7	0.7	0.8	1.1	0.4
150.	*	0.1	0.2	0.6	0.4	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.5	0.1	0.0	0.6	0.7	0.8	0.9	0.5
160.	*	0.1	0.2	0.6	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.0	0.4	0.7	0.9	0.9	0.6
170.	*	0.1	0.3	0.6	0.3	0.3	0.0	0.0	0.1	0.1	0.0	0.2	0.2	0.2	0.0	0.0	0.3	0.7	0.7	1.0	0.9
180.	*	0.1	0.3	0.8	0.3	0.3	0.0	0.0	0.3	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.3	0.6	0.7	0.8	0.8
190.	*	0.3	0.5	0.9	0.3	0.3	0.0	0.0	0.6	0.2	0.2	0.0	0.0	0.1	0.0	0.0	0.3	0.5	0.6	0.7	0.6
200.	*	0.5	0.6	0.8	0.5	0.3	0.0	0.1	0.7	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.5	0.4	0.5
210.	*	0.4	0.7	0.9	0.7	0.4	0.0	0.1	0.9	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.6	0.3	0.3
220.	*	0.6	0.6	0.7	0.7	0.4	0.1	0.1	0.9	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.7	0.3	0.2
230.	*	0.5	0.7	0.8	0.8	0.5	0.1	0.2	0.8	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.3	0.1
240.	*	0.4	0.8	0.8	1.0	0.6	0.1	0.2	0.7	0.5	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.2	0.1
250.	*	0.3	0.6	0.8	1.0	0.8	0.2	0.3	0.7	0.5	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.4	0.1	0.1
260.	*	0.2	0.5	0.8	0.9	0.7	0.2	0.3	0.9	0.6	0.2	0.0	0.0	0.2	0.1	0.1	0.3	0.3	0.4	0.1	0.0
270.	*	0.2	0.4	0.6	0.7	0.7	0.3	0.5	1.0	0.7	0.2	0.0	0.0	0.4	0.2	0.1	0.1	0.2	0.2	0.0	0.0
280.	*	0.2	0.2	0.5	0.6	0.5	0.5	0.6	1.3	0.8	0.2	0.0	0.0	0.8	0.3	0.2	0.1	0.1	0.1	0.0	0.0
290.	*	0.2	0.2	0.5	0.3	0.2	0.7	0.7	1.2	0.9	0.2	0.0	0.1	1.0	0.5	0.3	0.0	0.0	0.0	0.0	0.0
300.	*	0.2	0.2	0.5	0.2	0.1	0.4	0.8	1.1	1.1	0.3	0.1	0.2	1.0	0.6	0.4	0.0	0.0	0.0	0.0	0.0
310.	*	0.2	0.2	0.5	0.1	0.1	0.6	0.5	0.8	1.1	0.4	0.1	0.3	1.0	0.7	0.4	0.0	0.0	0.0	0.0	0.0
320.	*	0.2	0.2	0.4	0.1	0.1	0.6	0.5	0.7	1.1	0.6	0.1	0.4	1.0	0.8	0.4	0.0	0.0	0.0	0.0	0.0
330.	*	0.1	0.2	0.4	0.1	0.1	0.5	0.5	0.7	1.0	0.8	0.2	0.4	0.8	0.7	0.3	0.0	0.0	0.0	0.0	0.0
340.	*	0.1	0.2	0.3	0.1	0.0	0.4	0.5	0.7	0.9	0.9	0.2	0.4	0.7	0.8	0.3	0.0	0.0	0.0	0.0	0.0
350.	*	0.1	0.2	0.2	0.1	0.0	0.3	0.5	0.6	0.8	0.8	0.2	0.4	0.5	0.9	0.3	0.0	0.0	0.0	0.0	0.0
360.	*	0.1	0.2	0.2	0.0	0.0	0.3	0.4	0.5	0.6	0.5	0.3	0.4	0.4	0.9	0.3	0.0	0.0	0.0	0.0	0.0
MAX	*	0.6	0.8	0.9	1.0	0.8	0.7	0.8	1.3	1.1	0.9	0.7	0.8	1.0	1.3	0.9	0.9	0.7	0.9	1.1	0.9

DEGR. * 220 240 190 250 250 290 300 280 300 340 30 30 290 40 80 120 110 110
130 170

THE HIGHEST CONCENTRATION OF 1.30 PPM OCCURRED AT RECEPTOR REC4 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:12:41

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6049.9	5447.4	*	66.	290.	AG	275.	100.0	1.0	30.0	0.52	3.3
2. Char/Merr WB	*	6250.4	5435.2	6333.8	5501.2	*	106.	52.	AG	275.	100.0	1.0	30.0	0.77	5.4
3. Char/Merr NB R	*	6291.7	5369.7	6315.3	5353.7	*	29.	124.	AG	54.	100.0	1.0	10.0	0.14	1.5
4. Char/Merr NB LTT	*	6280.4	5347.2	6430.5	5241.4	*	184.	125.	AG	171.	100.0	1.0	20.0	0.92	9.3
5. Char/Merr EB	*	6104.2	5362.2	6060.5	5345.9	*	47.	250.	AG	191.	100.0	1.0	20.0	0.42	2.4
6. Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.5	*	108.	14.	AG	78.	100.0	1.0	10.0	0.71	5.5
7. Char/Cam SB TR	*	5360.8	4833.5	5398.9	4956.5	*	129.	17.	AG	190.	100.0	1.0	20.0	0.92	6.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	145.	100.0	1.0	20.0	0.27	2.2
9. Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	78.	100.0	1.0	10.0	0.60	4.7
10. Char/Cam NB TR	*	5383.3	4723.8	5384.4	4650.0	*	74.	179.	AG	190.	100.0	1.0	20.0	0.71	3.7
11. Char/Cam EB TTTR	*	5302.7	4739.8	5214.1	4740.7	*	89.	271.	AG	217.	100.0	1.0	30.0	0.54	4.5
12. Sud/Merr SB L	*	6532.7	5210.3	6487.5	5242.5	*	56.	305.	AG	104.	100.0	1.0	10.0	0.72	2.8
13. Sud/Merr SB TTT	*	6518.3	5190.8	6477.9	5214.2	*	47.	300.	AG	177.	100.0	1.0	30.0	0.24	2.4
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6673.5	5068.9	*	106.	150.	AG	228.	100.0	1.0	30.0	0.60	5.4
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6478.2	5118.7	*	53.	239.	AG	352.	100.0	1.0	40.0	0.38	2.7
16. Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	128.	100.0	1.0	20.0	0.34	3.3
17. Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	84.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6745.9	5240.5	*	52.	249.	AG	279.	100.0	1.0	30.0	0.43	2.7
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	877.	8.3	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1122.	8.3	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1326.	8.3	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	939.	8.3	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	849.	8.3	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1614.	8.3	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	950.	8.3	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1709.	8.3	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	318.	8.3	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	536.	8.3	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	8.3	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	373.	8.3	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	8.3	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1555.	8.3	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1648.	8.3	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	529.	8.3	1.0	78.0		

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
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ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. Char/Merr SB	*	100	76	3.0	476	1600	44.99	1	3
2. Char/Merr WB	*	100	76	3.0	703	1600	44.99	1	3
3. Char/Merr NB R	*	100	45	3.0	116	1600	44.99	1	3
4. Char/Merr NB LTT	*	100	71	3.0	709	1600	44.99	1	3

5. Char/Merr EB	*	100	79	3.0	217	1600	44.99	1	3
6. Char/Cam SB L	*	90	58	3.0	339	1600	44.99	1	3
7. Char/Cam SB TR	*	90	71	3.0	457	1600	44.99	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	294	1600	44.99	1	3
9. Char/Cam NB L	*	90	58	3.0	289	1600	44.99	1	3
10. Char/Cam NB TR	*	90	71	3.0	354	1600	44.99	1	3
11. Char/Cam EB TTTR	*	90	54	3.0	901	1600	44.99	1	3
12. Sud/Merr SB L	*	100	86	3.0	104	1600	44.99	1	3
13. Sud/Merr SB TTT	*	100	49	3.0	524	1600	44.99	1	3
14. Sud/Merr NB TTTR	*	100	63	3.0	924	1600	44.99	1	3
15. Sud/Merr EB LTTR	*	100	73	3.0	529	1600	44.99	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	455	1600	44.99	1	3
17. Sud/Sur SEB	*	100	70	3.0	26	1600	44.99	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	373	1600	44.99	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Sud/Merr NE1	*	6492.5	5309.9	6.0	*
2. Sud/Merr NE2	*	6554.8	5268.0	6.0	*
3. Sud/Merr NE3	*	6616.2	5224.9	6.0	*
4. Sud/Merr NE4	*	6684.7	5255.3	6.0	*
5. Sud/Merr NE5	*	6753.3	5285.7	6.0	*
6. Sud/Merr SE1	*	6792.9	5222.3	6.0	*
7. Sud/Merr SE2	*	6724.3	5191.9	6.0	*
8. Sud/Merr SE3	*	6655.7	5161.5	6.0	*
9. Sud/Merr SE4	*	6695.5	5097.9	6.0	*
10. Sud/Merr SE5	*	6735.2	5034.3	6.0	*
11. Sud/Merr SW1	*	6638.6	4981.3	6.0	*
12. Sud/Merr SW2	*	6598.9	5045.0	6.0	*
13. Sud/Merr SW3	*	6559.1	5108.6	6.0	*
14. Sud/Merr SW4	*	6493.4	5072.5	6.0	*
15. Sud/Merr SW5	*	6427.6	5036.5	6.0	*
16. Sud/Merr NW1	*	6347.8	5104.5	6.0	*
17. Sud/Merr NW2	*	6413.5	5140.5	6.0	*
18. Sud/Merr NW3	*	6479.3	5176.6	6.0	*
19. Sud/Merr NW4	*	6417.1	5218.5	6.0	*
20. Sud/Merr NW5	*	6354.9	5260.4	6.0	*
21. Sud/Sur NE1	*	6755.9	5445.7	6.0	*
22. Sud/Sur NE2	*	6801.0	5385.7	6.0	*
23. Sud/Sur NE3	*	6846.0	5325.7	6.0	*
24. Sud/Sur NE4	*	6908.8	5366.8	6.0	*
25. Sud/Sur NE5	*	6971.5	5407.9	6.0	*
26. Sud/Sur SE1	*	7002.4	5368.4	6.0	*
27. Sud/Sur SE2	*	6939.7	5327.3	6.0	*

JOB: Government Center Garage RUN: 2028NB

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RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
28. Sud/Sur SE3	*	6876.9	5286.2	6.0	*
29. Sud/Sur SE4	*	6931.7	5235.0	6.0	*
30. Sud/Sur SE5	*	6986.5	5183.8	6.0	*
31. Sud/Sur SW1	*	6932.3	5133.1	6.0	*
32. Sud/Sur SE2	*	6877.5	5184.3	6.0	*
33. Sud/Sur SE3	*	6822.7	5235.5	6.0	*
34. Sud/Sur SE4	*	6754.2	5205.1	6.0	*
35. Sud/Sur SE5	*	6685.6	5174.8	6.0	*
36. Sud/Sur NW1	*	6645.5	5237.9	6.0	*
37. Sud/Sur NW2	*	6714.1	5268.3	6.0	*
38. Sud/Sur NW3	*	6782.7	5298.7	6.0	*
39. Sud/Sur NW4	*	6709.5	5315.4	6.0	*
40. Sud/Sur NW5	*	6636.4	5332.0	6.0	*
41. Sud/Sur N1	*	6642.4	5493.7	6.0	*
42. Sud/Sur N2	*	6687.4	5433.7	6.0	*
43. Sud/Sur N3	*	6732.4	5373.8	6.0	*
44. Sud/Sur N4	*	6659.3	5390.4	6.0	*
45. Sud/Sur N5	*	6586.2	5407.1	6.0	*

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	(PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.1	0.0	0.0	0.0	0.2	0.6	0.2	0.1	0.0	0.1	0.6	0.5	0.5	1.0	0.4	0.4	0.4	0.7	0.8	0.9
10.	0.1	0.0	0.0	0.0	0.2	0.3	0.2	0.1	0.1	0.1	0.7	0.6	0.5	1.0	0.3	0.3	0.4	0.7	0.8	0.8
20.	0.0	0.0	0.0	0.1	0.2	0.1	0.4	0.1	0.1	0.1	0.6	0.7	0.5	0.9	0.5	0.3	0.2	0.8	0.6	0.8
30.	0.0	0.0	0.0	0.1	0.1	0.2	0.5	0.2	0.1	0.0	0.4	0.6	0.5	0.6	0.5	0.2	0.3	0.8	0.5	0.8
40.	0.0	0.0	0.0	0.0	0.1	0.1	0.5	0.2	0.1	0.0	0.3	0.7	0.5	0.5	0.6	0.1	0.3	0.8	0.4	0.7
50.	0.0	0.0	0.0	0.0	0.1	0.1	0.4	0.3	0.0	0.0	0.3	0.6	0.7	0.5	0.4	0.2	0.3	0.8	0.4	0.7
60.	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.0	0.0	0.3	0.6	0.7	0.3	0.4	0.4	0.3	0.7	0.3	0.8
70.	0.0	0.0	0.2	0.1	0.0	0.1	0.2	0.1	0.0	0.0	0.3	0.5	0.6	0.4	0.2	0.5	0.5	0.8	0.4	0.9
80.	0.0	0.0	0.2	0.3	0.0	0.1	0.1	0.0	0.0	0.0	0.3	0.4	0.6	0.4	0.2	0.5	0.7	0.8	0.5	0.9
90.	0.0	0.1	0.2	0.5	0.1	0.1	0.1	0.0	0.0	0.0	0.3	0.3	0.6	0.3	0.1	0.4	0.7	0.7	0.7	0.9
100.	0.1	0.1	0.2	0.5	0.2	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.7	0.3	0.1	0.4	0.8	0.7	0.7	1.0
110.	0.0	0.0	0.1	0.4	0.4	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.2	0.1	0.2	0.7	0.9	0.8	0.9
120.	0.2	0.0	0.1	0.2	0.5	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.2	0.1	0.2	0.5	0.9	0.9	0.9
130.	0.4	0.3	0.1	0.1	0.6	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.1	0.0	0.1	0.3	1.0	0.7	0.5
140.	0.5	0.6	0.3	0.1	0.6	0.0	0.0	0.1	0.1	0.1	0.3	0.3	0.4	0.0	0.0	0.1	0.1	0.9	0.5	0.3
150.	0.7	0.7	0.6	0.1	0.7	0.0	0.0	0.4	0.2	0.2	0.1	0.2	0.2	0.0	0.0	0.1	0.1	0.9	0.3	0.2
160.	0.8	0.7	0.9	0.2	0.7	0.0	0.1	0.7	0.4	0.3	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.8	0.2	0.0
170.	0.7	0.6	1.0	0.4	0.7	0.0	0.1	0.9	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.7	0.1	0.0
180.	0.7	0.6	0.8	0.4	0.6	0.1	0.2	1.0	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.5	0.1	0.0
190.	0.6	0.7	0.6	0.5	0.5	0.1	0.3	1.0	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.4	0.1	0.0
200.	0.5	0.8	0.5	0.5	0.5	0.1	0.3	1.0	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.3	0.1	0.0
210.	0.3	0.8	0.6	0.5	0.4	0.2	0.4	0.9	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.0
220.	0.4	0.8	0.7	0.5	0.3	0.2	0.4	0.9	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0
230.	0.5	0.5	0.6	0.6	0.4	0.2	0.5	0.9	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0
240.	0.5	0.5	0.8	0.5	0.5	0.2	0.5	1.1	0.8	0.3	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.0	0.0
250.	0.5	0.5	0.6	0.4	0.3	0.4	0.7	1.1	0.8	0.3	0.0	0.0	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0
260.	0.6	0.5	0.6	0.3	0.1	0.4	0.7	1.0	0.9	0.3	0.0	0.0	0.3	0.1	0.1	0.0	0.0	0.0	0.0	0.1
270.	0.6	0.6	0.6	0.3	0.3	0.4	0.4	1.0	1.1	0.3	0.0	0.1	0.4	0.1	0.1	0.0	0.0	0.0	0.0	0.2
280.	0.5	0.7	0.6	0.3	0.1	0.7	0.5	1.2	1.2	0.6	0.0	0.1	0.6	0.1	0.1	0.0	0.0	0.0	0.2	0.2
290.	0.7	0.4	0.5	0.2	0.1	0.5	0.4	1.0	1.3	0.7	0.0	0.2	0.7	0.1	0.1	0.0	0.1	0.3	0.2	0.4
300.	0.3	0.4	0.5	0.2	0.1	0.6	0.2	0.8	1.3	1.0	0.1	0.3	1.0	0.1	0.1	0.1	0.1	0.4	0.6	0.7
310.	0.2	0.3	0.3	0.1	0.1	0.7	0.2	0.6	0.9	0.9	0.1	0.6	1.0	0.2	0.1	0.1	0.2	0.6	0.7	0.7
320.	0.2	0.2	0.1	0.1	0.0	0.7	0.2	0.4	0.5	0.7	0.5	0.8	1.0	0.4	0.1	0.1	0.2	0.9	1.1	0.9
330.	0.1	0.1	0.1	0.0	0.0	0.7	0.1	0.3	0.2	0.4	0.4	0.6	0.9	0.7	0.3	0.1	0.5	0.8	1.1	1.0
340.	0.1	0.1	0.1	0.0	0.1	0.8	0.1	0.1	0.0	0.2	0.5	0.4	0.7	0.8	0.4	0.3	0.6	0.8	1.1	1.1
350.	0.1	0.1	0.0	0.0	0.2	0.8	0.1	0.1	0.0	0.0	0.7	0.4	0.5	1.0	0.4	0.4	0.6	0.6	1.0	0.9
360.	0.1	0.0	0.0	0.0	0.2	0.6	0.2	0.1	0.0	0.1	0.6	0.5	0.5	1.0	0.4	0.4	0.4	0.7	0.8	0.9
MAX	0.8	0.8	1.0	0.6	0.7	0.8	0.7	1.2	1.3	1.0	0.7	0.8	1.0	1.0	0.6	0.5	0.8	1.0	1.1	1.1
DEGR.	160	200	170	230	150	340	250	280	290	300	10	320	300	0	40	70	100	130	320	340

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.8	0.1	0.0	0.1	0.2	0.1	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.7	0.1	0.0	0.2	0.1	0.2	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.7	0.1	0.0	0.2	0.1	0.2	0.0
30.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.2	0.6	0.2	0.0	0.1	0.1	0.2	0.0
40.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.2	0.5	0.3	0.0	0.0	0.1	0.2	0.0
50.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.3	0.3	0.0	0.0	0.1	0.2	0.1
60.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.1	0.0	0.1	0.1	0.1
70.	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.2	0.1	0.1	0.1	0.1
80.	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.3	0.3	0.1	0.0	0.0
90.	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.3	0.5	0.1	0.0	0.0
100.	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.1	0.0	0.2	0.6	0.1	0.0	0.0
110.	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.0	0.1	0.7	0.1	0.2	0.1
120.	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.0	0.1	0.6	0.1	0.3	0.1
130.	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.4	0.1	0.3
140.	0.0	0.1	0.2	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.2	0.4	0.1
150.	0.3	0.1	0.2	0.1	0.0	0.0	0.0	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.3	0.3	0.0
160.	0.4	0.2	0.2	0.1	0.0	0.0	0.0	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.2	0.4	0.1	0.4	0.2	0.2
170.	0.4	0.2	0.2	0.2	0.0	0.0	0.1	0.2	0.1	0.1	0.0	0.0	0.0	0.1	0.4	0.6	0.2	0.5	0.3	0.3
180.	0.6	0.3	0.2	0.2	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.5	0.7	0.4	0.7	0.3	0.3
190.	0.7	0.4	0.3	0.2	0.0	0.0	0.1	0.2	0.1	0.1	0.0	0.0	0.1	0.2	0.6	0.7	0.4	0.8	0.4	0.3
200.	0.5	0.4	0.4	0.3	0.1	0.0	0.2	0.2	0.2	0.1	0.0	0.1	0.1	0.3	0.6	0.6	0.5	0.8	0.4	0.3
210.	0.4	0.4	0.5	0.3	0.2	0.1	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.3	0.7	0.5	0.5	0.7	0.2	0.4
220.	0.3	0.4	0.5	0.4	0.2	0.1	0.2	0.3	0.2	0.2	0.1	0.1	0.2	0.4	0.7	0.5	0.4	0.6	0.2	0.4
230.	0.3	0.4	0.5	0.4	0.3	0.1	0.4	0.4	0.2	0.2	0.1	0.1	0.2	0.4	0.7	0.6	0.5	0.4	0.4	0.4
240.	0.2	0.4	0.4	0.2	0.1	0.3	0.3	0.6	0.3	0.2	0.1	0.2	0.2	0.5	0.8	0.5	0.5	0.4	0.2	0.2
250.	0.3	0.4	0.3	0.1	0.0	0.2	0.2	0.5	0.3	0.3	0.1	0.2	0.5	0.6	0.7	0.6	0.3	0.1	0.1	0.2
260.	0.2	0.5	0.2	0.0	0.0	0.1	0.3	0.5	0.3	0.3	0.2	0.2	0.5	0.6	0.8	0.3	0.1	0.1	0.3	0.3
270.	0.3	0.4	0.1	0.2	0.0	0.1	0.1	0.4	0.3	0.2	0.2	0.3	0.6	0.3	0.7	0.5	0.3	0.3	0.3	0.2
280.	0.2	0.5	0.1	0.2	0.0	0.0	0.1	0.2	0.2	0.3	0.3	0.2	0.8	0.4	0.7	0.4	0.3	0.1	0.1	0.1
290.	0.2	0.5	0.3	0.3	0.0	0.0	0.2	0.2	0.2	0.3	0.1	0.1	0.6	0.4	0.6	0.3	0.1	0.1	0.2	0.2
300.	0.2	0.4	0.3	0.0	0.0	0.0	0.1	0.2	0.1	0.2	0.1	0.2	0.6	0.1	0.5	0.4	0.1	0.1	0.1	0.2
310.	0.1	0.2	0.2	0.0	0.0	0.0	0.1	0.3	0.2	0.1	0.2	0.2	0.5	0.1	0.2	0.2	0.1	0.1	0.1	0.1
320.	0.1	0.1	0.2	0.0	0.0	0.0	0.1	0.3	0.0	0.0	0.2	0.2	0.3	0.1	0.2	0.1	0.1	0.0	0.1	0.1
330.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.2	0.3	0.2	0.1	0.1	0.0	0.2	0.0	0.1
340.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.1	0.2	0.3	0.1	0.0	0.0	0.2	0.0	0.0
350.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.2	0.5	0.1	0.0	0.0	0.2	0.1	0.0
360.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.8	0.1	0.0	0.1	0.2	0.1	0.0

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------*-------------------------------------------------------------------------------------------------------------
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 MAX   *   0.7   0.5   0.5   0.4   0.3   0.3   0.4   0.6   0.3   0.3   0.3   0.3   0.8   0.8   0.8   0.7   0.7   0.8
0.4   0.4
 DEGR. *  190   260   210   220   230   240   230   240   240   250   280   270   280     0   240   180   110   190
140   210
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JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45
0.	0.1	0.1	0.2	0.0	0.0
10.	0.1	0.1	0.3	0.1	0.0
20.	0.1	0.1	0.3	0.1	0.0
30.	0.1	0.1	0.4	0.1	0.0
40.	0.1	0.1	0.4	0.1	0.0
50.	0.1	0.1	0.4	0.1	0.0
60.	0.1	0.1	0.4	0.1	0.0
70.	0.1	0.1	0.4	0.2	0.0
80.	0.1	0.1	0.3	0.2	0.0
90.	0.1	0.2	0.3	0.2	0.1
100.	0.1	0.2	0.2	0.2	0.1
110.	0.1	0.3	0.2	0.1	0.0
120.	0.2	0.3	0.1	0.0	0.1
130.	0.2	0.2	0.2	0.1	0.1
140.	0.2	0.2	0.2	0.1	0.1
150.	0.1	0.1	0.1	0.1	0.1
160.	0.0	0.1	0.2	0.2	0.2
170.	0.1	0.2	0.3	0.2	0.3
180.	0.2	0.2	0.2	0.3	0.3
190.	0.1	0.2	0.2	0.2	0.3
200.	0.1	0.1	0.2	0.2	0.2
210.	0.1	0.3	0.2	0.3	0.1
220.	0.1	0.1	0.3	0.2	0.1
230.	0.2	0.1	0.2	0.1	0.3
240.	0.2	0.2	0.1	0.2	0.2
250.	0.1	0.2	0.2	0.3	0.2
260.	0.2	0.1	0.2	0.2	0.3
270.	0.2	0.2	0.1	0.1	0.3
280.	0.1	0.2	0.2	0.2	0.2
290.	0.1	0.1	0.1	0.2	0.2
300.	0.1	0.1	0.1	0.1	0.1
310.	0.1	0.1	0.1	0.1	0.1
320.	0.1	0.1	0.1	0.1	0.1
330.	0.0	0.1	0.1	0.1	0.1
340.	0.0	0.1	0.1	0.0	0.1
350.	0.1	0.1	0.2	0.0	0.1
360.	0.1	0.1	0.2	0.0	0.0
MAX	0.2	0.3	0.4	0.3	0.3
DEGR.	120	110	30	180	170

THE HIGHEST CONCENTRATION OF 1.30 PPM OCCURRED AT RECEPTOR REC9 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:12:47

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6036.0	5452.4	*	80.	290.	AG	272.	100.0	1.0	30.0	0.61	4.1
2.	Char/Merr WB	*	6250.4	5435.2	6303.9	5477.6	*	68.	52.	AG	282.	100.0	1.0	30.0	0.59	3.5
3.	Char/Merr NB R	*	6291.7	5369.7	6345.2	5333.4	*	65.	124.	AG	56.	100.0	1.0	10.0	0.33	3.3
4.	Char/Merr NB LTT	*	6280.4	5347.2	6359.4	5291.5	*	97.	125.	AG	164.	100.0	1.0	20.0	0.60	4.9
5.	Char/Merr EB	*	6104.2	5362.2	5973.2	5313.5	*	140.	250.	AG	191.	100.0	1.0	20.0	0.91	7.1
6.	Char/Cam SB L	*	5384.1	4834.2	5402.3	4907.1	*	75.	14.	AG	72.	100.0	1.0	10.0	0.41	3.8
7.	Char/Cam SB TR	*	5360.8	4833.5	5375.6	4881.2	*	50.	17.	AG	174.	100.0	1.0	20.0	0.35	2.5
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	150.	100.0	1.0	20.0	0.41	3.7
9.	Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	72.	100.0	1.0	10.0	0.53	5.0
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.9	4614.7	*	109.	179.	AG	174.	100.0	1.0	20.0	0.73	5.5
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5211.5	4740.8	*	91.	271.	AG	224.	100.0	1.0	30.0	0.51	4.6
12.	Sud/Merr SB L	*	6532.7	5210.3	6492.2	5239.1	*	50.	305.	AG	101.	100.0	1.0	10.0	0.60	2.5
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6484.0	5210.7	*	40.	300.	AG	181.	100.0	1.0	30.0	0.20	2.0
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6677.8	5061.4	*	115.	150.	AG	239.	100.0	1.0	30.0	0.69	5.8
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6452.9	5103.5	*	82.	239.	AG	348.	100.0	1.0	40.0	0.57	4.2
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	169.	100.0	1.0	20.0	0.53	4.1
17.	Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	97.	100.0	1.0	10.0	0.15	0.8
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6715.8	5228.7	*	84.	249.	AG	181.	100.0	1.0	30.0	0.43	4.3
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	921.	8.3	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1336.	8.3	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1354.	8.3	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	940.	8.3	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	863.	8.3	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1593.	8.3	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1023.	8.3	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1636.	8.3	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	901.	8.3	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	488.	8.3	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	8.3	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	928.	8.3	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	8.3	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1317.	8.3	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1611.	8.3	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	837.	8.3	1.0	78.0		

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:12:47

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Char/Merr SB	*	100	75	3.0	589	1600	44.99	1	3
2.	Char/Merr WB	*	100	78	3.0	481	1600	44.99	1	3
3.	Char/Merr NB R	*	100	46	3.0	257	1600	44.99	1	3
4.	Char/Merr NB LTT	*	100	68	3.0	520	1600	44.99	1	3

5.	Char/Merr EB	*	100	79	3.0	468	1600	44.99	1	3
6.	Char/Cam SB L	*	100	60	3.0	229	1600	44.99	1	3
7.	Char/Cam SB TR	*	100	72	3.0	254	1600	44.99	1	3
8.	Char/Cam WB LTTR	*	100	62	3.0	435	1600	44.99	1	3
9.	Char/Cam NB L	*	100	60	3.0	299	1600	44.99	1	3
10.	Char/Cam NB TR	*	100	72	3.0	536	1600	44.99	1	3
11.	Char/Cam EB TTTR	*	100	62	3.0	809	1600	44.99	1	3
12.	Sud/Merr SB L	*	100	84	3.0	106	1600	44.99	1	3
13.	Sud/Merr SB TTT	*	100	50	3.0	435	1600	44.99	1	3
14.	Sud/Merr NB TTTR	*	100	66	3.0	954	1600	44.99	1	3
15.	Sud/Merr EB LTTR	*	100	72	3.0	837	1600	44.99	1	3
16.	Sud/Sur SB LTT	*	100	70	3.0	424	1600	44.99	1	3
17.	Sud/Sur SEB	*	100	80	3.0	37	1600	44.99	1	3
18.	Sud/Sur EB TTR	*	100	50	3.0	928	1600	44.99	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Sud/Merr NE1	*	6492.5	5309.9	6.0
2.	Sud/Merr NE2	*	6554.8	5268.0	6.0
3.	Sud/Merr NE3	*	6616.2	5224.9	6.0
4.	Sud/Merr NE4	*	6684.7	5255.3	6.0
5.	Sud/Merr NE5	*	6753.3	5285.7	6.0
6.	Sud/Merr SE1	*	6792.9	5222.3	6.0
7.	Sud/Merr SE2	*	6724.3	5191.9	6.0
8.	Sud/Merr SE3	*	6655.7	5161.5	6.0
9.	Sud/Merr SE4	*	6695.5	5097.9	6.0
10.	Sud/Merr SE5	*	6735.2	5034.3	6.0
11.	Sud/Merr SW1	*	6638.6	4981.3	6.0
12.	Sud/Merr SW2	*	6598.9	5045.0	6.0
13.	Sud/Merr SW3	*	6559.1	5108.6	6.0
14.	Sud/Merr SW4	*	6493.4	5072.5	6.0
15.	Sud/Merr SW5	*	6427.6	5036.5	6.0
16.	Sud/Merr NW1	*	6347.8	5104.5	6.0
17.	Sud/Merr NW2	*	6413.5	5140.5	6.0
18.	Sud/Merr NW3	*	6479.3	5176.6	6.0
19.	Sud/Merr NW4	*	6417.1	5218.5	6.0
20.	Sud/Merr NW5	*	6354.9	5260.4	6.0
21.	Sud/Sur NE1	*	6755.9	5445.7	6.0
22.	Sud/Sur NE2	*	6801.0	5385.7	6.0
23.	Sud/Sur NE3	*	6846.0	5325.7	6.0
24.	Sud/Sur NE4	*	6908.8	5366.8	6.0
25.	Sud/Sur NE5	*	6971.5	5407.9	6.0
26.	Sud/Sur SE1	*	7002.4	5368.4	6.0
27.	Sud/Sur SE2	*	6939.7	5327.3	6.0

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:12:47

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
28.	Sud/Sur SE3	*	6876.9	5286.2	6.0
29.	Sud/Sur SE4	*	6931.7	5235.0	6.0
30.	Sud/Sur SE5	*	6986.5	5183.8	6.0
31.	Sud/Sur SW1	*	6932.3	5133.1	6.0
32.	Sud/Sur SE2	*	6877.5	5184.3	6.0
33.	Sud/Sur SE3	*	6822.7	5235.5	6.0
34.	Sud/Sur SE4	*	6754.2	5205.1	6.0
35.	Sud/Sur SE5	*	6685.6	5174.8	6.0
36.	Sud/Sur NW1	*	6645.5	5237.9	6.0
37.	Sud/Sur NW2	*	6714.1	5268.3	6.0
38.	Sud/Sur NW3	*	6782.7	5298.7	6.0
39.	Sud/Sur NW4	*	6709.5	5315.4	6.0
40.	Sud/Sur NW5	*	6636.4	5332.0	6.0
41.	Sud/Sur N1	*	6642.4	5493.7	6.0
42.	Sud/Sur N2	*	6687.4	5433.7	6.0
43.	Sud/Sur N3	*	6732.4	5373.8	6.0
44.	Sud/Sur N4	*	6659.3	5390.4	6.0
45.	Sud/Sur N5	*	6586.2	5407.1	6.0

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.1	0.0	0.0	0.0	0.4	0.6	0.6	0.2	0.2	0.2	0.8	0.6	0.5	1.3	0.6	0.3	0.3	0.6	0.4	0.7
10.	*	0.1	0.0	0.0	0.1	0.2	0.3	0.7	0.2	0.2	0.2	0.8	0.7	0.5	1.1	0.5	0.2	0.3	0.6	0.4	0.6
20.	*	0.0	0.0	0.0	0.1	0.2	0.3	0.7	0.3	0.2	0.1	0.8	0.7	0.6	1.0	0.8	0.3	0.1	0.6	0.2	0.5
30.	*	0.0	0.0	0.1	0.1	0.1	0.2	0.6	0.4	0.2	0.0	0.6	0.8	0.5	0.7	0.8	0.1	0.2	0.8	0.3	0.4
40.	*	0.0	0.0	0.1	0.1	0.1	0.3	0.7	0.5	0.1	0.0	0.4	0.8	0.7	0.7	0.9	0.1	0.3	0.8	0.3	0.3
50.	*	0.0	0.1	0.0	0.0	0.1	0.2	0.5	0.4	0.0	0.0	0.3	0.6	0.8	0.6	0.7	0.1	0.3	0.8	0.2	0.3
60.	*	0.0	0.1	0.2	0.0	0.1	0.2	0.3	0.4	0.0	0.0	0.3	0.6	0.8	0.5	0.5	0.4	0.3	0.6	0.3	0.4
70.	*	0.0	0.0	0.3	0.3	0.1	0.1	0.1	0.2	0.0	0.0	0.3	0.5	0.7	0.5	0.2	0.7	0.7	0.9	0.3	0.4
80.	*	0.0	0.0	0.4	0.5	0.2	0.1	0.1	0.0	0.0	0.0	0.3	0.5	0.6	0.4	0.2	0.7	0.9	0.8	0.6	0.5
90.	*	0.0	0.2	0.5	0.5	0.2	0.1	0.1	0.0	0.0	0.0	0.3	0.4	0.6	0.3	0.2	0.7	0.9	0.8	0.7	0.4
100.	*	0.2	0.2	0.4	0.7	0.3	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.7	0.3	0.1	0.6	1.1	0.8	0.7	0.6
110.	*	0.2	0.2	0.2	0.6	0.3	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.2	0.1	0.4	1.1	1.0	0.8	0.7
120.	*	0.3	0.1	0.2	0.5	0.5	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.2	0.1	0.3	1.0	1.1	0.8	0.8
130.	*	0.4	0.4	0.2	0.4	0.6	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.4	0.1	0.0	0.2	0.7	1.1	0.8	0.7
140.	*	0.6	0.7	0.4	0.3	0.5	0.0	0.0	0.1	0.1	0.1	0.3	0.3	0.4	0.0	0.0	0.2	0.4	1.0	0.5	0.5
150.	*	0.5	0.8	0.8	0.3	0.6	0.0	0.0	0.5	0.2	0.2	0.1	0.2	0.2	0.0	0.0	0.2	0.3	1.0	0.4	0.3
160.	*	0.9	0.8	1.0	0.3	0.6	0.0	0.1	0.7	0.4	0.3	0.1	0.1	0.1	0.0	0.0	0.2	0.2	0.9	0.3	0.2
170.	*	0.9	0.7	1.0	0.5	0.7	0.0	0.1	0.9	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.9	0.2	0.1
180.	*	0.8	0.6	0.9	0.6	0.7	0.1	0.2	1.1	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.9	0.2	0.1
190.	*	0.6	0.6	0.8	0.6	0.8	0.1	0.3	1.1	0.6	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.1	0.1
200.	*	0.4	0.9	0.7	0.6	0.8	0.1	0.4	1.1	0.7	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.7	0.1	0.0
210.	*	0.4	0.9	0.7	0.6	0.8	0.2	0.4	0.9	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.0
220.	*	0.3	0.8	0.8	0.7	0.7	0.2	0.5	0.9	0.8	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.0	0.0
230.	*	0.3	0.6	0.9	0.6	0.8	0.3	0.5	0.9	0.8	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.0	0.0
240.	*	0.3	0.5	1.0	0.6	0.6	0.5	0.7	1.1	0.9	0.3	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0
250.	*	0.4	0.3	0.6	0.5	0.4	0.7	0.7	1.3	0.9	0.3	0.0	0.0	0.4	0.2	0.1	0.0	0.0	0.1	0.0	0.0
260.	*	0.4	0.4	0.6	0.1	0.1	0.7	0.8	1.2	1.1	0.3	0.0	0.1	0.5	0.2	0.2	0.0	0.0	0.0	0.0	0.1
270.	*	0.5	0.3	0.6	0.2	0.2	0.8	0.6	1.1	1.2	0.4	0.0	0.1	0.7	0.2	0.2	0.0	0.0	0.0	0.0	0.2
280.	*	0.6	0.5	0.4	0.2	0.1	0.9	0.5	1.1	1.3	0.7	0.1	0.2	0.8	0.3	0.2	0.0	0.0	0.0	0.2	0.3
290.	*	0.6	0.5	0.3	0.2	0.1	0.6	0.4	1.1	1.3	0.8	0.1	0.3	0.9	0.3	0.2	0.0	0.1	0.2	0.3	0.5
300.	*	0.3	0.4	0.4	0.1	0.1	0.8	0.4	0.8	1.3	1.2	0.2	0.4	0.9	0.5	0.2	0.1	0.1	0.4	0.5	0.7
310.	*	0.2	0.3	0.2	0.1	0.1	0.8	0.3	0.7	1.0	1.0	0.4	0.6	1.0	0.7	0.2	0.2	0.2	0.4	0.6	0.9
320.	*	0.1	0.1	0.1	0.1	0.1	0.6	0.3	0.5	0.8	0.8	0.6	0.6	1.0	0.9	0.2	0.1	0.2	0.7	0.7	0.9
330.	*	0.1	0.1	0.1	0.1	0.0	0.6	0.3	0.4	0.4	0.5	0.5	0.7	0.9	1.1	0.3	0.1	0.4	0.4	0.7	1.0
340.	*	0.1	0.1	0.1	0.0	0.2	0.8	0.3	0.2	0.1	0.3	0.5	0.6	0.8	1.2	0.4	0.3	0.5	0.4	0.7	1.0
350.	*	0.1	0.1	0.0	0.0	0.3	0.7	0.4	0.2	0.1	0.2	0.6	0.5	0.7	1.3	0.4	0.4	0.2	0.5	0.4	0.9
360.	*	0.1	0.0	0.0	0.0	0.4	0.6	0.6	0.2	0.2	0.2	0.8	0.6	0.5	1.3	0.6	0.3	0.3	0.6	0.4	0.7
MAX	*	0.9	0.9	1.0	0.7	0.8	0.9	0.8	1.3	1.3	1.2	0.8	0.8	1.0	1.3	0.9	0.7	1.1	1.1	0.8	1.0
DEGR.	*	170	200	160	220	210	280	260	250	280	300	0	30	310	0	40	70	100	120	110	330

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.1	0.2	0.1	0.7	0.2	0.0	0.1	0.2	0.2	0.0
10.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.1	0.2	0.2	0.7	0.4	0.0	0.1	0.2	0.2	0.0
20.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.0	0.0	0.1	0.2	0.2	0.6	0.4	0.1	0.1	0.1	0.3	0.0
30.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.0	0.0	0.1	0.1	0.3	0.5	0.4	0.1	0.1	0.1	0.3	0.0
40.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.0	0.0	0.1	0.1	0.3	0.5	0.5	0.1	0.0	0.1	0.2	0.1
50.	*	0.0	0.0	0.1	0.0	0.0	0.0	0.1	0.2	0.0	0.0	0.1	0.1	0.2	0.3	0.6	0.0	0.0	0.1	0.2	0.1
60.	*	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.2	0.4	0.4	0.2	0.1	0.2	0.3	0.1
70.	*	0.0	0.0	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.1
80.	*	0.0	0.0	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.4	0.3	0.2	0.2	0.1
90.	*	0.0	0.0	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.5	0.5	0.2	0.1	0.0
100.	*	0.0	0.1	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.5	0.6	0.2	0.1	0.0
110.	*	0.0	0.1	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.3	0.7	0.2	0.3	0.2
120.	*	0.1	0.1	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.2	0.6	0.1	0.3	0.2
130.	*	0.1	0.1	0.2	0.2	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.6	0.2	0.3	0.2
140.	*	0.1	0.2	0.3	0.2	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.2	0.6	0.2	0.3	0.2
150.	*	0.2	0.2	0.3	0.2	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.4	0.6	0.2	0.3	0.2
160.	*	0.3	0.3	0.3	0.2	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.2	0.6	0.6	0.4	0.3	0.3
170.	*	0.5	0.1	0.3	0.3	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.4	0.8	0.6	0.5	0.4	0.4
180.	*	0.8	0.4	0.3	0.3	0.1	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.5	0.8	0.7	0.6	0.4	0.4
190.	*	0.9	0.4	0.4	0.3	0.1	0.0	0.1	0.2	0.1	0.1	0.0	0.0	0.1	0.2	0.6	0.8	0.6	0.7	0.4	0.4
200.	*	0.8	0.5	0.5	0.5	0.2	0.0	0.2	0.2	0.2	0.1	0.0	0.1	0.1	0.3	0.7	0.7	0.7	0.8	0.3	0.4
210.	*	0.7	0.5	0.5	0.4	0.3	0.1	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.3	0.7	0.8	0.7	0.9	0.3	0.4
220.	*	0.7	0.6	0.6	0.6	0.3	0.1	0.2	0.3	0.2	0.2	0.1	0.1	0.2	0.4	0.6	0.6	0.7	0.8	0.5	0.3
230.	*	0.5	0.6	0.6	0.5	0.6	0.2	0.6	0.5	0.2	0.2	0.1	0.1	0.2	0.4	0.6	0.7	0.6	0.9	0.4	0.3
240.	*	0.4	0.5	0.6	0.5	0.3	0.5	0.5	0.7	0.3	0.2	0.1	0.2	0.4	0.7	0.7	0.6	0.6	0.6	0.3	0.1
250.	*	0.4	0.5	0.5	0.1	0.0	0.4	0.4	0.9	0.4	0.3	0.2	0.2	0.7	0.5	0.9	0.6	0.5	0.4	0.1	0.1
260.	*	0.3	0.6	0.2	0.0	0.1	0.2	0.5	0.7	0.6	0.3	0.2	0.4	1.0	0.7	0.9	0.3	0.1	0.1	0.2	0.2
270.	*	0.2	0.5	0.1	0.1	0.1	0.2	0.3	0.5	0.3	0.3	0.3	0.4	0.8	0.6	0.8	0.3	0.2	0.2	0.2	0.1
280.	*	0.2	0.6	0.1	0.3	0.1	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.9	0.6	0.7	0.3	0.2	0.1	0.1	0.2
290.	*	0.2	0.6	0.3	0.2	0.0	0.1	0.4	0.3	0.3	0.3	0.2	0.2	0.6	0.6	0.6	0.2	0.2	0.1	0.1	0.1
300.	*	0.2	0.5	0.3	0.1	0.0	0.0	0.3	0.5	0.3	0.1	0.2	0.3	0.6	0.5	0.5	0.3	0.1	0.1	0.1	0.1
310.	*	0.2	0.3	0.3	0.0	0.0	0.0	0.2	0.4	0.3	0.1	0.2	0.2	0.5	0.6	0.4	0.1	0.1	0.2	0.1	0.1
320.	*	0.1	0.2	0.2	0.0	0.0	0.0	0.2	0.4	0.2	0.1	0.1	0.3	0.3	0.7	0.3	0.1	0.1	0.2	0.1	0.1
330.	*	0.0	0.0	0.1	0.0	0.0	0.0	0.2	0.2	0.1	0.1	0.1	0.2	0.4	0.6	0.3	0.1	0.0	0.2	0.0	0.1
340.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.1	0.2	0.2	0.3	0.6	0.2	0.1	0.0	0.3	0.0	0.1
350.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.2	0.2	0.3	0.7	0.2	0.0	0.0	0.3	0.0	0.0
360.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.1	0.2	0.1	0.7	0.2	0.0	0.1	0.2	0.2	0.0

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------*-------------------------------------------------------------------------------------------------------------
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 MAX   *   0.9   0.6   0.6   0.6   0.6   0.5   0.6   0.9   0.6   0.3   0.3   0.4   1.0   0.7   0.9   0.8   0.7   0.9
0.5   0.4
 DEGR. *  190   220   220   220   230   240   230   250   260   250   270   260   260   240   250   210   110   230
220   170
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JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45
0.	0.1	0.1	0.4	0.0	0.0
10.	0.1	0.1	0.4	0.1	0.0
20.	0.1	0.1	0.5	0.1	0.0
30.	0.1	0.1	0.5	0.1	0.0
40.	0.1	0.1	0.5	0.1	0.0
50.	0.1	0.1	0.5	0.2	0.0
60.	0.1	0.1	0.5	0.2	0.0
70.	0.1	0.2	0.4	0.3	0.0
80.	0.1	0.2	0.4	0.3	0.1
90.	0.1	0.3	0.3	0.3	0.1
100.	0.1	0.4	0.4	0.2	0.1
110.	0.2	0.4	0.3	0.1	0.0
120.	0.2	0.4	0.2	0.0	0.0
130.	0.2	0.3	0.2	0.1	0.2
140.	0.2	0.2	0.1	0.2	0.2
150.	0.2	0.1	0.3	0.2	0.2
160.	0.2	0.2	0.3	0.3	0.3
170.	0.3	0.3	0.3	0.3	0.4
180.	0.2	0.3	0.3	0.3	0.3
190.	0.1	0.3	0.4	0.3	0.4
200.	0.2	0.2	0.3	0.2	0.3
210.	0.2	0.4	0.3	0.4	0.3
220.	0.1	0.3	0.3	0.3	0.1
230.	0.1	0.1	0.3	0.1	0.2
240.	0.1	0.1	0.1	0.1	0.1
250.	0.2	0.1	0.1	0.1	0.2
260.	0.1	0.1	0.1	0.1	0.2
270.	0.1	0.1	0.1	0.2	0.2
280.	0.1	0.1	0.1	0.1	0.2
290.	0.1	0.1	0.1	0.1	0.1
300.	0.1	0.1	0.1	0.1	0.1
310.	0.1	0.1	0.1	0.1	0.1
320.	0.1	0.1	0.1	0.1	0.1
330.	0.1	0.1	0.1	0.1	0.1
340.	0.0	0.1	0.2	0.0	0.1
350.	0.1	0.1	0.3	0.0	0.1
360.	0.1	0.1	0.4	0.0	0.0
MAX	0.3	0.4	0.5	0.4	0.4
DEGR.	170	100	20	210	170

THE HIGHEST CONCENTRATION OF 1.30 PPM OCCURRED AT RECEPTOR REC14.

2028 Build
Microscale Output Files
(Carbon Monoxide (CO))

JOB: Government Center Garage RUN: Build

DATE : 7/10/13
TIME : 15:36: 3

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1. Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	75.	100.0	1.0	10.0	0.71
2. Stan/Lom SB TRR	*	5173.5	5937.1	5105.0	6035.3	*	120.	325.	AG	151.	100.0	1.0	20.0	0.55
3. Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	183.	100.0	1.0	20.0	0.92
4. Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	75.	100.0	1.0	10.0	0.58
5. Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	98.	100.0	1.0	10.0	0.64
6. Stan/Lom NB TRR	*	5314.4	5765.3	5366.6	5747.7	*	55.	109.	AG	195.	100.0	1.0	20.0	0.44
7. Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	195.	100.0	1.0	20.0	0.68
8. Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	98.	100.0	1.0	10.0	0.93
9. Caus/Wash SB LTTRR	*	6548.6	6868.7	6144.6	7708.0	*	931.	334.	AG	302.	100.0	1.0	40.0	1.09
10. Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	191.	100.0	1.0	20.0	0.58
11. Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	84.	100.0	1.0	10.0	0.53
12. Caus/Wash NB TTR	*	6603.5	6751.9	6667.3	5333.6	*	1420.	177.	AG	193.	100.0	1.0	20.0	1.41
13. Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	282.	100.0	1.0	30.0	0.47
14. Tha/Val SB LTTR	*	6599.0	6224.0	6593.6	6363.6	*	140.	358.	AG	70.	100.0	1.0	20.0	0.80
15. Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	86.	100.0	1.0	10.0	1.23
16. Tha/Val NB TR	*	6645.6	6138.6	6647.7	6016.6	*	122.	179.	AG	35.	100.0	1.0	10.0	0.70
17. Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6099.5	*	136.	0.	AG	163.	100.0	1.0	30.0	0.69
18. Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	199.	100.0	1.0	30.0	0.18
19. Char/93 SB LLTTRR	*	6587.8	5740.0	6582.2	5885.7	*	146.	358.	AG	256.	100.0	1.0	40.0	0.75
20. Char/93 WB LTT	*	6702.8	5647.8	6766.7	5567.9	*	102.	141.	AG	167.	100.0	1.0	20.0	0.65
21. Char/93 EB TTR	*	6560.8	5622.5	6514.2	5588.4	*	58.	234.	AG	250.	100.0	1.0	30.0	0.37
22. North/Congress SB LT	*	6876.6	4408.9	6575.8	5898.4	*	1520.	349.	AG	326.	100.0	1.0	30.0	2.65
23. North/Con WB LLTR	*	6920.6	4378.3	7916.6	4730.8	*	1057.	71.	AG	145.	100.0	1.0	20.0	1.13
24. Nor/Con NB LTTTR	*	6914.9	4333.4	6921.1	4287.3	*	47.	172.	AG	268.	100.0	1.0	30.0	0.34
25. Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	72.	100.0	1.0	10.0	0.03
26. Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1464.	8.3	1.0	90.0	
27. Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1588.	8.3	1.0	78.0	
28. Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	967.	8.3	1.0	78.0	
29. Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	8.3	1.0	78.0	
30. Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3453.	8.3	1.0	90.0	
31. Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	8.3	1.0	66.0	
32. Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2405.	8.3	1.0	90.0	
33. Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	8.3	1.0	78.0	
34. Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2431.	8.3	1.0	90.0	
35. Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	8.3	1.0	38.0	
36. Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2871.	8.3	1.0	90.0	
37. Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	8.3	1.0	54.0	
38. Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2351.	8.3	1.0	66.0	
39. Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	8.3	1.0	48.0	
40. Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	542.	8.3	1.0	42.0	
41. Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	8.3	1.0	48.0	
42. Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	459.	8.3	1.0	54.0	
43. Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	729.	8.3	1.0	54.0	

44. Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	8.3	1.0	42.0	

JOB: Government Center Garage RUN: Build

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LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45. North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1629.	8.3	1.0	98.0	
46. North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1333.	8.3	1.0	66.0	
47. North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1545.	8.3	1.0	98.0	
48. North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	8.3	1.0	54.0	

JOB: Government Center Garage RUN: Build

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ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. Stan/Lom SB L	*	120	75	3.0	376	1600	44.99	1	3
2. Stan/Lom SB TRR	*	120	75	3.0	585	1600	44.99	1	3
3. Stan/Lom WB LTT	*	120	91	3.0	588	1600	44.99	1	3
4. Stan/Lom WB R	*	120	75	3.0	308	1600	44.99	1	3
5. Stan/Lom NB L	*	120	97	3.0	152	1600	44.99	1	3
6. Stan/Lom NB TRR	*	120	97	3.0	208	1600	44.99	1	3
7. Stan/Lom EB LLT	*	120	97	3.0	324	1600	44.99	1	3
8. Stan/Lom EB R	*	120	97	3.0	222	1600	44.99	1	3
9. Caus/Wash SB LTTRR	*	150	94	3.0	2380	1600	44.99	1	3
10. Caus/Wash WB LLTT	*	150	119	3.0	321	1600	44.99	1	3
11. Caus/Wash WB R	*	150	104	3.0	230	1600	44.99	1	3
12. Caus/Wash NB TTR	*	150	120	3.0	748	1600	44.99	1	3
13. Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	44.99	1	3
14. Tha/Val SB LTTR	*	104	30	3.0	1705	1600	44.99	1	3
15. Tha/Val NB L	*	104	74	3.0	472	1600	44.99	1	3
16. Tha/Val NB TR	*	104	30	3.0	744	1600	44.99	1	3
17. Bev/Was SB TTT	*	100	45	3.0	1655	1600	44.99	1	3
18. Bev/Was EB RRR	*	100	55	3.0	356	1600	44.99	1	3
19. Char/93 SB LLTTRR	*	100	53	3.0	2013	1600	44.99	1	3
20. Char/93 WB LTT	*	100	69	3.0	542	1600	44.99	1	3
21. Char/93 EB TTR	*	100	69	3.0	459	1600	44.99	1	3
22. North/Congress SB LT	*	100	90	3.0	636	1600	44.99	1	3
23. North/Con WB LLTR	*	100	60	3.0	1267	1600	44.99	1	3
24. Nor/Con NB LTTTR	*	100	74	3.0	345	1600	44.99	1	3
25. Nor/Con EB LTR	*	100	60	3.0	17	1600	44.99	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2. Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3. Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4. Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5. Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6. Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7. Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8. Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9. Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10. Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11. Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12. Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13. Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14. Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15. Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16. Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17. Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18. Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19. Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20. Stan/Lom NW5	*	5136.5	5935.7	6.0	*

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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
21. Caus/Wash NE1	6548.3	7035.9	6.0
22. Caus/Wash NE2	6581.4	6968.6	6.0
23. Caus/Wash NE3	6614.5	6901.3	6.0
24. Caus/Wash NE4	6669.8	6952.0	6.0
25. Caus/Wash NE5	6725.0	7002.7	6.0
26. Caus/Wash SE1	6753.6	6912.2	6.0
27. Caus/Wash SE2	6698.9	6862.0	6.0
28. Caus/Wash SE3	6643.1	6810.8	6.0
29. Caus/Wash SE4	6646.8	6736.4	6.0
30. Caus/Wash SE5	6650.0	6661.0	6.0
31. Caus/Wash SW1	6544.0	6561.0	6.0
32. Caus/Wash SW2	6540.9	6636.0	6.0
33. Caus/Wash SW3	6537.8	6710.9	6.0
34. Caus/Wash SW4	6476.8	6667.2	6.0
35. Caus/Wash SW5	6415.9	6623.4	6.0
36. Caus/Wash NW1	6407.4	6738.0	6.0
37. Caus/Wash NW2	6468.3	6781.7	6.0
38. Caus/Wash NW3	6529.3	6825.4	6.0
39. Caus/Wash NW4	6496.2	6892.7	6.0
40. Caus/Wash NW5	6463.1	6960.0	6.0
41. Tha/Val NE1	6667.3	6395.5	6.0
42. Tha/Val NE2	6668.3	6320.5	6.0
43. Tha/Val NE3	6669.3	6245.5	6.0
44. Tha/Val NE4	6744.3	6245.5	6.0
45. Tha/Val NE5	6819.2	6249.6	6.0
46. Tha/Val SE1	6822.3	6191.6	6.0
47. Tha/Val SE2	6747.3	6189.6	6.0
48. Tha/Val SE3	6672.3	6187.5	6.0
49. Tha/Val SE4	6671.6	6112.5	6.0
50. Tha/Val SE5	6670.9	6037.5	6.0
51. Tha/Val SW1	6560.2	5964.7	6.0
52. Tha/Val SW2	6560.9	6039.7	6.0
53. Tha/Val SW3	6561.6	6114.7	6.0
54. Tha/Val SW4	6502.2	6068.9	6.0
55. Tha/Val SW5	6442.7	6023.2	6.0
56. Tha/Val NW1	6441.0	6115.2	6.0
57. Tha/Val NW2	6500.4	6160.9	6.0
58. Tha/Val NW3	6559.8	6206.7	6.0
59. Tha/Val NW4	6558.8	6281.7	6.0
60. Tha/Val NW5	6557.8	6356.7	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.0	0.0	0.0	0.0	0.0	0.8	0.7	0.5	0.3	0.2	0.4	0.7	0.5	0.7	0.8	0.1	0.3	0.3	0.6	0.9
10.	0.0	0.0	0.0	0.0	0.0	0.7	0.8	0.5	0.4	0.2	0.3	0.7	0.6	0.6	0.7	0.2	0.1	0.2	0.5	0.8
20.	0.0	0.0	0.0	0.0	0.0	0.7	0.8	0.6	0.3	0.1	0.2	0.7	0.5	0.4	0.5	0.4	0.3	0.3	0.3	0.7
30.	0.0	0.0	0.0	0.0	0.1	0.7	0.7	0.6	0.3	0.1	0.3	0.6	0.5	0.4	0.4	0.5	0.5	0.5	0.3	0.7
40.	0.1	0.1	0.2	0.2	0.1	0.5	0.7	0.7	0.1	0.0	0.2	0.4	0.4	0.2	0.1	0.6	0.5	0.5	0.6	0.7
50.	0.1	0.0	0.4	0.3	0.1	0.2	0.4	0.4	0.0	0.0	0.2	0.3	0.4	0.3	0.1	0.8	0.4	0.5	0.7	0.7
60.	0.0	0.0	0.6	0.6	0.2	0.1	0.1	0.1	0.0	0.0	0.2	0.3	0.5	0.1	0.1	0.8	0.5	0.3	0.9	0.9
70.	0.0	0.2	1.0	0.9	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.1	0.8	0.5	0.1	0.8	0.9
80.	0.0	0.3	0.9	1.0	0.6	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.1	0.1	0.8	0.6	0.1	0.6	0.8
90.	0.2	0.5	0.8	1.0	0.7	0.0	0.0	0.0	0.1	0.1	0.4	0.4	0.5	0.2	0.1	0.9	0.7	0.2	0.4	0.8
100.	0.2	0.6	0.9	1.1	0.8	0.1	0.1	0.2	0.2	0.2	0.3	0.4	0.5	0.2	0.1	0.9	0.7	0.4	0.5	0.8
110.	0.3	0.6	0.6	1.0	0.8	0.1	0.1	0.3	0.3	0.3	0.3	0.3	0.3	0.1	0.1	0.8	0.8	0.6	0.4	0.6
120.	0.3	0.5	0.5	1.0	0.8	0.1	0.2	0.4	0.5	0.3	0.2	0.2	0.2	0.1	0.1	0.7	0.7	0.6	0.5	0.6
130.	0.3	0.5	0.5	1.0	0.8	0.1	0.2	0.6	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.5	0.7	0.3	0.4	0.4

140.	0.4	0.5	0.4	0.9	0.8	0.1	0.1	0.4	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.5	0.7	0.4	0.1	0.2
150.	0.4	0.5	0.6	0.9	0.9	0.1	0.2	0.4	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.5	0.8	0.4	0.2	0.2
160.	0.4	0.5	0.6	0.9	0.9	0.1	0.2	0.2	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.8	0.5	0.3	0.2
170.	0.6	0.5	0.5	0.9	1.0	0.1	0.3	0.3	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.7	0.7	0.4	0.2
180.	0.7	0.5	0.7	1.0	1.1	0.2	0.2	0.4	0.7	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.5	0.7	0.3	0.1
190.	0.7	0.4	0.8	1.0	1.2	0.2	0.3	0.6	0.7	0.2	0.0	0.0	0.2	0.1	0.1	0.3	0.3	0.5	0.2	0.1
200.	0.6	0.4	0.6	1.0	1.1	0.3	0.4	0.7	0.7	0.3	0.0	0.0	0.4	0.3	0.2	0.2	0.2	0.2	0.1	0.0
210.	0.6	0.5	0.6	0.7	1.0	0.2	0.4	0.4	0.8	0.4	0.0	0.1	0.7	0.6	0.3	0.1	0.1	0.1	0.0	0.0
220.	0.6	0.5	0.4	0.5	1.0	0.2	0.3	0.3	0.7	0.5	0.0	0.1	0.8	0.6	0.5	0.0	0.0	0.0	0.0	0.0
230.	0.6	0.6	0.4	0.4	0.5	0.2	0.1	0.1	0.6	0.7	0.1	0.3	0.9	0.6	0.5	0.0	0.0	0.0	0.0	0.0
240.	0.5	0.6	0.3	0.3	0.3	0.2	0.1	0.1	0.5	0.8	0.1	0.4	0.8	0.7	0.6	0.0	0.0	0.0	0.0	0.0
250.	0.5	0.6	0.3	0.3	0.2	0.4	0.2	0.0	0.3	0.8	0.1	0.4	0.7	0.7	0.5	0.0	0.0	0.0	0.0	0.0
260.	0.4	0.6	0.4	0.3	0.2	0.5	0.3	0.0	0.2	0.6	0.3	0.4	0.5	0.8	0.5	0.0	0.0	0.0	0.0	0.0
270.	0.4	0.6	0.4	0.4	0.1	0.6	0.4	0.0	0.2	0.6	0.2	0.4	0.4	0.8	0.5	0.0	0.0	0.0	0.0	0.0
280.	0.3	0.5	0.6	0.3	0.1	0.8	0.5	0.0	0.1	0.4	0.2	0.3	0.3	0.8	0.5	0.0	0.0	0.0	0.0	0.0
290.	0.4	0.6	0.7	0.2	0.1	0.8	0.7	0.1	0.1	0.3	0.2	0.3	0.3	0.8	0.5	0.0	0.0	0.0	0.0	0.0
300.	0.4	0.5	0.6	0.2	0.1	0.8	0.7	0.1	0.2	0.2	0.4	0.2	0.3	0.8	0.5	0.0	0.0	0.0	0.0	0.0
310.	0.3	0.4	0.6	0.1	0.0	0.8	0.7	0.4	0.4	0.3	0.5	0.4	0.3	0.8	0.5	0.0	0.0	0.0	0.1	0.0
320.	0.2	0.3	0.3	0.0	0.0	0.8	0.6	0.6	0.5	0.3	0.5	0.3	0.4	0.8	0.6	0.0	0.0	0.0	0.3	0.1
330.	0.1	0.1	0.2	0.0	0.0	0.7	0.4	0.7	0.4	0.3	0.6	0.7	0.6	0.9	0.8	0.0	0.0	0.2	0.5	0.4
340.	0.0	0.1	0.1	0.0	0.0	0.7	0.4	0.7	0.3	0.2	0.6	0.6	0.6	0.8	1.1	0.1	0.1	0.3	0.7	0.6
350.	0.0	0.0	0.0	0.0	0.0	0.7	0.6	0.6	0.3	0.2	0.4	0.7	0.5	0.7	1.1	0.1	0.3	0.3	0.7	0.8
360.	0.0	0.0	0.0	0.0	0.0	0.8	0.7	0.5	0.3	0.2	0.4	0.7	0.5	0.7	0.8	0.1	0.3	0.3	0.6	0.9
MAX	0.7	0.6	1.0	1.1	1.2	0.8	0.8	0.7	0.8	0.8	0.6	0.7	0.9	0.9	1.1	0.9	0.8	0.7	0.9	0.9
DEGR.	180	100	70	100	190	0	10	40	210	240	330	0	230	330	340	90	110	170	60	60

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.0	0.0	0.1	0.0	0.0	0.3	0.7	0.7	0.4	0.5	1.0	1.3	1.8	1.4	0.8	0.5	0.9	1.8	2.0	1.8
10.	0.0	0.0	0.0	0.0	0.0	0.2	0.6	0.7	0.4	0.3	1.2	1.1	1.6	1.6	0.9	0.6	0.8	1.6	1.9	1.7
20.	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.7	0.2	0.1	1.0	1.1	1.3	1.4	0.9	0.6	0.8	1.3	1.7	1.7
30.	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.5	0.2	0.0	1.0	1.1	1.1	1.4	0.9	0.6	0.7	1.0	1.5	1.5
40.	0.0	0.0	0.2	0.0	0.0	0.1	0.2	0.3	0.0	0.0	0.9	0.9	1.0	1.3	1.0	0.5	0.6	1.0	1.5	1.5
50.	0.0	0.0	0.3	0.1	0.0	0.1	0.1	0.1	0.0	0.0	0.8	0.8	1.0	1.0	0.8	0.6	0.8	1.2	1.5	1.5
60.	0.0	0.0	0.6	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.7	0.6	0.5	0.7	0.7	1.2	1.5	1.5
70.	0.0	0.0	0.7	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.7	0.4	0.3	0.7	0.8	1.0	1.7	1.5

```
  80.  *   0.0   0.1   0.8   0.5   0.1   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.7   0.5   0.3   0.9   0.7   1.0
1.7   1.4
  90.  *   0.0   0.1   0.9   0.6   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   1.0   0.7   0.8
1.6   1.7
 100.  *   0.1   0.3   0.9   0.6   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   1.0   0.8   0.8
1.6   1.7
 110.  *   0.1   0.3   0.8   0.6   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   0.9   0.9   0.7
1.4   1.8
 120.  *   0.2   0.4   0.7   0.7   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.3   0.8   1.2   0.9
1.3   1.8
 130.  *   0.3   0.4   0.7   0.7   0.2   0.0   0.0   0.0   0.0   0.0   0.8   0.8   0.8   0.5   0.4   0.7   1.2   0.9
1.3   1.8
 140.  *   0.3   0.5   0.5   0.7   0.2   0.0   0.0   0.0   0.0   0.0   0.9   0.9   0.9   0.6   0.4   0.9   1.3   1.1
1.0   1.5
 150.  *   0.6   0.5   0.6   0.8   0.2   0.0   0.0   0.0   0.0   0.0   0.9   1.0   1.0   0.5   0.5   0.7   1.4   1.2
1.0   1.2
 160.  *   1.0   0.8   0.8   0.8   0.2   0.0   0.0   0.1   0.1   0.1   1.2   1.3   1.2   0.7   0.5   0.7   1.4   1.6
1.1   1.1
 170.  *   1.6   1.4   1.3   1.1   0.4   0.1   0.2   0.6   0.6   0.6   1.2   1.2   1.3   0.6   0.4   0.8   1.4   1.6
1.2   0.9
 180.  *   1.9   1.9   1.7   1.6   0.8   0.2   0.6   1.1   1.2   1.2   0.8   0.8   0.8   0.3   0.1   0.4   0.8   1.4
0.8   0.5
 190.  *   1.7   1.5   1.7   1.7   1.1   0.6   0.8   1.4   1.4   1.4   0.3   0.3   0.3   0.0   0.0   0.3   0.5   0.9
0.3   0.1
 200.  *   1.5   1.4   1.4   1.6   1.3   0.5   0.7   1.1   1.2   1.2   0.0   0.0   0.0   0.0   0.0   0.3   0.4   0.7
0.3   0.1
 210.  *   1.3   1.3   1.2   1.3   1.3   0.4   0.5   0.9   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.3   0.3   0.7
0.1   0.1
 220.  *   1.2   1.3   1.2   1.1   1.1   0.5   0.6   0.8   1.0   1.0   0.0   0.0   0.0   0.0   0.0   0.3   0.3   0.5
0.1   0.0
 230.  *   1.2   1.2   1.1   0.8   0.8   0.9   0.8   1.0   0.9   0.9   0.0   0.0   0.1   0.1   0.1   0.2   0.2   0.3
0.0   0.0
 240.  *   1.2   1.2   1.0   0.7   0.5   0.8   0.9   0.9   1.0   0.9   0.0   0.0   0.4   0.2   0.2   0.1   0.1   0.1
0.0   0.0
 250.  *   1.2   1.2   1.0   0.7   0.5   1.1   0.9   1.1   1.1   0.9   0.0   0.1   0.5   0.3   0.2   0.0   0.0   0.0
0.0   0.0
 260.  *   1.2   1.2   1.1   0.7   0.5   1.1   1.0   0.9   1.2   1.0   0.0   0.1   0.7   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 270.  *   1.2   1.2   1.2   0.7   0.5   1.3   1.0   0.9   1.2   1.1   0.1   0.2   0.8   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 280.  *   1.2   1.2   1.3   0.7   0.6   1.3   1.2   0.9   1.2   1.1   0.1   0.2   0.9   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 290.  *   1.4   1.4   1.4   0.8   0.6   1.2   1.4   1.0   1.1   1.2   0.1   0.2   1.0   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 300.  *   1.4   1.5   1.5   0.8   0.5   1.1   1.5   1.3   1.0   1.2   0.1   0.3   1.0   0.3   0.3   0.0   0.0   0.0
0.0   0.0
 310.  *   1.4   1.5   1.5   0.7   0.4   0.9   1.4   1.6   1.0   1.3   0.1   0.4   1.0   0.3   0.3   0.0   0.0   0.1
0.1   0.1
 320.  *   1.3   1.4   1.5   0.5   0.2   0.6   1.3   1.9   1.5   1.4   0.2   0.4   1.1   0.4   0.3   0.0   0.0   0.4
0.3   0.3
 330.  *   0.9   1.0   1.2   0.3   0.1   0.3   0.9   1.7   1.7   1.7   0.3   0.7   1.2   0.6   0.3   0.0   0.1   1.0
1.0   0.8
 340.  *   0.4   0.5   0.5   0.1   0.0   0.2   0.7   1.2   1.3   1.5   0.7   1.0   1.6   0.8   0.3   0.1   0.4   1.8
1.7   1.5
 350.  *   0.1   0.1   0.1   0.0   0.0   0.2   0.6   1.0   0.8   1.0   1.1   1.3   1.9   1.2   0.6   0.4   0.8   2.1
2.0   1.9
 360.  *   0.0   0.0   0.1   0.0   0.0   0.3   0.7   0.7   0.4   0.5   1.0   1.3   1.8   1.4   0.8   0.5   0.9   1.8
2.0   1.8

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX   *   1.9   1.9   1.7   1.7   1.3   1.3   1.5   1.9   1.7   1.7   1.2   1.3   1.9   1.6   1.0   1.0   1.4   2.1
2.0   1.9
 DEGR. *  180   180   180   190   200   270   300   320   330   330    10     0   350    10    40    90   160   350
0   350
```


JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52 REC53 REC54 REC55 REC56 REC57 REC58
REC59 REC60

------*-------------------------------------------------------------------------------------------------------------
-------
   0.  *   0.5   0.8   0.8   0.0   0.0   0.0   0.0   0.7   1.0   1.1   1.1   1.0   1.0   0.6   0.2   0.2   0.4   0.9
0.8   0.8
  10.  *   0.1   0.3   0.3   0.0   0.0   0.0   0.0   0.3   0.3   0.3   1.5   1.3   1.4   0.6   0.6   0.4   0.6   1.2
1.1   1.1
  20.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.7   1.4   1.4   0.6   0.4   0.3   0.5   1.1
```



```
1.1   0.9
  30.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.7   1.4   1.2   0.7   0.5   0.5   0.7   1.0
1.0   0.9
  40.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.6   1.6   1.2   0.7   0.6   0.4   0.6   1.0
1.0   0.8
  50.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.4   1.4   1.0   0.7   0.5   0.4   0.6   0.9
0.9   0.8
  60.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.3   1.4   1.0   0.8   0.6   0.5   0.7   0.9
0.9   0.8
  70.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.3   1.2   0.8   0.7   0.5   0.5   0.8   0.9
0.9   0.8
  80.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.2   1.3   1.0   0.9   0.6   0.5   0.8   0.9
0.9   0.9
  90.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1   1.3   1.0   0.9   0.6   0.6   0.7   1.1
0.9   0.9
 100.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0   1.3   1.1   0.9   0.7   0.6   0.8   1.2
0.9   0.9
 110.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.9   1.3   1.1   0.9   0.6   0.6   0.7   1.2
0.9   0.9
 120.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.0   1.4   1.2   0.9   0.8   0.7   0.9   1.2
0.9   0.9
 130.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.1   1.4   1.3   0.8   1.0   0.7   0.9   1.2
1.0   1.0
 140.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.4   1.4   1.5   0.9   1.1   1.0   1.0   1.3
1.1   1.2
 150.  *   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   1.8   1.8   1.6   1.4   1.2   1.1   1.3   1.5
1.2   1.4
 160.  *   0.0   0.0   0.1   0.0   0.0   0.0   0.0   0.2   0.1   0.2   2.6   2.0   1.9   1.5   0.9   0.9   1.3   1.9
1.6   1.5
 170.  *   0.6   0.6   0.7   0.1   0.1   0.1   0.1   0.6   0.6   0.6   2.7   2.0   2.0   1.2   0.3   0.7   1.0   2.0
1.8   1.7
 180.  *   1.1   1.4   1.5   0.3   0.2   0.2   0.3   1.4   1.4   1.3   2.0   1.6   1.5   0.6   0.1   0.1   0.6   1.3
1.5   1.2
 190.  *   1.9   1.9   1.9   0.9   0.3   0.3   0.8   1.9   1.8   1.8   1.0   0.9   0.7   0.1   0.0   0.0   0.2   0.6
0.5   0.4
 200.  *   1.4   1.7   1.9   0.9   0.8   0.6   0.9   1.9   2.1   2.0   0.6   0.5   0.2   0.1   0.0   0.0   0.1   0.1
0.1   0.0
 210.  *   1.2   1.1   1.3   1.0   0.7   0.8   1.0   1.7   2.0   2.0   0.3   0.3   0.0   0.0   0.0   0.0   0.1   0.1
0.0   0.0
 220.  *   1.1   1.3   1.3   0.7   0.8   0.8   0.9   1.4   1.6   1.7   0.3   0.2   0.0   0.0   0.0   0.0   0.1   0.1
0.0   0.0
 230.  *   1.0   1.0   1.2   0.7   0.4   0.5   0.8   1.2   1.4   1.5   0.4   0.1   0.0   0.0   0.0   0.0   0.0   0.1
0.0   0.0
 240.  *   0.9   0.9   1.2   0.6   0.4   0.4   0.6   1.3   1.4   1.5   0.5   0.1   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 250.  *   0.8   0.9   0.9   0.6   0.4   0.3   0.6   1.1   1.3   1.4   0.6   0.1   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 260.  *   0.8   0.9   1.0   0.6   0.4   0.4   0.7   1.3   1.3   1.4   0.6   0.0   0.1   0.0   0.0   0.0   0.0   0.0
0.0   0.0
 270.  *   0.8   0.9   1.0   0.5   0.3   0.3   0.6   1.2   1.4   1.4   0.7   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 280.  *   0.8   0.9   1.0   0.6   0.3   0.4   0.6   1.1   1.3   1.4   0.7   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 290.  *   0.7   0.9   1.0   0.6   0.3   0.3   0.5   1.1   1.2   1.3   0.7   0.0   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 300.  *   0.8   0.9   1.0   0.5   0.3   0.3   0.6   1.1   1.4   1.4   0.6   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 310.  *   1.0   0.9   1.0   0.5   0.3   0.3   0.5   1.1   1.2   1.3   0.5   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.0
 320.  *   1.0   1.1   1.1   0.5   0.4   0.4   0.6   1.2   1.2   1.6   0.4   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.0   0.1
 330.  *   1.4   1.4   1.5   0.7   0.5   0.5   0.7   1.4   1.4   1.5   0.3   0.1   0.1   0.1   0.0   0.0   0.0   0.0
0.1   0.1
 340.  *   1.6   1.4   1.5   0.8   0.4   0.4   0.7   1.4   1.8   2.0   0.4   0.2   0.2   0.2   0.0   0.0   0.1   0.2
0.3   0.4
 350.  *   1.2   1.2   1.2   0.4   0.2   0.3   0.4   1.3   1.4   1.6   0.7   0.7   0.7   0.3   0.1   0.1   0.3   0.7
0.7   0.7
 360.  *   0.5   0.8   0.8   0.0   0.0   0.0   0.0   0.7   1.0   1.1   1.1   1.0   1.0   0.6   0.2   0.2   0.4   0.9
0.8   0.8

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX   *   1.9   1.9   1.9   1.0   0.8   0.8   1.0   1.9   2.1   2.0   2.7   2.0   2.0   1.5   1.2   1.1   1.3   2.0
1.8   1.7
 DEGR. *  190   190   190   210   200   210   210   190   200   200   170   160   170   160   150   150   150   170
170   170
```

THE HIGHEST CONCENTRATION OF 2.70 PPM OCCURRED AT RECEPTOR REC51.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Build

DATE : 7/10/13
TIME : 15:35:58

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	75.	100.0	1.0	10.0	0.71	7.8
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5105.0	6035.3	*	120.	325.	AG	151.	100.0	1.0	20.0	0.55	6.1
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	183.	100.0	1.0	20.0	0.92	9.6
4.	Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	75.	100.0	1.0	10.0	0.58	6.4
5.	Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	98.	100.0	1.0	10.0	0.64	4.1
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5366.6	5747.7	*	55.	109.	AG	195.	100.0	1.0	20.0	0.44	2.8
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	195.	100.0	1.0	20.0	0.68	4.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	98.	100.0	1.0	10.0	0.93	8.1
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6144.6	7708.0	*	931.	334.	AG	302.	100.0	1.0	40.0	1.09	47.3
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	191.	100.0	1.0	20.0	0.58	5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	84.	100.0	1.0	10.0	0.53	6.6
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6667.3	5333.6	*	1420.	177.	AG	193.	100.0	1.0	20.0	1.41	72.1
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	282.	100.0	1.0	30.0	0.47	4.6
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.6	6363.6	*	140.	358.	AG	70.	100.0	1.0	20.0	0.80	7.1
15.	Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	86.	100.0	1.0	10.0	1.23	59.7
16.	Tha/Val NB TR	*	6645.6	6138.6	6647.7	6016.6	*	122.	179.	AG	35.	100.0	1.0	10.0	0.70	6.2
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6099.5	*	136.	0.	AG	163.	100.0	1.0	30.0	0.69	6.9
18.	Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	199.	100.0	1.0	30.0	0.18	1.8
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.2	5885.7	*	146.	358.	AG	256.	100.0	1.0	40.0	0.75	7.4
20.	Char/93 WB LTT	*	6702.8	5647.8	6766.7	5567.9	*	102.	141.	AG	167.	100.0	1.0	20.0	0.65	5.2
21.	Char/93 EB TTR	*	6560.8	5622.5	6514.2	5588.4	*	58.	234.	AG	250.	100.0	1.0	30.0	0.37	2.9
22.	North/Congress SB LT	*	6876.6	4408.9	6575.8	5898.4	*	1520.	349.	AG	326.	100.0	1.0	30.0	2.65	77.2
23.	North/Con WB LLTR	*	6920.6	4378.3	7916.6	4730.8	*	1057.	71.	AG	145.	100.0	1.0	20.0	1.13	53.7
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6921.1	4287.3	*	47.	172.	AG	268.	100.0	1.0	30.0	0.34	2.4
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	72.	100.0	1.0	10.0	0.03	0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1464.	8.3	1.0	90.0		
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1588.	8.3	1.0	78.0		
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	967.	8.3	1.0	78.0		
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	8.3	1.0	78.0		
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3453.	8.3	1.0	90.0		
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	8.3	1.0	66.0		
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2405.	8.3	1.0	90.0		
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	8.3	1.0	78.0		
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2431.	8.3	1.0	90.0		
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	8.3	1.0	38.0		
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2871.	8.3	1.0	90.0		
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	8.3	1.0	54.0		
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2351.	8.3	1.0	66.0		
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	8.3	1.0	48.0		
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	542.	8.3	1.0	42.0		
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	8.3	1.0	48.0		
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	459.	8.3	1.0	54.0		
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	729.	8.3	1.0	54.0		

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	8.3	1.0	42.0		
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1629.	8.3	1.0	98.0		
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1333.	8.3	1.0	66.0		
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1545.	8.3	1.0	98.0		
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	8.3	1.0	54.0		

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JOB: Government Center Garage RUN: Build

DATE : 7/10/13
TIME : 15:35:58

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Stan/Lom SB L	*	120	75	3.0	376	1600	44.99	1	3
2.	Stan/Lom SB TRR	*	120	75	3.0	585	1600	44.99	1	3
3.	Stan/Lom WB LTT	*	120	91	3.0	588	1600	44.99	1	3
4.	Stan/Lom WB R	*	120	75	3.0	308	1600	44.99	1	3
5.	Stan/Lom NB L	*	120	97	3.0	152	1600	44.99	1	3
6.	Stan/Lom NB TRR	*	120	97	3.0	208	1600	44.99	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	324	1600	44.99	1	3
8.	Stan/Lom EB R	*	120	97	3.0	222	1600	44.99	1	3
9.	Caus/Wash SB LTTRR	*	150	94	3.0	2380	1600	44.99	1	3
10.	Caus/Wash WB LLTT	*	150	119	3.0	321	1600	44.99	1	3
11.	Caus/Wash WB R	*	150	104	3.0	230	1600	44.99	1	3
12.	Caus/Wash NB TTR	*	150	120	3.0	748	1600	44.99	1	3
13.	Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	44.99	1	3
14.	Tha/Val SB LTTR	*	104	30	3.0	1705	1600	44.99	1	3
15.	Tha/Val NB L	*	104	74	3.0	472	1600	44.99	1	3
16.	Tha/Val NB TR	*	104	30	3.0	744	1600	44.99	1	3
17.	Bev/Was SB TTT	*	100	45	3.0	1655	1600	44.99	1	3
18.	Bev/Was EB RRR	*	100	55	3.0	356	1600	44.99	1	3
19.	Char/93 SB LLTTRR	*	100	53	3.0	2013	1600	44.99	1	3
20.	Char/93 WB LTT	*	100	69	3.0	542	1600	44.99	1	3
21.	Char/93 EB TTR	*	100	69	3.0	459	1600	44.99	1	3
22.	North/Congress SB LT	*	100	90	3.0	636	1600	44.99	1	3
23.	North/Con WB LLTR	*	100	60	3.0	1267	1600	44.99	1	3
24.	Nor/Con NB LTTTR	*	100	74	3.0	345	1600	44.99	1	3
25.	Nor/Con EB LTR	*	100	60	3.0	17	1600	44.99	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Bev/Was N1	*	6562.0	6150.2	6.0	*
2.	Bev/Was N2	*	6561.2	6075.2	6.0	*
3.	Bev/Was N3	*	6560.5	6000.2	6.0	*
4.	Bev/Was N4	*	6515.8	6060.4	6.0	*
5.	Bev/Was N5	*	6471.1	6120.6	6.0	*
6.	Bev/Was SE1	*	6671.0	6049.7	6.0	*
7.	Bev/Was SE2	*	6670.2	5966.3	6.0	*
8.	Bev/Was SE3	*	6624.0	5907.2	6.0	*
9.	Bev/Was SE4	*	6626.1	5832.3	6.0	*
10.	Bev/Was SE5	*	6628.1	5757.3	6.0	*
11.	Bev/Was SW1	*	6541.8	5766.9	6.0	*
12.	Bev/Was SW2	*	6540.1	5841.9	6.0	*
13.	Bev/Was SW3	*	6537.7	5916.8	6.0	*
14.	Bev/Was SW4	*	6493.0	5977.0	6.0	*
15.	Bev/Was SW5	*	6448.3	6037.3	6.0	*
16.	Char/93 NE1	*	6625.0	5871.1	6.0	*
17.	Char/93 NE2	*	6627.1	5796.1	6.0	*
18.	Char/93 NE3	*	6629.1	5721.1	6.0	*
19.	Char/93 NE4	*	6699.8	5695.9	6.0	*
20.	Char/93 NE5	*	6750.6	5633.2	6.0	*

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JOB: Government Center Garage RUN: Build

DATE : 7/10/13
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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
21. Char/93 S1	6657.8	5466.0	6.0
22. Char/93 S2	6614.7	5527.4	6.0
23. Char/93 S3	6571.7	5588.8	6.0
24. Char/93 S4	6512.9	5542.2	6.0
25. Char/93 S5	6454.1	5495.6	6.0
26. Char/93 NW1	6424.1	5632.5	6.0
27. Char/93 NW2	6483.6	5678.2	6.0
28. Char/93 NW3	6543.0	5723.9	6.0
29. Char/93 NW4	6541.0	5798.8	6.0
30. Char/93 NW5	6538.9	5873.8	6.0
31. Wash/Cong NE1	6910.2	4571.2	6.0
32. Wash/Cong NE2	6925.8	4497.8	6.0
33. Wash/Cong NE3	6941.4	4424.5	6.0
34. Wash/Cong NE4	7012.0	4449.6	6.0
35. Wash/Cong NE5	7082.7	4474.9	6.0
36. Wash/Cong SE1	7095.4	4388.1	6.0
37. Wash/Cong SE2	7024.8	4362.9	6.0
38. Wash/Cong SE3	6954.1	4337.7	6.0
39. Wash/Cong SE4	6968.4	4264.1	6.0
40. Wash/Cong SE5	6982.7	4190.4	6.0
41. Wash/Cong SW1	6867.5	4164.7	6.0
42. Wash/Cong SW2	6853.3	4238.0	6.0
43. Wash/Cong SW3	6838.9	4312.0	6.0
44. Wash/Cong SW4	6765.6	4296.1	6.0
45. Wash/Cong SW5	6692.3	4280.2	6.0
46. Wash/Cong NW1	6682.4	4353.8	6.0
47. Wash/Cong NW2	6755.7	4369.7	6.0
48. Wash/Cong NW3	6828.9	4386.0	6.0
49. Wash/Cong NW4	6813.3	4459.4	6.0
50. Wash/Cong NW5	6797.8	4532.8	6.0

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	1.1	1.0	1.1	0.6	0.3	1.0	1.2	3.1	2.6	2.8	1.3	1.1	1.1	0.7	0.4	2.8	2.8	3.4	0.4	0.2
10.	1.3	1.4	1.3	0.7	0.5	0.3	0.3	2.6	2.3	2.0	2.0	1.3	1.3	0.6	0.6	2.4	2.2	2.1	0.1	0.0
20.	1.5	1.3	1.4	0.8	0.4	0.0	0.1	2.2	1.7	1.5	2.4	1.7	1.4	0.8	0.4	1.9	1.5	1.5	0.0	0.0
30.	1.3	1.2	1.6	0.8	0.5	0.0	0.0	1.8	1.3	1.1	2.3	1.9	1.4	0.8	0.5	1.5	1.2	1.1	0.0	0.0
40.	1.3	1.1	1.5	0.8	0.6	0.0	0.0	1.4	1.1	0.9	2.2	1.9	1.2	0.8	0.6	1.2	1.0	0.9	0.0	0.0
50.	1.3	1.3	1.4	0.8	0.6	0.0	0.0	1.2	0.9	0.8	2.1	2.0	1.2	1.0	0.5	1.0	0.9	0.7	0.0	0.0
60.	1.1	1.3	1.4	0.7	0.8	0.0	0.0	1.1	0.9	0.8	2.0	2.0	1.1	1.1	0.7	0.9	0.8	0.6	0.0	0.0
70.	1.2	1.1	1.2	0.9	0.7	0.0	0.0	1.0	0.9	0.7	2.0	2.0	0.9	1.2	0.5	0.9	0.8	0.6	0.0	0.0
80.	1.2	1.4	1.3	0.9	0.8	0.0	0.0	1.0	0.9	0.7	2.0	2.1	0.9	1.2	0.5	0.9	0.7	0.6	0.0	0.0
90.	1.1	1.4	1.3	0.9	0.7	0.0	0.0	0.9	0.8	0.6	2.0	2.1	1.0	1.1	0.7	0.9	0.7	0.6	0.0	0.0
100.	1.0	1.3	1.3	0.9	0.7	0.0	0.0	0.9	0.9	0.7	1.9	2.1	1.0	1.2	0.7	0.9	0.8	0.7	0.0	0.0
110.	1.1	1.3	1.3	0.9	0.8	0.0	0.0	1.0	0.9	0.7	1.8	2.1	1.3	1.0	0.8	0.9	0.8	0.7	0.0	0.0
120.	1.0	1.4	1.4	0.9	0.9	0.0	0.0	1.0	0.9	0.8	1.8	2.1	1.5	1.2	0.8	0.9	0.8	1.1	0.0	0.0
130.	1.1	1.4	1.2	0.9	0.9	0.0	0.0	1.2	0.9	1.0	1.8	2.3	2.0	1.2	0.9	1.1	0.9	1.1	0.0	0.0
140.	1.4	1.6	1.3	0.9	0.9	0.0	0.0	1.1	1.1	1.2	1.7	2.6	2.3	1.3	1.2	1.1	1.2	1.5	0.2	0.1
150.	1.5	1.6	1.6	1.4	1.2	0.0	0.0	1.4	1.6	1.6	1.6	2.3	2.7	1.6	1.2	1.4	1.6	1.8	0.6	0.2
160.	2.0	2.0	2.0	1.6	1.5	0.1	0.2	1.9	2.2	2.3	1.3	2.1	2.6	1.5	0.9	2.1	2.2	2.6	0.7	0.6
170.	2.0	2.0	2.3	1.4	0.9	0.6	0.5	2.5	2.7	2.9	1.1	1.5	1.8	0.8	0.5	2.5	2.7	3.6	1.1	0.8
180.	1.5	1.6	1.8	0.8	0.2	1.3	1.1	2.7	2.8	3.1	0.5	0.8	0.9	0.1	0.1	2.8	2.8	3.5	1.4	1.1
190.	0.8	0.6	1.0	0.3	0.1	1.8	1.6	2.5	2.6	2.6	0.2	0.3	0.3	0.0	0.0	2.6	2.5	3.0	1.3	1.2
200.	0.2	0.1	0.6	0.1	0.1	1.9	1.9	2.3	2.4	2.3	0.2	0.1	0.0	0.0	0.0	2.4	2.3	2.4	1.3	1.3
210.	0.1	0.2	0.4	0.1	0.1	1.9	1.9	2.1	2.3	2.1	0.1	0.0	0.0	0.0	0.0	2.3	2.2	2.1	1.2	1.3
220.	0.2	0.0	0.5	0.1	0.1	1.6	1.8	2.0	2.2	2.0	0.1	0.0	0.0	0.0	0.0	2.1	2.1	2.0	1.2	1.3
230.	0.2	0.0	0.4	0.1	0.1	1.6	1.6	1.7	2.0	1.6	0.0	0.0	0.0	0.0	0.0	2.0	2.3	1.8	1.2	1.3
240.	0.2	0.0	0.4	0.0	0.1	1.5	1.4	1.5	2.0	1.8	0.0	0.0	0.0	0.0	0.0	1.8	2.1	1.6	1.3	1.2
250.	0.2	0.0	0.3	0.0	0.0	1.3	1.2	1.3	2.0	1.9	0.0	0.0	0.0	0.0	0.0	1.8	2.0	1.4	1.3	1.4
260.	0.2	0.0	0.2	0.0	0.0	1.4	1.4	1.0	2.0	2.2	0.0	0.0	0.0	0.0	0.0	1.8	2.0	1.5	1.2	1.4
270.	0.1	0.1	0.1	0.0	0.0	1.4	1.3	0.8	2.0	2.2	0.0	0.0	0.0	0.0	0.0	1.7	2.0	1.3	1.1	1.5
280.	0.1	0.1	0.1	0.1	0.0	1.4	1.4	0.6	2.0	2.2	0.0	0.0	0.0	0.0	0.0	1.5	2.1	1.5	1.2	1.2
290.	0.1	0.1	0.1	0.1	0.0	1.3	1.3	0.6	2.0	2.3	0.0	0.0	0.0	0.0	0.0	1.3	2.1	1.9	1.3	1.2
300.	0.1	0.1	0.1	0.1	0.0	1.3	1.3	0.7	2.0	2.4	0.0	0.0	0.0	0.0	0.0	1.1	2.1	2.3	1.4	1.1
310.	0.1	0.1	0.1	0.1	0.0	1.3	1.4	0.8	1.8	2.7	0.0	0.0	0.0	0.0	0.0	1.0	2.4	2.7	1.6	1.3
320.	0.1	0.1	0.0	0.1	0.0	1.5	1.5	0.9	1.8	2.8	0.0	0.0	0.0	0.0	0.0	0.9	2.3	3.0	1.5	1.2
330.	0.1	0.1	0.1	0.1	0.0	1.5	1.6	1.1	1.8	2.9	0.0	0.0	0.2	0.0	0.0	1.0	2.3	3.4	1.3	0.9
340.	0.2	0.2	0.2	0.2	0.0	1.9	1.8	1.7	1.7	3.2	0.0	0.0	0.3	0.0	0.0	1.6	2.3	3.5	1.4	1.0
350.	0.6	0.7	0.7	0.3	0.2	1.5	1.8	2.6	2.4	3.0	0.3	0.4	0.6	0.2	0.1	2.4	2.8	3.8	1.2	0.6
360.	1.1	1.0	1.1	0.6	0.3	1.0	1.2	3.1	2.6	2.8	1.3	1.1	1.1	0.7	0.4	2.8	2.8	3.4	0.4	0.2
MAX	2.0	2.0	2.3	1.6	1.5	1.9	1.9	3.1	2.8	3.2	2.4	2.6	2.7	1.6	1.2	2.8	2.8	3.8	1.6	1.5
DEGR.	160	160	170	160	160	200	200	0	180	340	20	140	150	150	140	0	350	350	310	270

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	4.8	2.3	1.8	1.0	0.4	0.1	0.4	1.5	1.3	1.1	0.2	0.2	0.2	0.0	0.0	0.4	0.5	0.8	0.6	0.5
10.	4.1	2.4	1.9	1.6	0.8	0.3	0.7	1.9	1.6	1.3	0.0	0.0	0.0	0.0	0.0	0.5	0.6	0.5	0.3	0.2
20.	3.1	2.1	1.5	1.6	1.0	0.6	1.2	2.3	2.2	1.5	0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.6	0.2	0.2
30.	2.5	1.9	1.1	1.4	1.1	0.5	1.2	2.1	2.3	1.4	0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.6	0.3	0.2
40.	2.0	1.8	1.1	1.0	0.9	0.9	1.3	2.0	2.3	1.3	0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.6	0.3	0.1
50.	1.8	1.8	0.9	0.8	0.8	0.9	1.0	1.8	2.2	1.4	0.0	0.0	0.0	0.0	0.0	0.4	0.5	0.6	0.2	0.1
60.	1.7	1.8	1.0	0.7	0.7	0.7	1.1	1.6	2.0	1.6	0.0	0.0	0.2	0.1	0.1	0.3	0.5	0.6	0.1	0.1
70.	1.6	1.7	1.1	0.8	0.6	0.6	0.9	1.5	2.0	1.7	0.0	0.1	0.4	0.4	0.3	0.2	0.3	0.4	0.1	0.0
80.	1.6	1.8	1.2	0.8	0.6	0.8	0.6	1.3	2.0	2.0	0.1	0.2	0.6	0.5	0.4	0.1	0.1	0.2	0.0	0.0
90.	1.6	1.5	1.3	0.8	0.6	0.8	0.8	1.1	2.0	2.0	0.1	0.2	0.7	0.6	0.4	0.0	0.0	0.0	0.0	0.0
100.	1.6	1.6	1.3	0.8	0.5	1.0	0.9	0.9	2.0	2.0	0.1	0.3	0.7	0.7	0.4	0.0	0.0	0.0	0.0	0.0
110.	1.8	1.7	1.1	0.7	0.5	1.0	1.1	1.0	2.0	2.1	0.1	0.3	0.6	0.6	0.3	0.0	0.0	0.0	0.0	0.0
120.	1.8	1.8	1.1	0.7	0.5	0.9	1.1	1.2	2.1	2.2	0.1	0.3	0.6	0.6	0.3	0.0	0.0	0.0	0.0	0.0

130.	*	2.1	1.7	1.2	0.7	0.5	0.9	1.4	1.4	2.2	2.3	0.2	0.4	0.6	0.6	0.4	0.0	0.0	0.0
0.0	0.0																		
140.	*	2.5	1.8	1.2	0.6	0.4	0.8	1.1	1.3	2.2	2.5	0.2	0.3	0.6	0.6	0.4	0.0	0.0	0.0
0.0	0.0																		
150.	*	3.3	1.8	1.1	0.6	0.4	0.7	1.1	1.4	1.9	2.6	0.2	0.3	0.6	0.6	0.5	0.0	0.0	0.0
0.0	0.0																		
160.	*	3.9	1.8	1.0	0.4	0.2	0.5	1.0	1.3	1.6	2.3	0.4	0.4	0.7	0.6	0.5	0.0	0.0	0.1
0.1	0.1																		
170.	*	4.1	1.3	0.6	0.3	0.1	0.4	0.6	0.9	1.2	1.6	0.5	0.6	0.9	0.6	0.6	0.0	0.0	0.2
0.2	0.2																		
180.	*	3.5	0.7	0.2	0.0	0.0	0.2	0.3	0.7	0.6	0.9	0.9	0.7	1.0	0.7	0.6	0.0	0.1	0.4
0.3	0.3																		
190.	*	2.6	0.3	0.0	0.0	0.0	0.2	0.3	0.5	0.2	0.3	0.7	0.7	1.0	0.8	0.7	0.0	0.1	0.5
0.4	0.3																		
200.	*	1.7	0.1	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	1.0	0.8	1.1	0.9	0.7	0.1	0.2	0.6
0.4	0.4																		
210.	*	1.2	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.1	0.0	0.9	0.7	0.8	0.9	0.7	0.1	0.2	0.7
0.4	0.4																		
220.	*	0.9	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.0	0.0	0.9	0.7	0.6	0.9	0.9	0.1	0.3	0.8
0.3	0.3																		
230.	*	0.9	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.8	0.8	0.5	0.7	0.9	0.1	0.3	0.8
0.3	0.3																		
240.	*	0.6	0.0	0.1	0.1	0.0	0.0	0.0	0.1	0.0	0.0	0.8	0.8	0.5	0.6	0.6	0.3	0.4	0.8
0.3	0.3																		
250.	*	0.6	0.0	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.7	0.5	0.6	0.4	0.5	0.8
0.3	0.3																		
260.	*	0.7	0.0	0.5	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.6	0.5	0.4	0.6	0.5	0.7
0.3	0.3																		
270.	*	0.6	0.0	0.6	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.7	0.5	0.3	0.9	0.6	0.6
0.3	0.3																		
280.	*	0.6	0.1	0.7	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.8	0.5	0.3	1.0	0.8	0.6
0.4	0.3																		
290.	*	0.7	0.3	0.8	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.8	0.8	0.8	0.5	0.4	0.9	0.8	0.6
0.5	0.3																		
300.	*	0.8	0.3	0.8	0.2	0.1	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	0.6	0.4	1.0	1.0	0.6
0.6	0.3																		
310.	*	1.2	0.4	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	0.6	0.4	1.0	1.1	1.1
0.8	0.5																		
320.	*	1.6	0.4	0.7	0.2	0.2	0.0	0.0	0.0	0.0	0.0	1.1	1.1	1.1	0.6	0.4	0.9	1.1	1.4
1.0	0.7																		
330.	*	2.5	0.3	0.7	0.2	0.2	0.0	0.0	0.0	0.0	0.0	1.0	1.1	1.1	0.5	0.3	0.9	1.1	1.6
1.2	0.8																		
340.	*	3.8	0.9	0.7	0.3	0.2	0.0	0.0	0.0	0.0	0.1	1.1	1.1	1.2	0.5	0.3	0.8	1.1	1.6
1.3	1.2																		
350.	*	4.8	1.8	1.2	0.4	0.3	0.1	0.1	0.5	0.3	0.4	0.6	0.7	0.7	0.3	0.2	0.7	0.8	1.3
1.1	1.0																		
360.	*	4.8	2.3	1.8	1.0	0.4	0.1	0.4	1.5	1.3	1.1	0.2	0.2	0.2	0.0	0.0	0.4	0.5	0.8
0.6	0.5																		
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
-------																			
MAX	*	4.8	2.4	1.9	1.6	1.1	1.0	1.4	2.3	2.3	2.6	1.1	1.1	1.2	0.9	0.9	1.0	1.1	1.6
1.3	1.2																		
DEGR.	*	0	10	10	10	30	100	130	20	30	150	320	320	340	200	220	280	310	330
340	340																		

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) * REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50
0.	* 1.0	1.0	1.2	0.6	0.4	0.4	0.6	1.4	1.4	1.2
10.	* 0.8	0.8	1.0	0.6	0.4	0.4	0.7	1.2	1.2	1.2
20.	* 0.9	0.8	0.8	0.6	0.4	0.4	0.6	1.2	1.2	1.2
30.	* 0.7	0.8	0.7	0.5	0.4	0.4	0.6	1.1	1.1	1.1
40.	* 0.5	0.9	0.6	0.3	0.3	0.4	0.6	0.9	0.9	0.9
50.	* 0.4	0.8	0.8	0.5	0.3	0.4	0.5	0.8	0.9	0.9
60.	* 0.4	0.7	1.0	0.6	0.5	0.4	0.6	0.9	0.9	0.9
70.	* 0.3	0.5	1.0	0.6	0.4	0.5	0.7	1.0	1.0	0.9
80.	* 0.3	0.3	0.7	0.5	0.4	0.6	0.6	0.9	1.1	1.0
90.	* 0.3	0.3	0.6	0.3	0.2	0.3	0.5	1.0	1.2	1.0
100.	* 0.3	0.3	0.5	0.3	0.1	0.2	0.5	0.6	1.2	1.0
110.	* 0.3	0.3	0.5	0.2	0.1	0.1	0.3	0.8	1.2	1.1
120.	* 0.3	0.3	0.4	0.2	0.1	0.1	0.3	0.6	1.1	1.2
130.	* 0.4	0.4	0.4	0.2	0.1	0.1	0.2	0.5	1.0	1.2
140.	* 0.3	0.4	0.4	0.2	0.1	0.1	0.2	0.5	0.8	1.1
150.	* 0.3	0.4	0.4	0.1	0.0	0.0	0.1	0.5	0.7	1.1
160.	* 0.2	0.3	0.3	0.0	0.0	0.0	0.1	0.4	0.5	0.6
170.	* 0.1	0.2	0.2	0.0	0.0	0.0	0.0	0.3	0.3	0.3

180.	*	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.1	0.1
190.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
200.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
210.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
220.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
230.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
240.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
250.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
260.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
270.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
280.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
290.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
300.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
310.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
320.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
330.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1
340.	*	0.4	0.4	0.4	0.1	0.0	0.0	0.1	0.4	0.4	0.4
350.	*	0.8	0.9	1.0	0.3	0.1	0.2	0.4	1.0	0.9	0.9
360.	*	1.0	1.0	1.2	0.6	0.4	0.4	0.6	1.4	1.4	1.2
------	*	----	----	----	----	----	----	----	----	----	----
MAX	*	1.0	1.0	1.2	0.6	0.5	0.6	0.7	1.4	1.4	1.2
DEGR.	*	0	0	0	0	60	80	70	0	0	0

THE HIGHEST CONCENTRATION OF 4.80 PPM OCCURRED AT RECEPTOR REC21.

♀ CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Build

DATE : 7/10/13
TIME : 15:35:51

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH (VEH)	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE
1.	Stan/Lom SB L	*	5194.4	5948.0	5120.9	6056.9	*	131.	326.	AG	79.	100.0	1.0	10.0	0.63	6.7
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5090.5	6056.1	*	145.	325.	AG	159.	100.0	1.0	20.0	0.70	7.4
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5368.6	5981.0	*	80.	51.	AG	143.	100.0	1.0	20.0	0.35	4.1
4.	Stan/Lom WB R	*	5292.4	5947.7	5403.8	6033.2	*	140.	52.	AG	79.	100.0	1.0	10.0	0.68	7.1
5.	Stan/Lom NB L	*	5307.6	5737.4	5341.6	5726.9	*	36.	107.	AG	94.	100.0	1.0	10.0	0.24	1.8
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5393.9	5738.4	*	84.	109.	AG	187.	100.0	1.0	20.0	0.56	4.3
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5171.4	5556.9	*	155.	196.	AG	195.	100.0	1.0	20.0	0.92	7.9
8.	Stan/Lom EB R	*	5236.5	5698.5	4944.8	4671.4	*	1068.	196.	AG	98.	100.0	1.0	10.0	1.34	54.2
9.	Char/93 SB LLTTRR	*	6587.8	5740.0	6580.8	5923.0	*	183.	358.	AG	299.	100.0	1.0	40.0	0.87	9.3
10.	Char/93 WB LTT	*	6702.8	5647.8	6737.0	5605.0	*	55.	141.	AG	145.	100.0	1.0	20.0	0.30	2.8
11.	Char/93 EB TTR	*	6560.8	5622.5	6458.6	5547.7	*	127.	234.	AG	217.	100.0	1.0	30.0	0.69	6.4
12.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1691.	8.3	1.0	90.0		
13.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1414.	8.3	1.0	78.0		
14.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	1247.	8.3	1.0	78.0		
15.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1387.	8.3	1.0	78.0		
16.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2091.	8.3	1.0	66.0		
17.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	334.	8.3	1.0	42.0		
18.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	1059.	8.3	1.0	48.0		
19.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	1159.	8.3	1.0	54.0		
20.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	499.	8.3	1.0	54.0		
21.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	414.	8.3	1.0	42.0		

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JOB: Government Center Garage RUN: Build

DATE : 7/10/13
TIME : 15:35:51

ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Stan/Lom SB L	*	120	79	3.0	304	1600	44.99	1	3
2.	Stan/Lom SB TRR	*	120	79	3.0	672	1600	44.99	1	3
3.	Stan/Lom WB LTT	*	120	71	3.0	412	1600	44.99	1	3
4.	Stan/Lom WB R	*	120	79	3.0	325	1600	44.99	1	3
5.	Stan/Lom NB L	*	120	93	3.0	70	1600	44.99	1	3
6.	Stan/Lom NB TRR	*	120	93	3.0	331	1600	44.99	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	439	1600	44.99	1	3
8.	Stan/Lom EB R	*	120	97	3.0	320	1600	44.99	1	3
9.	Char/93 SB LLTTRR	*	100	62	3.0	1842	1600	44.99	1	3
10.	Char/93 WB LTT	*	100	60	3.0	334	1600	44.99	1	3
11.	Char/93 EB TTR	*	100	60	3.0	1159	1600	44.99	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*

8.	Stan/Lom SE3	*	5261.7	5823.6	6.0 *
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0 *
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0 *
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0 *
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0 *
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0 *
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0 *
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0 *
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0 *
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0 *
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0 *
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0 *
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0 *
21.	Char/93 NE1	*	6625.0	5871.1	6.0 *
22.	Char/93 NE2	*	6627.1	5796.1	6.0 *
23.	Char/93 NE3	*	6629.1	5721.1	6.0 *
24.	Char/93 NE4	*	6699.8	5695.9	6.0 *
25.	Char/93 NE5	*	6750.6	5633.2	6.0 *
26.	Char/93 S1	*	6657.8	5466.0	6.0 *
27.	Char/93 S2	*	6614.7	5527.4	6.0 *
28.	Char/93 S3	*	6571.7	5588.8	6.0 *
29.	Char/93 S4	*	6512.9	5542.2	6.0 *
30.	Char/93 S5	*	6454.1	5495.6	6.0 *
31.	Char/93 NW1	*	6424.1	5632.5	6.0 *
32.	Char/93 NW2	*	6483.6	5678.2	6.0 *
33.	Char/93 NW3	*	6543.0	5723.9	6.0 *
34.	Char/93 NW4	*	6541.0	5798.8	6.0 *

♀ PAGE 3

JOB: Government Center Garage RUN: Build

DATE : 7/10/13
TIME : 15:35:51

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
35.	Char/93 NW5	*	6538.9	5873.8	6.0	*

♀ PAGE 4

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)

(DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	0.0	0.0	0.0	0.0	0.0	0.5	0.6	0.5	0.3	0.1	0.4	0.6	0.5	0.6	0.8	0.2	0.3	0.4	0.6	0.9
10. *	0.0	0.0	0.0	0.0	0.0	0.3	0.6	0.4	0.3	0.1	0.4	0.7	0.6	0.5	0.8	0.2	0.2	0.3	0.6	0.9
20. *	0.0	0.0	0.0	0.0	0.0	0.4	0.7	0.6	0.2	0.1	0.3	0.6	0.5	0.3	0.4	0.3	0.3	0.3	0.4	0.9
30. *	0.0	0.0	0.0	0.0	0.0	0.4	0.5	0.6	0.1	0.0	0.3	0.6	0.5	0.3	0.3	0.4	0.3	0.4	0.3	0.8
40. *	0.0	0.0	0.1	0.1	0.0	0.3	0.4	0.5	0.1	0.0	0.2	0.5	0.5	0.2	0.2	0.6	0.4	0.5	0.4	0.8
50. *	0.0	0.0	0.3	0.2	0.1	0.2	0.2	0.3	0.0	0.0	0.3	0.4	0.5	0.3	0.1	0.7	0.4	0.5	0.8	0.7
60. *	0.0	0.0	0.6	0.4	0.2	0.1	0.1	0.1	0.0	0.0	0.3	0.4	0.6	0.3	0.1	0.7	0.3	0.2	0.7	0.8
70. *	0.0	0.1	0.8	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.2	0.1	0.9	0.6	0.1	0.7	0.8
80. *	0.0	0.1	0.8	0.6	0.3	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.2	0.1	0.8	0.6	0.1	0.6	0.8
90. *	0.1	0.3	0.7	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.1	0.1	0.8	0.6	0.3	0.4	0.8
100. *	0.1	0.4	0.6	0.6	0.4	0.0	0.0	0.1	0.1	0.1	0.3	0.3	0.4	0.1	0.0	0.8	0.6	0.4	0.3	0.7
110. *	0.1	0.4	0.4	0.7	0.4	0.0	0.0	0.3	0.3	0.2	0.2	0.2	0.2	0.0	0.0	0.7	0.7	0.5	0.3	0.7
120. *	0.2	0.4	0.4	0.7	0.4	0.0	0.1	0.5	0.5	0.3	0.1	0.1	0.1	0.0	0.0	0.7	0.6	0.5	0.4	0.5
130. *	0.3	0.4	0.4	0.8	0.5	0.1	0.1	0.6	0.7	0.4	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.4	0.4	0.6
140. *	0.3	0.4	0.4	0.9	0.5	0.1	0.3	0.5	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.3	0.2	0.3
150. *	0.4	0.5	0.6	0.9	0.6	0.1	0.3	0.4	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.4		

0.2	0.3																		
160.	*	0.6	0.5	0.6	0.9	0.6	0.1	0.3	0.2	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.7	0.8	0.5
0.3	0.2																		
170.	*	0.7	0.6	0.6	1.0	0.6	0.2	0.4	0.3	0.8	0.3	0.0	0.0	0.0	0.0	0.0	0.6	0.8	0.7
0.4	0.3																		
180.	*	0.9	0.8	0.9	0.9	0.7	0.2	0.3	0.6	0.8	0.3	0.0	0.0	0.1	0.1	0.1	0.6	0.7	0.7
0.4	0.3																		
190.	*	0.9	0.7	0.8	1.1	0.7	0.2	0.4	0.6	0.9	0.5	0.0	0.0	0.3	0.3	0.3	0.4	0.5	0.6
0.4	0.2																		
200.	*	0.7	0.5	0.8	1.0	1.1	0.4	0.5	0.8	0.9	0.7	0.0	0.1	0.7	0.5	0.5	0.2	0.3	0.4
0.1	0.0																		
210.	*	0.6	0.5	0.6	0.7	0.9	0.4	0.5	0.5	0.9	0.9	0.1	0.2	0.9	0.7	0.6	0.1	0.1	0.1
0.0	0.0																		
220.	*	0.6	0.5	0.4	0.5	0.7	0.3	0.4	0.3	0.8	0.9	0.1	0.2	0.9	0.9	0.6	0.0	0.0	0.0
0.0	0.0																		
230.	*	0.6	0.6	0.5	0.3	0.5	0.2	0.1	0.1	0.7	1.0	0.2	0.4	1.0	1.0	0.6	0.0	0.0	0.0
0.0	0.0																		
240.	*	0.6	0.6	0.3	0.3	0.3	0.3	0.1	0.1	0.5	1.2	0.2	0.5	0.7	0.9	0.6	0.0	0.0	0.0
0.0	0.0																		
250.	*	0.5	0.6	0.3	0.3	0.2	0.4	0.2	0.0	0.3	1.1	0.3	0.5	0.7	0.9	0.6	0.0	0.0	0.0
0.0	0.0																		
260.	*	0.4	0.6	0.4	0.3	0.2	0.4	0.3	0.0	0.3	0.8	0.3	0.5	0.5	0.8	0.7	0.0	0.0	0.0
0.0	0.0																		
270.	*	0.5	0.7	0.6	0.4	0.2	0.6	0.4	0.0	0.2	0.7	0.2	0.4	0.4	0.8	0.8	0.0	0.0	0.0
0.0	0.0																		
280.	*	0.4	0.7	0.7	0.3	0.1	0.7	0.5	0.0	0.1	0.4	0.3	0.3	0.3	0.8	0.8	0.0	0.0	0.0
0.0	0.0																		
290.	*	0.4	0.6	0.7	0.3	0.1	0.8	0.7	0.1	0.2	0.3	0.2	0.3	0.3	0.8	0.8	0.0	0.0	0.0
0.0	0.0																		
300.	*	0.4	0.5	0.7	0.2	0.1	0.9	0.8	0.2	0.1	0.2	0.3	0.3	0.3	0.8	0.8	0.0	0.0	0.0
0.0	0.0																		
310.	*	0.4	0.4	0.7	0.1	0.0	0.7	0.8	0.4	0.5	0.4	0.5	0.4	0.4	0.8	0.9	0.0	0.0	0.0
0.1	0.1																		
320.	*	0.3	0.3	0.4	0.0	0.0	0.7	0.7	0.6	0.5	0.3	0.6	0.4	0.4	0.8	0.9	0.0	0.0	0.0
0.3	0.3																		
330.	*	0.1	0.2	0.2	0.0	0.0	0.6	0.5	0.7	0.5	0.2	0.7	0.8	0.6	0.9	0.9	0.0	0.0	0.2
0.6	0.5																		
340.	*	0.1	0.1	0.1	0.0	0.0	0.6	0.4	0.7	0.3	0.2	0.7	0.8	0.6	0.9	1.1	0.1	0.1	0.3
0.9	0.7																		
350.	*	0.0	0.0	0.0	0.0	0.0	0.5	0.5	0.5	0.3	0.2	0.5	0.8	0.6	0.8	1.0	0.1	0.3	0.4
0.8	1.0																		
360.	*	0.0	0.0	0.0	0.0	0.0	0.5	0.6	0.5	0.3	0.1	0.4	0.6	0.5	0.6	0.8	0.2	0.3	0.4
0.6	0.9																		
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
-------																			
MAX	*	0.9	0.8	0.9	1.1	1.1	0.9	0.8	0.8	0.9	1.2	0.7	0.8	1.0	1.0	1.1	0.9	0.8	0.7
0.9	1.0																		
DEGR.	*	180	180	180	190	200	300	300	200	190	240	330	330	230	230	340	70	160	170
340	350																		

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35
0.	*	0.1	0.3	0.4	0.0	0.0	0.4	0.5	0.9	1.1	0.6	0.0	0.0	0.6	0.3	0.1
10.	*	0.0	0.1	0.2	0.0	0.0	0.2	0.4	0.8	1.2	0.9	0.0	0.2	1.0	0.7	0.1
20.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	1.1	1.1	0.2	0.4	1.2	1.1	0.3
30.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.4	1.0	0.9	0.3	0.5	1.2	1.2	0.6
40.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.3	0.5	0.8	0.4	0.6	1.2	1.2	0.7
50.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.2	0.3	0.5	0.3	0.5	1.0	1.2	1.0
60.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.3	0.3	0.4	0.9	1.2	1.0
70.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.4	0.1	0.1	0.1	0.3	0.7	1.1	1.1
80.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.4	0.1	0.1	0.4	0.1	0.4	1.2	1.2
90.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.1	0.4	0.2	0.3	1.2	1.2
100.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.1	0.5	0.2	0.1	1.1	1.1
110.	*	0.0	0.0	0.1	0.0	0.0	0.2	0.3	0.3	0.1	0.0	0.7	0.4	0.1	1.1	1.1
120.	*	0.0	0.0	0.1	0.0	0.0	0.2	0.2	0.3	0.0	0.0	0.7	0.5	0.1	1.1	1.2
130.	*	0.0	0.0	0.2	0.0	0.0	0.1	0.2	0.2	0.0	0.0	0.6	0.5	0.2	1.1	1.3
140.	*	0.0	0.0	0.3	0.2	0.0	0.0	0.1	0.1	0.0	0.0	0.6	0.6	0.4	1.0	1.4
150.	*	0.0	0.2	0.4	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.5	0.6	0.4	0.8	1.3
160.	*	0.1	0.2	0.3	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.6	0.4	0.5	1.1
170.	*	0.3	0.1	0.2	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.6	0.3	0.5	0.8
180.	*	0.5	0.2	0.2	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.2	0.5	0.4	0.4	0.5
190.	*	1.1	0.5	0.2	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.4	0.5	0.3	0.3
200.	*	1.3	0.8	0.4	0.2	0.3	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.5	0.3	0.2
210.	*	1.5	1.0	0.4	0.2	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.4	0.1	0.0
220.	*	1.3	1.3	0.6	0.3	0.5	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.3	0.0	0.0

230.	*	1.2	1.2	0.6	0.4	0.5	0.0	0.0	0.2	0.1	0.0	0.0	0.1	0.1	0.0	0.0
240.	*	1.2	1.1	0.3	0.5	0.5	0.0	0.0	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.0
250.	*	1.1	1.1	0.1	0.5	0.7	0.0	0.0	0.7	0.3	0.0	0.0	0.0	0.0	0.0	0.0
260.	*	1.2	1.2	0.1	0.5	0.7	0.0	0.1	0.8	0.4	0.1	0.0	0.0	0.0	0.0	0.0
270.	*	1.2	1.2	0.1	0.1	0.7	0.0	0.2	1.0	0.6	0.1	0.0	0.0	0.0	0.0	0.0
280.	*	1.1	1.1	0.4	0.3	0.5	0.1	0.3	1.0	0.8	0.1	0.0	0.0	0.0	0.0	0.0
290.	*	1.1	1.1	0.6	0.4	0.5	0.2	0.3	1.0	0.8	0.2	0.0	0.0	0.0	0.0	0.0
300.	*	1.1	1.2	0.8	0.5	0.4	0.2	0.3	0.9	0.9	0.2	0.0	0.0	0.0	0.0	0.0
310.	*	1.0	1.3	1.0	0.6	0.4	0.2	0.3	0.9	0.9	0.2	0.0	0.0	0.0	0.0	0.0
320.	*	0.8	1.3	1.2	0.6	0.4	0.2	0.3	0.9	0.9	0.4	0.0	0.0	0.0	0.0	0.0
330.	*	0.6	1.2	1.3	0.5	0.3	0.4	0.2	0.8	0.9	0.4	0.0	0.0	0.0	0.0	0.0
340.	*	0.3	0.9	1.2	0.2	0.2	0.4	0.6	0.8	0.8	0.4	0.0	0.0	0.0	0.0	0.0
350.	*	0.1	0.6	0.9	0.0	0.0	0.5	0.5	0.8	0.9	0.5	0.0	0.0	0.2	0.1	0.0
360.	*	0.1	0.3	0.4	0.0	0.0	0.4	0.5	0.9	1.1	0.6	0.0	0.0	0.6	0.3	0.1
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
MAX	*	1.5	1.3	1.3	0.6	0.7	0.5	0.6	1.0	1.2	1.1	0.7	0.6	1.2	1.2	1.4
DEGR.	*	210	220	330	310	250	350	340	270	10	20	110	40	20	30	140

THE HIGHEST CONCENTRATION OF 1.50 PPM OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
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The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6042.8	5450.0	*	73.	290.	AG	275.	100.0	1.0	30.0	0.58	3.7
2.	Char/Merr WB	*	6250.4	5435.2	6335.4	5502.4	*	108.	52.	AG	268.	100.0	1.0	30.0	0.75	5.5
3.	Char/Merr NB R	*	6291.7	5369.7	6314.8	5354.0	*	28.	124.	AG	53.	100.0	1.0	10.0	0.14	1.4
4.	Char/Merr NB LTT	*	6280.4	5347.2	7349.2	4593.4	*	1308.	125.	AG	169.	100.0	1.0	20.0	1.25	66.4
5.	Char/Merr EB	*	6104.2	5362.2	6046.8	5340.9	*	61.	250.	AG	193.	100.0	1.0	20.0	0.58	3.1
6.	Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.8	*	108.	14.	AG	78.	100.0	1.0	10.0	0.71	5.5
7.	Char/Cam SB TR	*	5360.8	4833.5	5403.4	4971.2	*	144.	17.	AG	190.	100.0	1.0	20.0	0.95	7.3
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	145.	100.0	1.0	20.0	0.27	2.2
9.	Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	78.	100.0	1.0	10.0	0.60	4.7
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.5	4645.8	*	78.	179.	AG	190.	100.0	1.0	20.0	0.74	4.0
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5210.5	4740.8	*	92.	271.	AG	217.	100.0	1.0	30.0	0.57	4.7
12.	Sud/Merr SB L	*	6532.7	5210.3	6385.1	5315.4	*	181.	305.	AG	107.	100.0	1.0	10.0	1.08	9.2
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6484.5	5210.4	*	39.	300.	AG	148.	100.0	1.0	30.0	0.20	2.0
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6678.7	5059.8	*	117.	150.	AG	188.	100.0	1.0	30.0	0.60	5.9
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6472.1	5115.0	*	60.	239.	AG	367.	100.0	1.0	40.0	0.47	3.0
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	128.	100.0	1.0	20.0	0.34	3.3
17.	Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	84.	100.0	1.0	10.0	0.06	0.5
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6739.6	5238.0	*	59.	249.	AG	279.	100.0	1.0	30.0	0.49	3.0
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	945.	8.3	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1232.	8.3	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1619.	8.3	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1565.	8.3	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	1016.	8.3	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1651.	8.3	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	964.	8.3	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1759.	8.3	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	360.	8.3	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	541.	8.3	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	8.3	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	420.	8.3	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	8.3	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1848.	8.3	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1944.	8.3	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	579.	8.3	1.0	78.0		

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JOB: Government Center Garage RUN: 2028BD

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ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Char/Merr SB	*	100	76	3.0	530	1600	44.99	1	3
2.	Char/Merr WB	*	100	74	3.0	757	1600	44.99	1	3
3.	Char/Merr NB R	*	100	44	3.0	116	1600	44.99	1	3
4.	Char/Merr NB LTT	*	100	70	3.0	1002	1600	44.99	1	3

5.	Char/Merr EB	*	100	80	3.0	281	1600	44.99	1	3
6.	Char/Cam SB L	*	90	58	3.0	340	1600	44.99	1	3
7.	Char/Cam SB TR	*	90	71	3.0	472	1600	44.99	1	3
8.	Char/Cam WB LTTR	*	90	54	3.0	294	1600	44.99	1	3
9.	Char/Cam NB L	*	90	58	3.0	289	1600	44.99	1	3
10.	Char/Cam NB TR	*	90	71	3.0	367	1600	44.99	1	3
11.	Char/Cam EB TTTR	*	90	54	3.0	937	1600	44.99	1	3
12.	Sud/Merr SB L	*	100	89	3.0	104	1600	44.99	1	3
13.	Sud/Merr SB TTT	*	100	41	3.0	524	1600	44.99	1	3
14.	Sud/Merr NB TTTR	*	100	52	3.0	1232	1600	44.99	1	3
15.	Sud/Merr EB LTTR	*	100	76	3.0	579	1600	44.99	1	3
16.	Sud/Sur SB LTT	*	100	53	3.0	455	1600	44.99	1	3
17.	Sud/Sur SEB	*	100	70	3.0	26	1600	44.99	1	3
18.	Sud/Sur EB TTR	*	100	77	3.0	420	1600	44.99	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Char/Merr NE1	*	6063.7	5511.0	6.0	*
2.	Char/Merr NE2	*	6133.9	5484.8	6.0	*
3.	Char/Merr NE3	*	6204.2	5458.5	6.0	*
4.	Char/Merr NE4	*	6265.6	5501.5	6.0	*
5.	Char/Merr NE5	*	6327.1	5544.5	6.0	*
6.	Char/Merr SE1	*	6443.7	5491.9	6.0	*
7.	Char/Merr SE2	*	6382.2	5448.9	6.0	*
8.	Char/Merr SE3	*	6320.8	5405.9	6.0	*
9.	Char/Merr SE4	*	6380.5	5360.4	6.0	*
10.	Char/Merr SE5	*	6440.1	5315.0	6.0	*
11.	Char/Merr SW1	*	6332.0	5249.0	6.0	*
12.	Char/Merr SW2	*	6272.3	5294.5	6.0	*
13.	Char/Merr SW3	*	6212.6	5339.9	6.0	*
14.	Char/Merr SW4	*	6141.6	5315.8	6.0	*
15.	Char/Merr SW5	*	6070.6	5291.7	6.0	*
16.	Char/Merr NW1	*	5902.1	5359.1	6.0	*
17.	Char/Merr NW2	*	5973.1	5383.2	6.0	*
18.	Char/Merr NW3	*	6044.1	5407.3	6.0	*
19.	Char/Merr NW4	*	5973.9	5433.5	6.0	*
20.	Char/Merr NW5	*	5903.6	5459.8	6.0	*
21.	Char/Cam NE1	*	5490.2	4963.0	6.0	*
22.	Char/Cam NE2	*	5459.0	4894.8	6.0	*
23.	Char/Cam NE3	*	5427.8	4826.6	6.0	*
24.	Char/Cam NE4	*	5500.4	4807.6	6.0	*
25.	Char/Cam NE5	*	5572.9	4788.7	6.0	*
26.	Char/Cam SE1	*	5553.9	4667.5	6.0	*
27.	Char/Cam SE2	*	5481.3	4686.5	6.0	*

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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
28.	Char/Cam SE3	*	5408.7	4705.4	6.0	*
29.	Char/Cam SE4	*	5409.4	4630.4	6.0	*
30.	Char/Cam SE5	*	5410.1	4555.4	6.0	*
31.	Char/Cam SW1	*	5312.0	4561.9	6.0	*
32.	Char/Cam SW2	*	5310.7	4636.9	6.0	*
33.	Char/Cam SW3	*	5310.7	4711.9	6.0	*
34.	Char/Cam SW4	*	5235.6	4712.1	6.0	*
35.	Char/Cam SW5	*	5160.6	4711.9	6.0	*
36.	Char/Cam NW1	*	5167.9	4822.4	6.0	*
37.	Char/Cam NW2	*	5242.9	4822.1	6.0	*
38.	Char/Cam NW3	*	5317.9	4821.9	6.0	*
39.	Char/Cam NW4	*	5349.1	4890.1	6.0	*
40.	Char/Cam NW5	*	5380.3	4958.3	6.0	*

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JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) *	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----

0.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.2	0.1	0.8	0.8	0.6	0.5	0.9	0.1	0.1	0.5	0.2	0.2
10.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.2	0.1	0.8	0.9	0.5	0.4	0.9	0.1	0.1	0.7	0.2	0.2
20.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.1	0.1	0.7	0.8	0.8	0.5	0.7	0.1	0.1	0.7	0.2	0.2
30.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.1	0.0	0.7	0.9	0.9	0.6	0.5	0.1	0.2	0.8	0.2	0.2
40.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.0	0.7	0.7	0.9	0.7	0.7	0.1	0.2	0.8	0.2	0.2
50.	*	0.0	0.0	0.2	0.1	0.1	0.2	0.2	0.2	0.0	0.0	0.7	0.7	0.7	0.8	0.8	0.2	0.3	0.8	0.2	0.2
60.	*	0.0	0.1	0.5	0.2	0.2	0.1	0.1	0.1	0.0	0.1	0.8	0.6	0.5	0.6	0.6	0.4	0.6	1.0	0.3	0.2
70.	*	0.1	0.2	0.7	0.4	0.3	0.0	0.0	0.0	0.0	0.1	0.9	0.6	0.5	0.5	0.3	0.6	0.7	1.0	0.6	0.2
80.	*	0.1	0.3	0.8	0.5	0.3	0.0	0.0	0.0	0.0	0.1	0.8	0.8	0.5	0.3	0.3	0.9	0.8	1.1	0.7	0.5
90.	*	0.2	0.4	0.8	0.7	0.3	0.0	0.0	0.0	0.0	0.1	0.8	0.9	0.7	0.5	0.3	0.7	0.9	1.0	0.9	0.6
100.	*	0.2	0.4	0.9	0.8	0.3	0.0	0.0	0.0	0.0	0.2	0.9	1.0	0.9	0.4	0.5	0.7	0.7	0.9	1.0	0.8
110.	*	0.5	0.7	0.9	0.8	0.3	0.0	0.0	0.0	0.1	0.3	1.0	1.0	1.0	0.5	0.3	0.6	1.0	0.8	0.8	0.5
120.	*	1.0	1.0	1.1	0.9	0.2	0.0	0.0	0.4	0.4	0.6	0.9	0.9	1.0	0.4	0.2	0.4	0.6	0.8	0.7	0.6
130.	*	0.9	0.8	1.2	1.2	0.3	0.1	0.3	0.9	1.1	1.2	0.5	0.5	0.5	0.2	0.0	0.3	0.4	0.7	0.4	0.4
140.	*	0.6	0.9	1.2	1.4	0.6	0.2	0.4	1.1	1.2	1.3	0.3	0.3	0.2	0.0	0.0	0.3	0.3	0.5	0.3	0.2
150.	*	0.7	0.6	0.8	1.5	0.8	0.3	0.7	1.0	1.1	1.4	0.1	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.3	0.2
160.	*	0.9	0.4	0.6	1.2	0.8	0.3	0.7	0.7	1.0	1.4	0.1	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.2	0.2
170.	*	0.9	0.4	0.6	1.1	0.7	0.5	0.6	0.7	0.8	1.0	0.1	0.0	0.0	0.0	0.0	0.3	0.3	0.5	0.2	0.2
180.	*	0.9	0.4	0.5	1.1	1.0	0.3	0.4	0.5	0.6	1.1	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.2
190.	*	0.8	0.6	0.5	0.9	1.2	0.3	0.3	0.5	0.5	0.8	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.4	0.2	0.2
200.	*	0.6	0.7	0.5	0.7	1.0	0.2	0.3	0.5	0.5	0.8	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.1
210.	*	0.5	0.8	0.6	0.6	1.0	0.2	0.3	0.4	0.5	0.8	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1
220.	*	0.3	0.9	0.7	0.6	0.8	0.2	0.3	0.4	0.5	0.8	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.4	0.4	0.2	0.0
230.	*	0.3	0.8	0.7	0.5	0.7	0.3	0.4	0.3	0.5	0.8	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.4	0.1	0.0
240.	*	0.2	0.7	0.8	0.5	0.6	0.5	0.5	0.5	0.5	0.8	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.1	0.0
250.	*	0.2	0.6	0.7	0.3	0.3	0.7	0.7	0.7	0.6	0.8	0.0	0.0	0.2	0.2	0.2	0.1	0.2	0.2	0.0	0.0
260.	*	0.2	0.3	0.6	0.3	0.2	0.9	1.0	0.9	0.7	0.8	0.0	0.1	0.5	0.3	0.3	0.0	0.1	0.1	0.0	0.0
270.	*	0.2	0.4	0.5	0.2	0.1	0.6	1.0	0.9	0.9	0.9	0.1	0.2	0.5	0.5	0.4	0.0	0.0	0.0	0.0	0.0
280.	*	0.2	0.2	0.3	0.1	0.0	0.5	0.8	1.0	0.7	0.9	0.1	0.3	0.5	0.5	0.4	0.0	0.0	0.0	0.0	0.0
290.	*	0.1	0.1	0.2	0.0	0.0	0.4	0.7	0.9	0.8	0.8	0.2	0.4	0.7	0.6	0.4	0.0	0.0	0.1	0.1	0.0
300.	*	0.0	0.1	0.1	0.0	0.0	0.2	0.6	0.7	0.5	0.6	0.4	0.5	0.7	0.6	0.3	0.0	0.0	0.2	0.1	0.1
310.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.5	0.7	0.4	0.3	0.5	0.5	0.7	0.7	0.3	0.0	0.0	0.2	0.2	0.1
320.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.7	0.3	0.3	0.7	0.6	0.7	0.7	0.5	0.0	0.1	0.2	0.2	0.1
330.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.7	0.3	0.2	0.7	0.6	0.5	0.7	0.5	0.0	0.1	0.2	0.2	0.2
340.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.6	0.3	0.1	0.8	0.5	0.5	0.6	0.7	0.1	0.1	0.3	0.2	0.2
350.	*	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.6	0.3	0.1	0.9	0.6	0.4	0.5	0.8	0.1	0.1	0.4	0.2	0.2
360.	*	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.6	0.2	0.1	0.8	0.8	0.6	0.5	0.9	0.1	0.1	0.5	0.2	0.2
MAX	*	1.0	1.0	1.2	1.5	1.2	0.9	1.0	1.1	1.2	1.4	1.0	1.0	1.0	0.8	0.9	0.9	1.0	1.1	1.0	0.8
DEGR.	*	120	120	130	150	190	260	260	140	140	150	110	100	110	50	0	80	110	80	100	100

angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	*	0.1	0.2	0.4	0.0	0.0	0.3	0.4	0.7	0.6	0.5	0.3	0.6	0.7	1.0	0.4	0.0	0.0	0.0	0.0	0.0
10.	*	0.1	0.2	0.2	0.0	0.0	0.3	0.3	0.6	0.3	0.3	0.7	0.6	0.7	0.9	0.3	0.0	0.0	0.1	0.0	0.0
20.	*	0.0	0.1	0.2	0.0	0.0	0.3	0.3	0.5	0.2	0.1	0.8	0.6	1.0	0.9	0.3	0.0	0.0	0.3	0.2	0.0
30.	*	0.0	0.0	0.1	0.0	0.1	0.3	0.3	0.4	0.2	0.1	0.5	0.9	0.9	1.2	0.4	0.0	0.0	0.5	0.4	0.2
40.	*	0.0	0.0	0.0	0.1	0.1	0.3	0.3	0.3	0.2	0.1	0.4	0.6	0.9	1.3	0.7	0.0	0.2	0.8	0.6	0.3
50.	*	0.1	0.1	0.1	0.1	0.0	0.3	0.3	0.3	0.2	0.1	0.4	0.7	0.8	1.3	0.8	0.0	0.2	0.8	0.8	0.5
60.	*	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.7	0.8	1.2	1.0	0.2	0.3	0.7	1.0	0.6
70.	*	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.7	0.7	1.0	1.0	0.2	0.3	0.6	0.8	0.6
80.	*	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.2	0.1	0.3	0.6	0.8	0.8	0.8	0.4	0.3	0.5	0.8	0.7
90.	*	0.1	0.0	0.1	0.1	0.0	0.3	0.4	0.4	0.1	0.0	0.2	0.5	0.8	0.6	0.8	0.5	0.5	0.6	0.8	0.7
100.	*	0.0	0.0	0.2	0.1	0.1	0.2	0.3	0.3	0.0	0.0	0.2	0.2	0.7	0.4	0.5	0.6	0.6	0.8	0.7	0.7
110.	*	0.0	0.0	0.3	0.3	0.2	0.1	0.1	0.2	0.0	0.0	0.2	0.2	0.6	0.3	0.1	0.7	0.7	0.9	0.8	0.8
120.	*	0.0	0.1	0.4	0.4	0.3	0.0	0.1	0.1	0.0	0.0	0.2	0.2	0.5	0.2	0.1	0.9	0.7	0.9	0.9	1.0
130.	*	0.1	0.2	0.4	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.1	0.1	0.7	0.8	0.9	1.2	1.0
140.	*	0.1	0.2	0.5	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.1	0.7	0.8	0.8	1.1	1.1
150.	*	0.1	0.2	0.6	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.0	0.7	0.7	0.9	1.1	1.1
160.	*	0.1	0.2	0.5	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.1	0.0	0.4	0.7	0.9	1.0	1.2
170.	*	0.1	0.2	0.6	0.3	0.3	0.0	0.0	0.1	0.1	0.0	0.2	0.2	0.2	0.0	0.0	0.3	0.7	0.8	1.0	1.4
180.	*	0.1	0.3	0.8	0.3	0.3	0.0	0.0	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.4	0.7	0.8	0.9	1.4
190.	*	0.2	0.5	0.7	0.3	0.3	0.0	0.0	0.4	0.2	0.2	0.0	0.0	0.1	0.0	0.0	0.3	0.5	0.5	0.7	1.0
200.	*	0.3	0.6	0.8	0.4	0.3	0.0	0.1	0.6	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.5	0.5	0.7
210.	*	0.5	0.7	0.8	0.5	0.4	0.0	0.1	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.5	0.7	0.3	0.4
220.	*	0.7	0.7	0.7	0.5	0.4	0.1	0.1	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.7	0.3	0.3
230.	*	0.8	0.8	0.8	0.6	0.5	0.1	0.1	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.3	0.2
240.	*	0.7	0.9	0.9	0.9	0.6	0.1	0.2	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.5	0.2	0.1
250.	*	0.5	0.7	0.8	0.9	0.7	0.1	0.2	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.3	0.4	0.5	0.2	0.1
260.	*	0.4	0.6	0.8	0.8	0.7	0.2	0.3	1.0	0.2	0.2	0.0	0.0	0.2	0.1	0.1	0.3	0.3	0.4	0.1	0.0
270.	*	0.3	0.5	0.6	0.7	0.8	0.3	0.6	1.1	0.2	0.2	0.0	0.0	0.4	0.2	0.1	0.2	0.2	0.2	0.0	0.0
280.	*	0.3	0.5	0.7	0.5	0.5	0.5	0.7	1.3	0.5	0.2	0.0	0.0	0.8	0.3	0.3	0.1	0.1	0.1	0.0	0.0
290.	*	0.2	0.5	0.5	0.3	0.3	0.8	0.7	1.4	0.6	0.2	0.0	0.1	1.0	0.5	0.3	0.0	0.0	0.0	0.0	0.0
300.	*	0.2	0.5	0.5	0.3	0.2	0.4	0.8	1.1	0.8	0.3	0.1	0.2	1.0	0.6	0.4	0.0	0.0	0.0	0.0	0.0
310.	*	0.2	0.5	0.6	0.4	0.2	0.7	0.5	0.9	0.9	0.4	0.1	0.3	1.0	0.7	0.4	0.0	0.0	0.0	0.0	0.0
320.	*	0.2	0.4	0.6	0.2	0.2	0.6	0.8	0.8	1.0	0.4	0.1	0.4	0.9	0.8	0.4	0.0	0.0	0.0	0.0	0.0
330.	*	0.2	0.3	0.6	0.2	0.1	0.6	0.7	0.8	1.1	0.6	0.2	0.4	0.9	0.8	0.4	0.0	0.0	0.0	0.0	0.0
340.	*	0.1	0.2	0.5	0.1	0.0	0.4	0.6	0.7	1.0	0.6	0.2	0.4	0.6	0.8	0.3	0.0	0.0	0.0	0.0	0.0
350.	*	0.1	0.2	0.6	0.1	0.0	0.3	0.6	0.8	0.9	0.8	0.2	0.4	0.5	0.9	0.3	0.0	0.0	0.0	0.0	0.0
360.	*	0.1	0.2	0.4	0.0	0.0	0.3	0.4	0.7	0.6	0.5	0.3	0.6	0.7	1.0	0.4	0.0	0.0	0.0	0.0	0.0
MAX	*	0.8	0.9	0.9	0.9	0.8	0.8	0.8	1.4	1.1	0.8	0.8	0.9	1.0	1.3	1.0	0.9	0.8	0.9	1.2	1.4

DEGR. * 230 240 240 240 270 290 320 290 330 350 20 30 20 40 60 120 130 110
130 170

THE HIGHEST CONCENTRATION OF 1.50 PPM OCCURRED AT RECEPTOR REC4 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15:15

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6030.2	5454.5	*	87.	290.	AG	275.	100.0	1.0	30.0	0.67	4.4
2. Char/Merr WB	*	6250.4	5435.2	6310.4	5482.7	*	77.	52.	AG	286.	100.0	1.0	30.0	0.67	3.9
3. Char/Merr NB R	*	6291.7	5369.7	6352.1	5328.7	*	73.	124.	AG	63.	100.0	1.0	10.0	0.37	3.7
4. Char/Merr NB LTT	*	6280.4	5347.2	6430.9	5241.1	*	184.	125.	AG	176.	100.0	1.0	20.0	0.94	9.4
5. Char/Merr EB	*	6104.2	5362.2	5936.5	5299.8	*	179.	250.	AG	174.	100.0	1.0	20.0	0.92	9.1
6. Char/Cam SB L	*	5384.1	4834.2	5402.6	4908.3	*	76.	14.	AG	72.	100.0	1.0	10.0	0.42	3.9
7. Char/Cam SB TR	*	5360.8	4833.5	5378.3	4889.9	*	59.	17.	AG	174.	100.0	1.0	20.0	0.41	3.0
8. Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	150.	100.0	1.0	20.0	0.41	3.7
9. Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	72.	100.0	1.0	10.0	0.53	5.0
10. Char/Cam NB TR	*	5383.3	4723.8	5385.0	4612.7	*	111.	179.	AG	174.	100.0	1.0	20.0	0.74	5.6
11. Char/Cam EB TTTR	*	5302.7	4739.8	5209.4	4740.8	*	93.	271.	AG	224.	100.0	1.0	30.0	0.52	4.7
12. Sud/Merr SB L	*	6532.7	5210.3	6461.3	5261.1	*	88.	305.	AG	106.	100.0	1.0	10.0	0.95	4.5
13. Sud/Merr SB TTT	*	6518.3	5190.8	6482.6	5211.5	*	41.	300.	AG	188.	100.0	1.0	30.0	0.21	2.1
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6684.5	5049.5	*	128.	150.	AG	232.	100.0	1.0	30.0	0.73	6.5
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6447.8	5100.4	*	88.	239.	AG	314.	100.0	1.0	40.0	0.52	4.5
16. Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	169.	100.0	1.0	20.0	0.53	4.1
17. Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	97.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6703.4	5223.8	*	98.	249.	AG	181.	100.0	1.0	30.0	0.50	5.0
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	989.	8.3	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1538.	8.3	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1494.	8.3	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1409.	8.3	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	921.	8.3	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1615.	8.3	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1034.	8.3	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1697.	8.3	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	1032.	8.3	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	504.	8.3	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	8.3	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	1075.	8.3	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	8.3	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1457.	8.3	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1759.	8.3	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	992.	8.3	1.0	78.0		

DATE : 8/ 7/13
TIME : 17:15:15

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. Char/Merr SB	*	100	76	3.0	615	1600	44.99	1	3
2. Char/Merr WB	*	100	79	3.0	517	1600	44.99	1	3
3. Char/Merr NB R	*	100	52	3.0	257	1600	44.99	1	3
4. Char/Merr NB LTT	*	100	73	3.0	660	1600	44.99	1	3

5. Char/Merr EB	*	100	72	3.0	679	1600	44.99	1	3
6. Char/Cam SB L	*	100	60	3.0	233	1600	44.99	1	3
7. Char/Cam SB TR	*	100	72	3.0	301	1600	44.99	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	435	1600	44.99	1	3
9. Char/Cam NB L	*	100	60	3.0	299	1600	44.99	1	3
10. Char/Cam NB TR	*	100	72	3.0	543	1600	44.99	1	3
11. Char/Cam EB TTTR	*	100	62	3.0	827	1600	44.99	1	3
12. Sud/Merr SB L	*	100	88	3.0	106	1600	44.99	1	3
13. Sud/Merr SB TTT	*	100	52	3.0	435	1600	44.99	1	3
14. Sud/Merr NB TTTR	*	100	64	3.0	1094	1600	44.99	1	3
15. Sud/Merr EB LTTR	*	100	65	3.0	992	1600	44.99	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	424	1600	44.99	1	3
17. Sud/Sur SEB	*	100	80	3.0	37	1600	44.99	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	1075	1600	44.99	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Char/Merr NE1	*	6063.7	5511.0	6.0	*
2. Char/Merr NE2	*	6133.9	5484.8	6.0	*
3. Char/Merr NE3	*	6204.2	5458.5	6.0	*
4. Char/Merr NE4	*	6265.6	5501.5	6.0	*
5. Char/Merr NE5	*	6327.1	5544.5	6.0	*
6. Char/Merr SE1	*	6443.7	5491.9	6.0	*
7. Char/Merr SE2	*	6382.2	5448.9	6.0	*
8. Char/Merr SE3	*	6320.8	5405.9	6.0	*
9. Char/Merr SE4	*	6380.5	5360.4	6.0	*
10. Char/Merr SE5	*	6440.1	5315.0	6.0	*
11. Char/Merr SW1	*	6332.0	5249.0	6.0	*
12. Char/Merr SW2	*	6272.3	5294.5	6.0	*
13. Char/Merr SW3	*	6212.6	5339.9	6.0	*
14. Char/Merr SW4	*	6141.6	5315.8	6.0	*
15. Char/Merr SW5	*	6070.6	5291.7	6.0	*
16. Char/Merr NW1	*	5902.1	5359.1	6.0	*
17. Char/Merr NW2	*	5973.1	5383.2	6.0	*
18. Char/Merr NW3	*	6044.1	5407.3	6.0	*
19. Char/Merr NW4	*	5973.9	5433.5	6.0	*
20. Char/Merr NW5	*	5903.6	5459.8	6.0	*
21. Char/Cam NE1	*	5490.2	4963.0	6.0	*
22. Char/Cam NE2	*	5459.0	4894.8	6.0	*
23. Char/Cam NE3	*	5427.8	4826.6	6.0	*
24. Char/Cam NE4	*	5500.4	4807.6	6.0	*
25. Char/Cam NE5	*	5572.9	4788.7	6.0	*
26. Char/Cam SE1	*	5553.9	4667.5	6.0	*
27. Char/Cam SE2	*	5481.3	4686.5	6.0	*

DATE : 8/ 7/13
TIME : 17:15:15

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
28. Char/Cam SE3	*	5408.7	4705.4	6.0	*
29. Char/Cam SE4	*	5409.4	4630.4	6.0	*
30. Char/Cam SE5	*	5410.1	4555.4	6.0	*
31. Char/Cam SW1	*	5312.0	4561.9	6.0	*
32. Char/Cam SW2	*	5310.7	4636.9	6.0	*
33. Char/Cam SW3	*	5310.7	4711.9	6.0	*
34. Char/Cam SW4	*	5235.6	4712.1	6.0	*
35. Char/Cam SW5	*	5160.6	4711.9	6.0	*
36. Char/Cam NW1	*	5167.9	4822.4	6.0	*
37. Char/Cam NW2	*	5242.9	4822.1	6.0	*
38. Char/Cam NW3	*	5317.9	4821.9	6.0	*
39. Char/Cam NW4	*	5349.1	4890.1	6.0	*
40. Char/Cam NW5	*	5380.3	4958.3	6.0	*

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

| | | |

BD_3p

DEGR. * 220 240 190 250 250 310 300 290 300 340 20 30 290 40 70 120 130 110
130 180

THE HIGHEST CONCENTRATION OF 1.50 PPM OCCURRED AT RECEPTOR REC4 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15:34

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6042.8	5450.0	*	73.	290.	AG	275.	100.0	1.0	30.0	0.58
2.	Char/Merr WB	*	6250.4	5435.2	6335.4	5502.4	*	108.	52.	AG	268.	100.0	1.0	30.0	0.75
3.	Char/Merr NB R	*	6291.7	5369.7	6314.8	5354.0	*	28.	124.	AG	53.	100.0	1.0	10.0	0.14
4.	Char/Merr NB LTT	*	6280.4	5347.2	7349.2	4593.4	*	1308.	125.	AG	169.	100.0	1.0	20.0	1.25
5.	Char/Merr EB	*	6104.2	5362.2	6046.8	5340.9	*	61.	250.	AG	193.	100.0	1.0	20.0	0.58
6.	Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.8	*	108.	14.	AG	78.	100.0	1.0	10.0	0.71
7.	Char/Cam SB TR	*	5360.8	4833.5	5403.4	4971.2	*	144.	17.	AG	190.	100.0	1.0	20.0	0.95
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	145.	100.0	1.0	20.0	0.27
9.	Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	78.	100.0	1.0	10.0	0.60
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.5	4645.8	*	78.	179.	AG	190.	100.0	1.0	20.0	0.74
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5210.5	4740.8	*	92.	271.	AG	217.	100.0	1.0	30.0	0.57
12.	Sud/Merr SB L	*	6532.7	5210.3	6385.1	5315.4	*	181.	305.	AG	107.	100.0	1.0	10.0	1.08
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6484.5	5210.4	*	39.	300.	AG	148.	100.0	1.0	30.0	0.20
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6678.7	5059.8	*	117.	150.	AG	188.	100.0	1.0	30.0	0.60
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6472.1	5115.0	*	60.	239.	AG	367.	100.0	1.0	40.0	0.47
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	128.	100.0	1.0	20.0	0.34
17.	Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	84.	100.0	1.0	10.0	0.06
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6739.6	5238.0	*	59.	249.	AG	279.	100.0	1.0	30.0	0.49
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	945.	8.3	1.0	84.0	
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1232.	8.3	1.0	90.0	
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1619.	8.3	1.0	98.0	
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1565.	8.3	1.0	98.0	
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	1016.	8.3	1.0	78.0	
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1651.	8.3	1.0	****	
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	964.	8.3	1.0	78.0	
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1759.	8.3	1.0	90.0	
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	360.	8.3	1.0	30.0	
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	541.	8.3	1.0	54.0	
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	8.3	1.0	42.0	
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	420.	8.3	1.0	54.0	
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	8.3	1.0	42.0	
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1848.	8.3	1.0	98.0	
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1944.	8.3	1.0	90.0	
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	579.	8.3	1.0	78.0	

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JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
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ADDITIONAL QUEUE LINK PARAMETERS

	LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1.	Char/Merr SB	*	100	76	3.0	530	1600	44.99	1	3
2.	Char/Merr WB	*	100	74	3.0	757	1600	44.99	1	3
3.	Char/Merr NB R	*	100	44	3.0	116	1600	44.99	1	3
4.	Char/Merr NB LTT	*	100	70	3.0	1002	1600	44.99	1	3

5. Char/Merr EB	*	100	80	3.0	281	1600	44.99	1	3
6. Char/Cam SB L	*	90	58	3.0	340	1600	44.99	1	3
7. Char/Cam SB TR	*	90	71	3.0	472	1600	44.99	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	294	1600	44.99	1	3
9. Char/Cam NB L	*	90	58	3.0	289	1600	44.99	1	3
10. Char/Cam NB TR	*	90	71	3.0	367	1600	44.99	1	3
11. Char/Cam EB TTTR	*	90	54	3.0	937	1600	44.99	1	3
12. Sud/Merr SB L	*	100	89	3.0	104	1600	44.99	1	3
13. Sud/Merr SB TTT	*	100	41	3.0	524	1600	44.99	1	3
14. Sud/Merr NB TTTR	*	100	52	3.0	1232	1600	44.99	1	3
15. Sud/Merr EB LTTR	*	100	76	3.0	579	1600	44.99	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	455	1600	44.99	1	3
17. Sud/Sur SEB	*	100	70	3.0	26	1600	44.99	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	420	1600	44.99	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Sud/Merr NE1	*	6492.5	5309.9	6.0	*
2.	Sud/Merr NE2	*	6554.8	5268.0	6.0	*
3.	Sud/Merr NE3	*	6616.2	5224.9	6.0	*
4.	Sud/Merr NE4	*	6684.7	5255.3	6.0	*
5.	Sud/Merr NE5	*	6753.3	5285.7	6.0	*
6.	Sud/Merr SE1	*	6792.9	5222.3	6.0	*
7.	Sud/Merr SE2	*	6724.3	5191.9	6.0	*
8.	Sud/Merr SE3	*	6655.7	5161.5	6.0	*
9.	Sud/Merr SE4	*	6695.5	5097.9	6.0	*
10.	Sud/Merr SE5	*	6735.2	5034.3	6.0	*
11.	Sud/Merr SW1	*	6638.6	4981.3	6.0	*
12.	Sud/Merr SW2	*	6598.9	5045.0	6.0	*
13.	Sud/Merr SW3	*	6559.1	5108.6	6.0	*
14.	Sud/Merr SW4	*	6493.4	5072.5	6.0	*
15.	Sud/Merr SW5	*	6427.6	5036.5	6.0	*
16.	Sud/Merr NW1	*	6347.8	5104.5	6.0	*
17.	Sud/Merr NW2	*	6413.5	5140.5	6.0	*
18.	Sud/Merr NW3	*	6479.3	5176.6	6.0	*
19.	Sud/Merr NW4	*	6417.1	5218.5	6.0	*
20.	Sud/Merr NW5	*	6354.9	5260.4	6.0	*
21.	Sud/Sur NE1	*	6755.9	5445.7	6.0	*
22.	Sud/Sur NE2	*	6801.0	5385.7	6.0	*
23.	Sud/Sur NE3	*	6846.0	5325.7	6.0	*
24.	Sud/Sur NE4	*	6908.8	5366.8	6.0	*
25.	Sud/Sur NE5	*	6971.5	5407.9	6.0	*
26.	Sud/Sur SE1	*	7002.4	5368.4	6.0	*
27.	Sud/Sur SE2	*	6939.7	5327.3	6.0	*

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JOB: Government Center Garage RUN: 2028BD

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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
28.	Sud/Sur SE3	*	6876.9	5286.2	6.0	*
29.	Sud/Sur SE4	*	6931.7	5235.0	6.0	*
30.	Sud/Sur SE5	*	6986.5	5183.8	6.0	*
31.	Sud/Sur SW1	*	6932.3	5133.1	6.0	*
32.	Sud/Sur SE2	*	6877.5	5184.3	6.0	*
33.	Sud/Sur SE3	*	6822.7	5235.5	6.0	*
34.	Sud/Sur SE4	*	6754.2	5205.1	6.0	*
35.	Sud/Sur SE5	*	6685.6	5174.8	6.0	*
36.	Sud/Sur NW1	*	6645.5	5237.9	6.0	*
37.	Sud/Sur NW2	*	6714.1	5268.3	6.0	*
38.	Sud/Sur NW3	*	6782.7	5298.7	6.0	*
39.	Sud/Sur NW4	*	6709.5	5315.4	6.0	*
40.	Sud/Sur NW5	*	6636.4	5332.0	6.0	*
41.	Sud/Sur N1	*	6642.4	5493.7	6.0	*
42.	Sud/Sur N2	*	6687.4	5433.7	6.0	*
43.	Sud/Sur N3	*	6732.4	5373.8	6.0	*
44.	Sud/Sur N4	*	6659.3	5390.4	6.0	*
45.	Sud/Sur N5	*	6586.2	5407.1	6.0	*

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JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.1	0.0	0.0	0.0	0.2	0.6	0.2	0.1	0.0	0.2	0.9	0.9	1.0	1.4	0.5	0.4	0.6	1.1	1.0	1.0
10.	*	0.1	0.0	0.0	0.0	0.2	0.3	0.3	0.1	0.1	0.2	0.9	0.8	0.9	1.4	0.5	0.3	0.7	1.0	0.9	0.9
20.	*	0.0	0.0	0.0	0.1	0.2	0.2	0.4	0.1	0.1	0.1	0.9	0.8	0.9	1.2	0.5	0.3	0.5	1.1	0.9	0.9
30.	*	0.0	0.0	0.0	0.1	0.1	0.2	0.5	0.2	0.1	0.0	0.8	1.0	1.0	0.9	0.6	0.3	0.5	1.2	0.9	0.9
40.	*	0.0	0.0	0.0	0.0	0.1	0.2	0.5	0.2	0.1	0.0	0.7	1.0	1.0	0.8	0.7	0.4	0.6	1.2	0.9	0.8
50.	*	0.0	0.0	0.0	0.0	0.1	0.1	0.4	0.3	0.0	0.0	0.6	1.0	1.1	0.7	0.6	0.3	0.6	1.2	0.8	0.9
60.	*	0.0	0.0	0.1	0.0	0.0	0.1	0.3	0.3	0.0	0.1	0.6	0.8	1.2	0.6	0.6	0.4	0.5	1.1	0.9	0.9
70.	*	0.0	0.0	0.2	0.1	0.0	0.1	0.2	0.1	0.0	0.1	0.6	0.9	1.0	0.5	0.4	0.6	0.9	1.2	0.9	1.0
80.	*	0.0	0.1	0.3	0.4	0.0	0.1	0.1	0.0	0.0	0.1	0.6	0.8	1.1	0.5	0.4	0.7	0.9	1.5	1.1	1.2
90.	*	0.0	0.1	0.2	0.6	0.1	0.1	0.1	0.0	0.0	0.2	0.6	0.8	1.1	0.5	0.4	0.8	1.2	1.3	1.2	1.2
100.	*	0.1	0.1	0.2	0.6	0.3	0.1	0.0	0.0	0.0	0.4	0.6	0.7	1.1	0.5	0.4	0.7	1.1	1.4	1.3	1.2
110.	*	0.1	0.2	0.1	0.5	0.4	0.1	0.0	0.0	0.1	0.8	0.7	0.8	1.2	0.4	0.2	0.4	1.1	1.4	1.5	1.5
120.	*	0.3	0.3	0.2	0.3	0.5	0.1	0.0	0.1	0.2	1.2	0.7	0.7	1.0	0.4	0.2	0.3	0.8	1.5	1.5	1.3
130.	*	0.7	0.7	0.4	0.3	0.6	0.0	0.1	0.3	0.4	1.4	0.5	0.6	0.8	0.2	0.0	0.1	0.4	1.4	1.1	1.0
140.	*	1.0	0.7	0.6	0.2	0.7	0.1	0.2	0.4	0.6	1.4	0.3	0.4	0.5	0.1	0.0	0.1	0.1	1.1	0.6	0.6
150.	*	1.0	1.0	0.9	0.3	0.8	0.1	0.2	0.7	0.8	1.3	0.2	0.2	0.2	0.0	0.0	0.1	0.1	0.9	0.3	0.3
160.	*	1.1	0.9	1.1	0.4	0.8	0.1	0.3	1.1	0.8	1.3	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.8	0.2	0.2
170.	*	1.1	0.8	1.1	0.6	0.9	0.1	0.4	1.2	0.9	1.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.8	0.1	0.1
180.	*	1.1	0.9	1.0	0.5	0.8	0.2	0.4	1.3	1.0	1.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.7	0.1	0.0
190.	*	1.0	0.9	0.8	0.7	0.8	0.2	0.5	1.2	1.0	1.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.5	0.1	0.0
200.	*	0.9	1.2	0.7	0.6	0.8	0.3	0.5	1.1	0.9	0.9	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.4	0.1	0.0
210.	*	0.7	1.1	0.9	0.5	0.7	0.4	0.6	1.1	1.0	0.9	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.3	0.1	0.0
220.	*	0.7	1.0	1.0	0.6	0.6	0.4	0.6	1.1	1.1	0.9	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.0
230.	*	0.7	0.8	1.0	0.7	0.5	0.4	0.6	1.1	1.1	0.9	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0
240.	*	0.7	0.8	0.9	0.6	0.6	0.4	0.7	1.3	1.2	1.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.0	0.1
250.	*	0.7	0.7	0.9	0.6	0.4	0.6	0.8	1.4	1.3	1.0	0.0	0.0	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1
260.	*	0.8	0.8	0.8	0.4	0.2	0.6	0.9	1.4	1.5	1.1	0.0	0.0	0.4	0.1	0.1	0.0	0.0	0.0	0.0	0.1
270.	*	0.8	0.8	1.0	0.6	0.4	0.6	0.6	1.4	1.5	1.3	0.0	0.1	0.6	0.1	0.1	0.0	0.0	0.0	0.1	0.2
280.	*	0.7	0.9	0.9	0.5	0.4	0.8	0.9	1.5	1.6	1.7	0.0	0.1	0.7	0.1	0.1	0.0	0.1	0.1	0.2	0.2
290.	*	0.8	0.8	0.7	0.3	0.1	0.8	0.5	1.4	1.9	2.1	0.0	0.3	0.8	0.2	0.1	0.1	0.1	0.3	0.3	0.4
300.	*	0.3	0.5	0.7	0.2	0.1	0.8	0.3	1.1	1.8	2.5	0.2	0.5	1.2	0.2	0.2	0.1	0.1	0.7	0.7	0.7
310.	*	0.2	0.3	0.3	0.1	0.1	0.9	0.2	0.9	1.4	2.2	0.3	0.8	1.1	0.4	0.2	0.1	0.3	0.8	0.9	1.0
320.	*	0.2	0.2	0.1	0.1	0.1	0.8	0.2	0.4	0.8	1.6	0.6	1.0	1.5	0.5	0.2	0.2	0.2	1.2	1.2	1.1
330.	*	0.1	0.1	0.1	0.1	0.0	0.7	0.1	0.3	0.2	0.8	0.7	1.2	1.6	1.0	0.3	0.2	0.5	1.4	1.2	1.1
340.	*	0.1	0.1	0.1	0.0	0.1	0.8	0.1	0.1	0.1	0.4	0.8	1.0	1.4	1.2	0.5	0.4	0.6	1.2	1.2	1.1
350.	*	0.1	0.1	0.0	0.0	0.2	0.8	0.1	0.1	0.0	0.2	0.9	0.8	1.1	1.4	0.4	0.5	0.7	1.2	1.2	1.0
360.	*	0.1	0.0	0.0	0.0	0.2	0.6	0.2	0.1	0.0	0.2	0.9	0.9	1.0	1.4	0.5	0.4	0.6	1.1	1.0	1.0
MAX	*	1.1	1.2	1.1	0.7	0.9	0.9	0.9	1.5	1.9	2.5	0.9	1.2	1.6	1.4	0.7	0.8	1.2	1.5	1.5	1.5
DEGR.	*	160	200	160	190	170	310	260	280	290	300	0	330	330	0	40	90	90	80	120	110

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.9	0.1	0.0	0.1	0.2	0.1	0.0
10.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.8	0.1	0.0	0.2	0.1	0.2	0.0
20.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.2	0.7	0.2	0.0	0.2	0.1	0.2	0.0
30.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.2	0.6	0.2	0.0	0.1	0.1	0.2	0.0
40.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.2	0.5	0.3	0.0	0.0	0.1	0.2	0.0
50.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.3	0.4	0.0	0.0	0.1	0.2	0.1
60.	*	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.3	0.1	0.0	0.1	0.1	0.1
70.	*	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.1	0.1	0.1	0.1
80.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.3	0.3	0.1	0.0
90.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.3	0.5	0.1	0.0
100.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.1	0.0	0.2	0.7	0.1	0.0
110.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.0	0.0	0.2	0.7	0.1	0.2	0.1
120.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.1	0.1	0.7	0.1	0.3	0.1
130.	*	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.6	0.1	0.5	0.2
140.	*	0.0	0.1	0.2	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.3	0.5	0.3	0.5	0.2
150.	*	0.4	0.2	0.3	0.1	0.0	0.0	0.0	0.3	0.2	0.2	0.1	0.1	0.1	0.2	0.3	0.4	0.4	0.4	0.5	0.2
160.	*	0.5	0.3	0.3	0.2	0.1	0.1	0.1	0.3	0.3	0.2	0.1	0.1	0.1	0.2	0.4	0.6	0.4	0.5	0.4	0.3
170.	*	0.5	0.3	0.3	0.3	0.1	0.1	0.2	0.3	0.2	0.2	0.1	0.1	0.1	0.3	0.6	0.8	0.3	0.6	0.4	0.4
180.	*	0.7	0.4	0.3	0.3	0.1	0.1	0.2	0.2	0.2	0.2	0.1	0.1	0.2	0.3	0.7	1.0	0.5	0.8	0.5	0.4
190.	*	0.7	0.5	0.4	0.3	0.2	0.1	0.2	0.3	0.2	0.2	0.1	0.2	0.2	0.3	0.7	0.8	0.5	0.9	0.5	0.4
200.	*	0.6	0.6	0.5	0.4	0.3	0.1	0.3	0.3	0.3	0.2	0.1	0.2	0.2	0.4	0.8	0.8	0.5	1.0	0.5	0.4
210.	*	0.5	0.5	0.5	0.4	0.3	0.2	0.3	0.3	0.3	0.3	0.2	0.2	0.2	0.4	0.8	0.7	0.5	0.9	0.5	0.5
220.	*	0.5	0.4	0.6	0.4	0.3	0.2	0.3	0.4	0.3	0.3	0.2	0.2	0.3	0.5	0.8	0.8	0.5	0.7	0.4	0.5
230.	*	0.4	0.6	0.6	0.5	0.4	0.2	0.5	0.5	0.3	0.3	0.2	0.2	0.4	0.5	0.8	0.9	0.6	0.7	0.5	0.5
240.	*	0.3	0.5	0.6	0.3	0.3	0.4	0.3	0.7	0.4	0.3	0.2	0.3	0.3	0.5	1.0	0.9	0.6	0.6	0.3	0.4
250.	*	0.3	0.5	0.4	0.2	0.2	0.3	0.5	0.8	0.4	0.4	0.2	0.3	0.6	0.7	0.9	0.8	0.4	0.4	0.2	0.5
260.	*	0.3	0.7	0.3	0.2	0.1	0.2	0.4	0.6	0.4	0.4	0.3	0.4	0.8	0.8	1.1	0.7	0.4	0.2	0.4	0.5
270.	*	0.3	0.6	0.3	0.2	0.0	0.1	0.2	0.6	0.4	0.4	0.3	0.3	0.7	0.5	0.9	0.8	0.5	0.4	0.4	0.4
280.	*	0.2	0.5	0.1	0.3	0.1	0.0	0.1	0.2	0.4	0.5	0.3	0.3	0.9	0.5	1.0	0.6	0.4	0.1	0.1	0.3
290.	*	0.2	0.5	0.3	0.3	0.0	0.0	0.3	0.3	0.2	0.3	0.3	0.5	0.6	0.4	0.9	0.6	0.2	0.1	0.2	0.2
300.	*	0.2	0.4	0.3	0.0	0.0	0.0	0.1	0.3	0.1	0.2	0.1	0.2	0.7	0.2	0.7	0.4	0.1	0.1	0.1	0.2
310.	*	0.1	0.2	0.2	0.0	0.0	0.0	0.1	0.3	0.2	0.1	0.2	0.2	0.5	0.2	0.3	0.2	0.1	0.1	0.1	0.1
320.	*	0.1	0.1	0.2	0.0	0.0	0.0	0.1	0.3	0.0	0.0	0.2	0.2	0.3	0.3	0.2	0.1	0.1	0.0	0.1	0.1
330.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.2	0.4	0.3	0.2	0.1	0.0	0.2	0.0	0.1
340.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.1	0.2	0.5	0.1	0.0	0.0	0.2	0.0	0.1
350.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.2	0.6	0.1	0.0	0.0	0.2	0.1	0.0
360.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.9	0.1	0.0	0.1	0.2	0.1	0.0

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------*-------------------------------------------------------------------------------------------------------------
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 MAX   *   0.7   0.7   0.6   0.5   0.4   0.4   0.5   0.8   0.4   0.5   0.3   0.5   0.9   0.9   1.1   1.0   0.7   1.0
0.5   0.5
 DEGR. *  180   260   220   230   230   240   230   250   240   280   260   290   280     0   260   180   100   200
130   210
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JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45
0.	0.1	0.1	0.2	0.0	0.0
10.	0.1	0.1	0.3	0.1	0.0
20.	0.1	0.1	0.3	0.1	0.0
30.	0.1	0.1	0.4	0.1	0.0
40.	0.1	0.1	0.4	0.1	0.0
50.	0.1	0.1	0.4	0.1	0.0
60.	0.1	0.1	0.4	0.1	0.0
70.	0.1	0.1	0.4	0.2	0.0
80.	0.1	0.1	0.3	0.2	0.0
90.	0.1	0.2	0.3	0.2	0.1
100.	0.1	0.2	0.2	0.2	0.1
110.	0.1	0.3	0.2	0.1	0.0
120.	0.2	0.3	0.1	0.0	0.1
130.	0.2	0.2	0.2	0.1	0.1
140.	0.3	0.4	0.3	0.2	0.2
150.	0.2	0.2	0.2	0.2	0.2
160.	0.3	0.2	0.3	0.3	0.4
170.	0.2	0.3	0.4	0.3	0.4
180.	0.3	0.3	0.3	0.4	0.5
190.	0.3	0.3	0.5	0.4	0.4
200.	0.4	0.2	0.4	0.4	0.3
210.	0.2	0.4	0.3	0.4	0.5
220.	0.2	0.3	0.4	0.3	0.3
230.	0.3	0.2	0.3	0.2	0.4
240.	0.2	0.3	0.2	0.2	0.3
250.	0.2	0.2	0.3	0.3	0.2
260.	0.4	0.2	0.4	0.3	0.3
270.	0.2	0.4	0.2	0.3	0.4
280.	0.1	0.2	0.2	0.2	0.2
290.	0.1	0.1	0.1	0.2	0.2
300.	0.1	0.1	0.1	0.1	0.1
310.	0.1	0.1	0.1	0.1	0.1
320.	0.1	0.1	0.2	0.1	0.1
330.	0.1	0.1	0.1	0.1	0.1
340.	0.0	0.1	0.1	0.0	0.1
350.	0.1	0.1	0.2	0.0	0.1
360.	0.1	0.1	0.2	0.0	0.0
MAX	0.4	0.4	0.5	0.4	0.5
DEGR.	200	140	190	180	180

THE HIGHEST CONCENTRATION OF 2.50 PPM OCCURRED AT RECEPTOR REC10.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15:28

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 PPM

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6030.2	5454.5	*	87.	290.	AG	275.	100.0	1.0	30.0	0.67	4.4
2. Char/Merr WB	*	6250.4	5435.2	6310.4	5482.7	*	77.	52.	AG	286.	100.0	1.0	30.0	0.67	3.9
3. Char/Merr NB R	*	6291.7	5369.7	6352.1	5328.7	*	73.	124.	AG	63.	100.0	1.0	10.0	0.37	3.7
4. Char/Merr NB LTT	*	6280.4	5347.2	6430.9	5241.1	*	184.	125.	AG	176.	100.0	1.0	20.0	0.94	9.4
5. Char/Merr EB	*	6104.2	5362.2	5936.5	5299.8	*	179.	250.	AG	174.	100.0	1.0	20.0	0.92	9.1
6. Char/Cam SB L	*	5384.1	4834.2	5402.6	4908.3	*	76.	14.	AG	72.	100.0	1.0	10.0	0.42	3.9
7. Char/Cam SB TR	*	5360.8	4833.5	5378.3	4889.9	*	59.	17.	AG	174.	100.0	1.0	20.0	0.41	3.0
8. Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	150.	100.0	1.0	20.0	0.41	3.7
9. Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	72.	100.0	1.0	10.0	0.53	5.0
10. Char/Cam NB TR	*	5383.3	4723.8	5385.0	4612.7	*	111.	179.	AG	174.	100.0	1.0	20.0	0.74	5.6
11. Char/Cam EB TTTR	*	5302.7	4739.8	5209.4	4740.8	*	93.	271.	AG	224.	100.0	1.0	30.0	0.52	4.7
12. Sud/Merr SB L	*	6532.7	5210.3	6461.3	5261.1	*	88.	305.	AG	106.	100.0	1.0	10.0	0.95	4.5
13. Sud/Merr SB TTT	*	6518.3	5190.8	6482.6	5211.5	*	41.	300.	AG	188.	100.0	1.0	30.0	0.21	2.1
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6684.5	5049.5	*	128.	150.	AG	232.	100.0	1.0	30.0	0.73	6.5
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6447.8	5100.4	*	88.	239.	AG	314.	100.0	1.0	40.0	0.52	4.5
16. Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	169.	100.0	1.0	20.0	0.53	4.1
17. Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	97.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6703.4	5223.8	*	98.	249.	AG	181.	100.0	1.0	30.0	0.50	5.0
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	989.	8.3	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1538.	8.3	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1494.	8.3	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1409.	8.3	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	921.	8.3	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1615.	8.3	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1034.	8.3	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1697.	8.3	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	1032.	8.3	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	504.	8.3	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	8.3	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	1075.	8.3	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	8.3	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1457.	8.3	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1759.	8.3	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	992.	8.3	1.0	78.0		

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JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15:28

ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
1. Char/Merr SB	*	100	76	3.0	615	1600	44.99	1	3
2. Char/Merr WB	*	100	79	3.0	517	1600	44.99	1	3
3. Char/Merr NB R	*	100	52	3.0	257	1600	44.99	1	3
4. Char/Merr NB LTT	*	100	73	3.0	660	1600	44.99	1	3

5. Char/Merr EB	*	100	72	3.0	679	1600	44.99	1	3
6. Char/Cam SB L	*	100	60	3.0	233	1600	44.99	1	3
7. Char/Cam SB TR	*	100	72	3.0	301	1600	44.99	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	435	1600	44.99	1	3
9. Char/Cam NB L	*	100	60	3.0	299	1600	44.99	1	3
10. Char/Cam NB TR	*	100	72	3.0	543	1600	44.99	1	3
11. Char/Cam EB TTTR	*	100	62	3.0	827	1600	44.99	1	3
12. Sud/Merr SB L	*	100	88	3.0	106	1600	44.99	1	3
13. Sud/Merr SB TTT	*	100	52	3.0	435	1600	44.99	1	3
14. Sud/Merr NB TTTR	*	100	64	3.0	1094	1600	44.99	1	3
15. Sud/Merr EB LTTR	*	100	65	3.0	992	1600	44.99	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	424	1600	44.99	1	3
17. Sud/Sur SEB	*	100	80	3.0	37	1600	44.99	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	1075	1600	44.99	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Sud/Merr NE1	*	6492.5	5309.9	6.0	*
2. Sud/Merr NE2	*	6554.8	5268.0	6.0	*
3. Sud/Merr NE3	*	6616.2	5224.9	6.0	*
4. Sud/Merr NE4	*	6684.7	5255.3	6.0	*
5. Sud/Merr NE5	*	6753.3	5285.7	6.0	*
6. Sud/Merr SE1	*	6792.9	5222.3	6.0	*
7. Sud/Merr SE2	*	6724.3	5191.9	6.0	*
8. Sud/Merr SE3	*	6655.7	5161.5	6.0	*
9. Sud/Merr SE4	*	6695.5	5097.9	6.0	*
10. Sud/Merr SE5	*	6735.2	5034.3	6.0	*
11. Sud/Merr SW1	*	6638.6	4981.3	6.0	*
12. Sud/Merr SW2	*	6598.9	5045.0	6.0	*
13. Sud/Merr SW3	*	6559.1	5108.6	6.0	*
14. Sud/Merr SW4	*	6493.4	5072.5	6.0	*
15. Sud/Merr SW5	*	6427.6	5036.5	6.0	*
16. Sud/Merr NW1	*	6347.8	5104.5	6.0	*
17. Sud/Merr NW2	*	6413.5	5140.5	6.0	*
18. Sud/Merr NW3	*	6479.3	5176.6	6.0	*
19. Sud/Merr NW4	*	6417.1	5218.5	6.0	*
20. Sud/Merr NW5	*	6354.9	5260.4	6.0	*
21. Sud/Sur NE1	*	6755.9	5445.7	6.0	*
22. Sud/Sur NE2	*	6801.0	5385.7	6.0	*
23. Sud/Sur NE3	*	6846.0	5325.7	6.0	*
24. Sud/Sur NE4	*	6908.8	5366.8	6.0	*
25. Sud/Sur NE5	*	6971.5	5407.9	6.0	*
26. Sud/Sur SE1	*	7002.4	5368.4	6.0	*
27. Sud/Sur SE2	*	6939.7	5327.3	6.0	*

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JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15:28

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
28. Sud/Sur SE3	*	6876.9	5286.2	6.0	*
29. Sud/Sur SE4	*	6931.7	5235.0	6.0	*
30. Sud/Sur SE5	*	6986.5	5183.8	6.0	*
31. Sud/Sur SW1	*	6932.3	5133.1	6.0	*
32. Sud/Sur SE2	*	6877.5	5184.3	6.0	*
33. Sud/Sur SE3	*	6822.7	5235.5	6.0	*
34. Sud/Sur SE4	*	6754.2	5205.1	6.0	*
35. Sud/Sur SE5	*	6685.6	5174.8	6.0	*
36. Sud/Sur NW1	*	6645.5	5237.9	6.0	*
37. Sud/Sur NW2	*	6714.1	5268.3	6.0	*
38. Sud/Sur NW3	*	6782.7	5298.7	6.0	*
39. Sud/Sur NW4	*	6709.5	5315.4	6.0	*
40. Sud/Sur NW5	*	6636.4	5332.0	6.0	*
41. Sud/Sur N1	*	6642.4	5493.7	6.0	*
42. Sud/Sur N2	*	6687.4	5433.7	6.0	*
43. Sud/Sur N3	*	6732.4	5373.8	6.0	*
44. Sud/Sur N4	*	6659.3	5390.4	6.0	*
45. Sud/Sur N5	*	6586.2	5407.1	6.0	*

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JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
	(PPM)																			
0.	0.1	0.1	0.0	0.0	0.4	0.6	0.7	0.2	0.2	0.2	0.8	0.6	0.6	1.4	0.7	0.3	0.5	0.7	0.9	0.9
10.	0.1	0.0	0.0	0.1	0.2	0.4	0.8	0.3	0.2	0.2	0.8	0.7	0.6	1.1	0.5	0.3	0.4	0.7	0.8	0.8
20.	0.0	0.0	0.0	0.1	0.2	0.3	0.8	0.5	0.2	0.1	0.9	0.8	0.6	1.0	0.8	0.4	0.3	0.8	0.6	0.8
30.	0.0	0.0	0.1	0.1	0.1	0.2	0.7	0.4	0.2	0.0	0.8	0.8	0.6	0.7	0.9	0.2	0.3	0.8	0.5	0.8
40.	0.0	0.0	0.1	0.1	0.1	0.4	0.8	0.5	0.2	0.0	0.4	0.8	0.8	0.7	0.8	0.1	0.4	0.8	0.4	0.7
50.	0.0	0.1	0.0	0.0	0.1	0.2	0.5	0.5	0.0	0.0	0.5	0.8	1.0	0.7	0.7	0.2	0.4	0.8	0.5	0.7
60.	0.0	0.1	0.2	0.2	0.1	0.2	0.3	0.4	0.0	0.0	0.4	0.7	0.9	0.6	0.5	0.4	0.5	0.9	0.4	0.8
70.	0.0	0.0	0.3	0.3	0.1	0.1	0.1	0.2	0.0	0.0	0.3	0.6	0.8	0.5	0.3	0.7	0.7	0.9	0.4	0.9
80.	0.0	0.1	0.5	0.5	0.2	0.1	0.1	0.0	0.0	0.0	0.3	0.5	0.6	0.4	0.2	0.9	0.9	1.0	0.6	0.9
90.	0.0	0.2	0.5	0.6	0.3	0.1	0.1	0.0	0.0	0.0	0.4	0.6	0.7	0.4	0.2	0.8	1.1	0.9	0.8	1.1
100.	0.2	0.2	0.4	0.8	0.4	0.1	0.0	0.0	0.0	0.0	0.4	0.5	0.7	0.3	0.2	0.6	1.1	0.9	1.0	1.1
110.	0.2	0.2	0.4	0.7	0.4	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.2	0.1	0.4	1.1	1.0	0.9	1.0
120.	0.3	0.1	0.3	0.7	0.5	0.1	0.0	0.0	0.0	0.0	0.4	0.4	0.7	0.2	0.1	0.3	1.0	1.1	0.8	1.1
130.	0.5	0.4	0.3	0.6	0.6	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.6	0.1	0.0	0.2	0.8	1.0	0.8	0.9
140.	0.6	0.7	0.4	0.5	0.5	0.0	0.0	0.2	0.1	0.1	0.3	0.3	0.4	0.1	0.0	0.2	0.5	1.0	0.5	0.6
150.	0.8	0.8	0.8	0.4	0.6	0.0	0.0	0.5	0.3	0.2	0.2	0.2	0.2	0.0	0.0	0.2	0.4	0.9	0.4	0.3
160.	1.0	0.9	1.1	0.4	0.6	0.0	0.1	0.8	0.4	0.3	0.1	0.1	0.1	0.0	0.0	0.2	0.3	0.9	0.3	0.3
170.	0.9	0.7	1.1	0.5	0.7	0.0	0.1	1.1	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.9	0.2	0.1
180.	0.8	0.6	1.0	0.6	0.7	0.1	0.2	1.1	0.6	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.9	0.2	0.1
190.	0.8	0.7	0.8	0.7	0.9	0.1	0.3	1.1	0.7	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.8	0.1	0.1
200.	0.6	0.8	0.8	0.7	1.0	0.1	0.4	1.1	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.7	0.1	0.0
210.	0.5	0.9	0.7	0.7	0.9	0.2	0.4	1.0	0.9	0.4	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.6	0.1	0.0
220.	0.4	0.9	0.9	0.8	0.8	0.3	0.5	0.9	0.8	0.3	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.4	0.1	0.0
230.	0.5	0.7	1.0	0.7	0.8	0.4	0.5	1.0	1.0	0.4	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.0	0.0
240.	0.5	0.5	1.0	0.6	0.7	0.5	0.7	1.2	1.0	0.4	0.0	0.0	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.1
250.	0.6	0.5	0.6	0.6	0.5	0.7	0.7	1.3	0.9	0.3	0.0	0.0	0.4	0.2	0.1	0.0	0.0	0.1	0.0	0.1
260.	0.7	0.6	0.7	0.1	0.1	0.9	0.8	1.2	1.1	0.3	0.0	0.1	0.6	0.2	0.2	0.0	0.0	0.0	0.0	0.1
270.	0.6	0.8	0.7	0.3	0.3	0.8	0.7	1.3	1.3	0.6	0.0	0.1	0.8	0.3	0.2	0.0	0.0	0.0	0.1	0.2
280.	0.6	0.7	0.7	0.4	0.2	1.0	0.8	1.3	1.3	0.8	0.1	0.2	0.9	0.3	0.2	0.0	0.1	0.1	0.3	0.3
290.	0.8	0.8	0.6	0.3	0.1	0.9	0.6	1.4	1.4	0.9	0.2	0.3	0.9	0.5	0.2	0.1	0.1	0.3	0.4	0.5
300.	0.3	0.4	0.5	0.1	0.1	0.9	0.6	1.0	1.6	1.3	0.2	0.5	1.0	0.6	0.3	0.2	0.2	0.6	0.8	0.7
310.	0.2	0.3	0.2	0.1	0.1	0.8	0.4	0.7	1.2	1.2	0.5	0.7	1.0	0.9	0.3	0.2	0.3	0.8	0.9	1.0
320.	0.2	0.1	0.1	0.1	0.1	0.7	0.4	0.5	0.8	1.0	0.6	0.8	1.1	1.0	0.3	0.2	0.2	0.9	1.2	1.0
330.	0.1	0.1	0.1	0.1	0.0	0.6	0.5	0.4	0.4	0.6	0.6	0.7	1.1	1.2	0.4	0.2	0.6	0.7	1.1	1.1
340.	0.1	0.1	0.1	0.0	0.2	0.8	0.5	0.3	0.2	0.3	0.7	0.6	0.8	1.3	0.5	0.3	0.6	0.7	1.1	1.3
350.	0.1	0.1	0.0	0.0	0.3	0.7	0.6	0.2	0.1	0.2	0.7	0.5	0.7	1.2	0.5	0.4	0.4	0.6	0.9	1.2
360.	0.1	0.1	0.0	0.0	0.4	0.6	0.7	0.2	0.2	0.2	0.8	0.6	0.6	1.4	0.7	0.3	0.5	0.7	0.9	0.9
MAX	1.0	0.9	1.1	0.8	1.0	1.0	0.8	1.4	1.6	1.3	0.9	0.8	1.1	1.4	0.9	0.9	1.1	1.1	1.2	1.3
DEGR.	160	210	160	100	200	280	280	290	300	300	20	320	320	0	30	80	90	120	320	340

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM)																			
	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.1	0.0	0.2	0.2	0.2	0.7	0.3	0.0	0.1	0.2	0.2	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.1	0.0	0.1	0.2	0.2	0.7	0.5	0.0	0.1	0.2	0.2	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.0	0.0	0.1	0.2	0.3	0.7	0.6	0.1	0.1	0.1	0.3	0.0
30.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.3	0.0	0.0	0.1	0.1	0.3	0.5	0.6	0.1	0.1	0.1	0.3	0.0
40.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.0	0.0	0.1	0.1	0.3	0.5	0.6	0.1	0.0	0.1	0.2	0.1
50.	0.0	0.0	0.1	0.0	0.0	0.0	0.1	0.2	0.0	0.0	0.1	0.1	0.2	0.4	0.7	0.0	0.0	0.1	0.2	0.1
60.	0.0	0.0	0.2	0.1	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.2	0.4	0.5	0.2	0.1	0.2	0.3	0.1
70.	0.0	0.0	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.5	0.2	0.2	0.2	0.1
80.	0.0	0.0	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.6	0.4	0.2	0.2	0.1
90.	0.0	0.1	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.6	0.6	0.2	0.1	0.1
100.	0.0	0.1	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.6	0.6	0.2	0.1	0.0
110.	0.0	0.1	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.0	0.0	0.5	0.8	0.2	0.3	0.2
120.	0.1	0.1	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.4	0.7	0.1	0.3	0.2
130.	0.1	0.1	0.2	0.2	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.6	0.2	0.3	0.3
140.	0.1	0.2	0.3	0.2	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.2	0.6	0.2	0.3	0.2
150.	0.2	0.2	0.3	0.2	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.4	0.6	0.4	0.4	0.3
160.	0.3	0.3	0.3	0.2	0.0	0.0	0.0	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.2	0.6	0.7	0.4	0.4	0.3
170.	0.6	0.1	0.3	0.3	0.1	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.4	0.8	0.7	0.5	0.5	0.4
180.	0.8	0.4	0.3	0.4	0.1	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.5	0.8	0.8	0.6	0.7	0.4
190.	0.9	0.4	0.4	0.4	0.1	0.0	0.1	0.2	0.1	0.1	0.0	0.1	0.1	0.2	0.6	0.9	1.0	0.8	0.6	0.4
200.	0.8	0.5	0.6	0.5	0.3	0.0	0.2	0.2	0.2	0.1	0.0	0.1	0.1	0.3	0.7	0.8	0.9	0.9	0.5	0.5
210.	0.7	0.5	0.6	0.4	0.3	0.1	0.2	0.2	0.2	0.2	0.1	0.1	0.2	0.4	0.7	0.8	0.8	0.9	0.3	0.4
220.	0.8	0.6	0.7	0.7	0.4	0.1	0.2	0.3	0.2	0.2	0.1	0.1	0.2	0.4	0.7	0.7	0.8	0.8	0.4	0.3
230.	0.5	0.6	0.6	0.6	0.6	0.3	0.6	0.5	0.3	0.2	0.1	0.2	0.2	0.4	0.7	0.9	0.8	0.9	0.5	0.4
240.	0.4	0.4	0.7	0.5	0.3	0.5	0.5	0.9	0.3	0.2	0.1	0.2	0.5	0.7	0.8	0.8	0.6	0.6	0.3	0.1
250.	0.5	0.5	0.4	0.2	0.0	0.5	0.5	0.9	0.4	0.3	0.2	0.2	0.2	0.7	0.7	1.1	0.6	0.5	0.1	0.3
260.	0.4	0.7	0.2	0.0	0.1	0.2	0.5	0.7	0.6	0.3	0.2	0.5	1.0	0.8	1.1	0.4	0.1	0.1	0.3	0.3
270.	0.2	0.7	0.2	0.1	0.1	0.2	0.3	0.6	0.4	0.4	0.3	0.6	0.8	0.8	0.8	0.5	0.3	0.3	0.4	0.3
280.	0.2	0.6	0.2	0.3	0.1	0.3	0.5	0.3	0.3	0.3	0.4	0.3	0.9	0.8	1.1	0.5	0.4	0.1	0.2	0.3
290.	0.2	0.6	0.3	0.2	0.1	0.2	0.5	0.3	0.4	0.3	0.2	0.3	0.8	0.9	0.8	0.3	0.2	0.1	0.1	0.2
300.	0.2	0.5	0.3	0.2	0.0	0.0	0.5	0.5	0.3	0.2	0.2	0.4	0.6	0.7	0.8	0.3	0.1	0.1	0.1	0.1
310.	0.2	0.4	0.4	0.0	0.0	0.0	0.2	0.4	0.3	0.2	0.3	0.3	0.5	0.7	0.4	0.1	0.1	0.2	0.1	0.1
320.	0.1	0.2	0.2	0.0	0.0	0.0	0.2	0.4	0.2	0.1	0.1	0.3	0.3	0.7	0.3	0.1	0.1	0.3	0.1	0.1
330.	0.0	0.0	0.1	0.0	0.0	0.0	0.2	0.2	0.1	0.1	0.1	0.2	0.4	0.6	0.3	0.1	0.1	0.2	0.1	0.1
340.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.1	0.2	0.2	0.3	0.6	0.2	0.1	0.0	0.3	0.0	0.1
350.	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.2	0.2	0.3	0.7	0.2	0.0	0.0	0.3	0.0	0.0
360.	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.3	0.1	0.0	0.2	0.2	0.2	0.7	0.3	0.0	0.1	0.2	0.2	0.0

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------*-------------------------------------------------------------------------------------------------------------
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 MAX   *   0.9   0.7   0.7   0.7   0.6   0.5   0.6   0.9   0.6   0.4   0.4   0.6   1.0   0.9   1.1   0.9   1.0   0.9
0.7   0.5
 DEGR. *  190   260   220   220   230   240   230   240   260   270   280   270   260   290   280   190   190   230
180   200
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JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45
0.	0.1	0.1	0.4	0.0	0.0
10.	0.1	0.1	0.4	0.1	0.0
20.	0.1	0.1	0.5	0.1	0.0
30.	0.1	0.1	0.5	0.1	0.0
40.	0.1	0.1	0.5	0.1	0.0
50.	0.1	0.1	0.5	0.2	0.0
60.	0.1	0.1	0.5	0.2	0.0
70.	0.1	0.2	0.4	0.3	0.0
80.	0.1	0.2	0.4	0.3	0.1
90.	0.1	0.3	0.4	0.3	0.1
100.	0.1	0.4	0.4	0.3	0.1
110.	0.2	0.5	0.3	0.2	0.0
120.	0.2	0.5	0.2	0.0	0.0
130.	0.2	0.3	0.2	0.1	0.2
140.	0.2	0.2	0.1	0.2	0.2
150.	0.2	0.2	0.3	0.2	0.3
160.	0.3	0.2	0.3	0.3	0.3
170.	0.3	0.3	0.4	0.4	0.4
180.	0.3	0.4	0.4	0.4	0.3
190.	0.1	0.3	0.4	0.3	0.4
200.	0.3	0.2	0.4	0.2	0.3
210.	0.3	0.4	0.3	0.4	0.3
220.	0.1	0.3	0.5	0.3	0.1
230.	0.2	0.1	0.3	0.1	0.3
240.	0.2	0.3	0.1	0.2	0.2
250.	0.3	0.2	0.2	0.3	0.2
260.	0.3	0.3	0.2	0.3	0.3
270.	0.3	0.2	0.3	0.3	0.4
280.	0.2	0.1	0.1	0.2	0.3
290.	0.2	0.1	0.1	0.1	0.2
300.	0.1	0.1	0.1	0.1	0.1
310.	0.1	0.1	0.1	0.1	0.1
320.	0.1	0.1	0.1	0.1	0.1
330.	0.1	0.1	0.1	0.1	0.1
340.	0.0	0.1	0.2	0.0	0.1
350.	0.1	0.1	0.3	0.0	0.1
360.	0.1	0.1	0.4	0.0	0.0
MAX	0.3	0.5	0.5	0.4	0.4
DEGR.	160	110	20	170	170

THE HIGHEST CONCENTRATION OF 1.60 PPM OCCURRED AT RECEPTOR REC9 .

2013 Existing Microscale Output Files (Particulate Matter 10 (PM10))

JOB: Government Center Garage RUN: Existing

DATE : 7/22/13
TIME : 15: 4:46

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Stan/Lom SB L	*	5194.4	5948.0	5135.6	6035.2	*	105.	326.	AG	0.	100.0	1.0	10.0	0.84	5.3
2. Stan/Lom SB TRR	*	5173.5	5937.1	5122.0	6010.9	*	90.	325.	AG	0.	100.0	1.0	20.0	0.71	4.6
3. Stan/Lom WB LTT	*	5306.8	5930.3	5403.5	6009.6	*	125.	51.	AG	0.	100.0	1.0	20.0	0.87	6.4
4. Stan/Lom WB R	*	5292.4	5947.7	5347.6	5990.1	*	70.	52.	AG	0.	100.0	1.0	10.0	0.40	3.5
5. Stan/Lom NB L	*	5307.6	5737.4	5359.5	5721.4	*	54.	107.	AG	0.	100.0	1.0	10.0	0.53	2.8
6. Stan/Lom NB TRR	*	5314.4	5765.3	5342.7	5755.7	*	30.	109.	AG	0.	100.0	1.0	20.0	0.25	1.5
7. Stan/Lom EB LLT	*	5214.5	5705.3	5200.8	5658.2	*	49.	196.	AG	0.	100.0	1.0	20.0	0.44	2.5
8. Stan/Lom EB R	*	5236.5	5698.5	5221.6	5646.0	*	55.	196.	AG	0.	100.0	1.0	10.0	0.32	2.8
9. Caus/Wash SB LTTRR	*	6548.6	6868.7	6475.2	7021.0	*	169.	334.	AG	0.	100.0	1.0	40.0	0.58	8.6
10. Caus/Wash WB LLTT	*	6635.9	6867.8	6714.6	6936.2	*	104.	49.	AG	0.	100.0	1.0	20.0	0.69	5.3
11. Caus/Wash WB R	*	6624.3	6883.3	6687.4	6942.0	*	86.	47.	AG	0.	100.0	1.0	10.0	0.28	4.4
12. Caus/Wash NB TTR	*	6603.5	6751.9	6613.9	6519.8	*	232.	177.	AG	0.	100.0	1.0	20.0	0.88	11.8
13. Caus/Wash EB LLTTR	*	6538.7	6754.8	6469.9	6706.8	*	84.	235.	AG	1.	100.0	1.0	30.0	0.47	4.3
14. Tha/Val SB LTTR	*	6599.0	6224.0	6593.3	6370.2	*	146.	358.	AG	0.	100.0	1.0	20.0	0.81	7.4
15. Tha/Val NB L	*	6631.0	6138.6	6630.2	6047.3	*	91.	180.	AG	0.	100.0	1.0	10.0	0.55	4.6
16. Tha/Val NB TR	*	6645.6	6138.6	6648.0	6000.5	*	138.	179.	AG	0.	100.0	1.0	10.0	0.76	7.0
17. Bev/Was SB TTT	*	6592.9	5963.9	6593.7	6089.2	*	125.	0.	AG	0.	100.0	1.0	30.0	0.64	6.4
18. Bev/Was EB RRR	*	6545.9	5954.3	6530.5	5976.1	*	27.	325.	AG	0.	100.0	1.0	30.0	0.14	1.4
19. Char/93 SB LLTTRR	*	6587.8	5740.0	6582.8	5870.1	*	130.	358.	AG	0.	100.0	1.0	40.0	0.67	6.6
20. Char/93 WB LTT	*	6702.8	5647.8	6712.2	5636.0	*	15.	141.	AG	0.	100.0	1.0	20.0	0.10	0.8
21. Char/93 EB TTR	*	6560.8	5622.5	6523.0	5594.9	*	47.	234.	AG	0.	100.0	1.0	30.0	0.30	2.4
22. North/Congress SB LT	*	6876.6	4408.9	6860.5	4488.9	*	82.	349.	AG	1.	100.0	1.0	30.0	0.62	4.1
23. North/Con WB LLTR	*	6920.6	4378.3	7073.6	4432.5	*	162.	71.	AG	0.	100.0	1.0	20.0	0.82	8.2
24. Nor/Con NB LTTTR	*	6914.9	4333.4	6920.4	4292.5	*	41.	172.	AG	0.	100.0	1.0	30.0	0.30	2.1
25. Nor/Con EB LTR	*	6869.7	4342.2	6864.6	4340.9	*	5.	256.	AG	0.	100.0	1.0	10.0	0.03	0.3
26. Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1120.	0.0	1.0	90.0		
27. Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1275.	0.0	1.0	78.0		
28. Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	817.	0.0	1.0	78.0		
29. Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1322.	0.0	1.0	78.0		
30. Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3211.	0.0	1.0	90.0		
31. Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1012.	0.0	1.0	66.0		
32. Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2221.	0.0	1.0	90.0		
33. Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1162.	0.0	1.0	78.0		
34. Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2247.	0.0	1.0	90.0		
35. Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	91.	0.0	1.0	38.0		
36. Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2524.	0.0	1.0	90.0		
37. Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	280.	0.0	1.0	54.0		
38. Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	1841.	0.0	1.0	66.0		
39. Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	269.	0.0	1.0	48.0		
40. Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	80.	0.0	1.0	42.0		
41. Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	811.	0.0	1.0	48.0		
42. Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	374.	0.0	1.0	54.0		
43. Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	650.	0.0	1.0	54.0		

44. Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	406.	0.0	1.0	42.0		

JOB: Government Center Garage RUN: Existing

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LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
45. North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1226.	0.0	1.0	98.0		
46. North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	978.	0.0	1.0	66.0		
47. North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1420.	0.0	1.0	98.0		
48. North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	44.	0.0	1.0	54.0		

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1. Stan/Lom SB L	*	90	70	3.0	223	1600	0.08	1	3
2. Stan/Lom SB TRR	*	90	66	3.0	481	1600	0.08	1	3
3. Stan/Lom WB LTT	*	90	68	3.0	527	1600	0.08	1	3
4. Stan/Lom WB R	*	90	48	3.0	265	1600	0.08	1	3
5. Stan/Lom NB L	*	90	70	3.0	142	1600	0.08	1	3
6. Stan/Lom NB TRR	*	90	66	3.0	166	1600	0.08	1	3
7. Stan/Lom EB LLT	*	90	68	3.0	265	1600	0.08	1	3
8. Stan/Lom EB R	*	90	48	3.0	208	1600	0.08	1	3
9. Caus/Wash SB LTTRR	*	150	56	3.0	2210	1600	0.08	1	3
10. Caus/Wash WB LLTT	*	150	125	3.0	296	1600	0.08	1	3
11. Caus/Wash WB R	*	150	73	3.0	216	1600	0.08	1	3
12. Caus/Wash NB TTR	*	150	108	3.0	693	1600	0.08	1	3
13. Caus/Wash EB LLTTR	*	150	119	3.0	388	1600	0.08	1	3
14. Tha/Val SB LTTR	*	100	34	3.0	1575	1600	0.08	1	3
15. Tha/Val NB L	*	100	66	3.0	253	1600	0.08	1	3
16. Tha/Val NB TR	*	100	34	3.0	743	1600	0.08	1	3
17. Bev/Was SB TTT	*	100	45	3.0	1528	1600	0.08	1	3
18. Bev/Was EB RRR	*	100	55	3.0	269	1600	0.08	1	3
19. Char/93 SB LLTTRR	*	100	53	3.0	1797	1600	0.08	1	3
20. Char/93 WB LTT	*	100	69	3.0	80	1600	0.08	1	3
21. Char/93 EB TTR	*	100	69	3.0	374	1600	0.08	1	3
22. North/Congress SB LT	*	100	75	3.0	598	1600	0.08	1	3
23. North/Con WB LLTR	*	100	60	3.0	916	1600	0.08	1	3
24. Nor/Con NB LTTTR	*	100	74	3.0	306	1600	0.08	1	3
25. Nor/Con EB LTR	*	100	60	3.0	16	1600	0.08	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2. Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3. Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4. Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5. Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6. Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7. Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8. Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9. Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10. Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11. Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12. Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13. Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14. Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15. Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16. Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17. Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18. Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19. Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20. Stan/Lom NW5	*	5136.5	5935.7	6.0	*
21. Caus/Wash NE1	*	6548.3	7035.9	6.0	*
22. Caus/Wash NE2	*	6581.4	6968.6	6.0	*
23. Caus/Wash NE3	*	6614.5	6901.3	6.0	*
24. Caus/Wash NE4	*	6669.8	6952.0	6.0	*
25. Caus/Wash NE5	*	6725.0	7002.7	6.0	*
26. Caus/Wash SE1	*	6753.6	6912.2	6.0	*

JOB: Government Center Garage RUN: Existing

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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Caus/Wash SE2	6698.9	6862.0	6.0
28. Caus/Wash SE3	6643.1	6810.8	6.0
29. Caus/Wash SE4	6646.8	6736.4	6.0
30. Caus/Wash SE5	6650.0	6661.0	6.0
31. Caus/Wash SW1	6544.0	6561.0	6.0
32. Caus/Wash SW2	6540.9	6636.0	6.0
33. Caus/Wash SW3	6537.8	6710.9	6.0
34. Caus/Wash SW4	6476.8	6667.2	6.0
35. Caus/Wash SW5	6415.9	6623.4	6.0
36. Caus/Wash NW1	6407.4	6738.0	6.0
37. Caus/Wash NW2	6468.3	6781.7	6.0
38. Caus/Wash NW3	6529.3	6825.4	6.0
39. Caus/Wash NW4	6496.2	6892.7	6.0
40. Caus/Wash NW5	6463.1	6960.0	6.0
41. Tha/Val NE1	6667.3	6395.5	6.0
42. Tha/Val NE2	6668.3	6320.5	6.0
43. Tha/Val NE3	6669.3	6245.5	6.0
44. Tha/Val NE4	6744.3	6245.5	6.0
45. Tha/Val NE5	6819.2	6249.6	6.0
46. Tha/Val SE1	6822.3	6191.6	6.0
47. Tha/Val SE2	6747.3	6189.6	6.0
48. Tha/Val SE3	6672.3	6187.5	6.0
49. Tha/Val SE4	6671.6	6112.5	6.0
50. Tha/Val SE5	6670.9	6037.5	6.0
51. Tha/Val SW1	6560.2	5964.7	6.0
52. Tha/Val SW2	6560.9	6039.7	6.0
53. Tha/Val SW3	6561.6	6114.7	6.0
54. Tha/Val SW4	6502.2	6068.9	6.0
55. Tha/Val SW5	6442.7	6023.2	6.0
56. Tha/Val NW1	6441.0	6115.2	6.0
57. Tha/Val NW2	6500.4	6160.9	6.0
58. Tha/Val NW3	6559.8	6206.7	6.0
59. Tha/Val NW4	6558.8	6281.7	6.0
60. Tha/Val NW5	6557.8	6356.7	6.0

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.
10.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	2.	2.	2.	1.	1.	1.	1.	2.
20.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	2.	2.	2.	1.	1.	1.	1.	2.
30.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	1.	2.	1.	1.	2.	2.	1.	1.	2.
40.	0.	0.	0.	0.	0.	1.	2.	2.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	2.	2.
50.	0.	0.	1.	1.	1.	1.	1.	2.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.
60.	0.	0.	2.	2.	1.	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	3.	2.	1.	3.	3.
70.	0.	0.	3.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	1.	3.	3.
80.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	0.	2.	3.
90.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	2.	3.
100.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	1.	2.
110.	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	1.	2.	2.	1.	2.
120.	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	2.
130.	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	2.
140.	1.	1.	2.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	1.
150.	1.	2.	2.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	1.
160.	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	4.	4.	5.	4.	2.	1.	2.	5.	5.	4.
10.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	4.	4.	5.	4.	3.	1.	2.	4.	5.	4.
20.	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	4.	4.	5.	4.	3.	2.	2.	4.	4.	4.
30.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	4.	4.	4.	4.	4.	2.	2.	4.	4.	4.
40.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	3.	3.	4.	4.	4.	2.	2.	4.	4.	4.
50.	0.	0.	1.	0.	0.	0.	0.	1.	0.	0.	3.	3.	3.	3.	3.	2.	3.	4.	4.	4.
60.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	3.	2.	2.	3.	3.	4.	4.	4.
70.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	3.	3.	4.	4.	4.
80.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	3.	3.	3.	2.	1.	3.	3.	4.	4.	4.
90.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	3.	3.	3.	2.	1.	3.	3.	4.	5.	4.
100.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	2.	1.	3.	3.	4.	5.	5.
170.	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
180.	2.	2.	2.	3.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.
190.	2.	2.	3.	3.	3.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.
200.	2.	2.	2.	3.	3.	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.
210.	2.	2.	2.	2.	3.	1.	1.	2.	2.	1.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.
220.	1.	2.	2.	2.	2.	1.	1.	1.	2.	1.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
230.	1.	2.	1.	1.	2.	1.	1.	0.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
240.	1.	2.	1.	1.	1.	1.	1.	0.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
250.	1.	2.	1.	1.	1.	1.	1.	0.	1.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.
260.	1.	2.	1.	1.	1.	2.	1.	0.	1.	2.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.
270.	1.	2.	2.	1.	1.	2.	2.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.
280.	1.	2.	2.	1.	0.	2.	2.	0.	0.	1.	1.	1.	1.	2.	1.	0.	0.	0.	0.	0.
290.	1.	2.	2.	1.	0.	3.	2.	0.	0.	1.	1.	1.	1.	2.	1.	0.	0.	0.	0.	0.
300.	1.	2.	2.	1.	0.	3.	3.	1.	1.	1.	1.	1.	1.	2.	1.	0.	0.	0.	0.	0.
310.	1.	1.	2.	0.	0.	2.	3.	1.	1.	1.	2.	1.	1.	2.	1.	0.	0.	0.	0.	0.
320.	1.	1.	1.	0.	0.	2.	2.	2.	2.	1.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.
330.	0.	0.	1.	0.	0.	2.	2.	2.	2.	1.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.	3.	2.	0.	0.	1.	2.	2.
350.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.
360.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.
MAX	2.	2.	3.	3.	3.	3.	3.	2.	2.	2.	2.	2.	2.	3.	2.	3.	2.	2.	3.	3.
DEGR.	180	180	70	200	200	300	310	330	210	250	320	330	230	340	350	60	90	170	60	70

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 110. *   0.   1.   2.   2.   1.   0.   0.   0.   0.   0.   2.   2.   2.   2.   1.   3.   3.   3.
4.   5.
 120. *   1.   1.   2.   2.   1.   0.   0.   0.   0.   0.   2.   3.   3.   2.   1.   3.   4.   4.
4.   5.
 130. *   1.   1.   2.   2.   1.   0.   0.   0.   0.   0.   2.   3.   3.   2.   1.   2.   4.   4.
4.   5.
 140. *   1.   1.   2.   2.   1.   0.   0.   0.   0.   0.   3.   3.   3.   2.   1.   2.   4.   4.
4.   5.
 150. *   2.   2.   2.   2.   1.   0.   0.   0.   0.   0.   3.   3.   3.   2.   1.   2.   4.   4.
4.   4.
 160. *   4.   3.   3.   2.   1.   0.   0.   0.   0.   0.   3.   3.   4.   2.   1.   2.   4.   5.
4.   3.
 170. *   6.   5.   5.   3.   2.   0.   0.   2.   1.   1.   3.   3.   3.   1.   1.   2.   3.   4.
3.   2.
 180. *   6.   6.   6.   4.   2.   1.   1.   3.   3.   3.   2.   2.   2.   0.   0.   2.   2.   4.
2.   2.
 190. *   5.   6.   6.   5.   3.   1.   2.   4.   4.   4.   1.   1.   1.   0.   0.   1.   2.   3.
1.   1.
 200. *   5.   5.   5.   5.   4.   1.   2.   4.   4.   4.   0.   0.   0.   0.   0.   1.   2.   2.
1.   0.
 210. *   4.   4.   5.   4.   4.   2.   2.   3.   4.   3.   0.   0.   0.   0.   0.   1.   2.   2.
1.   0.
 220. *   4.   4.   5.   4.   4.   2.   2.   3.   3.   3.   0.   0.   0.   0.   0.   1.   2.   2.
0.   0.
 230. *   4.   4.   4.   3.   3.   3.   3.   4.   3.   3.   0.   0.   1.   1.   1.   1.   1.   1.
0.   0.
 240. *   4.   4.   4.   2.   2.   3.   4.   4.   3.   3.   0.   0.   1.   1.   1.   1.   1.   1.
0.   0.
 250. *   4.   4.   4.   2.   2.   4.   4.   4.   4.   3.   0.   0.   2.   1.   1.   0.   0.   0.
0.   0.
 260. *   3.   3.   3.   2.   2.   4.   4.   4.   4.   3.   0.   0.   2.   1.   1.   0.   0.   0.
0.   0.
 270. *   3.   4.   4.   2.   2.   4.   4.   4.   4.   3.   0.   1.   2.   1.   1.   0.   0.   0.
0.   0.
 280. *   3.   4.   4.   2.   1.   4.   4.   4.   4.   4.   0.   1.   3.   1.   1.   0.   0.   0.
0.   0.
 290. *   3.   4.   4.   2.   1.   3.   4.   4.   3.   4.   0.   1.   3.   1.   1.   0.   0.   0.
0.   0.
 300. *   4.   4.   4.   2.   1.   3.   4.   5.   4.   4.   0.   1.   3.   1.   1.   0.   0.   0.
0.   0.
 310. *   3.   4.   4.   1.   0.   2.   4.   6.   4.   4.   1.   1.   3.   1.   1.   0.   0.   0.
0.   0.
 320. *   3.   4.   4.   1.   0.   2.   3.   6.   5.   4.   1.   1.   3.   1.   1.   0.   0.   1.
1.   0.
 330. *   2.   2.   3.   0.   0.   1.   2.   5.   5.   5.   1.   2.   3.   1.   1.   0.   0.   2.
2.   1.
 340. *   1.   1.   1.   0.   0.   1.   2.   4.   4.   5.   2.   2.   4.   2.   1.   0.   0.   4.
3.   3.
 350. *   0.   0.   0.   0.   0.   1.   2.   3.   3.   4.   3.   3.   5.   3.   1.   0.   1.   5.
5.   4.
 360. *   0.   0.   0.   0.   0.   1.   2.   2.   2.   2.   4.   4.   5.   4.   2.   1.   2.   5.
5.   4.

------*-----------------------------------------------------------------------------------------------------------
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 MAX  *   6.   6.   6.   5.   4.   4.   4.   6.   5.   5.   4.   4.   5.   4.   4.   3.   4.   5.
5.   5.
 DEGR. *  180   180   190   200   210   250   290   320   330   330    10    10     0    20    40    90   150     0
0   130
```



```
3.   2.
  60. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   3.   2.   2.   2.   2.   2.
2.   2.
  70. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   3.   2.   2.   2.   2.   2.   2.
2.   2.
  80. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   3.   2.   2.   2.   2.   2.   3.
2.   2.
  90. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   4.   3.   2.   2.   2.   2.   3.
2.   2.
 100. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   3.   3.   2.   2.   2.   2.   4.
2.   2.
 110. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   3.   3.   2.   2.   2.   2.   3.
2.   2.
 120. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   3.   3.   2.   2.   2.   2.   4.
3.   2.
 130. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   3.   3.   2.   2.   2.   2.   4.
3.   3.
 140. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   4.   4.   2.   1.   2.   2.   4.
3.   3.
 150. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   4.   4.   2.   1.   2.   2.   4.
4.   3.
 160. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   4.   2.   1.   2.   2.   4.
4.   4.
 170. *   1.   1.   1.   0.   0.   0.   0.   1.   1.   1.   4.   4.   4.   2.   1.   1.   2.   4.
4.   4.
 180. *   3.   2.   3.   0.   0.   0.   0.   2.   2.   2.   3.   3.   3.   1.   0.   0.   1.   3.
3.   3.
 190. *   4.   4.   4.   1.   0.   0.   1.   4.   3.   2.   2.   2.   1.   0.   0.   0.   1.   2.
2.   1.
 200. *   4.   4.   5.   2.   1.   0.   1.   4.   4.   4.   1.   1.   1.   0.   0.   0.   0.   1.
0.   0.
 210. *   3.   4.   4.   2.   1.   1.   2.   4.   4.   4.   1.   1.   0.   0.   0.   0.   0.   0.
0.   0.
 220. *   3.   3.   4.   2.   1.   1.   2.   4.   4.   4.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 230. *   2.   3.   3.   2.   2.   1.   2.   3.   4.   4.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 240. *   2.   2.   3.   2.   1.   1.   2.   3.   3.   3.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 250. *   2.   2.   3.   2.   2.   2.   2.   4.   3.   3.   2.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 260. *   2.   2.   3.   2.   2.   1.   2.   4.   3.   4.   2.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 270. *   2.   2.   2.   1.   1.   1.   2.   4.   3.   4.   2.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 280. *   2.   2.   2.   1.   1.   1.   2.   3.   3.   3.   2.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 290. *   2.   2.   2.   1.   1.   1.   2.   3.   3.   3.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 300. *   2.   2.   2.   2.   1.   1.   1.   3.   3.   3.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 310. *   2.   3.   3.   2.   1.   1.   2.   3.   3.   3.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 320. *   3.   3.   3.   2.   2.   1.   2.   3.   4.   4.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 330. *   3.   4.   3.   2.   2.   2.   2.   4.   4.   4.   1.   0.   0.   0.   0.   0.   0.   0.
0.   1.
 340. *   4.   4.   4.   2.   1.   2.   2.   4.   5.   5.   1.   1.   1.   0.   0.   0.   0.   1.
1.   1.
 350. *   4.   4.   4.   1.   1.   1.   2.   4.   4.   4.   2.   2.   2.   1.   0.   0.   1.   2.
2.   2.
 360. *   2.   2.   2.   0.   0.   0.   1.   2.   3.   3.   4.   3.   4.   2.   1.   1.   2.   3.
3.   3.

------*-----------------------------------------------------------------------------------------------------------
-------
 MAX  *   4.   4.   5.   2.   2.   2.   2.   4.   5.   5.   5.   4.   4.   3.   2.   2.   2.   4.
4.   4.
 DEGR. *  340   340   200   210   330   330   340   200   340   340    10    10    10    20    40    90    80   160
160   160

 THE HIGHEST CONCENTRATION OF      6. ug/m**3 OCCURRED AT RECEPTOR REC23.
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JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 WIND  * CONCENTRATION
 ANGLE *      (ug/m**3)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52 REC53 REC54 REC55 REC56 REC57 REC58
REC59 REC60

------*-----------------------------------------------------------------------------------------------------------
-------
   0. *   2.   2.   2.   0.   0.   0.   1.   2.   3.   3.   4.   3.   4.   2.   1.   1.   2.   3.
3.   3.
  10. *   1.   1.   1.   0.   0.   0.   0.   1.   1.   1.   5.   4.   4.   2.   1.   1.   2.   4.
4.   4.
  20. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   5.   4.   4.   2.   2.   1.   2.   4.
3.   3.
  30. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   4.   2.   2.   1.   2.   3.
3.   3.
  40. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   4.   2.   2.   1.   2.   3.
3.   2.
  50. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   3.   2.   2.   1.   2.   3.
```

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 6:33

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5135.6	6035.2	*	105.	326.	AG	0.	100.0	1.0	10.0	0.84	5.3
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5122.0	6010.9	*	90.	325.	AG	0.	100.0	1.0	20.0	0.71	4.6
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5403.5	6009.6	*	125.	51.	AG	0.	100.0	1.0	20.0	0.87	6.4
4.	Stan/Lom WB R	*	5292.4	5947.7	5347.6	5990.1	*	70.	52.	AG	0.	100.0	1.0	10.0	0.40	3.5
5.	Stan/Lom NB L	*	5307.6	5737.4	5359.5	5721.4	*	54.	107.	AG	0.	100.0	1.0	10.0	0.53	2.8
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5342.7	5755.7	*	30.	109.	AG	0.	100.0	1.0	20.0	0.25	1.5
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5200.8	5658.2	*	49.	196.	AG	0.	100.0	1.0	20.0	0.44	2.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5221.6	5646.0	*	55.	196.	AG	0.	100.0	1.0	10.0	0.32	2.8
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6475.2	7021.0	*	169.	334.	AG	0.	100.0	1.0	40.0	0.58	8.6
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.6	6936.2	*	104.	49.	AG	0.	100.0	1.0	20.0	0.69	5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6687.4	6942.0	*	86.	47.	AG	0.	100.0	1.0	10.0	0.28	4.4
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6613.9	6519.8	*	232.	177.	AG	0.	100.0	1.0	20.0	0.88	11.8
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6469.9	6706.8	*	84.	235.	AG	1.	100.0	1.0	30.0	0.47	4.3
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.3	6370.2	*	146.	358.	AG	0.	100.0	1.0	20.0	0.81	7.4
15.	Tha/Val NB L	*	6631.0	6138.6	6630.2	6047.3	*	91.	180.	AG	0.	100.0	1.0	10.0	0.55	4.6
16.	Tha/Val NB TR	*	6645.6	6138.6	6648.0	6000.5	*	138.	179.	AG	0.	100.0	1.0	10.0	0.76	7.0
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.7	6089.2	*	125.	0.	AG	0.	100.0	1.0	30.0	0.64	6.4
18.	Bev/Was EB RRR	*	6545.9	5954.3	6530.5	5976.1	*	27.	325.	AG	0.	100.0	1.0	30.0	0.14	1.4
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.8	5870.1	*	130.	358.	AG	0.	100.0	1.0	40.0	0.67	6.6
20.	Char/93 WB LTT	*	6702.8	5647.8	6712.2	5636.0	*	15.	141.	AG	0.	100.0	1.0	20.0	0.10	0.8
21.	Char/93 EB TTR	*	6560.8	5622.5	6523.0	5594.9	*	47.	234.	AG	0.	100.0	1.0	30.0	0.30	2.4
22.	North/Congress SB LT	*	6876.6	4408.9	6860.5	4488.9	*	82.	349.	AG	1.	100.0	1.0	30.0	0.62	4.1
23.	North/Con WB LLTR	*	6920.6	4378.3	7073.6	4432.5	*	162.	71.	AG	0.	100.0	1.0	20.0	0.82	8.2
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6920.4	4292.5	*	41.	172.	AG	0.	100.0	1.0	30.0	0.30	2.1
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.6	4340.9	*	5.	256.	AG	0.	100.0	1.0	10.0	0.03	0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1120.	0.0	1.0	90.0		
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1275.	0.0	1.0	78.0		
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	817.	0.0	1.0	78.0		
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1322.	0.0	1.0	78.0		
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3211.	0.0	1.0	90.0		
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1012.	0.0	1.0	66.0		
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2221.	0.0	1.0	90.0		
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1162.	0.0	1.0	78.0		
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2247.	0.0	1.0	90.0		
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	91.	0.0	1.0	38.0		
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2524.	0.0	1.0	90.0		
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	280.	0.0	1.0	54.0		
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	1841.	0.0	1.0	66.0		
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	269.	0.0	1.0	48.0		
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	80.	0.0	1.0	42.0		
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	811.	0.0	1.0	48.0		
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	374.	0.0	1.0	54.0		
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	650.	0.0	1.0	54.0		

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	406.	0.0	1.0	42.0		
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1226.	0.0	1.0	98.0		
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	978.	0.0	1.0	66.0		
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1420.	0.0	1.0	98.0		
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	44.	0.0	1.0	54.0		

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JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 6:33

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	90	70	3.0	223		1600	0.08		1	3				
2.	Stan/Lom SB TRR	*	90	66	3.0	481		1600	0.08		1	3				
3.	Stan/Lom WB LTT	*	90	68	3.0	527		1600	0.08		1	3				
4.	Stan/Lom WB R	*	90	48	3.0	265		1600	0.08		1	3				
5.	Stan/Lom NB L	*	90	70	3.0	142		1600	0.08		1	3				
6.	Stan/Lom NB TRR	*	90	66	3.0	166		1600	0.08		1	3				
7.	Stan/Lom EB LLT	*	90	68	3.0	265		1600	0.08		1	3				
8.	Stan/Lom EB R	*	90	48	3.0	208		1600	0.08		1	3				
9.	Caus/Wash SB LTTRR	*	150	56	3.0	2210		1600	0.08		1	3				
10.	Caus/Wash WB LLTT	*	150	125	3.0	296		1600	0.08		1	3				
11.	Caus/Wash WB R	*	150	73	3.0	216		1600	0.08		1	3				
12.	Caus/Wash NB TTR	*	150	108	3.0	693		1600	0.08		1	3				
13.	Caus/Wash EB LLTTR	*	150	119	3.0	388		1600	0.08		1	3				
14.	Tha/Val SB LTTR	*	100	34	3.0	1575		1600	0.08		1	3				
15.	Tha/Val NB L	*	100	66	3.0	253		1600	0.08		1	3				
16.	Tha/Val NB TR	*	100	34	3.0	743		1600	0.08		1	3				
17.	Bev/Was SB TTT	*	100	45	3.0	1528		1600	0.08		1	3				
18.	Bev/Was EB RRR	*	100	55	3.0	269		1600	0.08		1	3				
19.	Char/93 SB LLTTRR	*	100	53	3.0	1797		1600	0.08		1	3				
20.	Char/93 WB LTT	*	100	69	3.0	80		1600	0.08		1	3				
21.	Char/93 EB TTR	*	100	69	3.0	374		1600	0.08		1	3				
22.	North/Congress SB LT	*	100	75	3.0	598		1600	0.08		1	3				
23.	North/Con WB LLTR	*	100	60	3.0	916		1600	0.08		1	3				
24.	Nor/Con NB LTTTR	*	100	74	3.0	306		1600	0.08		1	3				
25.	Nor/Con EB LTR	*	100	60	3.0	16		1600	0.08		1	3				

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Bev/Was N1	*	6562.0	6150.2	6.0	*
2.	Bev/Was N2	*	6561.2	6075.2	6.0	*
3.	Bev/Was N3	*	6560.5	6000.2	6.0	*
4.	Bev/Was N4	*	6515.8	6060.4	6.0	*
5.	Bev/Was N5	*	6471.1	6120.6	6.0	*
6.	Bev/Was SE1	*	6671.0	6049.7	6.0	*
7.	Bev/Was SE2	*	6670.2	5966.3	6.0	*
8.	Bev/Was SE3	*	6624.0	5907.2	6.0	*
9.	Bev/Was SE4	*	6626.1	5832.3	6.0	*
10.	Bev/Was SE5	*	6628.1	5757.3	6.0	*
11.	Bev/Was SW1	*	6541.8	5766.9	6.0	*
12.	Bev/Was SW2	*	6540.1	5841.9	6.0	*
13.	Bev/Was SW3	*	6537.7	5916.8	6.0	*
14.	Bev/Was SW4	*	6493.0	5977.0	6.0	*
15.	Bev/Was SW5	*	6448.3	6037.3	6.0	*
16.	Char/93 NE1	*	6625.0	5871.1	6.0	*
17.	Char/93 NE2	*	6627.1	5796.1	6.0	*
18.	Char/93 NE3	*	6629.1	5721.1	6.0	*
19.	Char/93 NE4	*	6699.8	5695.9	6.0	*
20.	Char/93 NE5	*	6750.6	5633.2	6.0	*
21.	Char/93 S1	*	6657.8	5466.0	6.0	*
22.	Char/93 S2	*	6614.7	5527.4	6.0	*
23.	Char/93 S3	*	6571.7	5588.8	6.0	*
24.	Char/93 S4	*	6512.9	5542.2	6.0	*
25.	Char/93 S5	*	6454.1	5495.6	6.0	*
26.	Char/93 NW1	*	6424.1	5632.5	6.0	*

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JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 6:33

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Char/93 NW2	6483.6	5678.2	6.0
28. Char/93 NW3	6543.0	5723.9	6.0
29. Char/93 NW4	6541.0	5798.8	6.0
30. Char/93 NW5	6538.9	5873.8	6.0
31. Wash/Cong NE1	6910.2	4571.2	6.0
32. Wash/Cong NE2	6925.8	4497.8	6.0
33. Wash/Cong NE3	6941.4	4424.5	6.0
34. Wash/Cong NE4	7012.0	4449.6	6.0
35. Wash/Cong NE5	7082.7	4474.9	6.0
36. Wash/Cong SE1	7095.4	4388.1	6.0
37. Wash/Cong SE2	7024.8	4362.9	6.0
38. Wash/Cong SE3	6954.1	4337.7	6.0
39. Wash/Cong SE4	6968.4	4264.1	6.0
40. Wash/Cong SE5	6982.7	4190.4	6.0
41. Wash/Cong SW1	6867.5	4164.7	6.0
42. Wash/Cong SW2	6853.3	4238.0	6.0
43. Wash/Cong SW3	6838.9	4312.0	6.0
44. Wash/Cong SW4	6765.6	4296.1	6.0
45. Wash/Cong SW5	6692.3	4280.2	6.0
46. Wash/Cong NW1	6682.4	4353.8	6.0
47. Wash/Cong NW2	6755.7	4369.7	6.0
48. Wash/Cong NW3	6828.9	4386.0	6.0
49. Wash/Cong NW4	6813.3	4459.4	6.0
50. Wash/Cong NW5	6797.8	4532.8	6.0

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	4.	4.	3.	2.	1.	3.	3.	6.	4.	4.	3.	3.	3.	1.	1.	5.	4.	4.	1.	1.
10.	4.	4.	4.	2.	2.	1.	1.	5.	3.	2.	5.	4.	4.	2.	1.	4.	2.	2.	0.	0.
20.	4.	4.	5.	3.	2.	0.	0.	3.	1.	1.	5.	4.	4.	2.	2.	2.	1.	0.	0.	0.
30.	4.	4.	4.	2.	2.	0.	0.	2.	0.	0.	4.	4.	4.	2.	2.	1.	0.	0.	0.	0.
40.	4.	3.	4.	2.	2.	0.	0.	1.	0.	0.	4.	4.	4.	2.	2.	0.	0.	0.	0.	0.
50.	4.	3.	4.	2.	2.	0.	0.	1.	0.	0.	3.	3.	3.	2.	2.	0.	0.	0.	0.	0.
60.	4.	3.	4.	2.	2.	0.	0.	1.	0.	0.	3.	3.	3.	2.	2.	0.	0.	0.	0.	0.
70.	4.	3.	3.	2.	2.	0.	0.	0.	0.	0.	3.	3.	2.	2.	2.	0.	0.	0.	0.	0.
80.	3.	3.	3.	2.	2.	0.	0.	0.	0.	0.	3.	3.	2.	2.	2.	0.	0.	0.	0.	0.
90.	3.	4.	3.	2.	2.	0.	0.	0.	0.	0.	3.	3.	2.	2.	2.	0.	0.	0.	0.	0.
100.	3.	3.	3.	2.	2.	0.	0.	0.	0.	0.	3.	3.	2.	2.	2.	0.	0.	0.	0.	0.
110.	2.	3.	3.	2.	2.	0.	0.	0.	0.	0.	2.	3.	2.	2.	2.	0.	0.	0.	0.	0.
120.	3.	3.	3.	2.	2.	0.	0.	0.	0.	0.	2.	3.	2.	2.	2.	0.	0.	0.	0.	0.
130.	3.	3.	3.	2.	2.	0.	0.	0.	0.	0.	2.	3.	2.	2.	2.	0.	0.	0.	0.	0.
140.	3.	4.	3.	2.	2.	0.	0.	0.	0.	0.	2.	4.	3.	2.	2.	0.	0.	1.	0.	0.
150.	4.	4.	3.	2.	2.	0.	0.	0.	0.	0.	2.	4.	4.	2.	2.	0.	0.	1.	0.	0.
160.	4.	4.	4.	2.	2.	0.	0.	0.	1.	1.	2.	3.	4.	2.	1.	1.	1.	1.	1.	0.
170.	4.	4.	4.	2.	2.	1.	0.	1.	1.	1.	1.	2.	3.	1.	1.	1.	1.	1.	1.	1.
180.	3.	3.	3.	1.	1.	2.	1.	2.	1.	1.	1.	1.	2.	1.	0.	2.	1.	1.	1.	1.
190.	2.	2.	2.	1.	0.	3.	2.	3.	2.	1.	1.	1.	1.	0.	0.	3.	2.	1.	1.	1.
200.	1.	1.	1.	0.	0.	3.	3.	4.	3.	1.	1.	0.	0.	0.	0.	4.	2.	1.	1.	1.
210.	0.	0.	1.	0.	0.	4.	3.	4.	4.	2.	0.	0.	0.	0.	0.	4.	3.	1.	1.	1.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	2.	3.	4.	3.	2.	1.	1.	3.	3.	3.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.
10.	2.	2.	3.	3.	2.	1.	2.	4.	4.	4.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.
20.	1.	1.	2.	3.	2.	2.	2.	5.	4.	4.	0.	0.	0.	0.	0.	0.	2.	2.	1.	0.
30.	1.	1.	1.	2.	2.	2.	2.	4.	4.	4.	0.	0.	0.	0.	0.	0.	2.	2.	1.	0.
40.	1.	1.	1.	1.	1.	1.	2.	3.	4.	3.	0.	0.	0.	0.	0.	0.	1.	2.	0.	0.
50.	1.	1.	1.	1.	1.	1.	2.	3.	4.	3.	0.	0.	0.	0.	0.	0.	1.	2.	0.	0.
60.	1.	1.	1.	1.	0.	1.	1.	2.	3.	3.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
70.	1.	1.	1.	1.	0.	1.	1.	2.	3.	2.	0.	0.	1.	0.	0.	0.	0.	1.	0.	0.
80.	1.	1.	1.	1.	0.	1.	1.	1.	3.	2.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
90.	1.	1.	1.	1.	0.	2.	1.	1.	3.	2.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
100.	1.	1.	1.	1.	0.	2.	1.	0.	3.	3.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
110.	1.	1.	1.	0.	0.	2.	2.	0.	3.	3.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
120.	1.	1.	1.	0.	0.	1.	2.	1.	3.	3.	0.	1.	2.	2.	0.	0.	0.	0.	0.	0.
130.	0.	1.	1.	0.	0.	1.	2.	1.	3.	4.	0.	1.	2.	2.	0.	0.	0.	0.	0.	0.
140.	0.	0.	0.	0.	0.	1.	2.	2.	3.	4.	1.	1.	2.	2.	0.	0.	0.	0.	0.	0.
150.	0.	0.	0.	0.	0.	1.	2.	2.	3.	4.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
160.	1.	1.	1.	1.	0.	1.	2.	2.	3.	4.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
170.	1.	1.	1.	1.	0.	1.	2.	2.	3.	4.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
180.	1.	1.	1.	1.	0.	1.	2.	2.	3.	4.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
190.	1.	1.	1.	1.	0.	1.	2.	2.	3.	4.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
200.	1.	1.	1.	1.	0.	1.	2.	2.	3.	4.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
210.	1.	1.	1.	1.	0.	1.	2.	2.	3.	4.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
220.	0.	0.	1.	0.	0.	4.	3.	3.	4.	2.	0.	0.	0.	0.	0.	4.	3.	1.	1.	1.
230.	1.	0.	1.	0.	0.	4.	3.	3.	4.	2.	0.	0.	0.	0.	0.	3.	3.	1.	1.	1.
240.	1.	0.	1.	0.	0.	3.	3.	3.	3.	2.	0.	0.	0.	0.	0.	3.	3.	1.	1.	1.
250.	1.	0.	1.	0.	0.	3.	3.	2.	3.	2.	0.	0.	0.	0.	0.	3.	3.	1.	1.	1.
260.	1.	0.	1.	0.	0.	3.	3.	2.	3.	3.	0.	0.	0.	0.	0.	3.	3.	1.	1.	1.
270.	1.	0.	0.	0.	0.	4.	3.	2.	3.	3.	0.	0.	0.	0.	0.	3.	4.	1.	1.	1.
280.	0.	0.	0.	0.	0.	3.	3.	2.	3.	3.	0.	0.	0.	0.	0.	2.	3.	1.	2.	1.
290.	0.	0.	0.	0.	0.	3.	3.	2.	3.	3.	0.	0.	0.	0.	0.	2.	3.	2.	1.	1.
300.	0.	0.	0.	0.	0.	3.	3.	2.	3.	3.	0.	0.	0.	0.	0.	2.	3.	2.	1.	1.
310.	0.	0.	0.	0.	0.	3.	3.	3.	3.	3.	0.	0.	0.	0.	0.	2.	3.	3.	2.	1.
320.	0.	0.	0.	0.	0.	4.	4.	3.	3.	4.	0.	0.	0.	0.	0.	3.	4.	3.	2.	1.
330.	0.	0.	0.	0.	0.	4.	4.	4.	3.	4.	0.	0.	0.	0.	0.	3.	4.	4.	2.	2.
340.	1.	1.	1.	0.	0.	5.	4.	5.	4.	4.	0.	0.	1.	0.	0.	4.	4.	4.	2.	2.
350.	2.	2.	2.	1.	0.	4.	4.	6.	4.	4.	1.	1.	2.	1.	0.	5.	4.	4.	2.	2.
360.	4.	4.	3.	2.	1.	3.	3.	6.	4.	4.	3.	3.	3.	1.	1.	5.	4.	4.	1.	1.
MAX	4.	4.	5.	3.	2.	5.	4.	6.	4.	4.	5.	4.	4.	2.	2.	5.	4.	4.	2.	2.
DEGR.	20	10	20	20	150	340	340	0	350	340	20	10	10	90	20	350	340	340	350	280

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

160.	*	0.	0.	0.	0.	0.	1.	1.	2.	2.	4.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
170.	*	0.	0.	0.	0.	0.	1.	1.	2.	2.	3.	2.	2.	3.	2.	1.	0.	0.	1.
1.	1.																		
180.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	3.	2.	1.	0.	0.	2.
1.	1.																		
190.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	3.	2.	2.	0.	0.	2.
2.	1.																		
200.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	3.	3.	2.	0.	1.	2.
2.	2.																		
210.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	3.	2.	0.	1.	2.
2.	2.																		
220.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.
1.	1.																		
230.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
240.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
250.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	1.	2.	2.
1.	1.																		
260.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	2.	2.
1.	1.																		
270.	*	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.
1.	1.																		
280.	*	0.	1.	2.	1.	0.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.
1.	1.																		
290.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	3.	2.
2.	1.																		
300.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	3.	3.
2.	1.																		
310.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	3.
2.	2.																		
320.	*	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	3.
3.	2.																		
330.	*	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	3.
3.	2.																		
340.	*	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	3.
3.	2.																		
350.	*	3.	3.	3.	2.	1.	0.	0.	1.	2.	1.	1.	1.	1.	0.	0.	1.	2.	3.
2.	2.																		
360.	*	2.	3.	4.	3.	2.	1.	1.	3.	3.	3.	0.	0.	0.	0.	0.	1.	1.	2.
1.	1.																		
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
-------																			
MAX	*	3.	3.	4.	3.	2.	2.	2.	5.	4.	4.	2.	2.	3.	3.	2.	2.	3.	3.
3.	2.																		
DEGR.	*	350	0	0	10	20	100	30	20	10	10	180	180	190	210	210	280	290	330
330	330																		

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50
0.	*	2.	2.	2.	1.	0.	1.	1.	2.	2.	2.
10.	*	2.	2.	2.	1.	0.	0.	0.	2.	1.	1.
20.	*	2.	2.	2.	1.	0.	0.	1.	2.	1.	1.
30.	*	2.	3.	2.	1.	1.	0.	1.	2.	1.	1.
40.	*	2.	3.	2.	1.	1.	1.	1.	2.	1.	1.
50.	*	1.	2.	2.	2.	1.	1.	1.	2.	2.	1.
60.	*	1.	2.	3.	2.	1.	1.	1.	2.	2.	1.
70.	*	1.	2.	3.	2.	1.	1.	2.	2.	2.	1.
80.	*	1.	1.	2.	1.	1.	1.	2.	3.	2.	1.
90.	*	1.	1.	2.	1.	1.	1.	2.	3.	3.	1.
100.	*	1.	1.	2.	1.	1.	1.	2.	2.	3.	1.
110.	*	1.	1.	2.	1.	0.	1.	1.	2.	3.	2.
120.	*	1.	1.	2.	1.	1.	1.	1.	2.	3.	2.
130.	*	2.	2.	2.	1.	0.	0.	1.	2.	3.	3.
140.	*	2.	2.	2.	1.	0.	0.	1.	2.	2.	3.
150.	*	1.	2.	2.	0.	0.	0.	1.	2.	2.	3.
160.	*	1.	1.	1.	0.	0.	0.	0.	2.	2.	2.
170.	*	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
180.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
190.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
200.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
210.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
220.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

240.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
250.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
260.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
270.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
280.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
290.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
300.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
310.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
320.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
330.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
340.	*	1.	1.	0.	0.	0.	0.	0.	0.	0.
350.	*	1.	2.	2.	0.	0.	0.	2.	1.	1.
360.	*	2.	2.	2.	1.	0.	1.	2.	2.	2.
------	*	----	----	----	----	----	----	----	----	----
MAX	*	2.	3.	3.	2.	1.	1.	2.	3.	3.
DEGR.	*	10	30	60	60	70	80	90	80	110	140

THE HIGHEST CONCENTRATION OF 6. ug/m**3 OCCURRED AT RECEPTOR REC8 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Existing

DATE : 7/22/13
TIME : 15: 4:38

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5135.6	6035.1	*	105.	326.	AG	0.	100.0	1.0	10.0	0.81	5.3
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5086.9	6061.1	*	151.	325.	AG	0.	100.0	1.0	20.0	0.88	7.7
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5356.6	5971.2	*	64.	51.	AG	0.	100.0	1.0	20.0	0.43	3.3
4.	Stan/Lom WB R	*	5292.4	5947.7	5467.2	6081.9	*	220.	52.	AG	0.	100.0	1.0	10.0	1.01	11.2
5.	Stan/Lom NB L	*	5307.6	5737.4	5334.8	5729.0	*	29.	107.	AG	0.	100.0	1.0	10.0	0.26	1.4
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5348.1	5753.9	*	36.	109.	AG	0.	100.0	1.0	20.0	0.26	1.8
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5194.5	5636.4	*	72.	196.	AG	0.	100.0	1.0	20.0	0.48	3.6
8.	Stan/Lom EB R	*	5236.5	5698.5	5057.8	5069.3	*	654.	196.	AG	0.	100.0	1.0	10.0	1.17	33.2
9.	Char/93 SB LLTTRR	*	6587.8	5740.0	6583.0	5866.1	*	126.	358.	AG	1.	100.0	1.0	40.0	0.70	6.4
10.	Char/93 WB LTT	*	6702.8	5647.8	6733.3	5609.6	*	49.	141.	AG	0.	100.0	1.0	20.0	0.27	2.5
11.	Char/93 EB TTR	*	6560.8	5622.5	6480.8	5564.0	*	99.	234.	AG	0.	100.0	1.0	30.0	0.54	5.0
12.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1289.	0.0	1.0	90.0		
13.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1112.	0.0	1.0	78.0		
14.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	999.	0.0	1.0	78.0		
15.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1207.	0.0	1.0	78.0		
16.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	1635.	0.0	1.0	66.0		
17.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	298.	0.0	1.0	42.0		
18.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	847.	0.0	1.0	48.0		
19.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	908.	0.0	1.0	54.0		
20.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	449.	0.0	1.0	54.0		
21.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	314.	0.0	1.0	42.0		

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JOB: Government Center Garage RUN: Existing

DATE : 7/22/13
TIME : 15: 4:38

		*								
1.	Stan/Lom SB L	*	100	79	3.0	208	1600	0.08	1	3
2.	Stan/Lom SB TRR	*	100	74	3.0	595	1600	0.08	1	3
3.	Stan/Lom WB LTT	*	100	71	3.0	332	1600	0.08	1	3
4.	Stan/Lom WB R	*	100	79	3.0	259	1600	0.08	1	3
5.	Stan/Lom NB L	*	100	79	3.0	66	1600	0.08	1	3
6.	Stan/Lom NB TRR	*	100	74	3.0	176	1600	0.08	1	3
7.	Stan/Lom EB LLT	*	100	71	3.0	371	1600	0.08	1	3
8.	Stan/Lom EB R	*	100	79	3.0	300	1600	0.08	1	3
9.	Char/93 SB LLTTRR	*	100	62	3.0	1488	1600	0.08	1	3
10.	Char/93 WB LTT	*	100	60	3.0	298	1600	0.08	1	3
11.	Char/93 EB TTR	*	100	60	3.0	908	1600	0.08	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8.	Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0	*

		*			
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0 *
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0 *
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0 *
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0 *
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0 *
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0 *
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0 *
21.	Char/93 NE1	*	6625.0	5871.1	6.0 *
22.	Char/93 NE2	*	6627.1	5796.1	6.0 *
23.	Char/93 NE3	*	6629.1	5721.1	6.0 *
24.	Char/93 NE4	*	6699.8	5695.9	6.0 *
25.	Char/93 NE5	*	6750.6	5633.2	6.0 *
26.	Char/93 S1	*	6657.8	5466.0	6.0 *
27.	Char/93 S2	*	6614.7	5527.4	6.0 *
28.	Char/93 S3	*	6571.7	5588.8	6.0 *
29.	Char/93 S4	*	6512.9	5542.2	6.0 *
30.	Char/93 S5	*	6454.1	5495.6	6.0 *
31.	Char/93 NW1	*	6424.1	5632.5	6.0 *
32.	Char/93 NW2	*	6483.6	5678.2	6.0 *
33.	Char/93 NW3	*	6543.0	5723.9	6.0 *
34.	Char/93 NW4	*	6541.0	5798.8	6.0 *
35.	Char/93 NW5	*	6538.9	5873.8	6.0 *

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JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	1.	2.	2.	2.	3.	1.	1.	1.	2.	3.
10. *	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.
20. *	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.
30. *	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	1.	2.	1.	1.	2.	2.	2.	1.	2.
40. *	0.	0.	0.	0.	0.	1.	2.	2.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	2.	2.
50. *	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	1.	1.	2.	1.	0.	2.	2.	1.	2.	2.
60. *	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	1.	3.	3.
70. *	0.	0.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	0.	2.	3.
80. *	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	0.	2.	3.
90. *	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	1.	2.	3.
100. *	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	1.	2.
110. *	1.	1.	2.	2.	2.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	2.	2.	2.	1.	2.
120. *	1.	1.	1.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	2.
130. *	1.	1.	1.	2.	2.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	2.
140. *	1.	1.	2.	2.	2.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	1.
150. *	2.	2.	2.	3.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.
160. *	2.	2.	2.	3.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
170. *	2.	2.	2.	3.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
180. *	3.	2.	3.	3.	2.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
190. *	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	1.	2.	2.	1.	0.
200. *	2.	2.	3.	3.	3.	1.	2.	2.	2.	1.	0.	0.	2.	1.	1.	1.	1.	1.	0.	0.
210. *	2.	2.	2.	3.	3.	1.	2.	2.	3.	1.	0.	0.	2.	2.	2.	0.	0.	0.	0.	0.
220. *	2.	2.	2.	2.	2.	1.	1.	1.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
230. *	2.	2.	1.	1.	2.	1.	1.	0.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
240. *	2.	2.	1.	1.	1.	1.	0.	0.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.

0.	0.																	
250.	*	2.	2.	1.	1.	1.	1.	1.	0.	1.	2.	1.	1.	2.	2.	2.	0.	0.	0.
0.	0.																	
260.	*	2.	2.	2.	1.	1.	2.	1.	0.	1.	2.	1.	1.	2.	2.	2.	0.	0.	0.
0.	0.																	
270.	*	2.	2.	2.	1.	1.	2.	1.	0.	1.	2.	1.	1.	1.	2.	2.	0.	0.	0.
0.	0.																	
280.	*	2.	2.	2.	1.	1.	3.	2.	0.	1.	1.	1.	1.	1.	2.	2.	0.	0.	0.
0.	0.																	
290.	*	1.	2.	2.	1.	0.	3.	2.	0.	0.	1.	1.	1.	1.	2.	2.	0.	0.	0.
0.	0.																	
300.	*	2.	2.	2.	1.	0.	2.	3.	1.	1.	1.	1.	1.	1.	2.	2.	0.	0.	0.
0.	0.																	
310.	*	1.	2.	2.	0.	0.	2.	3.	1.	2.	1.	2.	1.	1.	2.	2.	0.	0.	0.
0.	0.																	
320.	*	1.	1.	2.	0.	0.	2.	2.	2.	2.	1.	2.	2.	2.	2.	2.	0.	0.	0.
1.	1.																	
330.	*	0.	1.	1.	0.	0.	2.	2.	3.	2.	1.	2.	2.	2.	3.	2.	0.	0.	1.
2.	2.																	
340.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	2.	2.	3.	3.	0.	0.	1.
2.	2.																	
350.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	2.	2.	2.	3.	1.	1.	1.
2.	3.																	
360.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	1.	2.	2.	2.	3.	1.	1.	1.
2.	3.																	

MAX	*	3.	2.	3.	3.	3.	3.	3.	3.	3.	2.	2.	2.	2.	3.	3.	2.	2.	2.
3.	3.																	
DEGR.	*	180	180	190	190	200	280	310	330	210	250	320	350	220	330	0	60	100	180
60	0																	

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35
0.	*	0.	1.	1.	0.	0.	2.	2.	2.	3.	2.	0.	0.	1.	1.	0.
10.	*	0.	0.	0.	0.	0.	1.	2.	2.	3.	2.	0.	0.	2.	2.	0.
20.	*	0.	0.	0.	0.	0.	1.	1.	2.	3.	3.	0.	1.	3.	2.	1.
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	3.	3.	1.	1.	3.	3.	1.
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.	1.	2.	3.	3.	1.
50.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	3.	3.	1.
60.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	3.	2.
70.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	3.	2.
80.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	3.	2.
90.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	1.	1.	3.	2.
100.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	1.	0.	3.	2.
110.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	3.	3.
120.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	1.	3.	3.
130.	*	0.	0.	1.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	3.	4.
140.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	3.	4.
150.	*	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	2.	2.	3.	4.
160.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	2.	3.
170.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	2.	2.
180.	*	2.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	1.
190.	*	3.	2.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.
200.	*	4.	2.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.
210.	*	4.	3.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
220.	*	4.	3.	2.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
230.	*	3.	3.	2.	2.	2.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
240.	*	3.	3.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
250.	*	3.	3.	1.	2.	2.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
260.	*	3.	3.	1.	1.	2.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
270.	*	2.	3.	1.	1.	2.	0.	1.	3.	2.	1.	0.	0.	0.	0.	0.
280.	*	2.	3.	1.	1.	2.	0.	1.	3.	2.	1.	0.	0.	0.	0.	0.
290.	*	2.	3.	2.	1.	2.	1.	1.	3.	2.	1.	0.	0.	0.	0.	0.
300.	*	2.	3.	2.	2.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
310.	*	1.	3.	3.	2.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
320.	*	1.	3.	3.	2.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
330.	*	1.	3.	3.	1.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
340.	*	1.	2.	3.	1.	0.	2.	1.	2.	2.	1.	0.	0.	0.	0.	0.
350.	*	0.	1.	2.	0.	0.	2.	2.	2.	3.	1.	0.	0.	0.	0.	0.
360.	*	0.	1.	1.	0.	0.	2.	2.	2.	3.	2.	0.	0.	1.	1.	0.
MAX	*	4.	3.	3.	2.	2.	2.	2.	3.	3.	3.	2.	2.	3.	3.	4.
DEGR.	*	210	220	330	240	270	350	350	280	10	20	110	130	30	130	150

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17: 9:33

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6054.9	5445.6	*	60.	290.	AG	1.	100.0	1.0	30.0	0.48	3.1
2. Char/Merr WB	*	6250.4	5435.2	6323.7	5493.2	*	93.	52.	AG	1.	100.0	1.0	30.0	0.71	4.7
3. Char/Merr NB R	*	6291.7	5369.7	6313.9	5354.6	*	27.	124.	AG	0.	100.0	1.0	10.0	0.14	1.4
4. Char/Merr NB LTT	*	6280.4	5347.2	6395.2	5266.3	*	140.	125.	AG	0.	100.0	1.0	20.0	0.83	7.1
5. Char/Merr EB	*	6104.2	5362.2	6064.9	5347.6	*	42.	250.	AG	0.	100.0	1.0	20.0	0.38	2.1
6. Char/Cam SB L	*	5384.1	4834.2	5408.6	4932.0	*	101.	14.	AG	0.	100.0	1.0	10.0	0.66	5.1
7. Char/Cam SB TR	*	5360.8	4833.5	5392.6	4936.4	*	108.	17.	AG	0.	100.0	1.0	20.0	0.86	5.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5448.9	4784.7	*	39.	103.	AG	0.	100.0	1.0	20.0	0.24	2.0
9. Char/Cam NB L	*	5363.0	4722.4	5361.1	4639.9	*	82.	181.	AG	0.	100.0	1.0	10.0	0.54	4.2
10. Char/Cam NB TR	*	5383.3	4723.8	5384.3	4657.5	*	66.	179.	AG	0.	100.0	1.0	20.0	0.67	3.4
11. Char/Cam EB TTTR	*	5302.7	4739.8	5222.9	4740.6	*	80.	271.	AG	0.	100.0	1.0	30.0	0.49	4.1
12. Sud/Merr SB L	*	6532.7	5210.3	6493.6	5238.2	*	48.	305.	AG	0.	100.0	1.0	10.0	0.66	2.4
13. Sud/Merr SB TTT	*	6518.3	5190.8	6480.9	5212.4	*	43.	300.	AG	0.	100.0	1.0	30.0	0.22	2.2
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6669.4	5076.1	*	98.	150.	AG	0.	100.0	1.0	30.0	0.55	5.0
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6482.0	5121.0	*	48.	239.	AG	1.	100.0	1.0	40.0	0.34	2.5
16. Sud/Sur SB LTT	*	6777.5	5369.7	6741.1	5415.5	*	59.	322.	AG	0.	100.0	1.0	20.0	0.30	3.0
17. Sud/Sur SEB	*	6757.2	5330.0	6747.9	5332.3	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6750.6	5242.3	*	47.	249.	AG	1.	100.0	1.0	30.0	0.39	2.4
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	802.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1038.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1204.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	870.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	923.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1472.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	877.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1546.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	285.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	483.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	405.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	338.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	25.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1421.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1512.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	487.	0.0	1.0	78.0		

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1. Char/Merr SB	*	100	76	3.0	436	1600	0.08	1	3
2. Char/Merr WB	*	100	76	3.0	650	1600	0.08	1	3
3. Char/Merr NB R	*	100	45	3.0	109	1600	0.08	1	3
4. Char/Merr NB LTT	*	100	71	3.0	637	1600	0.08	1	3
5. Char/Merr EB	*	100	79	3.0	194	1600	0.08	1	3
6. Char/Cam SB L	*	90	58	3.0	318	1600	0.08	1	3
7. Char/Cam SB TR	*	90	71	3.0	429	1600	0.08	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	265	1600	0.08	1	3
9. Char/Cam NB L	*	90	58	3.0	260	1600	0.08	1	3
10. Char/Cam NB TR	*	90	71	3.0	330	1600	0.08	1	3

11. Char/Cam EB TTTR	*	90	54	3.0	811	1600	0.08	1	3
12. Sud/Merr SB L	*	100	86	3.0	95	1600	0.08	1	3
13. Sud/Merr SB TTT	*	100	49	3.0	484	1600	0.08	1	3
14. Sud/Merr NB TTTR	*	100	63	3.0	854	1600	0.08	1	3
15. Sud/Merr EB LTTR	*	100	73	3.0	487	1600	0.08	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	405	1600	0.08	1	3
17. Sud/Sur SEB	*	100	70	3.0	25	1600	0.08	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	338	1600	0.08	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Char/Merr NE1	*	6063.7	5511.0	6.0	*
2. Char/Merr NE2	*	6133.9	5484.8	6.0	*
3. Char/Merr NE3	*	6204.2	5458.5	6.0	*
4. Char/Merr NE4	*	6265.6	5501.5	6.0	*
5. Char/Merr NE5	*	6327.1	5544.5	6.0	*
6. Char/Merr SE1	*	6443.7	5491.9	6.0	*
7. Char/Merr SE2	*	6382.2	5448.9	6.0	*
8. Char/Merr SE3	*	6320.8	5405.9	6.0	*
9. Char/Merr SE4	*	6380.5	5360.4	6.0	*
10. Char/Merr SE5	*	6440.1	5315.0	6.0	*
11. Char/Merr SW1	*	6332.0	5249.0	6.0	*
12. Char/Merr SW2	*	6272.3	5294.5	6.0	*
13. Char/Merr SW3	*	6212.6	5339.9	6.0	*
14. Char/Merr SW4	*	6141.6	5315.8	6.0	*
15. Char/Merr SW5	*	6070.6	5291.7	6.0	*
16. Char/Merr NW1	*	5902.1	5359.1	6.0	*
17. Char/Merr NW2	*	5973.1	5383.2	6.0	*
18. Char/Merr NW3	*	6044.1	5407.3	6.0	*
19. Char/Merr NW4	*	5973.9	5433.5	6.0	*
20. Char/Merr NW5	*	5903.6	5459.8	6.0	*
21. Char/Cam NE1	*	5490.2	4963.0	6.0	*
22. Char/Cam NE2	*	5459.0	4894.8	6.0	*
23. Char/Cam NE3	*	5427.8	4826.6	6.0	*
24. Char/Cam NE4	*	5500.4	4807.6	6.0	*
25. Char/Cam NE5	*	5572.9	4788.7	6.0	*
26. Char/Cam SE1	*	5553.9	4667.5	6.0	*
27. Char/Cam SE2	*	5481.3	4686.5	6.0	*
28. Char/Cam SE3	*	5408.7	4705.4	6.0	*
29. Char/Cam SE4	*	5409.4	4630.4	6.0	*
30. Char/Cam SE5	*	5410.1	4555.4	6.0	*
31. Char/Cam SW1	*	5312.0	4561.9	6.0	*
32. Char/Cam SW2	*	5310.7	4636.9	6.0	*
33. Char/Cam SW3	*	5310.7	4711.9	6.0	*

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RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
34. Char/Cam SW4	*	5235.6	4712.1	6.0	*
35. Char/Cam SW5	*	5160.6	4711.9	6.0	*
36. Char/Cam NW1	*	5167.9	4822.4	6.0	*
37. Char/Cam NW2	*	5242.9	4822.1	6.0	*
38. Char/Cam NW3	*	5317.9	4821.9	6.0	*
39. Char/Cam NW4	*	5349.1	4890.1	6.0	*
40. Char/Cam NW5	*	5380.3	4958.3	6.0	*

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	1.	2.	0.	0.	1.	1.	1.
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	1.	2.	0.	0.	1.	1.	1.
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	3.	3.	2.	2.	0.	0.	2.		

1.	1.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	0.	2.
1.	1.																		
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	1.	2.
1.	1.																		
50.	*	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
60.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	1.	2.	2.
1.	1.																		
70.	*	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	2.	1.	2.	2.	3.
2.	1.																		
80.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.
2.	2.																		
90.	*	1.	1.	2.	2.	1.	0.	0.	0.	0.	1.	2.	2.	2.	1.	1.	2.	2.	3.
3.	2.																		
100.	*	1.	2.	2.	2.	1.	0.	0.	0.	0.	1.	2.	3.	2.	1.	1.	2.	2.	3.
3.	2.																		
110.	*	2.	2.	2.	2.	1.	0.	0.	1.	1.	1.	2.	2.	3.	1.	1.	2.	2.	2.
2.	2.																		
120.	*	2.	2.	3.	2.	1.	0.	0.	1.	1.	2.	2.	2.	2.	1.	0.	1.	2.	2.
2.	2.																		
130.	*	2.	3.	4.	3.	1.	0.	1.	2.	2.	3.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
140.	*	2.	3.	4.	4.	2.	1.	1.	2.	3.	3.	0.	1.	1.	0.	0.	1.	1.	1.
1.	0.																		
150.	*	2.	2.	3.	4.	2.	1.	2.	2.	2.	3.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
160.	*	2.	2.	2.	3.	2.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	1.	1.	1.
1.	0.																		
170.	*	2.	1.	2.	3.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
180.	*	2.	2.	2.	3.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
190.	*	2.	2.	2.	3.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
1.	0.																		
200.	*	2.	2.	2.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
1.	0.																		
210.	*	1.	2.	2.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
220.	*	2.	3.	2.	2.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	2.
1.	0.																		
230.	*	1.	2.	2.	2.	2.	1.	1.	2.	2.	2.	0.	0.	0.	1.	1.	1.	1.	1.
1.	0.																		
240.	*	1.	2.	2.	2.	1.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
250.	*	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
260.	*	1.	1.	2.	1.	1.	2.	3.	3.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
270.	*	1.	1.	2.	0.	0.	2.	3.	3.	3.	2.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
280.	*	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	1.	2.	1.	1.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	1.	0.	0.	1.	2.	3.	2.	2.	1.	1.	2.	1.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	1.	2.	2.	2.	1.	0.	0.	1.
1.	0.																		
310.	*	0.	0.	0.	0.	0.	1.	1.	2.	2.	1.	2.	2.	2.	2.	1.	0.	0.	1.
1.	0.																		
320.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	1.	0.	0.	1.
1.	1.																		
330.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	1.	0.	0.	1.
1.	1.																		
340.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	1.	0.	0.	1.
1.	1.																		
350.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	2.	2.	0.	0.	1.
1.	1.																		
360.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	1.	2.	0.	0.	1.
1.	1.																		

MAX	*	2.	3.	4.	4.	3.	2.	3.	3.	3.	3.	2.	3.	3.	2.	2.	2.	2.	3.
3.	2.																		
DEGR.	*	130	130	130	140	200	260	260	270	140	150	350	100	30	50	30	90	90	90
100	100																		

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38
REC39	REC40																		
0.	*	0.	1.	1.	0.	0.	1.	1.	3.	2.	2.	2.	2.	2.	3.	2.	0.	0.	0.
0.	0.																		
10.	*	0.	1.	1.	0.	0.	1.	1.	2.	2.	1.	2.	2.	3.	3.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	1.	0.	0.	2.	1.	2.	1.	1.	2.	3.	3.	3.	1.	0.	0.	1.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	3.	4.	3.	2.	0.	0.	1.
1.	0.																		
40.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	3.	4.	4.	2.	0.	0.	2.
2.	1.																		
50.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	3.	3.	4.	3.	1.	1.	2.
2.	1.																		
60.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.	4.	3.	1.	1.	2.
3.	1.																		
70.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.	4.	3.	1.	1.	2.
2.	1.																		
80.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	1.	2.
2.	1.																		
90.	*	0.	0.	0.	0.	0.	1.	2.	2.	2.	0.	0.	1.	2.	3.	2.	2.	2.	3.
2.	1.																		
100.	*	0.	0.	1.	1.	0.	1.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	3.	3.
2.	1.																		
110.	*	0.	0.	1.	1.	1.	0.	0.	1.	0.	0.	0.	1.	1.	2.	1.	1.	3.	3.
4.	2.																		
120.	*	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	3.	3.
4.	3.																		
130.	*	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	3.	3.
3.	2.																		
140.	*	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	3.
3.	2.																		
150.	*	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	3.
3.	2.																		
160.	*	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.
4.	3.																		
170.	*	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.
3.	4.																		
180.	*	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	1.	0.	0.	2.	2.
3.	4.																		
190.	*	1.	2.	3.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
2.	3.																		
200.	*	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
2.	2.																		
210.	*	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
2.	2.																		
220.	*	2.	2.	3.	2.	2.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.
1.	1.																		
230.	*	3.	3.	3.	2.	2.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.
1.	1.																		
240.	*	2.	3.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.
1.	0.																		
250.	*	2.	2.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
1.	0.																		
260.	*	1.	2.	3.	3.	3.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.
0.	0.																		
270.	*	1.	2.	2.	3.	3.	1.	2.	3.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.
0.	0.																		
280.	*	1.	2.	2.	2.	2.	2.	2.	4.	1.	1.	0.	0.	2.	1.	1.	0.	0.	0.
0.	0.																		
290.	*	1.	2.	2.	1.	1.	2.	3.	4.	2.	1.	0.	0.	3.	2.	1.	0.	0.	0.
0.	0.																		
300.	*	1.	1.	2.	1.	1.	2.	2.	4.	2.	1.	0.	1.	3.	2.	2.	0.	0.	0.
0.	0.																		
310.	*	1.	1.	2.	1.	1.	2.	2.	4.	3.	2.	0.	1.	3.	2.	2.	0.	0.	0.
0.	0.																		
320.	*	1.	1.	2.	1.	0.	2.	2.	3.	3.	2.	1.	1.	3.	2.	2.	0.	0.	0.
0.	0.																		
330.	*	1.	1.	2.	1.	0.	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
340.	*	1.	1.	2.	0.	0.	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	1.	1.	0.	0.	1.	2.	3.	3.	2.	1.	2.	2.	2.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	1.	1.	0.	0.	1.	1.	3.	2.	2.	2.	2.	2.	3.	2.	0.	0.	0.
0.	0.																		

MAX	*	3.	3.	3.	3.	3.	2.	3.	4.	3.	2.	2.	3.	4.	4.	3.	3.	3.	4.
4.	4.																		
DEGR.	*	230	230	240	260	260	300	290	290	320	340	20	20	40	50	70	110	110	110
170	170																		

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC34.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17: 7:49

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6042.2	5450.2	*	74.	290.	AG	1.	100.0	1.0	30.0	0.56	3.8
2. Char/Merr WB	*	6250.4	5435.2	6300.3	5474.7	*	64.	52.	AG	1.	100.0	1.0	30.0	0.55	3.2
3. Char/Merr NB R	*	6291.7	5369.7	6341.8	5335.7	*	61.	124.	AG	0.	100.0	1.0	10.0	0.31	3.1
4. Char/Merr NB LTT	*	6280.4	5347.2	6349.1	5298.8	*	84.	125.	AG	0.	100.0	1.0	20.0	0.52	4.3
5. Char/Merr EB	*	6104.2	5362.2	6005.8	5325.6	*	105.	250.	AG	0.	100.0	1.0	20.0	0.81	5.3
6. Char/Cam SB L	*	5384.1	4834.2	5401.1	4902.3	*	70.	14.	AG	0.	100.0	1.0	10.0	0.38	3.6
7. Char/Cam SB TR	*	5360.8	4833.5	5374.3	4877.1	*	46.	17.	AG	0.	100.0	1.0	20.0	0.32	2.3
8. Char/Cam WB LTTR	*	5411.0	4793.5	5475.3	4778.6	*	66.	103.	AG	0.	100.0	1.0	20.0	0.37	3.4
9. Char/Cam NB L	*	5363.0	4722.4	5361.0	4631.8	*	91.	181.	AG	0.	100.0	1.0	10.0	0.49	4.6
10. Char/Cam NB TR	*	5383.3	4723.8	5384.8	4624.7	*	99.	179.	AG	0.	100.0	1.0	20.0	0.68	5.0
11. Char/Cam EB TTTR	*	5302.7	4739.8	5220.6	4740.7	*	82.	271.	AG	0.	100.0	1.0	30.0	0.46	4.2
12. Sud/Merr SB L	*	6532.7	5210.3	6496.1	5236.4	*	45.	305.	AG	0.	100.0	1.0	10.0	0.56	2.3
13. Sud/Merr SB TTT	*	6518.3	5190.8	6487.3	5208.8	*	36.	300.	AG	0.	100.0	1.0	30.0	0.18	1.8
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6672.2	5071.1	*	104.	150.	AG	0.	100.0	1.0	30.0	0.62	5.3
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6458.9	5107.1	*	75.	239.	AG	1.	100.0	1.0	40.0	0.52	3.8
16. Sud/Sur SB LTT	*	6777.5	5369.7	6739.2	5418.0	*	62.	322.	AG	0.	100.0	1.0	20.0	0.40	3.1
17. Sud/Sur SEB	*	6757.2	5330.0	6742.4	5333.7	*	15.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6722.2	5231.2	*	78.	249.	AG	0.	100.0	1.0	30.0	0.39	3.9
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	818.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1226.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1219.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	859.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	796.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1264.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	954.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1198.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	805.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	405.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	322.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	853.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	35.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1185.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1465.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	766.	0.0	1.0	78.0		

DATE : 8/ 7/13
TIME : 17: 7:49

1. Char/Merr SB	*	100	75	3.0	541	1600	0.08	1	3
2. Char/Merr WB	*	100	78	3.0	449	1600	0.08	1	3
3. Char/Merr NB R	*	100	46	3.0	241	1600	0.08	1	3
4. Char/Merr NB LTT	*	100	68	3.0	452	1600	0.08	1	3
5. Char/Merr EB	*	100	79	3.0	417	1600	0.08	1	3
6. Char/Cam SB L	*	100	60	3.0	214	1600	0.08	1	3
7. Char/Cam SB TR	*	100	72	3.0	233	1600	0.08	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	391	1600	0.08	1	3
9. Char/Cam NB L	*	100	60	3.0	276	1600	0.08	1	3
10. Char/Cam NB TR	*	100	72	3.0	503	1600	0.08	1	3

11. Char/Cam EB TTTR	*	100	62	3.0	726	1600	0.08	1	3
12. Sud/Merr SB L	*	100	84	3.0	98	1600	0.08	1	3
13. Sud/Merr SB TTT	*	100	50	3.0	394	1600	0.08	1	3
14. Sud/Merr NB TTTR	*	100	66	3.0	863	1600	0.08	1	3
15. Sud/Merr EB LTTR	*	100	72	3.0	766	1600	0.08	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	322	1600	0.08	1	3
17. Sud/Sur SEB	*	100	80	3.0	35	1600	0.08	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	853	1600	0.08	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Char/Merr NE1	*	6063.7	5511.0	6.0
2. Char/Merr NE2	*	6133.9	5484.8	6.0
3. Char/Merr NE3	*	6204.2	5458.5	6.0
4. Char/Merr NE4	*	6265.6	5501.5	6.0
5. Char/Merr NE5	*	6327.1	5544.5	6.0
6. Char/Merr SE1	*	6443.7	5491.9	6.0
7. Char/Merr SE2	*	6382.2	5448.9	6.0
8. Char/Merr SE3	*	6320.8	5405.9	6.0
9. Char/Merr SE4	*	6380.5	5360.4	6.0
10. Char/Merr SE5	*	6440.1	5315.0	6.0
11. Char/Merr SW1	*	6332.0	5249.0	6.0
12. Char/Merr SW2	*	6272.3	5294.5	6.0
13. Char/Merr SW3	*	6212.6	5339.9	6.0
14. Char/Merr SW4	*	6141.6	5315.8	6.0
15. Char/Merr SW5	*	6070.6	5291.7	6.0
16. Char/Merr NW1	*	5902.1	5359.1	6.0
17. Char/Merr NW2	*	5973.1	5383.2	6.0
18. Char/Merr NW3	*	6044.1	5407.3	6.0
19. Char/Merr NW4	*	5973.9	5433.5	6.0
20. Char/Merr NW5	*	5903.6	5459.8	6.0
21. Char/Cam NE1	*	5490.2	4963.0	6.0
22. Char/Cam NE2	*	5459.0	4894.8	6.0
23. Char/Cam NE3	*	5427.8	4826.6	6.0
24. Char/Cam NE4	*	5500.4	4807.6	6.0
25. Char/Cam NE5	*	5572.9	4788.7	6.0
26. Char/Cam SE1	*	5553.9	4667.5	6.0
27. Char/Cam SE2	*	5481.3	4686.5	6.0
28. Char/Cam SE3	*	5408.7	4705.4	6.0
29. Char/Cam SE4	*	5409.4	4630.4	6.0
30. Char/Cam SE5	*	5410.1	4555.4	6.0
31. Char/Cam SW1	*	5312.0	4561.9	6.0
32. Char/Cam SW2	*	5310.7	4636.9	6.0
33. Char/Cam SW3	*	5310.7	4711.9	6.0

DATE : 8/ 7/13
TIME : 17: 7:49

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Char/Cam SW4	*	5235.6	4712.1	6.0
35. Char/Cam SW5	*	5160.6	4711.9	6.0
36. Char/Cam NW1	*	5167.9	4822.4	6.0
37. Char/Cam NW2	*	5242.9	4822.1	6.0
38. Char/Cam NW3	*	5317.9	4821.9	6.0
39. Char/Cam NW4	*	5349.1	4890.1	6.0
40. Char/Cam NW5	*	5380.3	4958.3	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	1.	2.	0.	0.	1.	1.	1.
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	1.	2.	0.	0.	2.	1.	1.
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	3.	3.	2.	2.	0.	0.	2.		

1.	1.																			
30.	*	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	3.	2.	2.	0.	1.	2.	
1.	1.																			
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	3.	2.	2.	0.	1.	2.	
1.	1.																			
50.	*	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	1.	2.	3.	2.	2.	1.	1.	2.	
1.	1.																			
60.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	1.	2.	3.	
1.	1.																			
70.	*	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	2.	2.	2.	3.	
2.	1.																			
80.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.	
2.	2.																			
90.	*	1.	1.	2.	2.	1.	0.	0.	0.	0.	1.	2.	2.	2.	1.	1.	2.	2.	3.	
3.	2.																			
100.	*	1.	2.	3.	2.	1.	0.	0.	0.	0.	1.	2.	2.	2.	1.	1.	2.	2.	3.	
3.	2.																			
110.	*	2.	2.	3.	2.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	2.	2.	3.	
3.	2.																			
120.	*	2.	3.	3.	2.	1.	0.	0.	1.	1.	2.	2.	2.	2.	1.	0.	1.	2.	2.	
2.	2.																			
130.	*	2.	3.	4.	3.	1.	0.	1.	2.	2.	3.	2.	1.	2.	0.	0.	1.	2.	2.	
1.	1.																			
140.	*	2.	2.	4.	4.	2.	1.	1.	2.	3.	3.	1.	1.	1.	0.	0.	1.	1.	1.	
1.	1.																			
150.	*	2.	2.	3.	4.	2.	1.	2.	2.	2.	3.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
160.	*	2.	2.	2.	4.	2.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
170.	*	2.	1.	2.	3.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
180.	*	2.	2.	2.	3.	2.	1.	1.	2.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
190.	*	2.	2.	2.	3.	2.	1.	1.	2.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
200.	*	2.	2.	2.	2.	2.	1.	1.	2.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
210.	*	2.	2.	2.	2.	3.	1.	1.	2.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	1.																			
220.	*	2.	2.	2.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
230.	*	1.	3.	3.	2.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	1.	1.	1.	1.	
1.	0.																			
240.	*	1.	2.	2.	2.	2.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
0.	0.																			
250.	*	1.	2.	2.	1.	1.	3.	3.	3.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	
0.	0.																			
260.	*	1.	1.	2.	1.	1.	3.	3.	3.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	
0.	0.																			
270.	*	1.	1.	2.	1.	0.	2.	3.	3.	3.	2.	0.	1.	1.	1.	1.	0.	0.	0.	
0.	0.																			
280.	*	1.	1.	1.	0.	0.	2.	2.	3.	3.	3.	0.	1.	2.	2.	1.	0.	0.	0.	
0.	0.																			
290.	*	0.	0.	1.	0.	0.	1.	2.	3.	2.	3.	1.	1.	2.	2.	1.	0.	0.	0.	
0.	0.																			
300.	*	0.	0.	0.	0.	0.	1.	1.	2.	2.	2.	1.	2.	2.	2.	1.	0.	0.	1.	
1.	0.																			
310.	*	0.	0.	0.	0.	0.	1.	1.	2.	2.	1.	2.	2.	2.	2.	2.	0.	0.	1.	
1.	0.																			
320.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.	
1.	1.																			
330.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.	
1.	1.																			
340.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	3.	2.	2.	2.	2.	0.	0.	1.	
1.	1.																			
350.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.	
1.	1.																			
360.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	1.	2.	0.	0.	1.	
1.	1.																			
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
-------																				
MAX	*	2.	3.	4.	4.	3.	3.	3.	3.	3.	3.	3.	3.	3.	2.	2.	2.	2.	3.	
3.	2.																			
DEGR.	*	130	130	130	160	210	250	260	270	280	140	340	20	30	40	10	80	90	80	
100	100																			

ANGLE * (ug/m**3)

(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
------*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
0. *	0.	1.	1.	0.	0.	1.	1.	2.	2.	2.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.
10. *	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.
20. *	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	2.	1.	0.	0.	0.	0.	0.
30. *	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	3.	1.	0.	0.	1.	0.	0.
40. *	0.	0.	0.	0.	0.	2.	1.	2.	1.	1.	2.	3.	3.	4.	2.	0.	0.	2.	1.	1.
50. *	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	3.	3.	4.	2.	0.	1.	2.	1.	1.
60. *	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	3.	3.	4.	3.	1.	1.	2.	1.	1.
70. *	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	1.	2.	1.	1.
80. *	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	1.	2.	1.	1.
90. *	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	1.	2.	3.	2.	2.	2.	2.	2.	1.	1.
100. *	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	2.	2.	2.	3.	1.	1.
110. *	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	2.	1.
120. *	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	2.	1.
130. *	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	3.	3.	1.
140. *	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	3.	3.	1.
150. *	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	3.	2.
160. *	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	3.	3.	2.
170. *	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	3.	3.	2.
180. *	1.	1.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	1.	0.	0.	1.	2.	2.	3.	2.
190. *	1.	2.	3.	1.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.
200. *	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	2.	2.
210. *	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.
220. *	2.	2.	3.	2.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.
230. *	2.	2.	3.	2.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.
240. *	2.	2.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.
250. *	1.	2.	3.	3.	2.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.
260. *	1.	2.	3.	3.	2.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
270. *	1.	1.	2.	2.	2.	1.	2.	3.	2.	1.	0.	0.	1.	1.	0.	0.	1.	1.	0.	0.
280. *	1.	1.	2.	2.	2.	2.	2.	4.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.
290. *	1.	1.	2.	1.	1.	2.	2.	4.	3.	1.	0.	0.	3.	1.	1.	0.	0.	0.	0.	0.
300. *	1.	1.	2.	1.	1.	2.	2.	3.	3.	1.	0.	1.	3.	1.	1.	0.	0.	0.	0.	0.
310. *	1.	1.	1.	1.	0.	2.	2.	3.	3.	2.	0.	1.	3.	2.	1.	0.	0.	0.	0.	0.
320. *	1.	1.	1.	0.	0.	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
330. *	1.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
340. *	0.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
350. *	0.	1.	1.	0.	0.	1.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
360. *	0.	1.	1.	0.	0.	1.	1.	2.	2.	2.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.
------*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
MAX *	2.	2.	3.	3.	2.	2.	2.	4.	3.	2.	2.	3.	3.	4.	3.	2.	2.	3.	3.	2.
DEGR. *	220	220	200	250	260	300	290	290	320	350	30	40	50	50	70	110	110	110	170	180

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC3 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17:38:10

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6054.9	5445.6	*	60.	290.	AG	1.	100.0	1.0	30.0	0.48	3.1
2. Char/Merr WB	*	6250.4	5435.2	6323.7	5493.2	*	93.	52.	AG	1.	100.0	1.0	30.0	0.71	4.7
3. Char/Merr NB R	*	6291.7	5369.7	6313.9	5354.6	*	27.	124.	AG	0.	100.0	1.0	10.0	0.14	1.4
4. Char/Merr NB LTT	*	6280.4	5347.2	6395.2	5266.3	*	140.	125.	AG	0.	100.0	1.0	20.0	0.83	7.1
5. Char/Merr EB	*	6104.2	5362.2	6064.9	5347.6	*	42.	250.	AG	0.	100.0	1.0	20.0	0.38	2.1
6. Char/Cam SB L	*	5384.1	4834.2	5408.6	4932.0	*	101.	14.	AG	0.	100.0	1.0	10.0	0.66	5.1
7. Char/Cam SB TR	*	5360.8	4833.5	5392.6	4936.4	*	108.	17.	AG	0.	100.0	1.0	20.0	0.86	5.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5448.9	4784.7	*	39.	103.	AG	0.	100.0	1.0	20.0	0.24	2.0
9. Char/Cam NB L	*	5363.0	4722.4	5361.1	4639.9	*	82.	181.	AG	0.	100.0	1.0	10.0	0.54	4.2
10. Char/Cam NB TR	*	5383.3	4723.8	5384.3	4657.5	*	66.	179.	AG	0.	100.0	1.0	20.0	0.67	3.4
11. Char/Cam EB TTTR	*	5302.7	4739.8	5222.9	4740.6	*	80.	271.	AG	0.	100.0	1.0	30.0	0.49	4.1
12. Sud/Merr SB L	*	6532.7	5210.3	6493.6	5238.2	*	48.	305.	AG	0.	100.0	1.0	10.0	0.66	2.4
13. Sud/Merr SB TTT	*	6518.3	5190.8	6480.9	5212.4	*	43.	300.	AG	0.	100.0	1.0	30.0	0.22	2.2
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6669.4	5076.1	*	98.	150.	AG	0.	100.0	1.0	30.0	0.55	5.0
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6482.0	5121.0	*	48.	239.	AG	1.	100.0	1.0	40.0	0.34	2.5
16. Sud/Sur SB LTT	*	6777.5	5369.7	6741.1	5415.5	*	59.	322.	AG	0.	100.0	1.0	20.0	0.30	3.0
17. Sud/Sur SEB	*	6757.2	5330.0	6747.9	5332.3	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6750.6	5242.3	*	47.	249.	AG	1.	100.0	1.0	30.0	0.39	2.4
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	802.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1038.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1204.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	870.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	923.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1472.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	877.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1546.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	285.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	483.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	405.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	338.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	25.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1421.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1512.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	487.	0.0	1.0	78.0		

1. Char/Merr SB	*	100	76	3.0	436	1600	0.08	1	3
2. Char/Merr WB	*	100	76	3.0	650	1600	0.08	1	3
3. Char/Merr NB R	*	100	45	3.0	109	1600	0.08	1	3
4. Char/Merr NB LTT	*	100	71	3.0	637	1600	0.08	1	3
5. Char/Merr EB	*	100	79	3.0	194	1600	0.08	1	3
6. Char/Cam SB L	*	90	58	3.0	318	1600	0.08	1	3
7. Char/Cam SB TR	*	90	71	3.0	429	1600	0.08	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	265	1600	0.08	1	3
9. Char/Cam NB L	*	90	58	3.0	260	1600	0.08	1	3
10. Char/Cam NB TR	*	90	71	3.0	330	1600	0.08	1	3

11. Char/Cam EB TTTR	*	90	54	3.0	811	1600	0.08	1	3
12. Sud/Merr SB L	*	100	86	3.0	95	1600	0.08	1	3
13. Sud/Merr SB TTT	*	100	49	3.0	484	1600	0.08	1	3
14. Sud/Merr NB TTTR	*	100	63	3.0	854	1600	0.08	1	3
15. Sud/Merr EB LTTR	*	100	73	3.0	487	1600	0.08	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	405	1600	0.08	1	3
17. Sud/Sur SEB	*	100	70	3.0	25	1600	0.08	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	338	1600	0.08	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Sud/Merr NE1	*	6492.5	5309.9	6.0	*
2. Sud/Merr NE2	*	6554.8	5268.0	6.0	*
3. Sud/Merr NE3	*	6616.2	5224.9	6.0	*
4. Sud/Merr NE4	*	6684.7	5255.3	6.0	*
5. Sud/Merr NE5	*	6753.3	5285.7	6.0	*
6. Sud/Merr SE1	*	6792.9	5222.3	6.0	*
7. Sud/Merr SE2	*	6724.3	5191.9	6.0	*
8. Sud/Merr SE3	*	6655.7	5161.5	6.0	*
9. Sud/Merr SE4	*	6695.5	5097.9	6.0	*
10. Sud/Merr SE5	*	6735.2	5034.3	6.0	*
11. Sud/Merr SW1	*	6638.6	4981.3	6.0	*
12. Sud/Merr SW2	*	6598.9	5045.0	6.0	*
13. Sud/Merr SW3	*	6559.1	5108.6	6.0	*
14. Sud/Merr SW4	*	6493.4	5072.5	6.0	*
15. Sud/Merr SW5	*	6427.6	5036.5	6.0	*
16. Sud/Merr NW1	*	6347.8	5104.5	6.0	*
17. Sud/Merr NW2	*	6413.5	5140.5	6.0	*
18. Sud/Merr NW3	*	6479.3	5176.6	6.0	*
19. Sud/Merr NW4	*	6417.1	5218.5	6.0	*
20. Sud/Merr NW5	*	6354.9	5260.4	6.0	*
21. Sud/Sur NE1	*	6755.9	5445.7	6.0	*
22. Sud/Sur NE2	*	6801.0	5385.7	6.0	*
23. Sud/Sur NE3	*	6846.0	5325.7	6.0	*
24. Sud/Sur NE4	*	6908.8	5366.8	6.0	*
25. Sud/Sur NE5	*	6971.5	5407.9	6.0	*
26. Sud/Sur SE1	*	7002.4	5368.4	6.0	*
27. Sud/Sur SE2	*	6939.7	5327.3	6.0	*
28. Sud/Sur SE3	*	6876.9	5286.2	6.0	*
29. Sud/Sur SE4	*	6931.7	5235.0	6.0	*
30. Sud/Sur SE5	*	6986.5	5183.8	6.0	*
31. Sud/Sur SW1	*	6932.3	5133.1	6.0	*
32. Sud/Sur SE2	*	6877.5	5184.3	6.0	*
33. Sud/Sur SE3	*	6822.7	5235.5	6.0	*

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
34. Sud/Sur SE4	*	6754.2	5205.1	6.0	*
35. Sud/Sur SE5	*	6685.6	5174.8	6.0	*
36. Sud/Sur NW1	*	6645.5	5237.9	6.0	*
37. Sud/Sur NW2	*	6714.1	5268.3	6.0	*
38. Sud/Sur NW3	*	6782.7	5298.7	6.0	*
39. Sud/Sur NW4	*	6709.5	5315.4	6.0	*
40. Sud/Sur NW5	*	6636.4	5332.0	6.0	*
41. Sud/Sur N1	*	6642.4	5493.7	6.0	*
42. Sud/Sur N2	*	6687.4	5433.7	6.0	*
43. Sud/Sur N3	*	6732.4	5373.8	6.0	*
44. Sud/Sur N4	*	6659.3	5390.4	6.0	*
45. Sud/Sur N5	*	6586.2	5407.1	6.0	*

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

0.	*	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	3.	2.	2.	3.	1.	1.	1.	2.
2.	3.																		
10.	*	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.
2.	3.																		
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.
2.	2.																		
30.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	2.																		
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	2.																		
50.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	2.																		
60.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	2.	2.	1.	2.	2.
1.	2.																		
70.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	1.	2.	2.	3.
2.	3.																		
80.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	2.	3.
2.	2.																		
90.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.
2.	3.																		
100.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	3.
3.	3.																		
110.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.
3.	3.																		
120.	*	1.	1.	0.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.
3.	3.																		
130.	*	2.	1.	1.	0.	2.	0.	0.	0.	0.	0.	2.	2.	2.	0.	0.	0.	1.	3.
2.	2.																		
140.	*	2.	2.	1.	0.	2.	0.	0.	1.	0.	0.	1.	1.	2.	0.	0.	0.	1.	3.
1.	1.																		
150.	*	3.	3.	2.	0.	2.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	2.
1.	1.																		
160.	*	3.	3.	3.	1.	2.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	0.	0.	2.
1.	0.																		
170.	*	2.	2.	3.	1.	2.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	0.	0.	2.
0.	0.																		
180.	*	2.	2.	3.	2.	2.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
190.	*	2.	2.	2.	2.	2.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
200.	*	2.	2.	2.	2.	2.	1.	1.	3.	2.	2.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
210.	*	2.	2.	2.	2.	1.	1.	1.	3.	2.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
220.	*	2.	2.	2.	2.	2.	1.	1.	3.	2.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
230.	*	2.	2.	3.	2.	2.	1.	1.	3.	2.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
240.	*	2.	2.	3.	2.	2.	1.	2.	3.	2.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	1.																		
250.	*	2.	2.	2.	2.	1.	2.	2.	4.	3.	2.	0.	0.	1.	1.	1.	1.	0.	0.
0.	0.																		
260.	*	2.	2.	2.	1.	1.	2.	2.	4.	3.	2.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
270.	*	2.	2.	2.	1.	1.	2.	2.	3.	3.	2.	0.	0.	1.	1.	0.	0.	0.	0.
0.	1.																		
280.	*	2.	2.	2.	1.	1.	2.	2.	4.	4.	2.	0.	0.	2.	1.	0.	0.	0.	0.
1.	1.																		
290.	*	2.	2.	3.	1.	1.	2.	2.	4.	4.	3.	0.	1.	2.	1.	1.	0.	0.	1.
1.	2.																		
300.	*	1.	2.	2.	1.	0.	2.	2.	3.	4.	4.	1.	1.	3.	1.	1.	0.	0.	2.
2.	2.																		
310.	*	1.	1.	1.	0.	0.	2.	1.	2.	4.	4.	1.	2.	3.	1.	1.	0.	1.	2.
3.	3.																		
320.	*	1.	0.	0.	0.	0.	2.	0.	2.	2.	3.	2.	2.	3.	2.	1.	1.	1.	2.
3.	3.																		
330.	*	0.	0.	0.	0.	0.	2.	1.	1.	1.	2.	2.	2.	3.	2.	1.	1.	2.	2.
3.	3.																		
340.	*	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	2.	2.	3.	2.	2.	1.	2.	2.
2.	3.																		
350.	*	0.	0.	0.	0.	1.	2.	0.	0.	0.	0.	2.	2.	2.	2.	1.	1.	1.	2.
2.	3.																		
360.	*	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	3.	2.	2.	3.	1.	1.	1.	2.
2.	3.																		
MAX	*	3.	3.	3.	2.	2.	2.	2.	4.	4.	4.	3.	2.	3.	3.	2.	2.	2.	3.
3.	3.																		
DEGR.	*	150	160	170	230	160	290	260	290	300	310	0	30	310	0	30	80	80	120
320	340																		

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (ug/m**3)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40

0.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	0.	0.	0.	1.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	0.	1.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	0.	0.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
60.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
70.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
0.	0.																		
80.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
90.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.
0.	0.																		
100.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	2.	0.
0.	0.																		
110.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	2.	1.
1.	0.																		
120.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	1.	1.
1.	0.																		
130.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	0.																		
140.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	0.																		
150.	*	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	0.																		
160.	*	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	2.	1.
1.	1.																		
170.	*	2.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	2.	1.
1.	1.																		
180.	*	2.	1.	1.	1.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	2.	2.	1.	2.
1.	1.																		
190.	*	2.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	2.	2.	1.	2.
1.	1.																		
200.	*	2.	2.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	1.	2.	2.	1.	2.
1.	1.																		
210.	*	2.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	2.
1.	1.																		
220.	*	1.	2.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	1.	1.	2.	2.	2.	2.
1.	1.																		
230.	*	1.	2.	2.	1.	1.	1.	1.	2.	1.	1.	0.	1.	1.	1.	2.	2.	2.	2.
1.	1.																		
240.	*	1.	2.	2.	1.	1.	1.	2.	2.	1.	1.	0.	1.	1.	2.	2.	2.	2.	1.
1.	1.																		
250.	*	1.	2.	2.	1.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.	2.	2.	1.	1.
1.	1.																		
260.	*	1.	2.	1.	1.	1.	1.	1.	2.	2.	2.	1.	1.	2.	2.	3.	2.	1.	1.
1.	1.																		
270.	*	1.	2.	1.	1.	1.	1.	1.	2.	2.	2.	1.	1.	2.	2.	3.	2.	1.	1.
1.	1.																		
280.	*	1.	2.	1.	1.	0.	1.	1.	2.	2.	2.	1.	1.	2.	2.	3.	2.	1.	1.
1.	1.																		
290.	*	1.	2.	1.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	3.	2.	1.	1.
1.	1.																		
300.	*	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	2.	1.	2.	1.	0.	0.
0.	0.																		
310.	*	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
0.	0.																		
320.	*	0.	1.	1.	0.	0.	0.	0.	1.	1.	0.	1.	1.	1.	0.	1.	0.	0.	1.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	0.	0.	1.
0.	0.																		
MAX	*	2.	2.	2.	1.	1.	2.	2.	2.	2.	2.	1.	2.	2.	2.	3.	2.	2.	2.
1.	1.																		
DEGR.	*	190	270	230	240	230	250	250	250	260	270	280	290	270	260	260	240	230	190

210 220

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	1.	0.	0.
10.	0.	0.	1.	0.	0.
20.	0.	0.	1.	0.	0.
30.	0.	0.	1.	0.	0.
40.	0.	0.	1.	0.	0.
50.	0.	0.	1.	0.	0.
60.	0.	0.	1.	0.	0.
70.	0.	0.	1.	0.	0.
80.	0.	0.	1.	0.	0.
90.	0.	1.	1.	0.	0.
100.	0.	1.	1.	0.	0.
110.	1.	1.	1.	0.	0.
120.	1.	1.	1.	0.	0.
130.	1.	1.	1.	1.	0.
140.	1.	1.	1.	0.	0.
150.	1.	1.	1.	0.	0.
160.	0.	0.	1.	0.	1.
170.	1.	1.	1.	1.	1.
180.	1.	1.	1.	1.	1.
190.	1.	1.	1.	1.	1.
200.	1.	1.	1.	1.	1.
210.	1.	1.	1.	1.	1.
220.	0.	1.	1.	1.	1.
230.	1.	1.	1.	1.	1.
240.	1.	1.	1.	1.	1.
250.	1.	1.	1.	1.	1.
260.	1.	1.	1.	1.	1.
270.	1.	1.	1.	1.	1.
280.	1.	1.	1.	1.	1.
290.	0.	0.	0.	0.	1.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	1.	0.	0.
360.	0.	0.	1.	0.	0.
MAX	1.	1.	1.	1.	1.
DEGR.	250	120	230	190	180

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC9 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

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The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6042.2	5450.2	*	74.	290.	AG	1.	100.0	1.0	30.0	0.56	3.8
2. Char/Merr WB	*	6250.4	5435.2	6300.3	5474.7	*	64.	52.	AG	1.	100.0	1.0	30.0	0.55	3.2
3. Char/Merr NB R	*	6291.7	5369.7	6341.8	5335.7	*	61.	124.	AG	0.	100.0	1.0	10.0	0.31	3.1
4. Char/Merr NB LTT	*	6280.4	5347.2	6349.1	5298.8	*	84.	125.	AG	0.	100.0	1.0	20.0	0.52	4.3
5. Char/Merr EB	*	6104.2	5362.2	6005.8	5325.6	*	105.	250.	AG	0.	100.0	1.0	20.0	0.81	5.3
6. Char/Cam SB L	*	5384.1	4834.2	5401.1	4902.3	*	70.	14.	AG	0.	100.0	1.0	10.0	0.38	3.6
7. Char/Cam SB TR	*	5360.8	4833.5	5374.3	4877.1	*	46.	17.	AG	0.	100.0	1.0	20.0	0.32	2.3
8. Char/Cam WB LTTR	*	5411.0	4793.5	5475.3	4778.6	*	66.	103.	AG	0.	100.0	1.0	20.0	0.37	3.4
9. Char/Cam NB L	*	5363.0	4722.4	5361.0	4631.8	*	91.	181.	AG	0.	100.0	1.0	10.0	0.49	4.6
10. Char/Cam NB TR	*	5383.3	4723.8	5384.8	4624.7	*	99.	179.	AG	0.	100.0	1.0	20.0	0.68	5.0
11. Char/Cam EB TTTR	*	5302.7	4739.8	5220.6	4740.7	*	82.	271.	AG	0.	100.0	1.0	30.0	0.46	4.2
12. Sud/Merr SB L	*	6532.7	5210.3	6496.1	5236.4	*	45.	305.	AG	0.	100.0	1.0	10.0	0.56	2.3
13. Sud/Merr SB TTT	*	6518.3	5190.8	6487.3	5208.8	*	36.	300.	AG	0.	100.0	1.0	30.0	0.18	1.8
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6672.2	5071.1	*	104.	150.	AG	0.	100.0	1.0	30.0	0.62	5.3
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6458.9	5107.1	*	75.	239.	AG	1.	100.0	1.0	40.0	0.52	3.8
16. Sud/Sur SB LTT	*	6777.5	5369.7	6739.2	5418.0	*	62.	322.	AG	0.	100.0	1.0	20.0	0.40	3.1
17. Sud/Sur SEB	*	6757.2	5330.0	6742.4	5333.7	*	15.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6722.2	5231.2	*	78.	249.	AG	0.	100.0	1.0	30.0	0.39	3.9
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	818.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1226.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1219.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	859.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	796.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1264.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	954.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1198.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	805.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	405.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	322.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	853.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	35.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1185.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1465.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	766.	0.0	1.0	78.0		

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1. Char/Merr SB	*	100	75	3.0	541	1600	0.08	1	3
2. Char/Merr WB	*	100	78	3.0	449	1600	0.08	1	3
3. Char/Merr NB R	*	100	46	3.0	241	1600	0.08	1	3
4. Char/Merr NB LTT	*	100	68	3.0	452	1600	0.08	1	3
5. Char/Merr EB	*	100	79	3.0	417	1600	0.08	1	3
6. Char/Cam SB L	*	100	60	3.0	214	1600	0.08	1	3
7. Char/Cam SB TR	*	100	72	3.0	233	1600	0.08	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	391	1600	0.08	1	3
9. Char/Cam NB L	*	100	60	3.0	276	1600	0.08	1	3
10. Char/Cam NB TR	*	100	72	3.0	503	1600	0.08	1	3

11. Char/Cam EB TTTR	*	100	62	3.0	726	1600	0.08	1	3
12. Sud/Merr SB L	*	100	84	3.0	98	1600	0.08	1	3
13. Sud/Merr SB TTT	*	100	50	3.0	394	1600	0.08	1	3
14. Sud/Merr NB TTTR	*	100	66	3.0	863	1600	0.08	1	3
15. Sud/Merr EB LTTR	*	100	72	3.0	766	1600	0.08	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	322	1600	0.08	1	3
17. Sud/Sur SEB	*	100	80	3.0	35	1600	0.08	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	853	1600	0.08	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Sud/Merr NE1	*	6492.5	5309.9	6.0
2. Sud/Merr NE2	*	6554.8	5268.0	6.0
3. Sud/Merr NE3	*	6616.2	5224.9	6.0
4. Sud/Merr NE4	*	6684.7	5255.3	6.0
5. Sud/Merr NE5	*	6753.3	5285.7	6.0
6. Sud/Merr SE1	*	6792.9	5222.3	6.0
7. Sud/Merr SE2	*	6724.3	5191.9	6.0
8. Sud/Merr SE3	*	6655.7	5161.5	6.0
9. Sud/Merr SE4	*	6695.5	5097.9	6.0
10. Sud/Merr SE5	*	6735.2	5034.3	6.0
11. Sud/Merr SW1	*	6638.6	4981.3	6.0
12. Sud/Merr SW2	*	6598.9	5045.0	6.0
13. Sud/Merr SW3	*	6559.1	5108.6	6.0
14. Sud/Merr SW4	*	6493.4	5072.5	6.0
15. Sud/Merr SW5	*	6427.6	5036.5	6.0
16. Sud/Merr NW1	*	6347.8	5104.5	6.0
17. Sud/Merr NW2	*	6413.5	5140.5	6.0
18. Sud/Merr NW3	*	6479.3	5176.6	6.0
19. Sud/Merr NW4	*	6417.1	5218.5	6.0
20. Sud/Merr NW5	*	6354.9	5260.4	6.0
21. Sud/Sur NE1	*	6755.9	5445.7	6.0
22. Sud/Sur NE2	*	6801.0	5385.7	6.0
23. Sud/Sur NE3	*	6846.0	5325.7	6.0
24. Sud/Sur NE4	*	6908.8	5366.8	6.0
25. Sud/Sur NE5	*	6971.5	5407.9	6.0
26. Sud/Sur SE1	*	7002.4	5368.4	6.0
27. Sud/Sur SE2	*	6939.7	5327.3	6.0
28. Sud/Sur SE3	*	6876.9	5286.2	6.0
29. Sud/Sur SE4	*	6931.7	5235.0	6.0
30. Sud/Sur SE5	*	6986.5	5183.8	6.0
31. Sud/Sur SW1	*	6932.3	5133.1	6.0
32. Sud/Sur SE2	*	6877.5	5184.3	6.0
33. Sud/Sur SE3	*	6822.7	5235.5	6.0

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RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Sud/Sur SE4	*	6754.2	5205.1	6.0
35. Sud/Sur SE5	*	6685.6	5174.8	6.0
36. Sud/Sur NW1	*	6645.5	5237.9	6.0
37. Sud/Sur NW2	*	6714.1	5268.3	6.0
38. Sud/Sur NW3	*	6782.7	5298.7	6.0
39. Sud/Sur NW4	*	6709.5	5315.4	6.0
40. Sud/Sur NW5	*	6636.4	5332.0	6.0
41. Sud/Sur N1	*	6642.4	5493.7	6.0
42. Sud/Sur N2	*	6687.4	5433.7	6.0
43. Sud/Sur N3	*	6732.4	5373.8	6.0
44. Sud/Sur N4	*	6659.3	5390.4	6.0
45. Sud/Sur N5	*	6586.2	5407.1	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

```
   0.  *    0.    0.    0.    0.    1.    2.    2.    1.    1.    1.    3.    2.    2.    3.    2.    1.    1.    2.
2.    2.
  10.  *    0.    0.    0.    0.    1.    1.    2.    1.    1.    1.    3.    2.    2.    3.    2.    1.    1.    2.
1.    2.
  20.  *    0.    0.    0.    0.    0.    1.    2.    1.    1.    0.    2.    3.    2.    3.    2.    1.    1.    2.
1.    2.
  30.  *    0.    0.    0.    0.    0.    1.    2.    2.    1.    0.    2.    3.    2.    3.    2.    1.    1.    2.
1.    2.
  40.  *    0.    0.    0.    0.    0.    1.    2.    2.    1.    0.    2.    2.    3.    2.    3.    1.    1.    2.
1.    1.
  50.  *    0.    0.    0.    0.    0.    1.    2.    2.    0.    0.    2.    3.    3.    2.    2.    1.    1.    2.
1.    1.
  60.  *    0.    0.    1.    1.    0.    1.    1.    1.    0.    0.    2.    2.    3.    2.    2.    2.    2.    3.
1.    2.
  70.  *    0.    0.    1.    1.    1.    0.    1.    1.    0.    0.    1.    2.    3.    2.    1.    2.    3.    3.
1.    2.
  80.  *    0.    0.    2.    2.    1.    0.    0.    0.    0.    0.    1.    2.    2.    1.    1.    2.    3.    3.
2.    2.
  90.  *    0.    1.    2.    2.    1.    0.    0.    0.    0.    0.    1.    2.    2.    1.    1.    2.    3.    3.
2.    2.
 100.  *    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    2.    2.    2.    1.    1.    2.    3.    3.
3.    3.
 110.  *    1.    1.    1.    2.    1.    0.    0.    0.    0.    0.    2.    2.    2.    1.    0.    1.    3.    3.
3.    3.
 120.  *    1.    1.    1.    2.    2.    0.    0.    0.    0.    0.    2.    2.    2.    1.    0.    1.    2.    3.
3.    3.
 130.  *    2.    1.    1.    1.    2.    0.    0.    0.    0.    0.    1.    2.    2.    0.    0.    1.    2.    3.
2.    2.
 140.  *    2.    2.    2.    1.    2.    0.    0.    1.    0.    0.    1.    1.    2.    0.    0.    1.    1.    3.
2.    2.
 150.  *    3.    3.    3.    1.    2.    0.    0.    1.    1.    1.    1.    1.    1.    0.    0.    1.    1.    3.
1.    1.
 160.  *    3.    3.    4.    1.    2.    0.    0.    2.    2.    1.    0.    0.    0.    0.    0.    1.    1.    2.
1.    1.
 170.  *    2.    2.    4.    2.    2.    0.    1.    3.    2.    2.    0.    0.    0.    0.    0.    1.    1.    2.
1.    0.
 180.  *    2.    2.    3.    2.    2.    0.    1.    3.    2.    2.    0.    0.    0.    0.    0.    1.    1.    2.
0.    0.
 190.  *    2.    2.    3.    2.    2.    0.    1.    3.    2.    2.    0.    0.    0.    0.    0.    1.    1.    2.
0.    0.
 200.  *    2.    2.    3.    2.    2.    1.    1.    3.    2.    2.    0.    0.    0.    0.    0.    1.    1.    2.
0.    0.
 210.  *    2.    3.    3.    2.    2.    1.    1.    3.    2.    1.    0.    0.    0.    0.    0.    1.    1.    1.
0.    0.
 220.  *    1.    2.    3.    3.    2.    1.    1.    3.    2.    1.    0.    0.    0.    0.    0.    1.    1.    1.
0.    0.
 230.  *    1.    2.    3.    3.    2.    1.    2.    3.    2.    1.    0.    0.    0.    0.    0.    0.    1.    1.
0.    0.
 240.  *    2.    2.    3.    2.    2.    2.    2.    4.    3.    1.    0.    0.    1.    0.    0.    0.    1.    1.
0.    0.
 250.  *    2.    2.    3.    2.    2.    2.    3.    4.    3.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 260.  *    2.    2.    2.    1.    1.    3.    3.    4.    3.    2.    0.    0.    2.    1.    1.    0.    0.    0.
0.    0.
 270.  *    2.    2.    2.    1.    1.    3.    3.    4.    3.    2.    0.    0.    2.    1.    1.    0.    0.    0.
0.    1.
 280.  *    2.    2.    2.    1.    1.    3.    2.    4.    4.    2.    0.    1.    2.    1.    1.    0.    0.    0.
1.    1.
 290.  *    2.    2.    2.    1.    1.    3.    2.    4.    4.    3.    1.    1.    3.    1.    1.    0.    0.    1.
1.    2.
 300.  *    1.    2.    2.    1.    0.    2.    2.    4.    4.    4.    1.    2.    3.    2.    1.    0.    1.    2.
2.    2.
 310.  *    1.    1.    1.    0.    0.    2.    1.    3.    4.    4.    1.    2.    3.    2.    1.    1.    1.    2.
2.    3.
 320.  *    0.    1.    0.    0.    0.    2.    1.    2.    3.    3.    2.    3.    3.    3.    2.    1.    1.    2.
2.    3.
 330.  *    0.    0.    0.    0.    0.    2.    1.    2.    1.    2.    2.    2.    3.    3.    2.    1.    2.    2.
2.    3.
 340.  *    0.    0.    0.    0.    0.    2.    1.    1.    1.    1.    3.    2.    3.    3.    2.    1.    1.    2.
2.    3.
 350.  *    0.    0.    0.    0.    0.    2.    1.    1.    1.    1.    3.    2.    3.    3.    2.    1.    1.    2.
2.    3.
 360.  *    0.    0.    0.    0.    1.    2.    2.    1.    1.    1.    3.    2.    2.    3.    2.    1.    1.    2.
2.    2.
------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    3.    3.    4.    3.    2.    3.    3.    4.    4.    4.    3.    3.    3.    3.    3.    2.    3.    3.
3.    3.
 DEGR. *  150   160   170   230   190   260   260   260   300   310   340    20   300     0    40    80    90    80
100   330
```


JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

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 WIND  * CONCENTRATION
 ANGLE *     (ug/m**3)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38
REC39 REC40

------*-------------------------------------------------------------------------------------------------------------
-------
   0.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
  10.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.    1.    1.    2.    1.    0.    0.    0.
0.    0.
  20.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.    1.    1.    2.    1.    0.    0.    0.
0.    0.
  30.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.    1.    1.    2.    2.    0.    0.    0.
0.    0.
  40.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    2.    2.    0.    0.    0.
0.    0.
  50.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    2.    2.    0.    0.    0.
0.    0.
  60.  *    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.
0.    0.
  70.  *    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
0.    0.
  80.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    2.    1.    1.
1.    0.
  90.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    2.    2.    1.
1.    0.
 100.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    2.    2.    1.
0.    1.
 110.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    1.    2.    1.
1.    1.
 120.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 130.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 140.  *    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 150.  *    1.    1.    1.    1.    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 160.  *    1.    1.    1.    1.    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    1.    2.    2.    1.
1.    1.
 170.  *    2.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    3.    2.    1.
1.    2.
 180.  *    2.    1.    1.    1.    0.    0.    0.    1.    0.    0.    0.    0.    0.    1.    2.    3.    2.    2.
2.    2.
 190.  *    2.    2.    1.    1.    1.    0.    0.    1.    0.    0.    0.    0.    0.    1.    2.    3.    2.    2.
2.    1.
 200.  *    2.    2.    2.    2.    1.    0.    0.    1.    1.    0.    0.    0.    0.    1.    2.    3.    2.    2.
2.    1.
 210.  *    2.    2.    2.    2.    1.    0.    0.    1.    1.    1.    0.    0.    1.    1.    2.    2.    2.    3.
2.    2.
 220.  *    1.    2.    2.    2.    2.    1.    1.    1.    1.    1.    0.    0.    1.    1.    2.    3.    2.    3.
2.    2.
 230.  *    1.    2.    2.    2.    2.    1.    1.    2.    1.    1.    0.    1.    1.    1.    2.    3.    2.    3.
2.    1.
 240.  *    1.    2.    2.    2.    2.    2.    2.    2.    1.    1.    0.    1.    2.    2.    2.    3.    2.    2.
1.    1.
 250.  *    1.    2.    2.    1.    1.    2.    2.    3.    2.    1.    1.    1.    2.    2.    3.    2.    2.    1.
1.    1.
 260.  *    1.    2.    1.    1.    1.    2.    2.    2.    2.    2.    1.    1.    3.    3.    3.    2.    1.    1.
1.    1.
 270.  *    1.    2.    1.    1.    1.    1.    2.    2.    2.    2.    1.    2.    3.    2.    3.    2.    1.    1.
1.    1.
 280.  *    1.    2.    1.    1.    1.    1.    2.    2.    2.    2.    1.    2.    3.    2.    3.    2.    1.    1.
1.    1.
 290.  *    1.    2.    1.    1.    0.    1.    2.    2.    2.    1.    1.    2.    2.    2.    3.    2.    1.    1.
1.    1.
 300.  *    1.    1.    1.    0.    0.    0.    1.    2.    1.    1.    1.    1.    2.    2.    2.    1.    1.    0.
0.    1.
 310.  *    1.    1.    1.    0.    0.    0.    1.    2.    1.    1.    1.    1.    2.    2.    2.    1.    0.    0.
0.    0.
 320.  *    0.    0.    1.    0.    0.    0.    1.    2.    1.    1.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
 330.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
 340.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
 350.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
 360.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    2.    2.    2.    2.    2.    2.    2.    3.    2.    2.    1.    2.    3.    3.    3.    3.    2.    3.
2.    2.
 DEGR. *  180   220   230   230   230   250   250   250   260   270   280   280   270   260   260   180   220   220
```

190 220

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	1.	0.	0.
10.	0.	0.	1.	0.	0.
20.	0.	0.	1.	0.	0.
30.	0.	0.	1.	0.	0.
40.	0.	0.	1.	0.	0.
50.	0.	0.	1.	0.	0.
60.	0.	0.	1.	0.	0.
70.	0.	0.	1.	0.	0.
80.	0.	0.	1.	1.	0.
90.	0.	0.	1.	1.	0.
100.	0.	1.	1.	1.	0.
110.	1.	1.	1.	1.	0.
120.	1.	1.	1.	0.	0.
130.	1.	1.	1.	1.	0.
140.	1.	1.	1.	1.	0.
150.	1.	1.	1.	1.	1.
160.	0.	1.	1.	1.	1.
170.	1.	1.	1.	1.	1.
180.	1.	1.	1.	1.	1.
190.	1.	1.	1.	1.	1.
200.	1.	1.	1.	1.	1.
210.	1.	1.	1.	1.	1.
220.	1.	1.	1.	1.	1.
230.	0.	1.	1.	1.	1.
240.	1.	0.	1.	1.	1.
250.	1.	1.	1.	1.	1.
260.	1.	1.	1.	1.	1.
270.	1.	1.	1.	1.	1.
280.	1.	1.	1.	1.	1.
290.	1.	0.	1.	1.	1.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	1.	0.	0.
360.	0.	0.	1.	0.	0.
MAX	1.	1.	1.	1.	1.
DEGR.	270	120	230	190	170

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC9 .

2028 No-Build
Microscale Output Files
(Particulate Matter 10 (PM10))

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 5:34

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG TYPE (DEG)	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1. Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326. AG	0.	100.0	1.0	10.0	0.71
2. Stan/Lom SB TRR	*	5173.5	5937.1	5111.3	6026.2	*	109.	325. AG	0.	100.0	1.0	20.0	0.50
3. Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51. AG	0.	100.0	1.0	20.0	0.92
4. Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52. AG	0.	100.0	1.0	10.0	0.58
5. Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107. AG	0.	100.0	1.0	10.0	0.64
6. Stan/Lom NB TRR	*	5314.4	5765.3	5363.1	5748.8	*	51.	109. AG	0.	100.0	1.0	20.0	0.41
7. Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196. AG	0.	100.0	1.0	20.0	0.68
8. Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196. AG	0.	100.0	1.0	10.0	0.93
9. Caus/Wash SB LTTRR	*	6548.6	6868.7	6176.7	7641.4	*	857.	334. AG	0.	100.0	1.0	40.0	1.08
10. Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49. AG	0.	100.0	1.0	20.0	0.58
11. Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47. AG	0.	100.0	1.0	10.0	0.53
12. Caus/Wash NB TTR	*	6603.5	6751.9	6665.3	5376.7	*	1377.	177. AG	0.	100.0	1.0	20.0	1.39
13. Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235. AG	0.	100.0	1.0	30.0	0.47
14. Tha/Val SB LTTR	*	6599.0	6224.0	6593.7	6361.5	*	138.	358. AG	0.	100.0	1.0	20.0	0.79
15. Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180. AG	0.	100.0	1.0	10.0	1.23
16. Tha/Val NB TR	*	6645.6	6138.6	6647.7	6017.7	*	121.	179. AG	0.	100.0	1.0	10.0	0.69
17. Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6097.3	*	133.	0. AG	0.	100.0	1.0	30.0	0.68
18. Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325. AG	0.	100.0	1.0	30.0	0.18
19. Char/93 SB LLTTRR	*	6587.8	5740.0	6582.3	5883.7	*	144.	358. AG	0.	100.0	1.0	40.0	0.74
20. Char/93 WB LTT	*	6702.8	5647.8	6763.4	5572.1	*	97.	141. AG	0.	100.0	1.0	20.0	0.62
21. Char/93 EB TTR	*	6560.8	5622.5	6520.0	5592.6	*	51.	234. AG	0.	100.0	1.0	30.0	0.32
22. North/Congress SB LT	*	6876.6	4408.9	6569.4	5930.4	*	1552.	349. AG	0.	100.0	1.0	30.0	2.69
23. North/Con WB LLTR	*	6920.6	4378.3	7106.5	4444.1	*	197.	71. AG	0.	100.0	1.0	20.0	0.89
24. Nor/Con NB LTTTR	*	6914.9	4333.4	6920.9	4289.3	*	45.	172. AG	0.	100.0	1.0	30.0	0.33
25. Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256. AG	0.	100.0	1.0	10.0	0.03
26. Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326. AG	1396.	0.0	1.0	90.0	
27. Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52. AG	1568.	0.0	1.0	78.0	
28. Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111. AG	899.	0.0	1.0	78.0	
29. Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197. AG	1486.	0.0	1.0	78.0	
30. Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334. AG	3419.	0.0	1.0	90.0	
31. Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47. AG	1091.	0.0	1.0	66.0	
32. Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178. AG	2371.	0.0	1.0	90.0	
33. Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234. AG	1253.	0.0	1.0	78.0	
34. Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359. AG	2397.	0.0	1.0	90.0	
35. Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88. AG	39.	0.0	1.0	38.0	
36. Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181. AG	2837.	0.0	1.0	90.0	
37. Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232. AG	501.	0.0	1.0	54.0	
38. Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358. AG	2324.	0.0	1.0	66.0	
39. Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323. AG	356.	0.0	1.0	48.0	
40. Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141. AG	515.	0.0	1.0	42.0	
41. Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138. AG	903.	0.0	1.0	48.0	
42. Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232. AG	403.	0.0	1.0	54.0	
43. Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232. AG	702.	0.0	1.0	54.0	

44. Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145. AG	457.	0.0	1.0	42.0	

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
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LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG TYPE (DEG)	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45. North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348. AG	1343.	0.0	1.0	98.0	
46. North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70. AG	1063.	0.0	1.0	66.0	
47. North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169. AG	1529.	0.0	1.0	98.0	
48. North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258. AG	47.	0.0	1.0	54.0	

JOB: Government Center Garage RUN: No Build

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1. Stan/Lom SB L	*	120	75	3.0	376	1600	0.07	1	3
2. Stan/Lom SB TRR	*	120	75	3.0	531	1600	0.07	1	3
3. Stan/Lom WB LTT	*	120	91	3.0	588	1600	0.07	1	3
4. Stan/Lom WB R	*	120	75	3.0	308	1600	0.07	1	3
5. Stan/Lom NB L	*	120	97	3.0	152	1600	0.07	1	3
6. Stan/Lom NB TRR	*	120	97	3.0	194	1600	0.07	1	3
7. Stan/Lom EB LLT	*	120	97	3.0	324	1600	0.07	1	3
8. Stan/Lom EB R	*	120	97	3.0	222	1600	0.07	1	3
9. Caus/Wash SB LTTRR	*	150	94	3.0	2353	1600	0.07	1	3
10. Caus/Wash WB LLTT	*	150	119	3.0	321	1600	0.07	1	3
11. Caus/Wash WB R	*	150	104	3.0	230	1600	0.07	1	3
12. Caus/Wash NB TTR	*	150	120	3.0	741	1600	0.07	1	3
13. Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	0.07	1	3
14. Tha/Val SB LTTR	*	104	30	3.0	1678	1600	0.07	1	3
15. Tha/Val NB L	*	104	74	3.0	472	1600	0.07	1	3
16. Tha/Val NB TR	*	104	30	3.0	737	1600	0.07	1	3
17. Bev/Was SB TTT	*	100	45	3.0	1628	1600	0.07	1	3
18. Bev/Was EB RRR	*	100	55	3.0	356	1600	0.07	1	3
19. Char/93 SB LLTTRR	*	100	53	3.0	1986	1600	0.07	1	3
20. Char/93 WB LTT	*	100	69	3.0	515	1600	0.07	1	3
21. Char/93 EB TTR	*	100	69	3.0	403	1600	0.07	1	3
22. North/Congress SB LT	*	100	90	3.0	647	1600	0.07	1	3
23. North/Con WB LLTR	*	100	60	3.0	997	1600	0.07	1	3
24. Nor/Con NB LTTTR	*	100	74	3.0	332	1600	0.07	1	3
25. Nor/Con EB LTR	*	100	60	3.0	17	1600	0.07	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2. Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3. Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4. Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5. Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6. Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7. Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8. Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9. Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10. Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11. Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12. Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13. Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14. Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15. Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16. Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17. Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18. Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19. Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20. Stan/Lom NW5	*	5136.5	5935.7	6.0	*
21. Caus/Wash NE1	*	6548.3	7035.9	6.0	*
22. Caus/Wash NE2	*	6581.4	6968.6	6.0	*
23. Caus/Wash NE3	*	6614.5	6901.3	6.0	*
24. Caus/Wash NE4	*	6669.8	6952.0	6.0	*
25. Caus/Wash NE5	*	6725.0	7002.7	6.0	*
26. Caus/Wash SE1	*	6753.6	6912.2	6.0	*

JOB: Government Center Garage RUN: No Build

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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Caus/Wash SE2	6698.9	6862.0	6.0
28. Caus/Wash SE3	6643.1	6810.8	6.0
29. Caus/Wash SE4	6646.8	6736.4	6.0
30. Caus/Wash SE5	6650.0	6661.0	6.0
31. Caus/Wash SW1	6544.0	6561.0	6.0
32. Caus/Wash SW2	6540.9	6636.0	6.0
33. Caus/Wash SW3	6537.8	6710.9	6.0
34. Caus/Wash SW4	6476.8	6667.2	6.0
35. Caus/Wash SW5	6415.9	6623.4	6.0
36. Caus/Wash NW1	6407.4	6738.0	6.0
37. Caus/Wash NW2	6468.3	6781.7	6.0
38. Caus/Wash NW3	6529.3	6825.4	6.0
39. Caus/Wash NW4	6496.2	6892.7	6.0
40. Caus/Wash NW5	6463.1	6960.0	6.0
41. Tha/Val NE1	6667.3	6395.5	6.0
42. Tha/Val NE2	6668.3	6320.5	6.0
43. Tha/Val NE3	6669.3	6245.5	6.0
44. Tha/Val NE4	6744.3	6245.5	6.0
45. Tha/Val NE5	6819.2	6249.6	6.0
46. Tha/Val SE1	6822.3	6191.6	6.0
47. Tha/Val SE2	6747.3	6189.6	6.0
48. Tha/Val SE3	6672.3	6187.5	6.0
49. Tha/Val SE4	6671.6	6112.5	6.0
50. Tha/Val SE5	6670.9	6037.5	6.0
51. Tha/Val SW1	6560.2	5964.7	6.0
52. Tha/Val SW2	6560.9	6039.7	6.0
53. Tha/Val SW3	6561.6	6114.7	6.0
54. Tha/Val SW4	6502.2	6068.9	6.0
55. Tha/Val SW5	6442.7	6023.2	6.0
56. Tha/Val NW1	6441.0	6115.2	6.0
57. Tha/Val NW2	6500.4	6160.9	6.0
58. Tha/Val NW3	6559.8	6206.7	6.0
59. Tha/Val NW4	6558.8	6281.7	6.0
60. Tha/Val NW5	6557.8	6356.7	6.0

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	2.	2.	3.	1.	1.	1.	2.	2.
10.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	2.	2.	2.	1.	1.	1.	1.	2.
20.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	2.	2.	2.	1.	1.	1.	1.	2.
30.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	2.	1.	1.	2.	2.	2.	1.	2.
40.	0.	0.	1.	0.	0.	2.	2.	2.	1.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.
50.	0.	0.	1.	1.	1.	1.	2.	2.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	3.	2.
60.	0.	0.	2.	2.	1.	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	2.	2.	1.	3.	2.
70.	0.	1.	3.	2.	2.	0.	1.	0.	0.	0.	1.	1.	2.	1.	1.	3.	2.	1.	3.	3.
80.	0.	1.	3.	3.	2.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	3.	2.	0.	2.	3.
90.	1.	1.	3.	3.	2.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	1.	2.	3.
100.	1.	2.	2.	3.	2.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	2.	2.
110.	1.	1.	2.	2.	2.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	2.	2.	2.	1.	2.
120.	1.	1.	2.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	2.
130.	1.	1.	2.	2.	2.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	2.
140.	1.	1.	2.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.
150.	1.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	1.
160.	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	4.	4.	5.	4.	2.	1.	2.	5.	5.	5.
10.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	4.	4.	5.	4.	2.	2.	2.	4.	5.	5.
20.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	4.	4.	4.	4.	3.	2.	2.	4.	4.	4.
30.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	3.	3.	4.	4.	3.	2.	2.	3.	4.	4.
40.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	3.	3.	4.	4.	3.	2.	2.	3.	4.	4.
50.	0.	0.	1.	0.	0.	0.	0.	1.	0.	0.	2.	2.	3.	3.	2.	2.	2.	4.	4.	4.
60.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	2.	3.	4.	4.	4.
70.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	1.	3.	3.	4.	4.	4.
80.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	2.	1.	3.	2.	4.	4.	4.
90.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	3.	2.	3.	4.	4.
100.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	3.	2.	3.	5.	5.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3)
170.	2. 2. 2. 2. 2. 0. 1. 1. 2. 1. 0. 0. 0. 0. 0. 2. 2. 2.
180.	2. 2. 3. 3. 2. 0. 1. 1. 2. 1. 0. 0. 0. 0. 0. 2. 2. 2.
190.	2. 2. 3. 3. 3. 1. 1. 2. 2. 1. 0. 0. 1. 0. 0. 1. 1. 2.
200.	2. 2. 2. 3. 3. 1. 1. 2. 2. 1. 0. 0. 2. 1. 1. 1. 1. 1.
210.	2. 1. 2. 2. 3. 1. 1. 2. 2. 1. 0. 0. 2. 2. 1. 0. 0. 0.
220.	2. 1. 2. 2. 2. 1. 1. 1. 2. 2. 0. 1. 2. 2. 2. 0. 0. 0.
230.	2. 2. 1. 1. 2. 1. 1. 0. 2. 2. 0. 1. 2. 2. 2. 0. 0. 0.
240.	1. 2. 1. 1. 1. 1. 1. 0. 1. 2. 0. 1. 2. 2. 2. 0. 0. 0.
250.	1. 2. 1. 1. 1. 1. 1. 0. 1. 2. 1. 1. 2. 2. 2. 0. 0. 0.
260.	1. 2. 1. 1. 1. 2. 1. 0. 1. 2. 1. 1. 2. 2. 2. 0. 0. 0.
270.	1. 2. 1. 1. 1. 2. 2. 0. 1. 2. 1. 1. 1. 2. 2. 0. 0. 0.
280.	1. 2. 2. 1. 0. 2. 2. 0. 0. 1. 1. 1. 1. 2. 2. 0. 0. 0.
290.	1. 2. 2. 1. 0. 3. 2. 0. 0. 1. 1. 1. 1. 2. 2. 0. 0. 0.
300.	1. 2. 2. 1. 0. 2. 2. 0. 1. 1. 1. 1. 1. 2. 2. 0. 0. 0.
310.	1. 2. 2. 0. 0. 2. 3. 1. 1. 1. 2. 1. 1. 2. 2. 0. 0. 0.
320.	1. 1. 1. 0. 0. 2. 2. 2. 2. 1. 2. 2. 1. 2. 2. 0. 0. 0.
330.	0. 0. 1. 0. 0. 2. 2. 2. 2. 1. 2. 2. 2. 2. 2. 0. 0. 0.
340.	0. 0. 0. 0. 0. 2. 2. 2. 1. 1. 2. 2. 2. 2. 3. 0. 0. 1.
350.	0. 0. 0. 0. 0. 2. 2. 2. 1. 1. 2. 2. 2. 2. 3. 1. 1. 1.
360.	0. 0. 0. 0. 0. 2. 2. 2. 1. 1. 1. 2. 2. 2. 3. 1. 1. 1.
MAX	2. 2. 3. 3. 3. 3. 3. 2. 2. 2. 2. 2. 2. 2. 3. 3. 2. 2.
DEGR.	180 180 80 190 200 290 310 330 210 250 320 0 220 340 350 70 90 40 60 80

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

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 110. *   0.   1.   2.   2.   1.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   3.   3.   3.
4.    5.
 120. *   1.   1.   2.   2.   1.   0.   0.   0.   0.   0.   2.   2.   2.   2.   1.   2.   3.   3.
4.    5.
 130. *   1.   1.   2.   2.   1.   0.   0.   0.   0.   0.   2.   2.   2.   2.   1.   2.   3.   4.
4.    5.
 140. *   1.   1.   2.   2.   1.   0.   0.   0.   0.   0.   3.   3.   3.   2.   1.   2.   4.   4.
4.    4.
 150. *   2.   2.   2.   2.   1.   0.   0.   0.   0.   0.   3.   3.   3.   2.   1.   2.   4.   4.
3.    4.
 160. *   4.   3.   3.   2.   1.   0.   0.   0.   0.   1.   4.   3.   4.   2.   2.   2.   4.   4.
3.    3.
 170. *   6.   5.   4.   2.   2.   0.   0.   2.   2.   2.   4.   4.   4.   2.   1.   2.   4.   5.
3.    3.
 180. *   6.   6.   5.   4.   2.   1.   2.   4.   3.   4.   3.   2.   2.   1.   0.   2.   2.   4.
2.    2.
 190. *   5.   5.   6.   4.   3.   2.   2.   4.   4.   4.   1.   1.   1.   0.   0.   1.   2.   2.
2.    1.
 200. *   4.   4.   5.   4.   3.   1.   2.   3.   4.   4.   0.   0.   0.   0.   0.   1.   1.   2.
1.    0.
 210. *   4.   4.   4.   4.   3.   1.   2.   3.   3.   3.   0.   0.   0.   0.   0.   1.   1.   2.
1.    0.
 220. *   4.   4.   4.   4.   3.   2.   2.   3.   3.   3.   0.   0.   0.   0.   0.   1.   1.   2.
0.    0.
 230. *   4.   4.   4.   4.   3.   3.   2.   2.   3.   3.   3.   0.   0.   1.   1.   0.   1.   1.
0.    0.
 240. *   4.   4.   4.   4.   2.   2.   3.   3.   4.   3.   3.   0.   0.   1.   1.   1.   0.   1.
0.    0.
 250. *   4.   4.   3.   2.   2.   3.   3.   3.   3.   3.   3.   0.   0.   2.   1.   1.   0.   0.
0.    0.
 260. *   3.   3.   3.   2.   2.   3.   3.   3.   4.   3.   3.   0.   0.   2.   1.   1.   0.   0.
0.    0.
 270. *   3.   3.   3.   2.   2.   3.   3.   3.   4.   3.   3.   0.   1.   2.   1.   1.   0.   0.
0.    0.
 280. *   4.   4.   4.   4.   2.   2.   3.   4.   3.   3.   3.   0.   1.   2.   1.   1.   0.   0.
0.    0.
 290. *   4.   4.   4.   4.   2.   2.   3.   4.   4.   3.   3.   0.   1.   2.   1.   1.   0.   0.
0.    0.
 300. *   4.   4.   4.   4.   2.   1.   3.   4.   4.   3.   3.   0.   1.   2.   1.   1.   0.   0.
0.    0.
 310. *   4.   4.   5.   2.   1.   2.   4.   5.   4.   4.   0.   1.   2.   1.   1.   0.   0.   0.
0.    0.
 320. *   4.   4.   4.   1.   0.   2.   4.   6.   5.   4.   1.   1.   2.   1.   1.   0.   0.   1.
1.    1.
 330. *   2.   3.   3.   0.   0.   1.   3.   5.   5.   5.   1.   2.   3.   2.   1.   0.   0.   2.
2.    2.
 340. *   1.   1.   2.   0.   0.   1.   2.   4.   4.   5.   2.   2.   4.   2.   1.   0.   1.   4.
4.    4.
 350. *   0.   0.   0.   0.   0.   1.   2.   2.   3.   3.   3.   4.   5.   3.   2.   1.   2.   5.
5.    5.
 360. *   0.   0.   0.   0.   0.   1.   2.   2.   2.   2.   4.   4.   5.   4.   2.   1.   2.   5.
5.    5.

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 MAX   *   6.   6.   6.   4.   3.   3.   4.   6.   5.   5.   4.   4.   5.   4.   3.   3.   4.   5.
5.    5.
 DEGR. *  180   180   190   190   200   280   310   320   330   330   170     0     0    20    40    90   150   350
350   110
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3.    2.
  60. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   3.   2.   2.   2.   2.   3.
2.    2.
  70. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   3.   3.   2.   2.   2.   2.   2.
2.    2.
  80. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   4.   3.   2.   2.   2.   2.   3.
2.    2.
  90. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   4.   3.   2.   2.   2.   2.   3.
3.    3.
 100. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   3.   3.   2.   2.   2.   2.   4.
2.    2.
 110. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   3.   3.   2.   2.   2.   2.   4.
2.    2.
 120. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   4.   3.   2.   2.   2.   2.   4.
3.    3.
 130. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   4.   4.   2.   2.   2.   2.   4.
3.    3.
 140. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   4.   3.   3.   3.   3.   4.
4.    3.
 150. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   5.   5.   4.   3.   3.   3.   3.   5.
4.    4.
 160. *   0.   0.   0.   0.   0.   0.   0.   0.   1.   1.   7.   5.   5.   4.   2.   3.   4.   5.
5.    4.
 170. *   2.   2.   2.   0.   0.   0.   0.   2.   2.   2.   8.   6.   5.   3.   1.   2.   3.   5.
5.    5.
 180. *   4.   4.   4.   1.   1.   1.   1.   3.   3.   3.   6.   4.   4.   2.   0.   0.   2.   4.
4.    4.
 190. *   4.   5.   5.   2.   1.   1.   2.   5.   5.   4.   3.   2.   2.   1.   0.   0.   1.   2.
2.    2.
 200. *   4.   5.   5.   2.   1.   1.   2.   5.   5.   5.   2.   1.   1.   0.   0.   0.   0.   1.
0.    0.
 210. *   3.   4.   5.   2.   2.   2.   3.   5.   5.   5.   1.   1.   0.   0.   0.   0.   0.   0.
0.    0.
 220. *   3.   4.   4.   2.   2.   2.   2.   4.   4.   5.   1.   0.   0.   0.   0.   0.   0.   0.
0.    0.
 230. *   3.   3.   4.   2.   2.   2.   2.   4.   4.   4.   1.   0.   0.   0.   0.   0.   0.   0.
0.    0.
 240. *   3.   3.   3.   2.   1.   1.   2.   4.   4.   4.   1.   0.   0.   0.   0.   0.   0.   0.
0.    0.
 250. *   2.   3.   3.   2.   1.   2.   2.   4.   4.   4.   1.   0.   1.   0.   0.   0.   0.   0.
0.    0.
 260. *   3.   3.   3.   2.   1.   1.   2.   4.   3.   4.   2.   0.   1.   0.   0.   0.   0.   0.
0.    0.
 270. *   2.   3.   3.   2.   1.   1.   2.   4.   4.   4.   2.   0.   1.   0.   0.   0.   0.   0.
0.    0.
 280. *   2.   2.   3.   2.   1.   1.   2.   4.   3.   4.   2.   0.   0.   0.   0.   0.   0.   0.
0.    0.
 290. *   2.   2.   2.   2.   1.   1.   2.   3.   3.   4.   2.   0.   0.   0.   0.   0.   0.   0.
0.    0.
 300. *   3.   3.   3.   2.   1.   1.   2.   3.   4.   4.   1.   0.   0.   0.   0.   0.   0.   0.
0.    0.
 310. *   3.   3.   3.   2.   1.   1.   2.   3.   4.   4.   2.   0.   0.   0.   0.   0.   0.   0.
0.    0.
 320. *   3.   3.   3.   2.   2.   2.   2.   3.   4.   4.   1.   0.   1.   0.   0.   0.   0.   0.
0.    0.
 330. *   4.   4.   4.   2.   2.   2.   2.   4.   4.   5.   1.   0.   1.   0.   0.   0.   0.   0.
0.    0.
 340. *   4.   4.   4.   2.   1.   1.   2.   4.   5.   5.   1.   1.   1.   1.   0.   0.   0.   1.
1.    1.
 350. *   3.   4.   4.   2.   1.   1.   2.   4.   5.   5.   2.   2.   2.   1.   0.   1.   1.   2.
2.    2.
 360. *   2.   2.   2.   0.   0.   0.   0.   2.   3.   3.   4.   3.   4.   2.   1.   1.   2.   3.
3.    3.

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 MAX   *   4.   5.   5.   2.   2.   2.   3.   5.   5.   5.   8.   6.   5.   4.   3.   3.   3.   5.
5.    5.
 DEGR. *  190   190   200   210   210   220   210   200   200   210   170   170   170   160   150   150   160   160
170   170
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THE HIGHEST CONCENTRATION OF 8. ug/m**3 OCCURRED AT RECEPTOR REC51.

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

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 WIND  * CONCENTRATION
 ANGLE *      (ug/m**3)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52 REC53 REC54 REC55 REC56 REC57 REC58
REC59 REC60

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   0. *   2.   2.   2.   0.   0.   0.   0.   2.   3.   3.   4.   3.   4.   2.   1.   1.   2.   3.
3.    3.
  10. *   1.   1.   1.   0.   0.   0.   0.   1.   1.   1.   5.   4.   4.   2.   2.   1.   2.   4.
4.    3.
  20. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   5.   4.   4.   3.   2.   1.   2.   4.
3.    3.
  30. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   4.   2.   2.   1.   2.   3.
3.    3.
  40. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   4.   2.   2.   1.   2.   3.
3.    2.
  50. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   4.   4.   4.   2.   2.   2.   2.   3.
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CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 7:31

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	0.	100.0	1.0	10.0	0.71	7.8
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5111.3	6026.2	*	109.	325.	AG	0.	100.0	1.0	20.0	0.50	5.5
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	0.	100.0	1.0	20.0	0.92	9.6
4.	Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	0.	100.0	1.0	10.0	0.58	6.4
5.	Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	0.	100.0	1.0	10.0	0.64	4.1
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5363.1	5748.8	*	51.	109.	AG	0.	100.0	1.0	20.0	0.41	2.6
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	0.	100.0	1.0	20.0	0.68	4.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	0.	100.0	1.0	10.0	0.93	8.1
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6176.7	7641.4	*	857.	334.	AG	0.	100.0	1.0	40.0	1.08	43.6
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	0.	100.0	1.0	20.0	0.58	5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	0.	100.0	1.0	10.0	0.53	6.6
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6665.3	5376.7	*	1377.	177.	AG	0.	100.0	1.0	20.0	1.39	69.9
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	0.	100.0	1.0	30.0	0.47	4.6
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.7	6361.5	*	138.	358.	AG	0.	100.0	1.0	20.0	0.79	7.0
15.	Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	0.	100.0	1.0	10.0	1.23	59.7
16.	Tha/Val NB TR	*	6645.6	6138.6	6647.7	6017.7	*	121.	179.	AG	0.	100.0	1.0	10.0	0.69	6.1
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6097.3	*	133.	0.	AG	0.	100.0	1.0	30.0	0.68	6.8
18.	Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	0.	100.0	1.0	30.0	0.18	1.8
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.3	5883.7	*	144.	358.	AG	0.	100.0	1.0	40.0	0.74	7.3
20.	Char/93 WB LTT	*	6702.8	5647.8	6763.4	5572.1	*	97.	141.	AG	0.	100.0	1.0	20.0	0.62	4.9
21.	Char/93 EB TTR	*	6560.8	5622.5	6520.0	5592.6	*	51.	234.	AG	0.	100.0	1.0	30.0	0.32	2.6
22.	North/Congress SB LT	*	6876.6	4408.9	6569.4	5930.4	*	1552.	349.	AG	0.	100.0	1.0	30.0	2.69	78.8
23.	North/Con WB LLTR	*	6920.6	4378.3	7106.5	4444.1	*	197.	71.	AG	0.	100.0	1.0	20.0	0.89	10.0
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6920.9	4289.3	*	45.	172.	AG	0.	100.0	1.0	30.0	0.33	2.3
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	0.	100.0	1.0	10.0	0.03	0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1396.	0.0	1.0	90.0		
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1568.	0.0	1.0	78.0		
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	899.	0.0	1.0	78.0		
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	0.0	1.0	78.0		
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3419.	0.0	1.0	90.0		
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	0.0	1.0	66.0		
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2371.	0.0	1.0	90.0		
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	0.0	1.0	78.0		
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2397.	0.0	1.0	90.0		
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	0.0	1.0	38.0		
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2837.	0.0	1.0	90.0		
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	0.0	1.0	54.0		
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2324.	0.0	1.0	66.0		
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	0.0	1.0	48.0		
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	515.	0.0	1.0	42.0		
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	0.0	1.0	48.0		
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	403.	0.0	1.0	54.0		
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	702.	0.0	1.0	54.0		

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	0.0	1.0	42.0		
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1343.	0.0	1.0	98.0		
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1063.	0.0	1.0	66.0		
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1529.	0.0	1.0	98.0		
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	0.0	1.0	54.0		

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
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LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1343.	0.0	1.0	98.0		
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1063.	0.0	1.0	66.0		
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1529.	0.0	1.0	98.0		
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	0.0	1.0	54.0		

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
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	LINK DESCRIPTION	*	X1	Y1	X2	Y2	*	VPH	EF	H	W
1.	Stan/Lom SB L	*	120	75	3.0	376		1600	0.07	1	3
2.	Stan/Lom SB TRR	*	120	75	3.0	531		1600	0.07	1	3
3.	Stan/Lom WB LTT	*	120	91	3.0	588		1600	0.07	1	3
4.	Stan/Lom WB R	*	120	75	3.0	308		1600	0.07	1	3
5.	Stan/Lom NB L	*	120	97	3.0	152		1600	0.07	1	3
6.	Stan/Lom NB TRR	*	120	97	3.0	194		1600	0.07	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	324		1600	0.07	1	3
8.	Stan/Lom EB R	*	120	97	3.0	222		1600	0.07	1	3
9.	Caus/Wash SB LTTRR	*	150	94	3.0	2353		1600	0.07	1	3
10.	Caus/Wash WB LLTT	*	150	119	3.0	321		1600	0.07	1	3
11.	Caus/Wash WB R	*	150	104	3.0	230		1600	0.07	1	3
12.	Caus/Wash NB TTR	*	150	120	3.0	741		1600	0.07	1	3
13.	Caus/Wash EB LLTTR	*	150	117	3.0	422		1600	0.07	1	3
14.	Tha/Val SB LTTR	*	104	30	3.0	1678		1600	0.07	1	3
15.	Tha/Val NB L	*	104	74	3.0	472		1600	0.07	1	3
16.	Tha/Val NB TR	*	104	30	3.0	737		1600	0.07	1	3
17.	Bev/Was SB TTT	*	100	45	3.0	1628		1600	0.07	1	3
18.	Bev/Was EB RRR	*	100	55	3.0	356		1600	0.07	1	3
19.	Char/93 SB LLTTRR	*	100	53	3.0	1986		1600	0.07	1	3
20.	Char/93 WB LTT	*	100	69	3.0	515		1600	0.07	1	3
21.	Char/93 EB TTR	*	100	69	3.0	403		1600	0.07	1	3
22.	North/Congress SB LT	*	100	90	3.0	647		1600	0.07	1	3
23.	North/Con WB LLTR	*	100	60	3.0	997		1600	0.07	1	3
24.	Nor/Con NB LTTTR	*	100	74	3.0	332		1600	0.07	1	3
25.	Nor/Con EB LTR	*	100	60	3.0	17		1600	0.07	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Bev/Was N1	*	6562.0	6150.2	6.0	*
2.	Bev/Was N2	*	6561.2	6075.2	6.0	*
3.	Bev/Was N3	*	6560.5	6000.2	6.0	*
4.	Bev/Was N4	*	6515.8	6060.4	6.0	*
5.	Bev/Was N5	*	6471.1	6120.6	6.0	*
6.	Bev/Was SE1	*	6671.0	6049.7	6.0	*
7.	Bev/Was SE2	*	6670.2	5966.3	6.0	*
8.	Bev/Was SE3	*	6624.0	5907.2	6.0	*
9.	Bev/Was SE4	*	6626.1	5832.3	6.0	*
10.	Bev/Was SE5	*	6628.1	5757.3	6.0	*
11.	Bev/Was SW1	*	6541.8	5766.9	6.0	*
12.	Bev/Was SW2	*	6540.1	5841.9	6.0	*
13.	Bev/Was SW3	*	6537.7	5916.8	6.0	*
14.	Bev/Was SW4	*	6493.0	5977.0	6.0	*
15.	Bev/Was SW5	*	6448.3	6037.3	6.0	*
16.	Char/93 NE1	*	6625.0	5871.1	6.0	*
17.	Char/93 NE2	*	6627.1	5796.1	6.0	*
18.	Char/93 NE3	*	6629.1	5721.1	6.0	*
19.	Char/93 NE4	*	6699.8	5695.9	6.0	*
20.	Char/93 NE5	*	6750.6	5633.2	6.0	*
21.	Char/93 S1	*	6657.8	5466.0	6.0	*
22.	Char/93 S2	*	6614.7	5527.4	6.0	*
23.	Char/93 S3	*	6571.7	5588.8	6.0	*
24.	Char/93 S4	*	6512.9	5542.2	6.0	*
25.	Char/93 S5	*	6454.1	5495.6	6.0	*
26.	Char/93 NW1	*	6424.1	5632.5	6.0	*

JOB: Government Center Garage RUN: No Build

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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Char/93 NW2	6483.6	5678.2	6.0
28. Char/93 NW3	6543.0	5723.9	6.0
29. Char/93 NW4	6541.0	5798.8	6.0
30. Char/93 NW5	6538.9	5873.8	6.0
31. Wash/Cong NE1	6910.2	4571.2	6.0
32. Wash/Cong NE2	6925.8	4497.8	6.0
33. Wash/Cong NE3	6941.4	4424.5	6.0
34. Wash/Cong NE4	7012.0	4449.6	6.0
35. Wash/Cong NE5	7082.7	4474.9	6.0
36. Wash/Cong SE1	7095.4	4388.1	6.0
37. Wash/Cong SE2	7024.8	4362.9	6.0
38. Wash/Cong SE3	6954.1	4337.7	6.0
39. Wash/Cong SE4	6968.4	4264.1	6.0
40. Wash/Cong SE5	6982.7	4190.4	6.0
41. Wash/Cong SW1	6867.5	4164.7	6.0
42. Wash/Cong SW2	6853.3	4238.0	6.0
43. Wash/Cong SW3	6838.9	4312.0	6.0
44. Wash/Cong SW4	6765.6	4296.1	6.0
45. Wash/Cong SW5	6692.3	4280.2	6.0
46. Wash/Cong NW1	6682.4	4353.8	6.0
47. Wash/Cong NW2	6755.7	4369.7	6.0
48. Wash/Cong NW3	6828.9	4386.0	6.0
49. Wash/Cong NW4	6813.3	4459.4	6.0
50. Wash/Cong NW5	6797.8	4532.8	6.0

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	4.	4.	3.	2.	1.	3.	3.	8.	7.	6.	4.	3.	3.	2.	1.	7.	6.	7.	2.	1.
10.	5.	4.	4.	2.	2.	1.	1.	7.	5.	4.	6.	5.	4.	2.	2.	6.	5.	5.	0.	0.
20.	5.	4.	5.	3.	2.	0.	0.	5.	3.	3.	6.	5.	4.	2.	2.	4.	3.	3.	0.	0.
30.	4.	4.	4.	3.	2.	0.	0.	4.	3.	2.	6.	5.	4.	2.	2.	3.	2.	2.	0.	0.
40.	4.	4.	4.	2.	2.	0.	0.	3.	2.	2.	5.	5.	4.	2.	2.	2.	2.	2.	0.	0.
50.	4.	3.	4.	2.	2.	0.	0.	2.	2.	1.	5.	5.	4.	2.	2.	2.	2.	1.	0.	0.
60.	4.	3.	4.	2.	2.	0.	0.	2.	2.	1.	4.	5.	4.	2.	2.	2.	1.	1.	0.	0.
70.	4.	3.	3.	2.	2.	0.	0.	2.	2.	1.	4.	4.	4.	3.	2.	2.	1.	1.	0.	0.
80.	3.	3.	3.	2.	2.	0.	0.	2.	1.	1.	4.	4.	4.	3.	2.	2.	1.	1.	0.	0.
90.	3.	4.	4.	2.	2.	0.	0.	2.	1.	1.	4.	5.	4.	3.	2.	2.	1.	1.	0.	0.
100.	3.	4.	3.	2.	2.	0.	0.	2.	1.	1.	4.	4.	4.	3.	2.	2.	1.	1.	0.	0.
110.	3.	3.	3.	2.	2.	0.	0.	2.	2.	1.	4.	4.	4.	3.	2.	2.	1.	2.	0.	0.
120.	3.	4.	3.	2.	2.	0.	0.	2.	2.	1.	4.	5.	4.	3.	2.	2.	1.	2.	0.	0.
130.	3.	4.	3.	3.	2.	0.	0.	2.	2.	2.	4.	5.	5.	3.	2.	2.	2.	2.	0.	0.
140.	4.	4.	3.	3.	3.	0.	0.	2.	2.	3.	4.	6.	6.	3.	3.	2.	2.	3.	1.	0.
150.	4.	5.	4.	3.	3.	0.	0.	3.	3.	3.	4.	6.	6.	4.	3.	3.	3.	4.	1.	1.
160.	5.	5.	6.	4.	3.	0.	0.	4.	4.	5.	3.	5.	6.	3.	2.	4.	4.	5.	2.	1.
170.	5.	6.	6.	3.	3.	2.	2.	5.	5.	6.	2.	4.	5.	2.	1.	5.	6.	7.	3.	2.
180.	4.	4.	5.	2.	1.	3.	3.	6.	6.	6.	1.	2.	2.	1.	0.	6.	6.	7.	3.	3.
190.	2.	2.	3.	1.	1.	4.	4.	6.	6.	5.	1.	1.	1.	0.	0.	6.	5.	6.	3.	3.
200.	1.	1.	2.	0.	0.	5.	4.	6.	6.	4.	1.	0.	0.	0.	0.	6.	5.	5.	3.	3.
210.	1.	0.	1.	0.	0.	5.	5.	5.	5.	4.	0.	0.	0.	0.	0.	5.	5.	4.	3.	3.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	10.	6.	5.	3.	2.	1.	1.	4.	3.	3.	0.	0.	1.	0.	0.	1.	1.	2.	2.	1.
10.	8.	5.	5.	4.	2.	2.	2.	5.	5.	4.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
20.	6.	4.	4.	4.	3.	2.	3.	6.	6.	5.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.
30.	5.	4.	3.	3.	3.	2.	3.	6.	6.	5.	0.	0.	0.	0.	0.	0.	1.	2.	1.	0.
40.	4.	4.	2.	2.	2.	2.	3.	5.	6.	5.	0.	0.	0.	0.	0.	0.	1.	2.	0.	0.
50.	4.	4.	2.	2.	2.	2.	2.	4.	5.	5.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
60.	4.	4.	3.	2.	1.	2.	2.	4.	4.	5.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
70.	3.	4.	3.	2.	1.	2.	2.	3.	4.	4.	0.	0.	1.	0.	0.	0.	0.	1.	0.	0.
80.	3.	4.	3.	2.	1.	2.	2.	3.	4.	4.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
90.	3.	4.	3.	2.	1.	2.	2.	2.	4.	4.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
100.	3.	4.	3.	2.	1.	2.	2.	2.	4.	4.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
110.	3.	4.	3.	2.	1.	2.	3.	2.	4.	5.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
120.	3.	4.	3.	1.	1.	2.	3.	2.	5.	5.	0.	1.	2.	1.	0.	0.	0.	0.	0.	0.
130.	4.	3.	2.	1.	1.	2.	3.	3.	5.	5.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.
140.	5.	3.	2.	1.	1.	2.	3.	3.	5.	6.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.
150.	6.	3.	2.	1.	1.	2.	2.	3.	5.	6.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

	WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
MAX		5.	6.	6.	4.	3.	5.	5.	8.	7.	8.	6.	6.	6.	4.	3.	7.	7.	9.	4.	3.
DEGR.		170	170	170	160	150	340	340	0	0	350	20	150	150	150	150	0	350	340	320	260

160.	*	7.	3.	2.	1.	1.	1.	2.	3.	4.	6.	1.	1.	2.	1.	1.	0.	0.	0.
0.	0.																		
170.	*	7.	2.	1.	1.	0.	1.	2.	2.	3.	4.	2.	2.	2.	2.	1.	0.	0.	1.
1.	1.																		
180.	*	6.	1.	0.	0.	0.	1.	1.	1.	1.	2.	2.	2.	3.	2.	1.	0.	0.	1.
1.	1.																		
190.	*	4.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	3.	2.	2.	0.	0.	2.
1.	1.																		
200.	*	3.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	3.	2.	2.	0.	1.	2.
1.	1.																		
210.	*	2.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	2.	2.	0.	1.	2.
1.	1.																		
220.	*	2.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	2.	2.	0.	1.	2.
1.	1.																		
230.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
240.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
250.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	1.	2.
1.	1.																		
260.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.
1.	1.																		
270.	*	1.	0.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.
1.	1.																		
280.	*	2.	1.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.
1.	1.																		
290.	*	2.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.
1.	1.																		
300.	*	2.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	3.	2.
2.	1.																		
310.	*	2.	1.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.
2.	2.																		
320.	*	3.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.
3.	2.																		
330.	*	5.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	3.	1.	1.	2.	3.	4.
3.	2.																		
340.	*	8.	2.	2.	1.	1.	0.	0.	0.	0.	1.	2.	2.	3.	1.	1.	2.	2.	4.
3.	3.																		
350.	*	10.	4.	3.	2.	1.	0.	0.	2.	2.	2.	2.	2.	2.	1.	0.	2.	2.	3.
3.	2.																		
360.	*	10.	6.	5.	3.	2.	1.	1.	4.	3.	3.	0.	0.	1.	0.	0.	1.	1.	2.
2.	1.																		
------	*	----------																	

MAX	*	10.	6.	5.	4.	3.	2.	3.	6.	6.	6.	3.	2.	3.	2.	2.	2.	3.	4.
3.	3.																		
DEGR.	*	350	0	0	10	20	100	30	20	20	150	340	330	190	210	220	300	300	340
340	340																		

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50
0.	* 2.	3.	3.	1.	1.	1.	2.	3.	3.	3.
10.	* 2.	2.	2.	1.	1.	1.	1.	3.	3.	2.
20.	* 2.	2.	2.	1.	1.	1.	1.	3.	2.	2.
30.	* 2.	2.	2.	1.	1.	1.	1.	2.	2.	2.
40.	* 2.	2.	2.	1.	1.	1.	1.	2.	2.	2.
50.	* 1.	2.	2.	1.	1.	1.	1.	2.	2.	2.
60.	* 1.	2.	2.	2.	1.	1.	1.	2.	2.	2.
70.	* 1.	1.	2.	1.	1.	1.	1.	2.	2.	2.
80.	* 1.	1.	2.	1.	1.	1.	1.	2.	2.	2.
90.	* 1.	1.	2.	1.	1.	1.	2.	2.	2.	2.
100.	* 1.	1.	2.	1.	0.	1.	1.	2.	3.	2.
110.	* 1.	1.	2.	1.	0.	1.	1.	2.	3.	2.
120.	* 1.	1.	1.	1.	0.	0.	1.	2.	3.	3.
130.	* 1.	1.	1.	1.	0.	0.	1.	2.	2.	3.
140.	* 1.	1.	1.	1.	0.	0.	1.	2.	2.	3.
150.	* 1.	1.	2.	0.	0.	0.	0.	2.	2.	2.
160.	* 1.	1.	1.	0.	0.	0.	0.	1.	2.	2.
170.	* 0.	1.	1.	0.	0.	0.	0.	1.	1.	1.
180.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
190.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
200.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
210.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
220.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

240.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
250.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
260.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
270.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
280.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
290.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
300.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
310.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
320.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
330.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
340.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
350.	* 2.	2.	2.	1.	1.	1.	1.	3.	3.	3.
360.	* 2.	3.	3.	1.	1.	1.	2.	3.	3.	3.
------	* ----------									
MAX	* 2.	3.	3.	2.	1.	1.	2.	3.	3.	3.
DEGR.	* 0	0	0	60	70	0	0	0	0	0

THE HIGHEST CONCENTRATION OF 10. ug/m**3 OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 5:19

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5120.9	6056.9	*	131.	326.	AG	0.	100.0	1.0	10.0	0.63	6.7
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5093.7	6051.5	*	140.	325.	AG	0.	100.0	1.0	20.0	0.67	7.1
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5368.6	5981.0	*	80.	51.	AG	0.	100.0	1.0	20.0	0.35	4.1
4.	Stan/Lom WB R	*	5292.4	5947.7	5403.8	6033.2	*	140.	52.	AG	0.	100.0	1.0	10.0	0.68	7.1
5.	Stan/Lom NB L	*	5307.6	5737.4	5341.6	5726.9	*	36.	107.	AG	0.	100.0	1.0	10.0	0.24	1.8
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5383.7	5741.9	*	73.	109.	AG	0.	100.0	1.0	20.0	0.49	3.7
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5171.4	5556.9	*	155.	196.	AG	0.	100.0	1.0	20.0	0.92	7.9
8.	Stan/Lom EB R	*	5236.5	5698.5	4944.8	4671.4	*	1068.	196.	AG	0.	100.0	1.0	10.0	1.34	54.2
9.	Char/93 SB LLTTRR	*	6587.8	5740.0	6580.9	5920.1	*	180.	358.	AG	0.	100.0	1.0	40.0	0.87	9.2
10.	Char/93 WB LTT	*	6702.8	5647.8	6735.6	5606.8	*	52.	141.	AG	0.	100.0	1.0	20.0	0.29	2.7
11.	Char/93 EB TTR	*	6560.8	5622.5	6474.2	5559.1	*	107.	234.	AG	0.	100.0	1.0	30.0	0.58	5.5
12.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1623.	0.0	1.0	90.0		
13.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1414.	0.0	1.0	78.0		
14.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	1179.	0.0	1.0	78.0		
15.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1387.	0.0	1.0	78.0		
16.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2078.	0.0	1.0	66.0		
17.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	321.	0.0	1.0	42.0		
18.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	1059.	0.0	1.0	48.0		
19.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	983.	0.0	1.0	54.0		
20.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	488.	0.0	1.0	54.0		
21.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	414.	0.0	1.0	42.0		

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JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 5:19

		*								
1.	Stan/Lom SB L	*	120	79	3.0	304	1600	0.07	1	3
2.	Stan/Lom SB TRR	*	120	79	3.0	646	1600	0.07	1	3
3.	Stan/Lom WB LTT	*	120	71	3.0	412	1600	0.07	1	3
4.	Stan/Lom WB R	*	120	79	3.0	325	1600	0.07	1	3
5.	Stan/Lom NB L	*	120	93	3.0	70	1600	0.07	1	3
6.	Stan/Lom NB TRR	*	120	93	3.0	289	1600	0.07	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	439	1600	0.07	1	3
8.	Stan/Lom EB R	*	120	97	3.0	320	1600	0.07	1	3
9.	Char/93 SB LLTTRR	*	100	62	3.0	1829	1600	0.07	1	3
10.	Char/93 WB LTT	*	100	60	3.0	321	1600	0.07	1	3
11.	Char/93 EB TTR	*	100	60	3.0	983	1600	0.07	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8.	Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0	*

		*			
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0 *
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0 *
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0 *
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0 *
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0 *
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0 *
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0 *
21.	Char/93 NE1	*	6625.0	5871.1	6.0 *
22.	Char/93 NE2	*	6627.1	5796.1	6.0 *
23.	Char/93 NE3	*	6629.1	5721.1	6.0 *
24.	Char/93 NE4	*	6699.8	5695.9	6.0 *
25.	Char/93 NE5	*	6750.6	5633.2	6.0 *
26.	Char/93 S1	*	6657.8	5466.0	6.0 *
27.	Char/93 S2	*	6614.7	5527.4	6.0 *
28.	Char/93 S3	*	6571.7	5588.8	6.0 *
29.	Char/93 S4	*	6512.9	5542.2	6.0 *
30.	Char/93 S5	*	6454.1	5495.6	6.0 *
31.	Char/93 NW1	*	6424.1	5632.5	6.0 *
32.	Char/93 NW2	*	6483.6	5678.2	6.0 *
33.	Char/93 NW3	*	6543.0	5723.9	6.0 *
34.	Char/93 NW4	*	6541.0	5798.8	6.0 *
35.	Char/93 NW5	*	6538.9	5873.8	6.0 *

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JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) *	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	2.	2.	2.	3.	1.	1.	1.	2.	2.
10.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.
20.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	2.	2.	2.	2.	1.	1.	1.	1.	2.
30.	*	0.	0.	0.	0.	0.	1.	2.	2.	0.	0.	1.	1.	2.	1.	1.	2.	1.	2.	1.	2.
40.	*	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	2.	2.
50.	*	0.	0.	1.	1.	0.	1.	1.	1.	0.	0.	1.	1.	2.	1.	0.	2.	2.	1.	2.	2.
60.	*	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	1.	3.	2.
70.	*	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	0.	2.	2.
80.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	0.	2.	3.
90.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	1.	2.	2.
100.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	2.	2.	1.	2.
110.	*	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	2.	2.	2.	2.
120.	*	1.	1.	1.	2.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.
130.	*	1.	1.	2.	2.	1.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	1.	2.
140.	*	1.	1.	2.	2.	2.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	1.	1.
150.	*	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	1.	1.
160.	*	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.
170.	*	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.
180.	*	2.	2.	3.	2.	2.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.
190.	*	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	1.	2.	2.	2.	0.
200.	*	2.	2.	2.	3.	3.	1.	2.	2.	2.	1.	0.	0.	2.	2.	1.	1.	1.	1.	1.	0.
210.	*	2.	2.	2.	2.	3.	1.	2.	2.	2.	2.	0.	0.	2.	2.	2.	0.	0.	0.	0.	0.
220.	*	2.	2.	2.	2.	2.	1.	1.	1.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
230.	*	2.	2.	2.	1.	2.	1.	1.	0.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
240.	*	2.	2.	1.	1.	1.	1.	1.	0.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.

```
0.    0.
 250.  *    2.    2.    1.    1.    1.    1.    1.    0.    1.    3.    1.    1.    2.    2.    2.    0.    0.    0.
0.    0.
 260.  *    1.    2.    1.    1.    1.    2.    1.    0.    1.    2.    1.    1.    2.    2.    2.    0.    0.    0.
0.    0.
 270.  *    1.    2.    2.    1.    1.    2.    2.    0.    1.    2.    1.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 280.  *    1.    2.    2.    1.    1.    2.    2.    0.    1.    1.    1.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 290.  *    2.    2.    2.    1.    0.    2.    2.    0.    0.    1.    1.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 300.  *    2.    2.    2.    1.    0.    2.    3.    1.    1.    1.    1.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 310.  *    1.    2.    2.    0.    0.    2.    3.    1.    1.    1.    2.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 320.  *    1.    1.    1.    0.    0.    2.    2.    2.    2.    1.    2.    2.    2.    2.    2.    0.    0.    0.
1.    1.
 330.  *    0.    1.    1.    0.    0.    2.    2.    3.    2.    1.    2.    2.    2.    2.    2.    0.    0.    1.
2.    1.
 340.  *    0.    0.    0.    0.    0.    2.    2.    2.    1.    1.    2.    2.    2.    2.    3.    0.    0.    1.
2.    2.
 350.  *    0.    0.    0.    0.    0.    1.    1.    2.    1.    1.    2.    2.    2.    2.    3.    0.    1.    1.
2.    2.
 360.  *    0.    0.    0.    0.    0.    1.    2.    2.    1.    0.    1.    2.    2.    2.    3.    1.    1.    1.
2.    2.

------*-------------------------------------------------------------------------------------------------------------
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 MAX   *    2.    2.    3.    3.    3.    2.    3.    3.    2.    3.    2.    2.    2.    2.    3.    2.    2.    2.
3.    3.
 DEGR. *  180   170   190   190   200   290   310   330   210   250   320   340   220   350   350    70   160   180
60    80
```


JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35
0.	0.	1.	1.	0.	0.	2.	2.	2.	2.	1.	0.	0.	2.	1.	0.
10.	0.	0.	0.	0.	0.	1.	2.	2.	3.	2.	0.	0.	3.	2.	1.
20.	0.	0.	0.	0.	0.	1.	1.	2.	3.	2.	0.	1.	3.	3.	1.
30.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.	1.	2.	3.	3.	2.
40.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.	1.	2.	3.	3.	2.
50.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	3.	3.	2.
60.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	3.	3.
70.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	3.	3.
80.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	3.	3.
90.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	1.	1.	3.	3.
100.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	1.	0.	3.	3.
110.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	3.	3.
120.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	3.	3.
130.	0.	0.	1.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	3.	3.
140.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	3.	4.
150.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	2.	2.	3.	4.
160.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	2.	3.
170.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.
180.	2.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
190.	3.	2.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
200.	3.	2.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.
210.	4.	3.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.
220.	4.	3.	2.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
230.	3.	3.	1.	2.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
240.	3.	3.	1.	2.	2.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
250.	3.	3.	0.	1.	2.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
260.	3.	3.	1.	1.	2.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
270.	3.	3.	1.	1.	2.	0.	1.	2.	1.	0.	0.	0.	0.	0.	0.
280.	3.	3.	1.	1.	2.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.
290.	3.	3.	2.	1.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
300.	3.	3.	2.	1.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
310.	2.	3.	3.	2.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
320.	2.	3.	3.	2.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
330.	2.	3.	3.	1.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
340.	1.	3.	3.	1.	0.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.
350.	1.	2.	2.	0.	0.	2.	2.	2.	2.	1.	0.	0.	1.	0.	0.
360.	0.	1.	1.	0.	0.	2.	2.	2.	2.	1.	0.	0.	2.	1.	0.
MAX	4.	3.	3.	2.	2.	2.	2.	2.	3.	3.	2.	2.	3.	3.	4.
DEGR.	210	320	330	310	250	350	0	280	10	30	110	120	30	40	140

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:13:59

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6049.9	5447.4	*	66.	290.	AG	0.	100.0	1.0	30.0	0.52	3.3
2. Char/Merr WB	*	6250.4	5435.2	6333.8	5501.2	*	106.	52.	AG	0.	100.0	1.0	30.0	0.77	5.4
3. Char/Merr NB R	*	6291.7	5369.7	6315.3	5353.7	*	29.	124.	AG	0.	100.0	1.0	10.0	0.14	1.5
4. Char/Merr NB LTT	*	6280.4	5347.2	6430.5	5241.4	*	184.	125.	AG	0.	100.0	1.0	20.0	0.92	9.3
5. Char/Merr EB	*	6104.2	5362.2	6060.5	5345.9	*	47.	250.	AG	0.	100.0	1.0	20.0	0.42	2.4
6. Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.5	*	108.	14.	AG	0.	100.0	1.0	10.0	0.71	5.5
7. Char/Cam SB TR	*	5360.8	4833.5	5398.9	4956.5	*	129.	17.	AG	0.	100.0	1.0	20.0	0.92	6.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	0.	100.0	1.0	20.0	0.27	2.2
9. Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	0.	100.0	1.0	10.0	0.60	4.7
10. Char/Cam NB TR	*	5383.3	4723.8	5384.4	4650.0	*	74.	179.	AG	0.	100.0	1.0	20.0	0.71	3.7
11. Char/Cam EB TTTR	*	5302.7	4739.8	5214.1	4740.7	*	89.	271.	AG	0.	100.0	1.0	30.0	0.54	4.5
12. Sud/Merr SB L	*	6532.7	5210.3	6487.5	5242.5	*	56.	305.	AG	0.	100.0	1.0	10.0	0.72	2.8
13. Sud/Merr SB TTT	*	6518.3	5190.8	6477.9	5214.2	*	47.	300.	AG	0.	100.0	1.0	30.0	0.24	2.4
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6673.5	5068.9	*	106.	150.	AG	0.	100.0	1.0	30.0	0.60	5.4
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6478.2	5118.7	*	53.	239.	AG	1.	100.0	1.0	40.0	0.38	2.7
16. Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	0.	100.0	1.0	20.0	0.34	3.3
17. Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6745.9	5240.5	*	52.	249.	AG	0.	100.0	1.0	30.0	0.43	2.7
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	877.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1122.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1326.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	939.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	849.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1614.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	950.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1709.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	318.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	536.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	373.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1555.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1648.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	529.	0.0	1.0	78.0		

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	*								
1. Char/Merr SB	*	100	76	3.0	476	1600	0.07	1	3
2. Char/Merr WB	*	100	76	3.0	703	1600	0.07	1	3
3. Char/Merr NB R	*	100	45	3.0	116	1600	0.07	1	3
4. Char/Merr NB LTT	*	100	71	3.0	709	1600	0.07	1	3
5. Char/Merr EB	*	100	79	3.0	217	1600	0.07	1	3
6. Char/Cam SB L	*	90	58	3.0	339	1600	0.07	1	3
7. Char/Cam SB TR	*	90	71	3.0	457	1600	0.07	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	294	1600	0.07	1	3
9. Char/Cam NB L	*	90	58	3.0	289	1600	0.07	1	3
10. Char/Cam NB TR	*	90	71	3.0	354	1600	0.07	1	3

	*								
11. Char/Cam EB TTTR	*	90	54	3.0	901	1600	0.07	1	3
12. Sud/Merr SB L	*	100	86	3.0	104	1600	0.07	1	3
13. Sud/Merr SB TTT	*	100	49	3.0	524	1600	0.07	1	3
14. Sud/Merr NB TTTR	*	100	63	3.0	924	1600	0.07	1	3
15. Sud/Merr EB LTTR	*	100	73	3.0	529	1600	0.07	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	455	1600	0.07	1	3
17. Sud/Sur SEB	*	100	70	3.0	26	1600	0.07	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	373	1600	0.07	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Char/Merr NE1	*	6063.7	5511.0	6.0
2. Char/Merr NE2	*	6133.9	5484.8	6.0
3. Char/Merr NE3	*	6204.2	5458.5	6.0
4. Char/Merr NE4	*	6265.6	5501.5	6.0
5. Char/Merr NE5	*	6327.1	5544.5	6.0
6. Char/Merr SE1	*	6443.7	5491.9	6.0
7. Char/Merr SE2	*	6382.2	5448.9	6.0
8. Char/Merr SE3	*	6320.8	5405.9	6.0
9. Char/Merr SE4	*	6380.5	5360.4	6.0
10. Char/Merr SE5	*	6440.1	5315.0	6.0
11. Char/Merr SW1	*	6332.0	5249.0	6.0
12. Char/Merr SW2	*	6272.3	5294.5	6.0
13. Char/Merr SW3	*	6212.6	5339.9	6.0
14. Char/Merr SW4	*	6141.6	5315.8	6.0
15. Char/Merr SW5	*	6070.6	5291.7	6.0
16. Char/Merr NW1	*	5902.1	5359.1	6.0
17. Char/Merr NW2	*	5973.1	5383.2	6.0
18. Char/Merr NW3	*	6044.1	5407.3	6.0
19. Char/Merr NW4	*	5973.9	5433.5	6.0
20. Char/Merr NW5	*	5903.6	5459.8	6.0
21. Char/Cam NE1	*	5490.2	4963.0	6.0
22. Char/Cam NE2	*	5459.0	4894.8	6.0
23. Char/Cam NE3	*	5427.8	4826.6	6.0
24. Char/Cam NE4	*	5500.4	4807.6	6.0
25. Char/Cam NE5	*	5572.9	4788.7	6.0
26. Char/Cam SE1	*	5553.9	4667.5	6.0
27. Char/Cam SE2	*	5481.3	4686.5	6.0
28. Char/Cam SE3	*	5408.7	4705.4	6.0
29. Char/Cam SE4	*	5409.4	4630.4	6.0
30. Char/Cam SE5	*	5410.1	4555.4	6.0
31. Char/Cam SW1	*	5312.0	4561.9	6.0
32. Char/Cam SW2	*	5310.7	4636.9	6.0
33. Char/Cam SW3	*	5310.7	4711.9	6.0

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RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Char/Cam SW4	*	5235.6	4712.1	6.0
35. Char/Cam SW5	*	5160.6	4711.9	6.0
36. Char/Cam NW1	*	5167.9	4822.4	6.0
37. Char/Cam NW2	*	5242.9	4822.1	6.0
38. Char/Cam NW3	*	5317.9	4821.9	6.0
39. Char/Cam NW4	*	5349.1	4890.1	6.0
40. Char/Cam NW5	*	5380.3	4958.3	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	2.	1.	2.	0.	0.	1.	1.	1.
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	2.	1.	2.	0.	0.	1.	1.	1.
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	2.	1.	2.	0.	0.	2.		

1.	1.																				
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	1.	2.		
1.	1.																				
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	1.	2.		
1.	1.																				
50.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.		
1.	1.																				
60.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	2.	1.	2.	2.	2.	1.	1.	2.		
1.	1.																				
70.	*	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.	1.	2.	3.		
2.	1.																				
80.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.		
2.	1.																				
90.	*	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.		
2.	2.																				
100.	*	1.	1.	2.	2.	1.	0.	0.	0.	0.	1.	2.	2.	2.	1.	1.	2.	2.	2.		
2.	2.																				
110.	*	2.	2.	2.	2.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	1.	2.	2.		
2.	2.																				
120.	*	2.	2.	3.	2.	1.	0.	0.	1.	1.	2.	2.	2.	2.	1.	0.	1.	1.	2.		
2.	2.																				
130.	*	2.	3.	3.	2.	1.	0.	1.	2.	2.	3.	1.	1.	1.	0.	0.	1.	1.	2.		
1.	1.																				
140.	*	2.	2.	3.	3.	2.	0.	1.	2.	3.	3.	0.	0.	0.	0.	0.	1.	1.	1.		
1.	0.																				
150.	*	2.	2.	2.	3.	2.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	1.	1.	1.		
0.	0.																				
160.	*	2.	2.	2.	3.	2.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	1.	1.	1.		
0.	0.																				
170.	*	2.	1.	2.	3.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.		
0.	0.																				
180.	*	2.	1.	2.	3.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.		
0.	0.																				
190.	*	2.	2.	2.	2.	3.	1.	1.	2.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.		
1.	0.																				
200.	*	1.	2.	2.	2.	3.	1.	1.	1.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.		
1.	0.																				
210.	*	1.	2.	2.	2.	3.	1.	1.	1.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.		
1.	1.																				
220.	*	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.		
1.	0.																				
230.	*	1.	2.	2.	2.	2.	1.	1.	2.	1.	2.	0.	0.	0.	0.	1.	1.	1.	1.		
1.	0.																				
240.	*	1.	2.	2.	2.	1.	2.	2.	2.	2.	2.	0.	0.	0.	0.	1.	1.	1.	1.		
0.	0.																				
250.	*	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.	0.	1.	0.	0.	0.		
0.	0.																				
260.	*	1.	1.	2.	1.	1.	2.	2.	3.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.		
0.	0.																				
270.	*	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.		
0.	0.																				
280.	*	1.	1.	1.	0.	0.	1.	2.	3.	2.	2.	0.	1.	1.	1.	1.	0.	0.	0.		
0.	0.																				
290.	*	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.	0.		
0.	0.																				
300.	*	0.	0.	0.	0.	0.	1.	1.	2.	2.	2.	1.	1.	2.	1.	1.	0.	0.	0.		
0.	0.																				
310.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	1.	2.	2.	2.	2.	1.	0.	0.		
1.	0.																				
320.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	1.	0.	0.		
1.	0.																				
330.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	1.	0.	0.		
1.	1.																				
340.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	1.	0.	0.		
1.	1.																				
350.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	2.	1.	2.	0.	0.		
1.	1.																				
360.	*	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	2.	2.	1.	2.	0.	0.		
1.	1.																				
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----		

MAX	*	2.	3.	3.	3.	3.	2.	2.	3.	3.	3.	2.	2.	3.	2.	2.	2.	2.	3.		
2.	2.																				
DEGR.	*	140	130	130	150	200	260	260	280	140	150	0	110	30	50	50	90	80	90		
100	100																				

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE	*	(ug/m**3)																			
(DEGR)	*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38		
REC39	REC40																				
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----		

0.	*	0.	1.	1.	0.	0.	1.	1.	2.	2.	2.	1.	2.	2.	2.	1.	0.	0.	0.		
0.	0.																				
10.	*	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	1.	0.	0.	0.		
0.	0.																				
20.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	2.	1.	0.	0.	0.		
0.	0.																				
30.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	3.	1.	0.	0.	1.		
1.	0.																				
40.	*	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	2.	2.	3.	4.	2.	0.	0.	2.		
2.	1.																				
50.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	2.	3.	4.	2.	0.	1.	2.		
2.	1.																				
60.	*	0.	0.	0.	0.	0.	2.	1.	1.	1.	1.	1.	2.	3.	4.	3.	1.	1.	2.		
2.	1.																				
70.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	1.	2.		
2.	1.																				
80.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	1.	2.		
2.	1.																				
90.	*	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	1.	1.	2.	2.	2.	2.	2.	2.		
2.	1.																				
100.	*	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	2.	2.	3.		
2.	1.																				
110.	*	0.	0.	1.	1.	1.	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	3.	3.	3.		
2.	2.																				
120.	*	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	3.		
2.	2.																				
130.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.		
3.	2.																				
140.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.		
3.	2.																				
150.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.		
3.	3.																				
160.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	3.		
3.	3.																				
170.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	3.		
3.	3.																				
180.	*	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.		
3.	3.																				
190.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.		
2.	3.																				
200.	*	1.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.		
2.	2.																				
210.	*	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.		
1.	1.																				
220.	*	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.		
1.	1.																				
230.	*	2.	2.	3.	2.	2.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.		
1.	1.																				
240.	*	2.	2.	3.	2.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.		
1.	0.																				
250.	*	2.	2.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.		
1.	0.																				
260.	*	1.	2.	3.	3.	3.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.		
0.	0.																				
270.	*	1.	1.	2.	2.	2.	1.	1.	3.	1.	1.	0.	0.	1.	1.	0.	1.	1.	1.		
0.	0.																				
280.	*	1.	1.	2.	2.	2.	2.	2.	3.	1.	1.	0.	0.	2.	1.	1.	0.	0.	0.		
0.	0.																				
290.	*	1.	1.	1.	1.	1.	2.	2.	4.	2.	1.	0.	0.	3.	2.	1.	0.	0.	0.		
0.	0.																				
300.	*	1.	1.	1.	1.	1.	2.	2.	3.	2.	1.	0.	1.	3.	2.	1.	0.	0.	0.		
0.	0.																				
310.	*	1.	1.	1.	1.	0.	2.	2.	3.	3.	1.	0.	1.	2.	2.	2.	0.	0.	0.		
0.	0.																				
320.	*	1.	1.	1.	1.	0.	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.		
0.	0.																				
330.	*	0.	1.	1.	1.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.		
0.	0.																				
340.	*	0.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.		
0.	0.																				
350.	*	0.	1.	1.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.	2.	1.	0.	0.	0.		
0.	0.																				
360.	*	0.	1.	1.	0.	0.	1.	1.	2.	2.	2.	1.	2.	2.	2.	1.	0.	0.	0.		
0.	0.																				
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----		

MAX	*	2.	2.	3.	3.	3.	2.	2.	4.	3.	2.	2.	2.	3.	4.	3.	3.	3.	3.		
3.	3.																				
DEGR.	*	220	250	250	260	260	300	290	290	330	340	20	30	20	50	70	110	110	110		
160	170																				

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC34.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:13:32

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6036.0	5452.4	*	80.	290.	AG	0.	100.0	1.0	30.0	0.61	4.1
2.	Char/Merr WB	*	6250.4	5435.2	6303.9	5477.6	*	68.	52.	AG	0.	100.0	1.0	30.0	0.59	3.5
3.	Char/Merr NB R	*	6291.7	5369.7	6345.2	5333.4	*	65.	124.	AG	0.	100.0	1.0	10.0	0.33	3.3
4.	Char/Merr NB LTT	*	6280.4	5347.2	6359.4	5291.5	*	97.	125.	AG	0.	100.0	1.0	20.0	0.60	4.9
5.	Char/Merr EB	*	6104.2	5362.2	5973.2	5313.5	*	140.	250.	AG	0.	100.0	1.0	20.0	0.91	7.1
6.	Char/Cam SB L	*	5384.1	4834.2	5402.3	4907.1	*	75.	14.	AG	0.	100.0	1.0	10.0	0.41	3.8
7.	Char/Cam SB TR	*	5360.8	4833.5	5375.6	4881.2	*	50.	17.	AG	0.	100.0	1.0	20.0	0.35	2.5
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	0.	100.0	1.0	20.0	0.41	3.7
9.	Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	0.	100.0	1.0	10.0	0.53	5.0
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.9	4614.7	*	109.	179.	AG	0.	100.0	1.0	20.0	0.73	5.5
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5211.5	4740.8	*	91.	271.	AG	0.	100.0	1.0	30.0	0.51	4.6
12.	Sud/Merr SB L	*	6532.7	5210.3	6492.2	5239.1	*	50.	305.	AG	0.	100.0	1.0	10.0	0.60	2.5
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6484.0	5210.7	*	40.	300.	AG	0.	100.0	1.0	30.0	0.20	2.0
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6677.8	5061.4	*	115.	150.	AG	0.	100.0	1.0	30.0	0.69	5.8
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6452.9	5103.5	*	82.	239.	AG	1.	100.0	1.0	40.0	0.57	4.2
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	0.	100.0	1.0	20.0	0.53	4.1
17.	Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6715.8	5228.7	*	84.	249.	AG	0.	100.0	1.0	30.0	0.43	4.3
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	921.	0.0	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1336.	0.0	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1354.	0.0	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	940.	0.0	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	863.	0.0	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1593.	0.0	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1023.	0.0	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1636.	0.0	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	901.	0.0	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	488.	0.0	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	0.0	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	928.	0.0	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	0.0	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1317.	0.0	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1611.	0.0	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	837.	0.0	1.0	78.0		

DATE : 8/ 7/13
TIME : 17:13:32

		*								
1.	Char/Merr SB	*	100	75	3.0	589	1600	0.07	1	3
2.	Char/Merr WB	*	100	78	3.0	481	1600	0.07	1	3
3.	Char/Merr NB R	*	100	46	3.0	257	1600	0.07	1	3
4.	Char/Merr NB LTT	*	100	68	3.0	520	1600	0.07	1	3
5.	Char/Merr EB	*	100	79	3.0	468	1600	0.07	1	3
6.	Char/Cam SB L	*	100	60	3.0	229	1600	0.07	1	3
7.	Char/Cam SB TR	*	100	72	3.0	254	1600	0.07	1	3
8.	Char/Cam WB LTTR	*	100	62	3.0	435	1600	0.07	1	3
9.	Char/Cam NB L	*	100	60	3.0	299	1600	0.07	1	3
10.	Char/Cam NB TR	*	100	72	3.0	536	1600	0.07	1	3

		*								
11.	Char/Cam EB TTTR	*	100	62	3.0	809	1600	0.07	1	3
12.	Sud/Merr SB L	*	100	84	3.0	106	1600	0.07	1	3
13.	Sud/Merr SB TTT	*	100	50	3.0	435	1600	0.07	1	3
14.	Sud/Merr NB TTTR	*	100	66	3.0	954	1600	0.07	1	3
15.	Sud/Merr EB LTTR	*	100	72	3.0	837	1600	0.07	1	3
16.	Sud/Sur SB LTT	*	100	70	3.0	424	1600	0.07	1	3
17.	Sud/Sur SEB	*	100	80	3.0	37	1600	0.07	1	3
18.	Sud/Sur EB TTR	*	100	50	3.0	928	1600	0.07	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Char/Merr NE1	*	6063.7	5511.0	6.0
2.	Char/Merr NE2	*	6133.9	5484.8	6.0
3.	Char/Merr NE3	*	6204.2	5458.5	6.0
4.	Char/Merr NE4	*	6265.6	5501.5	6.0
5.	Char/Merr NE5	*	6327.1	5544.5	6.0
6.	Char/Merr SE1	*	6443.7	5491.9	6.0
7.	Char/Merr SE2	*	6382.2	5448.9	6.0
8.	Char/Merr SE3	*	6320.8	5405.9	6.0
9.	Char/Merr SE4	*	6380.5	5360.4	6.0
10.	Char/Merr SE5	*	6440.1	5315.0	6.0
11.	Char/Merr SW1	*	6332.0	5249.0	6.0
12.	Char/Merr SW2	*	6272.3	5294.5	6.0
13.	Char/Merr SW3	*	6212.6	5339.9	6.0
14.	Char/Merr SW4	*	6141.6	5315.8	6.0
15.	Char/Merr SW5	*	6070.6	5291.7	6.0
16.	Char/Merr NW1	*	5902.1	5359.1	6.0
17.	Char/Merr NW2	*	5973.1	5383.2	6.0
18.	Char/Merr NW3	*	6044.1	5407.3	6.0
19.	Char/Merr NW4	*	5973.9	5433.5	6.0
20.	Char/Merr NW5	*	5903.6	5459.8	6.0
21.	Char/Cam NE1	*	5490.2	4963.0	6.0
22.	Char/Cam NE2	*	5459.0	4894.8	6.0
23.	Char/Cam NE3	*	5427.8	4826.6	6.0
24.	Char/Cam NE4	*	5500.4	4807.6	6.0
25.	Char/Cam NE5	*	5572.9	4788.7	6.0
26.	Char/Cam SE1	*	5553.9	4667.5	6.0
27.	Char/Cam SE2	*	5481.3	4686.5	6.0
28.	Char/Cam SE3	*	5408.7	4705.4	6.0
29.	Char/Cam SE4	*	5409.4	4630.4	6.0
30.	Char/Cam SE5	*	5410.1	4555.4	6.0
31.	Char/Cam SW1	*	5312.0	4561.9	6.0
32.	Char/Cam SW2	*	5310.7	4636.9	6.0
33.	Char/Cam SW3	*	5310.7	4711.9	6.0

DATE : 8/ 7/13
TIME : 17:13:32

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
34.	Char/Cam SW4	*	5235.6	4712.1	6.0
35.	Char/Cam SW5	*	5160.6	4711.9	6.0
36.	Char/Cam NW1	*	5167.9	4822.4	6.0
37.	Char/Cam NW2	*	5242.9	4822.1	6.0
38.	Char/Cam NW3	*	5317.9	4821.9	6.0
39.	Char/Cam NW4	*	5349.1	4890.1	6.0
40.	Char/Cam NW5	*	5380.3	4958.3	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	* 0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	1.	2.	0.	0.	2.	1.
10.	* 0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	1.	2.	0.	0.	2.	1.
20.	* 0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	2.	2.	0.	0.	2.	

1.	1.																			
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	1.	2.	
1.	1.																			
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	3.	2.	2.	0.	1.	2.	
1.	1.																			
50.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.	
1.	1.																			
60.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.	
1.	1.																			
70.	*	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	2.	3.	
2.	1.																			
80.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.	
2.	2.																			
90.	*	1.	1.	2.	1.	1.	0.	0.	0.	0.	1.	2.	2.	2.	1.	1.	2.	2.	3.	
2.	2.																			
100.	*	1.	1.	2.	1.	1.	0.	0.	0.	0.	1.	2.	2.	2.	1.	1.	2.	2.	2.	
3.	2.																			
110.	*	2.	2.	2.	2.	1.	0.	0.	0.	1.	1.	2.	2.	2.	1.	1.	2.	2.	2.	
2.	2.																			
120.	*	2.	2.	3.	2.	1.	0.	0.	1.	1.	2.	2.	2.	2.	1.	0.	1.	2.	2.	
2.	2.																			
130.	*	2.	3.	3.	2.	1.	0.	1.	2.	2.	3.	1.	1.	1.	0.	0.	1.	1.	2.	
1.	1.																			
140.	*	2.	2.	3.	3.	2.	1.	1.	2.	2.	3.	1.	1.	1.	0.	0.	1.	1.	1.	
1.	1.																			
150.	*	2.	2.	3.	3.	2.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	1.																			
160.	*	2.	2.	2.	3.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
170.	*	2.	1.	2.	3.	2.	1.	1.	2.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
180.	*	2.	1.	2.	3.	2.	1.	1.	2.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
190.	*	2.	2.	2.	2.	2.	1.	1.	2.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
200.	*	2.	2.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
210.	*	2.	2.	2.	2.	2.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	
1.	0.																			
220.	*	1.	2.	2.	2.	2.	1.	1.	1.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.	
1.	0.																			
230.	*	1.	2.	2.	2.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	1.	1.	1.	1.	
1.	0.																			
240.	*	1.	2.	2.	2.	1.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	
0.	0.																			
250.	*	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	
0.	0.																			
260.	*	1.	1.	2.	1.	1.	2.	3.	3.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	
0.	0.																			
270.	*	1.	1.	2.	0.	0.	2.	3.	3.	2.	2.	0.	1.	1.	1.	1.	0.	0.	0.	
0.	0.																			
280.	*	1.	1.	1.	0.	0.	2.	2.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	
0.	0.																			
290.	*	0.	0.	1.	0.	0.	1.	2.	3.	2.	2.	1.	1.	2.	1.	1.	0.	0.	0.	
0.	0.																			
300.	*	0.	0.	0.	0.	0.	1.	1.	2.	2.	2.	1.	1.	2.	2.	1.	0.	0.	1.	
0.	0.																			
310.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	1.	2.	2.	2.	1.	0.	0.	1.	
1.	0.																			
320.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.	
1.	0.																			
330.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.	
1.	1.																			
340.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	2.	2.	0.	0.	1.	
1.	1.																			
350.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	1.	2.	0.	0.	1.	
1.	1.																			
360.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	1.	2.	0.	0.	2.	
1.	1.																			
------	*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
-------																				
MAX	*	2.	3.	3.	3.	2.	2.	3.	3.	3.	3.	2.	2.	3.	2.	2.	2.	2.	3.	
3.	2.																			
DEGR.	*	130	130	130	150	210	250	260	270	280	140	0	10	30	50	10	90	90	80	
100	100																			

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE * (ug/m**3)																				
(DEGR)*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38		
REC39	REC40																			
------*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
-------																				
0.	*	0.	1.	1.	0.	0.	1.	2.	2.	2.	2.	1.	2.	2.	2.	1.	0.	0.	0.	
0.	0.																			
10.	*	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	1.	0.	0.	0.	
0.	0.																			
20.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	2.	1.	0.	0.	0.	
0.	0.																			
30.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	3.	1.	0.	0.	1.	
0.	0.																			
40.	*	0.	0.	0.	0.	0.	2.	1.	2.	1.	1.	2.	2.	3.	3.	2.	0.	0.	1.	
1.	1.																			
50.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	2.	3.	4.	2.	0.	1.	2.	
1.	1.																			
60.	*	0.	0.	0.	0.	0.	2.	1.	2.	1.	1.	1.	2.	3.	4.	3.	0.	1.	2.	
1.	1.																			
70.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	1.	2.	
1.	1.																			
80.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	1.	2.	
1.	1.																			
90.	*	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	1.	2.	2.	2.	2.	2.	2.	2.	
1.	1.																			
100.	*	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	2.	2.	3.	
1.	1.																			
110.	*	0.	0.	1.	1.	1.	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	3.	3.	3.	
2.	1.																			
120.	*	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	3.	2.	3.	
2.	1.																			
130.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	3.	
3.	1.																			
140.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	
3.	1.																			
150.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	
3.	2.																			
160.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	
3.	2.																			
170.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	3.	
3.	2.																			
180.	*	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	1.	0.	0.	1.	2.	2.	
3.	2.																			
190.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	
2.	2.																			
200.	*	1.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	
2.	2.																			
210.	*	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	
1.	1.																			
220.	*	2.	2.	3.	2.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	
1.	1.																			
230.	*	2.	2.	3.	2.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	
1.	1.																			
240.	*	2.	2.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	
1.	0.																			
250.	*	1.	2.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	
0.	0.																			
260.	*	1.	1.	3.	3.	3.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	
0.	0.																			
270.	*	1.	1.	2.	2.	2.	1.	2.	3.	2.	1.	0.	0.	1.	1.	0.	1.	1.	1.	
0.	0.																			
280.	*	1.	1.	2.	2.	2.	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	
0.	0.																			
290.	*	1.	1.	1.	1.	1.	2.	2.	4.	2.	1.	0.	0.	3.	2.	1.	0.	0.	0.	
0.	0.																			
300.	*	1.	1.	1.	1.	1.	2.	2.	3.	3.	1.	0.	1.	3.	2.	1.	0.	0.	0.	
0.	0.																			
310.	*	1.	1.	1.	1.	0.	2.	2.	3.	3.	2.	0.	1.	3.	2.	1.	0.	0.	0.	
0.	0.																			
320.	*	1.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.	
0.	0.																			
330.	*	0.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.	
0.	0.																			
340.	*	0.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.	
0.	0.																			
350.	*	0.	1.	1.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.	2.	1.	0.	0.	0.	
0.	0.																			
360.	*	0.	1.	1.	0.	0.	1.	2.	2.	2.	2.	1.	2.	2.	2.	1.	0.	0.	0.	
0.	0.																			
------*	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----
-------																				
MAX	*	2.	2.	3.	3.	3.	2.	2.	4.	3.	2.	2.	2.	3.	4.	3.	3.	3.	3.	
3.	2.																			
DEGR.	*	220	230	230	250	260	300	290	290	320	340	40	40	40	50	70	110	110	110	
180	190																			

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC34.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:45: 4

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6049.9	5447.4	*	66.	290.	AG	0.	100.0	1.0	30.0	0.52	3.3
2. Char/Merr WB	*	6250.4	5435.2	6333.8	5501.2	*	106.	52.	AG	0.	100.0	1.0	30.0	0.77	5.4
3. Char/Merr NB R	*	6291.7	5369.7	6315.3	5353.7	*	29.	124.	AG	0.	100.0	1.0	10.0	0.14	1.5
4. Char/Merr NB LTT	*	6280.4	5347.2	6430.5	5241.4	*	184.	125.	AG	0.	100.0	1.0	20.0	0.92	9.3
5. Char/Merr EB	*	6104.2	5362.2	6060.5	5345.9	*	47.	250.	AG	0.	100.0	1.0	20.0	0.42	2.4
6. Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.5	*	108.	14.	AG	0.	100.0	1.0	10.0	0.71	5.5
7. Char/Cam SB TR	*	5360.8	4833.5	5398.9	4956.5	*	129.	17.	AG	0.	100.0	1.0	20.0	0.92	6.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	0.	100.0	1.0	20.0	0.27	2.2
9. Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	0.	100.0	1.0	10.0	0.60	4.7
10. Char/Cam NB TR	*	5383.3	4723.8	5384.4	4650.0	*	74.	179.	AG	0.	100.0	1.0	20.0	0.71	3.7
11. Char/Cam EB TTTR	*	5302.7	4739.8	5214.1	4740.7	*	89.	271.	AG	0.	100.0	1.0	30.0	0.54	4.5
12. Sud/Merr SB L	*	6532.7	5210.3	6487.5	5242.5	*	56.	305.	AG	0.	100.0	1.0	10.0	0.72	2.8
13. Sud/Merr SB TTT	*	6518.3	5190.8	6477.9	5214.2	*	47.	300.	AG	0.	100.0	1.0	30.0	0.24	2.4
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6673.5	5068.9	*	106.	150.	AG	0.	100.0	1.0	30.0	0.60	5.4
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6478.2	5118.7	*	53.	239.	AG	1.	100.0	1.0	40.0	0.38	2.7
16. Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	0.	100.0	1.0	20.0	0.34	3.3
17. Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6745.9	5240.5	*	52.	249.	AG	0.	100.0	1.0	30.0	0.43	2.7
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	877.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1122.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1326.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	939.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	849.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1614.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	950.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1709.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	318.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	536.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	373.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1555.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1648.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	529.	0.0	1.0	78.0		

1. Char/Merr SB	*	100	76	3.0	476	1600	0.07	1	3
2. Char/Merr WB	*	100	76	3.0	703	1600	0.07	1	3
3. Char/Merr NB R	*	100	45	3.0	116	1600	0.07	1	3
4. Char/Merr NB LTT	*	100	71	3.0	709	1600	0.07	1	3
5. Char/Merr EB	*	100	79	3.0	217	1600	0.07	1	3
6. Char/Cam SB L	*	90	58	3.0	339	1600	0.07	1	3
7. Char/Cam SB TR	*	90	71	3.0	457	1600	0.07	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	294	1600	0.07	1	3
9. Char/Cam NB L	*	90	58	3.0	289	1600	0.07	1	3
10. Char/Cam NB TR	*	90	71	3.0	354	1600	0.07	1	3

11. Char/Cam EB TTTR	*	90	54	3.0	901	1600	0.07	1	3
12. Sud/Merr SB L	*	100	86	3.0	104	1600	0.07	1	3
13. Sud/Merr SB TTT	*	100	49	3.0	524	1600	0.07	1	3
14. Sud/Merr NB TTTR	*	100	63	3.0	924	1600	0.07	1	3
15. Sud/Merr EB LTTR	*	100	73	3.0	529	1600	0.07	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	455	1600	0.07	1	3
17. Sud/Sur SEB	*	100	70	3.0	26	1600	0.07	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	373	1600	0.07	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Sud/Merr NE1	*	6492.5	5309.9	6.0
2. Sud/Merr NE2	*	6554.8	5268.0	6.0
3. Sud/Merr NE3	*	6616.2	5224.9	6.0
4. Sud/Merr NE4	*	6684.7	5255.3	6.0
5. Sud/Merr NE5	*	6753.3	5285.7	6.0
6. Sud/Merr SE1	*	6792.9	5222.3	6.0
7. Sud/Merr SE2	*	6724.3	5191.9	6.0
8. Sud/Merr SE3	*	6655.7	5161.5	6.0
9. Sud/Merr SE4	*	6695.5	5097.9	6.0
10. Sud/Merr SE5	*	6735.2	5034.3	6.0
11. Sud/Merr SW1	*	6638.6	4981.3	6.0
12. Sud/Merr SW2	*	6598.9	5045.0	6.0
13. Sud/Merr SW3	*	6559.1	5108.6	6.0
14. Sud/Merr SW4	*	6493.4	5072.5	6.0
15. Sud/Merr SW5	*	6427.6	5036.5	6.0
16. Sud/Merr NW1	*	6347.8	5104.5	6.0
17. Sud/Merr NW2	*	6413.5	5140.5	6.0
18. Sud/Merr NW3	*	6479.3	5176.6	6.0
19. Sud/Merr NW4	*	6417.1	5218.5	6.0
20. Sud/Merr NW5	*	6354.9	5260.4	6.0
21. Sud/Sur NE1	*	6755.9	5445.7	6.0
22. Sud/Sur NE2	*	6801.0	5385.7	6.0
23. Sud/Sur NE3	*	6846.0	5325.7	6.0
24. Sud/Sur NE4	*	6908.8	5366.8	6.0
25. Sud/Sur NE5	*	6971.5	5407.9	6.0
26. Sud/Sur SE1	*	7002.4	5368.4	6.0
27. Sud/Sur SE2	*	6939.7	5327.3	6.0
28. Sud/Sur SE3	*	6876.9	5286.2	6.0
29. Sud/Sur SE4	*	6931.7	5235.0	6.0
30. Sud/Sur SE5	*	6986.5	5183.8	6.0
31. Sud/Sur SW1	*	6932.3	5133.1	6.0
32. Sud/Sur SE2	*	6877.5	5184.3	6.0
33. Sud/Sur SE3	*	6822.7	5235.5	6.0

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Sud/Sur SE4	*	6754.2	5205.1	6.0
35. Sud/Sur SE5	*	6685.6	5174.8	6.0
36. Sud/Sur NW1	*	6645.5	5237.9	6.0
37. Sud/Sur NW2	*	6714.1	5268.3	6.0
38. Sud/Sur NW3	*	6782.7	5298.7	6.0
39. Sud/Sur NW4	*	6709.5	5315.4	6.0
40. Sud/Sur NW5	*	6636.4	5332.0	6.0
41. Sud/Sur N1	*	6642.4	5493.7	6.0
42. Sud/Sur N2	*	6687.4	5433.7	6.0
43. Sud/Sur N3	*	6732.4	5373.8	6.0
44. Sud/Sur N4	*	6659.3	5390.4	6.0
45. Sud/Sur N5	*	6586.2	5407.1	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION ANGLE * (ug/m**3) (DEGR)*	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

```
   0.  *    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.    2.    2.    2.    3.    1.    1.    1.    2.
2.    2.
  10.  *    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.    2.    2.    2.    3.    1.    1.    1.    2.
2.    2.
  20.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    2.    2.    2.    2.    2.    1.    1.    2.
2.    2.
  30.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    2.    2.    2.    2.    2.    1.    1.    2.
2.    2.
  40.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    2.    2.    2.    2.    2.    1.    1.    2.
1.    2.
  50.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    2.    2.    2.    2.    1.    1.    2.
1.    2.
  60.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    2.    2.    1.    1.    1.    2.    2.
1.    2.
  70.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    2.    2.    1.    1.    2.    2.    2.
2.    2.
  80.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    2.    2.    1.    1.    2.    2.    3.
2.    2.
  90.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    1.    2.    1.    1.    1.    2.    2.
2.    3.
 100.  *    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    1.    1.    2.    1.    0.    1.    2.    2.
2.    3.
 110.  *    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    2.    2.    2.    1.    0.    1.    2.    2.
2.    3.
 120.  *    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    2.    2.    2.    1.    0.    1.    1.    2.
2.    3.
 130.  *    1.    1.    0.    0.    1.    0.    0.    0.    0.    0.    1.    2.    2.    0.    0.    0.    1.    2.
2.    2.
 140.  *    2.    2.    1.    0.    1.    0.    0.    1.    0.    0.    1.    1.    1.    0.    0.    0.    1.    2.
1.    1.
 150.  *    3.    2.    2.    0.    1.    0.    0.    1.    1.    1.    0.    1.    1.    0.    0.    0.    0.    2.
1.    1.
 160.  *    2.    2.    2.    1.    1.    0.    0.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    2.
0.    0.
 170.  *    2.    2.    3.    1.    1.    0.    0.    2.    2.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 180.  *    2.    2.    2.    1.    2.    0.    1.    3.    2.    2.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 190.  *    2.    2.    2.    2.    2.    0.    1.    3.    2.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 200.  *    2.    2.    2.    2.    2.    0.    1.    2.    2.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 210.  *    2.    2.    2.    2.    1.    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 220.  *    2.    2.    2.    2.    1.    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 230.  *    2.    2.    2.    2.    1.    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 240.  *    2.    2.    2.    2.    1.    1.    2.    3.    2.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 250.  *    2.    2.    2.    2.    1.    2.    2.    3.    2.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 260.  *    2.    2.    2.    1.    1.    2.    2.    3.    3.    2.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 270.  *    2.    2.    2.    1.    1.    2.    2.    3.    3.    1.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 280.  *    2.    2.    2.    1.    1.    2.    2.    3.    3.    2.    0.    0.    1.    1.    0.    0.    0.    0.
0.    1.
 290.  *    2.    2.    2.    1.    1.    2.    2.    3.    4.    3.    0.    1.    2.    1.    1.    0.    0.    1.
1.    1.
 300.  *    1.    2.    2.    1.    0.    2.    1.    3.    4.    3.    1.    1.    2.    1.    1.    0.    0.    2.
2.    2.
 310.  *    1.    1.    1.    0.    0.    2.    1.    2.    3.    3.    1.    2.    3.    1.    1.    0.    1.    2.
2.    2.
 320.  *    0.    0.    0.    0.    0.    2.    0.    2.    2.    2.    2.    2.    3.    2.    1.    1.    1.    2.
3.    3.
 330.  *    0.    0.    0.    0.    0.    2.    0.    1.    1.    1.    2.    2.    3.    2.    1.    1.    1.    2.
3.    3.
 340.  *    0.    0.    0.    0.    0.    2.    0.    1.    1.    0.    2.    2.    2.    2.    1.    1.    1.    2.
3.    3.
 350.  *    0.    0.    0.    0.    0.    2.    0.    0.    0.    0.    2.    2.    2.    2.    1.    1.    1.    2.
2.    3.
 360.  *    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.    2.    2.    2.    3.    1.    1.    1.    2.
2.    2.
------*-------------------------------------------------------------------------------------------------------------
-------
 MAX   *    3.    2.    3.    2.    2.    2.    2.    3.    4.    3.    2.    2.    3.    3.    2.    2.    2.    3.
3.    3.
 DEGR. *  150   160   170   240   180   290   260   290   300   310   350   330   320     0    40    70    90    80
330   100
```


JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (ug/m**3)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38
REC39 REC40

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------*-------------------------------------------------------------------------------------------------------------
-------
   0.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    2.    0.    0.    0.    1.
0.    0.
  10.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    2.    0.    0.    0.    0.
0.    0.
  20.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
  30.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.    0.    0.    0.
0.    0.
  40.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
  50.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.
  60.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.
  70.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.
0.    0.
  80.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
0.    0.
  90.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
0.    0.
 100.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    0.
0.    0.
 110.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    0.
0.    0.
 120.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    1.    1.
1.    0.
 130.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.
1.    0.
 140.  *    1.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.
1.    0.
 150.  *    1.    1.    1.    0.    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    1.    0.    1.
1.    0.
 160.  *    1.    1.    1.    0.    0.    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    1.    0.
1.    1.
 170.  *    1.    1.    1.    0.    0.    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 180.  *    2.    1.    1.    1.    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 190.  *    2.    1.    1.    1.    0.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    2.    2.    1.
1.    1.
 200.  *    1.    1.    1.    1.    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    2.    2.    1.
1.    1.
 210.  *    2.    1.    1.    1.    1.    0.    0.    1.    1.    1.    0.    0.    0.    1.    1.    2.    2.    1.
1.    1.
 220.  *    1.    1.    1.    1.    1.    0.    0.    1.    1.    1.    1.    0.    0.    0.    1.    1.    2.    2.
1.    1.
 230.  *    1.    1.    2.    1.    1.    1.    1.    1.    1.    1.    1.    0.    0.    1.    1.    1.    2.    2.
1.    1.
 240.  *    1.    1.    2.    1.    1.    1.    2.    2.    1.    1.    0.    0.    1.    1.    1.    2.    2.    1.
1.    1.
 250.  *    1.    2.    1.    1.    1.    1.    2.    2.    1.    1.    1.    1.    2.    2.    2.    2.    1.    1.
1.    1.
 260.  *    1.    2.    1.    1.    1.    1.    1.    2.    2.    1.    1.    1.    2.    2.    2.    2.    1.    1.
1.    1.
 270.  *    1.    2.    1.    1.    1.    1.    1.    1.    2.    2.    1.    1.    2.    2.    2.    2.    1.    1.
1.    1.
 280.  *    1.    2.    1.    1.    0.    1.    1.    1.    2.    2.    1.    1.    2.    2.    2.    2.    1.    1.
1.    1.
 290.  *    1.    1.    1.    0.    0.    0.    1.    1.    1.    1.    1.    1.    2.    2.    2.    2.    1.    0.
0.    1.
 300.  *    1.    1.    1.    0.    0.    0.    1.    1.    1.    1.    1.    1.    2.    1.    2.    1.    0.    0.
0.    0.
 310.  *    1.    1.    1.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.    1.    0.    0.
0.    0.
 320.  *    0.    0.    1.    0.    0.    0.    0.    1.    1.    0.    1.    1.    1.    1.    1.    1.    0.    0.
0.    0.
 330.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.    0.
0.    1.
 340.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    0.    0.
0.    1.
 350.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    0.    0.
0.    1.
 360.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    2.    0.    0.    0.
0.    1.
------*-------------------------------------------------------------------------------------------------------------
-------
 MAX   *    2.    2.    2.    1.    1.    1.    2.    2.    2.    2.    1.    1.    2.    2.    2.    2.    1.    2.
1.    1.
 DEGR. *  190   270   230   230   230   240   240   250   270   270   280   280   280   260   290   230   100   200
```

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	1.	0.	0.
10.	0.	0.	1.	0.	0.
20.	0.	0.	1.	0.	0.
30.	0.	0.	1.	0.	0.
40.	0.	0.	1.	0.	0.
50.	0.	0.	1.	0.	0.
60.	0.	0.	1.	0.	0.
70.	0.	0.	1.	0.	0.
80.	0.	0.	1.	0.	0.
90.	0.	0.	1.	0.	0.
100.	0.	1.	1.	0.	0.
110.	0.	1.	1.	0.	0.
120.	1.	1.	1.	0.	0.
130.	1.	1.	1.	0.	0.
140.	1.	1.	1.	0.	0.
150.	1.	0.	1.	0.	0.
160.	0.	0.	1.	0.	1.
170.	1.	1.	1.	1.	1.
180.	1.	1.	1.	1.	1.
190.	1.	1.	1.	1.	1.
200.	1.	1.	1.	1.	1.
210.	1.	1.	1.	1.	1.
220.	1.	1.	1.	1.	1.
230.	1.	1.	1.	1.	1.
240.	1.	1.	1.	1.	1.
250.	1.	1.	1.	1.	1.
260.	1.	1.	1.	1.	1.
270.	1.	1.	1.	1.	1.
280.	1.	1.	1.	1.	1.
290.	0.	0.	0.	0.	1.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	1.	0.	0.
360.	0.	0.	1.	0.	0.
MAX	1.	1.	1.	1.	1.
DEGR.	240	120	210	200	180

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC9 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:12: 4

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6036.0	5452.4	*	80.	290.	AG	0.	100.0	1.0	30.0	0.61	4.1
2. Char/Merr WB	*	6250.4	5435.2	6303.9	5477.6	*	68.	52.	AG	0.	100.0	1.0	30.0	0.59	3.5
3. Char/Merr NB R	*	6291.7	5369.7	6345.2	5333.4	*	65.	124.	AG	0.	100.0	1.0	10.0	0.33	3.3
4. Char/Merr NB LTT	*	6280.4	5347.2	6359.4	5291.5	*	97.	125.	AG	0.	100.0	1.0	20.0	0.60	4.9
5. Char/Merr EB	*	6104.2	5362.2	5973.2	5313.5	*	140.	250.	AG	0.	100.0	1.0	20.0	0.91	7.1
6. Char/Cam SB L	*	5384.1	4834.2	5402.3	4907.1	*	75.	14.	AG	0.	100.0	1.0	10.0	0.41	3.8
7. Char/Cam SB TR	*	5360.8	4833.5	5375.6	4881.2	*	50.	17.	AG	0.	100.0	1.0	20.0	0.35	2.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	0.	100.0	1.0	20.0	0.41	3.7
9. Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	0.	100.0	1.0	10.0	0.53	5.0
10. Char/Cam NB TR	*	5383.3	4723.8	5384.9	4614.7	*	109.	179.	AG	0.	100.0	1.0	20.0	0.73	5.5
11. Char/Cam EB TTTR	*	5302.7	4739.8	5211.5	4740.8	*	91.	271.	AG	0.	100.0	1.0	30.0	0.51	4.6
12. Sud/Merr SB L	*	6532.7	5210.3	6492.2	5239.1	*	50.	305.	AG	0.	100.0	1.0	10.0	0.60	2.5
13. Sud/Merr SB TTT	*	6518.3	5190.8	6484.0	5210.7	*	40.	300.	AG	0.	100.0	1.0	30.0	0.20	2.0
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6677.8	5061.4	*	115.	150.	AG	0.	100.0	1.0	30.0	0.69	5.8
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6452.9	5103.5	*	82.	239.	AG	1.	100.0	1.0	40.0	0.57	4.2
16. Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	0.	100.0	1.0	20.0	0.53	4.1
17. Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6715.8	5228.7	*	84.	249.	AG	0.	100.0	1.0	30.0	0.43	4.3
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	921.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1336.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1354.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	940.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	863.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1593.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1023.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1636.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	901.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	488.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	928.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1317.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1611.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	837.	0.0	1.0	78.0		

1. Char/Merr SB	*	100	75	3.0	589	1600	0.07	1	3
2. Char/Merr WB	*	100	78	3.0	481	1600	0.07	1	3
3. Char/Merr NB R	*	100	46	3.0	257	1600	0.07	1	3
4. Char/Merr NB LTT	*	100	68	3.0	520	1600	0.07	1	3
5. Char/Merr EB	*	100	79	3.0	468	1600	0.07	1	3
6. Char/Cam SB L	*	100	60	3.0	229	1600	0.07	1	3
7. Char/Cam SB TR	*	100	72	3.0	254	1600	0.07	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	435	1600	0.07	1	3
9. Char/Cam NB L	*	100	60	3.0	299	1600	0.07	1	3
10. Char/Cam NB TR	*	100	72	3.0	536	1600	0.07	1	3

11. Char/Cam EB TTTR	*	100	62	3.0	809	1600	0.07	1	3
12. Sud/Merr SB L	*	100	84	3.0	106	1600	0.07	1	3
13. Sud/Merr SB TTT	*	100	50	3.0	435	1600	0.07	1	3
14. Sud/Merr NB TTTR	*	100	66	3.0	954	1600	0.07	1	3
15. Sud/Merr EB LTTR	*	100	72	3.0	837	1600	0.07	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	424	1600	0.07	1	3
17. Sud/Sur SEB	*	100	80	3.0	37	1600	0.07	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	928	1600	0.07	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Sud/Merr NE1	*	6492.5	5309.9	6.0
2. Sud/Merr NE2	*	6554.8	5268.0	6.0
3. Sud/Merr NE3	*	6616.2	5224.9	6.0
4. Sud/Merr NE4	*	6684.7	5255.3	6.0
5. Sud/Merr NE5	*	6753.3	5285.7	6.0
6. Sud/Merr SE1	*	6792.9	5222.3	6.0
7. Sud/Merr SE2	*	6724.3	5191.9	6.0
8. Sud/Merr SE3	*	6655.7	5161.5	6.0
9. Sud/Merr SE4	*	6695.5	5097.9	6.0
10. Sud/Merr SE5	*	6735.2	5034.3	6.0
11. Sud/Merr SW1	*	6638.6	4981.3	6.0
12. Sud/Merr SW2	*	6598.9	5045.0	6.0
13. Sud/Merr SW3	*	6559.1	5108.6	6.0
14. Sud/Merr SW4	*	6493.4	5072.5	6.0
15. Sud/Merr SW5	*	6427.6	5036.5	6.0
16. Sud/Merr NW1	*	6347.8	5104.5	6.0
17. Sud/Merr NW2	*	6413.5	5140.5	6.0
18. Sud/Merr NW3	*	6479.3	5176.6	6.0
19. Sud/Merr NW4	*	6417.1	5218.5	6.0
20. Sud/Merr NW5	*	6354.9	5260.4	6.0
21. Sud/Sur NE1	*	6755.9	5445.7	6.0
22. Sud/Sur NE2	*	6801.0	5385.7	6.0
23. Sud/Sur NE3	*	6846.0	5325.7	6.0
24. Sud/Sur NE4	*	6908.8	5366.8	6.0
25. Sud/Sur NE5	*	6971.5	5407.9	6.0
26. Sud/Sur SE1	*	7002.4	5368.4	6.0
27. Sud/Sur SE2	*	6939.7	5327.3	6.0
28. Sud/Sur SE3	*	6876.9	5286.2	6.0
29. Sud/Sur SE4	*	6931.7	5235.0	6.0
30. Sud/Sur SE5	*	6986.5	5183.8	6.0
31. Sud/Sur SW1	*	6932.3	5133.1	6.0
32. Sud/Sur SE2	*	6877.5	5184.3	6.0
33. Sud/Sur SE3	*	6822.7	5235.5	6.0

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Sud/Sur SE4	*	6754.2	5205.1	6.0
35. Sud/Sur SE5	*	6685.6	5174.8	6.0
36. Sud/Sur NW1	*	6645.5	5237.9	6.0
37. Sud/Sur NW2	*	6714.1	5268.3	6.0
38. Sud/Sur NW3	*	6782.7	5298.7	6.0
39. Sud/Sur NW4	*	6709.5	5315.4	6.0
40. Sud/Sur NW5	*	6636.4	5332.0	6.0
41. Sud/Sur N1	*	6642.4	5493.7	6.0
42. Sud/Sur N2	*	6687.4	5433.7	6.0
43. Sud/Sur N3	*	6732.4	5373.8	6.0
44. Sud/Sur N4	*	6659.3	5390.4	6.0
45. Sud/Sur N5	*	6586.2	5407.1	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

```
   0.  *    0.    0.    0.    0.    1.    1.    2.    1.    1.    1.    2.    2.    2.    3.    2.    1.    1.    2.
2.    2.
  10.  *    0.    0.    0.    0.    1.    1.    2.    1.    1.    1.    2.    2.    2.    3.    2.    1.    1.    2.
1.    2.
  20.  *    0.    0.    0.    0.    0.    1.    2.    1.    1.    0.    2.    2.    2.    2.    2.    1.    1.    2.
1.    2.
  30.  *    0.    0.    0.    0.    0.    1.    2.    1.    1.    0.    2.    2.    2.    2.    2.    0.    1.    2.
1.    1.
  40.  *    0.    0.    0.    0.    0.    1.    2.    2.    1.    0.    2.    2.    3.    2.    2.    0.    1.    2.
1.    1.
  50.  *    0.    0.    0.    0.    0.    1.    2.    2.    0.    0.    1.    2.    3.    2.    2.    1.    1.    2.
1.    1.
  60.  *    0.    0.    1.    0.    0.    1.    1.    1.    0.    0.    1.    2.    3.    2.    2.    1.    2.    2.
1.    1.
  70.  *    0.    0.    1.    1.    1.    0.    1.    1.    0.    0.    1.    2.    2.    2.    1.    2.    2.    2.
1.    2.
  80.  *    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    1.    2.    2.    1.    1.    2.    3.    3.
2.    2.
  90.  *    0.    1.    2.    2.    1.    0.    0.    0.    0.    0.    1.    1.    2.    1.    1.    2.    3.    3.
2.    2.
 100.  *    1.    1.    1.    2.    1.    0.    0.    0.    0.    0.    1.    2.    2.    1.    0.    2.    3.    3.
2.    3.
 110.  *    1.    1.    1.    2.    1.    0.    0.    0.    0.    0.    1.    2.    2.    1.    0.    1.    2.    3.
2.    2.
 120.  *    1.    1.    1.    2.    2.    0.    0.    0.    0.    0.    1.    2.    2.    1.    0.    1.    2.    3.
3.    2.
 130.  *    2.    1.    1.    1.    1.    0.    0.    0.    0.    0.    1.    2.    2.    0.    0.    1.    2.    3.
2.    2.
 140.  *    2.    2.    2.    1.    2.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    2.
2.    2.
 150.  *    2.    2.    2.    1.    2.    0.    0.    1.    1.    1.    0.    1.    1.    0.    0.    1.    1.    2.
1.    1.
 160.  *    2.    3.    3.    1.    2.    0.    0.    2.    1.    1.    0.    0.    0.    0.    0.    0.    1.    2.
1.    1.
 170.  *    2.    2.    3.    2.    2.    0.    0.    2.    2.    1.    0.    0.    0.    0.    0.    0.    1.    2.
1.    0.
 180.  *    2.    2.    3.    2.    2.    0.    1.    3.    2.    1.    0.    0.    0.    0.    0.    0.    1.    2.
0.    0.
 190.  *    2.    2.    2.    2.    2.    0.    1.    3.    2.    1.    0.    0.    0.    0.    0.    0.    1.    2.
0.    0.
 200.  *    2.    2.    2.    2.    2.    0.    1.    2.    2.    1.    0.    0.    0.    0.    0.    0.    1.    2.
0.    0.
 210.  *    1.    2.    2.    2.    2.    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    0.    1.    1.
0.    0.
 220.  *    1.    2.    3.    2.    2.    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    0.    1.    1.
0.    0.
 230.  *    1.    2.    3.    2.    2.    1.    1.    3.    2.    1.    0.    0.    0.    0.    0.    0.    1.    1.
0.    0.
 240.  *    1.    1.    3.    2.    2.    2.    2.    3.    2.    1.    0.    0.    1.    0.    0.    0.    1.    1.
0.    0.
 250.  *    2.    1.    2.    2.    1.    2.    2.    4.    2.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 260.  *    1.    1.    2.    1.    1.    2.    3.    4.    3.    2.    0.    0.    2.    1.    1.    0.    0.    0.
0.    0.
 270.  *    2.    2.    2.    1.    1.    2.    2.    4.    3.    2.    0.    0.    2.    1.    1.    0.    0.    0.
0.    0.
 280.  *    2.    2.    2.    1.    1.    2.    2.    3.    3.    2.    0.    1.    2.    1.    1.    0.    0.    0.
1.    1.
 290.  *    2.    2.    2.    1.    1.    2.    2.    4.    4.    3.    1.    1.    2.    1.    1.    0.    0.    1.
1.    1.
 300.  *    1.    1.    2.    1.    0.    2.    2.    4.    4.    3.    1.    1.    3.    2.    1.    0.    0.    2.
2.    2.
 310.  *    1.    1.    1.    0.    0.    2.    1.    2.    3.    3.    1.    2.    3.    2.    1.    1.    1.    2.
2.    2.
 320.  *    0.    0.    0.    0.    0.    2.    1.    2.    2.    2.    2.    2.    3.    2.    1.    1.    1.    2.
2.    3.
 330.  *    0.    0.    0.    0.    0.    2.    1.    1.    1.    2.    2.    2.    3.    3.    1.    1.    1.    2.
2.    3.
 340.  *    0.    0.    0.    0.    0.    2.    1.    1.    1.    1.    2.    2.    3.    3.    2.    1.    1.    2.
2.    3.
 350.  *    0.    0.    0.    0.    1.    2.    1.    1.    1.    1.    2.    2.    2.    3.    1.    1.    1.    2.
2.    2.
 360.  *    0.    0.    0.    0.    1.    1.    2.    1.    1.    1.    2.    2.    2.    3.    2.    1.    1.    2.
2.    2.
------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    2.    3.    3.    2.    2.    2.    3.    4.    4.    3.    2.    2.    3.    3.    2.    2.    3.    3.
3.    3.
 DEGR. *  150   160   170   230   210   280   260   260   300   300     0    20   320     0    40    80    80    80
120   330
```


JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 WIND  * CONCENTRATION
 ANGLE *     (ug/m**3)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38
REC39 REC40

------*-------------------------------------------------------------------------------------------------------------
-------
   0.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
  10.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.    1.    1.    2.    1.    0.    0.    0.
0.    0.
  20.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.    1.    1.    2.    1.    0.    0.    0.
0.    0.
  30.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.    0.    1.    2.    2.    0.    0.    0.
0.    0.
  40.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    2.    0.    0.    0.
0.    0.
  50.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    2.    0.    0.    0.
0.    0.
  60.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.
0.    0.
  70.  *    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
0.    0.
  80.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    2.    1.    1.
1.    0.
  90.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    2.    2.    1.
1.    0.
 100.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    2.    2.    1.
0.    1.
 110.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    1.    2.    1.
1.    1.
 120.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 130.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 140.  *    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 150.  *    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 160.  *    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 170.  *    2.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 180.  *    2.    1.    1.    1.    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    2.    2.    2.
1.    1.
 190.  *    2.    1.    1.    1.    1.    0.    0.    1.    0.    0.    0.    0.    0.    0.    1.    2.    2.    2.
1.    1.
 200.  *    2.    2.    2.    2.    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    2.    2.    2.
1.    1.
 210.  *    2.    2.    2.    2.    1.    0.    0.    1.    1.    1.    0.    0.    0.    1.    1.    2.    2.    2.
1.    1.
 220.  *    2.    2.    2.    2.    2.    1.    1.    1.    1.    1.    0.    0.    0.    1.    1.    2.    2.    2.
1.    1.
 230.  *    2.    2.    2.    2.    2.    1.    1.    2.    1.    1.    0.    0.    1.    1.    2.    3.    2.    2.
1.    1.
 240.  *    1.    2.    2.    2.    2.    2.    2.    2.    1.    1.    0.    1.    1.    2.    2.    2.    2.    2.
1.    1.
 250.  *    1.    2.    2.    1.    1.    2.    2.    2.    2.    1.    1.    1.    2.    2.    3.    2.    2.    2.
1.    1.
 260.  *    1.    2.    1.    1.    1.    1.    2.    2.    2.    1.    1.    1.    2.    2.    3.    1.    1.    1.
1.    1.
 270.  *    1.    2.    1.    1.    1.    1.    2.    2.    2.    2.    1.    1.    2.    2.    3.    1.    1.    1.
1.    1.
 280.  *    1.    2.    1.    1.    1.    1.    2.    2.    2.    2.    1.    2.    2.    2.    3.    1.    1.    1.
1.    1.
 290.  *    1.    2.    1.    1.    0.    1.    2.    2.    1.    1.    1.    1.    2.    2.    3.    1.    1.    0.
1.    1.
 300.  *    1.    1.    1.    0.    0.    0.    1.    2.    1.    1.    1.    1.    2.    2.    2.    1.    1.    0.
0.    0.
 310.  *    1.    1.    1.    0.    0.    0.    1.    2.    1.    1.    1.    1.    1.    2.    2.    1.    0.    0.
0.    0.
 320.  *    0.    1.    1.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
 330.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
 340.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
 350.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
 360.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
0.    0.
------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    2.    2.    2.    2.    2.    2.    2.    3.    2.    2.    1.    2.    2.    2.    3.    3.    2.    2.
1.    1.
 DEGR. *  200   220   230   210   220   240   250   250   270   270   280   280   260   260   260   230   230   210
```

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	1.	0.	0.
10.	0.	0.	1.	0.	0.
20.	0.	0.	1.	0.	0.
30.	0.	0.	1.	0.	0.
40.	0.	0.	1.	0.	0.
50.	0.	0.	1.	0.	0.
60.	0.	0.	1.	0.	0.
70.	0.	0.	1.	0.	0.
80.	0.	1.	1.	0.	0.
90.	0.	1.	1.	1.	0.
100.	0.	1.	1.	1.	0.
110.	1.	1.	1.	1.	0.
120.	1.	1.	1.	0.	0.
130.	1.	1.	1.	1.	0.
140.	1.	1.	1.	0.	0.
150.	1.	1.	1.	1.	1.
160.	0.	0.	1.	1.	1.
170.	1.	1.	1.	1.	1.
180.	1.	1.	1.	1.	1.
190.	1.	1.	1.	1.	1.
200.	1.	1.	1.	1.	1.
210.	1.	1.	1.	1.	1.
220.	0.	1.	1.	1.	1.
230.	0.	1.	1.	1.	1.
240.	1.	0.	1.	1.	1.
250.	1.	1.	1.	1.	1.
260.	1.	1.	1.	1.	1.
270.	1.	1.	1.	1.	1.
280.	1.	1.	1.	1.	1.
290.	0.	0.	0.	1.	1.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	1.	0.	0.
350.	0.	0.	1.	0.	0.
360.	0.	0.	1.	0.	0.
MAX	1.	1.	1.	1.	1.
DEGR.	260	110	180	200	270

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC9 .

2028 Build
Microscale Output Files
(Particulate Matter 10 (PM10))

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16:10:26

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	0.	100.0	1.0	10.0	0.71 7.8
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5105.0	6035.3	*	120.	325.	AG	0.	100.0	1.0	20.0	0.55 6.1
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	0.	100.0	1.0	20.0	0.92 9.6
4.	Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	0.	100.0	1.0	10.0	0.58 6.4
5.	Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	0.	100.0	1.0	10.0	0.64 4.1
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5366.6	5747.7	*	55.	109.	AG	0.	100.0	1.0	20.0	0.44 2.8
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	0.	100.0	1.0	20.0	0.68 4.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	0.	100.0	1.0	10.0	0.93 8.1
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6144.6	7708.0	*	931.	334.	AG	0.	100.0	1.0	40.0	1.09 47.3
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	0.	100.0	1.0	20.0	0.58 5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	0.	100.0	1.0	10.0	0.53 6.6
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6667.3	5333.6	*	1420.	177.	AG	0.	100.0	1.0	20.0	1.41 72.1
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	0.	100.0	1.0	30.0	0.47 4.6
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.6	6363.6	*	140.	358.	AG	0.	100.0	1.0	20.0	0.80 7.1
15.	Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	0.	100.0	1.0	10.0	1.23 59.7
16.	Tha/Val NB TR	*	6645.6	6138.6	6647.7	6016.6	*	122.	179.	AG	0.	100.0	1.0	10.0	0.70 6.2
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6099.5	*	136.	0.	AG	0.	100.0	1.0	30.0	0.69 6.9
18.	Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	0.	100.0	1.0	30.0	0.18 1.8
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.2	5885.7	*	146.	358.	AG	0.	100.0	1.0	40.0	0.75 7.4
20.	Char/93 WB LTT	*	6702.8	5647.8	6766.7	5567.9	*	102.	141.	AG	0.	100.0	1.0	20.0	0.65 5.2
21.	Char/93 EB TTR	*	6560.8	5622.5	6514.2	5588.4	*	58.	234.	AG	0.	100.0	1.0	30.0	0.37 2.9
22.	North/Congress SB LT	*	6876.6	4408.9	6575.8	5898.4	*	1520.	349.	AG	0.	100.0	1.0	30.0	2.65 77.2
23.	North/Con WB LLTR	*	6920.6	4378.3	7916.6	4730.8	*	1057.	71.	AG	0.	100.0	1.0	20.0	1.13 53.7
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6921.1	4287.3	*	47.	172.	AG	0.	100.0	1.0	30.0	0.34 2.4
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	0.	100.0	1.0	10.0	0.03 0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1464.	0.0	1.0	90.0	
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1588.	0.0	1.0	78.0	
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	967.	0.0	1.0	78.0	
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	0.0	1.0	78.0	
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3453.	0.0	1.0	90.0	
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	0.0	1.0	66.0	
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2405.	0.0	1.0	90.0	
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	0.0	1.0	78.0	
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2431.	0.0	1.0	90.0	
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	0.0	1.0	38.0	
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2871.	0.0	1.0	90.0	
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	0.0	1.0	54.0	
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2351.	0.0	1.0	66.0	
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	0.0	1.0	48.0	
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	542.	0.0	1.0	42.0	
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	0.0	1.0	48.0	
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	459.	0.0	1.0	54.0	
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	729.	0.0	1.0	54.0	

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	0.0	1.0	42.0	

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
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LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1629.	0.0	1.0	98.0	
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1333.	0.0	1.0	66.0	
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1545.	0.0	1.0	98.0	
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	0.0	1.0	54.0	

JOB: Government Center Garage RUN: Build

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1.	Stan/Lom SB L	*	120	75	3.0	376	1600	0.07	1	3
2.	Stan/Lom SB TRR	*	120	75	3.0	585	1600	0.07	1	3
3.	Stan/Lom WB LTT	*	120	91	3.0	588	1600	0.07	1	3
4.	Stan/Lom WB R	*	120	75	3.0	308	1600	0.07	1	3
5.	Stan/Lom NB L	*	120	97	3.0	152	1600	0.07	1	3
6.	Stan/Lom NB TRR	*	120	97	3.0	208	1600	0.07	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	324	1600	0.07	1	3
8.	Stan/Lom EB R	*	120	97	3.0	222	1600	0.07	1	3
9.	Caus/Wash SB LTTRR	*	150	94	3.0	2380	1600	0.07	1	3
10.	Caus/Wash WB LLTT	*	150	119	3.0	321	1600	0.07	1	3
11.	Caus/Wash WB R	*	150	104	3.0	230	1600	0.07	1	3
12.	Caus/Wash NB TTR	*	150	120	3.0	748	1600	0.07	1	3
13.	Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	0.07	1	3
14.	Tha/Val SB LTTR	*	104	30	3.0	1705	1600	0.07	1	3
15.	Tha/Val NB L	*	104	74	3.0	472	1600	0.07	1	3
16.	Tha/Val NB TR	*	104	30	3.0	744	1600	0.07	1	3
17.	Bev/Was SB TTT	*	100	45	3.0	1655	1600	0.07	1	3
18.	Bev/Was EB RRR	*	100	55	3.0	356	1600	0.07	1	3
19.	Char/93 SB LLTTRR	*	100	53	3.0	2013	1600	0.07	1	3
20.	Char/93 WB LTT	*	100	69	3.0	542	1600	0.07	1	3
21.	Char/93 EB TTR	*	100	69	3.0	459	1600	0.07	1	3
22.	North/Congress SB LT	*	100	90	3.0	636	1600	0.07	1	3
23.	North/Con WB LLTR	*	100	60	3.0	1267	1600	0.07	1	3
24.	Nor/Con NB LTTTR	*	100	74	3.0	345	1600	0.07	1	3
25.	Nor/Con EB LTR	*	100	60	3.0	17	1600	0.07	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8.	Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0	*
21.	Caus/Wash NE1	*	6548.3	7035.9	6.0	*
22.	Caus/Wash NE2	*	6581.4	6968.6	6.0	*
23.	Caus/Wash NE3	*	6614.5	6901.3	6.0	*
24.	Caus/Wash NE4	*	6669.8	6952.0	6.0	*
25.	Caus/Wash NE5	*	6725.0	7002.7	6.0	*
26.	Caus/Wash SE1	*	6753.6	6912.2	6.0	*

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16:10:26

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Caus/Wash SE2	6698.9	6862.0	6.0
28. Caus/Wash SE3	6643.1	6810.8	6.0
29. Caus/Wash SE4	6646.8	6736.4	6.0
30. Caus/Wash SE5	6650.0	6661.0	6.0
31. Caus/Wash SW1	6544.0	6561.0	6.0
32. Caus/Wash SW2	6540.9	6636.0	6.0
33. Caus/Wash SW3	6537.8	6710.9	6.0
34. Caus/Wash SW4	6476.8	6667.2	6.0
35. Caus/Wash SW5	6415.9	6623.4	6.0
36. Caus/Wash NW1	6407.4	6738.0	6.0
37. Caus/Wash NW2	6468.3	6781.7	6.0
38. Caus/Wash NW3	6529.3	6825.4	6.0
39. Caus/Wash NW4	6496.2	6892.7	6.0
40. Caus/Wash NW5	6463.1	6960.0	6.0
41. Tha/Val NE1	6667.3	6395.5	6.0
42. Tha/Val NE2	6668.3	6320.5	6.0
43. Tha/Val NE3	6669.3	6245.5	6.0
44. Tha/Val NE4	6744.3	6245.5	6.0
45. Tha/Val NE5	6819.2	6249.6	6.0
46. Tha/Val SE1	6822.3	6191.6	6.0
47. Tha/Val SE2	6747.3	6189.6	6.0
48. Tha/Val SE3	6672.3	6187.5	6.0
49. Tha/Val SE4	6671.6	6112.5	6.0
50. Tha/Val SE5	6670.9	6037.5	6.0
51. Tha/Val SW1	6560.2	5964.7	6.0
52. Tha/Val SW2	6560.9	6039.7	6.0
53. Tha/Val SW3	6561.6	6114.7	6.0
54. Tha/Val SW4	6502.2	6068.9	6.0
55. Tha/Val SW5	6442.7	6023.2	6.0
56. Tha/Val NW1	6441.0	6115.2	6.0
57. Tha/Val NW2	6500.4	6160.9	6.0
58. Tha/Val NW3	6559.8	6206.7	6.0
59. Tha/Val NW4	6558.8	6281.7	6.0
60. Tha/Val NW5	6557.8	6356.7	6.0

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	2.	2.	3.	1.	1.	1.	2.	2.
10.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.
20.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	2.	2.	2.	1.	1.	1.	1.	2.
30.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	2.	1.	1.	2.	2.	2.	1.	2.
40.	0.	0.	1.	0.	0.	2.	2.	2.	1.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.
50.	0.	0.	1.	1.	1.	1.	2.	2.	0.	0.	1.	1.	2.	1.	1.	3.	2.	2.	3.	2.
60.	0.	0.	2.	2.	1.	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	2.	2.	1.	3.	2.
70.	0.	1.	3.	3.	2.	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	3.	2.	1.	3.	3.
80.	1.	1.	3.	3.	2.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	3.	2.	0.	2.	3.
90.	1.	1.	3.	3.	2.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	1.	2.	3.
100.	1.	2.	2.	3.	2.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	2.	2.
110.	1.	1.	2.	2.	2.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	2.	2.	2.	1.	2.
120.	1.	1.	2.	2.	2.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	2.
130.	1.	1.	2.	2.	2.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	2.
140.	1.	1.	2.	2.	2.	0.	0.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.
150.	1.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	1.
160.	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
170.	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
180.	2.	2.	3.	3.	3.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
190.	2.	2.	3.	3.	3.	1.	1.	2.	2.	1.	0.	0.	1.	0.	0.	1.	1.	2.	1.	0.
200.	2.	2.	2.	3.	3.	1.	1.	2.	2.	1.	0.	0.	2.	1.	1.	1.	1.	1.	0.	0.
210.	2.	1.	2.	2.	3.	1.	1.	2.	2.	1.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.
220.	2.	1.	2.	2.	2.	1.	1.	1.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
230.	2.	2.	1.	1.	2.	1.	1.	0.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
240.	2.	2.	1.	1.	1.	1.	1.	0.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
250.	1.	2.	1.	1.	1.	2.	1.	0.	1.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.
260.	1.	2.	1.	1.	1.	2.	1.	0.	1.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.
270.	1.	2.	2.	1.	1.	2.	2.	0.	1.	2.	1.	1.	1.	2.	2.	0.	0.	0.	0.	0.
280.	1.	2.	2.	1.	0.	2.	2.	0.	0.	1.	1.	1.	1.	2.	2.	0.	0.	0.	0.	0.
290.	1.	2.	2.	1.	0.	3.	2.	0.	0.	1.	1.	1.	1.	2.	2.	0.	0.	0.	0.	0.
300.	1.	2.	2.	1.	0.	2.	3.	0.	1.	1.	1.	1.	1.	2.	2.	0.	0.	0.	0.	0.
310.	1.	2.	2.	0.	0.	2.	3.	1.	1.	1.	2.	1.	1.	2.	2.	0.	0.	0.	0.	0.
320.	1.	1.	1.	0.	0.	2.	2.	2.	2.	1.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.
330.	0.	0.	1.	0.	0.	2.	2.	2.	2.	1.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.	2.	3.	0.	0.	1.	0.	0.
350.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.	2.	3.	1.	1.	1.	0.	0.
360.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	2.	2.	3.	1.	1.	1.	0.	0.
MAX	2.	2.	3.	3.	3.	3.	3.	2.	2.	2.	2.	2.	2.	2.	3.	3.	2.	2.	1.	1.
DEGR.	170	180	80	190	200	290	300	330	210	240	320	0	220	340	350	70	90	40	60	80

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 110.  *    0.    1.    2.    2.    1.    0.    0.    0.    0.    0.    2.    2.    2.    2.    1.    3.    3.    3.
4.    5.
 120.  *    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    2.    2.    2.    2.    1.    2.    3.    3.
4.    5.
 130.  *    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    3.    2.    2.    2.    1.    2.    3.    4.
4.    5.
 140.  *    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    3.    3.    3.    2.    1.    2.    4.    4.
4.    4.
 150.  *    2.    2.    2.    2.    1.    0.    0.    0.    0.    0.    3.    3.    3.    2.    1.    2.    4.    4.
4.    4.
 160.  *    4.    3.    3.    2.    1.    0.    0.    0.    0.    1.    4.    4.    4.    2.    2.    2.    4.    4.
4.    3.
 170.  *    6.    5.    4.    2.    2.    0.    0.    2.    2.    2.    4.    4.    4.    2.    1.    2.    4.    5.
3.    3.
 180.  *    6.    6.    6.    4.    2.    1.    2.    4.    3.    4.    3.    2.    2.    1.    0.    2.    2.    4.
2.    2.
 190.  *    5.    5.    6.    4.    3.    2.    2.    4.    4.    4.    1.    1.    1.    0.    0.    1.    1.    2.
2.    1.
 200.  *    4.    4.    5.    4.    4.    1.    2.    4.    4.    4.    0.    0.    0.    0.    0.    1.    1.    2.
1.    0.
 210.  *    4.    4.    4.    4.    3.    2.    2.    3.    3.    3.    0.    0.    0.    0.    0.    1.    1.    2.
1.    0.
 220.  *    4.    4.    4.    4.    3.    2.    2.    3.    3.    3.    0.    0.    0.    0.    0.    1.    1.    2.
0.    0.
 230.  *    4.    4.    4.    4.    3.    3.    2.    2.    3.    3.    3.    0.    0.    1.    1.    1.    1.    1.
0.    0.
 240.  *    4.    4.    4.    4.    2.    2.    3.    3.    4.    3.    3.    0.    0.    1.    1.    1.    0.    1.
0.    0.
 250.  *    4.    4.    3.    2.    2.    3.    3.    3.    3.    3.    0.    0.    2.    1.    1.    0.    0.    0.
0.    0.
 260.  *    3.    3.    3.    2.    2.    3.    3.    3.    4.    3.    0.    0.    2.    1.    1.    0.    0.    0.
0.    0.
 270.  *    3.    4.    3.    2.    2.    3.    3.    3.    4.    3.    0.    1.    2.    1.    1.    0.    0.    0.
0.    0.
 280.  *    4.    4.    4.    2.    2.    3.    4.    3.    3.    3.    0.    1.    2.    1.    1.    0.    0.    0.
0.    0.
 290.  *    4.    4.    4.    2.    2.    3.    4.    4.    3.    3.    0.    1.    2.    1.    1.    0.    0.    0.
0.    0.
 300.  *    4.    4.    4.    2.    1.    3.    4.    4.    3.    3.    0.    1.    2.    1.    1.    0.    0.    0.
0.    0.
 310.  *    4.    4.    5.    2.    1.    2.    4.    5.    4.    4.    0.    1.    2.    1.    1.    0.    0.    0.
0.    0.
 320.  *    4.    4.    4.    1.    0.    2.    4.    6.    5.    4.    1.    1.    2.    1.    1.    0.    0.    1.
1.    1.
 330.  *    3.    3.    3.    0.    0.    1.    3.    5.    5.    5.    1.    2.    3.    2.    1.    0.    0.    2.
2.    2.
 340.  *    1.    1.    2.    0.    0.    1.    2.    4.    4.    5.    2.    3.    4.    2.    1.    0.    1.    4.
4.    4.
 350.  *    0.    0.    0.    0.    0.    1.    2.    2.    3.    3.    3.    4.    5.    3.    2.    1.    2.    6.
5.    5.
 360.  *    0.    0.    0.    0.    0.    1.    2.    2.    2.    2.    4.    4.    5.    4.    2.    1.    2.    5.
5.    5.

------*-------------------------------------------------------------------------------------------------------------
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 MAX   *    6.    6.    6.    4.    4.    3.    4.    6.    5.    5.    4.    4.    5.    4.    3.    3.    4.    6.
5.    5.
 DEGR. *  180   180   190   190   200   280   300   320   330   330   170     0     0    20    40    90   150   350
350   110
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```
3.    2.
  60.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    4.    4.    3.    2.    2.    2.    2.    3.
2.    2.
  70.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    3.    3.    3.    2.    2.    2.    2.    2.
2.    2.
  80.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    3.    4.    3.    2.    2.    2.    3.    3.
2.    2.
  90.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    3.    4.    3.    2.    2.    2.    2.    3.
3.    3.
 100.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    3.    3.    3.    2.    2.    2.    2.    4.
2.    2.
 110.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    3.    3.    3.    2.    2.    2.    2.    4.
2.    2.
 120.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    3.    4.    3.    2.    2.    2.    2.    4.
3.    3.
 130.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    3.    4.    4.    2.    2.    2.    2.    4.
3.    3.
 140.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    4.    4.    4.    3.    2.    3.    3.    4.
4.    3.
 150.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    5.    4.    5.    3.    2.    3.    3.    5.
4.    4.
 160.  *    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    6.    5.    5.    4.    2.    3.    4.    5.
5.    5.
 170.  *    2.    2.    2.    0.    0.    0.    1.    2.    2.    2.    7.    6.    5.    3.    1.    2.    3.    5.
5.    5.
 180.  *    4.    4.    4.    1.    1.    1.    1.    3.    3.    3.    5.    4.    4.    2.    0.    0.    2.    4.
4.    3.
 190.  *    4.    5.    5.    2.    1.    1.    2.    5.    5.    4.    3.    2.    2.    1.    0.    0.    1.    2.
2.    2.
 200.  *    4.    5.    5.    2.    1.    1.    2.    5.    5.    5.    1.    1.    1.    0.    0.    0.    0.    1.
0.    0.
 210.  *    3.    4.    5.    2.    2.    2.    2.    5.    5.    5.    1.    1.    0.    0.    0.    0.    0.    0.
0.    0.
 220.  *    3.    4.    4.    2.    2.    2.    2.    4.    4.    5.    1.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 230.  *    3.    3.    4.    2.    2.    2.    2.    4.    4.    4.    1.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 240.  *    3.    3.    4.    2.    1.    1.    2.    4.    4.    4.    1.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 250.  *    3.    3.    3.    2.    1.    2.    2.    4.    4.    4.    1.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 260.  *    3.    3.    3.    2.    2.    2.    2.    4.    4.    4.    2.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 270.  *    2.    3.    3.    2.    1.    1.    2.    4.    4.    4.    2.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 280.  *    2.    2.    3.    2.    1.    1.    2.    4.    3.    4.    2.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 290.  *    2.    2.    2.    2.    1.    1.    2.    3.    3.    4.    2.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 300.  *    3.    3.    3.    2.    1.    1.    2.    3.    4.    4.    1.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 310.  *    3.    3.    3.    2.    1.    1.    2.    3.    4.    4.    2.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 320.  *    3.    3.    3.    2.    2.    2.    2.    3.    4.    4.    1.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 330.  *    4.    4.    4.    2.    2.    2.    2.    4.    4.    5.    1.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 340.  *    4.    4.    4.    2.    1.    1.    2.    4.    5.    5.    1.    1.    1.    1.    0.    0.    0.    1.
1.    1.
 350.  *    3.    4.    4.    2.    1.    1.    2.    4.    5.    5.    2.    2.    2.    1.    0.    1.    1.    2.
2.    2.
 360.  *    2.    2.    2.    1.    0.    0.    1.    2.    3.    3.    4.    4.    4.    2.    1.    1.    2.    3.
3.    3.

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX   *    4.    5.    5.    2.    2.    2.    2.    5.    5.    5.    7.    6.    5.    4.    2.    3.    4.    5.
5.    5.
 DEGR. *  190   190   200   210   220   220   210   200   200   340   170   170   170   160   150   150   160   160
170   170

 THE HIGHEST CONCENTRATION OF      7. ug/m**3 OCCURRED AT RECEPTOR REC51.
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      JOB: Government Center Garage                          RUN: Build

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (ug/m**3)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52 REC53 REC54 REC55 REC56 REC57 REC58
REC59 REC60

------*-------------------------------------------------------------------------------------------------------------
-------
   0.  *    2.    2.    2.    1.    0.    0.    1.    2.    3.    3.    4.    4.    4.    2.    1.    1.    2.    3.
3.    3.
  10.  *    1.    1.    1.    0.    0.    0.    0.    1.    1.    1.    5.    4.    4.    2.    2.    1.    2.    4.
4.    3.
  20.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    5.    4.    4.    3.    2.    1.    2.    4.
3.    3.
  30.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    4.    4.    4.    2.    2.    1.    2.    3.
3.    3.
  40.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    4.    4.    4.    2.    2.    1.    2.    3.
3.    3.
  50.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    4.    4.    4.    2.    2.    2.    2.    3.
```

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16:10:32

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	0.	100.0	1.0	10.0	0.71 7.8
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5105.0	6035.3	*	120.	325.	AG	0.	100.0	1.0	20.0	0.55 6.1
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	0.	100.0	1.0	20.0	0.92 9.6
4.	Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	0.	100.0	1.0	10.0	0.58 6.4
5.	Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	0.	100.0	1.0	10.0	0.64 4.1
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5366.6	5747.7	*	55.	109.	AG	0.	100.0	1.0	20.0	0.44 2.8
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	0.	100.0	1.0	20.0	0.68 4.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	0.	100.0	1.0	10.0	0.93 8.1
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6144.6	7708.0	*	931.	334.	AG	0.	100.0	1.0	40.0	1.09 47.3
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	0.	100.0	1.0	20.0	0.58 5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	0.	100.0	1.0	10.0	0.53 6.6
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6667.3	5333.6	*	1420.	177.	AG	0.	100.0	1.0	20.0	1.41 72.1
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	0.	100.0	1.0	30.0	0.47 4.6
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.6	6363.6	*	140.	358.	AG	0.	100.0	1.0	20.0	0.80 7.1
15.	Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	0.	100.0	1.0	10.0	1.23 59.7
16.	Tha/Val NB TR	*	6645.6	6138.6	6647.7	6016.6	*	122.	179.	AG	0.	100.0	1.0	10.0	0.70 6.2
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6099.5	*	136.	0.	AG	0.	100.0	1.0	30.0	0.69 6.9
18.	Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	0.	100.0	1.0	30.0	0.18 1.8
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.2	5885.7	*	146.	358.	AG	0.	100.0	1.0	40.0	0.75 7.4
20.	Char/93 WB LTT	*	6702.8	5647.8	6766.7	5567.9	*	102.	141.	AG	0.	100.0	1.0	20.0	0.65 5.2
21.	Char/93 EB TTR	*	6560.8	5622.5	6514.2	5588.4	*	58.	234.	AG	0.	100.0	1.0	30.0	0.37 2.9
22.	North/Congress SB LT	*	6876.6	4408.9	6575.8	5898.4	*	1520.	349.	AG	0.	100.0	1.0	30.0	2.65 77.2
23.	North/Con WB LLTR	*	6920.6	4378.3	7916.6	4730.8	*	1057.	71.	AG	0.	100.0	1.0	20.0	1.13 53.7
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6921.1	4287.3	*	47.	172.	AG	0.	100.0	1.0	30.0	0.34 2.4
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	0.	100.0	1.0	10.0	0.03 0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1464.	0.0	1.0	90.0	
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1588.	0.0	1.0	78.0	
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	967.	0.0	1.0	78.0	
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	0.0	1.0	78.0	
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3453.	0.0	1.0	90.0	
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	0.0	1.0	66.0	
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2405.	0.0	1.0	90.0	
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	0.0	1.0	78.0	
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2431.	0.0	1.0	90.0	
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	0.0	1.0	38.0	
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2871.	0.0	1.0	90.0	
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	0.0	1.0	54.0	
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2351.	0.0	1.0	66.0	
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	0.0	1.0	48.0	
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	542.	0.0	1.0	42.0	
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	0.0	1.0	48.0	
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	459.	0.0	1.0	54.0	
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	729.	0.0	1.0	54.0	

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	0.0	1.0	42.0	

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
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LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1629.	0.0	1.0	98.0	
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1333.	0.0	1.0	66.0	
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1545.	0.0	1.0	98.0	
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	0.0	1.0	54.0	

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
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1.	Stan/Lom SB L	*	120	75	3.0	376	1600	0.07	1	3
2.	Stan/Lom SB TRR	*	120	75	3.0	585	1600	0.07	1	3
3.	Stan/Lom WB LTT	*	120	91	3.0	588	1600	0.07	1	3
4.	Stan/Lom WB R	*	120	75	3.0	308	1600	0.07	1	3
5.	Stan/Lom NB L	*	120	97	3.0	152	1600	0.07	1	3
6.	Stan/Lom NB TRR	*	120	97	3.0	208	1600	0.07	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	324	1600	0.07	1	3
8.	Stan/Lom EB R	*	120	97	3.0	222	1600	0.07	1	3
9.	Caus/Wash SB LTTRR	*	150	94	3.0	2380	1600	0.07	1	3
10.	Caus/Wash WB LLTT	*	150	119	3.0	321	1600	0.07	1	3
11.	Caus/Wash WB R	*	150	104	3.0	230	1600	0.07	1	3
12.	Caus/Wash NB TTR	*	150	120	3.0	748	1600	0.07	1	3
13.	Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	0.07	1	3
14.	Tha/Val SB LTTR	*	104	30	3.0	1705	1600	0.07	1	3
15.	Tha/Val NB L	*	104	74	3.0	472	1600	0.07	1	3
16.	Tha/Val NB TR	*	104	30	3.0	744	1600	0.07	1	3
17.	Bev/Was SB TTT	*	100	45	3.0	1655	1600	0.07	1	3
18.	Bev/Was EB RRR	*	100	55	3.0	356	1600	0.07	1	3
19.	Char/93 SB LLTTRR	*	100	53	3.0	2013	1600	0.07	1	3
20.	Char/93 WB LTT	*	100	69	3.0	542	1600	0.07	1	3
21.	Char/93 EB TTR	*	100	69	3.0	459	1600	0.07	1	3
22.	North/Congress SB LT	*	100	90	3.0	636	1600	0.07	1	3
23.	North/Con WB LLTR	*	100	60	3.0	1267	1600	0.07	1	3
24.	Nor/Con NB LTTTR	*	100	74	3.0	345	1600	0.07	1	3
25.	Nor/Con EB LTR	*	100	60	3.0	17	1600	0.07	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Bev/Was N1	*	6562.0	6150.2	6.0	*
2.	Bev/Was N2	*	6561.2	6075.2	6.0	*
3.	Bev/Was N3	*	6560.5	6000.2	6.0	*
4.	Bev/Was N4	*	6515.8	6060.4	6.0	*
5.	Bev/Was N5	*	6471.1	6120.6	6.0	*
6.	Bev/Was SE1	*	6671.0	6049.7	6.0	*
7.	Bev/Was SE2	*	6670.2	5966.3	6.0	*
8.	Bev/Was SE3	*	6624.0	5907.2	6.0	*
9.	Bev/Was SE4	*	6626.1	5832.3	6.0	*
10.	Bev/Was SE5	*	6628.1	5757.3	6.0	*
11.	Bev/Was SW1	*	6541.8	5766.9	6.0	*
12.	Bev/Was SW2	*	6540.1	5841.9	6.0	*
13.	Bev/Was SW3	*	6537.7	5916.8	6.0	*
14.	Bev/Was SW4	*	6493.0	5977.0	6.0	*
15.	Bev/Was SW5	*	6448.3	6037.3	6.0	*
16.	Char/93 NE1	*	6625.0	5871.1	6.0	*
17.	Char/93 NE2	*	6627.1	5796.1	6.0	*
18.	Char/93 NE3	*	6629.1	5721.1	6.0	*
19.	Char/93 NE4	*	6699.8	5695.9	6.0	*
20.	Char/93 NE5	*	6750.6	5633.2	6.0	*
21.	Char/93 S1	*	6657.8	5466.0	6.0	*
22.	Char/93 S2	*	6614.7	5527.4	6.0	*
23.	Char/93 S3	*	6571.7	5588.8	6.0	*
24.	Char/93 S4	*	6512.9	5542.2	6.0	*
25.	Char/93 S5	*	6454.1	5495.6	6.0	*
26.	Char/93 NW1	*	6424.1	5632.5	6.0	*

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Char/93 NW2	6483.6	5678.2	6.0
28. Char/93 NW3	6543.0	5723.9	6.0
29. Char/93 NW4	6541.0	5798.8	6.0
30. Char/93 NW5	6538.9	5873.8	6.0
31. Wash/Cong NE1	6910.2	4571.2	6.0
32. Wash/Cong NE2	6925.8	4497.8	6.0
33. Wash/Cong NE3	6941.4	4424.5	6.0
34. Wash/Cong NE4	7012.0	4449.6	6.0
35. Wash/Cong NE5	7082.7	4474.9	6.0
36. Wash/Cong SE1	7095.4	4388.1	6.0
37. Wash/Cong SE2	7024.8	4362.9	6.0
38. Wash/Cong SE3	6954.1	4337.7	6.0
39. Wash/Cong SE4	6968.4	4264.1	6.0
40. Wash/Cong SE5	6982.7	4190.4	6.0
41. Wash/Cong SW1	6867.5	4164.7	6.0
42. Wash/Cong SW2	6853.3	4238.0	6.0
43. Wash/Cong SW3	6838.9	4312.0	6.0
44. Wash/Cong SW4	6765.6	4296.1	6.0
45. Wash/Cong SW5	6692.3	4280.2	6.0
46. Wash/Cong NW1	6682.4	4353.8	6.0
47. Wash/Cong NW2	6755.7	4369.7	6.0
48. Wash/Cong NW3	6828.9	4386.0	6.0
49. Wash/Cong NW4	6813.3	4459.4	6.0
50. Wash/Cong NW5	6797.8	4532.8	6.0

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	4.	4.	4.	2.	1.	3.	3.	8.	6.	6.	4.	3.	3.	2.	1.	7.	6.	7.	2.	1.
10.	5.	4.	4.	2.	2.	1.	1.	7.	5.	4.	5.	4.	4.	2.	2.	6.	5.	5.	0.	0.
20.	5.	4.	5.	3.	2.	0.	0.	6.	3.	3.	6.	5.	4.	2.	2.	4.	3.	3.	0.	0.
30.	4.	4.	4.	3.	2.	0.	0.	4.	3.	2.	6.	5.	4.	2.	2.	3.	2.	2.	0.	0.
40.	4.	4.	4.	3.	2.	0.	0.	3.	2.	2.	5.	5.	4.	2.	2.	2.	2.	2.	0.	0.
50.	4.	4.	4.	2.	2.	0.	0.	2.	2.	1.	5.	5.	3.	2.	2.	2.	2.	1.	0.	0.
60.	4.	3.	4.	2.	2.	0.	0.	2.	2.	1.	4.	5.	3.	2.	2.	2.	1.	1.	0.	0.
70.	4.	3.	3.	2.	2.	0.	0.	2.	2.	1.	4.	4.	3.	3.	2.	2.	1.	1.	0.	0.
80.	4.	4.	3.	2.	2.	0.	0.	2.	1.	1.	4.	4.	3.	3.	2.	2.	1.	1.	0.	0.
90.	3.	4.	4.	2.	2.	0.	0.	2.	1.	1.	4.	5.	3.	3.	2.	2.	1.	1.	0.	0.
100.	3.	4.	4.	2.	2.	0.	0.	2.	1.	1.	4.	4.	3.	3.	2.	2.	1.	1.	0.	0.
110.	3.	3.	3.	2.	2.	0.	0.	2.	2.	1.	4.	4.	3.	3.	2.	2.	1.	2.	0.	0.
120.	3.	4.	3.	2.	2.	0.	0.	2.	2.	1.	4.	5.	4.	3.	2.	2.	1.	2.	0.	0.
130.	4.	4.	3.	2.	2.	0.	0.	2.	2.	2.	4.	5.	4.	3.	2.	2.	2.	2.	0.	0.
140.	4.	4.	3.	3.	3.	0.	0.	2.	2.	3.	4.	6.	6.	3.	2.	2.	2.	3.	1.	0.
150.	4.	5.	4.	3.	3.	0.	0.	3.	3.	3.	4.	6.	6.	4.	3.	3.	3.	4.	1.	1.
160.	5.	5.	6.	4.	3.	0.	1.	4.	4.	5.	3.	5.	6.	3.	2.	4.	4.	5.	2.	1.
170.	5.	5.	6.	3.	3.	2.	2.	5.	5.	6.	3.	4.	5.	2.	1.	5.	6.	7.	3.	2.
180.	4.	4.	5.	2.	1.	3.	3.	6.	6.	6.	2.	2.	2.	1.	0.	6.	6.	7.	3.	3.
190.	2.	2.	3.	1.	1.	4.	4.	6.	6.	5.	1.	1.	1.	0.	0.	6.	5.	6.	3.	3.
200.	1.	1.	2.	0.	0.	5.	4.	6.	6.	4.	1.	0.	0.	0.	0.	6.	5.	5.	3.	3.
210.	1.	0.	1.	0.	0.	5.	5.	5.	5.	4.	0.	0.	0.	0.	0.	5.	5.	4.	3.	3.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	10.	6.	5.	3.	2.	1.	1.	4.	3.	3.	0.	1.	1.	0.	0.	1.	2.	2.	2.	1.
10.	8.	5.	5.	4.	3.	2.	2.	6.	5.	4.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.
20.	6.	4.	4.	4.	3.	2.	3.	6.	6.	4.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.
30.	5.	4.	3.	3.	3.	2.	3.	6.	6.	4.	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.
40.	4.	4.	2.	2.	2.	2.	3.	5.	5.	4.	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.
50.	4.	4.	2.	2.	2.	2.	2.	4.	5.	4.	0.	0.	0.	0.	0.	1.	2.	2.	0.	0.
60.	4.	4.	3.	2.	1.	2.	2.	4.	4.	4.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.
70.	3.	4.	3.	2.	1.	2.	2.	3.	4.	4.	0.	0.	1.	1.	0.	0.	1.	1.	0.	0.
80.	3.	4.	3.	2.	1.	2.	2.	3.	4.	4.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.
90.	3.	4.	3.	2.	1.	2.	2.	2.	4.	4.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.
100.	3.	4.	3.	2.	1.	2.	2.	2.	4.	4.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.
110.	3.	4.	3.	2.	1.	2.	3.	2.	4.	5.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.
120.	3.	4.	3.	1.	1.	2.	3.	2.	5.	5.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.
130.	4.	3.	2.	1.	1.	2.	3.	3.	5.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
140.	5.	4.	2.	1.	1.	2.	3.	3.	5.	6.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
150.	6.	3.	2.	1.	1.	2.	2.	3.	5.	6.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
160.	6.	3.	2.	1.	1.	2.	2.	3.	5.	6.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
170.	6.	3.	2.	1.	1.	2.	2.	3.	5.	6.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
180.	6.	3.	2.	1.	1.	2.	2.	3.	5.	6.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
190.	6.	3.	2.	1.	1.	2.	2.	3.	5.	6.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
200.	6.	3.	2.	1.	1.	2.	2.	3.	5.	6.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
210.	6.	3.	2.	1.	1.	2.	2.	3.	5.	6.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
220.	5.	3.	2.	1.	1.	2.	2.	3.	5.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
230.	5.	3.	2.	1.	1.	2.	2.	3.	5.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
240.	4.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
250.	4.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
260.	4.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
270.	4.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
280.	4.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
290.	3.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
300.	3.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
310.	3.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
320.	3.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
330.	3.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
340.	3.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
350.	3.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
360.	3.	3.	2.	1.	1.	2.	2.	3.	4.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
MAX	10.	6.	5.	4.	3.	2.	3.	6.	6.	5.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
DEGR.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

160.	*	7.	3.	2.	1.	1.	1.	2.	3.	4.	6.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
170.	*	8.	3.	1.	1.	0.	1.	2.	2.	3.	4.	2.	2.	2.	2.	2.	0.	0.	1.
1.	1.																		
180.	*	6.	1.	0.	0.	0.	1.	1.	2.	2.	2.	2.	2.	3.	2.	2.	0.	0.	1.
1.	1.																		
190.	*	4.	0.	0.	0.	0.	1.	1.	1.	1.	1.	3.	2.	3.	2.	2.	0.	0.	2.
1.	1.																		
200.	*	3.	0.	0.	0.	0.	1.	1.	1.	1.	0.	3.	2.	3.	2.	2.	0.	1.	2.
1.	1.																		
210.	*	2.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	3.	2.	0.	1.	2.
1.	1.																		
220.	*	2.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	3.	3.	0.	1.	2.
1.	1.																		
230.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
240.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
250.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
260.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.
1.	1.																		
270.	*	1.	0.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.
1.	1.																		
280.	*	2.	1.	2.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.
1.	1.																		
290.	*	2.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	3.	3.	2.
1.	1.																		
300.	*	2.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	3.	3.	3.
2.	1.																		
310.	*	2.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	3.	3.
2.	2.																		
320.	*	3.	1.	2.	1.	1.	0.	0.	0.	0.	0.	3.	3.	3.	1.	1.	2.	3.	4.
3.	2.																		
330.	*	5.	1.	2.	1.	1.	0.	0.	0.	0.	0.	3.	3.	3.	1.	1.	2.	3.	4.
3.	3.																		
340.	*	8.	2.	2.	1.	1.	0.	0.	0.	0.	1.	3.	3.	3.	1.	1.	2.	3.	4.
4.	3.																		
350.	*	10.	4.	3.	2.	1.	0.	0.	2.	2.	2.	2.	2.	2.	1.	1.	2.	2.	4.
3.	3.																		
360.	*	10.	6.	5.	3.	2.	1.	1.	4.	3.	3.	0.	1.	1.	0.	0.	1.	2.	2.
2.	1.																		

MAX	*	10.	6.	5.	4.	3.	2.	3.	6.	6.	6.	3.	3.	3.	3.	3.	3.	3.	4.
4.	3.																		
DEGR.	*	350	0	10	10	20	100	30	20	20	150	340	340	190	210	220	300	310	340
340	340																		

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50
0.	* 3.	3.	3.	1.	1.	1.	2.	3.	3.	3.
10.	* 3.	3.	3.	1.	1.	1.	1.	3.	3.	3.
20.	* 2.	2.	2.	1.	1.	1.	1.	3.	3.	3.
30.	* 2.	2.	2.	1.	1.	1.	2.	3.	3.	3.
40.	* 2.	3.	2.	1.	1.	1.	1.	2.	2.	2.
50.	* 1.	2.	2.	1.	1.	1.	1.	2.	2.	2.
60.	* 1.	2.	3.	2.	1.	1.	1.	2.	2.	2.
70.	* 1.	2.	3.	2.	1.	1.	2.	2.	2.	2.
80.	* 1.	1.	2.	1.	1.	1.	2.	3.	3.	2.
90.	* 1.	1.	2.	1.	1.	1.	2.	3.	3.	2.
100.	* 1.	1.	2.	1.	1.	1.	1.	2.	3.	2.
110.	* 1.	1.	2.	1.	0.	1.	1.	2.	3.	3.
120.	* 1.	1.	1.	1.	0.	0.	1.	2.	3.	3.
130.	* 1.	1.	1.	1.	0.	0.	1.	2.	3.	3.
140.	* 1.	1.	2.	1.	0.	0.	1.	2.	2.	3.
150.	* 1.	1.	2.	0.	0.	0.	0.	2.	2.	3.
160.	* 1.	1.	1.	0.	0.	0.	0.	1.	2.	2.
170.	* 0.	1.	1.	0.	0.	0.	0.	1.	1.	1.
180.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
190.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
200.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
210.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
220.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

240.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
250.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
260.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
270.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
280.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
290.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
300.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
310.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
320.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
330.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.
340.	*	1.	1.	1.	0.	0.	0.	1.	1.	1.
350.	*	2.	2.	2.	1.	1.	1.	3.	3.	3.
360.	*	3.	3.	3.	1.	1.	1.	2.	3.	3.

MAX	*	3.	3.	3.	2.	1.	1.	2.	3.	3.
DEGR.	*	0	0	0	60	70	70	80	0	0

THE HIGHEST CONCENTRATION OF 10. ug/m**3 OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16:10:15

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5120.9	6056.9	*	131.	326.	AG	0.	100.0	1.0	10.0	0.63	6.7
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5090.5	6056.1	*	145.	325.	AG	0.	100.0	1.0	20.0	0.70	7.4
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5368.6	5981.0	*	80.	51.	AG	0.	100.0	1.0	20.0	0.35	4.1
4.	Stan/Lom WB R	*	5292.4	5947.7	5403.8	6033.2	*	140.	52.	AG	0.	100.0	1.0	10.0	0.68	7.1
5.	Stan/Lom NB L	*	5307.6	5737.4	5341.6	5726.9	*	36.	107.	AG	0.	100.0	1.0	10.0	0.24	1.8
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5393.9	5738.4	*	84.	109.	AG	0.	100.0	1.0	20.0	0.56	4.3
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5171.4	5556.9	*	155.	196.	AG	0.	100.0	1.0	20.0	0.92	7.9
8.	Stan/Lom EB R	*	5236.5	5698.5	4944.8	4671.4	*	1068.	196.	AG	0.	100.0	1.0	10.0	1.34	54.2
9.	Char/93 SB LLTTRR	*	6587.8	5740.0	6580.8	5923.0	*	183.	358.	AG	0.	100.0	1.0	40.0	0.87	9.3
10.	Char/93 WB LTT	*	6702.8	5647.8	6737.0	5605.0	*	55.	141.	AG	0.	100.0	1.0	20.0	0.30	2.8
11.	Char/93 EB TTR	*	6560.8	5622.5	6458.6	5547.7	*	127.	234.	AG	0.	100.0	1.0	30.0	0.69	6.4
12.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1691.	0.0	1.0	90.0		
13.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1414.	0.0	1.0	78.0		
14.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	1247.	0.0	1.0	78.0		
15.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1387.	0.0	1.0	78.0		
16.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2091.	0.0	1.0	66.0		
17.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	334.	0.0	1.0	42.0		
18.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	1059.	0.0	1.0	48.0		
19.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	1159.	0.0	1.0	54.0		
20.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	499.	0.0	1.0	54.0		
21.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	414.	0.0	1.0	42.0		

PAGE 2

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16:10:15

		*								
1.	Stan/Lom SB L	*	120	79	3.0	304	1600	0.07	1	3
2.	Stan/Lom SB TRR	*	120	79	3.0	672	1600	0.07	1	3
3.	Stan/Lom WB LTT	*	120	71	3.0	412	1600	0.07	1	3
4.	Stan/Lom WB R	*	120	79	3.0	325	1600	0.07	1	3
5.	Stan/Lom NB L	*	120	93	3.0	70	1600	0.07	1	3
6.	Stan/Lom NB TRR	*	120	93	3.0	331	1600	0.07	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	439	1600	0.07	1	3
8.	Stan/Lom EB R	*	120	97	3.0	320	1600	0.07	1	3
9.	Char/93 SB LLTTRR	*	100	62	3.0	1842	1600	0.07	1	3
10.	Char/93 WB LTT	*	100	60	3.0	334	1600	0.07	1	3
11.	Char/93 EB TTR	*	100	60	3.0	1159	1600	0.07	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8.	Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0	*

		*			
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0 *
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0 *
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0 *
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0 *
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0 *
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0 *
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0 *
21.	Char/93 NE1	*	6625.0	5871.1	6.0 *
22.	Char/93 NE2	*	6627.1	5796.1	6.0 *
23.	Char/93 NE3	*	6629.1	5721.1	6.0 *
24.	Char/93 NE4	*	6699.8	5695.9	6.0 *
25.	Char/93 NE5	*	6750.6	5633.2	6.0 *
26.	Char/93 S1	*	6657.8	5466.0	6.0 *
27.	Char/93 S2	*	6614.7	5527.4	6.0 *
28.	Char/93 S3	*	6571.7	5588.8	6.0 *
29.	Char/93 S4	*	6512.9	5542.2	6.0 *
30.	Char/93 S5	*	6454.1	5495.6	6.0 *
31.	Char/93 NW1	*	6424.1	5632.5	6.0 *
32.	Char/93 NW2	*	6483.6	5678.2	6.0 *
33.	Char/93 NW3	*	6543.0	5723.9	6.0 *
34.	Char/93 NW4	*	6541.0	5798.8	6.0 *
35.	Char/93 NW5	*	6538.9	5873.8	6.0 *

PAGE 3

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	2.	2.	2.	3.	1.	1.	1.	2.	2.
10. *	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.
20. *	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	1.	2.	2.	2.	2.	1.	1.	1.	1.	2.
30. *	0.	0.	0.	0.	0.	1.	2.	2.	0.	0.	1.	2.	2.	1.	1.	2.	1.	2.	2.	2.
40. *	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.
50. *	0.	0.	1.	1.	0.	1.	1.	1.	0.	0.	1.	1.	2.	1.	0.	2.	2.	1.	2.	2.
60. *	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	1.	3.	2.
70. *	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	0.	3.	2.
80. *	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	0.	2.	3.
90. *	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	1.	2.	2.
100. *	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	1.	2.
110. *	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	2.	2.	2.	1.	2.
120. *	1.	1.	1.	2.	1.	0.	0.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	2.
130. *	1.	1.	2.	2.	2.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	2.
140. *	1.	2.	2.	2.	2.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.
150. *	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.
160. *	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
170. *	2.	2.	2.	2.	2.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
180. *	3.	2.	3.	2.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
190. *	2.	2.	3.	3.	3.	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	1.	2.	2.	1.	0.
200. *	2.	2.	3.	3.	3.	1.	2.	2.	2.	2.	0.	0.	2.	2.	1.	1.	1.	1.	0.	0.
210. *	2.	2.	2.	2.	3.	1.	2.	2.	3.	2.	0.	0.	2.	2.	2.	0.	0.	0.	0.	0.
220. *	2.	2.	2.	2.	2.	1.	1.	1.	2.	2.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
230. *	2.	2.	2.	1.	2.	1.	1.	0.	2.	3.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.
240. *	2.	2.	1.	1.	1.	1.	1.	0.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.

```
0.    0.
 250.  *    2.    2.    1.    1.    1.    1.    1.    0.    1.    3.    1.    1.    2.    2.    2.    0.    0.    0.
0.    0.
 260.  *    2.    2.    1.    1.    1.    2.    1.    0.    1.    2.    1.    1.    2.    2.    2.    0.    0.    0.
0.    0.
 270.  *    2.    2.    2.    1.    1.    2.    2.    0.    1.    2.    1.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 280.  *    2.    2.    2.    1.    1.    2.    2.    0.    1.    1.    1.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 290.  *    2.    2.    2.    1.    0.    2.    2.    0.    0.    1.    1.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 300.  *    2.    2.    2.    1.    0.    2.    3.    1.    1.    1.    1.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 310.  *    2.    2.    2.    0.    0.    2.    3.    1.    1.    1.    2.    1.    1.    2.    2.    0.    0.    0.
0.    0.
 320.  *    1.    1.    1.    0.    0.    2.    2.    2.    2.    1.    2.    2.    2.    2.    2.    0.    0.    0.
1.    1.
 330.  *    0.    1.    1.    0.    0.    2.    2.    3.    2.    1.    2.    2.    2.    2.    2.    0.    0.    1.
2.    2.
 340.  *    0.    0.    0.    0.    0.    2.    2.    3.    1.    1.    2.    2.    2.    2.    3.    0.    0.    1.
2.    2.
 350.  *    0.    0.    0.    0.    0.    1.    1.    2.    1.    1.    2.    2.    2.    2.    3.    0.    1.    1.
2.    2.
 360.  *    0.    0.    0.    0.    0.    1.    2.    2.    1.    0.    1.    2.    2.    2.    3.    1.    1.    1.
2.    2.

------*-------------------------------------------------------------------------------------------------------------
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 MAX   *    3.    2.    3.    3.    3.    2.    3.    3.    3.    3.    2.    2.    2.    2.    3.    2.    2.    2.
3.    3.
 DEGR. *  180   180   190   190   200   290   310   330   210   240   320   330   220   340   350    70    90   180
60    80
```


JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35
0.	0.	1.	1.	0.	0.	2.	2.	3.	3.	2.	0.	0.	2.	1.	0.
10.	0.	0.	0.	0.	0.	1.	2.	2.	3.	2.	0.	0.	3.	2.	1.
20.	0.	0.	0.	0.	0.	1.	1.	2.	3.	3.	0.	1.	3.	3.	1.
30.	0.	0.	0.	0.	0.	1.	1.	1.	2.	3.	1.	2.	3.	3.	2.
40.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.	1.	2.	3.	3.	2.
50.	0.	0.	0.	0.	0.	1.	1.	1.	1.	2.	1.	1.	3.	3.	2.
60.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	3.	3.
70.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	3.	3.
80.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	3.	3.
90.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	1.	1.	3.	3.
100.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	1.	0.	3.	3.
110.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	3.	3.
120.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	1.	3.	3.
130.	0.	0.	1.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	3.	3.
140.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.	3.	4.
150.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	2.	2.	3.	4.
160.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	2.	3.
170.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	2.	2.
180.	2.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	2.
190.	3.	2.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.
200.	4.	2.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	2.	1.	0.
210.	4.	3.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.
220.	4.	3.	2.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
230.	3.	3.	2.	2.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
240.	3.	3.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
250.	3.	3.	0.	2.	2.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
260.	3.	3.	1.	1.	2.	0.	0.	2.	1.	0.	0.	0.	0.	0.	0.
270.	3.	3.	1.	1.	2.	0.	1.	3.	2.	1.	0.	0.	0.	0.	0.
280.	3.	3.	1.	1.	2.	0.	1.	3.	2.	1.	0.	0.	0.	0.	0.
290.	3.	3.	2.	1.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
300.	3.	3.	2.	1.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
310.	2.	3.	3.	2.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
320.	2.	3.	3.	2.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
330.	2.	3.	3.	1.	1.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.
340.	1.	3.	3.	1.	0.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.
350.	1.	2.	2.	0.	0.	2.	2.	2.	2.	2.	0.	0.	1.	0.	0.
360.	0.	1.	1.	0.	0.	2.	2.	3.	3.	2.	0.	0.	2.	1.	0.
MAX	4.	3.	3.	2.	2.	2.	2.	3.	3.	3.	2.	2.	3.	3.	4.
DEGR.	210	320	330	230	260	350	350	280	10	20	110	120	30	40	150

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:14:43

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6042.8	5450.0	*	73.	290.	AG	0.	100.0	1.0	30.0	0.58	3.7
2. Char/Merr WB	*	6250.4	5435.2	6335.4	5502.4	*	108.	52.	AG	0.	100.0	1.0	30.0	0.75	5.5
3. Char/Merr NB R	*	6291.7	5369.7	6314.8	5354.0	*	28.	124.	AG	0.	100.0	1.0	10.0	0.14	1.4
4. Char/Merr NB LTT	*	6280.4	5347.2	7349.2	4593.4	*	1308.	125.	AG	0.	100.0	1.0	20.0	1.25	66.4
5. Char/Merr EB	*	6104.2	5362.2	6046.8	5340.9	*	61.	250.	AG	0.	100.0	1.0	20.0	0.58	3.1
6. Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.8	*	108.	14.	AG	0.	100.0	1.0	10.0	0.71	5.5
7. Char/Cam SB TR	*	5360.8	4833.5	5403.4	4971.2	*	144.	17.	AG	0.	100.0	1.0	20.0	0.95	7.3
8. Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	0.	100.0	1.0	20.0	0.27	2.2
9. Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	0.	100.0	1.0	10.0	0.60	4.7
10. Char/Cam NB TR	*	5383.3	4723.8	5384.5	4645.8	*	78.	179.	AG	0.	100.0	1.0	20.0	0.74	4.0
11. Char/Cam EB TTTR	*	5302.7	4739.8	5210.5	4740.8	*	92.	271.	AG	0.	100.0	1.0	30.0	0.57	4.7
12. Sud/Merr SB L	*	6532.7	5210.3	6385.1	5315.4	*	181.	305.	AG	0.	100.0	1.0	10.0	1.08	9.2
13. Sud/Merr SB TTT	*	6518.3	5190.8	6484.5	5210.4	*	39.	300.	AG	0.	100.0	1.0	30.0	0.20	2.0
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6678.7	5059.8	*	117.	150.	AG	0.	100.0	1.0	30.0	0.60	5.9
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6472.1	5115.0	*	60.	239.	AG	1.	100.0	1.0	40.0	0.47	3.0
16. Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	0.	100.0	1.0	20.0	0.34	3.3
17. Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6739.6	5238.0	*	59.	249.	AG	0.	100.0	1.0	30.0	0.49	3.0
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	945.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1232.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1619.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1565.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	1016.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1651.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	964.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1759.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	360.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	541.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	420.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1848.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1944.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	579.	0.0	1.0	78.0		

DATE : 8/ 7/13
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1. Char/Merr SB	*	100	76	3.0	530	1600	0.07	1	3
2. Char/Merr WB	*	100	74	3.0	757	1600	0.07	1	3
3. Char/Merr NB R	*	100	44	3.0	116	1600	0.07	1	3
4. Char/Merr NB LTT	*	100	70	3.0	1002	1600	0.07	1	3
5. Char/Merr EB	*	100	80	3.0	281	1600	0.07	1	3
6. Char/Cam SB L	*	90	58	3.0	340	1600	0.07	1	3
7. Char/Cam SB TR	*	90	71	3.0	472	1600	0.07	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	294	1600	0.07	1	3
9. Char/Cam NB L	*	90	58	3.0	289	1600	0.07	1	3
10. Char/Cam NB TR	*	90	71	3.0	367	1600	0.07	1	3

11. Char/Cam EB TTTR	*	90	54	3.0	937	1600	0.07	1	3
12. Sud/Merr SB L	*	100	89	3.0	104	1600	0.07	1	3
13. Sud/Merr SB TTT	*	100	41	3.0	524	1600	0.07	1	3
14. Sud/Merr NB TTTR	*	100	52	3.0	1232	1600	0.07	1	3
15. Sud/Merr EB LTTR	*	100	76	3.0	579	1600	0.07	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	455	1600	0.07	1	3
17. Sud/Sur SEB	*	100	70	3.0	26	1600	0.07	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	420	1600	0.07	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Char/Merr NE1	*	6063.7	5511.0	6.0
2. Char/Merr NE2	*	6133.9	5484.8	6.0
3. Char/Merr NE3	*	6204.2	5458.5	6.0
4. Char/Merr NE4	*	6265.6	5501.5	6.0
5. Char/Merr NE5	*	6327.1	5544.5	6.0
6. Char/Merr SE1	*	6443.7	5491.9	6.0
7. Char/Merr SE2	*	6382.2	5448.9	6.0
8. Char/Merr SE3	*	6320.8	5405.9	6.0
9. Char/Merr SE4	*	6380.5	5360.4	6.0
10. Char/Merr SE5	*	6440.1	5315.0	6.0
11. Char/Merr SW1	*	6332.0	5249.0	6.0
12. Char/Merr SW2	*	6272.3	5294.5	6.0
13. Char/Merr SW3	*	6212.6	5339.9	6.0
14. Char/Merr SW4	*	6141.6	5315.8	6.0
15. Char/Merr SW5	*	6070.6	5291.7	6.0
16. Char/Merr NW1	*	5902.1	5359.1	6.0
17. Char/Merr NW2	*	5973.1	5383.2	6.0
18. Char/Merr NW3	*	6044.1	5407.3	6.0
19. Char/Merr NW4	*	5973.9	5433.5	6.0
20. Char/Merr NW5	*	5903.6	5459.8	6.0
21. Char/Cam NE1	*	5490.2	4963.0	6.0
22. Char/Cam NE2	*	5459.0	4894.8	6.0
23. Char/Cam NE3	*	5427.8	4826.6	6.0
24. Char/Cam NE4	*	5500.4	4807.6	6.0
25. Char/Cam NE5	*	5572.9	4788.7	6.0
26. Char/Cam SE1	*	5553.9	4667.5	6.0
27. Char/Cam SE2	*	5481.3	4686.5	6.0
28. Char/Cam SE3	*	5408.7	4705.4	6.0
29. Char/Cam SE4	*	5409.4	4630.4	6.0
30. Char/Cam SE5	*	5410.1	4555.4	6.0
31. Char/Cam SW1	*	5312.0	4561.9	6.0
32. Char/Cam SW2	*	5310.7	4636.9	6.0
33. Char/Cam SW3	*	5310.7	4711.9	6.0

DATE : 8/ 7/13
TIME : 17:14:43

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Char/Cam SW4	*	5235.6	4712.1	6.0
35. Char/Cam SW5	*	5160.6	4711.9	6.0
36. Char/Cam NW1	*	5167.9	4822.4	6.0
37. Char/Cam NW2	*	5242.9	4822.1	6.0
38. Char/Cam NW3	*	5317.9	4821.9	6.0
39. Char/Cam NW4	*	5349.1	4890.1	6.0
40. Char/Cam NW5	*	5380.3	4958.3	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	2.	2.	0.	0.	1.	1.	1.
10.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	2.	2.	0.	0.	2.	1.	1.
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	2.	2.	2.	0.	0.	2.		

1.	1.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	1.	2.
1.	1.																		
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	1.	1.	2.
1.	1.																		
50.	*	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
60.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.
1.	1.																		
70.	*	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	2.	2.	3.
2.	1.																		
80.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.
2.	2.																		
90.	*	1.	1.	2.	2.	1.	0.	0.	0.	0.	1.	3.	3.	2.	1.	1.	3.	3.	3.
3.	2.																		
100.	*	1.	1.	2.	2.	1.	0.	0.	0.	0.	1.	3.	3.	3.	2.	2.	2.	3.	3.
3.	2.																		
110.	*	2.	2.	3.	2.	1.	0.	0.	1.	1.	2.	3.	3.	3.	2.	1.	2.	3.	3.
3.	2.																		
120.	*	2.	3.	3.	2.	1.	0.	1.	1.	2.	2.	2.	2.	3.	1.	1.	2.	2.	3.
2.	2.																		
130.	*	3.	3.	4.	3.	1.	0.	1.	3.	3.	4.	1.	2.	2.	0.	0.	1.	2.	2.
2.	1.																		
140.	*	2.	3.	4.	4.	2.	1.	2.	3.	4.	4.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
150.	*	2.	2.	3.	4.	3.	1.	2.	3.	3.	4.	0.	0.	0.	0.	0.	1.	1.	2.
1.	1.																		
160.	*	2.	2.	2.	3.	3.	2.	2.	2.	3.	4.	0.	0.	0.	0.	0.	1.	1.	2.
1.	1.																		
170.	*	2.	2.	2.	3.	2.	1.	2.	2.	2.	3.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
180.	*	2.	2.	2.	3.	3.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
190.	*	2.	2.	2.	3.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
200.	*	2.	2.	2.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
210.	*	2.	2.	2.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.
1.	1.																		
220.	*	2.	3.	2.	2.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.
1.	0.																		
230.	*	1.	2.	3.	2.	2.	1.	2.	2.	2.	2.	0.	0.	0.	0.	1.	1.	2.	2.
1.	0.																		
240.	*	1.	2.	3.	2.	2.	2.	2.	2.	2.	2.	0.	0.	1.	1.	1.	1.	1.	1.
0.	0.																		
250.	*	1.	2.	2.	1.	1.	2.	3.	3.	2.	2.	0.	0.	1.	1.	1.	0.	1.	1.
0.	0.																		
260.	*	1.	1.	2.	1.	1.	3.	3.	3.	2.	3.	0.	0.	2.	1.	1.	0.	0.	0.
0.	0.																		
270.	*	1.	1.	1.	0.	0.	2.	3.	3.	3.	3.	0.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
280.	*	1.	1.	1.	0.	0.	2.	2.	3.	3.	3.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	1.	0.	0.	1.	2.	3.	2.	3.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	0.	0.	0.	1.	2.	2.	2.	2.	1.	2.	2.	2.	1.	0.	0.	1.
1.	0.																		
310.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	1.	0.	0.	1.
1.	0.																		
320.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.
1.	0.																		
330.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.
1.	1.																		
340.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	0.	0.	1.
1.	1.																		
350.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	2.	2.	0.	0.	1.
1.	1.																		
360.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	2.	2.	0.	0.	1.
1.	1.																		

MAX	*	3.	3.	4.	4.	3.	3.	3.	3.	4.	4.	3.	3.	3.	2.	2.	3.	3.	3.
3.	2.																		
DEGR.	*	130	130	130	140	200	260	260	260	140	140	100	110	110	40	50	90	90	100
100	100																		

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE	*	(ug/m**3)																	
(DEGR)	*	REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38
REC39	REC40																		
0.	*	0.	1.	1.	0.	0.	1.	1.	2.	2.	2.	2.	2.	2.	2.	1.	0.	0.	0.
0.	0.																		
10.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	2.	1.	0.	0.	1.
1.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	3.	3.	3.	1.	0.	0.	1.
1.	0.																		
40.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.	4.	2.	0.	0.	2.
2.	1.																		
50.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.	4.	3.	0.	1.	2.
2.	2.																		
60.	*	1.	0.	0.	1.	0.	2.	2.	2.	1.	1.	2.	2.	3.	4.	3.	1.	1.	2.
2.	2.																		
70.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	1.	2.	3.	3.	3.	1.	2.	2.
2.	2.																		
80.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	2.	2.
2.	2.																		
90.	*	0.	0.	0.	0.	0.	1.	2.	2.	0.	0.	1.	1.	3.	2.	2.	2.	2.	2.
2.	2.																		
100.	*	0.	0.	1.	1.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	2.	2.	3.
2.	2.																		
110.	*	0.	0.	1.	1.	1.	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	3.	3.	3.
2.	2.																		
120.	*	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	3.	3.	3.
3.	2.																		
130.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	3.
3.	2.																		
140.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.
3.	3.																		
150.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.
3.	3.																		
160.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.
3.	3.																		
170.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	3.
3.	4.																		
180.	*	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	2.	2.
3.	3.																		
190.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
2.	3.																		
200.	*	1.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
2.	2.																		
210.	*	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
1.	1.																		
220.	*	2.	2.	3.	2.	2.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.
1.	1.																		
230.	*	2.	2.	3.	2.	2.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.
1.	1.																		
240.	*	2.	2.	3.	2.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.
1.	0.																		
250.	*	2.	2.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
1.	0.																		
260.	*	1.	2.	3.	3.	3.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.
0.	0.																		
270.	*	1.	2.	2.	3.	2.	1.	1.	3.	1.	1.	0.	0.	1.	1.	0.	1.	1.	1.
0.	0.																		
280.	*	1.	1.	2.	2.	2.	2.	2.	3.	1.	1.	0.	0.	2.	1.	1.	0.	0.	0.
0.	0.																		
290.	*	1.	1.	2.	1.	1.	2.	2.	4.	2.	1.	0.	0.	3.	2.	1.	0.	0.	0.
0.	0.																		
300.	*	1.	1.	2.	1.	1.	2.	2.	3.	2.	1.	0.	1.	3.	2.	1.	0.	0.	0.
0.	0.																		
310.	*	1.	1.	2.	1.	1.	2.	2.	3.	3.	1.	0.	1.	3.	2.	2.	0.	0.	0.
0.	0.																		
320.	*	1.	1.	2.	1.	0.	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
330.	*	1.	1.	2.	1.	0.	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	1.	2.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	1.	1.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	1.	1.	0.	0.	1.	1.	2.	2.	2.	2.	2.	2.	2.	1.	0.	0.	0.
0.	0.																		

MAX	*	2.	2.	3.	3.	3.	2.	2.	4.	3.	2.	2.	3.	3.	4.	3.	3.	3.	3.
3.	3.																		
DEGR.	*	230	230	250	250	260	300	300	290	320	340	20	30	40	50	70	110	110	120
160	170																		

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC3 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15: 1

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT)				*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
			X1	Y1	X2	Y2										
1.	Char/Merr SB	*	6111.6	5425.1	6030.2	5454.5	*	87.	290.	AG	0.	100.0	1.0	30.0	0.67	4.4
2.	Char/Merr WB	*	6250.4	5435.2	6310.4	5482.7	*	77.	52.	AG	0.	100.0	1.0	30.0	0.67	3.9
3.	Char/Merr NB R	*	6291.7	5369.7	6352.1	5328.7	*	73.	124.	AG	0.	100.0	1.0	10.0	0.37	3.7
4.	Char/Merr NB LTT	*	6280.4	5347.2	6430.9	5241.1	*	184.	125.	AG	0.	100.0	1.0	20.0	0.94	9.4
5.	Char/Merr EB	*	6104.2	5362.2	5936.5	5299.8	*	179.	250.	AG	0.	100.0	1.0	20.0	0.92	9.1
6.	Char/Cam SB L	*	5384.1	4834.2	5402.6	4908.3	*	76.	14.	AG	0.	100.0	1.0	10.0	0.42	3.9
7.	Char/Cam SB TR	*	5360.8	4833.5	5378.3	4889.9	*	59.	17.	AG	0.	100.0	1.0	20.0	0.41	3.0
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	0.	100.0	1.0	20.0	0.41	3.7
9.	Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	0.	100.0	1.0	10.0	0.53	5.0
10.	Char/Cam NB TR	*	5383.3	4723.8	5385.0	4612.7	*	111.	179.	AG	0.	100.0	1.0	20.0	0.74	5.6
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5209.4	4740.8	*	93.	271.	AG	0.	100.0	1.0	30.0	0.52	4.7
12.	Sud/Merr SB L	*	6532.7	5210.3	6461.3	5261.1	*	88.	305.	AG	0.	100.0	1.0	10.0	0.95	4.5
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6482.6	5211.5	*	41.	300.	AG	0.	100.0	1.0	30.0	0.21	2.1
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6684.5	5049.5	*	128.	150.	AG	0.	100.0	1.0	30.0	0.73	6.5
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6447.8	5100.4	*	88.	239.	AG	0.	100.0	1.0	40.0	0.52	4.5
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	0.	100.0	1.0	20.0	0.53	4.1
17.	Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6703.4	5223.8	*	98.	249.	AG	0.	100.0	1.0	30.0	0.50	5.0
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	989.	0.0	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1538.	0.0	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1494.	0.0	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1409.	0.0	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	921.	0.0	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1615.	0.0	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1034.	0.0	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1697.	0.0	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	1032.	0.0	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	504.	0.0	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	0.0	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	1075.	0.0	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	0.0	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1457.	0.0	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1759.	0.0	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	992.	0.0	1.0	78.0		

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		*								
1.	Char/Merr SB	*	100	76	3.0	615	1600	0.07	1	3
2.	Char/Merr WB	*	100	79	3.0	517	1600	0.07	1	3
3.	Char/Merr NB R	*	100	52	3.0	257	1600	0.07	1	3
4.	Char/Merr NB LTT	*	100	73	3.0	660	1600	0.07	1	3
5.	Char/Merr EB	*	100	72	3.0	679	1600	0.07	1	3
6.	Char/Cam SB L	*	100	60	3.0	233	1600	0.07	1	3
7.	Char/Cam SB TR	*	100	72	3.0	301	1600	0.07	1	3
8.	Char/Cam WB LTTR	*	100	62	3.0	435	1600	0.07	1	3
9.	Char/Cam NB L	*	100	60	3.0	299	1600	0.07	1	3
10.	Char/Cam NB TR	*	100	72	3.0	543	1600	0.07	1	3

		*								
11.	Char/Cam EB TTTR	*	100	62	3.0	827	1600	0.07	1	3
12.	Sud/Merr SB L	*	100	88	3.0	106	1600	0.07	1	3
13.	Sud/Merr SB TTT	*	100	52	3.0	435	1600	0.07	1	3
14.	Sud/Merr NB TTTR	*	100	64	3.0	1094	1600	0.07	1	3
15.	Sud/Merr EB LTTR	*	100	65	3.0	992	1600	0.07	1	3
16.	Sud/Sur SB LTT	*	100	70	3.0	424	1600	0.07	1	3
17.	Sud/Sur SEB	*	100	80	3.0	37	1600	0.07	1	3
18.	Sud/Sur EB TTR	*	100	50	3.0	1075	1600	0.07	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Char/Merr NE1	*	6063.7	5511.0	6.0
2.	Char/Merr NE2	*	6133.9	5484.8	6.0
3.	Char/Merr NE3	*	6204.2	5458.5	6.0
4.	Char/Merr NE4	*	6265.6	5501.5	6.0
5.	Char/Merr NE5	*	6327.1	5544.5	6.0
6.	Char/Merr SE1	*	6443.7	5491.9	6.0
7.	Char/Merr SE2	*	6382.2	5448.9	6.0
8.	Char/Merr SE3	*	6320.8	5405.9	6.0
9.	Char/Merr SE4	*	6380.5	5360.4	6.0
10.	Char/Merr SE5	*	6440.1	5315.0	6.0
11.	Char/Merr SW1	*	6332.0	5249.0	6.0
12.	Char/Merr SW2	*	6272.3	5294.5	6.0
13.	Char/Merr SW3	*	6212.6	5339.9	6.0
14.	Char/Merr SW4	*	6141.6	5315.8	6.0
15.	Char/Merr SW5	*	6070.6	5291.7	6.0
16.	Char/Merr NW1	*	5902.1	5359.1	6.0
17.	Char/Merr NW2	*	5973.1	5383.2	6.0
18.	Char/Merr NW3	*	6044.1	5407.3	6.0
19.	Char/Merr NW4	*	5973.9	5433.5	6.0
20.	Char/Merr NW5	*	5903.6	5459.8	6.0
21.	Char/Cam NE1	*	5490.2	4963.0	6.0
22.	Char/Cam NE2	*	5459.0	4894.8	6.0
23.	Char/Cam NE3	*	5427.8	4826.6	6.0
24.	Char/Cam NE4	*	5500.4	4807.6	6.0
25.	Char/Cam NE5	*	5572.9	4788.7	6.0
26.	Char/Cam SE1	*	5553.9	4667.5	6.0
27.	Char/Cam SE2	*	5481.3	4686.5	6.0
28.	Char/Cam SE3	*	5408.7	4705.4	6.0
29.	Char/Cam SE4	*	5409.4	4630.4	6.0
30.	Char/Cam SE5	*	5410.1	4555.4	6.0
31.	Char/Cam SW1	*	5312.0	4561.9	6.0
32.	Char/Cam SW2	*	5310.7	4636.9	6.0
33.	Char/Cam SW3	*	5310.7	4711.9	6.0

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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
34.	Char/Cam SW4	*	5235.6	4712.1	6.0
35.	Char/Cam SW5	*	5160.6	4711.9	6.0
36.	Char/Cam NW1	*	5167.9	4822.4	6.0
37.	Char/Cam NW2	*	5242.9	4822.1	6.0
38.	Char/Cam NW3	*	5317.9	4821.9	6.0
39.	Char/Cam NW4	*	5349.1	4890.1	6.0
40.	Char/Cam NW5	*	5380.3	4958.3	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	2.	2.	0.	0.	2.	1.	1.
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	2.	2.	2.	0.	0.	2.	1.	1.
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	2.	3.	2.	2.	0.	1.	2.		

1.	1.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	3.	2.	2.	0.	1.	2.
1.	1.																		
40.	*	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	2.	2.	3.	2.	2.	1.	1.	2.
1.	1.																		
50.	*	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	3.	2.	1.	1.	2.
1.	1.																		
60.	*	0.	0.	1.	1.	1.	0.	0.	1.	0.	0.	2.	2.	2.	2.	2.	1.	2.	2.
1.	1.																		
70.	*	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	2.	2.	3.
2.	1.																		
80.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.
2.	2.																		
90.	*	1.	1.	2.	2.	2.	0.	0.	0.	0.	1.	2.	2.	2.	1.	1.	2.	3.	3.
3.	2.																		
100.	*	1.	1.	2.	2.	1.	0.	0.	0.	0.	1.	2.	3.	2.	1.	1.	3.	3.	3.
3.	3.																		
110.	*	2.	2.	3.	2.	1.	0.	0.	1.	1.	1.	2.	3.	3.	1.	1.	2.	3.	3.
3.	2.																		
120.	*	2.	3.	3.	2.	1.	0.	0.	1.	1.	2.	2.	2.	2.	1.	0.	2.	2.	2.
2.	2.																		
130.	*	3.	3.	4.	3.	1.	0.	1.	2.	2.	3.	1.	1.	1.	0.	0.	2.	2.	2.
1.	1.																		
140.	*	2.	3.	4.	4.	2.	1.	1.	3.	3.	3.	1.	1.	1.	0.	0.	1.	2.	2.
1.	1.																		
150.	*	2.	2.	3.	4.	2.	1.	2.	2.	3.	3.	0.	0.	0.	0.	0.	1.	1.	2.
1.	1.																		
160.	*	2.	2.	3.	4.	2.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	1.	2.	2.
1.	1.																		
170.	*	2.	2.	2.	3.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
180.	*	2.	2.	2.	3.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
190.	*	2.	2.	2.	3.	2.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	2.	1.
1.	1.																		
200.	*	2.	2.	2.	3.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	2.	2.
1.	1.																		
210.	*	2.	3.	2.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	1.	2.	2.
1.	1.																		
220.	*	2.	3.	2.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.
1.	0.																		
230.	*	2.	3.	3.	2.	2.	1.	2.	2.	2.	2.	0.	0.	0.	0.	1.	1.	1.	2.
1.	0.																		
240.	*	1.	2.	3.	2.	2.	2.	2.	2.	2.	2.	0.	0.	1.	1.	0.	1.	1.	1.
0.	0.																		
250.	*	1.	2.	2.	1.	1.	3.	3.	3.	2.	2.	0.	0.	1.	1.	1.	0.	1.	1.
0.	0.																		
260.	*	1.	1.	2.	1.	1.	3.	3.	3.	2.	2.	0.	0.	2.	1.	1.	0.	0.	0.
0.	0.																		
270.	*	1.	1.	2.	1.	0.	2.	3.	4.	3.	3.	0.	1.	2.	2.	2.	0.	0.	0.
0.	0.																		
280.	*	1.	1.	1.	0.	0.	2.	2.	3.	3.	3.	1.	1.	2.	2.	2.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	1.	0.	0.	1.	2.	3.	2.	3.	1.	1.	2.	2.	2.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	0.	0.	0.	1.	1.	2.	2.	2.	1.	2.	2.	2.	2.	2.	0.	1.
1.	0.																		
310.	*	0.	0.	0.	0.	0.	1.	1.	2.	2.	1.	2.	2.	2.	2.	2.	2.	0.	1.
1.	0.																		
320.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	2.	0.	1.
1.	1.																		
330.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	2.	0.	1.
1.	1.																		
340.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	2.	0.	1.
1.	1.																		
350.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	2.	2.	0.	2.
1.	1.																		
360.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	2.	2.	2.	2.	2.	0.	2.
1.	1.																		
MAX	*	3.	3.	4.	4.	3.	3.	3.	4.	3.	3.	2.	3.	3.	3.	2.	3.	3.	3.
3.	3.																		
DEGR.	*	130	130	130	150	210	250	260	270	280	140	90	100	30	50	50	100	90	80
100	100																		

♀

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38
REC39	REC40																		
0.	*	0.	1.	1.	0.	0.	1.	2.	2.	2.	2.	1.	2.	2.	2.	1.	0.	0.	0.
0.	0.																		
10.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	2.	2.	2.	2.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	2.	1.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	2.	2.	3.	3.	1.	0.	0.	1.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	3.	3.	3.	2.	0.	0.	2.
1.	1.																		
50.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.	4.	3.	0.	1.	2.
1.	1.																		
60.	*	1.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	3.	4.	3.	1.	1.	2.
1.	1.																		
70.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	1.	2.
1.	1.																		
80.	*	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.	3.	3.	1.	1.	2.
1.	1.																		
90.	*	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	1.	2.	2.	2.	2.	2.	2.	2.
1.	1.																		
100.	*	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	2.	2.	3.
2.	1.																		
110.	*	0.	0.	1.	1.	1.	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	3.	3.	3.
2.	1.																		
120.	*	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	3.	3.	3.
2.	1.																		
130.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	2.	3.	3.
3.	1.																		
140.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	2.	3.	3.
3.	1.																		
150.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.
3.	2.																		
160.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.
3.	2.																		
170.	*	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.
3.	2.																		
180.	*	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	1.	0.	0.	1.	2.	2.
3.	2.																		
190.	*	1.	1.	2.	1.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
2.	2.																		
200.	*	1.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
2.	2.																		
210.	*	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
1.	1.																		
220.	*	2.	2.	3.	2.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
1.	1.																		
230.	*	2.	2.	3.	2.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.
1.	1.																		
240.	*	2.	2.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
1.	0.																		
250.	*	1.	2.	3.	3.	2.	0.	1.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.
1.	0.																		
260.	*	1.	2.	3.	3.	3.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.
0.	0.																		
270.	*	1.	1.	2.	2.	2.	1.	2.	3.	2.	1.	0.	0.	1.	1.	0.	1.	1.	1.
0.	0.																		
280.	*	1.	1.	2.	2.	2.	2.	2.	3.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.
0.	0.																		
290.	*	1.	1.	1.	1.	1.	2.	2.	4.	2.	1.	0.	0.	3.	2.	1.	0.	0.	0.
0.	0.																		
300.	*	1.	1.	1.	1.	1.	2.	2.	3.	3.	1.	0.	1.	3.	2.	1.	0.	0.	0.
0.	0.																		
310.	*	1.	1.	1.	1.	0.	2.	2.	3.	3.	2.	0.	1.	3.	2.	2.	0.	0.	0.
0.	0.																		
320.	*	1.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
330.	*	1.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	1.	1.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	1.	1.	0.	0.	1.	2.	2.	2.	2.	1.	2.	2.	2.	1.	0.	0.	0.
0.	0.																		
MAX	*	2.	2.	3.	3.	3.	2.	2.	4.	3.	3.	2.	3.	3.	4.	3.	3.	3.	3.
3.	2.																		
DEGR.	*	230	230	250	250	260	300	290	290	320	340	30	40	40	50	70	110	120	110
160	190																		

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC3 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15:41

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6042.8	5450.0	*	73.	290.	AG	0.	100.0	1.0	30.0	0.58	3.7
2. Char/Merr WB	*	6250.4	5435.2	6335.4	5502.4	*	108.	52.	AG	0.	100.0	1.0	30.0	0.75	5.5
3. Char/Merr NB R	*	6291.7	5369.7	6314.8	5354.0	*	28.	124.	AG	0.	100.0	1.0	10.0	0.14	1.4
4. Char/Merr NB LTT	*	6280.4	5347.2	7349.2	4593.4	*	1308.	125.	AG	0.	100.0	1.0	20.0	1.25	66.4
5. Char/Merr EB	*	6104.2	5362.2	6046.8	5340.9	*	61.	250.	AG	0.	100.0	1.0	20.0	0.58	3.1
6. Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.8	*	108.	14.	AG	0.	100.0	1.0	10.0	0.71	5.5
7. Char/Cam SB TR	*	5360.8	4833.5	5403.4	4971.2	*	144.	17.	AG	0.	100.0	1.0	20.0	0.95	7.3
8. Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	0.	100.0	1.0	20.0	0.27	2.2
9. Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	0.	100.0	1.0	10.0	0.60	4.7
10. Char/Cam NB TR	*	5383.3	4723.8	5384.5	4645.8	*	78.	179.	AG	0.	100.0	1.0	20.0	0.74	4.0
11. Char/Cam EB TTTR	*	5302.7	4739.8	5210.5	4740.8	*	92.	271.	AG	0.	100.0	1.0	30.0	0.57	4.7
12. Sud/Merr SB L	*	6532.7	5210.3	6385.1	5315.4	*	181.	305.	AG	0.	100.0	1.0	10.0	1.08	9.2
13. Sud/Merr SB TTT	*	6518.3	5190.8	6484.5	5210.4	*	39.	300.	AG	0.	100.0	1.0	30.0	0.20	2.0
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6678.7	5059.8	*	117.	150.	AG	0.	100.0	1.0	30.0	0.60	5.9
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6472.1	5115.0	*	60.	239.	AG	1.	100.0	1.0	40.0	0.47	3.0
16. Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	0.	100.0	1.0	20.0	0.34	3.3
17. Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6739.6	5238.0	*	59.	249.	AG	0.	100.0	1.0	30.0	0.49	3.0
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	945.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1232.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1619.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1565.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	1016.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1651.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	964.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1759.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	360.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	541.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	420.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1848.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1944.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	579.	0.0	1.0	78.0		

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1. Char/Merr SB	*	100	76	3.0	530	1600	0.07	1	3
2. Char/Merr WB	*	100	74	3.0	757	1600	0.07	1	3
3. Char/Merr NB R	*	100	44	3.0	116	1600	0.07	1	3
4. Char/Merr NB LTT	*	100	70	3.0	1002	1600	0.07	1	3
5. Char/Merr EB	*	100	80	3.0	281	1600	0.07	1	3
6. Char/Cam SB L	*	90	58	3.0	340	1600	0.07	1	3
7. Char/Cam SB TR	*	90	71	3.0	472	1600	0.07	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	294	1600	0.07	1	3
9. Char/Cam NB L	*	90	58	3.0	289	1600	0.07	1	3
10. Char/Cam NB TR	*	90	71	3.0	367	1600	0.07	1	3

11. Char/Cam EB TTTR	*	90	54	3.0	937	1600	0.07	1	3
12. Sud/Merr SB L	*	100	89	3.0	104	1600	0.07	1	3
13. Sud/Merr SB TTT	*	100	41	3.0	524	1600	0.07	1	3
14. Sud/Merr NB TTTR	*	100	52	3.0	1232	1600	0.07	1	3
15. Sud/Merr EB LTTR	*	100	76	3.0	579	1600	0.07	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	455	1600	0.07	1	3
17. Sud/Sur SEB	*	100	70	3.0	26	1600	0.07	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	420	1600	0.07	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Sud/Merr NE1	*	6492.5	5309.9	6.0
2. Sud/Merr NE2	*	6554.8	5268.0	6.0
3. Sud/Merr NE3	*	6616.2	5224.9	6.0
4. Sud/Merr NE4	*	6684.7	5255.3	6.0
5. Sud/Merr NE5	*	6753.3	5285.7	6.0
6. Sud/Merr SE1	*	6792.9	5222.3	6.0
7. Sud/Merr SE2	*	6724.3	5191.9	6.0
8. Sud/Merr SE3	*	6655.7	5161.5	6.0
9. Sud/Merr SE4	*	6695.5	5097.9	6.0
10. Sud/Merr SE5	*	6735.2	5034.3	6.0
11. Sud/Merr SW1	*	6638.6	4981.3	6.0
12. Sud/Merr SW2	*	6598.9	5045.0	6.0
13. Sud/Merr SW3	*	6559.1	5108.6	6.0
14. Sud/Merr SW4	*	6493.4	5072.5	6.0
15. Sud/Merr SW5	*	6427.6	5036.5	6.0
16. Sud/Merr NW1	*	6347.8	5104.5	6.0
17. Sud/Merr NW2	*	6413.5	5140.5	6.0
18. Sud/Merr NW3	*	6479.3	5176.6	6.0
19. Sud/Merr NW4	*	6417.1	5218.5	6.0
20. Sud/Merr NW5	*	6354.9	5260.4	6.0
21. Sud/Sur NE1	*	6755.9	5445.7	6.0
22. Sud/Sur NE2	*	6801.0	5385.7	6.0
23. Sud/Sur NE3	*	6846.0	5325.7	6.0
24. Sud/Sur NE4	*	6908.8	5366.8	6.0
25. Sud/Sur NE5	*	6971.5	5407.9	6.0
26. Sud/Sur SE1	*	7002.4	5368.4	6.0
27. Sud/Sur SE2	*	6939.7	5327.3	6.0
28. Sud/Sur SE3	*	6876.9	5286.2	6.0
29. Sud/Sur SE4	*	6931.7	5235.0	6.0
30. Sud/Sur SE5	*	6986.5	5183.8	6.0
31. Sud/Sur SW1	*	6932.3	5133.1	6.0
32. Sud/Sur SE2	*	6877.5	5184.3	6.0
33. Sud/Sur SE3	*	6822.7	5235.5	6.0

JOB: Government Center Garage RUN: 2028BD

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RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Sud/Sur SE4	*	6754.2	5205.1	6.0
35. Sud/Sur SE5	*	6685.6	5174.8	6.0
36. Sud/Sur NW1	*	6645.5	5237.9	6.0
37. Sud/Sur NW2	*	6714.1	5268.3	6.0
38. Sud/Sur NW3	*	6782.7	5298.7	6.0
39. Sud/Sur NW4	*	6709.5	5315.4	6.0
40. Sud/Sur NW5	*	6636.4	5332.0	6.0
41. Sud/Sur N1	*	6642.4	5493.7	6.0
42. Sud/Sur N2	*	6687.4	5433.7	6.0
43. Sud/Sur N3	*	6732.4	5373.8	6.0
44. Sud/Sur N4	*	6659.3	5390.4	6.0
45. Sud/Sur N5	*	6586.2	5407.1	6.0

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

```
   0.  *    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    3.    3.    3.    3.    2.    1.    2.    3.
3.    3.
  10.  *    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    3.    3.    3.    3.    2.    1.    1.    3.
2.    3.
  20.  *    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    2.    3.    3.    3.    2.    1.    1.    3.
2.    2.
  30.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    2.    3.    3.    2.    2.    1.    1.    3.
2.    2.
  40.  *    0.    0.    0.    0.    0.    1.    2.    1.    0.    0.    2.    2.    3.    2.    2.    1.    1.    3.
2.    2.
  50.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    2.    3.    3.    2.    2.    1.    2.    3.
2.    2.
  60.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    2.    2.    3.    2.    2.    2.    2.    3.
2.    3.
  70.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    2.    2.    3.    2.    1.    2.    2.    3.
2.    3.
  80.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    2.    2.    3.    2.    1.    2.    3.    4.
3.    3.
  90.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    2.    2.    3.    2.    1.    2.    3.    4.
3.    4.
 100.  *    0.    0.    1.    1.    1.    0.    0.    0.    0.    1.    2.    2.    3.    1.    1.    2.    3.    4.
4.    4.
 110.  *    0.    0.    1.    1.    1.    0.    0.    0.    0.    1.    2.    2.    3.    1.    1.    1.    2.    4.
4.    4.
 120.  *    1.    1.    1.    1.    1.    0.    0.    0.    0.    2.    2.    2.    3.    1.    0.    1.    2.    4.
3.    4.
 130.  *    2.    2.    1.    1.    2.    0.    0.    1.    1.    3.    2.    2.    2.    1.    0.    1.    1.    3.
3.    3.
 140.  *    3.    2.    2.    0.    1.    0.    0.    1.    1.    3.    1.    1.    2.    0.    0.    0.    1.    3.
2.    2.
 150.  *    3.    3.    2.    1.    2.    0.    0.    2.    2.    3.    1.    1.    1.    0.    0.    0.    0.    2.
1.    1.
 160.  *    3.    3.    3.    1.    2.    0.    1.    3.    2.    3.    0.    0.    0.    0.    0.    0.    0.    2.
1.    0.
 170.  *    3.    3.    3.    1.    2.    0.    1.    3.    2.    3.    0.    0.    0.    0.    0.    0.    0.    2.
0.    0.
 180.  *    3.    2.    3.    2.    2.    1.    1.    3.    2.    3.    0.    0.    0.    0.    0.    0.    0.    2.
0.    0.
 190.  *    2.    3.    3.    2.    2.    1.    1.    3.    3.    3.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 200.  *    2.    3.    2.    2.    2.    1.    1.    3.    3.    3.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 210.  *    2.    3.    3.    2.    2.    1.    2.    3.    3.    2.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 220.  *    2.    3.    3.    2.    2.    1.    2.    3.    3.    2.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 230.  *    2.    2.    3.    2.    2.    1.    2.    3.    3.    2.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 240.  *    2.    2.    3.    2.    2.    1.    2.    3.    3.    2.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 250.  *    2.    2.    3.    2.    2.    2.    2.    4.    3.    3.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 260.  *    2.    2.    3.    2.    1.    2.    2.    4.    3.    3.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 270.  *    3.    3.    3.    2.    1.    2.    3.    4.    4.    3.    0.    0.    1.    1.    0.    0.    0.    0.
0.    1.
 280.  *    2.    3.    3.    2.    1.    3.    2.    4.    4.    4.    0.    1.    2.    1.    1.    0.    0.    0.
1.    1.
 290.  *    2.    3.    3.    1.    1.    2.    2.    4.    5.    5.    0.    1.    2.    1.    1.    0.    0.    1.
1.    2.
 300.  *    1.    2.    2.    1.    0.    2.    2.    4.    5.    6.    1.    2.    3.    1.    1.    0.    1.    2.
2.    2.
 310.  *    1.    1.    1.    0.    0.    2.    1.    3.    4.    6.    2.    2.    4.    1.    1.    1.    1.    3.
3.    3.
 320.  *    1.    0.    0.    0.    0.    2.    0.    2.    3.    4.    2.    3.    4.    2.    1.    1.    1.    3.
3.    3.
 330.  *    0.    0.    0.    0.    0.    2.    1.    1.    1.    2.    3.    3.    4.    3.    1.    1.    2.    3.
3.    3.
 340.  *    0.    0.    0.    0.    0.    2.    1.    1.    0.    1.    3.    3.    4.    3.    2.    1.    2.    3.
3.    3.
 350.  *    0.    0.    0.    0.    0.    2.    0.    0.    0.    1.    3.    3.    3.    3.    2.    1.    2.    3.
3.    3.
 360.  *    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    3.    3.    3.    3.    2.    1.    2.    3.
3.    3.
------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    3.    3.    3.    2.    2.    3.    3.    4.    5.    6.    3.    3.    4.    3.    2.    2.    3.    4.
4.    4.
 DEGR. *  160   150   170   230   180   280   270   280   290   300   340   330   330     0    40    80    90   110
110   110
```


JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 WIND  * CONCENTRATION
 ANGLE *     (ug/m**3)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38
REC39 REC40

------*-------------------------------------------------------------------------------------------------------------
-------
   0.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    2.    0.    0.    0.    1.
0.    0.
  10.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    2.    1.    0.    0.    0.
0.    0.
  20.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.    0.    0.    0.
0.    0.
  30.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.    0.    0.    0.
0.    0.
  40.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
  50.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
  60.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.
0.    0.
  70.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.
0.    0.
  80.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
0.    0.
  90.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
0.    0.
 100.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    2.
0.    0.
 110.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    2.
0.    0.
 120.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    1.    2.    1.
1.    1.
 130.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.
1.    1.
 140.  *    1.    0.    1.    0.    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.
1.    0.
 150.  *    1.    1.    1.    0.    0.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    1.
 160.  *    1.    1.    1.    1.    0.    0.    0.    1.    1.    1.    0.    0.    0.    0.    1.    2.    1.    1.
1.    1.
 170.  *    2.    1.    1.    1.    0.    0.    0.    1.    1.    1.    0.    0.    0.    1.    2.    2.    1.    1.
1.    1.
 180.  *    2.    1.    1.    1.    0.    0.    0.    1.    1.    1.    0.    0.    0.    1.    2.    2.    1.    2.
1.    2.
 190.  *    2.    1.    1.    1.    1.    0.    0.    1.    1.    1.    0.    0.    1.    1.    2.    2.    2.    2.
1.    1.
 200.  *    2.    2.    1.    1.    1.    0.    1.    1.    1.    1.    0.    1.    1.    1.    2.    2.    2.    2.
1.    1.
 210.  *    2.    2.    2.    1.    1.    1.    1.    1.    1.    1.    0.    1.    1.    1.    2.    2.    2.    2.
1.    2.
 220.  *    1.    2.    2.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    2.    2.    2.    2.
2.    2.
 230.  *    2.    2.    2.    2.    1.    1.    1.    2.    1.    1.    1.    1.    1.    1.    2.    3.    2.    2.
2.    2.
 240.  *    1.    2.    2.    2.    1.    1.    2.    2.    1.    1.    1.    1.    1.    2.    2.    3.    2.    2.
1.    1.
 250.  *    1.    2.    2.    1.    1.    2.    2.    2.    2.    1.    1.    1.    2.    2.    3.    3.    2.    2.
1.    1.
 260.  *    1.    2.    1.    1.    1.    1.    2.    2.    2.    2.    1.    1.    2.    2.    3.    2.    1.    1.
1.    1.
 270.  *    1.    2.    1.    1.    1.    1.    1.    2.    2.    2.    1.    1.    3.    2.    3.    2.    1.    1.
1.    1.
 280.  *    1.    2.    1.    1.    1.    1.    1.    2.    2.    2.    1.    1.    2.    2.    2.    3.    2.    1.
1.    1.
 290.  *    1.    2.    1.    0.    0.    0.    1.    1.    2.    1.    1.    1.    2.    2.    3.    2.    1.    1.
1.    1.
 300.  *    1.    1.    1.    0.    0.    0.    1.    1.    1.    1.    1.    1.    2.    1.    2.    1.    0.    0.
0.    0.
 310.  *    1.    1.    1.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 320.  *    0.    0.    1.    0.    0.    0.    0.    1.    1.    0.    1.    1.    1.    1.    1.    0.    0.    1.
0.    0.
 330.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
0.    0.
 340.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 350.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    2.    0.    0.    0.
0.    0.
 360.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    2.    0.    0.    0.
0.    0.

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    2.    2.    2.    2.    1.    2.    2.    2.    2.    2.    1.    2.    3.    2.    3.    3.    2.    2.
2.    2.
 DEGR. *  190   270   230   240   230   250   240   260   260   270   280   280   270   260   280   240   240   200
```

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	1.	0.	0.
10.	0.	0.	1.	0.	0.
20.	0.	0.	1.	0.	0.
30.	0.	0.	1.	0.	0.
40.	0.	0.	1.	0.	0.
50.	0.	0.	1.	0.	0.
60.	0.	0.	1.	0.	0.
70.	0.	0.	1.	0.	0.
80.	0.	0.	1.	0.	0.
90.	0.	0.	1.	0.	0.
100.	0.	1.	1.	0.	0.
110.	0.	1.	1.	0.	0.
120.	1.	1.	1.	0.	0.
130.	1.	1.	1.	1.	0.
140.	1.	1.	1.	0.	0.
150.	1.	1.	1.	1.	1.
160.	1.	1.	1.	1.	1.
170.	1.	1.	1.	1.	1.
180.	1.	1.	1.	1.	2.
190.	1.	1.	1.	1.	1.
200.	1.	1.	1.	1.	1.
210.	1.	1.	1.	1.	1.
220.	1.	1.	1.	1.	1.
230.	1.	1.	1.	1.	1.
240.	1.	1.	1.	1.	1.
250.	1.	1.	1.	1.	1.
260.	1.	1.	1.	1.	1.
270.	1.	1.	1.	1.	1.
280.	1.	1.	1.	1.	1.
290.	0.	0.	0.	0.	1.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	1.	0.	0.
360.	0.	0.	1.	0.	0.
MAX	1.	1.	1.	1.	2.
DEGR.	190	200	180	190	180

THE HIGHEST CONCENTRATION OF 6. ug/m**3 OCCURRED AT RECEPTOR REC10.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:16: 2

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6030.2	5454.5	*	87.	290.	AG	0.	100.0	1.0	30.0	0.67	4.4
2.	Char/Merr WB	*	6250.4	5435.2	6310.4	5482.7	*	77.	52.	AG	0.	100.0	1.0	30.0	0.67	3.9
3.	Char/Merr NB R	*	6291.7	5369.7	6352.1	5328.7	*	73.	124.	AG	0.	100.0	1.0	10.0	0.37	3.7
4.	Char/Merr NB LTT	*	6280.4	5347.2	6430.9	5241.1	*	184.	125.	AG	0.	100.0	1.0	20.0	0.94	9.4
5.	Char/Merr EB	*	6104.2	5362.2	5936.5	5299.8	*	179.	250.	AG	0.	100.0	1.0	20.0	0.92	9.1
6.	Char/Cam SB L	*	5384.1	4834.2	5402.6	4908.3	*	76.	14.	AG	0.	100.0	1.0	10.0	0.42	3.9
7.	Char/Cam SB TR	*	5360.8	4833.5	5378.3	4889.9	*	59.	17.	AG	0.	100.0	1.0	20.0	0.41	3.0
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	0.	100.0	1.0	20.0	0.41	3.7
9.	Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	0.	100.0	1.0	10.0	0.53	5.0
10.	Char/Cam NB TR	*	5383.3	4723.8	5385.0	4612.7	*	111.	179.	AG	0.	100.0	1.0	20.0	0.74	5.6
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5209.4	4740.8	*	93.	271.	AG	0.	100.0	1.0	30.0	0.52	4.7
12.	Sud/Merr SB L	*	6532.7	5210.3	6461.3	5261.1	*	88.	305.	AG	0.	100.0	1.0	10.0	0.95	4.5
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6482.6	5211.5	*	41.	300.	AG	0.	100.0	1.0	30.0	0.21	2.1
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6684.5	5049.5	*	128.	150.	AG	0.	100.0	1.0	30.0	0.73	6.5
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6447.8	5100.4	*	88.	239.	AG	0.	100.0	1.0	40.0	0.52	4.5
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	0.	100.0	1.0	20.0	0.53	4.1
17.	Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6703.4	5223.8	*	98.	249.	AG	0.	100.0	1.0	30.0	0.50	5.0
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	989.	0.0	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1538.	0.0	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1494.	0.0	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1409.	0.0	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	921.	0.0	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1615.	0.0	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1034.	0.0	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1697.	0.0	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	1032.	0.0	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	504.	0.0	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	0.0	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	1075.	0.0	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	0.0	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1457.	0.0	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1759.	0.0	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	992.	0.0	1.0	78.0		

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		*								
1.	Char/Merr SB	*	100	76	3.0	615	1600	0.07	1	3
2.	Char/Merr WB	*	100	79	3.0	517	1600	0.07	1	3
3.	Char/Merr NB R	*	100	52	3.0	257	1600	0.07	1	3
4.	Char/Merr NB LTT	*	100	73	3.0	660	1600	0.07	1	3
5.	Char/Merr EB	*	100	72	3.0	679	1600	0.07	1	3
6.	Char/Cam SB L	*	100	60	3.0	233	1600	0.07	1	3
7.	Char/Cam SB TR	*	100	72	3.0	301	1600	0.07	1	3
8.	Char/Cam WB LTTR	*	100	62	3.0	435	1600	0.07	1	3
9.	Char/Cam NB L	*	100	60	3.0	299	1600	0.07	1	3
10.	Char/Cam NB TR	*	100	72	3.0	543	1600	0.07	1	3

		*								
11.	Char/Cam EB TTTR	*	100	62	3.0	827	1600	0.07	1	3
12.	Sud/Merr SB L	*	100	88	3.0	106	1600	0.07	1	3
13.	Sud/Merr SB TTT	*	100	52	3.0	435	1600	0.07	1	3
14.	Sud/Merr NB TTTR	*	100	64	3.0	1094	1600	0.07	1	3
15.	Sud/Merr EB LTTR	*	100	65	3.0	992	1600	0.07	1	3
16.	Sud/Sur SB LTT	*	100	70	3.0	424	1600	0.07	1	3
17.	Sud/Sur SEB	*	100	80	3.0	37	1600	0.07	1	3
18.	Sud/Sur EB TTR	*	100	50	3.0	1075	1600	0.07	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Sud/Merr NE1	*	6492.5	5309.9	6.0
2.	Sud/Merr NE2	*	6554.8	5268.0	6.0
3.	Sud/Merr NE3	*	6616.2	5224.9	6.0
4.	Sud/Merr NE4	*	6684.7	5255.3	6.0
5.	Sud/Merr NE5	*	6753.3	5285.7	6.0
6.	Sud/Merr SE1	*	6792.9	5222.3	6.0
7.	Sud/Merr SE2	*	6724.3	5191.9	6.0
8.	Sud/Merr SE3	*	6655.7	5161.5	6.0
9.	Sud/Merr SE4	*	6695.5	5097.9	6.0
10.	Sud/Merr SE5	*	6735.2	5034.3	6.0
11.	Sud/Merr SW1	*	6638.6	4981.3	6.0
12.	Sud/Merr SW2	*	6598.9	5045.0	6.0
13.	Sud/Merr SW3	*	6559.1	5108.6	6.0
14.	Sud/Merr SW4	*	6493.4	5072.5	6.0
15.	Sud/Merr SW5	*	6427.6	5036.5	6.0
16.	Sud/Merr NW1	*	6347.8	5104.5	6.0
17.	Sud/Merr NW2	*	6413.5	5140.5	6.0
18.	Sud/Merr NW3	*	6479.3	5176.6	6.0
19.	Sud/Merr NW4	*	6417.1	5218.5	6.0
20.	Sud/Merr NW5	*	6354.9	5260.4	6.0
21.	Sud/Sur NE1	*	6755.9	5445.7	6.0
22.	Sud/Sur NE2	*	6801.0	5385.7	6.0
23.	Sud/Sur NE3	*	6846.0	5325.7	6.0
24.	Sud/Sur NE4	*	6908.8	5366.8	6.0
25.	Sud/Sur NE5	*	6971.5	5407.9	6.0
26.	Sud/Sur SE1	*	7002.4	5368.4	6.0
27.	Sud/Sur SE2	*	6939.7	5327.3	6.0
28.	Sud/Sur SE3	*	6876.9	5286.2	6.0
29.	Sud/Sur SE4	*	6931.7	5235.0	6.0
30.	Sud/Sur SE5	*	6986.5	5183.8	6.0
31.	Sud/Sur SW1	*	6932.3	5133.1	6.0
32.	Sud/Sur SE2	*	6877.5	5184.3	6.0
33.	Sud/Sur SE3	*	6822.7	5235.5	6.0

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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
34.	Sud/Sur SE4	*	6754.2	5205.1	6.0
35.	Sud/Sur SE5	*	6685.6	5174.8	6.0
36.	Sud/Sur NW1	*	6645.5	5237.9	6.0
37.	Sud/Sur NW2	*	6714.1	5268.3	6.0
38.	Sud/Sur NW3	*	6782.7	5298.7	6.0
39.	Sud/Sur NW4	*	6709.5	5315.4	6.0
40.	Sud/Sur NW5	*	6636.4	5332.0	6.0
41.	Sud/Sur N1	*	6642.4	5493.7	6.0
42.	Sud/Sur N2	*	6687.4	5433.7	6.0
43.	Sud/Sur N3	*	6732.4	5373.8	6.0
44.	Sud/Sur N4	*	6659.3	5390.4	6.0
45.	Sud/Sur N5	*	6586.2	5407.1	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

0.	*	0.	0.	0.	0.	1.	2.	2.	1.	1.	1.	3.	2.	2.	3.	2.	1.	1.	2.
2.	3.																		
10.	*	0.	0.	0.	0.	1.	1.	2.	1.	1.	1.	3.	2.	2.	3.	2.	1.	1.	2.
2.	2.																		
20.	*	0.	0.	0.	0.	0.	1.	2.	1.	1.	0.	2.	2.	2.	3.	2.	1.	1.	2.
2.	2.																		
30.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	2.	2.	3.	2.	2.	1.	1.	2.
2.	2.																		
40.	*	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	2.	2.	3.	2.	3.	1.	1.	2.
2.	2.																		
50.	*	0.	0.	0.	0.	0.	1.	2.	2.	0.	0.	2.	2.	3.	2.	2.	1.	1.	2.
1.	2.																		
60.	*	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	2.	2.	3.
1.	2.																		
70.	*	0.	0.	1.	1.	1.	0.	1.	1.	0.	0.	1.	2.	2.	2.	1.	2.	2.	3.
2.	3.																		
80.	*	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	3.	3.
2.	3.																		
90.	*	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	2.	3.	3.
2.	3.																		
100.	*	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	3.	3.
3.	3.																		
110.	*	1.	1.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	2.	3.	3.
3.	3.																		
120.	*	1.	1.	1.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.	1.	2.	3.
3.	3.																		
130.	*	2.	1.	1.	2.	2.	0.	0.	0.	0.	0.	1.	2.	2.	0.	0.	1.	2.	3.
2.	2.																		
140.	*	2.	2.	2.	1.	2.	0.	0.	1.	0.	0.	1.	1.	2.	0.	0.	1.	2.	2.
2.	2.																		
150.	*	3.	3.	3.	1.	2.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
160.	*	3.	3.	3.	2.	2.	0.	0.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.
1.	1.																		
170.	*	2.	2.	3.	2.	2.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	1.	1.	2.
1.	0.																		
180.	*	2.	2.	3.	2.	2.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	1.	1.	2.
1.	0.																		
190.	*	2.	2.	3.	2.	2.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	1.	1.	2.
0.	0.																		
200.	*	2.	3.	3.	2.	2.	1.	1.	3.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.
0.	0.																		
210.	*	2.	2.	3.	2.	3.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	2.
0.	0.																		
220.	*	2.	2.	3.	2.	2.	1.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
230.	*	2.	2.	3.	3.	2.	1.	2.	3.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
240.	*	2.	2.	3.	2.	2.	2.	2.	3.	2.	1.	0.	0.	1.	0.	0.	1.	1.	1.
0.	0.																		
250.	*	2.	2.	3.	2.	2.	2.	2.	4.	3.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
260.	*	2.	2.	2.	2.	1.	3.	3.	4.	3.	2.	0.	0.	2.	1.	1.	0.	0.	0.
0.	0.																		
270.	*	2.	2.	2.	1.	1.	3.	3.	4.	3.	2.	0.	0.	2.	1.	1.	0.	0.	0.
0.	1.																		
280.	*	2.	2.	2.	1.	1.	3.	3.	4.	4.	2.	0.	1.	2.	1.	1.	0.	0.	1.
1.	1.																		
290.	*	2.	2.	2.	1.	1.	3.	2.	4.	4.	3.	1.	1.	2.	2.	1.	0.	0.	1.
2.	2.																		
300.	*	1.	2.	2.	1.	0.	2.	2.	4.	4.	4.	1.	2.	3.	2.	1.	0.	1.	2.
2.	2.																		
310.	*	1.	1.	1.	0.	0.	2.	2.	3.	4.	4.	1.	2.	3.	2.	1.	1.	1.	3.
3.	3.																		
320.	*	1.	1.	0.	0.	0.	2.	2.	2.	2.	3.	2.	3.	4.	3.	2.	1.	1.	3.
3.	3.																		
330.	*	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	2.	2.	3.	3.	2.	1.	2.	2.
3.	3.																		
340.	*	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.	2.	2.	3.	3.	2.	1.	2.	2.
3.	3.																		
350.	*	0.	0.	0.	0.	1.	2.	2.	1.	1.	1.	2.	2.	3.	3.	2.	1.	2.	2.
3.	3.																		
360.	*	0.	0.	0.	0.	1.	2.	2.	1.	1.	1.	3.	2.	2.	3.	2.	1.	1.	2.
2.	3.																		

MAX	*	3.	3.	3.	3.	3.	3.	3.	4.	4.	4.	3.	3.	4.	3.	3.	2.	3.	3.
3.	3.																		
DEGR.	*	150	160	230	230	210	280	280	280	290	300	10	320	320	340	40	70	80	80
320	100																		

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38
REC39	REC40																		
0.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	2.	2.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	2.	2.	0.	0.	0.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	2.	2.	0.	0.	0.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	2.	0.	0.	0.
0.	0.																		
60.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.
0.	0.																		
70.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
0.	0.																		
80.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	1.	1.
1.	0.																		
90.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	2.	1.
1.	0.																		
100.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	2.	2.	1.
1.	1.																		
110.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	2.	2.	1.
1.	1.																		
120.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	2.	1.
1.	1.																		
130.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	2.	1.
1.	1.																		
140.	*	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	2.	1.
1.	1.																		
150.	*	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	2.	1.
1.	1.																		
160.	*	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	2.	1.
1.	1.																		
170.	*	2.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	2.	1.
2.	1.																		
180.	*	2.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	2.	3.	2.
2.	2.																		
190.	*	2.	2.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	1.	2.	3.	2.
2.	1.																		
200.	*	2.	2.	2.	2.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	2.
2.	1.																		
210.	*	2.	2.	2.	2.	1.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	2.	2.
2.	2.																		
220.	*	2.	2.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.	1.	1.	2.	2.	2.	3.
2.	2.																		
230.	*	2.	2.	2.	2.	2.	1.	1.	2.	1.	1.	0.	1.	1.	1.	2.	3.	2.	2.
2.	1.																		
240.	*	1.	2.	2.	2.	2.	2.	2.	2.	1.	1.	0.	1.	2.	2.	2.	3.	2.	2.
1.	1.																		
250.	*	2.	2.	2.	1.	1.	2.	2.	3.	2.	1.	1.	1.	2.	2.	3.	2.	2.	2.
1.	1.																		
260.	*	1.	2.	1.	1.	1.	2.	2.	3.	2.	2.	1.	1.	3.	3.	3.	2.	1.	1.
1.	1.																		
270.	*	1.	2.	1.	1.	1.	1.	2.	2.	2.	2.	1.	2.	3.	3.	3.	2.	1.	1.
1.	1.																		
280.	*	1.	2.	1.	1.	1.	1.	2.	2.	2.	2.	2.	2.	3.	3.	4.	2.	1.	1.
1.	1.																		
290.	*	1.	2.	1.	1.	0.	1.	2.	2.	2.	1.	1.	2.	2.	3.	3.	2.	1.	1.
1.	1.																		
300.	*	1.	1.	1.	0.	0.	0.	1.	2.	1.	1.	1.	1.	2.	2.	3.	1.	1.	0.
0.	1.																		
310.	*	1.	1.	1.	0.	0.	0.	1.	2.	1.	1.	1.	1.	1.	2.	2.	1.	0.	0.
0.	0.																		
320.	*	0.	1.	1.	0.	0.	0.	1.	2.	1.	1.	1.	1.	1.	2.	1.	0.	0.	1.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
0.	0.																		

MAX	*	2.	2.	2.	2.	2.	2.	2.	3.	2.	2.	2.	2.	3.	3.	4.	3.	2.	3.
2.	2.																		
DEGR.	*	200	270	230	230	230	250	250	250	260	280	280	280	270	280	280	230	190	220

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	1.	0.	0.
10.	0.	0.	1.	0.	0.
20.	0.	0.	1.	0.	0.
30.	0.	0.	1.	0.	0.
40.	0.	0.	1.	0.	0.
50.	0.	0.	1.	0.	0.
60.	0.	0.	1.	0.	0.
70.	0.	0.	1.	0.	0.
80.	0.	1.	1.	1.	0.
90.	0.	1.	1.	1.	0.
100.	0.	1.	1.	1.	0.
110.	1.	1.	1.	1.	0.
120.	1.	1.	1.	0.	0.
130.	1.	1.	1.	1.	0.
140.	1.	1.	1.	1.	0.
150.	1.	1.	1.	1.	1.
160.	0.	1.	1.	1.	1.
170.	1.	1.	1.	1.	1.
180.	1.	1.	1.	1.	1.
190.	1.	1.	1.	1.	1.
200.	1.	1.	1.	1.	1.
210.	1.	1.	1.	1.	1.
220.	1.	1.	1.	1.	1.
230.	1.	1.	1.	1.	1.
240.	1.	1.	1.	1.	1.
250.	1.	1.	1.	1.	1.
260.	1.	1.	1.	1.	1.
270.	1.	1.	1.	1.	1.
280.	1.	1.	1.	1.	1.
290.	1.	0.	1.	1.	1.
300.	1.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	1.	0.	0.
350.	0.	0.	1.	0.	0.
360.	0.	0.	1.	0.	0.
MAX	1.	1.	1.	1.	1.
DEGR.	260	110	200	190	270

THE HIGHEST CONCENTRATION OF 4. ug/m**3 OCCURRED AT RECEPTOR REC9 .

2013 Existing Microscale Output Files (Particulate Matter 2.5 (PM2.5))

JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 5:51

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG TYPE (DEG)	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1. Stan/Lom SB L	*	5194.4	5948.0	5135.6	6035.2	*	105.	326. AG	0.	100.0	1.0	10.0	0.84 5.3
2. Stan/Lom SB TRR	*	5173.5	5937.1	5122.0	6010.9	*	90.	325. AG	0.	100.0	1.0	20.0	0.71 4.6
3. Stan/Lom WB LTT	*	5306.8	5930.3	5403.5	6009.6	*	125.	51. AG	0.	100.0	1.0	20.0	0.87 6.4
4. Stan/Lom WB R	*	5292.4	5947.7	5347.6	5990.1	*	70.	52. AG	0.	100.0	1.0	10.0	0.40 3.5
5. Stan/Lom NB L	*	5307.6	5737.4	5359.5	5721.4	*	54.	107. AG	0.	100.0	1.0	10.0	0.53 2.8
6. Stan/Lom NB TRR	*	5314.4	5765.3	5342.7	5755.7	*	30.	109. AG	0.	100.0	1.0	20.0	0.25 1.5
7. Stan/Lom EB LLT	*	5214.5	5705.3	5200.8	5658.2	*	49.	196. AG	0.	100.0	1.0	20.0	0.44 2.5
8. Stan/Lom EB R	*	5236.5	5698.5	5221.6	5646.0	*	55.	196. AG	0.	100.0	1.0	10.0	0.32 2.8
9. Caus/Wash SB LTTRR	*	6548.6	6868.7	6475.2	7021.0	*	169.	334. AG	0.	100.0	1.0	40.0	0.58 8.6
10. Caus/Wash WB LLTT	*	6635.9	6867.8	6714.6	6936.2	*	104.	49. AG	0.	100.0	1.0	20.0	0.69 5.3
11. Caus/Wash WB R	*	6624.3	6883.3	6687.4	6942.0	*	86.	47. AG	0.	100.0	1.0	10.0	0.28 4.4
12. Caus/Wash NB TTR	*	6603.5	6751.9	6613.9	6519.8	*	232.	177. AG	0.	100.0	1.0	20.0	0.88 11.8
13. Caus/Wash EB LLTTR	*	6538.7	6754.8	6469.9	6706.8	*	84.	235. AG	0.	100.0	1.0	30.0	0.47 4.3
14. Tha/Val SB LTTR	*	6599.0	6224.0	6593.3	6370.2	*	146.	358. AG	0.	100.0	1.0	20.0	0.81 7.4
15. Tha/Val NB L	*	6631.0	6138.6	6630.2	6047.3	*	91.	180. AG	0.	100.0	1.0	10.0	0.55 4.6
16. Tha/Val NB TR	*	6645.6	6138.6	6648.0	6000.5	*	138.	179. AG	0.	100.0	1.0	10.0	0.76 7.0
17. Bev/Was SB TTT	*	6592.9	5963.9	6593.7	6089.2	*	125.	0. AG	0.	100.0	1.0	30.0	0.64 6.4
18. Bev/Was EB RRR	*	6545.9	5954.3	6530.5	5976.1	*	27.	325. AG	0.	100.0	1.0	30.0	0.14 1.4
19. Char/93 SB LLTTRR	*	6587.8	5740.0	6582.8	5870.1	*	130.	358. AG	0.	100.0	1.0	40.0	0.67 6.6
20. Char/93 WB LTT	*	6702.8	5647.8	6712.2	5636.0	*	15.	141. AG	0.	100.0	1.0	20.0	0.10 0.8
21. Char/93 EB TTR	*	6560.8	5622.5	6523.0	5594.9	*	47.	234. AG	0.	100.0	1.0	30.0	0.30 2.4
22. North/Congress SB LT	*	6876.6	4408.9	6860.5	4488.9	*	82.	349. AG	0.	100.0	1.0	30.0	0.62 4.1
23. North/Con WB LLTR	*	6920.6	4378.3	7073.6	4432.5	*	162.	71. AG	0.	100.0	1.0	20.0	0.82 8.2
24. Nor/Con NB LTTTR	*	6914.9	4333.4	6920.4	4292.5	*	41.	172. AG	0.	100.0	1.0	30.0	0.30 2.1
25. Nor/Con EB LTR	*	6869.7	4342.2	6864.6	4340.9	*	5.	256. AG	0.	100.0	1.0	10.0	0.03 0.3
26. Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326. AG	1120.	0.0	1.0	90.0	
27. Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52. AG	1275.	0.0	1.0	78.0	
28. Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111. AG	817.	0.0	1.0	78.0	
29. Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197. AG	1322.	0.0	1.0	78.0	
30. Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334. AG	3211.	0.0	1.0	90.0	
31. Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47. AG	1012.	0.0	1.0	66.0	
32. Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178. AG	2221.	0.0	1.0	90.0	
33. Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234. AG	1162.	0.0	1.0	78.0	
34. Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359. AG	2247.	0.0	1.0	90.0	
35. Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88. AG	91.	0.0	1.0	38.0	
36. Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181. AG	2524.	0.0	1.0	90.0	
37. Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232. AG	280.	0.0	1.0	54.0	
38. Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358. AG	1841.	0.0	1.0	66.0	
39. Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323. AG	269.	0.0	1.0	48.0	
40. Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141. AG	80.	0.0	1.0	42.0	
41. Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138. AG	811.	0.0	1.0	48.0	
42. Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232. AG	374.	0.0	1.0	54.0	
43. Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232. AG	650.	0.0	1.0	54.0	

44. Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145. AG	406.	0.0	1.0	42.0	

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LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG TYPE (DEG)	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45. North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348. AG	1226.	0.0	1.0	98.0	
46. North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70. AG	978.	0.0	1.0	66.0	
47. North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169. AG	1420.	0.0	1.0	98.0	
48. North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258. AG	44.	0.0	1.0	54.0	

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1. Stan/Lom SB L	*	90	70	3.0	223	1600	0.05	1	3
2. Stan/Lom SB TRR	*	90	66	3.0	481	1600	0.05	1	3
3. Stan/Lom WB LTT	*	90	68	3.0	527	1600	0.05	1	3
4. Stan/Lom WB R	*	90	48	3.0	265	1600	0.05	1	3
5. Stan/Lom NB L	*	90	70	3.0	142	1600	0.05	1	3
6. Stan/Lom NB TRR	*	90	66	3.0	166	1600	0.05	1	3
7. Stan/Lom EB LLT	*	90	68	3.0	265	1600	0.05	1	3
8. Stan/Lom EB R	*	90	48	3.0	208	1600	0.05	1	3
9. Caus/Wash SB LTTRR	*	150	56	3.0	2210	1600	0.05	1	3
10. Caus/Wash WB LLTT	*	150	125	3.0	296	1600	0.05	1	3
11. Caus/Wash WB R	*	150	73	3.0	216	1600	0.05	1	3
12. Caus/Wash NB TTR	*	150	108	3.0	693	1600	0.05	1	3
13. Caus/Wash EB LLTTR	*	150	119	3.0	388	1600	0.05	1	3
14. Tha/Val SB LTTR	*	100	34	3.0	1575	1600	0.05	1	3
15. Tha/Val NB L	*	100	66	3.0	253	1600	0.05	1	3
16. Tha/Val NB TR	*	100	34	3.0	743	1600	0.05	1	3
17. Bev/Was SB TTT	*	100	45	3.0	1528	1600	0.05	1	3
18. Bev/Was EB RRR	*	100	55	3.0	269	1600	0.05	1	3
19. Char/93 SB LLTTRR	*	100	53	3.0	1797	1600	0.05	1	3
20. Char/93 WB LTT	*	100	69	3.0	80	1600	0.05	1	3
21. Char/93 EB TTR	*	100	69	3.0	374	1600	0.05	1	3
22. North/Congress SB LT	*	100	75	3.0	598	1600	0.05	1	3
23. North/Con WB LLTR	*	100	60	3.0	916	1600	0.05	1	3
24. Nor/Con NB LTTTR	*	100	74	3.0	306	1600	0.05	1	3
25. Nor/Con EB LTR	*	100	60	3.0	16	1600	0.05	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2. Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3. Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4. Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5. Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6. Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7. Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8. Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9. Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10. Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11. Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12. Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13. Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14. Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15. Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16. Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17. Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18. Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19. Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20. Stan/Lom NW5	*	5136.5	5935.7	6.0	*
21. Caus/Wash NE1	*	6548.3	7035.9	6.0	*
22. Caus/Wash NE2	*	6581.4	6968.6	6.0	*
23. Caus/Wash NE3	*	6614.5	6901.3	6.0	*
24. Caus/Wash NE4	*	6669.8	6952.0	6.0	*
25. Caus/Wash NE5	*	6725.0	7002.7	6.0	*
26. Caus/Wash SE1	*	6753.6	6912.2	6.0	*

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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Caus/Wash SE2	6698.9	6862.0	6.0
28. Caus/Wash SE3	6643.1	6810.8	6.0
29. Caus/Wash SE4	6646.8	6736.4	6.0
30. Caus/Wash SE5	6650.0	6661.0	6.0
31. Caus/Wash SW1	6544.0	6561.0	6.0
32. Caus/Wash SW2	6540.9	6636.0	6.0
33. Caus/Wash SW3	6537.8	6710.9	6.0
34. Caus/Wash SW4	6476.8	6667.2	6.0
35. Caus/Wash SW5	6415.9	6623.4	6.0
36. Caus/Wash NW1	6407.4	6738.0	6.0
37. Caus/Wash NW2	6468.3	6781.7	6.0
38. Caus/Wash NW3	6529.3	6825.4	6.0
39. Caus/Wash NW4	6496.2	6892.7	6.0
40. Caus/Wash NW5	6463.1	6960.0	6.0
41. Tha/Val NE1	6667.3	6395.5	6.0
42. Tha/Val NE2	6668.3	6320.5	6.0
43. Tha/Val NE3	6669.3	6245.5	6.0
44. Tha/Val NE4	6744.3	6245.5	6.0
45. Tha/Val NE5	6819.2	6249.6	6.0
46. Tha/Val SE1	6822.3	6191.6	6.0
47. Tha/Val SE2	6747.3	6189.6	6.0
48. Tha/Val SE3	6672.3	6187.5	6.0
49. Tha/Val SE4	6671.6	6112.5	6.0
50. Tha/Val SE5	6670.9	6037.5	6.0
51. Tha/Val SW1	6560.2	5964.7	6.0
52. Tha/Val SW2	6560.9	6039.7	6.0
53. Tha/Val SW3	6561.6	6114.7	6.0
54. Tha/Val SW4	6502.2	6068.9	6.0
55. Tha/Val SW5	6442.7	6023.2	6.0
56. Tha/Val NW1	6441.0	6115.2	6.0
57. Tha/Val NW2	6500.4	6160.9	6.0
58. Tha/Val NW3	6559.8	6206.7	6.0
59. Tha/Val NW4	6558.8	6281.7	6.0
60. Tha/Val NW5	6557.8	6356.7	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.
10.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
20.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.
30.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.
40.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.
50.	0.	0.	1.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.
60.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	0.	1.	0.	0.	1.	1.	1.	2.	1.
70.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.	1.
80.	0.	0.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.	1.
90.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.	1.
100.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.
110.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
120.	0.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
130.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.
140.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.
150.	1.	1.	1.	2.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
160.	1.	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	3.	2.	1.	0.	1.	3.	3.	2.
10.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	3.	2.	2.	1.	1.	2.	3.	2.
20.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	3.	2.	2.	1.	1.	2.	2.	2.
30.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	3.	2.	1.	1.	2.	2.	2.
40.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.	2.	2.
50.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	1.	1.	2.	2.	2.
60.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	1.	2.	2.	2.	2.
70.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	2.	2.
80.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	2.	2.
90.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	2.	2.	2.	3.	2.
100.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
110.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
120.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
130.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
140.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
150.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
160.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
170.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
180.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
190.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
200.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
210.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
220.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
230.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
240.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
250.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
260.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
270.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
280.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
290.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
300.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
310.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
320.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
330.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
340.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
350.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
360.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	3.	3.
MAX	0.	0.	1.	1.	0.	1.	1.	1.	1.	1.	2.	2.	3.	2.	2.	2.	2.	2.	3.	3.
DEGR.	0	0	70	70	0	60	60	60	60	60	10	10	10	10	10	10	10	10	10	10

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
MAX	1.	1.	2.	2.	2.	1.	2.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	2.	1.
DEGR.	170	170	80	200	210	290	310	330	220	250	320	340	230	330	0	40	40	40	60	70

```
 110. *   0.   1.   1.   1.   0.   0.   0.   0.   0.   0.   1.   1.   1.   1.   1.   2.   2.   2.
3.   3.
 120. *   0.   1.   1.   1.   0.   0.   0.   0.   0.   0.   1.   2.   2.   1.   1.   1.   2.   2.
2.   3.
 130. *   0.   1.   1.   1.   1.   0.   0.   0.   0.   0.   1.   2.   2.   1.   0.   1.   2.   2.
2.   3.
 140. *   1.   1.   1.   1.   1.   0.   0.   0.   0.   0.   1.   2.   2.   1.   1.   1.   2.   2.
2.   3.
 150. *   1.   1.   1.   1.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   2.   2.
2.   2.
 160. *   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   0.   1.   2.   2.
2.   2.
 170. *   3.   3.   2.   2.   1.   0.   0.   1.   1.   1.   2.   2.   2.   1.   0.   1.   2.   2.
2.   1.
 180. *   3.   3.   3.   2.   1.   0.   0.   2.   2.   2.   1.   1.   1.   0.   0.   1.   1.   2.
1.   1.
 190. *   3.   3.   3.   2.   2.   0.   1.   2.   2.   2.   0.   0.   0.   0.   0.   1.   1.   2.
1.   0.
 200. *   3.   3.   3.   2.   2.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   1.   1.   1.
1.   0.
 210. *   2.   2.   3.   2.   2.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   1.   1.   1.
0.   0.
 220. *   2.   2.   3.   2.   2.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   1.   1.   1.
0.   0.
 230. *   2.   2.   2.   2.   2.   2.   2.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   1.
0.   0.
 240. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   2.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 250. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   2.   0.   0.   1.   1.   1.   0.   0.   0.
0.   0.
 260. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   2.   0.   0.   1.   1.   1.   0.   0.   0.
0.   0.
 270. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   2.   0.   0.   1.   1.   1.   0.   0.   0.
0.   0.
 280. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   2.   0.   0.   1.   1.   1.   0.   0.   0.
0.   0.
 290. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   2.   0.   0.   1.   1.   1.   0.   0.   0.
0.   0.
 300. *   2.   2.   2.   1.   0.   2.   2.   3.   2.   2.   0.   0.   1.   1.   1.   0.   0.   0.
0.   0.
 310. *   2.   2.   2.   1.   0.   1.   2.   3.   2.   2.   0.   1.   2.   1.   1.   0.   0.   0.
0.   0.
 320. *   2.   2.   2.   0.   0.   1.   2.   3.   3.   3.   0.   1.   2.   1.   1.   0.   0.   0.
0.   0.
 330. *   1.   1.   2.   0.   0.   0.   1.   3.   3.   3.   1.   1.   2.   1.   1.   0.   0.   1.
1.   1.
 340. *   0.   1.   1.   0.   0.   0.   1.   2.   2.   3.   1.   1.   2.   1.   1.   0.   0.   2.
2.   1.
 350. *   0.   0.   0.   0.   0.   1.   1.   2.   2.   2.   2.   2.   3.   2.   1.   0.   1.   3.
2.   2.
 360. *   0.   0.   0.   0.   0.   1.   1.   1.   1.   1.   2.   2.   3.   2.   1.   0.   1.   3.
3.   2.

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 MAX  *   3.   3.   3.   2.   2.   2.   2.   3.   3.   3.   2.   2.   3.   3.   2.   2.   2.   3.
3.   3.
 DEGR. *  180   180   190   200   210   260   300   320   330   330    10    10     0    30    40   100   140     0
0   120
```



```
1.   1.
  60. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   1.
1.   1.
  70. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   1.
1.   1.
  80. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   2.
1.   1.
  90. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   2.
1.   1.
 100. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   2.
1.   1.
 110. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   1.   1.   1.   1.   1.   2.
1.   1.
 120. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   2.   1.   1.   1.   1.   2.
1.   1.
 130. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   2.   1.   1.   1.   1.   2.
2.   2.
 140. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   2.   1.   1.   1.   1.   2.
2.   2.
 150. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   2.
2.   2.
 160. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   0.   1.   1.   2.
2.   2.
 170. *   0.   0.   1.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   0.   0.   1.   2.
2.   2.
 180. *   1.   1.   2.   0.   0.   0.   0.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   2.
2.   1.
 190. *   2.   2.   2.   1.   0.   0.   0.   2.   2.   1.   1.   1.   1.   0.   0.   0.   0.   1.
1.   1.
 200. *   2.   2.   2.   1.   0.   0.   1.   2.   2.   2.   1.   1.   0.   0.   0.   0.   0.   0.
0.   0.
 210. *   2.   2.   2.   1.   1.   0.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 220. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 230. *   1.   1.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 240. *   1.   1.   2.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 250. *   1.   1.   2.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 260. *   1.   1.   1.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 270. *   1.   1.   1.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 280. *   1.   1.   1.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 290. *   1.   1.   1.   1.   0.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 300. *   1.   1.   1.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 310. *   1.   1.   2.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 320. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 330. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 340. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   3.   1.   0.   1.   0.   0.   0.   0.   0.
0.   1.
 350. *   2.   2.   2.   1.   0.   0.   1.   2.   2.   2.   1.   1.   1.   0.   0.   0.   0.   1.
1.   1.
 360. *   1.   1.   1.   0.   0.   0.   0.   1.   2.   1.   2.   2.   2.   1.   0.   0.   1.   2.
2.   2.

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *   2.   2.   2.   1.   1.   1.   1.   2.   2.   3.   2.   2.   3.   1.   1.   1.   1.   2.
2.   2.
 DEGR. *  340   340   200   220   330   330   340   200   340   340    20    10    10    20    60   130    80   150
160   170
```

THE HIGHEST CONCENTRATION OF   3. ug/m**3 OCCURRED AT RECEPTOR REC28.

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 WIND  * CONCENTRATION
 ANGLE *      (ug/m**3)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52 REC53 REC54 REC55 REC56 REC57 REC58
REC59 REC60

------*-------------------------------------------------------------------------------------------------------------
-------
   0. *   1.   1.   1.   0.   0.   0.   0.   1.   2.   1.   2.   2.   2.   1.   0.   0.   1.   2.
2.   2.
  10. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   2.
2.   2.
  20. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   2.
2.   2.
  30. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   2.
2.   1.
  40. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   2.
2.   1.
  50. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   1.
```

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 6:46

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5135.6	6035.2	*	105.	326.	AG	0.	100.0	1.0	10.0	0.84 5.3
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5122.0	6010.9	*	90.	325.	AG	0.	100.0	1.0	20.0	0.71 4.6
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5403.5	6009.6	*	125.	51.	AG	0.	100.0	1.0	20.0	0.87 6.4
4.	Stan/Lom WB R	*	5292.4	5947.7	5347.6	5990.1	*	70.	52.	AG	0.	100.0	1.0	10.0	0.40 3.5
5.	Stan/Lom NB L	*	5307.6	5737.4	5359.5	5721.4	*	54.	107.	AG	0.	100.0	1.0	10.0	0.53 2.8
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5342.7	5755.7	*	30.	109.	AG	0.	100.0	1.0	20.0	0.25 1.5
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5200.8	5658.2	*	49.	196.	AG	0.	100.0	1.0	20.0	0.44 2.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5221.6	5646.0	*	55.	196.	AG	0.	100.0	1.0	10.0	0.32 2.8
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6475.2	7021.0	*	169.	334.	AG	0.	100.0	1.0	40.0	0.58 8.6
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.6	6936.2	*	104.	49.	AG	0.	100.0	1.0	20.0	0.69 5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6687.4	6942.0	*	86.	47.	AG	0.	100.0	1.0	10.0	0.28 4.4
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6613.9	6519.8	*	232.	177.	AG	0.	100.0	1.0	20.0	0.88 11.8
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6469.9	6706.8	*	84.	235.	AG	0.	100.0	1.0	30.0	0.47 4.3
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.3	6370.2	*	146.	358.	AG	0.	100.0	1.0	20.0	0.81 7.4
15.	Tha/Val NB L	*	6631.0	6138.6	6630.2	6047.3	*	91.	180.	AG	0.	100.0	1.0	10.0	0.55 4.6
16.	Tha/Val NB TR	*	6645.6	6138.6	6648.0	6000.5	*	138.	179.	AG	0.	100.0	1.0	10.0	0.76 7.0
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.7	6089.2	*	125.	0.	AG	0.	100.0	1.0	30.0	0.64 6.4
18.	Bev/Was EB RRR	*	6545.9	5954.3	6530.5	5976.1	*	27.	325.	AG	0.	100.0	1.0	30.0	0.14 1.4
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.8	5870.1	*	130.	358.	AG	0.	100.0	1.0	40.0	0.67 6.6
20.	Char/93 WB LTT	*	6702.8	5647.8	6712.2	5636.0	*	15.	141.	AG	0.	100.0	1.0	20.0	0.10 0.8
21.	Char/93 EB TTR	*	6560.8	5622.5	6523.0	5594.9	*	47.	234.	AG	0.	100.0	1.0	30.0	0.30 2.4
22.	North/Congress SB LT	*	6876.6	4408.9	6860.5	4488.9	*	82.	349.	AG	0.	100.0	1.0	30.0	0.62 4.1
23.	North/Con WB LLTR	*	6920.6	4378.3	7073.6	4432.5	*	162.	71.	AG	0.	100.0	1.0	20.0	0.82 8.2
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6920.4	4292.5	*	41.	172.	AG	0.	100.0	1.0	30.0	0.30 2.1
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.6	4340.9	*	5.	256.	AG	0.	100.0	1.0	10.0	0.03 0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1120.	0.0	1.0	90.0	
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1275.	0.0	1.0	78.0	
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	817.	0.0	1.0	78.0	
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1322.	0.0	1.0	78.0	
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3211.	0.0	1.0	90.0	
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1012.	0.0	1.0	66.0	
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2221.	0.0	1.0	90.0	
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1162.	0.0	1.0	78.0	
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2247.	0.0	1.0	90.0	
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	91.	0.0	1.0	38.0	
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2524.	0.0	1.0	90.0	
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	280.	0.0	1.0	54.0	
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	1841.	0.0	1.0	66.0	
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	269.	0.0	1.0	48.0	
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	80.	0.0	1.0	42.0	
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	811.	0.0	1.0	48.0	
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	374.	0.0	1.0	54.0	
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	650.	0.0	1.0	54.0	

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	406.	0.0	1.0	42.0	

JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 6:46

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1226.	0.0	1.0	98.0	
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	978.	0.0	1.0	66.0	
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1420.	0.0	1.0	98.0	
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	44.	0.0	1.0	54.0	

JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 6:46

	LINK DESCRIPTION	*	X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)
1.	Stan/Lom SB L	*	90	70	3.0	223		1600	0.05		1	3		
2.	Stan/Lom SB TRR	*	90	66	3.0	481		1600	0.05		1	3		
3.	Stan/Lom WB LTT	*	90	68	3.0	527		1600	0.05		1	3		
4.	Stan/Lom WB R	*	90	48	3.0	265		1600	0.05		1	3		
5.	Stan/Lom NB L	*	90	70	3.0	142		1600	0.05		1	3		
6.	Stan/Lom NB TRR	*	90	66	3.0	166		1600	0.05		1	3		
7.	Stan/Lom EB LLT	*	90	68	3.0	265		1600	0.05		1	3		
8.	Stan/Lom EB R	*	90	48	3.0	208		1600	0.05		1	3		
9.	Caus/Wash SB LTTRR	*	150	56	3.0	2210		1600	0.05		1	3		
10.	Caus/Wash WB LLTT	*	150	125	3.0	296		1600	0.05		1	3		
11.	Caus/Wash WB R	*	150	73	3.0	216		1600	0.05		1	3		
12.	Caus/Wash NB TTR	*	150	108	3.0	693		1600	0.05		1	3		
13.	Caus/Wash EB LLTTR	*	150	119	3.0	388		1600	0.05		1	3		
14.	Tha/Val SB LTTR	*	100	34	3.0	1575		1600	0.05		1	3		
15.	Tha/Val NB L	*	100	66	3.0	253		1600	0.05		1	3		
16.	Tha/Val NB TR	*	100	34	3.0	743		1600	0.05		1	3		
17.	Bev/Was SB TTT	*	100	45	3.0	1528		1600	0.05		1	3		
18.	Bev/Was EB RRR	*	100	55	3.0	269		1600	0.05		1	3		
19.	Char/93 SB LLTTRR	*	100	53	3.0	1797		1600	0.05		1	3		
20.	Char/93 WB LTT	*	100	69	3.0	80		1600	0.05		1	3		
21.	Char/93 EB TTR	*	100	69	3.0	374		1600	0.05		1	3		
22.	North/Congress SB LT	*	100	75	3.0	598		1600	0.05		1	3		
23.	North/Con WB LLTR	*	100	60	3.0	916		1600	0.05		1	3		
24.	Nor/Con NB LTTTR	*	100	74	3.0	306		1600	0.05		1	3		
25.	Nor/Con EB LTR	*	100	60	3.0	16		1600	0.05		1	3		

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Bev/Was N1	*	6562.0	6150.2	6.0	*
2.	Bev/Was N2	*	6561.2	6075.2	6.0	*
3.	Bev/Was N3	*	6560.5	6000.2	6.0	*
4.	Bev/Was N4	*	6515.8	6060.4	6.0	*
5.	Bev/Was N5	*	6471.1	6120.6	6.0	*
6.	Bev/Was SE1	*	6671.0	6049.7	6.0	*
7.	Bev/Was SE2	*	6670.2	5966.3	6.0	*
8.	Bev/Was SE3	*	6624.0	5907.2	6.0	*
9.	Bev/Was SE4	*	6626.1	5832.3	6.0	*
10.	Bev/Was SE5	*	6628.1	5757.3	6.0	*
11.	Bev/Was SW1	*	6541.8	5766.9	6.0	*
12.	Bev/Was SW2	*	6540.1	5841.9	6.0	*
13.	Bev/Was SW3	*	6537.7	5916.8	6.0	*
14.	Bev/Was SW4	*	6493.0	5977.0	6.0	*
15.	Bev/Was SW5	*	6448.3	6037.3	6.0	*
16.	Char/93 NE1	*	6625.0	5871.1	6.0	*
17.	Char/93 NE2	*	6627.1	5796.1	6.0	*
18.	Char/93 NE3	*	6629.1	5721.1	6.0	*
19.	Char/93 NE4	*	6699.8	5695.9	6.0	*
20.	Char/93 NE5	*	6750.6	5633.2	6.0	*
21.	Char/93 S1	*	6657.8	5466.0	6.0	*
22.	Char/93 S2	*	6614.7	5527.4	6.0	*
23.	Char/93 S3	*	6571.7	5588.8	6.0	*
24.	Char/93 S4	*	6512.9	5542.2	6.0	*
25.	Char/93 S5	*	6454.1	5495.6	6.0	*
26.	Char/93 NW1	*	6424.1	5632.5	6.0	*

JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 6:46

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Char/93 NW2	6483.6	5678.2	6.0
28. Char/93 NW3	6543.0	5723.9	6.0
29. Char/93 NW4	6541.0	5798.8	6.0
30. Char/93 NW5	6538.9	5873.8	6.0
31. Wash/Cong NE1	6910.2	4571.2	6.0
32. Wash/Cong NE2	6925.8	4497.8	6.0
33. Wash/Cong NE3	6941.4	4424.5	6.0
34. Wash/Cong NE4	7012.0	4449.6	6.0
35. Wash/Cong NE5	7082.7	4474.9	6.0
36. Wash/Cong SE1	7095.4	4388.1	6.0
37. Wash/Cong SE2	7024.8	4362.9	6.0
38. Wash/Cong SE3	6954.1	4337.7	6.0
39. Wash/Cong SE4	6968.4	4264.1	6.0
40. Wash/Cong SE5	6982.7	4190.4	6.0
41. Wash/Cong SW1	6867.5	4164.7	6.0
42. Wash/Cong SW2	6853.3	4238.0	6.0
43. Wash/Cong SW3	6838.9	4312.0	6.0
44. Wash/Cong SW4	6765.6	4296.1	6.0
45. Wash/Cong SW5	6692.3	4280.2	6.0
46. Wash/Cong NW1	6682.4	4353.8	6.0
47. Wash/Cong NW2	6755.7	4369.7	6.0
48. Wash/Cong NW3	6828.9	4386.0	6.0
49. Wash/Cong NW4	6813.3	4459.4	6.0
50. Wash/Cong NW5	6797.8	4532.8	6.0

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	2.	2.	2.	1.	0.	1.	2.	3.	2.	2.	2.	2.	2.	1.	0.	2.	2.	2.	1.	0.
10.	2.	2.	2.	1.	1.	0.	1.	3.	2.	1.	2.	2.	2.	1.	1.	2.	1.	1.	0.	0.
20.	2.	2.	2.	1.	1.	0.	0.	2.	1.	0.	2.	2.	2.	1.	1.	1.	0.	0.	0.	0.
30.	2.	2.	2.	1.	1.	0.	0.	1.	0.	0.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.
40.	2.	2.	2.	1.	1.	0.	0.	1.	0.	0.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.
50.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.
60.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.	0.	0.	0.	0.	0.
70.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.	0.	0.	0.	0.	0.
80.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.	0.	0.	0.	0.	0.
90.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	1.	2.	1.	0.	0.	0.	0.	0.
100.	1.	2.	2.	1.	1.	0.	0.	0.	0.	0.	2.	2.	1.	1.	1.	0.	0.	0.	0.	0.
110.	1.	2.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	1.	0.	0.	0.	0.	0.
120.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	1.	0.	0.	0.	0.	0.
130.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	1.	1.	1.	0.	0.	0.	0.	0.
140.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	0.	0.	0.	0.	0.
150.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.	0.	0.	0.	0.	0.
160.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	0.
170.	2.	2.	2.	1.	1.	0.	0.	0.	0.	0.	1.	1.	2.	0.	0.	1.	0.	1.	1.	0.
180.	2.	2.	2.	1.	0.	1.	0.	1.	1.	0.	0.	1.	1.	0.	0.	1.	0.	0.	1.	0.
190.	1.	1.	1.	0.	0.	1.	1.	2.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.	0.
200.	0.	0.	1.	0.	0.	2.	1.	2.	2.	1.	0.	0.	0.	0.	0.	2.	1.	1.	0.	0.
210.	0.	0.	0.	0.	0.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	1.	0.	0.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	1.	2.	2.	1.	1.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.
10.	1.	1.	2.	2.	1.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
20.	1.	1.	1.	2.	1.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
30.	0.	0.	1.	1.	1.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
40.	0.	0.	0.	1.	1.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
50.	0.	0.	0.	0.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
60.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
70.	0.	0.	0.	0.	0.	1.	1.	1.	2.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
80.	0.	0.	0.	0.	0.	1.	0.	1.	2.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
90.	1.	1.	0.	0.	0.	1.	1.	0.	2.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
100.	1.	1.	1.	0.	0.	1.	1.	0.	2.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
110.	0.	1.	1.	0.	0.	1.	1.	0.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
120.	0.	0.	1.	0.	0.	1.	1.	0.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
130.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
140.	0.	0.	0.	0.	0.	0.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
150.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
160.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
170.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
180.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
190.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
200.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
210.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
220.	0.	0.	0.	0.	0.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	1.	0.	0.
230.	0.	0.	0.	0.	0.	2.	2.	2.	2.	1.	0.	0.	0.	0.	0.	2.	2.	1.	0.	0.
240.	0.	0.	0.	0.	0.	2.	2.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	0.	0.	0.
250.	0.	0.	0.	0.	0.	2.	2.	1.	2.	1.	0.	0.	0.	0.	0.	2.	2.	0.	1.	1.
260.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	2.	2.	0.	0.	1.
270.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	1.	2.	0.	0.	1.
280.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	1.	2.	1.	0.	0.
290.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	1.	2.	1.	0.	0.
300.	1.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	1.	2.	1.	1.	0.
310.	1.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.
320.	1.	1.	0.	0.	0.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	1.	2.	2.	1.	0.
330.	1.	1.	0.	0.	0.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.
340.	1.	1.	0.	0.	0.	3.	2.	3.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.	1.	0.
350.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	1.	1.	1.	0.	0.	3.	2.	2.	1.	0.
360.	2.	2.	2.	1.	0.	1.	2.	3.	2.	2.	2.	2.	2.	1.	0.	2.	2.	2.	1.	0.
MAX	2.	2.	2.	1.	1.	3.	2.	3.	2.	2.	2.	2.	2.	2.	1.	3.	2.	2.	1.	1.
DEGR.	10	10	30	40	70	340	340	350	350	340	20	20	20	90	140	350	340	350	340	340

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

160.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	2.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
170.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
180.	*	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.	1.	1.	0.	0.	1.
1.	1.																		
190.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.
1.	1.																		
200.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.
1.	1.																		
210.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.
1.	1.																		
220.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	2.	0.	0.	1.
1.	1.																		
230.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	2.	0.	0.	1.
1.	1.																		
240.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
1.	1.																		
250.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.
1.	1.																		
260.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
270.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
280.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
290.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	1.
1.	1.																		
300.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
310.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
320.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
330.	*	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.
2.	1.																		
340.	*	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
350.	*	1.	2.	2.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
360.	*	1.	2.	2.	1.	1.	0.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.
1.	0.																		

MAX	*	1.	2.	2.	2.	1.	1.	1.	2.	2.	2.	1.	1.	2.	2.	2.	1.	2.	2.
2.	1.																		
DEGR.	*	0	0	0	10	10	100	20	20	20	20	180	190	190	200	220	280	290	330
330	340																		

JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50
0.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
10.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
20.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
30.	* 1.	2.	1.	0.	0.	0.	0.	1.	1.	1.
40.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
50.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
60.	* 1.	1.	2.	1.	0.	0.	1.	1.	1.	1.
70.	* 1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
80.	* 1.	1.	1.	1.	0.	1.	1.	1.	1.	1.
90.	* 1.	1.	1.	1.	0.	1.	1.	1.	1.	1.
100.	* 1.	1.	1.	0.	0.	0.	1.	1.	2.	1.
110.	* 1.	1.	1.	0.	0.	0.	1.	1.	2.	1.
120.	* 1.	1.	1.	0.	0.	0.	1.	1.	2.	1.
130.	* 1.	1.	1.	0.	0.	0.	0.	1.	2.	1.
140.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	2.
150.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	2.
160.	* 0.	1.	1.	0.	0.	0.	0.	1.	1.	1.
170.	* 0.	0.	0.	0.	0.	0.	0.	1.	0.	1.
180.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
190.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
200.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
210.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
220.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

240.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
250.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
260.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
270.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
280.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
290.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
300.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
310.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
320.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
330.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
340.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
350.	* 1.	1.	1.	0.	0.	0.	0.	0.	0.	0.
360.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.

MAX	* 1.	2.	2.	1.	1.	1.	1.	1.	2.	2.
DEGR.	* 10	30	60	70	70	70	70	90	110	140

THE HIGHEST CONCENTRATION OF 3. ug/m**3 OCCURRED AT RECEPTOR REC8 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 6: 3

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH (G/MI)	EF	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5135.6	6035.1	*	105.	326.	AG	0.	100.0	1.0	10.0	0.81	5.3
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5086.9	6061.1	*	151.	325.	AG	0.	100.0	1.0	20.0	0.88	7.7
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5356.6	5971.2	*	64.	51.	AG	0.	100.0	1.0	20.0	0.43	3.3
4.	Stan/Lom WB R	*	5292.4	5947.7	5467.2	6081.9	*	220.	52.	AG	0.	100.0	1.0	10.0	1.01	11.2
5.	Stan/Lom NB L	*	5307.6	5737.4	5334.8	5729.0	*	29.	107.	AG	0.	100.0	1.0	10.0	0.26	1.4
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5348.1	5753.9	*	36.	109.	AG	0.	100.0	1.0	20.0	0.26	1.8
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5194.5	5636.4	*	72.	196.	AG	0.	100.0	1.0	20.0	0.48	3.6
8.	Stan/Lom EB R	*	5236.5	5698.5	5057.8	5069.3	*	654.	196.	AG	0.	100.0	1.0	10.0	1.17	33.2
9.	Char/93 SB LLTTRR	*	6587.8	5740.0	6583.0	5866.1	*	126.	358.	AG	0.	100.0	1.0	40.0	0.70	6.4
10.	Char/93 WB LTT	*	6702.8	5647.8	6733.3	5609.6	*	49.	141.	AG	0.	100.0	1.0	20.0	0.27	2.5
11.	Char/93 EB TTR	*	6560.8	5622.5	6480.8	5564.0	*	99.	234.	AG	0.	100.0	1.0	30.0	0.54	5.0
12.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1289.	0.0	1.0	90.0		
13.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1112.	0.0	1.0	78.0		
14.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	999.	0.0	1.0	78.0		
15.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1207.	0.0	1.0	78.0		
16.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	1635.	0.0	1.0	66.0		
17.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	298.	0.0	1.0	42.0		
18.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	847.	0.0	1.0	48.0		
19.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	908.	0.0	1.0	54.0		
20.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	449.	0.0	1.0	54.0		
21.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	314.	0.0	1.0	42.0		

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JOB: Government Center Garage RUN: Existing

DATE : 7/19/13
TIME : 16: 6: 3

		*								
1.	Stan/Lom SB L	*	100	79	3.0	208	1600	0.05	1	3
2.	Stan/Lom SB TRR	*	100	74	3.0	595	1600	0.05	1	3
3.	Stan/Lom WB LTT	*	100	71	3.0	332	1600	0.05	1	3
4.	Stan/Lom WB R	*	100	79	3.0	259	1600	0.05	1	3
5.	Stan/Lom NB L	*	100	79	3.0	66	1600	0.05	1	3
6.	Stan/Lom NB TRR	*	100	74	3.0	176	1600	0.05	1	3
7.	Stan/Lom EB LLT	*	100	71	3.0	371	1600	0.05	1	3
8.	Stan/Lom EB R	*	100	79	3.0	300	1600	0.05	1	3
9.	Char/93 SB LLTTRR	*	100	62	3.0	1488	1600	0.05	1	3
10.	Char/93 WB LTT	*	100	60	3.0	298	1600	0.05	1	3
11.	Char/93 EB TTR	*	100	60	3.0	908	1600	0.05	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8.	Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0	*

		*			
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0 *
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0 *
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0 *
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0 *
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0 *
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0 *
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0 *
21.	Char/93 NE1	*	6625.0	5871.1	6.0 *
22.	Char/93 NE2	*	6627.1	5796.1	6.0 *
23.	Char/93 NE3	*	6629.1	5721.1	6.0 *
24.	Char/93 NE4	*	6699.8	5695.9	6.0 *
25.	Char/93 NE5	*	6750.6	5633.2	6.0 *
26.	Char/93 S1	*	6657.8	5466.0	6.0 *
27.	Char/93 S2	*	6614.7	5527.4	6.0 *
28.	Char/93 S3	*	6571.7	5588.8	6.0 *
29.	Char/93 S4	*	6512.9	5542.2	6.0 *
30.	Char/93 S5	*	6454.1	5495.6	6.0 *
31.	Char/93 NW1	*	6424.1	5632.5	6.0 *
32.	Char/93 NW2	*	6483.6	5678.2	6.0 *
33.	Char/93 NW3	*	6543.0	5723.9	6.0 *
34.	Char/93 NW4	*	6541.0	5798.8	6.0 *
35.	Char/93 NW5	*	6538.9	5873.8	6.0 *

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JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	2.	0.	0.	1.	1.
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	1.	1.
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
60.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	2.
70.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.
80.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.
90.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.
100.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.
110.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
120.	*	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.
130.	*	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.
140.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.
150.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.
160.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.
170.	*	1.	1.	1.	2.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
180.	*	1.	1.	1.	2.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
190.	*	1.	1.	2.	2.	1.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.
200.	*	1.	1.	1.	2.	2.	1.	1.	1.	1.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.
210.	*	1.	1.	1.	1.	2.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.
220.	*	1.	1.	1.	1.	1.	0.	1.	1.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
230.	*	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.
240.	*	1.	1.	1.	0.	1.	1.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.

```
0.    0.
 250. *    1.    1.    1.    0.    0.    1.    0.    0.    1.    1.    0.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 260. *    1.    1.    1.    1.    0.    1.    1.    0.    1.    1.    0.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 270. *    1.    1.    1.    1.    0.    1.    1.    0.    0.    1.    0.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 280. *    1.    1.    1.    1.    0.    1.    1.    0.    0.    1.    0.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 290. *    1.    1.    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 300. *    1.    1.    1.    0.    0.    2.    1.    0.    0.    1.    1.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 310. *    1.    1.    1.    0.    0.    1.    2.    1.    1.    1.    1.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 320. *    0.    1.    1.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 330. *    0.    0.    0.    0.    0.    1.    1.    2.    1.    1.    1.    1.    1.    1.    1.    0.    0.    0.
1.    1.
 340. *    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    2.    2.    0.    0.    1.
1.    1.
 350. *    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    2.    2.    0.    0.    1.
1.    1.
 360. *    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    1.    2.    0.    0.    1.
1.    1.

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    1.    1.    2.    2.    2.    2.    2.    2.    1.    1.    1.    1.    1.    2.    2.    1.    1.    1.
2.    2.
 DEGR. *  170   180   190   190   200   300   310   330   210   240   320   330   220   350     0    70   110   170
60    80
```


JOB: Government Center Garage RUN: Existing

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35
0.	0.	0.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.	0.	0.
10.	0.	0.	0.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.	1.	0.
20.	0.	0.	0.	0.	0.	1.	1.	1.	2.	1.	0.	0.	2.	1.	0.
30.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	2.	2.	0.
40.	0.	0.	0.	0.	0.	1.	1.	0.	1.	1.	0.	1.	2.	2.	1.
50.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	2.	2.	1.
60.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	1.	2.	1.
70.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	0.	1.	2.	1.
80.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	0.	1.	2.	1.
90.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	0.	2.	1.
100.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	0.	2.	1.
110.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	2.	2.
120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	2.	2.
130.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.
140.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.
150.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.
160.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.
170.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
180.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
190.	2.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
200.	2.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
210.	2.	2.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
220.	2.	2.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	2.	2.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
240.	2.	2.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
250.	2.	2.	0.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
260.	2.	2.	0.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
270.	1.	2.	0.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
280.	1.	2.	1.	0.	1.	0.	1.	2.	1.	0.	0.	0.	0.	0.	0.
290.	1.	2.	1.	1.	1.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.
300.	1.	2.	1.	1.	1.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.
310.	1.	2.	2.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.
320.	1.	2.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.
330.	0.	2.	2.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.
340.	0.	1.	2.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.
350.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.
360.	0.	0.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.	0.	0.
MAX	2.	2.	2.	1.	1.	1.	1.	2.	2.	1.	1.	1.	2.	2.	2.
DEGR.	210	220	320	240	250	340	0	280	20	30	110	140	30	120	150

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17: 9:27

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6054.9	5445.6	*	60.	290.	AG	0.	100.0	1.0	30.0	0.48	3.1
2. Char/Merr WB	*	6250.4	5435.2	6323.7	5493.2	*	93.	52.	AG	0.	100.0	1.0	30.0	0.71	4.7
3. Char/Merr NB R	*	6291.7	5369.7	6313.9	5354.6	*	27.	124.	AG	0.	100.0	1.0	10.0	0.14	1.4
4. Char/Merr NB LTT	*	6280.4	5347.2	6395.2	5266.3	*	140.	125.	AG	0.	100.0	1.0	20.0	0.83	7.1
5. Char/Merr EB	*	6104.2	5362.2	6064.9	5347.6	*	42.	250.	AG	0.	100.0	1.0	20.0	0.38	2.1
6. Char/Cam SB L	*	5384.1	4834.2	5408.6	4932.0	*	101.	14.	AG	0.	100.0	1.0	10.0	0.66	5.1
7. Char/Cam SB TR	*	5360.8	4833.5	5392.6	4936.4	*	108.	17.	AG	0.	100.0	1.0	20.0	0.86	5.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5448.9	4784.7	*	39.	103.	AG	0.	100.0	1.0	20.0	0.24	2.0
9. Char/Cam NB L	*	5363.0	4722.4	5361.1	4639.9	*	82.	181.	AG	0.	100.0	1.0	10.0	0.54	4.2
10. Char/Cam NB TR	*	5383.3	4723.8	5384.3	4657.5	*	66.	179.	AG	0.	100.0	1.0	20.0	0.67	3.4
11. Char/Cam EB TTTR	*	5302.7	4739.8	5222.9	4740.6	*	80.	271.	AG	0.	100.0	1.0	30.0	0.49	4.1
12. Sud/Merr SB L	*	6532.7	5210.3	6493.6	5238.2	*	48.	305.	AG	0.	100.0	1.0	10.0	0.66	2.4
13. Sud/Merr SB TTT	*	6518.3	5190.8	6480.9	5212.4	*	43.	300.	AG	0.	100.0	1.0	30.0	0.22	2.2
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6669.4	5076.1	*	98.	150.	AG	0.	100.0	1.0	30.0	0.55	5.0
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6482.0	5121.0	*	48.	239.	AG	0.	100.0	1.0	40.0	0.34	2.5
16. Sud/Sur SB LTT	*	6777.5	5369.7	6741.1	5415.5	*	59.	322.	AG	0.	100.0	1.0	20.0	0.30	3.0
17. Sud/Sur SEB	*	6757.2	5330.0	6747.9	5332.3	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6750.6	5242.3	*	47.	249.	AG	0.	100.0	1.0	30.0	0.39	2.4
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	802.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1038.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1204.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	870.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	923.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1472.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	877.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1546.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	285.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	483.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	405.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	338.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	25.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1421.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1512.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	487.	0.0	1.0	78.0		

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1. Char/Merr SB	*	100	76	3.0	436	1600	0.05	1	3
2. Char/Merr WB	*	100	76	3.0	650	1600	0.05	1	3
3. Char/Merr NB R	*	100	45	3.0	109	1600	0.05	1	3
4. Char/Merr NB LTT	*	100	71	3.0	637	1600	0.05	1	3
5. Char/Merr EB	*	100	79	3.0	194	1600	0.05	1	3
6. Char/Cam SB L	*	90	58	3.0	318	1600	0.05	1	3
7. Char/Cam SB TR	*	90	71	3.0	429	1600	0.05	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	265	1600	0.05	1	3
9. Char/Cam NB L	*	90	58	3.0	260	1600	0.05	1	3
10. Char/Cam NB TR	*	90	71	3.0	330	1600	0.05	1	3

11. Char/Cam EB TTTR	*	90	54	3.0	811	1600	0.05	1	3
12. Sud/Merr SB L	*	100	86	3.0	95	1600	0.05	1	3
13. Sud/Merr SB TTT	*	100	49	3.0	484	1600	0.05	1	3
14. Sud/Merr NB TTTR	*	100	63	3.0	854	1600	0.05	1	3
15. Sud/Merr EB LTTR	*	100	73	3.0	487	1600	0.05	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	405	1600	0.05	1	3
17. Sud/Sur SEB	*	100	70	3.0	25	1600	0.05	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	338	1600	0.05	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Char/Merr NE1	*	6063.7	5511.0	6.0	*
2. Char/Merr NE2	*	6133.9	5484.8	6.0	*
3. Char/Merr NE3	*	6204.2	5458.5	6.0	*
4. Char/Merr NE4	*	6265.6	5501.5	6.0	*
5. Char/Merr NE5	*	6327.1	5544.5	6.0	*
6. Char/Merr SE1	*	6443.7	5491.9	6.0	*
7. Char/Merr SE2	*	6382.2	5448.9	6.0	*
8. Char/Merr SE3	*	6320.8	5405.9	6.0	*
9. Char/Merr SE4	*	6380.5	5360.4	6.0	*
10. Char/Merr SE5	*	6440.1	5315.0	6.0	*
11. Char/Merr SW1	*	6332.0	5249.0	6.0	*
12. Char/Merr SW2	*	6272.3	5294.5	6.0	*
13. Char/Merr SW3	*	6212.6	5339.9	6.0	*
14. Char/Merr SW4	*	6141.6	5315.8	6.0	*
15. Char/Merr SW5	*	6070.6	5291.7	6.0	*
16. Char/Merr NW1	*	5902.1	5359.1	6.0	*
17. Char/Merr NW2	*	5973.1	5383.2	6.0	*
18. Char/Merr NW3	*	6044.1	5407.3	6.0	*
19. Char/Merr NW4	*	5973.9	5433.5	6.0	*
20. Char/Merr NW5	*	5903.6	5459.8	6.0	*
21. Char/Cam NE1	*	5490.2	4963.0	6.0	*
22. Char/Cam NE2	*	5459.0	4894.8	6.0	*
23. Char/Cam NE3	*	5427.8	4826.6	6.0	*
24. Char/Cam NE4	*	5500.4	4807.6	6.0	*
25. Char/Cam NE5	*	5572.9	4788.7	6.0	*
26. Char/Cam SE1	*	5553.9	4667.5	6.0	*
27. Char/Cam SE2	*	5481.3	4686.5	6.0	*
28. Char/Cam SE3	*	5408.7	4705.4	6.0	*
29. Char/Cam SE4	*	5409.4	4630.4	6.0	*
30. Char/Cam SE5	*	5410.1	4555.4	6.0	*
31. Char/Cam SW1	*	5312.0	4561.9	6.0	*
32. Char/Cam SW2	*	5310.7	4636.9	6.0	*
33. Char/Cam SW3	*	5310.7	4711.9	6.0	*

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RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
34. Char/Cam SW4	*	5235.6	4712.1	6.0	*
35. Char/Cam SW5	*	5160.6	4711.9	6.0	*
36. Char/Cam NW1	*	5167.9	4822.4	6.0	*
37. Char/Cam NW2	*	5242.9	4822.1	6.0	*
38. Char/Cam NW3	*	5317.9	4821.9	6.0	*
39. Char/Cam NW4	*	5349.1	4890.1	6.0	*
40. Char/Cam NW5	*	5380.3	4958.3	6.0	*

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.		

0.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
60.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	2.
1.	0.																		
70.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.
1.	1.																		
80.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.
1.	1.																		
90.	*	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.
1.	1.																		
100.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
110.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
120.	*	1.	1.	2.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
130.	*	1.	2.	2.	2.	1.	0.	0.	1.	1.	2.	1.	1.	1.	0.	0.	0.	0.	1.
0.	0.																		
140.	*	1.	1.	2.	2.	1.	0.	1.	1.	2.	2.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
150.	*	1.	1.	2.	2.	1.	0.	1.	1.	1.	2.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
160.	*	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
170.	*	1.	1.	1.	2.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
180.	*	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
190.	*	1.	1.	1.	1.	2.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
200.	*	1.	1.	1.	1.	2.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
210.	*	1.	1.	1.	1.	2.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
220.	*	1.	1.	1.	1.	2.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
230.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
240.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
250.	*	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
260.	*	0.	1.	1.	0.	0.	2.	2.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
270.	*	0.	0.	1.	0.	0.	1.	2.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		

MAX	*	1.	2.	2.	2.	2.	2.	2.	2.	2.	2.	1.	1.	2.	1.	1.	1.	1.	2.
1.	1.																		
DEGR.	*	120	130	130	150	210	260	260	270	140	140	350	10	30	40	40	80	100	80
90	90																		

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38

REC39 REC40

0.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	1.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	2.	2.	1.	0.	0.	1.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	1.	0.	0.	1.
1.	0.																		
50.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.
1.	1.																		
60.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	2.	0.	1.	1.
1.	1.																		
70.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	2.	0.	1.	1.
1.	1.																		
80.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	2.	1.	1.	1.
1.	0.																		
90.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	1.	1.	1.
1.	1.																		
100.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	2.
1.	0.																		
110.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	2.	2.	2.
1.	1.																		
120.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	2.	2.	2.
2.	1.																		
130.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	2.	2.
2.	1.																		
140.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	2.	2.
2.	1.																		
150.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.
2.	1.																		
160.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.
2.	2.																		
170.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
2.	2.																		
180.	*	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
2.	2.																		
190.	*	0.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	2.																		
200.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
210.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
220.	*	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
230.	*	1.	2.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	0.																		
240.	*	1.	2.	2.	2.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
250.	*	1.	1.	2.	2.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
260.	*	1.	1.	2.	2.	1.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
270.	*	0.	1.	1.	1.	2.	1.	1.	2.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	1.	1.	1.	1.	1.	1.	2.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.
0.	0.																		
290.	*	0.	1.	1.	1.	1.	1.	1.	2.	1.	0.	0.	0.	2.	1.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	1.	1.	1.	0.	1.	2.	2.	1.	1.	0.	0.	2.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	1.	2.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	1.	0.	0.	1.	1.	2.	2.	1.	0.	1.	2.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	1.	0.	0.	1.	1.	2.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	1.	0.	0.	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		

MAX	*	1.	2.	2.	2.	2.	1.	2.	2.	2.	1.	1.	2.	2.	2.	2.	2.	2.	2.
2.	2.																		
DEGR.	*	220	230	240	260	270	290	300	290	340	330	20	30	30	50	70	110	110	120
150	180																		

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC34.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17: 9:12

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6042.2	5450.2	*	74.	290.	AG	0.	100.0	1.0	30.0	0.56	3.8
2. Char/Merr WB	*	6250.4	5435.2	6300.3	5474.7	*	64.	52.	AG	0.	100.0	1.0	30.0	0.55	3.2
3. Char/Merr NB R	*	6291.7	5369.7	6341.8	5335.7	*	61.	124.	AG	0.	100.0	1.0	10.0	0.31	3.1
4. Char/Merr NB LTT	*	6280.4	5347.2	6349.1	5298.8	*	84.	125.	AG	0.	100.0	1.0	20.0	0.52	4.3
5. Char/Merr EB	*	6104.2	5362.2	6005.8	5325.6	*	105.	250.	AG	0.	100.0	1.0	20.0	0.81	5.3
6. Char/Cam SB L	*	5384.1	4834.2	5401.1	4902.3	*	70.	14.	AG	0.	100.0	1.0	10.0	0.38	3.6
7. Char/Cam SB TR	*	5360.8	4833.5	5374.3	4877.1	*	46.	17.	AG	0.	100.0	1.0	20.0	0.32	2.3
8. Char/Cam WB LTTR	*	5411.0	4793.5	5475.3	4778.6	*	66.	103.	AG	0.	100.0	1.0	20.0	0.37	3.4
9. Char/Cam NB L	*	5363.0	4722.4	5361.0	4631.8	*	91.	181.	AG	0.	100.0	1.0	10.0	0.49	4.6
10. Char/Cam NB TR	*	5383.3	4723.8	5384.8	4624.7	*	99.	179.	AG	0.	100.0	1.0	20.0	0.68	5.0
11. Char/Cam EB TTTR	*	5302.7	4739.8	5220.6	4740.7	*	82.	271.	AG	0.	100.0	1.0	30.0	0.46	4.2
12. Sud/Merr SB L	*	6532.7	5210.3	6496.1	5236.4	*	45.	305.	AG	0.	100.0	1.0	10.0	0.56	2.3
13. Sud/Merr SB TTT	*	6518.3	5190.8	6487.3	5208.8	*	36.	300.	AG	0.	100.0	1.0	30.0	0.18	1.8
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6672.2	5071.1	*	104.	150.	AG	0.	100.0	1.0	30.0	0.62	5.3
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6458.9	5107.1	*	75.	239.	AG	0.	100.0	1.0	40.0	0.52	3.8
16. Sud/Sur SB LTT	*	6777.5	5369.7	6739.2	5418.0	*	62.	322.	AG	0.	100.0	1.0	20.0	0.40	3.1
17. Sud/Sur SEB	*	6757.2	5330.0	6742.4	5333.7	*	15.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6722.2	5231.2	*	78.	249.	AG	0.	100.0	1.0	30.0	0.39	3.9
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	818.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1226.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1219.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	859.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	796.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1264.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	954.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1198.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	805.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	405.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	322.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	853.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	35.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1185.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1465.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	766.	0.0	1.0	78.0		

DATE : 8/ 7/13
TIME : 17: 9:12

	*								
1. Char/Merr SB	*	100	75	3.0	541	1600	0.05	1	3
2. Char/Merr WB	*	100	78	3.0	449	1600	0.05	1	3
3. Char/Merr NB R	*	100	46	3.0	241	1600	0.05	1	3
4. Char/Merr NB LTT	*	100	68	3.0	452	1600	0.05	1	3
5. Char/Merr EB	*	100	79	3.0	417	1600	0.05	1	3
6. Char/Cam SB L	*	100	60	3.0	214	1600	0.05	1	3
7. Char/Cam SB TR	*	100	72	3.0	233	1600	0.05	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	391	1600	0.05	1	3
9. Char/Cam NB L	*	100	60	3.0	276	1600	0.05	1	3
10. Char/Cam NB TR	*	100	72	3.0	503	1600	0.05	1	3

	*								
11. Char/Cam EB TTTR	*	100	62	3.0	726	1600	0.05	1	3
12. Sud/Merr SB L	*	100	84	3.0	98	1600	0.05	1	3
13. Sud/Merr SB TTT	*	100	50	3.0	394	1600	0.05	1	3
14. Sud/Merr NB TTTR	*	100	66	3.0	863	1600	0.05	1	3
15. Sud/Merr EB LTTR	*	100	72	3.0	766	1600	0.05	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	322	1600	0.05	1	3
17. Sud/Sur SEB	*	100	80	3.0	35	1600	0.05	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	853	1600	0.05	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Char/Merr NE1	*	6063.7	5511.0	6.0	*
2. Char/Merr NE2	*	6133.9	5484.8	6.0	*
3. Char/Merr NE3	*	6204.2	5458.5	6.0	*
4. Char/Merr NE4	*	6265.6	5501.5	6.0	*
5. Char/Merr NE5	*	6327.1	5544.5	6.0	*
6. Char/Merr SE1	*	6443.7	5491.9	6.0	*
7. Char/Merr SE2	*	6382.2	5448.9	6.0	*
8. Char/Merr SE3	*	6320.8	5405.9	6.0	*
9. Char/Merr SE4	*	6380.5	5360.4	6.0	*
10. Char/Merr SE5	*	6440.1	5315.0	6.0	*
11. Char/Merr SW1	*	6332.0	5249.0	6.0	*
12. Char/Merr SW2	*	6272.3	5294.5	6.0	*
13. Char/Merr SW3	*	6212.6	5339.9	6.0	*
14. Char/Merr SW4	*	6141.6	5315.8	6.0	*
15. Char/Merr SW5	*	6070.6	5291.7	6.0	*
16. Char/Merr NW1	*	5902.1	5359.1	6.0	*
17. Char/Merr NW2	*	5973.1	5383.2	6.0	*
18. Char/Merr NW3	*	6044.1	5407.3	6.0	*
19. Char/Merr NW4	*	5973.9	5433.5	6.0	*
20. Char/Merr NW5	*	5903.6	5459.8	6.0	*
21. Char/Cam NE1	*	5490.2	4963.0	6.0	*
22. Char/Cam NE2	*	5459.0	4894.8	6.0	*
23. Char/Cam NE3	*	5427.8	4826.6	6.0	*
24. Char/Cam NE4	*	5500.4	4807.6	6.0	*
25. Char/Cam NE5	*	5572.9	4788.7	6.0	*
26. Char/Cam SE1	*	5553.9	4667.5	6.0	*
27. Char/Cam SE2	*	5481.3	4686.5	6.0	*
28. Char/Cam SE3	*	5408.7	4705.4	6.0	*
29. Char/Cam SE4	*	5409.4	4630.4	6.0	*
30. Char/Cam SE5	*	5410.1	4555.4	6.0	*
31. Char/Cam SW1	*	5312.0	4561.9	6.0	*
32. Char/Cam SW2	*	5310.7	4636.9	6.0	*
33. Char/Cam SW3	*	5310.7	4711.9	6.0	*

DATE : 8/ 7/13
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RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
34. Char/Cam SW4	*	5235.6	4712.1	6.0	*
35. Char/Cam SW5	*	5160.6	4711.9	6.0	*
36. Char/Cam NW1	*	5167.9	4822.4	6.0	*
37. Char/Cam NW2	*	5242.9	4822.1	6.0	*
38. Char/Cam NW3	*	5317.9	4821.9	6.0	*
39. Char/Cam NW4	*	5349.1	4890.1	6.0	*
40. Char/Cam NW5	*	5380.3	4958.3	6.0	*

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.		

0.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	0.	1.	1.
0.	0.																		
60.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
1.	0.																		
70.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.
1.	1.																		
80.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.
1.	1.																		
90.	*	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.
1.	1.																		
100.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
110.	*	1.	1.	2.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	2.
1.	1.																		
120.	*	1.	1.	2.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
130.	*	1.	2.	2.	1.	1.	0.	0.	1.	1.	2.	1.	1.	1.	0.	0.	0.	1.	1.
1.	0.																		
140.	*	1.	1.	2.	2.	1.	0.	1.	1.	1.	2.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
150.	*	1.	1.	2.	2.	1.	0.	1.	1.	1.	2.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
160.	*	1.	1.	1.	2.	1.	1.	1.	1.	1.	2.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
170.	*	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
180.	*	1.	1.	1.	2.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
190.	*	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
200.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
220.	*	1.	1.	1.	1.	2.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
230.	*	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
240.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
250.	*	0.	1.	1.	1.	0.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
260.	*	0.	1.	1.	0.	0.	2.	2.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.
0.	0.																		
270.	*	0.	1.	1.	0.	0.	1.	2.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		

MAX	*	1.	2.	2.	2.	2.	2.	2.	2.	1.	2.	1.	1.	2.	1.	1.	1.	1.	2.
1.	1.																		
DEGR.	*	130	130	130	150	220	260	260	270	260	140	340	10	40	40	40	80	70	80
90	90																		

♀

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38

REC39 REC40

0.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	1.	1.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	0.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	2.	2.	2.	1.	0.	0.	1.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.
1.	1.																		
60.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.
1.	1.																		
70.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	2.	0.	0.	1.
0.	0.																		
80.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	1.	1.
0.	0.																		
90.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	2.	1.	1.	1.	1.	1.
0.	0.																		
100.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.
1.	0.																		
110.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.
1.	0.																		
120.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	2.
1.	0.																		
130.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.
2.	1.																		
140.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.
2.	1.																		
150.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.
2.	1.																		
160.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.
2.	1.																		
170.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.
2.	1.																		
180.	*	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
2.	1.																		
190.	*	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
200.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
210.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
1.	0.																		
220.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
230.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
240.	*	1.	1.	2.	2.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
250.	*	1.	1.	2.	2.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
260.	*	0.	1.	1.	2.	1.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
270.	*	0.	1.	1.	1.	1.	0.	1.	2.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	0.	1.	1.	1.	1.	1.	2.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	1.	1.	0.	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	2.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	1.	0.	0.	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	1.	1.	0.	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		

MAX	*	1.	1.	2.	2.	1.	1.	1.	2.	2.	1.	1.	2.	2.	2.	2.	1.	2.	2.
2.	1.																		
DEGR.	*	220	230	190	240	260	290	300	290	320	340	20	40	50	50	70	110	120	110
170	170																		

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC4 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17:38:16

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6054.9	5445.6	*	60.	290.	AG	0.	100.0	1.0	30.0	0.48	3.1
2. Char/Merr WB	*	6250.4	5435.2	6323.7	5493.2	*	93.	52.	AG	0.	100.0	1.0	30.0	0.71	4.7
3. Char/Merr NB R	*	6291.7	5369.7	6313.9	5354.6	*	27.	124.	AG	0.	100.0	1.0	10.0	0.14	1.4
4. Char/Merr NB LTT	*	6280.4	5347.2	6395.2	5266.3	*	140.	125.	AG	0.	100.0	1.0	20.0	0.83	7.1
5. Char/Merr EB	*	6104.2	5362.2	6064.9	5347.6	*	42.	250.	AG	0.	100.0	1.0	20.0	0.38	2.1
6. Char/Cam SB L	*	5384.1	4834.2	5408.6	4932.0	*	101.	14.	AG	0.	100.0	1.0	10.0	0.66	5.1
7. Char/Cam SB TR	*	5360.8	4833.5	5392.6	4936.4	*	108.	17.	AG	0.	100.0	1.0	20.0	0.86	5.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5448.9	4784.7	*	39.	103.	AG	0.	100.0	1.0	20.0	0.24	2.0
9. Char/Cam NB L	*	5363.0	4722.4	5361.1	4639.9	*	82.	181.	AG	0.	100.0	1.0	10.0	0.54	4.2
10. Char/Cam NB TR	*	5383.3	4723.8	5384.3	4657.5	*	66.	179.	AG	0.	100.0	1.0	20.0	0.67	3.4
11. Char/Cam EB TTTR	*	5302.7	4739.8	5222.9	4740.6	*	80.	271.	AG	0.	100.0	1.0	30.0	0.49	4.1
12. Sud/Merr SB L	*	6532.7	5210.3	6493.6	5238.2	*	48.	305.	AG	0.	100.0	1.0	10.0	0.66	2.4
13. Sud/Merr SB TTT	*	6518.3	5190.8	6480.9	5212.4	*	43.	300.	AG	0.	100.0	1.0	30.0	0.22	2.2
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6669.4	5076.1	*	98.	150.	AG	0.	100.0	1.0	30.0	0.55	5.0
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6482.0	5121.0	*	48.	239.	AG	0.	100.0	1.0	40.0	0.34	2.5
16. Sud/Sur SB LTT	*	6777.5	5369.7	6741.1	5415.5	*	59.	322.	AG	0.	100.0	1.0	20.0	0.30	3.0
17. Sud/Sur SEB	*	6757.2	5330.0	6747.9	5332.3	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6750.6	5242.3	*	47.	249.	AG	0.	100.0	1.0	30.0	0.39	2.4
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	802.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1038.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1204.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	870.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	923.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1472.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	877.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1546.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	285.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	483.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	405.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	338.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	25.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1421.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1512.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	487.	0.0	1.0	78.0		

DATE : 8/ 7/13
TIME : 17:38:16

1. Char/Merr SB	*	100	76	3.0	436	1600	0.05	1	3
2. Char/Merr WB	*	100	76	3.0	650	1600	0.05	1	3
3. Char/Merr NB R	*	100	45	3.0	109	1600	0.05	1	3
4. Char/Merr NB LTT	*	100	71	3.0	637	1600	0.05	1	3
5. Char/Merr EB	*	100	79	3.0	194	1600	0.05	1	3
6. Char/Cam SB L	*	90	58	3.0	318	1600	0.05	1	3
7. Char/Cam SB TR	*	90	71	3.0	429	1600	0.05	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	265	1600	0.05	1	3
9. Char/Cam NB L	*	90	58	3.0	260	1600	0.05	1	3
10. Char/Cam NB TR	*	90	71	3.0	330	1600	0.05	1	3
11. Char/Cam EB TTTR	*	90	54	3.0	811	1600	0.05	1	3
12. Sud/Merr SB L	*	100	86	3.0	95	1600	0.05	1	3
13. Sud/Merr SB TTT	*	100	49	3.0	484	1600	0.05	1	3
14. Sud/Merr NB TTTR	*	100	63	3.0	854	1600	0.05	1	3
15. Sud/Merr EB LTTR	*	100	73	3.0	487	1600	0.05	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	405	1600	0.05	1	3
17. Sud/Sur SEB	*	100	70	3.0	25	1600	0.05	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	338	1600	0.05	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Sud/Merr NE1	*	6492.5	5309.9	6.0	*
2. Sud/Merr NE2	*	6554.8	5268.0	6.0	*
3. Sud/Merr NE3	*	6616.2	5224.9	6.0	*
4. Sud/Merr NE4	*	6684.7	5255.3	6.0	*
5. Sud/Merr NE5	*	6753.3	5285.7	6.0	*
6. Sud/Merr SE1	*	6792.9	5222.3	6.0	*
7. Sud/Merr SE2	*	6724.3	5191.9	6.0	*
8. Sud/Merr SE3	*	6655.7	5161.5	6.0	*
9. Sud/Merr SE4	*	6695.5	5097.9	6.0	*
10. Sud/Merr SE5	*	6735.2	5034.3	6.0	*
11. Sud/Merr SW1	*	6638.6	4981.3	6.0	*
12. Sud/Merr SW2	*	6598.9	5045.0	6.0	*
13. Sud/Merr SW3	*	6559.1	5108.6	6.0	*
14. Sud/Merr SW4	*	6493.4	5072.5	6.0	*
15. Sud/Merr SW5	*	6427.6	5036.5	6.0	*
16. Sud/Merr NW1	*	6347.8	5104.5	6.0	*
17. Sud/Merr NW2	*	6413.5	5140.5	6.0	*
18. Sud/Merr NW3	*	6479.3	5176.6	6.0	*
19. Sud/Merr NW4	*	6417.1	5218.5	6.0	*
20. Sud/Merr NW5	*	6354.9	5260.4	6.0	*
21. Sud/Sur NE1	*	6755.9	5445.7	6.0	*
22. Sud/Sur NE2	*	6801.0	5385.7	6.0	*
23. Sud/Sur NE3	*	6846.0	5325.7	6.0	*
24. Sud/Sur NE4	*	6908.8	5366.8	6.0	*
25. Sud/Sur NE5	*	6971.5	5407.9	6.0	*
26. Sud/Sur SE1	*	7002.4	5368.4	6.0	*
27. Sud/Sur SE2	*	6939.7	5327.3	6.0	*
28. Sud/Sur SE3	*	6876.9	5286.2	6.0	*
29. Sud/Sur SE4	*	6931.7	5235.0	6.0	*
30. Sud/Sur SE5	*	6986.5	5183.8	6.0	*
31. Sud/Sur SW1	*	6932.3	5133.1	6.0	*
32. Sud/Sur SE2	*	6877.5	5184.3	6.0	*
33. Sud/Sur SE3	*	6822.7	5235.5	6.0	*

DATE : 8/ 7/13
TIME : 17:38:16

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
34. Sud/Sur SE4	*	6754.2	5205.1	6.0	*
35. Sud/Sur SE5	*	6685.6	5174.8	6.0	*
36. Sud/Sur NW1	*	6645.5	5237.9	6.0	*
37. Sud/Sur NW2	*	6714.1	5268.3	6.0	*
38. Sud/Sur NW3	*	6782.7	5298.7	6.0	*
39. Sud/Sur NW4	*	6709.5	5315.4	6.0	*
40. Sud/Sur NW5	*	6636.4	5332.0	6.0	*
41. Sud/Sur N1	*	6642.4	5493.7	6.0	*
42. Sud/Sur N2	*	6687.4	5433.7	6.0	*
43. Sud/Sur N3	*	6732.4	5373.8	6.0	*
44. Sud/Sur N4	*	6659.3	5390.4	6.0	*
45. Sud/Sur N5	*	6586.2	5407.1	6.0	*

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) *	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

```
   0.  *    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    1.    2.    1.    1.    1.    1.
1.    2.
  10.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
1.    1.
  20.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
1.    1.
  30.  *    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
1.    1.
  40.  *    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
1.    1.
  50.  *    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
1.    1.
  60.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.
1.    1.
  70.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.
1.    1.
  80.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    2.
1.    1.
  90.  *    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    2.
1.    1.
 100.  *    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    2.
2.    2.
 110.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    2.
1.    2.
 120.  *    0.    0.    0.    0.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.    1.    2.
1.    2.
 130.  *    1.    1.    0.    0.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.    0.    2.
1.    1.
 140.  *    1.    1.    1.    0.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.    0.    1.
1.    1.
 150.  *    1.    1.    1.    0.    1.    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 160.  *    2.    2.    2.    0.    1.    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 170.  *    1.    1.    2.    1.    1.    0.    0.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 180.  *    1.    1.    2.    1.    1.    0.    0.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 190.  *    1.    1.    1.    1.    1.    0.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 200.  *    1.    1.    1.    1.    1.    0.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 210.  *    1.    1.    1.    1.    1.    0.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 220.  *    1.    1.    1.    1.    1.    0.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 230.  *    1.    1.    2.    1.    1.    0.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 240.  *    1.    1.    2.    1.    1.    1.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 250.  *    1.    1.    1.    1.    1.    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 260.  *    1.    1.    1.    1.    0.    1.    1.    2.    2.    1.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 270.  *    1.    1.    1.    1.    0.    1.    1.    2.    2.    1.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 280.  *    1.    1.    1.    1.    0.    1.    1.    2.    2.    1.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 290.  *    1.    1.    1.    1.    0.    1.    1.    2.    2.    2.    0.    0.    1.    0.    0.    0.    0.    0.
1.    1.
 300.  *    1.    1.    1.    0.    0.    1.    1.    2.    2.    2.    0.    1.    2.    0.    0.    0.    0.    1.
1.    1.
 310.  *    0.    0.    0.    0.    0.    1.    0.    1.    2.    2.    1.    1.    2.    0.    0.    0.    0.    1.
1.    2.
 320.  *    0.    0.    0.    0.    0.    1.    0.    1.    1.    2.    1.    1.    2.    1.    0.    0.    1.    1.
2.    2.
 330.  *    0.    0.    0.    0.    0.    1.    0.    0.    1.    1.    1.    1.    2.    1.    1.    0.    1.    1.
2.    2.
 340.  *    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    2.    1.    1.    1.    1.    1.
1.    2.
 350.  *    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.
1.    2.
 360.  *    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    1.    2.    1.    1.    1.    1.
1.    2.

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    2.    2.    2.    1.    1.    1.    1.    2.    2.    2.    1.    1.    2.    2.    1.    1.    1.    2.
2.    2.
 DEGR. *  160   160   170   230   140   330   250   290   300   300   340   320   320    10    30    70    80   100
100   320
```


JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 WIND  * CONCENTRATION
 ANGLE *     (ug/m**3)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38
REC39 REC40

------*-------------------------------------------------------------------------------------------------------------
-------
   0.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  10.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  20.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  30.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  40.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  50.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
  60.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
  70.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
  80.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
  90.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 100.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 110.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 120.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 130.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 140.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 150.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 160.  *    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.
0.    0.
 170.  *    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    1.
0.    1.
 180.  *    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
0.    1.
 190.  *    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    1.
 200.  *    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    1.
 210.  *    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
0.    1.
 220.  *    1.    1.    1.    1.    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    1.
 230.  *    0.    1.    1.    1.    1.    0.    0.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    1.
 240.  *    0.    1.    1.    1.    0.    0.    1.    1.    1.    0.    0.    0.    1.    1.    1.    1.    1.    1.
1.    0.
 250.  *    0.    1.    1.    0.    0.    1.    1.    1.    1.    1.    0.    1.    1.    1.    2.    1.    1.    1.
0.    0.
 260.  *    0.    1.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    1.    1.    0.    0.
0.    1.
 270.  *    1.    1.    0.    1.    0.    1.    1.    1.    1.    1.    0.    1.    1.    1.    1.    1.    1.    0.
0.    1.
 280.  *    1.    1.    1.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    0.
0.    1.
 290.  *    0.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    2.    1.    0.    0.
0.    0.
 300.  *    0.    1.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    0.    1.    0.    0.    0.
0.    0.
 310.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    0.    1.    0.    0.    0.
0.    0.
 320.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 330.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 340.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 350.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
 360.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    2.    1.    1.    1.
1.    1.
 DEGR. *  190   270   210   220   230   250   250   250   260   280   280   280   280   260   250   240   230   200
```

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	0.	0.	0.
10.	0.	0.	0.	0.	0.
20.	0.	0.	0.	0.	0.
30.	0.	0.	0.	0.	0.
40.	0.	0.	0.	0.	0.
50.	0.	0.	0.	0.	0.
60.	0.	0.	0.	0.	0.
70.	0.	0.	0.	0.	0.
80.	0.	0.	0.	0.	0.
90.	0.	0.	0.	0.	0.
100.	0.	0.	0.	0.	0.
110.	0.	0.	0.	0.	0.
120.	0.	1.	0.	0.	0.
130.	0.	0.	0.	0.	0.
140.	0.	0.	0.	0.	0.
150.	0.	0.	0.	0.	0.
160.	0.	0.	0.	0.	0.
170.	0.	0.	0.	0.	1.
180.	0.	0.	0.	1.	0.
190.	0.	0.	0.	0.	1.
200.	0.	0.	0.	0.	1.
210.	0.	0.	0.	0.	0.
220.	0.	0.	0.	1.	0.
230.	0.	0.	0.	0.	0.
240.	0.	0.	0.	0.	0.
250.	0.	0.	0.	0.	0.
260.	1.	0.	0.	0.	1.
270.	1.	1.	0.	0.	1.
280.	0.	0.	0.	0.	1.
290.	0.	0.	0.	0.	0.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	0.	0.	0.
360.	0.	0.	0.	0.	0.
MAX	1.	1.	0.	1.	1.
DEGR.	260	120	10	180	270

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC9 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2013EX

DATE : 8/ 7/13
TIME : 17:10:51

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6042.2	5450.2	*	74.	290.	AG	0.	100.0	1.0	30.0	0.56	3.8
2. Char/Merr WB	*	6250.4	5435.2	6300.3	5474.7	*	64.	52.	AG	0.	100.0	1.0	30.0	0.55	3.2
3. Char/Merr NB R	*	6291.7	5369.7	6341.8	5335.7	*	61.	124.	AG	0.	100.0	1.0	10.0	0.31	3.1
4. Char/Merr NB LTT	*	6280.4	5347.2	6349.1	5298.8	*	84.	125.	AG	0.	100.0	1.0	20.0	0.52	4.3
5. Char/Merr EB	*	6104.2	5362.2	6005.8	5325.6	*	105.	250.	AG	0.	100.0	1.0	20.0	0.81	5.3
6. Char/Cam SB L	*	5384.1	4834.2	5401.1	4902.3	*	70.	14.	AG	0.	100.0	1.0	10.0	0.38	3.6
7. Char/Cam SB TR	*	5360.8	4833.5	5374.3	4877.1	*	46.	17.	AG	0.	100.0	1.0	20.0	0.32	2.3
8. Char/Cam WB LTTR	*	5411.0	4793.5	5475.3	4778.6	*	66.	103.	AG	0.	100.0	1.0	20.0	0.37	3.4
9. Char/Cam NB L	*	5363.0	4722.4	5361.0	4631.8	*	91.	181.	AG	0.	100.0	1.0	10.0	0.49	4.6
10. Char/Cam NB TR	*	5383.3	4723.8	5384.8	4624.7	*	99.	179.	AG	0.	100.0	1.0	20.0	0.68	5.0
11. Char/Cam EB TTTR	*	5302.7	4739.8	5220.6	4740.7	*	82.	271.	AG	0.	100.0	1.0	30.0	0.46	4.2
12. Sud/Merr SB L	*	6532.7	5210.3	6496.1	5236.4	*	45.	305.	AG	0.	100.0	1.0	10.0	0.56	2.3
13. Sud/Merr SB TTT	*	6518.3	5190.8	6487.3	5208.8	*	36.	300.	AG	0.	100.0	1.0	30.0	0.18	1.8
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6672.2	5071.1	*	104.	150.	AG	0.	100.0	1.0	30.0	0.62	5.3
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6458.9	5107.1	*	75.	239.	AG	0.	100.0	1.0	40.0	0.52	3.8
16. Sud/Sur SB LTT	*	6777.5	5369.7	6739.2	5418.0	*	62.	322.	AG	0.	100.0	1.0	20.0	0.40	3.1
17. Sud/Sur SEB	*	6757.2	5330.0	6742.4	5333.7	*	15.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6722.2	5231.2	*	78.	249.	AG	0.	100.0	1.0	30.0	0.39	3.9
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	818.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1226.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1219.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	859.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	796.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1264.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	954.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1198.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	805.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	405.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	322.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	853.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	35.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1185.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1465.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	766.	0.0	1.0	78.0		

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1. Char/Merr SB	*	100	75	3.0	541	1600	0.05	1	3
2. Char/Merr WB	*	100	78	3.0	449	1600	0.05	1	3
3. Char/Merr NB R	*	100	46	3.0	241	1600	0.05	1	3
4. Char/Merr NB LTT	*	100	68	3.0	452	1600	0.05	1	3
5. Char/Merr EB	*	100	79	3.0	417	1600	0.05	1	3
6. Char/Cam SB L	*	100	60	3.0	214	1600	0.05	1	3
7. Char/Cam SB TR	*	100	72	3.0	233	1600	0.05	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	391	1600	0.05	1	3
9. Char/Cam NB L	*	100	60	3.0	276	1600	0.05	1	3
10. Char/Cam NB TR	*	100	72	3.0	503	1600	0.05	1	3

11. Char/Cam EB TTTR	*	100	62	3.0	726	1600	0.05	1	3
12. Sud/Merr SB L	*	100	84	3.0	98	1600	0.05	1	3
13. Sud/Merr SB TTT	*	100	50	3.0	394	1600	0.05	1	3
14. Sud/Merr NB TTTR	*	100	66	3.0	863	1600	0.05	1	3
15. Sud/Merr EB LTTR	*	100	72	3.0	766	1600	0.05	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	322	1600	0.05	1	3
17. Sud/Sur SEB	*	100	80	3.0	35	1600	0.05	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	853	1600	0.05	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Sud/Merr NE1	*	6492.5	5309.9	6.0
2. Sud/Merr NE2	*	6554.8	5268.0	6.0
3. Sud/Merr NE3	*	6616.2	5224.9	6.0
4. Sud/Merr NE4	*	6684.7	5255.3	6.0
5. Sud/Merr NE5	*	6753.3	5285.7	6.0
6. Sud/Merr SE1	*	6792.9	5222.3	6.0
7. Sud/Merr SE2	*	6724.3	5191.9	6.0
8. Sud/Merr SE3	*	6655.7	5161.5	6.0
9. Sud/Merr SE4	*	6695.5	5097.9	6.0
10. Sud/Merr SE5	*	6735.2	5034.3	6.0
11. Sud/Merr SW1	*	6638.6	4981.3	6.0
12. Sud/Merr SW2	*	6598.9	5045.0	6.0
13. Sud/Merr SW3	*	6559.1	5108.6	6.0
14. Sud/Merr SW4	*	6493.4	5072.5	6.0
15. Sud/Merr SW5	*	6427.6	5036.5	6.0
16. Sud/Merr NW1	*	6347.8	5104.5	6.0
17. Sud/Merr NW2	*	6413.5	5140.5	6.0
18. Sud/Merr NW3	*	6479.3	5176.6	6.0
19. Sud/Merr NW4	*	6417.1	5218.5	6.0
20. Sud/Merr NW5	*	6354.9	5260.4	6.0
21. Sud/Sur NE1	*	6755.9	5445.7	6.0
22. Sud/Sur NE2	*	6801.0	5385.7	6.0
23. Sud/Sur NE3	*	6846.0	5325.7	6.0
24. Sud/Sur NE4	*	6908.8	5366.8	6.0
25. Sud/Sur NE5	*	6971.5	5407.9	6.0
26. Sud/Sur SE1	*	7002.4	5368.4	6.0
27. Sud/Sur SE2	*	6939.7	5327.3	6.0
28. Sud/Sur SE3	*	6876.9	5286.2	6.0
29. Sud/Sur SE4	*	6931.7	5235.0	6.0
30. Sud/Sur SE5	*	6986.5	5183.8	6.0
31. Sud/Sur SW1	*	6932.3	5133.1	6.0
32. Sud/Sur SE2	*	6877.5	5184.3	6.0
33. Sud/Sur SE3	*	6822.7	5235.5	6.0

DATE : 8/ 7/13
TIME : 17:10:51

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Sud/Sur SE4	*	6754.2	5205.1	6.0
35. Sud/Sur SE5	*	6685.6	5174.8	6.0
36. Sud/Sur NW1	*	6645.5	5237.9	6.0
37. Sud/Sur NW2	*	6714.1	5268.3	6.0
38. Sud/Sur NW3	*	6782.7	5298.7	6.0
39. Sud/Sur NW4	*	6709.5	5315.4	6.0
40. Sud/Sur NW5	*	6636.4	5332.0	6.0
41. Sud/Sur N1	*	6642.4	5493.7	6.0
42. Sud/Sur N2	*	6687.4	5433.7	6.0
43. Sud/Sur N3	*	6732.4	5373.8	6.0
44. Sud/Sur N4	*	6659.3	5390.4	6.0
45. Sud/Sur N5	*	6586.2	5407.1	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

```
   0.  *    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.    1.    1.    1.    2.    1.    1.    1.    1.
1.    1.
  10.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
1.    1.
  20.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    2.    1.    0.    0.    1.
1.    1.
  30.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
1.    1.
  40.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    2.    1.    1.    2.    0.    0.    1.
1.    1.
  50.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    2.    1.    1.    0.    0.    1.
1.    1.
  60.  *    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    1.    1.    2.    1.    1.    1.    1.    1.
1.    1.
  70.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    2.
1.    1.
  80.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    2.    2.
1.    1.
  90.  *    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    2.    2.
1.    1.
 100.  *    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    2.    2.
1.    1.
 110.  *    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    2.    2.
2.    2.
 120.  *    0.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    2.
1.    1.
 130.  *    1.    1.    1.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.    1.    2.
1.    1.
 140.  *    1.    1.    1.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.    1.    2.
1.    1.
 150.  *    1.    2.    2.    1.    1.    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.
1.    1.
 160.  *    2.    2.    2.    1.    1.    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 170.  *    1.    1.    2.    1.    1.    0.    0.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 180.  *    1.    1.    2.    1.    1.    0.    0.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 190.  *    1.    1.    2.    1.    1.    0.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 200.  *    1.    2.    1.    1.    1.    0.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 210.  *    1.    1.    2.    1.    1.    0.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 220.  *    1.    1.    2.    1.    1.    0.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 230.  *    1.    1.    2.    1.    1.    1.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 240.  *    1.    1.    2.    1.    1.    1.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 250.  *    1.    1.    1.    1.    1.    1.    2.    2.    2.    1.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 260.  *    1.    1.    1.    1.    0.    1.    1.    2.    2.    1.    0.    0.    1.    1.    0.    0.    0.    0.
0.    0.
 270.  *    1.    1.    1.    0.    0.    2.    1.    2.    2.    1.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 280.  *    1.    1.    1.    1.    0.    2.    1.    2.    2.    1.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 290.  *    1.    1.    1.    1.    0.    2.    1.    2.    2.    2.    0.    0.    1.    1.    0.    0.    0.    0.
1.    1.
 300.  *    1.    1.    1.    0.    0.    1.    1.    2.    3.    2.    0.    1.    2.    1.    0.    0.    0.    1.
1.    1.
 310.  *    0.    0.    0.    0.    0.    1.    1.    1.    2.    2.    1.    1.    2.    1.    1.    0.    0.    1.
1.    2.
 320.  *    0.    0.    0.    0.    0.    1.    1.    1.    1.    2.    1.    1.    2.    1.    1.    0.    1.    1.
1.    2.
 330.  *    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    2.    2.    1.    0.    1.    1.
1.    2.
 340.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    2.    2.    1.    0.    1.    1.
1.    2.
 350.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    2.    1.    1.    1.    1.
1.    2.
 360.  *    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.    1.    1.    1.    2.    1.    1.    1.    1.
1.    1.

------*-----------------------------------------------------------------------------------------------------------
-------
 MAX  *    2.    2.    2.    1.    1.    2.    2.    2.    3.    2.    1.    2.    2.    2.    2.    1.    2.    2.
2.    2.
 DEGR. *  160   160   160   230   200   270   250   260   300   310    10    40   310   350    40    80    90   100
110   330
```


JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (ug/m**3)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38
REC39 REC40

```
------*-----------------------------------------------------------------------------------------------------------
-------
   0.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.
  10.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.
  20.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.
  30.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
  40.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
  50.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.
  60.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.
0.    0.
  70.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
  80.  *    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
0.    0.
  90.  *    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
0.    0.
 100.  *    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
0.    0.
 110.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
0.    0.
 120.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 130.  *    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
1.    0.
 140.  *    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
1.    0.
 150.  *    0.    0.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.
1.    0.
 160.  *    1.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.
1.    1.
 170.  *    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.
1.    1.
 180.  *    1.    0.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 190.  *    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    2.    1.
1.    1.
 200.  *    1.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.
2.    1.
 210.  *    1.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.
1.    1.
 220.  *    1.    1.    1.    1.    1.    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.
1.    1.
 230.  *    1.    1.    1.    1.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.
1.    1.
 240.  *    0.    1.    1.    1.    1.    1.    1.    1.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.
1.    0.
 250.  *    0.    1.    1.    1.    0.    1.    1.    1.    1.    1.    0.    1.    1.    1.    2.    1.    1.    1.
0.    0.
 260.  *    0.    1.    0.    0.    0.    1.    1.    2.    1.    1.    0.    1.    1.    1.    2.    1.    1.    0.
0.    0.
 270.  *    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.    2.    1.    2.    1.    0.    0.
0.    1.
 280.  *    0.    1.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    2.    1.    2.    1.    1.    0.
0.    0.
 290.  *    0.    1.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.    1.    2.    1.    0.    0.
0.    0.
 300.  *    0.    1.    0.    0.    0.    0.    1.    1.    1.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 310.  *    0.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 320.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 330.  *    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 340.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.
 350.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.
0.    0.
 360.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.

------*-----------------------------------------------------------------------------------------------------------
-------
 MAX  *    1.    1.    1.    1.    1.    1.    1.    2.    1.    1.    1.    1.    2.    1.    2.    2.    1.    2.
1.    1.
 DEGR. *  190   220   240   220   230   240   250   260   260   280   270   290   270   270   260   180   220   200
```

220 180

JOB: Government Center Garage RUN: 2013EX

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	0.	0.	0.
10.	0.	0.	0.	0.	0.
20.	0.	0.	0.	0.	0.
30.	0.	0.	1.	0.	0.
40.	0.	0.	1.	0.	0.
50.	0.	0.	1.	0.	0.
60.	0.	0.	1.	0.	0.
70.	0.	0.	1.	0.	0.
80.	0.	0.	1.	0.	0.
90.	0.	0.	1.	0.	0.
100.	0.	0.	1.	0.	0.
110.	0.	0.	0.	0.	0.
120.	0.	1.	0.	0.	0.
130.	0.	1.	0.	0.	0.
140.	0.	0.	0.	0.	0.
150.	0.	0.	0.	0.	0.
160.	0.	0.	0.	0.	0.
170.	0.	0.	1.	1.	1.
180.	0.	1.	0.	1.	1.
190.	1.	0.	1.	0.	1.
200.	0.	1.	1.	1.	0.
210.	0.	0.	1.	0.	0.
220.	0.	0.	1.	1.	0.
230.	0.	0.	0.	0.	0.
240.	0.	0.	0.	0.	0.
250.	0.	0.	0.	0.	0.
260.	1.	0.	0.	0.	0.
270.	0.	0.	0.	0.	1.
280.	0.	0.	0.	0.	1.
290.	0.	0.	0.	0.	0.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	0.	0.	0.
360.	0.	0.	0.	0.	0.
MAX	1.	1.	1.	1.	1.
DEGR.	190	200	190	200	170

THE HIGHEST CONCENTRATION OF 3. ug/m**3 OCCURRED AT RECEPTOR REC9 .

2028 No-Build
Microscale Output Files
(Particulate Matter 2.5 (PM2.5))

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 5:41

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	0.	100.0	1.0	10.0	0.71	7.8
2. Stan/Lom SB TRR	*	5173.5	5937.1	5111.3	6026.2	*	109.	325.	AG	0.	100.0	1.0	20.0	0.50	5.5
3. Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	0.	100.0	1.0	20.0	0.92	9.6
4. Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	0.	100.0	1.0	10.0	0.58	6.4
5. Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	0.	100.0	1.0	10.0	0.64	4.1
6. Stan/Lom NB TRR	*	5314.4	5765.3	5363.1	5748.8	*	51.	109.	AG	0.	100.0	1.0	20.0	0.41	2.6
7. Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	0.	100.0	1.0	20.0	0.68	4.5
8. Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	0.	100.0	1.0	10.0	0.93	8.1
9. Caus/Wash SB LTTRR	*	6548.6	6868.7	6176.7	7641.4	*	857.	334.	AG	0.	100.0	1.0	40.0	1.08	43.6
10. Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	0.	100.0	1.0	20.0	0.58	5.3
11. Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	0.	100.0	1.0	10.0	0.53	6.6
12. Caus/Wash NB TTR	*	6603.5	6751.9	6665.3	5376.7	*	1377.	177.	AG	0.	100.0	1.0	20.0	1.39	69.9
13. Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	0.	100.0	1.0	30.0	0.47	4.6
14. Tha/Val SB LTTR	*	6599.0	6224.0	6593.7	6361.5	*	138.	358.	AG	0.	100.0	1.0	20.0	0.79	7.0
15. Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	0.	100.0	1.0	10.0	1.23	59.7
16. Tha/Val NB TR	*	6645.6	6138.6	6647.7	6017.7	*	121.	179.	AG	0.	100.0	1.0	10.0	0.69	6.1
17. Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6097.3	*	133.	0.	AG	0.	100.0	1.0	30.0	0.68	6.8
18. Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	0.	100.0	1.0	30.0	0.18	1.8
19. Char/93 SB LLTTRR	*	6587.8	5740.0	6582.3	5883.7	*	144.	358.	AG	0.	100.0	1.0	40.0	0.74	7.3
20. Char/93 WB LTT	*	6702.8	5647.8	6763.4	5572.1	*	97.	141.	AG	0.	100.0	1.0	20.0	0.62	4.9
21. Char/93 EB TTR	*	6560.8	5622.5	6520.0	5592.6	*	51.	234.	AG	0.	100.0	1.0	30.0	0.32	2.6
22. North/Congress SB LT	*	6876.6	4408.9	6569.4	5930.4	*	1552.	349.	AG	0.	100.0	1.0	30.0	2.69	78.8
23. North/Con WB LLTR	*	6920.6	4378.3	7106.5	4444.1	*	197.	71.	AG	0.	100.0	1.0	20.0	0.89	10.0
24. Nor/Con NB LTTTR	*	6914.9	4333.4	6920.9	4289.3	*	45.	172.	AG	0.	100.0	1.0	30.0	0.33	2.3
25. Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	0.	100.0	1.0	10.0	0.03	0.3
26. Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1396.	0.0	1.0	90.0		
27. Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1568.	0.0	1.0	78.0		
28. Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	899.	0.0	1.0	78.0		
29. Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	0.0	1.0	78.0		
30. Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3419.	0.0	1.0	90.0		
31. Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	0.0	1.0	66.0		
32. Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2371.	0.0	1.0	90.0		
33. Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	0.0	1.0	78.0		
34. Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2397.	0.0	1.0	90.0		
35. Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	0.0	1.0	38.0		
36. Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2837.	0.0	1.0	90.0		
37. Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	0.0	1.0	54.0		
38. Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2324.	0.0	1.0	66.0		
39. Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	0.0	1.0	48.0		
40. Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	515.	0.0	1.0	42.0		
41. Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	0.0	1.0	48.0		
42. Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	403.	0.0	1.0	54.0		
43. Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	702.	0.0	1.0	54.0		

44. Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	0.0	1.0	42.0		

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 5:41

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
45. North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1343.	0.0	1.0	98.0		
46. North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1063.	0.0	1.0	66.0		
47. North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1529.	0.0	1.0	98.0		
48. North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	0.0	1.0	54.0		

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 5:41

1. Stan/Lom SB L	*	120	75	3.0	376	1600	0.03	1	3
2. Stan/Lom SB TRR	*	120	75	3.0	531	1600	0.03	1	3
3. Stan/Lom WB LTT	*	120	91	3.0	588	1600	0.03	1	3
4. Stan/Lom WB R	*	120	75	3.0	308	1600	0.03	1	3
5. Stan/Lom NB L	*	120	97	3.0	152	1600	0.03	1	3
6. Stan/Lom NB TRR	*	120	97	3.0	194	1600	0.03	1	3
7. Stan/Lom EB LLT	*	120	97	3.0	324	1600	0.03	1	3
8. Stan/Lom EB R	*	120	97	3.0	222	1600	0.03	1	3
9. Caus/Wash SB LTTRR	*	150	94	3.0	2353	1600	0.03	1	3
10. Caus/Wash WB LLTT	*	150	119	3.0	321	1600	0.03	1	3
11. Caus/Wash WB R	*	150	104	3.0	230	1600	0.03	1	3
12. Caus/Wash NB TTR	*	150	120	3.0	741	1600	0.03	1	3
13. Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	0.03	1	3
14. Tha/Val SB LTTR	*	104	30	3.0	1678	1600	0.03	1	3
15. Tha/Val NB L	*	104	74	3.0	472	1600	0.03	1	3
16. Tha/Val NB TR	*	104	30	3.0	737	1600	0.03	1	3
17. Bev/Was SB TTT	*	100	45	3.0	1628	1600	0.03	1	3
18. Bev/Was EB RRR	*	100	55	3.0	356	1600	0.03	1	3
19. Char/93 SB LLTTRR	*	100	53	3.0	1986	1600	0.03	1	3
20. Char/93 WB LTT	*	100	69	3.0	515	1600	0.03	1	3
21. Char/93 EB TTR	*	100	69	3.0	403	1600	0.03	1	3
22. North/Congress SB LT	*	100	90	3.0	647	1600	0.03	1	3
23. North/Con WB LLTR	*	100	60	3.0	997	1600	0.03	1	3
24. Nor/Con NB LTTTR	*	100	74	3.0	332	1600	0.03	1	3
25. Nor/Con EB LTR	*	100	60	3.0	17	1600	0.03	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2. Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3. Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4. Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5. Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6. Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7. Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8. Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9. Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10. Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11. Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12. Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13. Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14. Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15. Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16. Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17. Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18. Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19. Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20. Stan/Lom NW5	*	5136.5	5935.7	6.0	*
21. Caus/Wash NE1	*	6548.3	7035.9	6.0	*
22. Caus/Wash NE2	*	6581.4	6968.6	6.0	*
23. Caus/Wash NE3	*	6614.5	6901.3	6.0	*
24. Caus/Wash NE4	*	6669.8	6952.0	6.0	*
25. Caus/Wash NE5	*	6725.0	7002.7	6.0	*
26. Caus/Wash SE1	*	6753.6	6912.2	6.0	*

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 5:41

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Caus/Wash SE2	6698.9	6862.0	6.0
28. Caus/Wash SE3	6643.1	6810.8	6.0
29. Caus/Wash SE4	6646.8	6736.4	6.0
30. Caus/Wash SE5	6650.0	6661.0	6.0
31. Caus/Wash SW1	6544.0	6561.0	6.0
32. Caus/Wash SW2	6540.9	6636.0	6.0
33. Caus/Wash SW3	6537.8	6710.9	6.0
34. Caus/Wash SW4	6476.8	6667.2	6.0
35. Caus/Wash SW5	6415.9	6623.4	6.0
36. Caus/Wash NW1	6407.4	6738.0	6.0
37. Caus/Wash NW2	6468.3	6781.7	6.0
38. Caus/Wash NW3	6529.3	6825.4	6.0
39. Caus/Wash NW4	6496.2	6892.7	6.0
40. Caus/Wash NW5	6463.1	6960.0	6.0
41. Tha/Val NE1	6667.3	6395.5	6.0
42. Tha/Val NE2	6668.3	6320.5	6.0
43. Tha/Val NE3	6669.3	6245.5	6.0
44. Tha/Val NE4	6744.3	6245.5	6.0
45. Tha/Val NE5	6819.2	6249.6	6.0
46. Tha/Val SE1	6822.3	6191.6	6.0
47. Tha/Val SE2	6747.3	6189.6	6.0
48. Tha/Val SE3	6672.3	6187.5	6.0
49. Tha/Val SE4	6671.6	6112.5	6.0
50. Tha/Val SE5	6670.9	6037.5	6.0
51. Tha/Val SW1	6560.2	5964.7	6.0
52. Tha/Val SW2	6560.9	6039.7	6.0
53. Tha/Val SW3	6561.6	6114.7	6.0
54. Tha/Val SW4	6502.2	6068.9	6.0
55. Tha/Val SW5	6442.7	6023.2	6.0
56. Tha/Val NW1	6441.0	6115.2	6.0
57. Tha/Val NW2	6500.4	6160.9	6.0
58. Tha/Val NW3	6559.8	6206.7	6.0
59. Tha/Val NW4	6558.8	6281.7	6.0
60. Tha/Val NW5	6557.8	6356.7	6.0

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
10.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.
20.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.
30.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.
40.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.
50.	0.	0.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
60.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
70.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
80.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
90.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	0.	1.	1.
100.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
110.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.
120.	0.	0.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
130.	0.	0.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.
140.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
150.	1.	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
160.	1.	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.	2.
10.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	2.	1.	1.	1.	2.	2.	2.
20.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	2.	1.	1.	1.	2.	2.	2.
30.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.	2.	2.
40.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	2.	2.	1.	1.	1.	1.	2.	2.
50.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	2.	2.
60.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	2.	2.
70.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	2.	2.
80.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	2.
90.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	2.	2.
100.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	2.	2.
110.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	2.	2.
120.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	2.	2.
130.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	2.	2.
140.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	2.	2.
150.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	2.	2.
160.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	2.	2.
170.	0.	0.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.
180.	0.	0.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.
190.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	2.	2.
200.	0.	0.	1.	1.	1.	2.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.
210.	0.	0.	1.	1.	1.	2.	0.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.
220.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.
230.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.
240.	0.	0.	1.	1.	0.	0.	0.	1.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
250.	0.	0.	1.	1.	0.	0.	0.	1.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
260.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	0.	0.	0.	1.	1.	1.	0.	0.	0.
270.	0.	0.	0.	1.	1.	0.	0.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.
280.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
290.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
300.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
310.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
320.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
330.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
340.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.
350.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.
360.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.
MAX	1.	1.	1.	1.	1.	2.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
DEGR.	180	170	190	190	200	290	310	200	210	240	320	340	220	290	0	40	100	170	60	70

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 110. *   0.   0.   1.   1.   0.   0.   0.   0.   0.   0.   1.   1.   1.   1.   0.   1.   1.   2.
2.   2.
 120. *   0.   0.   1.   1.   0.   0.   0.   0.   0.   0.   1.   1.   1.   1.   0.   1.   1.   1.
2.   2.
 130. *   0.   0.   1.   1.   0.   0.   0.   0.   0.   0.   1.   1.   1.   1.   0.   1.   1.   2.
2.   2.
 140. *   0.   0.   1.   1.   0.   0.   0.   0.   0.   0.   1.   1.   1.   1.   0.   1.   2.   2.
2.   2.
 150. *   1.   1.   1.   1.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   0.   1.   2.   2.
2.   2.
 160. *   1.   1.   1.   1.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   2.   2.
2.   2.
 170. *   2.   2.   2.   1.   0.   0.   0.   1.   1.   1.   2.   2.   2.   1.   1.   1.   1.   2.
1.   1.
 180. *   3.   2.   2.   2.   1.   0.   1.   1.   1.   2.   1.   1.   1.   0.   0.   1.   1.   2.
1.   1.
 190. *   2.   2.   3.   2.   2.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   1.   1.
0.   0.
 200. *   2.   2.   2.   2.   2.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   1.   1.   1.
0.   0.
 210. *   2.   2.   2.   2.   2.   1.   1.   1.   1.   2.   0.   0.   0.   0.   0.   1.   1.   1.
0.   0.
 220. *   2.   2.   2.   2.   2.   1.   1.   1.   1.   1.   0.   0.   0.   0.   0.   0.   1.   1.
0.   0.
 230. *   2.   2.   2.   2.   1.   1.   1.   1.   1.   1.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 240. *   2.   2.   2.   1.   1.   1.   1.   2.   1.   1.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 250. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   1.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 260. *   2.   2.   1.   1.   1.   2.   2.   2.   2.   1.   0.   0.   1.   1.   0.   0.   0.   0.
0.   0.
 270. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   1.   0.   0.   1.   1.   0.   0.   0.   0.
0.   0.
 280. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   1.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 290. *   2.   2.   2.   1.   1.   2.   2.   2.   1.   2.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 300. *   2.   2.   2.   1.   0.   1.   2.   2.   1.   2.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 310. *   2.   2.   2.   1.   0.   1.   2.   2.   2.   2.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 320. *   2.   2.   2.   0.   0.   1.   2.   3.   2.   2.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 330. *   1.   1.   2.   0.   0.   0.   1.   2.   2.   2.   1.   1.   1.   1.   0.   0.   0.   1.
1.   1.
 340. *   0.   1.   1.   0.   0.   0.   1.   2.   2.   2.   1.   1.   2.   1.   0.   0.   0.   2.
2.   2.
 350. *   0.   0.   0.   0.   0.   0.   1.   1.   1.   2.   1.   2.   2.   1.   1.   0.   1.   2.
2.   2.
 360. *   0.   0.   0.   0.   0.   0.   1.   1.   1.   1.   2.   2.   2.   2.   1.   1.   1.   2.
2.   2.

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 MAX   *   3.   2.   3.   2.   2.   2.   2.   3.   2.   2.   2.   2.   2.   2.   2.   1.   2.   2.
2.   2.
 DEGR. *  180   180   190   190   190   280   300   320   330   340   160     0    10    20    30    90   150   350
0   110
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```
1.   1.
  60. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   1.
1.   1.
  70. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   1.
1.   1.
  80. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   1.
1.   1.
  90. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   2.
1.   1.
 100. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   1.   1.   1.   1.   1.   2.
1.   1.
 110. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   1.   1.   1.   1.   1.   2.
1.   1.
 120. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   2.   1.   1.   1.   1.   2.
1.   1.
 130. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   2.   1.   1.   1.   1.   2.
1.   1.
 140. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   2.
2.   2.
 150. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   2.   2.   2.   1.   1.   1.   2.
2.   2.
 160. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   2.   2.   2.   1.   1.   2.   2.
2.   2.
 170. *   1.   1.   1.   0.   0.   0.   0.   0.   1.   1.   3.   3.   2.   1.   0.   0.   1.   2.
2.   2.
 180. *   2.   2.   2.   0.   0.   0.   0.   2.   1.   1.   3.   2.   2.   1.   0.   0.   1.   2.
2.   1.
 190. *   2.   2.   2.   1.   0.   0.   1.   2.   2.   2.   1.   1.   1.   0.   0.   0.   0.   1.
1.   1.
 200. *   2.   2.   2.   1.   1.   0.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 210. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 220. *   1.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 230. *   1.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 240. *   1.   1.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 250. *   1.   1.   1.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 260. *   1.   1.   1.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 270. *   1.   1.   1.   1.   0.   0.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 280. *   1.   1.   1.   1.   0.   0.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 290. *   1.   1.   1.   1.   0.   0.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 300. *   1.   1.   1.   1.   0.   0.   1.   1.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 310. *   1.   1.   1.   1.   0.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 320. *   1.   2.   2.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 330. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 340. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   3.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 350. *   2.   2.   2.   1.   0.   0.   1.   2.   2.   2.   1.   1.   1.   1.   0.   0.   0.   1.
1.   1.
 360. *   1.   1.   1.   0.   0.   0.   0.   1.   1.   1.   2.   1.   2.   1.   0.   0.   1.   1.
1.   1.

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 MAX   *   2.   2.   2.   1.   1.   1.   1.   2.   2.   3.   3.   3.   3.   2.   1.   1.   2.   2.
2.   2.
 DEGR. *  190   200   190   210   330   210   210   200   210   340   170   170   160   160   130   150   160   170
160   170

 THE HIGHEST CONCENTRATION OF      3. ug/m**3 OCCURRED AT RECEPTOR REC51.
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JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

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 WIND  * CONCENTRATION
 ANGLE *      (ug/m**3)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52 REC53 REC54 REC55 REC56 REC57 REC58
REC59 REC60

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   0. *   1.   1.   1.   0.   0.   0.   0.   1.   1.   1.   2.   1.   2.   1.   0.   0.   1.   1.
1.   1.
  10. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   2.
2.   2.
  20. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   0.   1.   2.
2.   2.
  30. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   0.   1.   2.
2.   1.
  40. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   1.
1.   1.
  50. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   1.
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CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 7:21

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	0.	100.0	1.0	10.0	0.71 7.8
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5111.3	6026.2	*	109.	325.	AG	0.	100.0	1.0	20.0	0.50 5.5
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	0.	100.0	1.0	20.0	0.92 9.6
4.	Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	0.	100.0	1.0	10.0	0.58 6.4
5.	Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	0.	100.0	1.0	10.0	0.64 4.1
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5363.1	5748.8	*	51.	109.	AG	0.	100.0	1.0	20.0	0.41 2.6
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	0.	100.0	1.0	20.0	0.68 4.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	0.	100.0	1.0	10.0	0.93 8.1
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6176.7	7641.4	*	857.	334.	AG	0.	100.0	1.0	40.0	1.08 43.6
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	0.	100.0	1.0	20.0	0.58 5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	0.	100.0	1.0	10.0	0.53 6.6
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6665.3	5376.7	*	1377.	177.	AG	0.	100.0	1.0	20.0	1.39 69.9
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	0.	100.0	1.0	30.0	0.47 4.6
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.7	6361.5	*	138.	358.	AG	0.	100.0	1.0	20.0	0.79 7.0
15.	Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	0.	100.0	1.0	10.0	1.23 59.7
16.	Tha/Val NB TR	*	6645.6	6138.6	6647.7	6017.7	*	121.	179.	AG	0.	100.0	1.0	10.0	0.69 6.1
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6097.3	*	133.	0.	AG	0.	100.0	1.0	30.0	0.68 6.8
18.	Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	0.	100.0	1.0	30.0	0.18 1.8
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.3	5883.7	*	144.	358.	AG	0.	100.0	1.0	40.0	0.74 7.3
20.	Char/93 WB LTT	*	6702.8	5647.8	6763.4	5572.1	*	97.	141.	AG	0.	100.0	1.0	20.0	0.62 4.9
21.	Char/93 EB TTR	*	6560.8	5622.5	6520.0	5592.6	*	51.	234.	AG	0.	100.0	1.0	30.0	0.32 2.6
22.	North/Congress SB LT	*	6876.6	4408.9	6569.4	5930.4	*	1552.	349.	AG	0.	100.0	1.0	30.0	2.69 78.8
23.	North/Con WB LLTR	*	6920.6	4378.3	7106.5	4444.1	*	197.	71.	AG	0.	100.0	1.0	20.0	0.89 10.0
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6920.9	4289.3	*	45.	172.	AG	0.	100.0	1.0	30.0	0.33 2.3
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	0.	100.0	1.0	10.0	0.03 0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1396.	0.0	1.0	90.0	
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1568.	0.0	1.0	78.0	
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	899.	0.0	1.0	78.0	
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	0.0	1.0	78.0	
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3419.	0.0	1.0	90.0	
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	0.0	1.0	66.0	
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2371.	0.0	1.0	90.0	
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	0.0	1.0	78.0	
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2397.	0.0	1.0	90.0	
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	0.0	1.0	38.0	
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2837.	0.0	1.0	90.0	
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	0.0	1.0	54.0	
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2324.	0.0	1.0	66.0	
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	0.0	1.0	48.0	
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	515.	0.0	1.0	42.0	
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	0.0	1.0	48.0	
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	403.	0.0	1.0	54.0	
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	702.	0.0	1.0	54.0	

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	0.0	1.0	42.0	

JOB: Government Center Garage RUN: No Build

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LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1343.	0.0	1.0	98.0	
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1063.	0.0	1.0	66.0	
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1529.	0.0	1.0	98.0	
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	0.0	1.0	54.0	

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1.	Stan/Lom SB L	*	120	75	3.0	376	1600	0.03	1	3
2.	Stan/Lom SB TRR	*	120	75	3.0	531	1600	0.03	1	3
3.	Stan/Lom WB LTT	*	120	91	3.0	588	1600	0.03	1	3
4.	Stan/Lom WB R	*	120	75	3.0	308	1600	0.03	1	3
5.	Stan/Lom NB L	*	120	97	3.0	152	1600	0.03	1	3
6.	Stan/Lom NB TRR	*	120	97	3.0	194	1600	0.03	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	324	1600	0.03	1	3
8.	Stan/Lom EB R	*	120	97	3.0	222	1600	0.03	1	3
9.	Caus/Wash SB LTTRR	*	150	94	3.0	2353	1600	0.03	1	3
10.	Caus/Wash WB LLTT	*	150	119	3.0	321	1600	0.03	1	3
11.	Caus/Wash WB R	*	150	104	3.0	230	1600	0.03	1	3
12.	Caus/Wash NB TTR	*	150	120	3.0	741	1600	0.03	1	3
13.	Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	0.03	1	3
14.	Tha/Val SB LTTR	*	104	30	3.0	1678	1600	0.03	1	3
15.	Tha/Val NB L	*	104	74	3.0	472	1600	0.03	1	3
16.	Tha/Val NB TR	*	104	30	3.0	737	1600	0.03	1	3
17.	Bev/Was SB TTT	*	100	45	3.0	1628	1600	0.03	1	3
18.	Bev/Was EB RRR	*	100	55	3.0	356	1600	0.03	1	3
19.	Char/93 SB LLTTRR	*	100	53	3.0	1986	1600	0.03	1	3
20.	Char/93 WB LTT	*	100	69	3.0	515	1600	0.03	1	3
21.	Char/93 EB TTR	*	100	69	3.0	403	1600	0.03	1	3
22.	North/Congress SB LT	*	100	90	3.0	647	1600	0.03	1	3
23.	North/Con WB LLTR	*	100	60	3.0	997	1600	0.03	1	3
24.	Nor/Con NB LTTTR	*	100	74	3.0	332	1600	0.03	1	3
25.	Nor/Con EB LTR	*	100	60	3.0	17	1600	0.03	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Bev/Was N1	*	6562.0	6150.2	6.0	*
2.	Bev/Was N2	*	6561.2	6075.2	6.0	*
3.	Bev/Was N3	*	6560.5	6000.2	6.0	*
4.	Bev/Was N4	*	6515.8	6060.4	6.0	*
5.	Bev/Was N5	*	6471.1	6120.6	6.0	*
6.	Bev/Was SE1	*	6671.0	6049.7	6.0	*
7.	Bev/Was SE2	*	6670.2	5966.3	6.0	*
8.	Bev/Was SE3	*	6624.0	5907.2	6.0	*
9.	Bev/Was SE4	*	6626.1	5832.3	6.0	*
10.	Bev/Was SE5	*	6628.1	5757.3	6.0	*
11.	Bev/Was SW1	*	6541.8	5766.9	6.0	*
12.	Bev/Was SW2	*	6540.1	5841.9	6.0	*
13.	Bev/Was SW3	*	6537.7	5916.8	6.0	*
14.	Bev/Was SW4	*	6493.0	5977.0	6.0	*
15.	Bev/Was SW5	*	6448.3	6037.3	6.0	*
16.	Char/93 NE1	*	6625.0	5871.1	6.0	*
17.	Char/93 NE2	*	6627.1	5796.1	6.0	*
18.	Char/93 NE3	*	6629.1	5721.1	6.0	*
19.	Char/93 NE4	*	6699.8	5695.9	6.0	*
20.	Char/93 NE5	*	6750.6	5633.2	6.0	*
21.	Char/93 S1	*	6657.8	5466.0	6.0	*
22.	Char/93 S2	*	6614.7	5527.4	6.0	*
23.	Char/93 S3	*	6571.7	5588.8	6.0	*
24.	Char/93 S4	*	6512.9	5542.2	6.0	*
25.	Char/93 S5	*	6454.1	5495.6	6.0	*
26.	Char/93 NW1	*	6424.1	5632.5	6.0	*

JOB: Government Center Garage RUN: No Build

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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Char/93 NW2	6483.6	5678.2	6.0
28. Char/93 NW3	6543.0	5723.9	6.0
29. Char/93 NW4	6541.0	5798.8	6.0
30. Char/93 NW5	6538.9	5873.8	6.0
31. Wash/Cong NE1	6910.2	4571.2	6.0
32. Wash/Cong NE2	6925.8	4497.8	6.0
33. Wash/Cong NE3	6941.4	4424.5	6.0
34. Wash/Cong NE4	7012.0	4449.6	6.0
35. Wash/Cong NE5	7082.7	4474.9	6.0
36. Wash/Cong SE1	7095.4	4388.1	6.0
37. Wash/Cong SE2	7024.8	4362.9	6.0
38. Wash/Cong SE3	6954.1	4337.7	6.0
39. Wash/Cong SE4	6968.4	4264.1	6.0
40. Wash/Cong SE5	6982.7	4190.4	6.0
41. Wash/Cong SW1	6867.5	4164.7	6.0
42. Wash/Cong SW2	6853.3	4238.0	6.0
43. Wash/Cong SW3	6838.9	4312.0	6.0
44. Wash/Cong SW4	6765.6	4296.1	6.0
45. Wash/Cong SW5	6692.3	4280.2	6.0
46. Wash/Cong NW1	6682.4	4353.8	6.0
47. Wash/Cong NW2	6755.7	4369.7	6.0
48. Wash/Cong NW3	6828.9	4386.0	6.0
49. Wash/Cong NW4	6813.3	4459.4	6.0
50. Wash/Cong NW5	6797.8	4532.8	6.0

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	2.	2.	2.	1.	0.	1.	1.	3.	3.	3.	2.	2.	1.	1.	0.	3.	3.	3.	1.	0.
10.	2.	2.	2.	1.	1.	1.	0.	3.	2.	2.	2.	2.	2.	1.	1.	3.	2.	2.	0.	0.
20.	2.	2.	2.	1.	1.	0.	0.	3.	2.	1.	3.	3.	2.	1.	1.	2.	1.	1.	0.	0.
30.	2.	2.	2.	1.	1.	0.	0.	2.	1.	1.	3.	3.	2.	1.	1.	1.	1.	1.	0.	0.
40.	2.	2.	2.	1.	1.	0.	0.	2.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
50.	2.	2.	2.	1.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
60.	2.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	2.	1.	1.	1.	1.	0.	0.	0.
70.	2.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	2.	1.	1.	1.	1.	0.	0.	0.
80.	2.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	2.	1.	1.	1.	1.	0.	0.	0.
90.	1.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
100.	1.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
110.	1.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
120.	1.	2.	2.	1.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
130.	2.	2.	2.	1.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
140.	2.	2.	2.	1.	1.	0.	0.	1.	1.	1.	2.	3.	3.	2.	1.	1.	1.	1.	0.	0.
150.	2.	2.	2.	2.	1.	0.	0.	1.	1.	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.
160.	2.	2.	3.	2.	2.	0.	0.	2.	2.	2.	1.	2.	3.	2.	1.	2.	2.	2.	1.	1.
170.	2.	2.	3.	2.	1.	1.	1.	2.	2.	3.	1.	2.	2.	1.	0.	2.	2.	3.	1.	1.
180.	2.	2.	2.	1.	0.	1.	1.	2.	2.	3.	0.	1.	1.	0.	0.	2.	3.	3.	2.	1.
190.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	0.	0.	0.	0.	3.	2.	2.	2.	1.
200.	0.	0.	1.	0.	0.	2.	2.	2.	3.	2.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
210.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	5.	3.	2.	1.	1.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.
10.	4.	2.	2.	2.	1.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
20.	3.	2.	2.	2.	1.	1.	1.	3.	3.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
30.	2.	2.	1.	2.	1.	1.	1.	2.	3.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
40.	2.	2.	1.	1.	1.	1.	1.	2.	3.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
50.	2.	2.	1.	1.	1.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
60.	2.	2.	1.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
70.	2.	2.	1.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
80.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
90.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
100.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
110.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
120.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
130.	2.	2.	1.	0.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
140.	2.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
150.	3.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
160.	3.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
170.	3.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
180.	3.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
190.	3.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
200.	3.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
210.	3.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
220.	3.	2.	2.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	1.	0.
230.	3.	2.	2.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	1.	0.
240.	3.	2.	2.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	1.	0.
250.	3.	2.	2.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	1.	0.
260.	3.	2.	2.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	1.	0.
270.	3.	2.	1.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	1.	0.
280.	3.	2.	1.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.
290.	3.	2.	1.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.
300.	3.	2.	1.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.
310.	3.	2.	1.	2.	0.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.
320.	3.	2.	1.	2.	0.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	0.	2.	3.	3.	2.
330.	3.	2.	2.	2.	0.	1.	1.	2.	2.	3.	0.	0.	0.	0.	0.	0.	2.	3.	3.	2.
340.	4.	3.	2.	2.	0.	1.	2.	3.	2.	3.	0.	0.	0.	0.	0.	0.	2.	3.	4.	2.
350.	4.	3.	3.	3.	1.	1.	1.	3.	3.	3.	1.	1.	1.	0.	0.	0.	3.	3.	4.	2.
360.	3.	3.	3.	2.	2.	1.	1.	3.	3.	3.	2.	2.	1.	1.	0.	0.	3.	3.	3.	1.
MAX	5.	4.	3.	3.	2.	1.	2.	3.	3.	3.	3.	3.	3.	3.	2.	1.	3.	3.	4.	2.
DEGR.	170	160	160	160	160	340	340	0	350	350	20	30	150	140	140	350	350	350	310	260

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

160.	*	3.	1.	1.	0.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
170.	*	3.	1.	0.	0.	0.	0.	1.	1.	1.	2.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
180.	*	3.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
190.	*	2.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
200.	*	1.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
210.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
220.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
230.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
240.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
250.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
0.	0.																		
260.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
0.	0.																		
270.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
0.	0.																		
280.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.
1.	0.																		
290.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.
1.	0.																		
300.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
310.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
320.	*	2.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	2.
1.	1.																		
330.	*	2.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	2.
2.	1.																		
340.	*	4.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	2.
2.	1.																		
350.	*	5.	2.	2.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
360.	*	5.	3.	2.	1.	1.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	0.	1.	1.
1.	0.																		

MAX	*	5.	3.	2.	2.	1.	1.	1.	3.	3.	3.	1.	1.	1.	1.	1.	1.	1.	2.
2.	1.																		
DEGR.	*	350	0	10	20	20	100	130	10	30	150	190	330	190	210	210	280	290	330
330	340																		

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50
0.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
10.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
20.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
30.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
40.	* 1.	1.	1.	0.	0.	0.	1.	1.	1.	1.
50.	* 1.	1.	1.	0.	0.	0.	1.	1.	1.	1.
60.	* 0.	1.	1.	1.	0.	0.	1.	1.	1.	1.
70.	* 0.	0.	1.	1.	0.	0.	1.	1.	1.	1.
80.	* 0.	0.	1.	0.	0.	0.	1.	1.	1.	1.
90.	* 0.	0.	1.	0.	0.	0.	1.	1.	1.	1.
100.	* 0.	0.	1.	0.	0.	0.	0.	1.	1.	1.
110.	* 0.	0.	1.	0.	0.	0.	0.	1.	1.	1.
120.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
130.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
140.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
150.	* 0.	1.	1.	0.	0.	0.	0.	1.	1.	1.
160.	* 0.	0.	1.	0.	0.	0.	0.	1.	1.	1.
170.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
180.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
190.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
200.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
210.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
220.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

240.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
250.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
260.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
270.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
280.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
290.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
300.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
310.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
320.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
330.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
340.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
350.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
360.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.

MAX	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
DEGR.	* 10	0	0	70	60	80	70	0	10	130

THE HIGHEST CONCENTRATION OF 5. ug/m**3 OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 5:13

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5120.9	6056.9	*	131.	326.	AG	0.	100.0	1.0	10.0	0.63	6.7
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5093.7	6051.5	*	140.	325.	AG	0.	100.0	1.0	20.0	0.67	7.1
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5368.6	5981.0	*	80.	51.	AG	0.	100.0	1.0	20.0	0.35	4.1
4.	Stan/Lom WB R	*	5292.4	5947.7	5403.8	6033.2	*	140.	52.	AG	0.	100.0	1.0	10.0	0.68	7.1
5.	Stan/Lom NB L	*	5307.6	5737.4	5341.6	5726.9	*	36.	107.	AG	0.	100.0	1.0	10.0	0.24	1.8
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5383.7	5741.9	*	73.	109.	AG	0.	100.0	1.0	20.0	0.49	3.7
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5171.4	5556.9	*	155.	196.	AG	0.	100.0	1.0	20.0	0.92	7.9
8.	Stan/Lom EB R	*	5236.5	5698.5	4944.8	4671.4	*	1068.	196.	AG	0.	100.0	1.0	10.0	1.34	54.2
9.	Char/93 SB LLTTRR	*	6587.8	5740.0	6580.9	5920.1	*	180.	358.	AG	0.	100.0	1.0	40.0	0.87	9.2
10.	Char/93 WB LTT	*	6702.8	5647.8	6735.6	5606.8	*	52.	141.	AG	0.	100.0	1.0	20.0	0.29	2.7
11.	Char/93 EB TTR	*	6560.8	5622.5	6474.2	5559.1	*	107.	234.	AG	0.	100.0	1.0	30.0	0.58	5.5
12.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1623.	0.0	1.0	90.0		
13.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1414.	0.0	1.0	78.0		
14.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	1179.	0.0	1.0	78.0		
15.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1387.	0.0	1.0	78.0		
16.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2078.	0.0	1.0	66.0		
17.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	321.	0.0	1.0	42.0		
18.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	1059.	0.0	1.0	48.0		
19.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	983.	0.0	1.0	54.0		
20.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	488.	0.0	1.0	54.0		
21.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	414.	0.0	1.0	42.0		

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JOB: Government Center Garage RUN: No Build

DATE : 7/19/13
TIME : 16: 5:13

		*								
1.	Stan/Lom SB L	*	120	79	3.0	304	1600	0.03	1	3
2.	Stan/Lom SB TRR	*	120	79	3.0	646	1600	0.03	1	3
3.	Stan/Lom WB LTT	*	120	71	3.0	412	1600	0.03	1	3
4.	Stan/Lom WB R	*	120	79	3.0	325	1600	0.03	1	3
5.	Stan/Lom NB L	*	120	93	3.0	70	1600	0.03	1	3
6.	Stan/Lom NB TRR	*	120	93	3.0	289	1600	0.03	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	439	1600	0.03	1	3
8.	Stan/Lom EB R	*	120	97	3.0	320	1600	0.03	1	3
9.	Char/93 SB LLTTRR	*	100	62	3.0	1829	1600	0.03	1	3
10.	Char/93 WB LTT	*	100	60	3.0	321	1600	0.03	1	3
11.	Char/93 EB TTR	*	100	60	3.0	983	1600	0.03	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8.	Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0	*

		*			
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0 *
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0 *
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0 *
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0 *
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0 *
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0 *
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0 *
21.	Char/93 NE1	*	6625.0	5871.1	6.0 *
22.	Char/93 NE2	*	6627.1	5796.1	6.0 *
23.	Char/93 NE3	*	6629.1	5721.1	6.0 *
24.	Char/93 NE4	*	6699.8	5695.9	6.0 *
25.	Char/93 NE5	*	6750.6	5633.2	6.0 *
26.	Char/93 S1	*	6657.8	5466.0	6.0 *
27.	Char/93 S2	*	6614.7	5527.4	6.0 *
28.	Char/93 S3	*	6571.7	5588.8	6.0 *
29.	Char/93 S4	*	6512.9	5542.2	6.0 *
30.	Char/93 S5	*	6454.1	5495.6	6.0 *
31.	Char/93 NW1	*	6424.1	5632.5	6.0 *
32.	Char/93 NW2	*	6483.6	5678.2	6.0 *
33.	Char/93 NW3	*	6543.0	5723.9	6.0 *
34.	Char/93 NW4	*	6541.0	5798.8	6.0 *
35.	Char/93 NW5	*	6538.9	5873.8	6.0 *

PAGE 3

JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.
10. *	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.
20. *	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	0.	1.	1.	0.	1.	1.	1.
30. *	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.
40. *	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.
50. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
60. *	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
70. *	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
80. *	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.	1.
90. *	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.	1.
100. *	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.
110. *	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.
120. *	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
130. *	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.
140. *	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.
150. *	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
160. *	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
170. *	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.
180. *	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.
190. *	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
200. *	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.
210. *	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.
220. *	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.
230. *	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.
240. *	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.

```
0.    0.
 250.  *    1.    1.    1.    0.    0.    1.    0.    0.    0.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 260.  *    1.    1.    1.    0.    0.    1.    0.    0.    0.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 270.  *    1.    1.    1.    0.    0.    1.    1.    0.    0.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 280.  *    1.    1.    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.
 290.  *    1.    1.    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 300.  *    1.    1.    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 310.  *    1.    1.    1.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 320.  *    0.    1.    1.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 330.  *    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    1.    1.    0.    0.    0.
1.    1.
 340.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.    0.
1.    1.
 350.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
1.    1.
 360.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
1.    1.

------*-------------------------------------------------------------------------------------------------------------
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 MAX   *    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.
1.    1.
 DEGR. *  180   180   190   200   200   280   300   330   210   250   320   340   220   350     0    60    90   180
60     0
```


JOB: Government Center Garage RUN: No Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35
0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
10.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	0.
20.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	2.	1.	0.
30.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.	2.	2.	1.
40.	0.	0.	0.	0.	0.	0.	1.	0.	1.	1.	0.	1.	2.	2.	1.
50.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	0.	0.	1.	2.	1.
60.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	1.
70.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
80.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	1.	1.
90.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	0.	0	1.	1.
100.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
110.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.	1.
120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.	1.
130.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.
140.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	2.
150.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.
160.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
170.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
180.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.
190.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
200.	2.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
210.	2.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
220.	2.	1.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	2.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
240.	1.	1.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
250.	1.	1.	0.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
260.	1.	1.	0.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
270.	1.	1.	0.	0.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
280.	1.	1.	0.	0.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
290.	1.	1.	1.	0.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
300.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
310.	1.	2.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
320.	1.	2.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
330.	1.	2.	2.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.
340.	0.	1.	2.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.
350.	0.	1.	1.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.
360.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
MAX	2.	2.	2.	1.	1.	1.	1.	1.	1.	1.	1.	1.	2.	2.	2.
DEGR.	210	310	330	240	250	340	350	0	20	30	110	120	20	30	150

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:14: 6

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6049.9	5447.4	*	66.	290.	AG	0.	100.0	1.0	30.0	0.52	3.3
2.	Char/Merr WB	*	6250.4	5435.2	6333.8	5501.2	*	106.	52.	AG	0.	100.0	1.0	30.0	0.77	5.4
3.	Char/Merr NB R	*	6291.7	5369.7	6315.3	5353.7	*	29.	124.	AG	0.	100.0	1.0	10.0	0.14	1.5
4.	Char/Merr NB LTT	*	6280.4	5347.2	6430.5	5241.4	*	184.	125.	AG	0.	100.0	1.0	20.0	0.92	9.3
5.	Char/Merr EB	*	6104.2	5362.2	6060.5	5345.9	*	47.	250.	AG	0.	100.0	1.0	20.0	0.42	2.4
6.	Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.5	*	108.	14.	AG	0.	100.0	1.0	10.0	0.71	5.5
7.	Char/Cam SB TR	*	5360.8	4833.5	5398.9	4956.5	*	129.	17.	AG	0.	100.0	1.0	20.0	0.92	6.5
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	0.	100.0	1.0	20.0	0.27	2.2
9.	Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	0.	100.0	1.0	10.0	0.60	4.7
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.4	4650.0	*	74.	179.	AG	0.	100.0	1.0	20.0	0.71	3.7
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5214.1	4740.7	*	89.	271.	AG	0.	100.0	1.0	30.0	0.54	4.5
12.	Sud/Merr SB L	*	6532.7	5210.3	6487.5	5242.5	*	56.	305.	AG	0.	100.0	1.0	10.0	0.72	2.8
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6477.9	5214.2	*	47.	300.	AG	0.	100.0	1.0	30.0	0.24	2.4
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6673.5	5068.9	*	106.	150.	AG	0.	100.0	1.0	30.0	0.60	5.4
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6478.2	5118.7	*	53.	239.	AG	0.	100.0	1.0	40.0	0.38	2.7
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	0.	100.0	1.0	20.0	0.34	3.3
17.	Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6745.9	5240.5	*	52.	249.	AG	0.	100.0	1.0	30.0	0.43	2.7
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	877.	0.0	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1122.	0.0	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1326.	0.0	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	939.	0.0	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	849.	0.0	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1614.	0.0	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	950.	0.0	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1709.	0.0	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	318.	0.0	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	536.	0.0	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	0.0	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	373.	0.0	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	0.0	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1555.	0.0	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1648.	0.0	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	529.	0.0	1.0	78.0		

		*								
1.	Char/Merr SB	*	100	76	3.0	476	1600	0.03	1	3
2.	Char/Merr WB	*	100	76	3.0	703	1600	0.03	1	3
3.	Char/Merr NB R	*	100	45	3.0	116	1600	0.03	1	3
4.	Char/Merr NB LTT	*	100	71	3.0	709	1600	0.03	1	3
5.	Char/Merr EB	*	100	79	3.0	217	1600	0.03	1	3
6.	Char/Cam SB L	*	90	58	3.0	339	1600	0.03	1	3
7.	Char/Cam SB TR	*	90	71	3.0	457	1600	0.03	1	3
8.	Char/Cam WB LTTR	*	90	54	3.0	294	1600	0.03	1	3
9.	Char/Cam NB L	*	90	58	3.0	289	1600	0.03	1	3
10.	Char/Cam NB TR	*	90	71	3.0	354	1600	0.03	1	3

		*								
11.	Char/Cam EB TTTR	*	90	54	3.0	901	1600	0.03	1	3
12.	Sud/Merr SB L	*	100	86	3.0	104	1600	0.03	1	3
13.	Sud/Merr SB TTT	*	100	49	3.0	524	1600	0.03	1	3
14.	Sud/Merr NB TTTR	*	100	63	3.0	924	1600	0.03	1	3
15.	Sud/Merr EB LTTR	*	100	73	3.0	529	1600	0.03	1	3
16.	Sud/Sur SB LTT	*	100	53	3.0	455	1600	0.03	1	3
17.	Sud/Sur SEB	*	100	70	3.0	26	1600	0.03	1	3
18.	Sud/Sur EB TTR	*	100	77	3.0	373	1600	0.03	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Char/Merr NE1	*	6063.7	5511.0	6.0
2.	Char/Merr NE2	*	6133.9	5484.8	6.0
3.	Char/Merr NE3	*	6204.2	5458.5	6.0
4.	Char/Merr NE4	*	6265.6	5501.5	6.0
5.	Char/Merr NE5	*	6327.1	5544.5	6.0
6.	Char/Merr SE1	*	6443.7	5491.9	6.0
7.	Char/Merr SE2	*	6382.2	5448.9	6.0
8.	Char/Merr SE3	*	6320.8	5405.9	6.0
9.	Char/Merr SE4	*	6380.5	5360.4	6.0
10.	Char/Merr SE5	*	6440.1	5315.0	6.0
11.	Char/Merr SW1	*	6332.0	5249.0	6.0
12.	Char/Merr SW2	*	6272.3	5294.5	6.0
13.	Char/Merr SW3	*	6212.6	5339.9	6.0
14.	Char/Merr SW4	*	6141.6	5315.8	6.0
15.	Char/Merr SW5	*	6070.6	5291.7	6.0
16.	Char/Merr NW1	*	5902.1	5359.1	6.0
17.	Char/Merr NW2	*	5973.1	5383.2	6.0
18.	Char/Merr NW3	*	6044.1	5407.3	6.0
19.	Char/Merr NW4	*	5973.9	5433.5	6.0
20.	Char/Merr NW5	*	5903.6	5459.8	6.0
21.	Char/Cam NE1	*	5490.2	4963.0	6.0
22.	Char/Cam NE2	*	5459.0	4894.8	6.0
23.	Char/Cam NE3	*	5427.8	4826.6	6.0
24.	Char/Cam NE4	*	5500.4	4807.6	6.0
25.	Char/Cam NE5	*	5572.9	4788.7	6.0
26.	Char/Cam SE1	*	5553.9	4667.5	6.0
27.	Char/Cam SE2	*	5481.3	4686.5	6.0
28.	Char/Cam SE3	*	5408.7	4705.4	6.0
29.	Char/Cam SE4	*	5409.4	4630.4	6.0
30.	Char/Cam SE5	*	5410.1	4555.4	6.0
31.	Char/Cam SW1	*	5312.0	4561.9	6.0
32.	Char/Cam SW2	*	5310.7	4636.9	6.0
33.	Char/Cam SW3	*	5310.7	4711.9	6.0

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
34.	Char/Cam SW4	*	5235.6	4712.1	6.0
35.	Char/Cam SW5	*	5160.6	4711.9	6.0
36.	Char/Cam NW1	*	5167.9	4822.4	6.0
37.	Char/Cam NW2	*	5242.9	4822.1	6.0
38.	Char/Cam NW3	*	5317.9	4821.9	6.0
39.	Char/Cam NW4	*	5349.1	4890.1	6.0
40.	Char/Cam NW5	*	5380.3	4958.3	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	1.	0.	0.	0.	0.
10.	*	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	1.	0.	0.	1.	0.
20.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.		

0.	0.																		
30.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
60.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
0.	0.																		
70.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
1.	0.																		
80.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.
1.	1.																		
90.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.
1.	1.																		
100.	*	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.
1.	1.																		
110.	*	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.
1.	1.																		
120.	*	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.
1.	0.																		
130.	*	1.	1.	1.	1.	0.	0.	0.	1.	1.	1.	0.	1.	1.	0.	0.	0.	0.	0.
0.	0.																		
140.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	2.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
150.	*	1.	1.	1.	2.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
160.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
170.	*	1.	0.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
180.	*	1.	0.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
190.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
200.	*	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
230.	*	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
240.	*	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
250.	*	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
260.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
270.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	1.	0.	0.	0.
0.	0.																		

MAX	*	1.	1.	1.	2.	1.	1.	1.	1.	1.	2.	1.	1.	1.	1.	1.	1.	1.	1.
1.	1.																		
DEGR.	*	120	120	120	150	200	250	270	270	150	140	110	0	40	40	50	80	80	70
90	90																		

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38

REC39 REC40

0.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
1.	0.																		
50.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
1.	0.																		
60.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
1.	0.																		
70.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.
1.	0.																		
80.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.
1.	0.																		
90.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.
1.	0.																		
100.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.	1.
1.	1.																		
110.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.
1.	1.																		
120.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	1.																		
130.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	1.																		
140.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.
1.	1.																		
150.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
160.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
170.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	2.																		
180.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	2.																		
190.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
200.	*	0.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
230.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
240.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
250.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
260.	*	0.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
270.	*	0.	1.	1.	1.	1.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	1.	1.	1.	1.	1.	1.	2.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
290.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		

MAX	*	1.	1.	1.	1.	1.	1.	1.	2.	1.	1.	1.	1.	1.	2.	1.	1.	1.	2.
1.	2.																		
DEGR.	*	220	240	240	260	260	300	290	280	320	330	20	40	20	50	70	110	110	110
140	170																		

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC34.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:13:37

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6036.0	5452.4	*	80.	290.	AG	0.	100.0	1.0	30.0	0.61	4.1
2. Char/Merr WB	*	6250.4	5435.2	6303.9	5477.6	*	68.	52.	AG	0.	100.0	1.0	30.0	0.59	3.5
3. Char/Merr NB R	*	6291.7	5369.7	6345.2	5333.4	*	65.	124.	AG	0.	100.0	1.0	10.0	0.33	3.3
4. Char/Merr NB LTT	*	6280.4	5347.2	6359.4	5291.5	*	97.	125.	AG	0.	100.0	1.0	20.0	0.60	4.9
5. Char/Merr EB	*	6104.2	5362.2	5973.2	5313.5	*	140.	250.	AG	0.	100.0	1.0	20.0	0.91	7.1
6. Char/Cam SB L	*	5384.1	4834.2	5402.3	4907.1	*	75.	14.	AG	0.	100.0	1.0	10.0	0.41	3.8
7. Char/Cam SB TR	*	5360.8	4833.5	5375.6	4881.2	*	50.	17.	AG	0.	100.0	1.0	20.0	0.35	2.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	0.	100.0	1.0	20.0	0.41	3.7
9. Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	0.	100.0	1.0	10.0	0.53	5.0
10. Char/Cam NB TR	*	5383.3	4723.8	5384.9	4614.7	*	109.	179.	AG	0.	100.0	1.0	20.0	0.73	5.5
11. Char/Cam EB TTTR	*	5302.7	4739.8	5211.5	4740.8	*	91.	271.	AG	0.	100.0	1.0	30.0	0.51	4.6
12. Sud/Merr SB L	*	6532.7	5210.3	6492.2	5239.1	*	50.	305.	AG	0.	100.0	1.0	10.0	0.60	2.5
13. Sud/Merr SB TTT	*	6518.3	5190.8	6484.0	5210.7	*	40.	300.	AG	0.	100.0	1.0	30.0	0.20	2.0
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6677.8	5061.4	*	115.	150.	AG	0.	100.0	1.0	30.0	0.69	5.8
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6452.9	5103.5	*	82.	239.	AG	0.	100.0	1.0	40.0	0.57	4.2
16. Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	0.	100.0	1.0	20.0	0.53	4.1
17. Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6715.8	5228.7	*	84.	249.	AG	0.	100.0	1.0	30.0	0.43	4.3
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	921.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1336.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1354.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	940.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	863.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1593.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1023.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1636.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	901.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	488.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	928.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1317.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1611.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	837.	0.0	1.0	78.0		

DATE : 8/ 7/13
TIME : 17:13:37

1. Char/Merr SB	*	100	75	3.0	589	1600	0.03	1	3
2. Char/Merr WB	*	100	78	3.0	481	1600	0.03	1	3
3. Char/Merr NB R	*	100	46	3.0	257	1600	0.03	1	3
4. Char/Merr NB LTT	*	100	68	3.0	520	1600	0.03	1	3
5. Char/Merr EB	*	100	79	3.0	468	1600	0.03	1	3
6. Char/Cam SB L	*	100	60	3.0	229	1600	0.03	1	3
7. Char/Cam SB TR	*	100	72	3.0	254	1600	0.03	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	435	1600	0.03	1	3
9. Char/Cam NB L	*	100	60	3.0	299	1600	0.03	1	3
10. Char/Cam NB TR	*	100	72	3.0	536	1600	0.03	1	3

11. Char/Cam EB TTTR	*	100	62	3.0	809	1600	0.03	1	3
12. Sud/Merr SB L	*	100	84	3.0	106	1600	0.03	1	3
13. Sud/Merr SB TTT	*	100	50	3.0	435	1600	0.03	1	3
14. Sud/Merr NB TTTR	*	100	66	3.0	954	1600	0.03	1	3
15. Sud/Merr EB LTTR	*	100	72	3.0	837	1600	0.03	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	424	1600	0.03	1	3
17. Sud/Sur SEB	*	100	80	3.0	37	1600	0.03	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	928	1600	0.03	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Char/Merr NE1	*	6063.7	5511.0	6.0
2. Char/Merr NE2	*	6133.9	5484.8	6.0
3. Char/Merr NE3	*	6204.2	5458.5	6.0
4. Char/Merr NE4	*	6265.6	5501.5	6.0
5. Char/Merr NE5	*	6327.1	5544.5	6.0
6. Char/Merr SE1	*	6443.7	5491.9	6.0
7. Char/Merr SE2	*	6382.2	5448.9	6.0
8. Char/Merr SE3	*	6320.8	5405.9	6.0
9. Char/Merr SE4	*	6380.5	5360.4	6.0
10. Char/Merr SE5	*	6440.1	5315.0	6.0
11. Char/Merr SW1	*	6332.0	5249.0	6.0
12. Char/Merr SW2	*	6272.3	5294.5	6.0
13. Char/Merr SW3	*	6212.6	5339.9	6.0
14. Char/Merr SW4	*	6141.6	5315.8	6.0
15. Char/Merr SW5	*	6070.6	5291.7	6.0
16. Char/Merr NW1	*	5902.1	5359.1	6.0
17. Char/Merr NW2	*	5973.1	5383.2	6.0
18. Char/Merr NW3	*	6044.1	5407.3	6.0
19. Char/Merr NW4	*	5973.9	5433.5	6.0
20. Char/Merr NW5	*	5903.6	5459.8	6.0
21. Char/Cam NE1	*	5490.2	4963.0	6.0
22. Char/Cam NE2	*	5459.0	4894.8	6.0
23. Char/Cam NE3	*	5427.8	4826.6	6.0
24. Char/Cam NE4	*	5500.4	4807.6	6.0
25. Char/Cam NE5	*	5572.9	4788.7	6.0
26. Char/Cam SE1	*	5553.9	4667.5	6.0
27. Char/Cam SE2	*	5481.3	4686.5	6.0
28. Char/Cam SE3	*	5408.7	4705.4	6.0
29. Char/Cam SE4	*	5409.4	4630.4	6.0
30. Char/Cam SE5	*	5410.1	4555.4	6.0
31. Char/Cam SW1	*	5312.0	4561.9	6.0
32. Char/Cam SW2	*	5310.7	4636.9	6.0
33. Char/Cam SW3	*	5310.7	4711.9	6.0

DATE : 8/ 7/13
TIME : 17:13:37

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Char/Cam SW4	*	5235.6	4712.1	6.0
35. Char/Cam SW5	*	5160.6	4711.9	6.0
36. Char/Cam NW1	*	5167.9	4822.4	6.0
37. Char/Cam NW2	*	5242.9	4822.1	6.0
38. Char/Cam NW3	*	5317.9	4821.9	6.0
39. Char/Cam NW4	*	5349.1	4890.1	6.0
40. Char/Cam NW5	*	5380.3	4958.3	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	1.	0.	0.	1.	0.	0.
10.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
20.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.		

0.	0.																		
30.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
60.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.
1.	0.																		
70.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	0.																		
80.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
90.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
100.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
110.	*	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
120.	*	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
130.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	1.	1.	0.	0.	0.	1.	1.
0.	0.																		
140.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
150.	*	1.	1.	1.	2.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
160.	*	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
170.	*	1.	0.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
180.	*	1.	0.	1.	1.	1.	0.	0.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
190.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
200.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
230.	*	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
240.	*	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
250.	*	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
260.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
270.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.
0.	0.																		
310.	*	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	1.	0.	0.	1.
0.	0.																		

MAX	*	1.	1.	2.	2.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
1.	1.																		
DEGR.	*	140	120	140	150	210	260	270	280	270	140	0	0	30	40	0	80	100	70
90	100																		

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38

REC39 REC40

0.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
0.	0.																		
60.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
0.	0.																		
70.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
80.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
90.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.
0.	0.																		
100.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.
1.	0.																		
110.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.
1.	0.																		
120.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	0.																		
130.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	0.																		
140.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	1.																		
150.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	1.																		
160.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
170.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
180.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
190.	*	0.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
200.	*	0.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
1.	1.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	0.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
230.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
240.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
250.	*	0.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
260.	*	0.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
270.	*	0.	0.	1.	1.	1.	0.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	0.	1.	1.	1.	1.	1.	2.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	1.	0.	0.	1.	1.	2.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		

MAX	*	1.	1.	1.	1.	1.	1.	1.	2.	1.	1.	1.	1.	1.	2.	1.	1.	1.	2.
1.	1.																		
DEGR.	*	220	240	250	250	260	300	290	280	320	330	20	40	30	60	70	130	110	110
160	180																		

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC34.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:44:58

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6049.9	5447.4	*	66.	290.	AG	0.	100.0	1.0	30.0	0.52	3.3
2. Char/Merr WB	*	6250.4	5435.2	6333.8	5501.2	*	106.	52.	AG	0.	100.0	1.0	30.0	0.77	5.4
3. Char/Merr NB R	*	6291.7	5369.7	6315.3	5353.7	*	29.	124.	AG	0.	100.0	1.0	10.0	0.14	1.5
4. Char/Merr NB LTT	*	6280.4	5347.2	6430.5	5241.4	*	184.	125.	AG	0.	100.0	1.0	20.0	0.92	9.3
5. Char/Merr EB	*	6104.2	5362.2	6060.5	5345.9	*	47.	250.	AG	0.	100.0	1.0	20.0	0.42	2.4
6. Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.5	*	108.	14.	AG	0.	100.0	1.0	10.0	0.71	5.5
7. Char/Cam SB TR	*	5360.8	4833.5	5398.9	4956.5	*	129.	17.	AG	0.	100.0	1.0	20.0	0.92	6.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	0.	100.0	1.0	20.0	0.27	2.2
9. Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	0.	100.0	1.0	10.0	0.60	4.7
10. Char/Cam NB TR	*	5383.3	4723.8	5384.4	4650.0	*	74.	179.	AG	0.	100.0	1.0	20.0	0.71	3.7
11. Char/Cam EB TTTR	*	5302.7	4739.8	5214.1	4740.7	*	89.	271.	AG	0.	100.0	1.0	30.0	0.54	4.5
12. Sud/Merr SB L	*	6532.7	5210.3	6487.5	5242.5	*	56.	305.	AG	0.	100.0	1.0	10.0	0.72	2.8
13. Sud/Merr SB TTT	*	6518.3	5190.8	6477.9	5214.2	*	47.	300.	AG	0.	100.0	1.0	30.0	0.24	2.4
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6673.5	5068.9	*	106.	150.	AG	0.	100.0	1.0	30.0	0.60	5.4
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6478.2	5118.7	*	53.	239.	AG	0.	100.0	1.0	40.0	0.38	2.7
16. Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	0.	100.0	1.0	20.0	0.34	3.3
17. Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6745.9	5240.5	*	52.	249.	AG	0.	100.0	1.0	30.0	0.43	2.7
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	877.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1122.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1326.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	939.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	849.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1614.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	950.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1709.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	318.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	536.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	373.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1555.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1648.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	529.	0.0	1.0	78.0		

JOB: Government Center Garage RUN: 2028NB

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1. Char/Merr SB	*	100	76	3.0	476	1600	0.03	1	3
2. Char/Merr WB	*	100	76	3.0	703	1600	0.03	1	3
3. Char/Merr NB R	*	100	45	3.0	116	1600	0.03	1	3
4. Char/Merr NB LTT	*	100	71	3.0	709	1600	0.03	1	3
5. Char/Merr EB	*	100	79	3.0	217	1600	0.03	1	3
6. Char/Cam SB L	*	90	58	3.0	339	1600	0.03	1	3
7. Char/Cam SB TR	*	90	71	3.0	457	1600	0.03	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	294	1600	0.03	1	3
9. Char/Cam NB L	*	90	58	3.0	289	1600	0.03	1	3
10. Char/Cam NB TR	*	90	71	3.0	354	1600	0.03	1	3

11. Char/Cam EB TTTR	*	90	54	3.0	901	1600	0.03	1	3
12. Sud/Merr SB L	*	100	86	3.0	104	1600	0.03	1	3
13. Sud/Merr SB TTT	*	100	49	3.0	524	1600	0.03	1	3
14. Sud/Merr NB TTTR	*	100	63	3.0	924	1600	0.03	1	3
15. Sud/Merr EB LTTR	*	100	73	3.0	529	1600	0.03	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	455	1600	0.03	1	3
17. Sud/Sur SEB	*	100	70	3.0	26	1600	0.03	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	373	1600	0.03	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Sud/Merr NE1	*	6492.5	5309.9	6.0
2. Sud/Merr NE2	*	6554.8	5268.0	6.0
3. Sud/Merr NE3	*	6616.2	5224.9	6.0
4. Sud/Merr NE4	*	6684.7	5255.3	6.0
5. Sud/Merr NE5	*	6753.3	5285.7	6.0
6. Sud/Merr SE1	*	6792.9	5222.3	6.0
7. Sud/Merr SE2	*	6724.3	5191.9	6.0
8. Sud/Merr SE3	*	6655.7	5161.5	6.0
9. Sud/Merr SE4	*	6695.5	5097.9	6.0
10. Sud/Merr SE5	*	6735.2	5034.3	6.0
11. Sud/Merr SW1	*	6638.6	4981.3	6.0
12. Sud/Merr SW2	*	6598.9	5045.0	6.0
13. Sud/Merr SW3	*	6559.1	5108.6	6.0
14. Sud/Merr SW4	*	6493.4	5072.5	6.0
15. Sud/Merr SW5	*	6427.6	5036.5	6.0
16. Sud/Merr NW1	*	6347.8	5104.5	6.0
17. Sud/Merr NW2	*	6413.5	5140.5	6.0
18. Sud/Merr NW3	*	6479.3	5176.6	6.0
19. Sud/Merr NW4	*	6417.1	5218.5	6.0
20. Sud/Merr NW5	*	6354.9	5260.4	6.0
21. Sud/Sur NE1	*	6755.9	5445.7	6.0
22. Sud/Sur NE2	*	6801.0	5385.7	6.0
23. Sud/Sur NE3	*	6846.0	5325.7	6.0
24. Sud/Sur NE4	*	6908.8	5366.8	6.0
25. Sud/Sur NE5	*	6971.5	5407.9	6.0
26. Sud/Sur SE1	*	7002.4	5368.4	6.0
27. Sud/Sur SE2	*	6939.7	5327.3	6.0
28. Sud/Sur SE3	*	6876.9	5286.2	6.0
29. Sud/Sur SE4	*	6931.7	5235.0	6.0
30. Sud/Sur SE5	*	6986.5	5183.8	6.0
31. Sud/Sur SW1	*	6932.3	5133.1	6.0
32. Sud/Sur SE2	*	6877.5	5184.3	6.0
33. Sud/Sur SE3	*	6822.7	5235.5	6.0

JOB: Government Center Garage RUN: 2028NB

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RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Sud/Sur SE4	*	6754.2	5205.1	6.0
35. Sud/Sur SE5	*	6685.6	5174.8	6.0
36. Sud/Sur NW1	*	6645.5	5237.9	6.0
37. Sud/Sur NW2	*	6714.1	5268.3	6.0
38. Sud/Sur NW3	*	6782.7	5298.7	6.0
39. Sud/Sur NW4	*	6709.5	5315.4	6.0
40. Sud/Sur NW5	*	6636.4	5332.0	6.0
41. Sud/Sur N1	*	6642.4	5493.7	6.0
42. Sud/Sur N2	*	6687.4	5433.7	6.0
43. Sud/Sur N3	*	6732.4	5373.8	6.0
44. Sud/Sur N4	*	6659.3	5390.4	6.0
45. Sud/Sur N5	*	6586.2	5407.1	6.0

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

0.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.
10.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.
20.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.
30.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.
40.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.
60.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.
70.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.
80.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.
90.	*	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.
100.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.
110.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.
120.	*	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.
130.	*	1.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	1.	1.
140.	*	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	1.
150.	*	1.	1.	1.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
160.	*	1.	1.	1.	0.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
170.	*	1.	1.	1.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
180.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
190.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
200.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
220.	*	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
240.	*	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
250.	*	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
260.	*	1.	1.	1.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.
270.	*	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
280.	*	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.
290.	*	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.	0.	0.	0.	0.	0.
300.	*	1.	1.	1.	0.	0.	1.	0.	1.	2.	1.	0.	0.	1.	0.	0.	0.	0.	1.
310.	*	0.	0.	0.	0.	0.	1.	0.	1.	1.	1.	0.	1.	1.	0.	0.	0.	0.	1.
320.	*	0.	0.	0.	0.	0.	1.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.	1.
330.	*	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	1.
340.	*	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
350.	*	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
360.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.

MAX	*	1.	1.	1.	1.	1.	1.	1.	2.	2.	1.	1.	1.	1.	1.	1.	1.	1.	1.
DEGR.	*	160	150	160	190	200	290	250	290	290	310	330	10	310	0	30	80	90	120

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.
10.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.
20.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.
30.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
40.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
60.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
70.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
80.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
90.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
100.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
110.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
120.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
130.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
140.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
150.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
160.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.
170.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
180.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.	0.	1.
190.	*	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.
200.	*	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.
210.	*	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.
220.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.
230.	*	0.	1.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.
240.	*	0.	0.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
250.	*	0.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.
260.	*	0.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.
270.	*	0.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.
280.	*	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.
290.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.
300.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	1.	0.	0.	0.	0.	0.
310.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
320.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
330.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
340.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
350.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
360.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.

MAX	*	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.
DEGR.	*	190	210	220	210	200	230	250	250	270	280	270	260	280	250	280	240	230	200		

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	0.	0.	0.
10.	0.	0.	0.	0.	0.
20.	0.	0.	0.	0.	0.
30.	0.	0.	0.	0.	0.
40.	0.	0.	0.	0.	0.
50.	0.	0.	0.	0.	0.
60.	0.	0.	0.	0.	0.
70.	0.	0.	0.	0.	0.
80.	0.	0.	0.	0.	0.
90.	0.	0.	0.	0.	0.
100.	0.	0.	0.	0.	0.
110.	0.	0.	0.	0.	0.
120.	0.	0.	0.	0.	0.
130.	0.	0.	0.	0.	0.
140.	0.	0.	0.	0.	0.
150.	0.	0.	0.	0.	0.
160.	0.	0.	0.	0.	0.
170.	0.	0.	0.	0.	0.
180.	0.	0.	0.	0.	0.
190.	0.	0.	0.	0.	0.
200.	0.	0.	0.	0.	0.
210.	0.	0.	0.	0.	0.
220.	0.	0.	0.	0.	0.
230.	0.	0.	0.	0.	0.
240.	0.	0.	0.	0.	0.
250.	0.	0.	0.	0.	0.
260.	1.	0.	0.	0.	0.
270.	0.	0.	0.	0.	0.
280.	0.	0.	0.	0.	0.
290.	0.	0.	0.	0.	0.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	0.	0.	0.
360.	0.	0.	0.	0.	0.
MAX	1.	0.	0.	0.	0.
DEGR.	260	130	10	180	190

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC9 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028NB

DATE : 8/ 7/13
TIME : 17:11:58

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6036.0	5452.4	*	80.	290.	AG	0.	100.0	1.0	30.0	0.61	4.1
2. Char/Merr WB	*	6250.4	5435.2	6303.9	5477.6	*	68.	52.	AG	0.	100.0	1.0	30.0	0.59	3.5
3. Char/Merr NB R	*	6291.7	5369.7	6345.2	5333.4	*	65.	124.	AG	0.	100.0	1.0	10.0	0.33	3.3
4. Char/Merr NB LTT	*	6280.4	5347.2	6359.4	5291.5	*	97.	125.	AG	0.	100.0	1.0	20.0	0.60	4.9
5. Char/Merr EB	*	6104.2	5362.2	5973.2	5313.5	*	140.	250.	AG	0.	100.0	1.0	20.0	0.91	7.1
6. Char/Cam SB L	*	5384.1	4834.2	5402.3	4907.1	*	75.	14.	AG	0.	100.0	1.0	10.0	0.41	3.8
7. Char/Cam SB TR	*	5360.8	4833.5	5375.6	4881.2	*	50.	17.	AG	0.	100.0	1.0	20.0	0.35	2.5
8. Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	0.	100.0	1.0	20.0	0.41	3.7
9. Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	0.	100.0	1.0	10.0	0.53	5.0
10. Char/Cam NB TR	*	5383.3	4723.8	5384.9	4614.7	*	109.	179.	AG	0.	100.0	1.0	20.0	0.73	5.5
11. Char/Cam EB TTTR	*	5302.7	4739.8	5211.5	4740.8	*	91.	271.	AG	0.	100.0	1.0	30.0	0.51	4.6
12. Sud/Merr SB L	*	6532.7	5210.3	6492.2	5239.1	*	50.	305.	AG	0.	100.0	1.0	10.0	0.60	2.5
13. Sud/Merr SB TTT	*	6518.3	5190.8	6484.0	5210.7	*	40.	300.	AG	0.	100.0	1.0	30.0	0.20	2.0
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6677.8	5061.4	*	115.	150.	AG	0.	100.0	1.0	30.0	0.69	5.8
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6452.9	5103.5	*	82.	239.	AG	0.	100.0	1.0	40.0	0.57	4.2
16. Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	0.	100.0	1.0	20.0	0.53	4.1
17. Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6715.8	5228.7	*	84.	249.	AG	0.	100.0	1.0	30.0	0.43	4.3
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	921.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1336.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1354.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	940.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	863.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1593.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1023.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1636.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	901.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	488.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	928.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1317.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1611.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	837.	0.0	1.0	78.0		

1. Char/Merr SB	*	100	75	3.0	589	1600	0.03	1	3
2. Char/Merr WB	*	100	78	3.0	481	1600	0.03	1	3
3. Char/Merr NB R	*	100	46	3.0	257	1600	0.03	1	3
4. Char/Merr NB LTT	*	100	68	3.0	520	1600	0.03	1	3
5. Char/Merr EB	*	100	79	3.0	468	1600	0.03	1	3
6. Char/Cam SB L	*	100	60	3.0	229	1600	0.03	1	3
7. Char/Cam SB TR	*	100	72	3.0	254	1600	0.03	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	435	1600	0.03	1	3
9. Char/Cam NB L	*	100	60	3.0	299	1600	0.03	1	3
10. Char/Cam NB TR	*	100	72	3.0	536	1600	0.03	1	3

11. Char/Cam EB TTTR	*	100	62	3.0	809	1600	0.03	1	3
12. Sud/Merr SB L	*	100	84	3.0	106	1600	0.03	1	3
13. Sud/Merr SB TTT	*	100	50	3.0	435	1600	0.03	1	3
14. Sud/Merr NB TTTR	*	100	66	3.0	954	1600	0.03	1	3
15. Sud/Merr EB LTTR	*	100	72	3.0	837	1600	0.03	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	424	1600	0.03	1	3
17. Sud/Sur SEB	*	100	80	3.0	37	1600	0.03	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	928	1600	0.03	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Sud/Merr NE1	*	6492.5	5309.9	6.0
2. Sud/Merr NE2	*	6554.8	5268.0	6.0
3. Sud/Merr NE3	*	6616.2	5224.9	6.0
4. Sud/Merr NE4	*	6684.7	5255.3	6.0
5. Sud/Merr NE5	*	6753.3	5285.7	6.0
6. Sud/Merr SE1	*	6792.9	5222.3	6.0
7. Sud/Merr SE2	*	6724.3	5191.9	6.0
8. Sud/Merr SE3	*	6655.7	5161.5	6.0
9. Sud/Merr SE4	*	6695.5	5097.9	6.0
10. Sud/Merr SE5	*	6735.2	5034.3	6.0
11. Sud/Merr SW1	*	6638.6	4981.3	6.0
12. Sud/Merr SW2	*	6598.9	5045.0	6.0
13. Sud/Merr SW3	*	6559.1	5108.6	6.0
14. Sud/Merr SW4	*	6493.4	5072.5	6.0
15. Sud/Merr SW5	*	6427.6	5036.5	6.0
16. Sud/Merr NW1	*	6347.8	5104.5	6.0
17. Sud/Merr NW2	*	6413.5	5140.5	6.0
18. Sud/Merr NW3	*	6479.3	5176.6	6.0
19. Sud/Merr NW4	*	6417.1	5218.5	6.0
20. Sud/Merr NW5	*	6354.9	5260.4	6.0
21. Sud/Sur NE1	*	6755.9	5445.7	6.0
22. Sud/Sur NE2	*	6801.0	5385.7	6.0
23. Sud/Sur NE3	*	6846.0	5325.7	6.0
24. Sud/Sur NE4	*	6908.8	5366.8	6.0
25. Sud/Sur NE5	*	6971.5	5407.9	6.0
26. Sud/Sur SE1	*	7002.4	5368.4	6.0
27. Sud/Sur SE2	*	6939.7	5327.3	6.0
28. Sud/Sur SE3	*	6876.9	5286.2	6.0
29. Sud/Sur SE4	*	6931.7	5235.0	6.0
30. Sud/Sur SE5	*	6986.5	5183.8	6.0
31. Sud/Sur SW1	*	6932.3	5133.1	6.0
32. Sud/Sur SE2	*	6877.5	5184.3	6.0
33. Sud/Sur SE3	*	6822.7	5235.5	6.0

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Sud/Sur SE4	*	6754.2	5205.1	6.0
35. Sud/Sur SE5	*	6685.6	5174.8	6.0
36. Sud/Sur NW1	*	6645.5	5237.9	6.0
37. Sud/Sur NW2	*	6714.1	5268.3	6.0
38. Sud/Sur NW3	*	6782.7	5298.7	6.0
39. Sud/Sur NW4	*	6709.5	5315.4	6.0
40. Sud/Sur NW5	*	6636.4	5332.0	6.0
41. Sud/Sur N1	*	6642.4	5493.7	6.0
42. Sud/Sur N2	*	6687.4	5433.7	6.0
43. Sud/Sur N3	*	6732.4	5373.8	6.0
44. Sud/Sur N4	*	6659.3	5390.4	6.0
45. Sud/Sur N5	*	6586.2	5407.1	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

0.	*	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
10.	*	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
20.	*	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
30.	*	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	1.																		
40.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	1.																		
60.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.
0.	1.																		
70.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
80.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
90.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.
1.	1.																		
100.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.
1.	1.																		
110.	*	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.
1.	1.																		
120.	*	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.
1.	1.																		
130.	*	1.	1.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.
1.	1.																		
140.	*	1.	1.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.
1.	1.																		
150.	*	1.	1.	1.	0.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
1.	0.																		
160.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
170.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
180.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
190.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
200.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
230.	*	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
240.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
250.	*	1.	0.	1.	1.	1.	1.	1.	2.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
260.	*	1.	1.	1.	0.	0.	1.	1.	2.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
270.	*	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
290.	*	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	1.																		
300.	*	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	1.	1.	1.	0.	0.	0.	0.
1.	1.																		
310.	*	0.	0.	0.	0.	0.	1.	0.	1.	2.	2.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
320.	*	0.	0.	0.	0.	0.	1.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
330.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
340.	*	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
350.	*	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
360.	*	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		

MAX	*	1.	1.	2.	1.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	1.	1.	1.
1.	1.																		
DEGR.	*	160	150	170	230	220	270	260	280	300	310	350	30	310	0	30	80	100	110
110	330																		

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38
REC39	REC40																		
0.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
0.	0.																		
60.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
70.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
80.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
0.	0.																		
90.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
100.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
110.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
120.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
0.	0.																		
130.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
0.	0.																		
140.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
0.	0.																		
150.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
160.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
170.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	1.																		
180.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	1.																		
190.	*	1.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	0.																		
200.	*	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	1.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	0.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	1.																		
230.	*	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
0.	0.																		
240.	*	1.	1.	1.	1.	0.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.
0.	0.																		
250.	*	0.	1.	1.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.
0.	0.																		
260.	*	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.
0.	0.																		
270.	*	0.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
280.	*	0.	1.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.
0.	0.																		
290.	*	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.
0.	0.																		
300.	*	0.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		

MAX	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	1.	1.
1.	1.																		
DEGR.	*	220	220	230	230	220	250	250	250	260	260	270	260	260	250	260	180	230	230

JOB: Government Center Garage RUN: 2028NB

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	0.	0.	0.
10.	0.	0.	0.	0.	0.
20.	0.	0.	0.	0.	0.
30.	0.	0.	0.	0.	0.
40.	0.	0.	0.	0.	0.
50.	0.	0.	0.	0.	0.
60.	0.	0.	0.	0.	0.
70.	0.	0.	0.	0.	0.
80.	0.	0.	0.	0.	0.
90.	0.	0.	0.	0.	0.
100.	0.	0.	0.	0.	0.
110.	0.	1.	0.	0.	0.
120.	0.	1.	0.	0.	0.
130.	0.	1.	0.	0.	0.
140.	0.	0.	0.	0.	0.
150.	0.	0.	0.	0.	0.
160.	0.	0.	0.	0.	0.
170.	0.	0.	0.	0.	0.
180.	0.	0.	0.	0.	1.
190.	0.	0.	1.	0.	0.
200.	0.	0.	0.	1.	0.
210.	0.	0.	0.	0.	0.
220.	0.	0.	0.	0.	0.
230.	0.	0.	0.	0.	0.
240.	0.	0.	0.	0.	0.
250.	0.	0.	0.	0.	0.
260.	0.	0.	0.	0.	0.
270.	0.	0.	0.	0.	0.
280.	0.	0.	0.	0.	0.
290.	0.	0.	0.	0.	0.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	0.	0.	0.
360.	0.	0.	0.	0.	0.
MAX	0.	1.	1.	1.	1.
DEGR.	260	110	190	200	180

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC8 .

2028 Build
Microscale Output Files
(Particulate Matter 2.5 (PM2.5))

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16: 9: 0

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	0.	100.0	1.0	10.0	0.71 7.8
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5105.0	6035.3	*	120.	325.	AG	0.	100.0	1.0	20.0	0.55 6.1
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	0.	100.0	1.0	20.0	0.92 9.6
4.	Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	0.	100.0	1.0	10.0	0.58 6.4
5.	Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	0.	100.0	1.0	10.0	0.64 4.1
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5366.6	5747.7	*	55.	109.	AG	0.	100.0	1.0	20.0	0.44 2.8
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	0.	100.0	1.0	20.0	0.68 4.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	0.	100.0	1.0	10.0	0.93 8.1
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6144.6	7708.0	*	931.	334.	AG	0.	100.0	1.0	40.0	1.09 47.3
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	0.	100.0	1.0	20.0	0.58 5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	0.	100.0	1.0	10.0	0.53 6.6
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6667.3	5333.6	*	1420.	177.	AG	0.	100.0	1.0	20.0	1.41 72.1
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	0.	100.0	1.0	30.0	0.47 4.6
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.6	6363.6	*	140.	358.	AG	0.	100.0	1.0	20.0	0.80 7.1
15.	Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	0.	100.0	1.0	10.0	1.23 59.7
16.	Tha/Val NB TR	*	6645.6	6138.6	6647.7	6016.6	*	122.	179.	AG	0.	100.0	1.0	10.0	0.70 6.2
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6099.5	*	136.	0.	AG	0.	100.0	1.0	30.0	0.69 6.9
18.	Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	0.	100.0	1.0	30.0	0.18 1.8
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.2	5885.7	*	146.	358.	AG	0.	100.0	1.0	40.0	0.75 7.4
20.	Char/93 WB LTT	*	6702.8	5647.8	6766.7	5567.9	*	102.	141.	AG	0.	100.0	1.0	20.0	0.65 5.2
21.	Char/93 EB TTR	*	6560.8	5622.5	6514.2	5588.4	*	58.	234.	AG	0.	100.0	1.0	30.0	0.37 2.9
22.	North/Congress SB LT	*	6876.6	4408.9	6575.8	5898.4	*	1520.	349.	AG	0.	100.0	1.0	30.0	2.65 77.2
23.	North/Con WB LLTR	*	6920.6	4378.3	7916.6	4730.8	*	1057.	71.	AG	0.	100.0	1.0	20.0	1.13 53.7
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6921.1	4287.3	*	47.	172.	AG	0.	100.0	1.0	30.0	0.34 2.4
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	0.	100.0	1.0	10.0	0.03 0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1464.	0.0	1.0	90.0	
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1588.	0.0	1.0	78.0	
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	967.	0.0	1.0	78.0	
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	0.0	1.0	78.0	
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3453.	0.0	1.0	90.0	
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	0.0	1.0	66.0	
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2405.	0.0	1.0	90.0	
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	0.0	1.0	78.0	
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2431.	0.0	1.0	90.0	
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	0.0	1.0	38.0	
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2871.	0.0	1.0	90.0	
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	0.0	1.0	54.0	
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2351.	0.0	1.0	66.0	
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	0.0	1.0	48.0	
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	542.	0.0	1.0	42.0	
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	0.0	1.0	48.0	
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	459.	0.0	1.0	54.0	
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	729.	0.0	1.0	54.0	

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	0.0	1.0	42.0	

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16: 9: 0

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1629.	0.0	1.0	98.0	
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1333.	0.0	1.0	66.0	
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1545.	0.0	1.0	98.0	
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	0.0	1.0	54.0	

JOB: Government Center Garage RUN: Build

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1.	Stan/Lom SB L	*	120	75	3.0	376	1600	0.03	1	3
2.	Stan/Lom SB TRR	*	120	75	3.0	585	1600	0.03	1	3
3.	Stan/Lom WB LTT	*	120	91	3.0	588	1600	0.03	1	3
4.	Stan/Lom WB R	*	120	75	3.0	308	1600	0.03	1	3
5.	Stan/Lom NB L	*	120	97	3.0	152	1600	0.03	1	3
6.	Stan/Lom NB TRR	*	120	97	3.0	208	1600	0.03	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	324	1600	0.03	1	3
8.	Stan/Lom EB R	*	120	97	3.0	222	1600	0.03	1	3
9.	Caus/Wash SB LTTRR	*	150	94	3.0	2380	1600	0.03	1	3
10.	Caus/Wash WB LLTT	*	150	119	3.0	321	1600	0.03	1	3
11.	Caus/Wash WB R	*	150	104	3.0	230	1600	0.03	1	3
12.	Caus/Wash NB TTR	*	150	120	3.0	748	1600	0.03	1	3
13.	Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	0.03	1	3
14.	Tha/Val SB LTTR	*	104	30	3.0	1705	1600	0.03	1	3
15.	Tha/Val NB L	*	104	74	3.0	472	1600	0.03	1	3
16.	Tha/Val NB TR	*	104	30	3.0	744	1600	0.03	1	3
17.	Bev/Was SB TTT	*	100	45	3.0	1655	1600	0.03	1	3
18.	Bev/Was EB RRR	*	100	55	3.0	356	1600	0.03	1	3
19.	Char/93 SB LLTTRR	*	100	53	3.0	2013	1600	0.03	1	3
20.	Char/93 WB LTT	*	100	69	3.0	542	1600	0.03	1	3
21.	Char/93 EB TTR	*	100	69	3.0	459	1600	0.03	1	3
22.	North/Congress SB LT	*	100	90	3.0	636	1600	0.03	1	3
23.	North/Con WB LLTR	*	100	60	3.0	1267	1600	0.03	1	3
24.	Nor/Con NB LTTTR	*	100	74	3.0	345	1600	0.03	1	3
25.	Nor/Con EB LTR	*	100	60	3.0	17	1600	0.03	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8.	Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0	*
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0	*
21.	Caus/Wash NE1	*	6548.3	7035.9	6.0	*
22.	Caus/Wash NE2	*	6581.4	6968.6	6.0	*
23.	Caus/Wash NE3	*	6614.5	6901.3	6.0	*
24.	Caus/Wash NE4	*	6669.8	6952.0	6.0	*
25.	Caus/Wash NE5	*	6725.0	7002.7	6.0	*
26.	Caus/Wash SE1	*	6753.6	6912.2	6.0	*

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
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RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Caus/Wash SE2	6698.9	6862.0	6.0
28. Caus/Wash SE3	6643.1	6810.8	6.0
29. Caus/Wash SE4	6646.8	6736.4	6.0
30. Caus/Wash SE5	6650.0	6661.0	6.0
31. Caus/Wash SW1	6544.0	6561.0	6.0
32. Caus/Wash SW2	6540.9	6636.0	6.0
33. Caus/Wash SW3	6537.8	6710.9	6.0
34. Caus/Wash SW4	6476.8	6667.2	6.0
35. Caus/Wash SW5	6415.9	6623.4	6.0
36. Caus/Wash NW1	6407.4	6738.0	6.0
37. Caus/Wash NW2	6468.3	6781.7	6.0
38. Caus/Wash NW3	6529.3	6825.4	6.0
39. Caus/Wash NW4	6496.2	6892.7	6.0
40. Caus/Wash NW5	6463.1	6960.0	6.0
41. Tha/Val NE1	6667.3	6395.5	6.0
42. Tha/Val NE2	6668.3	6320.5	6.0
43. Tha/Val NE3	6669.3	6245.5	6.0
44. Tha/Val NE4	6744.3	6245.5	6.0
45. Tha/Val NE5	6819.2	6249.6	6.0
46. Tha/Val SE1	6822.3	6191.6	6.0
47. Tha/Val SE2	6747.3	6189.6	6.0
48. Tha/Val SE3	6672.3	6187.5	6.0
49. Tha/Val SE4	6671.6	6112.5	6.0
50. Tha/Val SE5	6670.9	6037.5	6.0
51. Tha/Val SW1	6560.2	5964.7	6.0
52. Tha/Val SW2	6560.9	6039.7	6.0
53. Tha/Val SW3	6561.6	6114.7	6.0
54. Tha/Val SW4	6502.2	6068.9	6.0
55. Tha/Val SW5	6442.7	6023.2	6.0
56. Tha/Val NW1	6441.0	6115.2	6.0
57. Tha/Val NW2	6500.4	6160.9	6.0
58. Tha/Val NW3	6559.8	6206.7	6.0
59. Tha/Val NW4	6558.8	6281.7	6.0
60. Tha/Val NW5	6557.8	6356.7	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.
10.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.
20.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	1.
30.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.
40.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.
50.	0.	0.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
60.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
70.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
80.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
90.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	0.	1.	0.	0.	1.	1.	0.	1.	1.
100.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.
110.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
120.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
130.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.
140.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
150.	1.	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
160.	1.	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	2.	2.	2.	2.	1.	1.	1.	2.	2.	2.
10.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	2.	2.	2.	2.	1.	1.	1.	2.	2.	2.
20.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	2.	2.	2.	2.	1.	1.	1.	2.	2.	2.
30.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	2.	2.	2.	2.	1.	1.	2.	2.	2.
40.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	2.	2.	1.	1.	1.	1.	2.	2.
50.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	2.	2.
60.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	2.	2.
70.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	2.	2.
80.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	2.
90.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	2.	2.
100.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	2.
110.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	2.
120.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	2.
130.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	2.
140.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	2.
150.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	2.
160.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.	2.	2.
170.	0.	0.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
180.	0.	0.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
190.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
200.	0.	0.	1.	1.	1.	2.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.
210.	0.	0.	1.	1.	1.	2.	0.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.
220.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.
230.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.
240.	0.	0.	1.	1.	0.	0.	0.	1.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
250.	0.	0.	1.	1.	0.	0.	0.	1.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
260.	0.	0.	1.	1.	0.	0.	0.	1.	0.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.
270.	0.	0.	0.	1.	1.	0.	0.	1.	1.	0.	0.	1.	0.	0.	1.	1.	1.	0.	0.	0.
280.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
290.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
300.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
310.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
320.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
330.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
340.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.
350.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.
360.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.
MAX	1.	1.	1.	1.	1.	2.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
DEGR.	180	170	190	190	200	290	310	200	210	240	320	340	220	290	0	40	100	170	60	70

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

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 110. *   0.   0.   1.   1.   0.   0.   0.   0.   0.   1.   1.   1.   1.   0.   1.   1.   2.
2.   2.
 120. *   0.   0.   1.   1.   0.   0.   0.   0.   0.   1.   1.   1.   1.   0.   1.   1.   1.
2.   2.
 130. *   0.   0.   1.   1.   0.   0.   0.   0.   0.   0.   1.   1.   1.   1.   0.   1.   2.   2.
2.   2.
 140. *   0.   0.   1.   1.   0.   0.   0.   0.   0.   0.   1.   1.   1.   1.   0.   1.   2.   2.
2.   2.
 150. *   1.   1.   1.   1.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   0.   1.   2.   2.
2.   2.
 160. *   1.   1.   1.   1.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   2.   2.
2.   2.
 170. *   2.   2.   2.   1.   0.   0.   0.   1.   1.   1.   2.   2.   2.   1.   0.   1.   1.   2.
1.   1.
 180. *   3.   2.   3.   2.   1.   0.   1.   2.   1.   2.   1.   1.   1.   0.   0.   1.   1.   2.
1.   1.
 190. *   2.   2.   3.   2.   2.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   1.   1.
0.   0.
 200. *   2.   2.   2.   2.   2.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   1.   1.   1.
0.   0.
 210. *   2.   2.   2.   2.   2.   1.   1.   1.   1.   2.   0.   0.   0.   0.   0.   1.   1.   1.
0.   0.
 220. *   2.   2.   2.   2.   2.   1.   1.   1.   1.   1.   0.   0.   0.   0.   0.   0.   1.   1.
0.   0.
 230. *   2.   2.   2.   2.   1.   1.   1.   1.   2.   1.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 240. *   2.   2.   2.   1.   1.   1.   1.   2.   1.   1.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 250. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   1.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 260. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   1.   0.   0.   1.   1.   0.   0.   0.   0.
0.   0.
 270. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   1.   0.   0.   1.   1.   0.   0.   0.   0.
0.   0.
 280. *   2.   2.   2.   1.   1.   2.   2.   2.   2.   1.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 290. *   2.   2.   2.   1.   1.   2.   2.   2.   1.   2.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 300. *   2.   2.   2.   1.   1.   1.   2.   2.   1.   2.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 310. *   2.   2.   2.   1.   0.   1.   2.   2.   2.   2.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 320. *   2.   2.   2.   1.   0.   1.   2.   3.   2.   2.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 330. *   1.   1.   2.   0.   0.   0.   1.   2.   2.   2.   1.   1.   1.   1.   0.   0.   0.   1.
1.   1.
 340. *   0.   1.   1.   0.   0.   0.   1.   2.   2.   2.   1.   1.   2.   1.   0.   0.   0.   2.
2.   2.
 350. *   0.   0.   0.   0.   0.   0.   1.   1.   1.   2.   1.   2.   2.   1.   1.   0.   1.   3.
2.   2.
 360. *   0.   0.   0.   0.   0.   0.   1.   1.   1.   1.   2.   2.   2.   2.   1.   1.   1.   2.
2.   2.

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX   *   3.   2.   3.   2.   2.   2.   2.   3.   2.   2.   2.   2.   2.   2.   2.   1.   2.   3.
2.   2.
 DEGR. *  180   190   180   190   190   280   300   320   330   320    10     0    10    20    30    90   140   350
0   110
```


JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 WIND  * CONCENTRATION
 ANGLE *      (ug/m**3)
 (DEGR)* REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52 REC53 REC54 REC55 REC56 REC57 REC58
REC59 REC60

------*-------------------------------------------------------------------------------------------------------------
-------
   0. *   1.   1.   1.   0.   0.   0.   0.   1.   1.   1.   2.   1.   2.   1.   0.   0.   1.   1.
1.   1.
  10. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   2.
2.   2.
  20. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   0.   1.   2.
2.   2.
  30. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   0.   1.   2.
2.   1.
  40. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   1.
1.   1.
  50. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   1.
```



```
1.   1.
  60. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   1.
1.   1.
  70. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   1.
1.   1.
  80. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   1.
1.   1.
  90. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   1.   1.   1.   1.   1.   2.
1.   1.
 100. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   1.   1.   1.   1.   1.   2.
1.   1.
 110. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   1.   1.   1.   1.   1.   2.
1.   1.
 120. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   2.   1.   1.   1.   1.   2.
1.   1.
 130. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   1.   2.   2.   1.   1.   1.   1.   2.
1.   1.
 140. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   1.   1.   1.   1.   2.
2.   2.
 150. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   2.   2.   2.   2.   1.   1.   1.   2.
2.   2.
 160. *   0.   0.   0.   0.   0.   0.   0.   0.   0.   0.   3.   2.   2.   2.   1.   1.   2.   2.
2.   2.
 170. *   1.   1.   1.   0.   0.   0.   0.   1.   1.   1.   3.   2.   2.   1.   0.   0.   1.   2.
2.   2.
 180. *   2.   2.   2.   0.   0.   0.   0.   2.   1.   1.   2.   2.   2.   1.   0.   0.   1.   2.
2.   2.
 190. *   2.   2.   2.   1.   0.   0.   1.   2.   2.   2.   1.   1.   1.   0.   0.   0.   0.   1.
1.   1.
 200. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 210. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 220. *   1.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 230. *   1.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 240. *   1.   1.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 250. *   1.   1.   1.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 260. *   1.   1.   1.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 270. *   1.   1.   1.   1.   0.   0.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 280. *   1.   1.   1.   1.   0.   0.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 290. *   1.   1.   1.   1.   0.   0.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 300. *   1.   1.   1.   1.   0.   0.   1.   1.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 310. *   1.   1.   1.   1.   0.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 320. *   1.   2.   2.   1.   1.   1.   1.   2.   2.   2.   1.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 330. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   2.   0.   0.   0.   0.   0.   0.   0.   0.
0.   0.
 340. *   2.   2.   2.   1.   1.   1.   1.   2.   2.   3.   0.   0.   1.   0.   0.   0.   0.   0.
0.   0.
 350. *   2.   2.   2.   1.   0.   0.   1.   2.   2.   2.   1.   1.   1.   1.   0.   0.   0.   1.
1.   1.
 360. *   1.   1.   1.   0.   0.   0.   0.   1.   1.   1.   2.   1.   2.   1.   0.   0.   1.   1.
1.   1.

------*-------------------------------------------------------------------------------------------------------------
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 MAX   *   2.   2.   2.   1.   1.   1.   1.   2.   2.   3.   3.   2.   3.   2.   1.   1.   2.   2.
2.   2.
 DEGR. *  200   190   190   210   330   210   210   200   210   340   170   170   160   160   150   150   160   170
160   170
```

THE HIGHEST CONCENTRATION OF 3. ug/m**3 OCCURRED AT RECEPTOR REC51.

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16:10:43

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5108.1	6075.9	*	154.	326.	AG	0.	100.0	1.0	10.0	0.71 7.8
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5105.0	6035.3	*	120.	325.	AG	0.	100.0	1.0	20.0	0.55 6.1
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5453.6	6050.8	*	190.	51.	AG	0.	100.0	1.0	20.0	0.92 9.6
4.	Stan/Lom WB R	*	5292.4	5947.7	5392.6	6024.6	*	126.	52.	AG	0.	100.0	1.0	10.0	0.58 6.4
5.	Stan/Lom NB L	*	5307.6	5737.4	5385.1	5713.6	*	81.	107.	AG	0.	100.0	1.0	10.0	0.64 4.1
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5366.6	5747.7	*	55.	109.	AG	0.	100.0	1.0	20.0	0.44 2.8
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5189.9	5620.6	*	88.	196.	AG	0.	100.0	1.0	20.0	0.68 4.5
8.	Stan/Lom EB R	*	5236.5	5698.5	5192.6	5544.2	*	160.	196.	AG	0.	100.0	1.0	10.0	0.93 8.1
9.	Caus/Wash SB LTTRR	*	6548.6	6868.7	6144.6	7708.0	*	931.	334.	AG	0.	100.0	1.0	40.0	1.09 47.3
10.	Caus/Wash WB LLTT	*	6635.9	6867.8	6714.4	6936.1	*	104.	49.	AG	0.	100.0	1.0	20.0	0.58 5.3
11.	Caus/Wash WB R	*	6624.3	6883.3	6720.0	6972.4	*	131.	47.	AG	0.	100.0	1.0	10.0	0.53 6.6
12.	Caus/Wash NB TTR	*	6603.5	6751.9	6667.3	5333.6	*	1420.	177.	AG	0.	100.0	1.0	20.0	1.41 72.1
13.	Caus/Wash EB LLTTR	*	6538.7	6754.8	6465.2	6703.6	*	90.	235.	AG	0.	100.0	1.0	30.0	0.47 4.6
14.	Tha/Val SB LTTR	*	6599.0	6224.0	6593.6	6363.6	*	140.	358.	AG	0.	100.0	1.0	20.0	0.80 7.1
15.	Tha/Val NB L	*	6631.0	6138.6	6620.8	4964.2	*	1174.	180.	AG	0.	100.0	1.0	10.0	1.23 59.7
16.	Tha/Val NB TR	*	6645.6	6138.6	6647.7	6016.6	*	122.	179.	AG	0.	100.0	1.0	10.0	0.70 6.2
17.	Bev/Was SB TTT	*	6592.9	5963.9	6593.8	6099.5	*	136.	0.	AG	0.	100.0	1.0	30.0	0.69 6.9
18.	Bev/Was EB RRR	*	6545.9	5954.3	6525.4	5983.2	*	35.	325.	AG	0.	100.0	1.0	30.0	0.18 1.8
19.	Char/93 SB LLTTRR	*	6587.8	5740.0	6582.2	5885.7	*	146.	358.	AG	0.	100.0	1.0	40.0	0.75 7.4
20.	Char/93 WB LTT	*	6702.8	5647.8	6766.7	5567.9	*	102.	141.	AG	0.	100.0	1.0	20.0	0.65 5.2
21.	Char/93 EB TTR	*	6560.8	5622.5	6514.2	5588.4	*	58.	234.	AG	0.	100.0	1.0	30.0	0.37 2.9
22.	North/Congress SB LT	*	6876.6	4408.9	6575.8	5898.4	*	1520.	349.	AG	0.	100.0	1.0	30.0	2.65 77.2
23.	North/Con WB LLTR	*	6920.6	4378.3	7916.6	4730.8	*	1057.	71.	AG	0.	100.0	1.0	20.0	1.13 53.7
24.	Nor/Con NB LTTTR	*	6914.9	4333.4	6921.1	4287.3	*	47.	172.	AG	0.	100.0	1.0	30.0	0.34 2.4
25.	Nor/Con EB LTR	*	6869.7	4342.2	6864.3	4340.8	*	6.	256.	AG	0.	100.0	1.0	10.0	0.03 0.3
26.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1464.	0.0	1.0	90.0	
27.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1588.	0.0	1.0	78.0	
28.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	967.	0.0	1.0	78.0	
29.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1486.	0.0	1.0	78.0	
30.	Wash/Caus N	*	6596.9	6812.4	6408.3	7196.1	*	428.	334.	AG	3453.	0.0	1.0	90.0	
31.	Wash/Caus E	*	6592.0	6822.3	6793.8	7007.5	*	274.	47.	AG	1091.	0.0	1.0	66.0	
32.	Wash/Caus S	*	6588.7	6809.1	6603.5	6455.0	*	354.	178.	AG	2405.	0.0	1.0	90.0	
33.	Wash/Caus W	*	6583.8	6804.2	6263.9	6574.7	*	394.	234.	AG	1253.	0.0	1.0	78.0	
34.	Wash/Tha/Val N	*	6615.4	6167.3	6611.7	6439.1	*	272.	359.	AG	2431.	0.0	1.0	90.0	
35.	Wash/Tha/Val E	*	6617.2	6215.0	6951.7	6224.2	*	335.	88.	AG	39.	0.0	1.0	38.0	
36.	Wash/Tha/Val S	*	6617.4	6197.5	6614.7	5917.3	*	280.	181.	AG	2871.	0.0	1.0	90.0	
37.	Wash/Tha/Val W	*	6609.9	6198.5	6449.9	6075.4	*	202.	232.	AG	501.	0.0	1.0	54.0	
38.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2351.	0.0	1.0	66.0	
39.	Wash/Bev W	*	6569.6	5930.8	6486.7	6042.5	*	139.	323.	AG	356.	0.0	1.0	48.0	
40.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	542.	0.0	1.0	42.0	
41.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	903.	0.0	1.0	48.0	
42.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	459.	0.0	1.0	54.0	
43.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	729.	0.0	1.0	54.0	

44.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	457.	0.0	1.0	42.0	

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
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LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C QUEUE (VEH)
45.	North/Congress N	*	6888.9	4387.5	6808.2	4767.6	*	389.	348.	AG	1629.	0.0	1.0	98.0	
46.	North/Congress East	*	6893.5	4361.7	7106.5	4437.7	*	226.	70.	AG	1333.	0.0	1.0	66.0	
47.	North/Congress South	*	6884.6	4386.6	6960.4	3995.3	*	399.	169.	AG	1545.	0.0	1.0	98.0	
48.	North/Congress West	*	6893.5	4361.7	6745.2	4329.5	*	152.	258.	AG	47.	0.0	1.0	54.0	

JOB: Government Center Garage RUN: Build

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1.	Stan/Lom SB L	*	120	75	3.0	376	1600	0.03	1	3
2.	Stan/Lom SB TRR	*	120	75	3.0	585	1600	0.03	1	3
3.	Stan/Lom WB LTT	*	120	91	3.0	588	1600	0.03	1	3
4.	Stan/Lom WB R	*	120	75	3.0	308	1600	0.03	1	3
5.	Stan/Lom NB L	*	120	97	3.0	152	1600	0.03	1	3
6.	Stan/Lom NB TRR	*	120	97	3.0	208	1600	0.03	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	324	1600	0.03	1	3
8.	Stan/Lom EB R	*	120	97	3.0	222	1600	0.03	1	3
9.	Caus/Wash SB LTTRR	*	150	94	3.0	2380	1600	0.03	1	3
10.	Caus/Wash WB LLTT	*	150	119	3.0	321	1600	0.03	1	3
11.	Caus/Wash WB R	*	150	104	3.0	230	1600	0.03	1	3
12.	Caus/Wash NB TTR	*	150	120	3.0	748	1600	0.03	1	3
13.	Caus/Wash EB LLTTR	*	150	117	3.0	422	1600	0.03	1	3
14.	Tha/Val SB LTTR	*	104	30	3.0	1705	1600	0.03	1	3
15.	Tha/Val NB L	*	104	74	3.0	472	1600	0.03	1	3
16.	Tha/Val NB TR	*	104	30	3.0	744	1600	0.03	1	3
17.	Bev/Was SB TTT	*	100	45	3.0	1655	1600	0.03	1	3
18.	Bev/Was EB RRR	*	100	55	3.0	356	1600	0.03	1	3
19.	Char/93 SB LLTTRR	*	100	53	3.0	2013	1600	0.03	1	3
20.	Char/93 WB LTT	*	100	69	3.0	542	1600	0.03	1	3
21.	Char/93 EB TTR	*	100	69	3.0	459	1600	0.03	1	3
22.	North/Congress SB LT	*	100	90	3.0	636	1600	0.03	1	3
23.	North/Con WB LLTR	*	100	60	3.0	1267	1600	0.03	1	3
24.	Nor/Con NB LTTTR	*	100	74	3.0	345	1600	0.03	1	3
25.	Nor/Con EB LTR	*	100	60	3.0	17	1600	0.03	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Bev/Was N1	*	6562.0	6150.2	6.0	*
2.	Bev/Was N2	*	6561.2	6075.2	6.0	*
3.	Bev/Was N3	*	6560.5	6000.2	6.0	*
4.	Bev/Was N4	*	6515.8	6060.4	6.0	*
5.	Bev/Was N5	*	6471.1	6120.6	6.0	*
6.	Bev/Was SE1	*	6671.0	6049.7	6.0	*
7.	Bev/Was SE2	*	6670.2	5966.3	6.0	*
8.	Bev/Was SE3	*	6624.0	5907.2	6.0	*
9.	Bev/Was SE4	*	6626.1	5832.3	6.0	*
10.	Bev/Was SE5	*	6628.1	5757.3	6.0	*
11.	Bev/Was SW1	*	6541.8	5766.9	6.0	*
12.	Bev/Was SW2	*	6540.1	5841.9	6.0	*
13.	Bev/Was SW3	*	6537.7	5916.8	6.0	*
14.	Bev/Was SW4	*	6493.0	5977.0	6.0	*
15.	Bev/Was SW5	*	6448.3	6037.3	6.0	*
16.	Char/93 NE1	*	6625.0	5871.1	6.0	*
17.	Char/93 NE2	*	6627.1	5796.1	6.0	*
18.	Char/93 NE3	*	6629.1	5721.1	6.0	*
19.	Char/93 NE4	*	6699.8	5695.9	6.0	*
20.	Char/93 NE5	*	6750.6	5633.2	6.0	*
21.	Char/93 S1	*	6657.8	5466.0	6.0	*
22.	Char/93 S2	*	6614.7	5527.4	6.0	*
23.	Char/93 S3	*	6571.7	5588.8	6.0	*
24.	Char/93 S4	*	6512.9	5542.2	6.0	*
25.	Char/93 S5	*	6454.1	5495.6	6.0	*
26.	Char/93 NW1	*	6424.1	5632.5	6.0	*

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16:10:43

RECEPTOR LOCATIONS

RECEPTOR	COORDINATES (FT) X	Y	Z
27. Char/93 NW2	6483.6	5678.2	6.0
28. Char/93 NW3	6543.0	5723.9	6.0
29. Char/93 NW4	6541.0	5798.8	6.0
30. Char/93 NW5	6538.9	5873.8	6.0
31. Wash/Cong NE1	6910.2	4571.2	6.0
32. Wash/Cong NE2	6925.8	4497.8	6.0
33. Wash/Cong NE3	6941.4	4424.5	6.0
34. Wash/Cong NE4	7012.0	4449.6	6.0
35. Wash/Cong NE5	7082.7	4474.9	6.0
36. Wash/Cong SE1	7095.4	4388.1	6.0
37. Wash/Cong SE2	7024.8	4362.9	6.0
38. Wash/Cong SE3	6954.1	4337.7	6.0
39. Wash/Cong SE4	6968.4	4264.1	6.0
40. Wash/Cong SE5	6982.7	4190.4	6.0
41. Wash/Cong SW1	6867.5	4164.7	6.0
42. Wash/Cong SW2	6853.3	4238.0	6.0
43. Wash/Cong SW3	6838.9	4312.0	6.0
44. Wash/Cong SW4	6765.6	4296.1	6.0
45. Wash/Cong SW5	6692.3	4280.2	6.0
46. Wash/Cong NW1	6682.4	4353.8	6.0
47. Wash/Cong NW2	6755.7	4369.7	6.0
48. Wash/Cong NW3	6828.9	4386.0	6.0
49. Wash/Cong NW4	6813.3	4459.4	6.0
50. Wash/Cong NW5	6797.8	4532.8	6.0

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	2.	2.	2.	1.	0.	1.	1.	3.	3.	3.	2.	2.	1.	1.	0.	3.	3.	3.	1.	0.
10.	2.	2.	2.	1.	1.	1.	1.	3.	2.	2.	2.	2.	2.	1.	1.	3.	2.	2.	0.	0.
20.	2.	2.	2.	1.	1.	0.	0.	3.	2.	1.	3.	2.	2.	1.	1.	2.	1.	1.	0.	0.
30.	2.	2.	2.	1.	1.	0.	0.	2.	1.	1.	3.	2.	2.	1.	1.	1.	1.	1.	0.	0.
40.	2.	2.	2.	1.	1.	0.	0.	2.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
50.	2.	2.	2.	1.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
60.	2.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	2.	1.	1.	1.	1.	0.	0.	0.
70.	2.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	1.	1.	1.	1.	1.	0.	0.	0.
80.	2.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	1.	1.	1.	1.	1.	0.	0.	0.
90.	1.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
100.	1.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	1.	1.	1.	1.	1.	1.	0.	0.
110.	1.	2.	2.	1.	1.	0.	0.	1.	1.	0.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
120.	1.	2.	2.	1.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
130.	2.	2.	2.	1.	1.	0.	0.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	0.	0.
140.	2.	2.	2.	1.	1.	0.	0.	1.	1.	1.	2.	3.	3.	2.	1.	1.	1.	1.	0.	0.
150.	2.	2.	2.	2.	1.	0.	0.	1.	1.	2.	2.	3.	3.	2.	1.	1.	2.	2.	1.	0.
160.	2.	2.	3.	2.	2.	0.	0.	2.	2.	2.	1.	2.	3.	1.	1.	2.	2.	2.	1.	1.
170.	2.	2.	3.	2.	1.	1.	1.	2.	2.	3.	1.	2.	2.	1.	0.	2.	2.	3.	1.	1.
180.	2.	2.	2.	1.	0.	1.	1.	2.	2.	3.	0.	1.	1.	0.	0.	2.	3.	3.	2.	1.
190.	1.	1.	1.	0.	0.	2.	2.	3.	2.	2.	0.	0.	0.	0.	0.	0.	3.	2.	2.	1.
200.	0.	0.	1.	0.	0.	2.	2.	2.	3.	2.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.
210.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	0.	2.	2.	2.	1.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	5.	3.	2.	2.	1.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
10.	4.	2.	2.	2.	1.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
20.	3.	2.	2.	2.	1.	1.	1.	3.	3.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
30.	2.	2.	1.	2.	1.	1.	1.	2.	3.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
40.	2.	2.	1.	1.	1.	1.	1.	2.	3.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
50.	2.	2.	1.	1.	1.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
60.	2.	2.	1.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
70.	2.	2.	1.	1.	1.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
80.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
90.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
100.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
110.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
120.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
130.	2.	2.	1.	0.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
140.	2.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
150.	3.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3)																			
220.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
230.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
240.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	2.	2.	1.	2.	1.
250.	0.	0.	0.	0.	0.	2.	2.	2.	2.	2.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.
260.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	2.	2.	1.	1.	2.
270.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	2.	2.	1.	1.	2.
280.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	2.	2.	2.	1.	1.
290.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	1.	2.	2.	1.	1.
300.	0.	0.	0.	0.	0.	2.	2.	1.	2.	2.	0.	0.	0.	0.	0.	1.	2.	2.	2.	1.
310.	0.	0.	0.	0.	0.	2.	2.	1.	2.	3.	0.	0.	0.	0.	0.	2.	2.	2.	2.	1.
320.	0.	0.	0.	0.	0.	2.	2.	1.	2.	3.	0.	0.	0.	0.	0.	2.	3.	3.	2.	1.
330.	0.	0.	0.	0.	0.	2.	2.	2.	2.	3.	0.	0.	0.	0.	0.	1.	2.	3.	1.	1.
340.	1.	0.	0.	0.	0.	2.	3.	3.	2.	3.	0.	0.	0.	0.	0.	2.	3.	4.	2.	1.
350.	1.	1.	1.	1.	0.	2.	2.	3.	3.	3.	1.	1.	1.	0.	0.	3.	3.	4.	2.	1.
360.	2.	2.	2.	1.	0.	1.	1.	3.	3.	3.	2.	2.	1.	1.	0.	3.	3.	3.	1.	0.
MAX	2.	2.	3.	2.	2.	2.	3.	3.	3.	3.	3.	3.	3.	2.	1.	3.	3.	4.	2.	2.
DEGR.	160	160	160	160	160	340	340	0	0	350	20	150	150	140	150	350	350	350	310	260

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
0.	5.	3.	2.	2.	1.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
10.	4.	2.	2.	2.	1.	0.	1.	3.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
20.	3.	2.	2.	2.	1.	1.	1.	3.	3.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
30.	2.	2.	1.	2.	1.	1.	1.	2.	3.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
40.	2.	2.	1.	1.	1.	1.	1.	2.	3.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
50.	2.	2.	1.	1.	1.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
60.	2.	2.	1.	1.	0.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
70.	2.	2.	1.	1.	1.	1.	1.	2.	2.	2.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
80.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
90.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
100.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
110.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
120.	2.	2.	1.	1.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
130.	2.	2.	1.	0.	0.	1.	1.	1.	2.	2.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
140.	2.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
150.	3.	2.	1.	0.	0.	1.	1.	2.	2.	3.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.

160.	*	3.	2.	1.	0.	0.	1.	1.	1.	2.	2.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
170.	*	3.	1.	1.	0.	0.	0.	1.	1.	1.	2.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
180.	*	3.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.
1.	0.																		
190.	*	2.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.
1.	1.																		
200.	*	1.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.
1.	1.																		
210.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
220.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
230.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
240.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
250.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.
0.	0.																		
260.	*	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
0.	0.																		
270.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
0.	0.																		
280.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	0.																		
290.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	0.																		
300.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
310.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
320.	*	2.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.
1.	1.																		
330.	*	2.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.
2.	1.																		
340.	*	3.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.
2.	1.																		
350.	*	5.	2.	2.	1.	0.	0.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
360.	*	5.	3.	2.	2.	1.	0.	1.	2.	2.	1.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
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MAX	*	5.	3.	2.	2.	1.	1.	1.	3.	3.	3.	1.	1.	2.	1.	1.	1.	1.	2.
2.	1.																		
DEGR.	*	350	0	10	20	20	100	30	20	20	150	190	330	190	210	210	300	330	330
340	340																		

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50
0.	* 1.	1.	1.	1.	0.	0.	0.	1.	1.	1.
10.	* 1.	1.	1.	1.	0.	0.	1.	2.	1.	1.
20.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
30.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
40.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
50.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
60.	* 1.	1.	1.	1.	0.	0.	1.	1.	1.	1.
70.	* 0.	1.	1.	1.	1.	0.	1.	1.	1.	1.
80.	* 0.	0.	1.	1.	0.	1.	1.	1.	1.	1.
90.	* 0.	0.	1.	0.	0.	1.	1.	1.	1.	1.
100.	* 0.	0.	1.	0.	0.	0.	1.	1.	1.	1.
110.	* 0.	0.	1.	0.	0.	0.	0.	1.	1.	1.
120.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
130.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	2.
140.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
150.	* 0.	1.	1.	0.	0.	0.	0.	1.	1.	1.
160.	* 0.	0.	1.	0.	0.	0.	0.	1.	1.	1.
170.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
180.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
190.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
200.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
210.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
220.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

240.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
250.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
260.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
270.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
280.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
290.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
300.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
310.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
320.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
330.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
340.	* 0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
350.	* 1.	1.	1.	0.	0.	0.	0.	1.	1.	1.
360.	* 1.	1.	1.	1.	0.	0.	0.	1.	1.	1.
------	* ----------									
MAX	* 1.	1.	1.	1.	1.	1.	1.	2.	1.	2.
DEGR.	* 0	0	0	70	70	80	70	10	0	130

THE HIGHEST CONCENTRATION OF 5. ug/m**3 OCCURRED AT RECEPTOR REC21.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16: 9:54

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Stan/Lom SB L	*	5194.4	5948.0	5120.9	6056.9	*	131.	326.	AG	0.	100.0	1.0	10.0	0.63	6.7
2.	Stan/Lom SB TRR	*	5173.5	5937.1	5090.5	6056.1	*	145.	325.	AG	0.	100.0	1.0	20.0	0.70	7.4
3.	Stan/Lom WB LTT	*	5306.8	5930.3	5368.6	5981.0	*	80.	51.	AG	0.	100.0	1.0	20.0	0.35	4.1
4.	Stan/Lom WB R	*	5292.4	5947.7	5403.8	6033.2	*	140.	52.	AG	0.	100.0	1.0	10.0	0.68	7.1
5.	Stan/Lom NB L	*	5307.6	5737.4	5341.6	5726.9	*	36.	107.	AG	0.	100.0	1.0	10.0	0.24	1.8
6.	Stan/Lom NB TRR	*	5314.4	5765.3	5393.9	5738.4	*	84.	109.	AG	0.	100.0	1.0	20.0	0.56	4.3
7.	Stan/Lom EB LLT	*	5214.5	5705.3	5171.4	5556.9	*	155.	196.	AG	0.	100.0	1.0	20.0	0.92	7.9
8.	Stan/Lom EB R	*	5236.5	5698.5	4944.8	4671.4	*	1068.	196.	AG	0.	100.0	1.0	10.0	1.34	54.2
9.	Char/93 SB LLTTRR	*	6587.8	5740.0	6580.8	5923.0	*	183.	358.	AG	0.	100.0	1.0	40.0	0.87	9.3
10.	Char/93 WB LTT	*	6702.8	5647.8	6737.0	5605.0	*	55.	141.	AG	0.	100.0	1.0	20.0	0.30	2.8
11.	Char/93 EB TTR	*	6560.8	5622.5	6458.6	5547.7	*	127.	234.	AG	0.	100.0	1.0	30.0	0.69	6.4
12.	Merr/Stan/Cau/Loma N	*	5250.5	5866.7	4995.3	6239.2	*	452.	326.	AG	1691.	0.0	1.0	90.0		
13.	Merr/Stan/Cau/Loma E	*	5239.6	5868.5	5518.3	6083.7	*	352.	52.	AG	1414.	0.0	1.0	78.0		
14.	Merr/Stan/Cau/Loma S	*	5248.7	5770.8	5717.4	5595.4	*	500.	111.	AG	1247.	0.0	1.0	78.0		
15.	Merr/Stan/Cau/Loma W	*	5232.2	5770.9	5117.2	5398.9	*	389.	197.	AG	1387.	0.0	1.0	78.0		
16.	Wash/Bev S	*	6585.9	5730.0	6580.5	5926.3	*	196.	358.	AG	2091.	0.0	1.0	66.0		
17.	Char/93 Sumner	*	6646.8	5712.0	6863.6	5444.5	*	344.	141.	AG	334.	0.0	1.0	42.0		
18.	Char/93 S	*	6584.2	5677.4	6839.9	5392.5	*	383.	138.	AG	1059.	0.0	1.0	48.0		
19.	Char/93 W EB	*	6579.7	5642.4	6410.0	5507.8	*	217.	232.	AG	1159.	0.0	1.0	54.0		
20.	Char/93 W WB	*	6568.3	5696.7	6372.6	5546.3	*	247.	232.	AG	499.	0.0	1.0	54.0		
21.	Char/93 S SW	*	6596.5	5607.4	6730.4	5416.5	*	233.	145.	AG	414.	0.0	1.0	42.0		

PAGE 2

JOB: Government Center Garage RUN: Build

DATE : 7/19/13
TIME : 16: 9:54

		*								
1.	Stan/Lom SB L	*	120	79	3.0	304	1600	0.03	1	3
2.	Stan/Lom SB TRR	*	120	79	3.0	672	1600	0.03	1	3
3.	Stan/Lom WB LTT	*	120	71	3.0	412	1600	0.03	1	3
4.	Stan/Lom WB R	*	120	79	3.0	325	1600	0.03	1	3
5.	Stan/Lom NB L	*	120	93	3.0	70	1600	0.03	1	3
6.	Stan/Lom NB TRR	*	120	93	3.0	331	1600	0.03	1	3
7.	Stan/Lom EB LLT	*	120	97	3.0	439	1600	0.03	1	3
8.	Stan/Lom EB R	*	120	97	3.0	320	1600	0.03	1	3
9.	Char/93 SB LLTTRR	*	100	62	3.0	1842	1600	0.03	1	3
10.	Char/93 WB LTT	*	100	60	3.0	334	1600	0.03	1	3
11.	Char/93 EB TTR	*	100	60	3.0	1159	1600	0.03	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1.	Stan/Lom NE1	*	5177.0	6071.2	6.0	*
2.	Stan/Lom NE2	*	5219.4	6009.4	6.0	*
3.	Stan/Lom NE3	*	5261.8	5947.5	6.0	*
4.	Stan/Lom NE4	*	5321.1	5993.3	6.0	*
5.	Stan/Lom NE5	*	5380.5	6039.2	6.0	*
6.	Stan/Lom SE1	*	5380.4	5915.2	6.0	*
7.	Stan/Lom SE2	*	5321.0	5869.4	6.0	*
8.	Stan/Lom SE3	*	5261.7	5823.6	6.0	*
9.	Stan/Lom SE4	*	5330.0	5792.7	6.0	*
10.	Stan/Lom SE5	*	5400.3	5766.4	6.0	*
11.	Stan/Lom SW1	*	5405.8	5659.6	6.0	*
12.	Stan/Lom SW2	*	5335.6	5685.9	6.0	*
13.	Stan/Lom SW3	*	5265.4	5712.2	6.0	*

		*				
14.	Stan/Lom SW4	*	5243.2	5640.6	6.0	*
15.	Stan/Lom SW5	*	5221.0	5568.9	6.0	*
16.	Stan/Lom NW1	*	5144.0	5651.7	6.0	*
17.	Stan/Lom NW2	*	5166.2	5723.3	6.0	*
18.	Stan/Lom NW3	*	5188.4	5795.0	6.0	*
19.	Stan/Lom NW4	*	5181.7	5869.7	6.0	*
20.	Stan/Lom NW5	*	5136.5	5935.7	6.0	*
21.	Char/93 NE1	*	6625.0	5871.1	6.0	*
22.	Char/93 NE2	*	6627.1	5796.1	6.0	*
23.	Char/93 NE3	*	6629.1	5721.1	6.0	*
24.	Char/93 NE4	*	6699.8	5695.9	6.0	*
25.	Char/93 NE5	*	6750.6	5633.2	6.0	*
26.	Char/93 S1	*	6657.8	5466.0	6.0	*
27.	Char/93 S2	*	6614.7	5527.4	6.0	*
28.	Char/93 S3	*	6571.7	5588.8	6.0	*
29.	Char/93 S4	*	6512.9	5542.2	6.0	*
30.	Char/93 S5	*	6454.1	5495.6	6.0	*
31.	Char/93 NW1	*	6424.1	5632.5	6.0	*
32.	Char/93 NW2	*	6483.6	5678.2	6.0	*
33.	Char/93 NW3	*	6543.0	5723.9	6.0	*
34.	Char/93 NW4	*	6541.0	5798.8	6.0	*
35.	Char/93 NW5	*	6538.9	5873.8	6.0	*

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JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (ug/m**3) * REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0. *	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.
10. *	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	1.	1.
20. *	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	0.	1.	1.	0.	1.	1.	1.
30. *	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.
40. *	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.
50. *	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.
60. *	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
70. *	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
80. *	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.	1.
90. *	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	0.	1.	1.
100. *	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.
110. *	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.
120. *	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
130. *	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
140. *	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.
150. *	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
160. *	1.	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
170. *	1.	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.
180. *	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.
190. *	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.
200. *	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
210. *	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.
220. *	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.
230. *	1.	1.	1.	1.	1.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.
240. *	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.

```
0.    0.
 250.  *    1.    1.    1.    0.    0.    1.    0.    0.    1.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 260.  *    1.    1.    1.    0.    0.    1.    0.    0.    0.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 270.  *    1.    1.    1.    0.    0.    1.    1.    0.    0.    1.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 280.  *    1.    1.    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.    0.
0.    0.
 290.  *    1.    1.    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 300.  *    1.    1.    1.    0.    0.    1.    1.    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    0.
0.    0.
 310.  *    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 320.  *    0.    1.    1.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    1.    1.    0.    0.    0.
0.    0.
 330.  *    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    1.    1.    0.    0.    0.
1.    1.
 340.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.    0.
1.    1.
 350.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
1.    1.
 360.  *    0.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.
1.    1.

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX   *    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.
1.    1.
 DEGR. *  180   180   190   200   200   280   310   330   210   230   320   340   220   340     0    60    90   180
60     0
```


THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC21.

JOB: Government Center Garage RUN: Build

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35
0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
10.	0.	0.	0.	0.	0.	0.	1.	1.	2.	1.	0.	0.	1.	1.	0.
20.	0.	0.	0.	0.	0.	0.	0.	1.	2.	1.	0.	0.	2.	1.	0.
30.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.	2.	2.	1.
40.	0.	0.	0.	0.	0.	0.	1.	0.	1.	1.	0.	1.	2.	2.	1.
50.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	0.	0.	1.	2.	1.
60.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	1.
70.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	1.	1.
80.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	1.	1.
90.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	0.	0	1.	1.
100.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	0.	1.	1.
110.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.	1.
120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.	1.
130.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.
140.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	2.
150.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	2.
160.	0.	0.	0.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
170.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
180.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	1.
190.	1.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
200.	2.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
210.	2.	1.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.
220.	2.	1.	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
230.	2.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
240.	1.	1.	0.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
250.	1.	1.	0.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.
260.	1.	1.	0.	0.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
270.	1.	1.	0.	0.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
280.	1.	1.	0.	0.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
290.	1.	1.	1.	0.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
300.	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
310.	1.	2.	1.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.
320.	1.	2.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.
330.	1.	2.	2.	0.	0.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.
340.	0.	1.	2.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.
350.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.
360.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
MAX	2.	2.	2.	1.	1.	1.	1.	1.	2.	1.	1.	1.	2.	2.	2.
DEGR.	210	310	330	240	260	340	350	0	10	30	110	120	20	30	140

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:14:36

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6042.8	5450.0	*	73.	290.	AG	0.	100.0	1.0	30.0	0.58	3.7
2. Char/Merr WB	*	6250.4	5435.2	6335.4	5502.4	*	108.	52.	AG	0.	100.0	1.0	30.0	0.75	5.5
3. Char/Merr NB R	*	6291.7	5369.7	6314.8	5354.0	*	28.	124.	AG	0.	100.0	1.0	10.0	0.14	1.4
4. Char/Merr NB LTT	*	6280.4	5347.2	7349.2	4593.4	*	1308.	125.	AG	0.	100.0	1.0	20.0	1.25	66.4
5. Char/Merr EB	*	6104.2	5362.2	6046.8	5340.9	*	61.	250.	AG	0.	100.0	1.0	20.0	0.58	3.1
6. Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.8	*	108.	14.	AG	0.	100.0	1.0	10.0	0.71	5.5
7. Char/Cam SB TR	*	5360.8	4833.5	5403.4	4971.2	*	144.	17.	AG	0.	100.0	1.0	20.0	0.95	7.3
8. Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	0.	100.0	1.0	20.0	0.27	2.2
9. Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	0.	100.0	1.0	10.0	0.60	4.7
10. Char/Cam NB TR	*	5383.3	4723.8	5384.5	4645.8	*	78.	179.	AG	0.	100.0	1.0	20.0	0.74	4.0
11. Char/Cam EB TTTR	*	5302.7	4739.8	5210.5	4740.8	*	92.	271.	AG	0.	100.0	1.0	30.0	0.57	4.7
12. Sud/Merr SB L	*	6532.7	5210.3	6385.1	5315.4	*	181.	305.	AG	0.	100.0	1.0	10.0	1.08	9.2
13. Sud/Merr SB TTT	*	6518.3	5190.8	6484.5	5210.4	*	39.	300.	AG	0.	100.0	1.0	30.0	0.20	2.0
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6678.7	5059.8	*	117.	150.	AG	0.	100.0	1.0	30.0	0.60	5.9
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6472.1	5115.0	*	60.	239.	AG	0.	100.0	1.0	40.0	0.47	3.0
16. Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	0.	100.0	1.0	20.0	0.34	3.3
17. Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18. Sud/Sur EB TTR	*	6794.5	5259.6	6739.6	5238.0	*	59.	249.	AG	0.	100.0	1.0	30.0	0.49	3.0
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	945.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1232.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1619.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1565.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	1016.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1651.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	964.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1759.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	360.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	541.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	420.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1848.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1944.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	579.	0.0	1.0	78.0		

1. Char/Merr SB	*	100	76	3.0	530	1600	0.03	1	3
2. Char/Merr WB	*	100	74	3.0	757	1600	0.03	1	3
3. Char/Merr NB R	*	100	44	3.0	116	1600	0.03	1	3
4. Char/Merr NB LTT	*	100	70	3.0	1002	1600	0.03	1	3
5. Char/Merr EB	*	100	80	3.0	281	1600	0.03	1	3
6. Char/Cam SB L	*	90	58	3.0	340	1600	0.03	1	3
7. Char/Cam SB TR	*	90	71	3.0	472	1600	0.03	1	3
8. Char/Cam WB LTTR	*	90	54	3.0	294	1600	0.03	1	3
9. Char/Cam NB L	*	90	58	3.0	289	1600	0.03	1	3
10. Char/Cam NB TR	*	90	71	3.0	367	1600	0.03	1	3

11. Char/Cam EB TTTR	*	90	54	3.0	937	1600	0.03	1	3
12. Sud/Merr SB L	*	100	89	3.0	104	1600	0.03	1	3
13. Sud/Merr SB TTT	*	100	41	3.0	524	1600	0.03	1	3
14. Sud/Merr NB TTTR	*	100	52	3.0	1232	1600	0.03	1	3
15. Sud/Merr EB LTTR	*	100	76	3.0	579	1600	0.03	1	3
16. Sud/Sur SB LTT	*	100	53	3.0	455	1600	0.03	1	3
17. Sud/Sur SEB	*	100	70	3.0	26	1600	0.03	1	3
18. Sud/Sur EB TTR	*	100	77	3.0	420	1600	0.03	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Char/Merr NE1	*	6063.7	5511.0	6.0
2. Char/Merr NE2	*	6133.9	5484.8	6.0
3. Char/Merr NE3	*	6204.2	5458.5	6.0
4. Char/Merr NE4	*	6265.6	5501.5	6.0
5. Char/Merr NE5	*	6327.1	5544.5	6.0
6. Char/Merr SE1	*	6443.7	5491.9	6.0
7. Char/Merr SE2	*	6382.2	5448.9	6.0
8. Char/Merr SE3	*	6320.8	5405.9	6.0
9. Char/Merr SE4	*	6380.5	5360.4	6.0
10. Char/Merr SE5	*	6440.1	5315.0	6.0
11. Char/Merr SW1	*	6332.0	5249.0	6.0
12. Char/Merr SW2	*	6272.3	5294.5	6.0
13. Char/Merr SW3	*	6212.6	5339.9	6.0
14. Char/Merr SW4	*	6141.6	5315.8	6.0
15. Char/Merr SW5	*	6070.6	5291.7	6.0
16. Char/Merr NW1	*	5902.1	5359.1	6.0
17. Char/Merr NW2	*	5973.1	5383.2	6.0
18. Char/Merr NW3	*	6044.1	5407.3	6.0
19. Char/Merr NW4	*	5973.9	5433.5	6.0
20. Char/Merr NW5	*	5903.6	5459.8	6.0
21. Char/Cam NE1	*	5490.2	4963.0	6.0
22. Char/Cam NE2	*	5459.0	4894.8	6.0
23. Char/Cam NE3	*	5427.8	4826.6	6.0
24. Char/Cam NE4	*	5500.4	4807.6	6.0
25. Char/Cam NE5	*	5572.9	4788.7	6.0
26. Char/Cam SE1	*	5553.9	4667.5	6.0
27. Char/Cam SE2	*	5481.3	4686.5	6.0
28. Char/Cam SE3	*	5408.7	4705.4	6.0
29. Char/Cam SE4	*	5409.4	4630.4	6.0
30. Char/Cam SE5	*	5410.1	4555.4	6.0
31. Char/Cam SW1	*	5312.0	4561.9	6.0
32. Char/Cam SW2	*	5310.7	4636.9	6.0
33. Char/Cam SW3	*	5310.7	4711.9	6.0

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Char/Cam SW4	*	5235.6	4712.1	6.0
35. Char/Cam SW5	*	5160.6	4711.9	6.0
36. Char/Cam NW1	*	5167.9	4822.4	6.0
37. Char/Cam NW2	*	5242.9	4822.1	6.0
38. Char/Cam NW3	*	5317.9	4821.9	6.0
39. Char/Cam NW4	*	5349.1	4890.1	6.0
40. Char/Cam NW5	*	5380.3	4958.3	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
10.	*	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
20.	*	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.		

0.	0.																		
30.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
60.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
1.	0.																		
70.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.
1.	0.																		
80.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.
1.	1.																		
90.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
100.	*	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.
1.	1.																		
110.	*	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
120.	*	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	1.	1.	1.
1.	1.																		
130.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	2.	1.	1.	1.	0.	0.	0.	1.	1.
1.	0.																		
140.	*	1.	1.	2.	2.	1.	0.	0.	1.	2.	2.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
150.	*	1.	1.	1.	2.	1.	0.	1.	1.	2.	2.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
160.	*	1.	1.	1.	2.	1.	0.	1.	1.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
170.	*	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
180.	*	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
190.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	0.	1.
0.	0.																		
200.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
230.	*	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
240.	*	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
250.	*	0.	1.	1.	0.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
260.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
270.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
280.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		

MAX	*	1.	1.	2.	2.	1.	1.	1.	2.	2.	2.	1.	1.	1.	1.	1.	1.	1.	2.
1.	1.																		
DEGR.	*	130	120	130	140	190	250	270	280	140	150	80	100	30	40	40	100	100	100
90	100																		

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38

REC39 REC40

0.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	0.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.
1.	0.																		
50.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
1.	1.																		
60.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
1.	1.																		
70.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
80.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
90.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.
1.	1.																		
100.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.
1.	1.																		
110.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.
1.	1.																		
120.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	1.																		
130.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	1.																		
140.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.
2.	1.																		
150.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
160.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
170.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
2.	2.																		
180.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	2.																		
190.	*	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
200.	*	0.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
230.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
240.	*	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
250.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
260.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
270.	*	0.	1.	1.	1.	1.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	1.	1.	1.	1.	1.	1.	2.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
290.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	1.	0.	0.	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		

MAX	*	1.	1.	2.	1.	1.	1.	1.	2.	2.	1.	1.	1.	2.	2.	1.	1.	1.	2.
2.	2.																		
DEGR.	*	230	240	240	260	260	300	290	280	330	330	20	40	30	50	80	110	110	110
170	170																		

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC10.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221 PAGE 1

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15: 7

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT)				*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
			X1	Y1	X2	Y2										
1.	Char/Merr SB	*	6111.6	5425.1	6030.2	5454.5	*	87.	290.	AG	0.	100.0	1.0	30.0	0.67	4.4
2.	Char/Merr WB	*	6250.4	5435.2	6310.4	5482.7	*	77.	52.	AG	0.	100.0	1.0	30.0	0.67	3.9
3.	Char/Merr NB R	*	6291.7	5369.7	6352.1	5328.7	*	73.	124.	AG	0.	100.0	1.0	10.0	0.37	3.7
4.	Char/Merr NB LTT	*	6280.4	5347.2	6430.9	5241.1	*	184.	125.	AG	0.	100.0	1.0	20.0	0.94	9.4
5.	Char/Merr EB	*	6104.2	5362.2	5936.5	5299.8	*	179.	250.	AG	0.	100.0	1.0	20.0	0.92	9.1
6.	Char/Cam SB L	*	5384.1	4834.2	5402.6	4908.3	*	76.	14.	AG	0.	100.0	1.0	10.0	0.42	3.9
7.	Char/Cam SB TR	*	5360.8	4833.5	5378.3	4889.9	*	59.	17.	AG	0.	100.0	1.0	20.0	0.41	3.0
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	0.	100.0	1.0	20.0	0.41	3.7
9.	Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	0.	100.0	1.0	10.0	0.53	5.0
10.	Char/Cam NB TR	*	5383.3	4723.8	5385.0	4612.7	*	111.	179.	AG	0.	100.0	1.0	20.0	0.74	5.6
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5209.4	4740.8	*	93.	271.	AG	0.	100.0	1.0	30.0	0.52	4.7
12.	Sud/Merr SB L	*	6532.7	5210.3	6461.3	5261.1	*	88.	305.	AG	0.	100.0	1.0	10.0	0.95	4.5
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6482.6	5211.5	*	41.	300.	AG	0.	100.0	1.0	30.0	0.21	2.1
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6684.5	5049.5	*	128.	150.	AG	0.	100.0	1.0	30.0	0.73	6.5
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6447.8	5100.4	*	88.	239.	AG	0.	100.0	1.0	40.0	0.52	4.5
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	0.	100.0	1.0	20.0	0.53	4.1
17.	Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6703.4	5223.8	*	98.	249.	AG	0.	100.0	1.0	30.0	0.50	5.0
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	989.	0.0	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1538.	0.0	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1494.	0.0	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1409.	0.0	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	921.	0.0	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1615.	0.0	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1034.	0.0	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1697.	0.0	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	1032.	0.0	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	504.	0.0	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	0.0	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	1075.	0.0	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	0.0	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1457.	0.0	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1759.	0.0	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	992.	0.0	1.0	78.0		

DATE : 8/ 7/13
TIME : 17:15: 7

		*								
1.	Char/Merr SB	*	100	76	3.0	615	1600	0.03	1	3
2.	Char/Merr WB	*	100	79	3.0	517	1600	0.03	1	3
3.	Char/Merr NB R	*	100	52	3.0	257	1600	0.03	1	3
4.	Char/Merr NB LTT	*	100	73	3.0	660	1600	0.03	1	3
5.	Char/Merr EB	*	100	72	3.0	679	1600	0.03	1	3
6.	Char/Cam SB L	*	100	60	3.0	233	1600	0.03	1	3
7.	Char/Cam SB TR	*	100	72	3.0	301	1600	0.03	1	3
8.	Char/Cam WB LTTR	*	100	62	3.0	435	1600	0.03	1	3
9.	Char/Cam NB L	*	100	60	3.0	299	1600	0.03	1	3
10.	Char/Cam NB TR	*	100	72	3.0	543	1600	0.03	1	3

		*								
11.	Char/Cam EB TTTR	*	100	62	3.0	827	1600	0.03	1	3
12.	Sud/Merr SB L	*	100	88	3.0	106	1600	0.03	1	3
13.	Sud/Merr SB TTT	*	100	52	3.0	435	1600	0.03	1	3
14.	Sud/Merr NB TTTR	*	100	64	3.0	1094	1600	0.03	1	3
15.	Sud/Merr EB LTTR	*	100	65	3.0	992	1600	0.03	1	3
16.	Sud/Sur SB LTT	*	100	70	3.0	424	1600	0.03	1	3
17.	Sud/Sur SEB	*	100	80	3.0	37	1600	0.03	1	3
18.	Sud/Sur EB TTR	*	100	50	3.0	1075	1600	0.03	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Char/Merr NE1	*	6063.7	5511.0	6.0
2.	Char/Merr NE2	*	6133.9	5484.8	6.0
3.	Char/Merr NE3	*	6204.2	5458.5	6.0
4.	Char/Merr NE4	*	6265.6	5501.5	6.0
5.	Char/Merr NE5	*	6327.1	5544.5	6.0
6.	Char/Merr SE1	*	6443.7	5491.9	6.0
7.	Char/Merr SE2	*	6382.2	5448.9	6.0
8.	Char/Merr SE3	*	6320.8	5405.9	6.0
9.	Char/Merr SE4	*	6380.5	5360.4	6.0
10.	Char/Merr SE5	*	6440.1	5315.0	6.0
11.	Char/Merr SW1	*	6332.0	5249.0	6.0
12.	Char/Merr SW2	*	6272.3	5294.5	6.0
13.	Char/Merr SW3	*	6212.6	5339.9	6.0
14.	Char/Merr SW4	*	6141.6	5315.8	6.0
15.	Char/Merr SW5	*	6070.6	5291.7	6.0
16.	Char/Merr NW1	*	5902.1	5359.1	6.0
17.	Char/Merr NW2	*	5973.1	5383.2	6.0
18.	Char/Merr NW3	*	6044.1	5407.3	6.0
19.	Char/Merr NW4	*	5973.9	5433.5	6.0
20.	Char/Merr NW5	*	5903.6	5459.8	6.0
21.	Char/Cam NE1	*	5490.2	4963.0	6.0
22.	Char/Cam NE2	*	5459.0	4894.8	6.0
23.	Char/Cam NE3	*	5427.8	4826.6	6.0
24.	Char/Cam NE4	*	5500.4	4807.6	6.0
25.	Char/Cam NE5	*	5572.9	4788.7	6.0
26.	Char/Cam SE1	*	5553.9	4667.5	6.0
27.	Char/Cam SE2	*	5481.3	4686.5	6.0
28.	Char/Cam SE3	*	5408.7	4705.4	6.0
29.	Char/Cam SE4	*	5409.4	4630.4	6.0
30.	Char/Cam SE5	*	5410.1	4555.4	6.0
31.	Char/Cam SW1	*	5312.0	4561.9	6.0
32.	Char/Cam SW2	*	5310.7	4636.9	6.0
33.	Char/Cam SW3	*	5310.7	4711.9	6.0

DATE : 8/ 7/13
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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
34.	Char/Cam SW4	*	5235.6	4712.1	6.0
35.	Char/Cam SW5	*	5160.6	4711.9	6.0
36.	Char/Cam NW1	*	5167.9	4822.4	6.0
37.	Char/Cam NW2	*	5242.9	4822.1	6.0
38.	Char/Cam NW3	*	5317.9	4821.9	6.0
39.	Char/Cam NW4	*	5349.1	4890.1	6.0
40.	Char/Cam NW5	*	5380.3	4958.3	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.		

0.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
60.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
1.	0.																		
70.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.
1.	0.																		
80.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
90.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
100.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	2.
1.	1.																		
110.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
120.	*	1.	1.	2.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
130.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
140.	*	1.	1.	2.	2.	1.	0.	0.	1.	1.	2.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
150.	*	1.	1.	1.	2.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
160.	*	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
170.	*	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
180.	*	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
190.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
200.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
1.	0.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
230.	*	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
240.	*	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
250.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
260.	*	0.	1.	1.	0.	0.	1.	2.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
270.	*	0.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
280.	*	0.	0.	0.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		

MAX	*	1.	1.	2.	2.	1.	1.	2.	2.	1.	2.	1.	1.	2.	1.	1.	1.	1.	2.
1.	1.																		
DEGR.	*	130	130	130	140	190	260	260	250	270	140	330	20	40	40	0	80	100	100
90	90																		

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION

ANGLE (DEGR)	*	(ug/m**3) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38

REC39 REC40

0.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.
0.	0.																		
60.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	2.	1.	0.	0.	1.
1.	0.																		
70.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
0.	0.																		
80.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	0.	0.	1.
1.	0.																		
90.	*	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.
1.	0.																		
100.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.
1.	0.																		
110.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.
1.	0.																		
120.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	0.																		
130.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	0.																		
140.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	2.
1.	1.																		
150.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	1.	1.	1.
1.	1.																		
160.	*	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
170.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
180.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
190.	*	0.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
200.	*	0.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	1.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.
1.	0.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
230.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
240.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
250.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.
0.	0.																		
260.	*	0.	1.	1.	1.	1.	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.	1.
0.	0.																		
270.	*	0.	1.	1.	1.	1.	0.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	0.	0.	1.	1.	1.	1.	1.	2.	1.	0.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
290.	*	0.	0.	1.	0.	0.	1.	1.	2.	1.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
300.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	1.	0.	0.	1.	1.	1.	2.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.																		

MAX	*	1.	1.	2.	1.	1.	1.	1.	2.	2.	1.	1.	1.	2.	2.	1.	1.	1.	2.
1.	1.																		
DEGR.	*	220	240	240	250	260	300	290	280	330	330	20	40	50	50	70	130	110	110
160	180																		

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC4 .

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15:47

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

	LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1.	Char/Merr SB	*	6111.6	5425.1	6042.8	5450.0	*	73.	290.	AG	0.	100.0	1.0	30.0	0.58	3.7
2.	Char/Merr WB	*	6250.4	5435.2	6335.4	5502.4	*	108.	52.	AG	0.	100.0	1.0	30.0	0.75	5.5
3.	Char/Merr NB R	*	6291.7	5369.7	6314.8	5354.0	*	28.	124.	AG	0.	100.0	1.0	10.0	0.14	1.4
4.	Char/Merr NB LTT	*	6280.4	5347.2	7349.2	4593.4	*	1308.	125.	AG	0.	100.0	1.0	20.0	1.25	66.4
5.	Char/Merr EB	*	6104.2	5362.2	6046.8	5340.9	*	61.	250.	AG	0.	100.0	1.0	20.0	0.58	3.1
6.	Char/Cam SB L	*	5384.1	4834.2	5410.2	4938.8	*	108.	14.	AG	0.	100.0	1.0	10.0	0.71	5.5
7.	Char/Cam SB TR	*	5360.8	4833.5	5403.4	4971.2	*	144.	17.	AG	0.	100.0	1.0	20.0	0.95	7.3
8.	Char/Cam WB LTTR	*	5411.0	4793.5	5453.2	4783.7	*	43.	103.	AG	0.	100.0	1.0	20.0	0.27	2.2
9.	Char/Cam NB L	*	5363.0	4722.4	5360.9	4630.7	*	92.	181.	AG	0.	100.0	1.0	10.0	0.60	4.7
10.	Char/Cam NB TR	*	5383.3	4723.8	5384.5	4645.8	*	78.	179.	AG	0.	100.0	1.0	20.0	0.74	4.0
11.	Char/Cam EB TTTR	*	5302.7	4739.8	5210.5	4740.8	*	92.	271.	AG	0.	100.0	1.0	30.0	0.57	4.7
12.	Sud/Merr SB L	*	6532.7	5210.3	6385.1	5315.4	*	181.	305.	AG	0.	100.0	1.0	10.0	1.08	9.2
13.	Sud/Merr SB TTT	*	6518.3	5190.8	6484.5	5210.4	*	39.	300.	AG	0.	100.0	1.0	30.0	0.20	2.0
14.	Sud/Merr NB TTTR	*	6621.0	5161.1	6678.7	5059.8	*	117.	150.	AG	0.	100.0	1.0	30.0	0.60	5.9
15.	Sud/Merr EB LTTR	*	6523.3	5145.9	6472.1	5115.0	*	60.	239.	AG	0.	100.0	1.0	40.0	0.47	3.0
16.	Sud/Sur SB LTT	*	6777.5	5369.7	6736.6	5421.2	*	66.	322.	AG	0.	100.0	1.0	20.0	0.34	3.3
17.	Sud/Sur SEB	*	6757.2	5330.0	6747.6	5332.4	*	10.	284.	AG	0.	100.0	1.0	10.0	0.06	0.5
18.	Sud/Sur EB TTR	*	6794.5	5259.6	6739.6	5238.0	*	59.	249.	AG	0.	100.0	1.0	30.0	0.49	3.0
19.	Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	945.	0.0	1.0	84.0		
20.	Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1232.	0.0	1.0	90.0		
21.	Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1619.	0.0	1.0	98.0		
22.	Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1565.	0.0	1.0	98.0		
23.	Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	1016.	0.0	1.0	78.0		
24.	Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1651.	0.0	1.0	****		
25.	Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	964.	0.0	1.0	78.0		
26.	Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1759.	0.0	1.0	90.0		
27.	Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	360.	0.0	1.0	30.0		
28.	Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	541.	0.0	1.0	54.0		
29.	Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	455.	0.0	1.0	42.0		
30.	Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	420.	0.0	1.0	54.0		
31.	Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	26.	0.0	1.0	42.0		
32.	Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1848.	0.0	1.0	98.0		
33.	Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1944.	0.0	1.0	90.0		
34.	Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	579.	0.0	1.0	78.0		

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
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1.	Char/Merr SB	*	100	76	3.0	530	1600	0.03	1	3
2.	Char/Merr WB	*	100	74	3.0	757	1600	0.03	1	3
3.	Char/Merr NB R	*	100	44	3.0	116	1600	0.03	1	3
4.	Char/Merr NB LTT	*	100	70	3.0	1002	1600	0.03	1	3
5.	Char/Merr EB	*	100	80	3.0	281	1600	0.03	1	3
6.	Char/Cam SB L	*	90	58	3.0	340	1600	0.03	1	3
7.	Char/Cam SB TR	*	90	71	3.0	472	1600	0.03	1	3
8.	Char/Cam WB LTTR	*	90	54	3.0	294	1600	0.03	1	3
9.	Char/Cam NB L	*	90	58	3.0	289	1600	0.03	1	3
10.	Char/Cam NB TR	*	90	71	3.0	367	1600	0.03	1	3

11.	Char/Cam EB TTTR	*	90	54	3.0	937	1600	0.03	1	3
12.	Sud/Merr SB L	*	100	89	3.0	104	1600	0.03	1	3
13.	Sud/Merr SB TTT	*	100	41	3.0	524	1600	0.03	1	3
14.	Sud/Merr NB TTTR	*	100	52	3.0	1232	1600	0.03	1	3
15.	Sud/Merr EB LTTR	*	100	76	3.0	579	1600	0.03	1	3
16.	Sud/Sur SB LTT	*	100	53	3.0	455	1600	0.03	1	3
17.	Sud/Sur SEB	*	100	70	3.0	26	1600	0.03	1	3
18.	Sud/Sur EB TTR	*	100	77	3.0	420	1600	0.03	1	3

RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
1.	Sud/Merr NE1	*	6492.5	5309.9	6.0
2.	Sud/Merr NE2	*	6554.8	5268.0	6.0
3.	Sud/Merr NE3	*	6616.2	5224.9	6.0
4.	Sud/Merr NE4	*	6684.7	5255.3	6.0
5.	Sud/Merr NE5	*	6753.3	5285.7	6.0
6.	Sud/Merr SE1	*	6792.9	5222.3	6.0
7.	Sud/Merr SE2	*	6724.3	5191.9	6.0
8.	Sud/Merr SE3	*	6655.7	5161.5	6.0
9.	Sud/Merr SE4	*	6695.5	5097.9	6.0
10.	Sud/Merr SE5	*	6735.2	5034.3	6.0
11.	Sud/Merr SW1	*	6638.6	4981.3	6.0
12.	Sud/Merr SW2	*	6598.9	5045.0	6.0
13.	Sud/Merr SW3	*	6559.1	5108.6	6.0
14.	Sud/Merr SW4	*	6493.4	5072.5	6.0
15.	Sud/Merr SW5	*	6427.6	5036.5	6.0
16.	Sud/Merr NW1	*	6347.8	5104.5	6.0
17.	Sud/Merr NW2	*	6413.5	5140.5	6.0
18.	Sud/Merr NW3	*	6479.3	5176.6	6.0
19.	Sud/Merr NW4	*	6417.1	5218.5	6.0
20.	Sud/Merr NW5	*	6354.9	5260.4	6.0
21.	Sud/Sur NE1	*	6755.9	5445.7	6.0
22.	Sud/Sur NE2	*	6801.0	5385.7	6.0
23.	Sud/Sur NE3	*	6846.0	5325.7	6.0
24.	Sud/Sur NE4	*	6908.8	5366.8	6.0
25.	Sud/Sur NE5	*	6971.5	5407.9	6.0
26.	Sud/Sur SE1	*	7002.4	5368.4	6.0
27.	Sud/Sur SE2	*	6939.7	5327.3	6.0
28.	Sud/Sur SE3	*	6876.9	5286.2	6.0
29.	Sud/Sur SE4	*	6931.7	5235.0	6.0
30.	Sud/Sur SE5	*	6986.5	5183.8	6.0
31.	Sud/Sur SW1	*	6932.3	5133.1	6.0
32.	Sud/Sur SE2	*	6877.5	5184.3	6.0
33.	Sud/Sur SE3	*	6822.7	5235.5	6.0

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
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RECEPTOR LOCATIONS

	RECEPTOR	*	COORDINATES (FT) X	Y	Z
34.	Sud/Sur SE4	*	6754.2	5205.1	6.0
35.	Sud/Sur SE5	*	6685.6	5174.8	6.0
36.	Sud/Sur NW1	*	6645.5	5237.9	6.0
37.	Sud/Sur NW2	*	6714.1	5268.3	6.0
38.	Sud/Sur NW3	*	6782.7	5298.7	6.0
39.	Sud/Sur NW4	*	6709.5	5315.4	6.0
40.	Sud/Sur NW5	*	6636.4	5332.0	6.0
41.	Sud/Sur N1	*	6642.4	5493.7	6.0
42.	Sud/Sur N2	*	6687.4	5433.7	6.0
43.	Sud/Sur N3	*	6732.4	5373.8	6.0
44.	Sud/Sur N4	*	6659.3	5390.4	6.0
45.	Sud/Sur N5	*	6586.2	5407.1	6.0

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (ug/m**3)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20

```
   0.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    2.    1.    0.    1.    1.
1.    1.
  10.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    0.    1.    1.
1.    1.
  20.  *    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    1.    1.    1.    1.    1.    0.    1.    1.
1.    1.
  30.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    0.    1.    1.
1.    1.
  40.  *    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    1.    1.    1.    1.    1.    0.    1.    1.
1.    1.
  50.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    0.    1.    1.
1.    1.
  60.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.
1.    1.
  70.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    2.
1.    1.
  80.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    2.
1.    2.
  90.  *    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    2.
2.    2.
 100.  *    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    2.
2.    2.
 110.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    0.    0.    1.    2.
2.    2.
 120.  *    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    1.    1.    0.    0.    0.    1.    2.
2.    2.
 130.  *    1.    1.    0.    0.    1.    0.    0.    0.    0.    1.    1.    1.    1.    0.    0.    0.    1.    2.
1.    1.
 140.  *    1.    1.    1.    0.    1.    0.    0.    1.    1.    1.    0.    1.    1.    0.    0.    0.    0.    1.
1.    1.
 150.  *    2.    2.    1.    0.    1.    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 160.  *    2.    2.    2.    0.    1.    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 170.  *    2.    1.    2.    1.    1.    0.    0.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 180.  *    1.    1.    2.    1.    1.    0.    0.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    1.
0.    0.
 190.  *    1.    1.    1.    1.    1.    0.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 200.  *    1.    1.    1.    1.    1.    0.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 210.  *    1.    2.    1.    1.    1.    0.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 220.  *    1.    1.    1.    1.    1.    0.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 230.  *    1.    1.    1.    1.    1.    0.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 240.  *    1.    1.    2.    1.    1.    1.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 250.  *    1.    1.    1.    1.    1.    1.    1.    2.    2.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 260.  *    1.    1.    1.    1.    0.    1.    1.    2.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 270.  *    1.    1.    1.    1.    0.    1.    1.    2.    2.    2.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 280.  *    1.    1.    1.    1.    0.    1.    1.    2.    2.    2.    0.    0.    1.    0.    0.    0.    0.    0.
0.    0.
 290.  *    1.    1.    1.    0.    0.    1.    1.    2.    2.    2.    0.    0.    1.    0.    0.    0.    0.    1.
1.    1.
 300.  *    1.    1.    1.    0.    0.    1.    0.    2.    2.    3.    0.    1.    1.    0.    0.    0.    0.    1.
1.    1.
 310.  *    0.    0.    0.    0.    0.    1.    0.    1.    2.    2.    1.    1.    2.    1.    0.    0.    0.    1.
1.    1.
 320.  *    0.    0.    0.    0.    0.    1.    0.    1.    1.    2.    1.    1.    2.    1.    0.    0.    1.    1.
2.    1.
 330.  *    0.    0.    0.    0.    0.    1.    0.    0.    1.    1.    1.    1.    2.    1.    1.    0.    1.    2.
1.    2.
 340.  *    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    2.    1.    1.    0.    1.    1.
2.    2.
 350.  *    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.    1.    1.    2.    2.    1.    1.    1.    1.
1.    1.
 360.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    2.    1.    0.    1.    1.
1.    1.

------*-------------------------------------------------------------------------------------------------------------
-------
 MAX  *    2.    2.    2.    1.    1.    1.    1.    2.    2.    3.    1.    1.    2.    2.    1.    1.    1.    2.
2.    2.
 DEGR. *  150   150   160   220   230   290   270   290   290   300     0   350   320     0    30    80    90   120
110   110
```


JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

```
 WIND  * CONCENTRATION
 ANGLE *     (ug/m**3)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38
REC39 REC40

------*-------------------------------------------------------------------------------------------------------------
-------
   0.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  10.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  20.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  30.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  40.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
  50.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
  60.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
  70.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
  80.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
  90.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 100.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 110.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 120.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 130.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 140.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.
0.    0.
 150.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.
0.    0.
 160.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    0.
0.    0.
 170.  *    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    0.    1.
0.    1.
 180.  *    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
0.    1.
 190.  *    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    1.
 200.  *    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    1.
 210.  *    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    1.
 220.  *    1.    1.    1.    1.    1.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    1.
 230.  *    1.    1.    1.    1.    0.    0.    0.    1.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.
1.    0.
 240.  *    0.    1.    1.    1.    0.    1.    1.    1.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.
1.    1.
 250.  *    1.    1.    1.    0.    0.    0.    1.    1.    1.    0.    0.    0.    1.    1.    2.    1.    1.    1.
0.    1.
 260.  *    0.    1.    0.    0.    0.    0.    1.    1.    1.    0.    0.    1.    1.    1.    1.    1.    0.    0.
0.    1.
 270.  *    1.    1.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    0.    0.
0.    0.
 280.  *    0.    1.    0.    0.    0.    0.    1.    1.    1.    1.    0.    1.    1.    1.    1.    1.    1.    0.
0.    0.
 290.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    1.    1.    1.    1.    1.    0.    0.
0.    0.
 300.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    1.    0.    0.
0.    0.
 310.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.
0.    0.
 320.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 330.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.
0.    0.
 340.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.
0.    0.
 350.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.
 360.  *    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    0.    1.    0.    0.    0.    0.
0.    0.

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-------
 MAX  *    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    2.    1.    1.    1.
1.    1.
 DEGR. *  180   210   220   220   220   240   250   240   270   280   270   280   270   260   250   240   230   210
```

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	0.	0.	0.
10.	0.	0.	0.	0.	0.
20.	0.	0.	0.	0.	0.
30.	0.	0.	0.	0.	0.
40.	0.	0.	0.	0.	0.
50.	0.	0.	0.	0.	0.
60.	0.	0.	0.	0.	0.
70.	0.	0.	0.	0.	0.
80.	0.	0.	0.	0.	0.
90.	0.	0.	0.	0.	0.
100.	0.	0.	0.	0.	0.
110.	0.	0.	0.	0.	0.
120.	0.	0.	0.	0.	0.
130.	0.	0.	0.	0.	0.
140.	0.	0.	0.	0.	0.
150.	0.	0.	0.	0.	0.
160.	0.	0.	0.	0.	1.
170.	0.	0.	0.	0.	1.
180.	0.	0.	0.	1.	0.
190.	0.	0.	1.	0.	1.
200.	0.	0.	1.	0.	1.
210.	0.	0.	0.	1.	0.
220.	0.	0.	0.	0.	0.
230.	0.	0.	1.	0.	0.
240.	0.	0.	0.	0.	0.
250.	0.	0.	0.	0.	0.
260.	1.	0.	0.	0.	0.
270.	0.	0.	0.	0.	0.
280.	0.	0.	0.	0.	1.
290.	0.	0.	0.	0.	0.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	0.	0.	0.
360.	0.	0.	0.	0.	0.
MAX	1.	0.	1.	1.	1.
DEGR.	260	170	190	180	190

THE HIGHEST CONCENTRATION OF 3. ug/m**3 OCCURRED AT RECEPTOR REC10.

CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221

JOB: Government Center Garage RUN: 2028BD

DATE : 8/ 7/13
TIME : 17:15:56

The MODE flag has been set to P for calculating PM averages.

SITE & METEOROLOGICAL VARIABLES

VS = 0.0 CM/S VD = 0.0 CM/S Z0 = 175. CM
U = 1.0 M/S CLAS = 4 (D) ATIM = 60. MINUTES MIXH = 1000. M AMB = 0.0 ug/m**3

LINK VARIABLES

LINK DESCRIPTION	*	LINK COORDINATES (FT) X1	Y1	X2	Y2	*	LENGTH (FT)	BRG (DEG)	TYPE	VPH	EF (G/MI)	H (FT)	W (FT)	V/C	QUEUE (VEH)
1. Char/Merr SB	*	6111.6	5425.1	6030.2	5454.5	*	87.	290.	AG	0.	100.0	1.0	30.0	0.67	4.4
2. Char/Merr WB	*	6250.4	5435.2	6310.4	5482.7	*	77.	52.	AG	0.	100.0	1.0	30.0	0.67	3.9
3. Char/Merr NB R	*	6291.7	5369.7	6352.1	5328.7	*	73.	124.	AG	0.	100.0	1.0	10.0	0.37	3.7
4. Char/Merr NB LTT	*	6280.4	5347.2	6430.9	5241.1	*	184.	125.	AG	0.	100.0	1.0	20.0	0.94	9.4
5. Char/Merr EB	*	6104.2	5362.2	5936.5	5299.8	*	179.	250.	AG	0.	100.0	1.0	20.0	0.92	9.1
6. Char/Cam SB L	*	5384.1	4834.2	5402.6	4908.3	*	76.	14.	AG	0.	100.0	1.0	10.0	0.42	3.9
7. Char/Cam SB TR	*	5360.8	4833.5	5378.3	4889.9	*	59.	17.	AG	0.	100.0	1.0	20.0	0.41	3.0
8. Char/Cam WB LTTR	*	5411.0	4793.5	5482.6	4776.9	*	74.	103.	AG	0.	100.0	1.0	20.0	0.41	3.7
9. Char/Cam NB L	*	5363.0	4722.4	5360.8	4624.3	*	98.	181.	AG	0.	100.0	1.0	10.0	0.53	5.0
10. Char/Cam NB TR	*	5383.3	4723.8	5385.0	4612.7	*	111.	179.	AG	0.	100.0	1.0	20.0	0.74	5.6
11. Char/Cam EB TTTR	*	5302.7	4739.8	5209.4	4740.8	*	93.	271.	AG	0.	100.0	1.0	30.0	0.52	4.7
12. Sud/Merr SB L	*	6532.7	5210.3	6461.3	5261.1	*	88.	305.	AG	0.	100.0	1.0	10.0	0.95	4.5
13. Sud/Merr SB TTT	*	6518.3	5190.8	6482.6	5211.5	*	41.	300.	AG	0.	100.0	1.0	30.0	0.21	2.1
14. Sud/Merr NB TTTR	*	6621.0	5161.1	6684.5	5049.5	*	128.	150.	AG	0.	100.0	1.0	30.0	0.73	6.5
15. Sud/Merr EB LTTR	*	6523.3	5145.9	6447.8	5100.4	*	88.	239.	AG	0.	100.0	1.0	40.0	0.52	4.5
16. Sud/Sur SB LTT	*	6777.5	5369.7	6727.0	5433.2	*	81.	322.	AG	0.	100.0	1.0	20.0	0.53	4.1
17. Sud/Sur SEB	*	6757.2	5330.0	6741.5	5333.9	*	16.	284.	AG	0.	100.0	1.0	10.0	0.15	0.8
18. Sud/Sur EB TTR	*	6794.5	5259.6	6703.4	5223.8	*	98.	249.	AG	0.	100.0	1.0	30.0	0.50	5.0
19. Char/Merr N	*	6202.3	5403.7	5845.3	5537.0	*	381.	290.	AG	989.	0.0	1.0	84.0		
20. Char/Merr E	*	6201.9	5389.8	6552.4	5635.1	*	428.	55.	AG	1538.	0.0	1.0	90.0		
21. Char/Merr S	*	6215.0	5412.2	6411.8	5262.4	*	247.	127.	AG	1494.	0.0	1.0	98.0		
22. Char/Merr W	*	6198.1	5397.3	5806.4	5264.3	*	414.	251.	AG	1409.	0.0	1.0	98.0		
23. Char/Camb N	*	5352.5	4779.7	5466.5	5028.9	*	274.	25.	AG	921.	0.0	1.0	78.0		
24. Char/Camb E	*	5334.7	4787.8	5780.9	4671.3	*	461.	105.	AG	1615.	0.0	1.0	****		
25. Char/Camb S	*	5359.2	4760.4	5362.4	4406.8	*	354.	179.	AG	1034.	0.0	1.0	78.0		
26. Char/Camb W	*	5364.5	4766.8	5009.5	4767.8	*	355.	270.	AG	1697.	0.0	1.0	90.0		
27. Sur/Sud E	*	6831.8	5286.6	6967.4	5375.3	*	162.	57.	AG	1032.	0.0	1.0	30.0		
28. Sur/Sud S	*	6823.4	5285.6	7028.2	5094.0	*	280.	133.	AG	504.	0.0	1.0	54.0		
29. Sur/Sud N	*	6816.3	5313.7	6641.1	5547.0	*	292.	323.	AG	424.	0.0	1.0	42.0		
30. Sur/Sud W	*	6584.4	5170.4	6806.2	5268.7	*	243.	66.	AG	1075.	0.0	1.0	54.0		
31. Sur/Sud NW	*	6797.9	5327.0	6702.8	5348.7	*	98.	283.	AG	37.	0.0	1.0	42.0		
32. Merr/Sud N	*	6569.4	5187.0	6420.9	5287.0	*	179.	304.	AG	1457.	0.0	1.0	98.0		
33. Merr/Sud S	*	6567.7	5198.7	6786.2	4848.7	*	413.	148.	AG	1759.	0.0	1.0	90.0		
34. Merr/Sud W	*	6576.0	5173.7	6284.1	5013.7	*	333.	241.	AG	992.	0.0	1.0	78.0		

1. Char/Merr SB	*	100	76	3.0	615	1600	0.03	1	3
2. Char/Merr WB	*	100	79	3.0	517	1600	0.03	1	3
3. Char/Merr NB R	*	100	52	3.0	257	1600	0.03	1	3
4. Char/Merr NB LTT	*	100	73	3.0	660	1600	0.03	1	3
5. Char/Merr EB	*	100	72	3.0	679	1600	0.03	1	3
6. Char/Cam SB L	*	100	60	3.0	233	1600	0.03	1	3
7. Char/Cam SB TR	*	100	72	3.0	301	1600	0.03	1	3
8. Char/Cam WB LTTR	*	100	62	3.0	435	1600	0.03	1	3
9. Char/Cam NB L	*	100	60	3.0	299	1600	0.03	1	3
10. Char/Cam NB TR	*	100	72	3.0	543	1600	0.03	1	3

11. Char/Cam EB TTTR	*	100	62	3.0	827	1600	0.03	1	3
12. Sud/Merr SB L	*	100	88	3.0	106	1600	0.03	1	3
13. Sud/Merr SB TTT	*	100	52	3.0	435	1600	0.03	1	3
14. Sud/Merr NB TTTR	*	100	64	3.0	1094	1600	0.03	1	3
15. Sud/Merr EB LTTR	*	100	65	3.0	992	1600	0.03	1	3
16. Sud/Sur SB LTT	*	100	70	3.0	424	1600	0.03	1	3
17. Sud/Sur SEB	*	100	80	3.0	37	1600	0.03	1	3
18. Sud/Sur EB TTR	*	100	50	3.0	1075	1600	0.03	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
1. Sud/Merr NE1	*	6492.5	5309.9	6.0
2. Sud/Merr NE2	*	6554.8	5268.0	6.0
3. Sud/Merr NE3	*	6616.2	5224.9	6.0
4. Sud/Merr NE4	*	6684.7	5255.3	6.0
5. Sud/Merr NE5	*	6753.3	5285.7	6.0
6. Sud/Merr SE1	*	6792.9	5222.3	6.0
7. Sud/Merr SE2	*	6724.3	5191.9	6.0
8. Sud/Merr SE3	*	6655.7	5161.5	6.0
9. Sud/Merr SE4	*	6695.5	5097.9	6.0
10. Sud/Merr SE5	*	6735.2	5034.3	6.0
11. Sud/Merr SW1	*	6638.6	4981.3	6.0
12. Sud/Merr SW2	*	6598.9	5045.0	6.0
13. Sud/Merr SW3	*	6559.1	5108.6	6.0
14. Sud/Merr SW4	*	6493.4	5072.5	6.0
15. Sud/Merr SW5	*	6427.6	5036.5	6.0
16. Sud/Merr NW1	*	6347.8	5104.5	6.0
17. Sud/Merr NW2	*	6413.5	5140.5	6.0
18. Sud/Merr NW3	*	6479.3	5176.6	6.0
19. Sud/Merr NW4	*	6417.1	5218.5	6.0
20. Sud/Merr NW5	*	6354.9	5260.4	6.0
21. Sud/Sur NE1	*	6755.9	5445.7	6.0
22. Sud/Sur NE2	*	6801.0	5385.7	6.0
23. Sud/Sur NE3	*	6846.0	5325.7	6.0
24. Sud/Sur NE4	*	6908.8	5366.8	6.0
25. Sud/Sur NE5	*	6971.5	5407.9	6.0
26. Sud/Sur SE1	*	7002.4	5368.4	6.0
27. Sud/Sur SE2	*	6939.7	5327.3	6.0
28. Sud/Sur SE3	*	6876.9	5286.2	6.0
29. Sud/Sur SE4	*	6931.7	5235.0	6.0
30. Sud/Sur SE5	*	6986.5	5183.8	6.0
31. Sud/Sur SW1	*	6932.3	5133.1	6.0
32. Sud/Sur SE2	*	6877.5	5184.3	6.0
33. Sud/Sur SE3	*	6822.7	5235.5	6.0

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z
34. Sud/Sur SE4	*	6754.2	5205.1	6.0
35. Sud/Sur SE5	*	6685.6	5174.8	6.0
36. Sud/Sur NW1	*	6645.5	5237.9	6.0
37. Sud/Sur NW2	*	6714.1	5268.3	6.0
38. Sud/Sur NW3	*	6782.7	5298.7	6.0
39. Sud/Sur NW4	*	6709.5	5315.4	6.0
40. Sud/Sur NW5	*	6636.4	5332.0	6.0
41. Sud/Sur N1	*	6642.4	5493.7	6.0
42. Sud/Sur N2	*	6687.4	5433.7	6.0
43. Sud/Sur N3	*	6732.4	5373.8	6.0
44. Sud/Sur N4	*	6659.3	5390.4	6.0
45. Sud/Sur N5	*	6586.2	5407.1	6.0

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (ug/m**3) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20

0.	*	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	2.	1.	0.	1.	1.
1.	1.																		
10.	*	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
20.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
30.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
40.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
50.	*	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
60.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.
1.	1.																		
70.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.
1.	1.																		
80.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.
1.	1.																		
90.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
100.	*	0.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
110.	*	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	2.
1.	2.																		
120.	*	0.	0.	0.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	1.	1.	1.
1.	1.																		
130.	*	1.	1.	0.	1.	1.	0.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.	1.	1.
1.	1.																		
140.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.
1.	1.																		
150.	*	1.	1.	1.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.
1.	0.																		
160.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
170.	*	1.	1.	2.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
180.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
190.	*	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
200.	*	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
210.	*	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
220.	*	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	1.
0.	0.																		
230.	*	1.	1.	2.	1.	1.	0.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
240.	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
250.	*	1.	1.	1.	1.	1.	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
260.	*	1.	1.	1.	1.	0.	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
270.	*	1.	1.	1.	0.	0.	1.	1.	2.	1.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
280.	*	1.	1.	1.	1.	0.	1.	1.	2.	2.	1.	0.	0.	1.	0.	0.	0.	0.	0.
0.	0.																		
290.	*	1.	1.	1.	0.	0.	1.	1.	2.	2.	1.	0.	0.	1.	1.	0.	0.	0.	0.
1.	1.																		
300.	*	1.	1.	1.	0.	0.	1.	1.	2.	2.	2.	0.	1.	1.	1.	0.	0.	0.	1.
1.	1.																		
310.	*	0.	0.	0.	0.	0.	1.	1.	1.	2.	2.	1.	1.	2.	1.	0.	0.	0.	1.
1.	1.																		
320.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	2.	2.	1.	0.	1.	1.
2.	2.																		
330.	*	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	1.
1.	1.																		
340.	*	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
1.	2.																		
350.	*	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.
1.	1.																		
360.	*	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.	1.	1.	1.	2.	1.	0.	1.	1.
1.	1.																		

MAX	*	1.	1.	2.	1.	1.	1.	1.	2.	2.	2.	1.	1.	2.	2.	1.	1.	1.	2.
2.	2.																		
DEGR.	*	150	160	170	220	190	270	290	280	300	300	10	30	310	0	30	80	90	80
320	110																		

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum

concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (ug/m**3)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40

0.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		
10.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
0.	0.																		
20.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
0.	0.																		
30.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
0.	0.																		
40.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
0.	0.																		
50.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.	0.
0.	0.																		
60.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.
0.	0.																		
70.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.																		
80.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
90.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
100.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
110.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
120.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
130.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
0.	0.																		
140.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.
0.	0.																		
150.	*	0.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
0.	0.																		
160.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	0.
1.	0.																		
170.	*	1.	0.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	1.																		
180.	*	1.	0.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	1.																		
190.	*	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	1.																		
200.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	1.																		
210.	*	1.	1.	1.	1.	1.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	1.																		
220.	*	1.	1.	1.	1.	1.	0.	0.	0.	1.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	1.																		
230.	*	1.	1.	1.	1.	1.	0.	1.	1.	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.
1.	0.																		
240.	*	1.	1.	1.	1.	1.	1.	1.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.
0.	0.																		
250.	*	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.	0.	1.	1.	1.	1.	1.	0.
0.	0.																		
260.	*	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	0.	1.	1.	1.	1.	1.	0.	0.
0.	0.																		
270.	*	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	0.	1.	1.	2.	1.	0.	0.
0.	1.																		
280.	*	0.	1.	1.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	0.
0.	0.																		
290.	*	0.	1.	0.	0.	0.	0.	1.	1.	1.	1.	1.	1.	1.	1.	2.	1.	0.	0.
0.	0.																		
300.	*	0.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
310.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	1.	0.	0.	0.
0.	0.																		
320.	*	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.	1.	1.	0.	0.	0.	0.
0.	0.																		
330.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		
340.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		
350.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		
360.	*	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.	0.	0.	0.	0.
0.	0.																		

MAX	*	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	2.	1.	1.	1.
1.	1.																		
DEGR.	*	190	220	230	220	220	250	250	250	270	280	290	280	270	270	290	180	230	220

180 170

JOB: Government Center Garage RUN: 2028BD

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (ug/m**3) REC41	REC42	REC43	REC44	REC45
0.	0.	0.	0.	0.	0.
10.	0.	0.	0.	0.	0.
20.	0.	0.	0.	0.	0.
30.	0.	0.	0.	0.	0.
40.	0.	0.	0.	0.	0.
50.	0.	0.	0.	0.	0.
60.	0.	0.	0.	0.	0.
70.	0.	0.	0.	0.	0.
80.	0.	0.	0.	0.	0.
90.	0.	0.	0.	0.	0.
100.	0.	0.	0.	0.	0.
110.	0.	1.	0.	0.	0.
120.	0.	1.	0.	0.	0.
130.	0.	1.	0.	0.	0.
140.	0.	0.	0.	0.	0.
150.	0.	0.	0.	0.	0.
160.	0.	0.	0.	0.	0.
170.	0.	0.	0.	0.	0.
180.	0.	0.	0.	0.	1.
190.	0.	0.	1.	0.	0.
200.	0.	0.	0.	0.	0.
210.	0.	0.	1.	0.	0.
220.	0.	0.	0.	0.	0.
230.	0.	0.	0.	0.	0.
240.	0.	0.	0.	0.	0.
250.	0.	0.	0.	0.	0.
260.	0.	0.	0.	0.	0.
270.	0.	0.	0.	0.	0.
280.	0.	0.	0.	0.	1.
290.	0.	0.	0.	0.	0.
300.	0.	0.	0.	0.	0.
310.	0.	0.	0.	0.	0.
320.	0.	0.	0.	0.	0.
330.	0.	0.	0.	0.	0.
340.	0.	0.	0.	0.	0.
350.	0.	0.	0.	0.	0.
360.	0.	0.	0.	0.	0.
MAX	0.	1.	1.	0.	1.
DEGR.	190	110	190	170	180

THE HIGHEST CONCENTRATION OF 2. ug/m**3 OCCURRED AT RECEPTOR REC9 .

Microscale Results

11679.00 Government Center Garage

Pollutant	Time Period	Background Concentration	Persistence Factor
Carbon Monoxide (CO)	1-hour	3	
	8-hour	2.1	0.7
Particulate Matter 10 (PM10)	24-Hour	39.3	0.4
Particulate Matter 2.5 (PM2.5)	Annual	9.2	0.08
	24-Hour	20.7	0.4

		EVENING PEAK HOUR																							
Intersection	Receptor	1-Hour CO Raw			1-Hour CO Total			8-Hour CO Total			1-Hour PM10 Raw			24-Hour PM10 Total			1-Hour PM2.5 Raw			24-Hour PM2.5 Total			Annual Hour PM2.5 Total		
		Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build
Merrimack Street at	NE1	0.8	0.9	0.9	3.8	3.9	3.9	2.7	2.7	2.7	3	2	3	40.5	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
Staniford Street, Causeway Street	NE2	0.7	0.8	0.8	3.7	3.8	3.8	2.6	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
and Lomasney Way (Lowell Square)	NE3	0.9	0.9	0.9	3.9	3.9	3.9	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NE4	1.2	1.1	1.1	4.2	4.1	4.1	2.9	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NE5	1.1	1.1	1.1	4.1	4.1	4.1	2.9	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE1	1	0.9	0.9	4.0	3.9	3.9	2.8	2.7	2.7	3	2	2	40.5	40.1	40.1	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE2	0.8	0.8	0.8	3.8	3.8	3.8	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE3	0.8	0.8	0.8	3.8	3.8	3.8	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE4	0.9	0.9	0.9	3.9	3.9	3.9	2.7	2.7	2.7	3	2	3	40.5	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE5	0.7	1.1	1.2	3.7	4.1	4.2	2.6	2.9	2.9	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW1	0.6	0.7	0.7	3.6	3.7	3.7	2.5	2.6	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW2	0.8	0.8	0.8	3.8	3.8	3.8	2.7	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW3	0.9	1	1	3.9	4	4	2.7	2.8	2.8	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW4	0.9	1	1	3.9	4	4	2.7	2.8	2.8	3	2	2	40.5	40.1	40.1	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SW5	1.1	1.1	1.1	4.1	4.1	4.1	2.9	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW1	0.8	0.9	0.9	3.8	3.9	3.9	2.7	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.7	0.8	0.8	3.7	3.8	3.8	2.6	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	0.7	0.7	0.7	3.7	3.7	3.7	2.6	2.6	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW4	0.9	0.8	0.9	3.9	3.8	3.9	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW5	1.1	0.9	1	4.1	3.9	4.0	2.9	2.7	2.8	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
New Chardon Street at	NE1	1.6	1.5	1.5	4.6	4.5	4.5	3.2	3.2	3.2	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
North Washington Street and	NE2	1.4	1.3	1.3	4.4	4.3	4.3	3.1	3.0	3.0	3	3	3	40.5	40.5	40.5	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
the Sumner Tunnel Off-Ramp	NE3	1.4	1.3	1.3	4.4	4.3	4.3	3.1	3.0	3.0	3	3	3	40.5	40.5	40.5	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
and I-93 Southbound and	NE4	0.6	0.6	0.6	3.6	3.6	3.6	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
Callahan Tunnel On-Ramps	NE5	0.8	0.7	0.7	3.8	3.7	3.7	2.7	2.6	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	S1	0.4	0.5	0.5	3.4	3.5	3.5	2.4	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	S2	0.6	0.6	0.6	3.6	3.6	3.6	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	S3	1.1	1	1	4.1	4	4	2.9	2.8	2.8	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	S4	1.3	1.2	1.2	4.3	4.2	4.2	3.0	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	S5	0.9	1	1.1	3.9	4	4.1	2.7	2.8	2.9	3	3	3	40.5	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW1	0.6	0.6	0.7	3.6	3.6	3.7	2.5	2.5	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.6	0.6	0.6	3.6	3.6	3.6	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	1.3	1.2	1.2	4.3	4.2	4.2	3.0	2.9	2.9	3	3	3	40.5	40.5	40.5	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NW4	1.3	1.2	1.2	4.3	4.2	4.2	3.0	2.9	2.9	3	3	3	40.5	40.5	40.5	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NW5	1.4	1.4	1.4	4.4	4.4	4.4	3.1	3.1	3.1	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
New Chardon Street at	NE1	0.9	0.8	0.9	3.9	3.8	3.9	2.7	2.7	2.7	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
Congress Street/Merrimac Street	NE2	1	0.8	1	4	3.8	4	2.8	2.7	2.8	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NE3	1.2	1	1.1	4.2	4	4.1	2.9	2.8	2.9	4	3	4	40.9	40.5	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NE4	1.6	1.3	1.5	4.6	4.3	4.5	3.2	3.0	3.2	4	3	4	40.9	40.5	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NE5	0.8	0.8	1	3.8	3.8	4	2.7	2.7	2.8	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE1	0.9	0.8	0.9	3.9	3.8	3.9	2.7	2.7	2.7	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE2	1	1	1.1	4	4	4.1	2.8	2.8	2.9	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	SE3	1	1	1	4	4	4	2.8	2.8	2.8	3	3	4	40.5	40.5	40.9	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	SE4	0.9	0.9	1	3.9	3.9	4	2.7	2.7	2.8	3	3	3	40.5	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE5	1	0.9	1.1	4	3.9	4.1	2.8	2.7	2.9	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	SW1	0.8	0.8	0.8	3.8	3.8	3.8	2.7	2.7	2.7	3	2	2	40.5	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW2	0.9	0.8	0.9	3.9	3.8	3.9	2.7	2.7	2.7	3	2	3	40.5	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW3	1	0.9	0.9	4	3.9	3.9	2.8	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	SW4	0.7	0.6	0.7	3.7	3.6	3.7	2.6	2.5	2.6	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW5	0.9	0.8	0.9	3.9	3.8	3.9	2.7	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW1	0.7	0.6	0.8	3.7	3.6	3.8	2.6	2.5	2.7	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.8	0.7	0.8	3.8	3.7	3.8	2.7	2.6	2.7	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	1.2	1.1	1.1	4.2	4.1	4.1	2.9	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	NW4	1	1	1	4	4	4	2.8	2.8	2.8	3	3	3	40.5	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW5	0.7	0.7	0.7	3.7	3.7	3.7	2.6	2.6	2.6	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3

New Chardon Street at	NE1	0.6	0.6	0.6	3.6	3.6	3.6	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
Cambridge Street	NE2	0.8	0.8	0.8	3.8	3.8	3.8	2.7	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NE3	1	0.9	0.9	4	3.9	3.9	2.8	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	NE4	1	1	1	4	4	4	2.8	2.8	2.8	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NE5	0.8	0.8	0.8	3.8	3.8	3.8	2.7	2.7	2.7	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE1	0.6	0.7	0.7	3.6	3.7	3.7	2.5	2.6	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE2	0.7	0.8	0.8	3.7	3.8	3.8	2.6	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE3	1.3	1.3	1.3	4.3	4.3	4.3	3.0	3.0	3.0	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE4	1.4	1.1	1.1	4.4	4.1	4.1	3.1	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	SE5	0.8	0.9	0.9	3.8	3.9	3.9	2.7	2.7	2.7	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW1	0.7	0.7	0.7	3.7	3.7	3.7	2.6	2.6	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW2	0.9	0.8	0.8	3.9	3.8	3.8	2.7	2.7	2.7	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SW3	1.1	1	1	4.1	4	4	2.9	2.8	2.8	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	SW4	1.4	1.3	1.3	4.4	4.3	4.3	3.1	3.0	3.0	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SW5	1	0.9	1	4	3.9	4	2.8	2.7	2.8	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW1	0.8	0.9	0.9	3.8	3.9	3.9	2.7	2.7	2.7	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.8	0.7	0.8	3.8	3.7	3.8	2.7	2.6	2.7	2	3	3	40.1	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW3	1.1	0.9	0.9	4.1	3.9	3.9	2.9	2.7	2.7	3	3	3	40.5	40.5	40.5	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NW4	1	1.1	1.1	4	4.1	4.1	2.8	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW5	0.8	0.9	0.9	3.8	3.9	3.9	2.7	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
New Sudbury Street at	NE1	1	0.9	1	4	3.9	4	2.8	2.7	2.8	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
Congress Street	NE2	1	0.9	0.9	4	3.9	3.9	2.8	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NE3	1.2	1	1.1	4.2	4	4.1	2.9	2.8	2.9	4	3	3	40.9	40.5	40.5	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NE4	0.8	0.7	0.8	3.8	3.7	3.8	2.7	2.6	2.7	3	2	3	40.5	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NE5	1	0.8	1	4	3.8	4	2.8	2.7	2.8	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE1	0.9	0.9	1	3.9	3.9	4	2.7	2.7	2.8	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE2	0.9	0.8	0.8	3.9	3.8	3.8	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE3	1.4	1.3	1.4	4.4	4.3	4.4	3.1	3.0	3.1	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE4	1.6	1.3	1.6	4.6	4.3	4.6	3.2	3.0	3.2	4	4	4	40.9	40.9	40.9	3	2	2	21.9	21.5	21.5	9.4	9.4	9.4
	SE5	1.1	1.2	1.3	4.1	4.2	4.3	2.9	2.9	3.0	4	3	4	40.9	40.5	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SW1	0.8	0.8	0.9	3.8	3.8	3.9	2.7	2.7	2.7	3	2	3	40.5	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW2	0.9	0.8	0.8	3.9	3.8	3.8	2.7	2.7	2.7	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SW3	1.1	1	1.1	4.1	4	4.1	2.9	2.8	2.9	3	3	4	40.5	40.5	40.9	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	SW4	1.5	1.3	1.4	4.5	4.3	4.4	3.2	3.0	3.1	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	SW5	0.9	0.9	0.9	3.9	3.9	3.9	2.7	2.7	2.7	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW1	0.8	0.7	0.9	3.8	3.7	3.9	2.7	2.6	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	1.2	1.1	1.1	4.2	4.1	4.1	2.9	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW3	1.2	1.1	1.1	4.2	4.1	4.1	2.9	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	NW4	0.9	0.8	1.2	3.9	3.8	4.2	2.7	2.7	2.9	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	NW5	1	1	1.3	4	4	4.3	2.8	2.8	3.0	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
New Sudbury Street at	NE1	0.9	0.9	0.9	3.9	3.9	3.9	2.7	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
Blackstone Street/Surface Road	NE2	0.7	0.6	0.7	3.7	3.6	3.7	2.6	2.5	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NE3	0.8	0.6	0.7	3.8	3.6	3.7	2.7	2.5	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NE4	0.6	0.6	0.7	3.6	3.6	3.7	2.5	2.5	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NE5	0.6	0.6	0.6	3.6	3.6	3.6	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE1	0.6	0.5	0.5	3.6	3.5	3.5	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE2	0.6	0.6	0.6	3.6	3.6	3.6	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE3	1	0.9	0.9	4	3.9	3.9	2.8	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE4	0.6	0.6	0.6	3.6	3.6	3.6	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE5	0.4	0.3	0.4	3.4	3.3	3.4	2.4	2.3	2.4	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW1	0.3	0.3	0.4	3.3	3.3	3.4	2.3	2.3	2.4	1	1	2	39.7	39.7	40.1	1	0	1	21.1	20.7	21.1	9.3	9.2	9.3
	SW2	0.5	0.4	0.6	3.5	3.4	3.6	2.5	2.4	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW3	1	1	1	4	4	4	2.8	2.8	2.8	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SW4	0.8	0.7	0.9	3.8	3.7	3.9	2.7	2.6	2.7	3	2	3	40.5	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW5	1	0.9	1.1	4	3.9	4.1	2.8	2.7	2.9	3	3	4	40.5	40.5	40.9	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW1	0.9	0.8	0.9	3.9	3.8	3.9	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW2	0.8	0.7	1	3.8	3.7	4	2.7	2.6	2.8	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	1	0.9	0.9	4	3.9	3.9	2.8	2.7	2.7	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW4	0.5	0.5	0.7	3.5	3.5	3.7	2.5	2.5	2.6	2	1	2	40.1	39.7	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW5	0.6	0.4	0.5	3.6	3.4	3.5	2.5	2.4	2.5	2	1	2	40.1	39.7	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	N1	0.3	0.3	0.3	3.3	3.3	3.3	2.3	2.3	2.3	1	1	1	39.7	39.7	39.7	1	0	0	21.1	20.7	20.7	9.3	9.2	9.2
	N2	0.4	0.4	0.5	3.4	3.4	3.5	2.4	2.4	2.5	1	1	1	39.7	39.7	39.7	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	N3	0.5	0.5	0.5	3.5	3.5	3.5	2.5	2.5	2.5	1	1	1	39.7	39.7	39.7	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	N4	0.4	0.4	0.4	3.4	3.4	3.4	2.4	2.4	2.4	1	1	1	39.7	39.7	39.7	1	1	0	21.1	21.1	20.7	9.3	9.3	9.2
	N5	0.4	0.4	0.4	3.4	3.4	3.4	2.4	2.4	2.4	1	1	1	39.7	39.7	39.7	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3

11679.00 Redevelopment of Government Center Garage

Pollutant	Time Period	Background Concentration	Persistence Factor
Carbon Monoxide (CO)	1-hour	3	-
	8-hour	2.1	0.7
Particulate Matter 10 (PM10)	24-Hour	39.3	0.4
Particulate Matter 2.5 (PM2.5)	Annual	9.2	0.08
	24-Hour	20.7	0.4

		MORNING PEAK HOUR																					
Intersection	Receptor	1-Hour CO Raw			1-Hour CO Total			8-Hour CO Total			1-Hour PM10 Raw			24-Hour PM10 Total			1-Hour PM2.5 Raw			24-Hour PM2.5 Total			Annual PM2.5 Total		
		Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build
Merrimack Street at	NE1	0.7	0.7	0.7	3.7	3.7	3.7	2.6	2.6	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
Staniford Street, Causeway Street	NE2	0.7	0.6	0.6	3.7	3.6	3.6	2.6	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
and Lomasney Way (Lowell Square)	NE3	0.9	1	1	3.9	4	4	2.7	2.8	2.8	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NE4	1.1	1.1	1.1	4.1	4.1	4.1	2.9	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NE5	1.1	1.2	1.2	4.1	4.2	4.2	2.9	2.9	2.9	3	3	3	40.5	40.5	40.5	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE1	0.9	0.8	0.8	3.9	3.8	3.8	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE2	0.8	0.8	0.8	3.8	3.8	3.8	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE3	0.7	0.7	0.7	3.7	3.7	3.7	2.6	2.6	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE4	0.7	0.8	0.8	3.7	3.8	3.8	2.6	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE5	0.7	0.8	0.8	3.7	3.8	3.8	2.6	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW1	0.6	0.6	0.6	3.6	3.6	3.6	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW2	0.7	0.7	0.7	3.7	3.7	3.7	2.6	2.6	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW3	0.8	0.9	0.9	3.8	3.9	3.9	2.7	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW4	1	0.9	0.9	4	3.9	3.9	2.8	2.7	2.7	3	2	2	40.5	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW5	0.7	1.1	1.1	3.7	4.1	4.1	2.6	2.9	2.9	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW1	0.8	0.9	0.9	3.8	3.9	3.9	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.7	0.8	0.8	3.7	3.8	3.8	2.6	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	0.5	0.7	0.7	3.5	3.7	3.7	2.5	2.6	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW4	0.9	0.9	0.9	3.9	3.9	3.9	2.7	2.7	2.7	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW5	1	0.9	0.9	4	3.9	3.9	2.8	2.7	2.7	3	3	3	40.5	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
North Washington Street at	NE1	1.7	1.9	1.9	4.7	4.9	4.9	3.3	3.4	3.4	6	6	6	41.7	41.7	41.7	3	3	3	21.9	21.9	21.9	9.4	9.4	9.4
Causeway Street (Keany Square)	NE2	1.8	1.9	1.9	4.8	4.9	4.9	3.4	3.4	3.4	6	6	6	41.7	41.7	41.7	3	2	2	21.9	21.5	21.5	9.4	9.4	9.4
	NE3	1.7	1.7	1.7	4.7	4.7	4.7	3.3	3.3	3.3	6	6	6	41.7	41.7	41.7	3	3	3	21.9	21.9	21.9	9.4	9.4	9.4
	NE4	1.6	1.7	1.7	4.6	4.7	4.7	3.2	3.3	3.3	5	4	4	41.3	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NE5	1.3	1.3	1.3	4.3	4.3	4.3	3.0	3.0	3.0	4	3	4	40.9	40.5	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE1	1.3	1.3	1.3	4.3	4.3	4.3	3.0	3.0	3.0	4	3	3	40.9	40.5	40.5	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE2	1.4	1.5	1.5	4.4	4.5	4.5	3.1	3.2	3.2	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE3	1.7	1.9	1.9	4.7	4.9	4.9	3.3	3.4	3.4	6	6	6	41.7	41.7	41.7	3	3	3	21.9	21.9	21.9	9.4	9.4	9.4
	SE4	1.4	1.6	1.7	4.4	4.6	4.7	3.1	3.2	3.3	5	5	5	41.3	41.3	41.3	3	2	2	21.9	21.5	21.5	9.4	9.4	9.4
	SE5	1.5	1.7	1.7	4.5	4.7	4.7	3.2	3.3	3.3	5	5	5	41.3	41.3	41.3	3	2	2	21.9	21.5	21.5	9.4	9.4	9.4
	SW1	1.3	1.2	1.2	4.3	4.2	4.2	3.0	2.9	2.9	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SW2	1.2	1.3	1.3	4.2	4.3	4.3	2.9	3.0	3.0	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SW3	1.8	1.9	1.9	4.8	4.9	4.9	3.4	3.4	3.4	5	5	5	41.3	41.3	41.3	3	2	2	21.9	21.5	21.5	9.4	9.4	9.4
	SW4	1.7	1.5	1.6	4.7	4.5	4.6	3.3	3.2	3.2	4	4	4	40.9	40.9	40.9	3	2	2	21.9	21.5	21.5	9.4	9.4	9.4
	SW5	1.1	1	1	4.1	4	4	2.9	2.8	2.8	4	3	3	40.9	40.5	40.5	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NW1	1.1	1	1	4.1	4	4	2.9	2.8	2.8	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW2	1.4	1.4	1.4	4.4	4.4	4.4	3.1	3.1	3.1	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NW3	1.5	2	2.1	4.5	5	5.1	3.2	3.5	3.6	5	5	6	41.3	41.3	41.7	3	2	3	21.9	21.5	21.9	9.4	9.4	9.4
	NW4	1.6	2	2	4.6	5	5	3.2	3.5	3.5	5	5	5	41.3	41.3	41.3	3	2	2	21.9	21.5	21.5	9.4	9.4	9.4
	NW5	1.7	1.9	1.9	4.7	4.9	4.9	3.3	3.4	3.4	5	5	5	41.3	41.3	41.3	3	2	2	21.9	21.5	21.5	9.4	9.4	9.4
North Washington Street at	NE1	1.3	1.8	1.9	4.3	4.8	4.9	3.0	3.4	3.4	4	4	4	40.9	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
Thatcher Street and Valenti Way	NE2	1.1	1.9	1.9	4.1	4.9	4.9	2.9	3.4	3.4	4	5	5	40.9	41.3	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NE3	1.3	2	1.9	4.3	5	4.9	3.0	3.5	3.4	5	5	5	41.3	41.3	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NE4	0.6	1	1	3.6	4	4	2.5	2.8	2.8	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NE5	0.4	0.8	0.8	3.4	3.8	3.8	2.4	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE1	0.5	0.8	0.8	3.5	3.8	3.8	2.5	2.7	2.7	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE2	0.6	1.1	1	3.6	4.1	4	2.5	2.9	2.8	2	3	2	40.1	40.5	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE3	1.4	1.9	1.9	4.4	4.9	4.9	3.1	3.4	3.4	4	5	5	40.9	41.3	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE4	1.3	2.1	2.1	4.3	5.1	5.1	3.0	3.6	3.6	5	5	5	41.3	41.3	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE5	1.4	2	2	4.4	5	5	3.1	3.5	3.5	5	5	5	41.3	41.3	41.3	3	3	3	21.9	21.9	21.9	9.4	9.4	9.4
	SW1	1.5	3.1	2.7	4.5	6.1	5.7	3.2	4.3	4.0	5	8	7	41.3	42.5	42.1	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	SW2	1.3	2.1	2	4.3	5.1	5	3.0	3.6	3.5	4	6	6	40.9	41.7	41.7	2	3	2	21.5	21.9	21.5	9.4	9.4	9.4
	SW3	1.4	2.1	2	4.4	5.1	5	3.1	3.6	3.5	4	5	5	40.9	41.3	41.3	3	3	3	21.9	21.9	21.9	9.4	9.4	9.4
	SW4	0.7	1.6	1.5	3.7	4.6	4.5	2.6	3.2	3.2	3	4	4	40.5	40.9	40.9	1	2	2	21.1	21.5	21.5	9.3	9.4	9.4
	SW5	0.6	1.2	1.2	3.6	4.2	4.2	2.5	2.9	2.9	2	3	2	40.1	40.5	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW1	0.6	1.2	1.1	3.6	4.2	4.1	2.5	2.9	2.9	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.8	1.3	1.3	3.8	4.3	4.3	2.7	3.0	3.0	2	3	4	40.1	40.5	40.9	1	2	2	21.1	21.5	21.5	9.3	9.4	9.4
	NW3	1.2	2	2	4.2	5	5	2.9	3.5	3.5	4	5	5	40.9	41.3	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NW4	1	1.8	1.8	4	4.8	4.8	2.8	3.4	3.4	4	5	5	40.9	41.3	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	NW5	1.1	1.7	1.7	4.1	4.7	4.7	2.9	3.3	3.3	4	5	5	40.9	41.3	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4

11679.00 Redevelopment of Government Center Garage

Pollutant	Time Period	Background Concentration	Persistence Factor
Carbon Monoxide (CO)	1-hour	3	-
	8-hour	2.1	0.7
Particulate Matter 10 (PM10)	24-Hour	39.3	0.4
Particulate Matter 2.5 (PM2.5)	Annual	9.2	0.08
	24-Hour	20.7	0.4

		MORNING PEAK HOUR																					
Intersection	Receptor	1-Hour CO Raw			1-Hour CO Total			8-Hour CO Total			1-Hour PM10 Raw			24-Hour PM10 Total			1-Hour PM2.5 Raw			24-Hour PM2.5 Total			Annual PM2.5 Total		
		Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build
North Washington Street at	N1	1.3	2	2	4.3	5	5	3.0	3.5	3.5	4	5	5	40.9	41.3	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
Beverly Street	N2	1.3	2	2	4.3	5	5	3.0	3.5	3.5	4	6	5	40.9	41.7	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	N3	1.4	2.5	2.3	4.4	5.5	5.3	3.1	3.9	3.7	5	6	6	41.3	41.7	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	N4	0.8	1.7	1.6	3.8	4.7	4.6	2.7	3.3	3.2	3	4	4	40.5	40.9	40.9	1	2	2	21.1	21.5	21.5	9.3	9.4	9.4
	N5	0.6	1.4	1.5	3.6	4.4	4.5	2.5	3.1	3.2	2	3	3	40.1	40.5	40.5	1	2	2	21.1	21.5	21.5	9.3	9.4	9.4
	SE1	1.4	2	1.9	4.4	5	4.9	3.1	3.5	3.4	5	5	5	41.3	41.3	41.3	3	2	2	21.9	21.5	21.5	9.4	9.4	9.4
	SE2	1.4	1.9	1.9	4.4	4.9	4.9	3.1	3.4	3.4	4	5	6	40.9	41.3	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	SE3	1.7	3.1	3.1	4.7	6.1	6.1	3.3	4.3	4.3	6	8	8	41.7	42.5	42.5	3	3	3	21.9	21.9	21.9	9.4	9.4	9.4
	SE4	1.4	2.8	2.8	4.4	5.8	5.8	3.1	4.1	4.1	4	7	6	40.9	42.1	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	SE5	1.4	3.1	3.2	4.4	6.1	6.2	3.1	4.3	4.3	4	8	7	40.9	42.5	42.1	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	SW1	1.5	2.4	2.4	4.5	5.4	5.4	3.2	3.8	3.8	5	6	6	41.3	41.7	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	SW2	1.3	2.6	2.6	4.3	5.6	5.6	3.0	3.9	3.9	4	6	6	40.9	41.7	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	SW3	1.3	2.8	2.7	4.3	5.8	5.7	3.0	4.1	4.0	4	6	6	40.9	41.7	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	SW4	1	1.7	1.6	4	4.7	4.6	2.8	3.3	3.2	2	4	4	40.1	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SW5	0.6	1.3	1.2	3.6	4.3	4.2	2.5	3.0	2.9	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
New Chardon Street at	NE1	1.4	2.8	2.8	4.4	5.8	5.8	3.1	4.1	4.1	5	7	7	41.3	42.1	42.1	3	3	3	21.9	21.9	21.9	9.4	9.4	9.4
North Washington Street and	NE2	1.3	2.9	2.8	4.3	5.9	5.8	3.0	4.1	4.1	4	7	7	40.9	42.1	42.1	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
the Sumner Tunnel Off-Ramp	NE3	1.3	3.9	3.8	4.3	6.9	6.8	3.0	4.8	4.8	4	9	9	40.9	42.9	42.9	2	4	4	21.5	22.3	22.3	9.4	9.5	9.5
and I-93 Southbound and	NE4	0.6	1.6	1.6	3.6	4.6	4.6	2.5	3.2	3.2	2	4	3	40.1	40.9	40.5	1	2	2	21.1	21.5	21.5	9.3	9.4	9.4
Callahan Tunnel On-Ramps	NE5	0.5	1.5	1.5	3.5	4.5	4.5	2.5	3.2	3.2	2	3	3	40.1	40.5	40.5	1	2	2	21.1	21.5	21.5	9.3	9.4	9.4
	S1	0.6	4.8	4.8	3.6	7.8	7.8	2.5	5.5	5.5	3	10	10	40.5	43.3	43.3	1	5	5	21.1	22.7	22.7	9.3	9.6	9.6
	S2	0.7	2.4	2.4	3.7	5.4	5.4	2.6	3.8	3.8	3	6	6	40.5	41.7	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	S3	1.3	1.9	1.9	4.3	4.9	4.9	3.0	3.4	3.4	4	5	5	40.9	41.3	41.3	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	S4	1	1.5	1.6	4	4.5	4.6	2.8	3.2	3.2	3	4	4	40.5	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	S5	0.6	1.2	1.1	3.6	4.2	4.1	2.5	2.9	2.9	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW1	0.6	1	1	3.6	4	4	2.5	2.8	2.8	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.8	1.3	1.4	3.8	4.3	4.4	2.7	3.0	3.1	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	1.6	2.3	2.3	4.6	5.3	5.3	3.2	3.7	3.7	5	6	6	41.3	41.7	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	NW4	1.4	2.4	2.3	4.4	5.4	5.3	3.1	3.8	3.7	4	6	6	40.9	41.7	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
	NW5	1.3	2.6	2.6	4.3	5.6	5.6	3.0	3.9	3.9	4	6	6	40.9	41.7	41.7	2	3	3	21.5	21.9	21.9	9.4	9.4	9.4
North Street at	NE1	0.8	1	1.1	3.8	4	4.1	2.7	2.8	2.9	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
Congress Street	NE2	0.8	1.1	1.1	3.8	4.1	4.1	2.7	2.9	2.9	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NE3	1.1	1.1	1.2	4.1	4.1	4.2	2.9	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4
	NE4	1	0.9	0.9	4	3.9	3.9	2.8	2.7	2.7	3	2	3	40.5	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NE5	0.9	0.8	0.9	3.9	3.8	3.9	2.7	2.7	2.7	2	2	3	40.1	40.1	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE1	0.8	1	1	3.8	4	4	2.7	2.8	2.8	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SE2	1	1	1.1	4	4	4.1	2.8	2.8	2.9	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SE3	1.1	1.5	1.6	4.1	4.5	4.6	2.9	3.2	3.2	3	4	4	40.5	40.9	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE4	1.1	1.3	1.3	4.1	4.3	4.3	2.9	3.0	3.0	3	3	4	40.5	40.5	40.9	2	2	2	21.5	21.5	21.5	9.4	9.4	9.4
	SE5	0.8	1.1	1.2	3.8	4.1	4.2	2.7	2.9	2.9	2	3	3	40.1	40.5	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW1	0.8	0.8	1	3.8	3.8	4	2.7	2.7	2.8	2	2	3	40.1	40.1	40.5	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW2	0.8	1	1	3.8	4	4	2.7	2.8	2.8	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SW3	0.8	1.1	1.2	3.8	4.1	4.2	2.7	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	SW4	0.5	0.6	0.6	3.5	3.6	3.6	2.5	2.5	2.5	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	SW5	0.5	0.5	0.5	3.5	3.5	3.5	2.5	2.5	2.5	1	1	1	39.7	39.7	39.7	1	0	1	21.1	20.7	21.1	9.3	9.2	9.3
	NW1	0.5	0.5	0.6	3.5	3.5	3.6	2.5	2.5	2.5	1	1	1	39.7	39.7	39.7	1	0	1	21.1	20.7	21.1	9.3	9.2	9.3
	NW2	0.5	0.6	0.7	3.5	3.6	3.7	2.5	2.5	2.6	2	2	2	40.1	40.1	40.1	1	1	1	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	0.9	1.3	1.4	3.9	4.3	4.4	2.7	3.0	3.1	3	3	3	40.5	40.5	40.5	1	1	2	21.1	21.1	21.5	9.3	9.3	9.4
	NW4	1.2	1.3	1.4	4.2	4.3	4.4	2.9	3.0	3.1	3	3	3	40.5	40.5	40.5	2	1	1	21.5	21.1	21.1	9.4	9.3	9.3
	NW5	1	1.2	1.2	4	4.2	4.2	2.8	2.9	2.9	3	3	3	40.5	40.5	40.5	2	1	2	21.5	21.1	21.5	9.4	9.3	9.4

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Pollutant	Time Period	Background Concentration	Persistence Factor
Carbon Monoxide (CO)	1-hour	3	-
	8-hour	2.1	0.7
Particulate Matter 10 (PM10)	24-Hour	39.3	0.4
Particulate Matter 2.5 (PM2.5)	Annual	9.2	0.08
	24-Hour	20.7	0.4

		MORNING PEAK HOUR																							
Intersection	Receptor	1-Hour CO Raw			1-Hour CO Total			8-Hour CO Total			1-Hour PM10 Raw			24-Hour PM10 Total			1-Hour PM2.5 Raw			24-Hour PM2.5 Total			Annual PM2.5 Total		
		Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build	Existing	No Build	Build
New Chardon Street at	NE1	0.8	0.8	1.0	3.8	3.8	4.0	2.7	2.7	2.8	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
Congress Street/Merrimac Street	NE2	0.9	0.7	1.0	3.9	3.7	4.0	2.7	2.6	2.8	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	NE3	1.0	0.9	1.2	4.0	3.9	4.2	2.8	2.7	2.9	4.0	3.0	4.0	40.9	40.5	40.9	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	NE4	1.5	1.2	1.5	4.5	4.2	4.5	3.2	2.9	3.2	4.0	3.0	4.0	40.9	40.5	40.9	2.0	2.0	2.0	21.5	21.5	21.5	9.4	9.4	9.4
	NE5	1.0	1.1	1.2	4.0	4.1	4.2	2.8	2.9	2.9	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	SE1	0.9	0.8	0.9	3.9	3.8	3.9	2.7	2.7	2.7	2.0	2.0	3.0	40.1	40.1	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	SE2	1.1	1.0	1.0	4.1	4.0	4.0	2.9	2.8	2.8	3.0	2.0	3.0	40.5	40.1	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	SE3	0.9	0.8	1.1	3.9	3.8	4.1	2.7	2.7	2.9	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	SE4	0.8	0.7	1.2	3.8	3.7	4.2	2.7	2.6	2.9	3.0	3.0	4.0	40.5	40.5	40.9	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	SE5	1.1	0.9	1.4	4.1	3.9	4.4	2.9	2.7	3.1	3.0	3.0	4.0	40.5	40.5	40.9	2.0	2.0	2.0	21.5	21.5	21.5	9.4	9.4	9.4
	SW1	0.9	0.8	1.0	3.9	3.8	4.0	2.7	2.7	2.8	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW2	0.9	0.9	1.0	3.9	3.9	4.0	2.7	2.7	2.8	3.0	2.0	3.0	40.5	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW3	0.9	0.9	1.0	3.9	3.9	4.0	2.7	2.7	2.8	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	SW4	0.7	0.6	0.8	3.7	3.6	3.8	2.6	2.5	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW5	0.7	0.7	0.9	3.7	3.7	3.9	2.6	2.6	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW1	0.7	0.6	0.9	3.7	3.6	3.9	2.6	2.5	2.7	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.8	0.7	1.0	3.8	3.7	4.0	2.7	2.6	2.8	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	1.1	1.0	1.1	4.1	4.0	4.1	2.9	2.8	2.9	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	NW4	0.9	0.9	1.0	3.9	3.9	4.0	2.7	2.7	2.8	3.0	2.0	3.0	40.5	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW5	0.7	0.6	0.8	3.7	3.6	3.8	2.6	2.5	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
New Chardon Street at	NE1	0.8	0.7	0.8	3.8	3.7	3.8	2.7	2.6	2.7	3.0	2.0	2.0	40.5	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
Cambridge Street	NE2	1.0	0.9	0.9	4.0	3.9	3.9	2.8	2.7	2.7	3.0	2.0	2.0	40.5	40.1	40.1	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	NE3	1.0	0.8	0.9	4.0	3.8	3.9	2.8	2.7	2.7	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	NE4	1.0	0.9	0.9	4.0	3.9	3.9	2.8	2.7	2.7	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	NE5	0.9	0.7	0.8	3.9	3.7	3.8	2.7	2.6	2.7	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	SE1	0.8	0.7	0.8	3.8	3.7	3.8	2.7	2.6	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SE2	0.8	0.8	0.8	3.8	3.8	3.8	2.7	2.7	2.7	3.0	2.0	2.0	40.5	40.1	40.1	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	SE3	1.5	1.4	1.4	4.5	4.4	4.4	3.2	3.1	3.1	4.0	4.0	4.0	40.9	40.9	40.9	2.0	2.0	2.0	21.5	21.5	21.5	9.4	9.4	9.4
	SE4	1.1	1.0	1.1	4.1	4.0	4.1	2.9	2.8	2.9	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	SE5	0.8	0.7	0.8	3.8	3.7	3.8	2.7	2.6	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW1	0.8	0.8	0.8	3.8	3.8	3.8	2.7	2.7	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW2	0.9	0.9	0.9	3.9	3.9	3.9	2.7	2.7	2.7	3.0	2.0	3.0	40.5	40.1	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	SW3	1.2	1.0	1.0	4.2	4.0	4.0	2.9	2.8	2.8	4.0	3.0	3.0	40.9	40.5	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	SW4	1.5	1.3	1.3	4.5	4.3	4.3	3.2	3.0	3.0	4.0	4.0	4.0	40.9	40.9	40.9	2.0	2.0	2.0	21.5	21.5	21.5	9.4	9.4	9.4
	SW5	1.0	1.0	1.0	4.0	4.0	4.0	2.8	2.8	2.8	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	NW1	0.9	0.9	0.9	3.9	3.9	3.9	2.7	2.7	2.7	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	NW2	0.9	0.8	0.8	3.9	3.8	3.8	2.7	2.7	2.7	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	1.0	21.5	21.1	21.1	9.4	9.3	9.3
	NW3	1.0	0.9	0.9	4.0	3.9	3.9	2.8	2.7	2.7	4.0	3.0	3.0	40.9	40.5	40.5	2.0	2.0	2.0	21.5	21.5	21.5	9.4	9.4	9.4
	NW4	1.2	1.2	1.2	4.2	4.2	4.2	2.9	2.9	2.9	4.0	3.0	3.0	40.9	40.5	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	NW5	1.5	1.4	1.4	4.5	4.4	4.4	3.2	3.1	3.1	4.0	3.0	3.0	40.9	40.5	40.5	2.0	2.0	2.0	21.5	21.5	21.5	9.4	9.4	9.4
New Sudbury Street at	NE1	0.9	0.8	1.1	3.9	3.8	4.1	2.7	2.7	2.9	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
Congress Street	NE2	0.9	0.8	1.2	3.9	3.8	4.2	2.7	2.7	2.9	3.0	2.0	3.0	40.5	40.1	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	NE3	1.0	1.0	1.1	4.0	4.0	4.1	2.8	2.8	2.9	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	NE4	0.6	0.6	0.7	3.6	3.6	3.7	2.5	2.5	2.6	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NE5	0.8	0.7	0.9	3.8	3.7	3.9	2.7	2.6	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SE1	1.0	0.8	0.9	4.0	3.8	3.9	2.8	2.7	2.7	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SE2	0.7	0.7	0.9	3.7	3.7	3.9	2.6	2.6	2.7	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SE3	1.3	1.2	1.5	4.3	4.2	4.5	3.0	2.9	3.2	4.0	3.0	4.0	40.9	40.5	40.9	2.0	2.0	2.0	21.5	21.5	21.5	9.4	9.4	9.4
	SE4	1.6	1.3	1.9	4.6	4.3	4.9	3.2	3.0	3.4	4.0	4.0	5.0	40.9	40.9	41.3	2.0	2.0	2.0	21.5	21.5	21.5	9.4	9.4	9.4
	SE5	1.0	1.0	2.5	4.0	4.0	5.5	2.8	2.8	3.9	4.0	3.0	6.0	40.9	40.5	41.7	2.0	1.0	3.0	21.5	21.1	21.9	9.4	9.3	9.4
	SW1	0.7	0.7	0.9	3.7	3.7	3.9	2.6	2.6	2.7	3.0	2.0	3.0	40.5	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW2	0.9	0.8	1.2	3.9	3.8	4.2	2.7	2.7	2.9	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW3	1.2	1.0	1.6	4.2	4.0	4.6	2.9	2.8	3.2	3.0	3.0	4.0	40.5	40.5	40.9	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	SW4	1.1	1.0	1.4	4.1	4.0	4.4	2.9	2.8	3.1	3.0	3.0	3.0	40.5	40.5	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	SW5	0.6	0.6	0.7	3.6	3.6	3.7	2.5	2.5	2.6	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW1	0.5	0.5	0.8	3.5	3.5	3.8	2.5	2.5	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.8	0.8	1.2	3.8	3.8	4.2	2.7	2.7	2.9	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	1.1	1.0	1.5	4.1	4.0	4.5	2.9	2.8	3.2	3.0	3.0	4.0	40.5	40.5	40.9	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	NW4	1.0	1.1	1.5	4.0	4.1	4.5	2.8	2.9	3.2	3.0	3.0	4.0	40.5	40.5	40.9	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	NW5	1.2	1.1	1.5	4.2	4.1	4.5	2.9	2.9	3.2	3.0	3.0	4.0	40.5	40.5	40.9	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
New Sudbury Street at	NE1	0.7	0.7	0.7	3.7	3.7	3.7	2.6	2.6	2.6	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
Blackstone Street/Surface Road	NE2	0.6	0.5	0.7	3.6	3.5	3.7	2.5	2.5	2.6	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NE3	0.6	0.5	0.6	3.6	3.5	3.6	2.5	2.5	2.5	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NE4	0.4	0.4	0.5	3.4	3.4	3.5	2.4	2.4	2.5	1.0	1.0	2.0	39.7	39.7	40.1	1.0	0.0	1.0	21.1	20.7	21.1	9.3	9.2	9.3
	NE5	0.4	0.3	0.4	3.4	3.3	3.4	2.4	2.3	2.4	1.0	1.0	1.0	39.7	39.7	39.7	1.0	0.0	1.0	21.1	20.7	21.1	9.3	9.2	9.3
	SE1	0.3	0.3	0.4	3.3	3.3	3.4	2.3	2.3	2.4	2.0	1.0	2.0	40.1	39.7	40.1	1.0	0.0	1.0	21.1	20.7	21.1	9.3	9.2	9.3
	SE2	0.4	0.4	0.5	3.4	3.4	3.5	2.4	2.4	2.5	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SE3	0.7	0.6	0.8	3.7	3.6	3.8	2.6	2.5	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SE4	0.4	0.3	0.4	3.4	3.3	3.4	2.4	2.3	2.4	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SE5	0.4	0.3	0.5	3.4	3.3	3.5	2.4	2.3	2.5	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW1	0.3	0.3	0.3	3.3	3.3	3.3	2.3	2.3	2.3	1.0	1.0	1.0	39.7	39.7	39.7	1.0	0.0	1.0	21.1	20.7	21.1	9.3	9.2	9.3
	SW2	0.3	0.3	0.5	3.3	3.3	3.5	2.3	2.3	2.5	2.0	1.0	2.0	40.1	39.7	40.1	1.0	0.0	1.0	21.1	20.7	21.1	9.3	9.2	9.3
	SW3	0.9	0.8	0.9	3.9	3.8	3.9	2.7	2.7	2.7	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW4	0.8	0.8	0.9	3.8	3.8	3.9	2.7	2.7	2.7	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	SW5	1.0	0.8	1.1	4.0	3.8	4.1	2.8	2.7	2.9	3.0	2.0	3.0	40.5	40.1	40.5	2.0	1.0	2.0	21.5	21.1	21.5	9.4	9.3	9.4
	NW1	0.8	0.7	1.0	3.8	3.7	4.0	2.7	2.6	2.8	2.0	2.0	3.0	40.1	40.1	40.5	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW2	0.7	0.7	0.7	3.7	3.7	3.7	2.6	2.6	2.6	2.0	1.0	2.0	40.1	39.7	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW3	0.9	0.8	1.0	3.9	3.8	4.0	2.7	2.7	2.8	2.0	2.0	2.0	40.1	40.1	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW4	0.5	0.4	0.5	3.5	3.4	3.5	2.5	2.4	2.5	1.0	1.0	2.0	39.7	39.7	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	NW5	0.4	0.4	0.5	3.4	3.4	3.5	2.4	2.4	2.5	1.0	1.0	2.0	39.7	39.7	40.1	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	N1	0.3	0.2	0.4	3.3	3.2	3.4	2.3	2.2	2.4	1.0	1.0	1.0	39.7	39.7	39.7	1.0	1.0	1.0	21.1	21.1	21.1	9.3	9.3	9.3
	N2	0.3	0.3	0.4	3.3	3.3	3.4	2.3	2.3	2.4	1.0	1.0	1.0	39.7	39.7	39.7	1.0	0.0	0.0	21.1	20.7	20.7	9.3	9.2	9.2
	N3	0.4	0.4	0.5	3.4	3.4	3.5	2.4	2.4	2.5	1.0	1.0	1.0	39.7	39.7	39.7	0.0	0.0	1.0	20.7	20.7	21.1	9.2	9.2	9.3
	N4	0.4	0.3	0.4	3.4	3.3	3.4	2.4	2.3	2.4	1.0	1.0	1.0	39.7	39.7	39.7	1.0	0.0	1.0	21.1	20.7	21.1	9.3	9.2	9.3
	N5	0.4	0.3	0.5	3.4	3.3	3.5	2.4	2.3	2.5	1.0	1.0	2.0	39.7	39.7	40.1	1.0	0.0	1.0	21.1	20.7	21.1	9.3	9.2	9.3

Stationary Source Analysis

BREEZE AERMOD Model Results

Max. Annual (5 YEARS) Results of Pollutant: CO (ug/m**3)

Group ID	High	Avg. Conc.	UTM		Elev.	Hill Ht.	Flag Ht.	Rec. Type	Grid ID
			East (m)	North (m)	(m)	(m)	(m)		
ALL	1ST	0.01832	330107.59	4692173.39	6.50	6.50	0.00	GP	D971N00I
	2ND	0.01829	330098.19	4692176.81	6.50	6.50	0.00	GP	D971N00I
	3RD	0.01828	330116.99	4692169.97	6.50	6.50	0.00	GP	D971N00I
	4TH	0.01819	330088.80	4692180.23	6.50	6.50	0.00	GP	D971N00I
	5TH	0.01814	330126.38	4692166.55	6.50	6.50	0.00	GP	D971N00I
	6TH	0.01803	330079.40	4692183.65	6.50	6.50	0.00	GP	D971N00I
	7TH	0.01788	330137.61	4692214.20	5.60	5.60	0.00	GP	D971N00I
	8TH	0.01784	330104.35	4692025.58	11.70	11.70	0.00	GP	D971N00I
	9TH	0.01783	330128.95	4692219.20	5.50	5.50	0.00	GP	D971N00I
	10TH	0.01782	330070.00	4692187.07	6.50	6.50	0.00	GP	D971N00I

Highest Results of Pollutant: CO

Avg. Per.	Grp ID	High	Type	Val	Units	Date	UTM		Elev.	Hill Ht.	Flag Ht.	Rec. Type	Grid ID
						YYMMDDHH	East (m)	North (m)	(m)	(m)	(m)		
1-HR	ALL	1ST	Avg. Conc.	5.79114	ug/m**3	08100508	330305.10	4692204.10	5.00	5.00	0.00	GP	D971N00I
8-HR	ALL	1ST	Avg. Conc.	0.94823	ug/m**3	08100516	330288.17	4692151.33	5.60	5.60	0.00	GP	D971N00I

Summary of Total Messages

#	Message Type
0	Fatal Error Message(s)
4	Warning Message(s)
668	Informational Message(s)
43848	Hours Were Processed
90	Calm Hours Identified
578	Missing Hours Identified (1.32 Percent)

Error & Warning Messages

Msg. Type	Pathway	Ref. #	Description
WARNING	ME	W186	THRESH_1MIN 1-min ASOS wind speed threshold used 0.50
WARNING	OU	W565	Possible Conflict With Dynamically Allocated FUNIT PLOTFILE
WARNING	OU	W565	Possible Conflict With Dynamically Allocated FUNIT PLOTFILE
WARNING	OU	W565	Possible Conflict With Dynamically Allocated FUNIT PLOTFILE

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Appendix D
Noise Supporting Documentation

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Noise Monitoring Data

Mechanical Equipment Sound Level Data

- Exhaust Fans
- Cooling Towers
- Emergency Generators

Mechanical Equipment Sound Level Calculation

Logan International Airport DNL Contour

Noise Monitoring Data

Summary	
Filename	VHB.002
Serial Number	2555
Model	Model 831
Firmware Version	2.201
User	QVT
Location	Friend Street
Job Description	Government Center Garage Redevelopment
Note	
Measurement Description	
Start	2013/06/26 23:37:08
Stop	2013/06/26 23:55:16
Duration	0:18:07.8
Run Time	0:18:07.8
Pause	0:00:00.0

Results	
LAeq	59.7 dB
LAS1.00	67.0 dB
LAS5.00	63.8 dB
LAS10.00	61.8 dB
LAS50.00	58.2 dB
LAS70.00	57.3 dB
LAS90.00	56.5 dB

Summary	
Filename	VHB.003
Serial Number	2555
Model	Model 831
Firmware Version	2.201
User	QVT
Location	Stillman Place
Job Description	Government Center Garage Redevelopment
Note	
Measurement Description	
Start	2013/06/27 0:03:37
Stop	2013/06/27 0:18:44
Duration	0:15:03.4
Run Time	0:14:16.8
Pause	0:00:46.6

Results	
LAeq	62.1 dB
LAS1.00	71.8 dB
LAS5.00	65.7 dB
LAS10.00	64.5 dB
LAS50.00	59.6 dB
LAS70.00	57.5 dB
LAS90.00	55.1 dB

Mechanical Equipment Sound Level Data

Exhaust Fans

GOVERNMENT CENTER GARAGE REDEVELOPMENT
- DPIR INFORMATION -

BUILDING	STORIES	PARKING / LOADING AREA (GSF)	RESIDENTIAL /AMENITY AREA (GSF)	OFFICE AREA (GSF)	RETAIL AREA (GSF)	TOTAL AREA (GSF)	# OF UNITS OR KEYS	COOLING ⑧		HEATING ⑨		DOMESTIC HOT WATER ⑩	KITCHEN/RESTAURANT PLUMBING ⑪		GARAGE EXHAUST ⑤		GENERAL EXHAUST ⑥		RETAIL KITCHEN HOOD EXHAUST ⑦	EMERGENCY GENERATOR ②
								SF/TON	TONS	BTUH/SF	MBH	MBH	COOKING MBH	DHW MBH	CFM/SF	CFM	CFM/SF or CFM/UNIT	CFM	CFM	kW
WEST BUILDING 1 (RESIDENTIAL)	45	0	490,541	0	2,354	492,895	403	548	900	14	7,000	3,000	750	750	0.75	0	62	25,000	1,000	1,000
WEST BUILDING 2 (OFFICE)	48	124,564	0	1,018,568	9,060	1,152,192	N/A	411	2,800	29	30,000	0	1,000	750	0.75	93,423	0.08	89,400	3,000	1,500
WEST BUILDING 3 (RESIDENTIAL)	24	19,968	268,912	0	8,400	297,280	248	595	500	13	4,000	2,000	1,000	750	0.75	14,976	60	15,000	3,000	800
WEST GARAGE	11	458,444	0	35,000	0	493,444	N/A	389	90 ③	0	0	0	0	0	0.75	343,833	0	0	0	③
EAST BUILDING 1 (HOTEL/CONDO)	23	0	285,042	0	0	285,042	324	570	500	14	4,000	2,300	0	0	0.75	0	62	20,000	0	800
EAST BUILDING 2 (OFFICE)	9	0	0	116,829	20,302	137,131	N/A	392	350	31	4,200	0	1,200	750	0.75	0	0.09	12,600	5,000	600
EAST BUILDING 3 (RETAIL)	4	0	0	0	24,980	24,980	N/A	250	100 ④	20	500	0	1,500	750	0.75	0	0.06	1,500	4,000	①
TOTALS		**602,976**	**1,044,495**	**1,170,397**	**65,096**	**2,882,964**			**5,050**		**49,700**	**7,300**	**5,450**	**3,750**		**452,232**		**163,500**	**16,000**	

Notes:

① Generator not required by code - elevator power feed shall be connected ahead of main.
② All generators shall be housed in a -30 db enclosure (see attached cutsheets for acoustic information w/o the enclosure).
③ The cooling capacity and emergency power will be provided by West Building 2.
④ The cooling capacity for the retail building will be combined with East Building 2.
⑤ Garage exhaust locations will be a minimum of 10'-0" above the green roof and discharge through a louver. Anticipated acoustic performance is between 55 to 59 dbA at maximum capacity.
⑥ General exhaust locations will be at the roof of each building. Anticipated acoustic performance is between 60 to 64 dbA.
⑦ Kitchen hood exhaust for restaurants will be a minimum of 10'-0" above grade and discharge through a louver. Anticipated acoustic performance is between 55 to 59 dbA.
⑧ See attached cutsheets for cooling tower acoustic data.
⑨ Heating boilers will be condensing type and be located at the roof of each building in a mechanical room.
⑩ Domestic hot water heaters will be located at the roof of each building in a mechanical room.
⑪ Restaurant domestic water heaters (DWH) are assumed to be gas-fired sealed combustion type provided by the tenant.

Cooling Towers

Cooling Tower Data Sheet

Chris Wilson
FLUID EQUIPMENT SOLUTIONS OF NEW ENGLAND, LLC

Project : Government Square Garage
Equipment Reference: EB2
Product Type : AT/UT/USS Cooling Tower

Date: 6/24/2013 Page: 1

	Selection Criteria
Capacity (Tons):	450.00
Capacity (MBH):	6,750.00
Fluid Type:	Water
Flow (GPM):	1350.0
Entering Fluid Temp (°F):	95.0
Leaving Fluid Temp (°F):	85.0
Wet Bulb (°F):	78.0

IBC Design Criteria

Seismic Design Force (g)	1g
Velocity Pressure (psf)	up to 60

CTI Certified Cooling Tower

Qty	Model	Capacity (Tons)	Percent Capacity
1	UT-112-712	460.80	102.4

All Weights, Dimensions and Technical Data are Shown per Unit

Fans:	1	Overall Length:	11' 11.750"
# Fan Motors @ HP:	(1) @ 30.00 (460/3/60)	Overall Width:	11' 10.000"
# Heaters @ kW:	(2) @ 6.00	Overall Height**:	16' 3.750"
Air Flow (CFM)	99,500		
Inlet Pressure Drop (psi):	2.8	Operating Weight (lbs)**:	15,090
Evaporated Water Rate (gpm):	10.80	Shipping Weight (lbs)**:	8,880
** Adjusted for options selected below.		Heaviest Section (lbs):	6,440

Options Selected

Fan Motor: Inverter Capable, Premium Efficient
EVAPAK Fill
IBC Compliant up to 1g
El. Heaters (0F / -18C ambient) (2) 6 kW
Vibration Switch
Equalizer Connection; Bottom; 12"; ASA
304 Stainless Steel Cold Water Basin
External Service Platform with Ladder
Safety Cage
Super Low Sound Fan

Sound Data (Sound Pressure Levels in dB(A))

	End	Mtr Side	Opp End	Opp Mtr Side	Top
S.P.L. dB(A) at 5'	77	78	77	78	72
S.P.L. dB(A) at 50'	60	61	60	61	60

Note 1: Sound Data shown is for 1 Cell operating at full speed

Note 2: The use of frequency inverters (Variable Frequency Drives) can increase sound levels.

Note 3: Sound option(s) selected: Super Low Sound Fan

Layout Criteria

Recommended Clearances Around Units (Feet)

From Unit Ends to Wall:	3.00	Between Unit Ends:	3.00
From Sides to Wall:	3.00	Between Unit Sides:	6.00

Refer to the Equipment Layout Manual or contact your Sales Representative for more details on layout criteria.

Shipping Data

Description		Domestic Skidded Dimensions (in)			Cubic Feet	Total Cubic Feet	Gross Wt (lbs)	Total Gross Wt (lbs)
Section		**Length**	**Width**	**Height**				
Basin	1	150	142	67	825	825	2,440	2,440
Casing	1	166	142	117	1,596	1,596	5,740	5,740
	2				2,421	2,421	8,180	8,180

Note: Above dimensions and weights are for a standard unit without option(s). Consult the factory for dimension/weight impact.

Cooling Tower Data Sheet

Chris Wilson
FLUID EQUIPMENT SOLUTIONS OF NEW ENGLAND, LLC

Project : Government Square Garage
Equipment Reference: EB1
Product Type : AT/UT/USS Cooling Tower

Date: 6/24/2013 Page: 1

	Selection Criteria
Capacity (Tons):	500.00
Capacity (MBH):	7,500.00
Fluid Type:	Water
Flow (GPM):	1500.0
Entering Fluid Temp (°F):	95.0
Leaving Fluid Temp (°F):	85.0
Wet Bulb (°F):	78.0

IBC Design Criteria

Seismic Design Force (g)	1g
Velocity Pressure (psf)	up to 60

CTI Certified Cooling Tower

Qty	Model	Capacity (Tons)	Percent Capacity
1	UT-112-614	501.00	100.2

All Weights, Dimensions and Technical Data are Shown per Unit

Fans:	1	Overall Length:	13' 11.750"
# Fan Motors @ HP:	(1) @ 30.00 (460/3/60)	Overall Width:	11' 10.000"
# Heaters @ kW:	(2) @ 7.00	Overall Height**:	16' 9.750"
Air Flow (CFM)	108,300		
Inlet Pressure Drop (psi):	2.1	Operating Weight (lbs)**:	16,960
Evaporated Water Rate (gpm):	12.00	Shipping Weight (lbs)**:	9,630
** Adjusted for options selected below.		Heaviest Section (lbs):	6,980

Options Selected

Fan Motor: Inverter Capable, Premium Efficient
EVAPAK Fill
IBC Compliant up to 1g
El. Heaters (0F / -18C ambient) (2) 7 kW
Vibration Switch
Equalizer Connection; Bottom; 12"; ASA
304 Stainless Steel Cold Water Basin
External Service Platform with Ladder
Safety Cage
Super Low Sound Fan

Sound Data (Sound Pressure Levels in dB(A))

	End	Mtr Side	Opp End	Opp Mtr Side	Top
S.P.L. dB(A) at 5'	78	78	78	78	72
S.P.L. dB(A) at 50'	60	61	60	61	61

Note 1: Sound Data shown is for 1 Cell operating at full speed

Note 2: The use of frequency inverters (Variable Frequency Drives) can increase sound levels.

Note 3: Sound option(s) selected: Super Low Sound Fan

Layout Criteria

Recommended Clearances Around Units (Feet)

From Unit Ends to Wall:	3.00	Between Unit Ends:	3.00
From Sides to Wall:	3.00	Between Unit Sides:	6.00

Refer to the Equipment Layout Manual or contact your Sales Representative for more details on layout criteria.

Shipping Data

Description		Domestic Skidded Dimensions (in)			Cubic Feet	Total Cubic Feet	Gross Wt (lbs)	Total Gross Wt (lbs)
Section		**Length**	**Width**	**Height**				
Basin	1	174	142	73	1,043	1,043	2,650	2,650
Casing	1	190	142	117	1,826	1,826	6,280	6,280
	2				2,869	2,869	8,930	8,930

Note: Above dimensions and weights are for a standard unit without option(s). Consult the factory for dimension/weight impact.

Cooling Tower Data Sheet

Chris Wilson
FLUID EQUIPMENT SOLUTIONS OF NEW ENGLAND, LLC

Project : Government Square Garage
Equipment Reference: WB1
Product Type : AT/UT/USS Cooling Tower

Date: 6/24/2013

Selection Criteria	
Capacity (Tons):	900.00
Capacity (MBH):	13,500.00
Fluid Type:	Water
Flow (GPM):	2700.0
Entering Fluid Temp (°F):	95.0
Leaving Fluid Temp (°F):	85.0
Wet Bulb (°F):	78.0

IBC Design Criteria	
Seismic Design Force (g)	1g
Velocity Pressure (psf)	up to 60

CTI Certified Cooling Tower

Qty	Model	Capacity (Tons)	Percent Capacity
1	UT-212-624	908.10	100.9

All Weights, Dimensions and Technical Data are Shown per Unit

Fans:	2	Overall Length:	24' 2.000"
# Fan Motors @ HP:	(2) @ 25.00 (460/3/60)	Overall Width:	11' 10.000"
# Heaters @ kW:	(4) @ 6.00	Overall Height**:	18' 3.750"
Air Flow (CFM)	184,800		
Inlet Pressure Drop (psi):	2.8	Operating Weight (lbs)**:	30,920
Evaporated Water Rate (gpm):	21.60	Shipping Weight (lbs)**:	18,500
** Adjusted for options selected below.		Heaviest Section (lbs):	6,830

Options Selected

(2) Fan Motor: Inverter Capable, Premium Efficient
EVAPAK Fill
IBC Compliant up to 1g
El. Heaters (0F / -18C ambient) (4) 6 kW
Vibration Switch
Equalizer Connection; Bottom; 12"; ASA
304 Stainless Steel Cold Water Basin
External Service Platform with Ladder
Safety Cage
Super Low Sound Fan

Sound Data (Sound Pressure Levels in dB(A))

	End	Mtr Side	Opp End	Opp Mtr Side	Top
S.P.L. dB(A) at 5'	78	80	78	80	74
S.P.L. dB(A) at 50'	61	64	61	64	63

Note 1: Sound Data shown is for 2 Cells operating at full speed

Note 2: The use of frequency inverters (Variable Frequency Drives) can increase sound levels.

Note 3: Sound option(s) selected: Super Low Sound Fan

Layout Criteria

Recommended Clearances Around Units (Feet)

From Unit Ends to Wall:	3.00	Between Unit Ends:	3.00
From Sides to Wall:	3.00	Between Unit Sides:	6.00

Refer to the Equipment Layout Manual or contact your Sales Representative for more details on layout criteria.

Shipping Data

Description		Domestic Skidded Dimensions (in)			Cubic Feet	Total Cubic Feet	Gross Wt (lbs)	Total Gross Wt (lbs)
Section		**Length**	**Width**	**Height**				
Basin	2	296	142	79	1,921	3,842	3,120	6,240
Casing	2	167	142	129	1,770	3,540	6,130	12,260
	4				3,691	7,382	9,250	18,500

Note: Above dimensions and weights are for a standard unit without option(s). Consult the factory for dimension/weight impact.

Cooling Tower Data Sheet

Chris Wilson
FLUID EQUIPMENT SOLUTIONS OF NEW ENGLAND, LLC

Project : Government Square Garage
Equipment Reference: WB2
Product Type : AT/UT/USS Cooling Tower

Date: 6/24/2013 Page: 1

Selection Criteria	
Capacity (Tons):	2,933.00
Capacity (MBH):	44,000.00
Fluid Type:	Water
Flow (GPM):	8800.0
Entering Fluid Temp (°F):	95.0
Leaving Fluid Temp (°F):	85.0
Wet Bulb (°F):	78.0

IBC Design Criteria	
Seismic Design Force (g)	1g
Velocity Pressure (psf)	up to 60

CTI Certified Cooling Tower

Qty	Model	Capacity (Tons)	Percent Capacity
1	UT-424-836	2,939.20	100.2

All Weights, Dimensions and Technical Data are Shown per Unit

Fans:	4	Overall Length:	36' 2.250"
# Fan Motors @ HP:	(4) @ 50.00 (460/3/60)	Overall Width:	24' 1.125"
# Heaters @ kW:	(4) @ 20.00	Overall Height**:	19' 9.750"
Air Flow (CFM)	598,800		
Inlet Pressure Drop (psi):	3.3	Operating Weight (lbs)**:	92,080
Evaporated Water Rate (gpm):	70.40	Shipping Weight (lbs)**:	54,800
** Adjusted for options selected below.		Heaviest Section (lbs):	9,960

Options Selected

(4) Fan Motor: Inverter Capable, Premium Efficient
Louver Access Door
EVAPAK Fill
IBC Compliant up to 1g
El. Heaters (0F / -18C ambient) (4) 20 kW
Vibration Switch
Equalizer Connection; Bottom; 12"; ASA
304 Stainless Steel Cold Water Basin
External Service Platform with Ladder
Safety Cage
Super Low Sound Fan

Sound Data (Sound Pressure Levels in dB(A))

	End	Mtr Side	Opp End	Opp Mtr Side	Top
S.P.L. dB(A) at 5'	81	81	81	81	76
S.P.L. dB(A) at 50'	66	67	66	67	68

Note 1: Sound Data shown is for 4 Cells operating at full speed

Note 2: The use of frequency inverters (Variable Frequency Drives) can increase sound levels.

Note 3: Sound option(s) selected: Super Low Sound Fan

Layout Criteria

Recommended Clearances Around Units (Feet)

From Unit Ends to Wall:	4.50	Between Unit Ends:	9.00
From Sides to Wall:	6.00	Between Unit Sides:	11.00

Refer to the Equipment Layout Manual or contact your Sales Representative for more details on layout criteria.

Shipping Data

Description		Domestic Skidded Dimensions (in)			Cubic Feet	Total Cubic Feet	Gross Wt (lbs)	Total Gross Wt (lbs)
Section		**Length**	**Width**	**Height**				
Basin	2	440	289	104	7,653	15,306	18,640	37,280
Casing	4	239	289	130	5,196	20,784	8,760	35,040
	6				12,849	36,090	27,400	72,320

Note: Above dimensions and weights are for a standard unit without option(s). Consult the factory for dimension/weight impact.

Emergency Generators

PACKAGE DATA [C18DE97]

APRIL 29, 2010

For Help Desk Phone Numbers Click here

Feature Code:	C18DE97	**Rating Type:**	STANDBY	**Sales model Package:**	PGS600
Engine Sales Model:	C18	**Engine Arrangement Number:**	2726915	**Hertz:**	60
EKW W/F:	600.0	**Noise Reduction:**	0 dBA	**Back Pressure:**	0.0 inH2O

Engine Package Information

Engine Package Data

Package Cooling Information

Data not available.

Package Sound Information

Open Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	105.3	106.0	98.5	96.5	102.4	100.0	99.6	93.5	87.0
450.0	75.0	104.8	104.3	96.7	96.1	102.3	99.3	98.7	92.2	89.2
300.0	50.0	104.0	102.4	94.8	96.0	102.3	98.6	97.4	90.6	89.3
150.0	25.0	103.6	101.4	94.1	96.3	102.2	98.2	96.4	89.6	87.3

Distance: 23.0 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	95.3	96.0	88.5	86.5	92.4	90.0	89.6	83.5	77.0
450.0	75.0	94.8	94.3	86.7	86.1	92.3	89.3	88.7	82.2	79.2
300.0	50.0	94.0	92.4	84.8	86.0	92.3	88.6	87.4	80.6	79.3
150.0	25.0	93.6	91.4	84.1	86.3	92.2	88.2	86.4	79.6	77.3

Distance: 49.2 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	89.3	90.0	82.5	80.5	86.4	84.0	83.6	77.5	71.0
450.0	75.0	88.8	88.3	80.7	80.1	86.3	83.3	82.7	76.2	73.2
300.0	50.0	88.0	86.4	78.8	80.0	86.3	82.6	81.4	74.6	73.3
150.0	25.0	87.6	85.4	78.1	80.3	86.2	82.2	80.4	73.6	71.3

SA Canopy Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	85.7	98.8	93.9	89.4	82.4	75.9	74.1	72.4	65.5
450.0	75.0	84.7	98.1	92.6	88.6	81.8	75.2	73.1	68.7	65.3
300.0	50.0	83.5	96.4	91.0	87.6	81.3	74.3	71.8	65.1	63.6
150.0	25.0	83.0	94.9	90.0	87.0	81.1	73.9	71.1	63.9	61.6

Distance: 23.0 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	76.6	91.1	85.1	81.4	72.1	65.8	63.4	60.9	54.5
450.0	75.0	75.6	90.3	83.4	80.3	71.7	65.3	62.7	58.3	54.8
300.0	50.0	74.4	8.5	81.5	78.9	71.5	64.5	61.7	55.5	53.5
150.0	25.0	73.8	87.0	80.7	78.3	71.5	64.1	61.1	54.5	51.5

Distance: 49.2 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	70.6	85.1	79.1	75.4	66.1	59.8	57.4	54.9	48.5
450.0	75.0	69.6	84.3	77.4	74.3	65.7	59.3	56.7	52.3	48.8
300.0	50.0	68.4	82.5	75.5	72.9	65.5	58.5	55.7	49.5	47.5
150.0	25.0	67.8	81.0	74.7	72.3	65.5	58.1	55.1	48.5	45.5

WP Canopy - Industrial Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	98.3	99.3	97.8	94.1	95.2	91.4	89.9	88.6	92.0
450.0	75.0	97.1	98.6	96.6	93.7	94.7	90.6	89.0	87.0	88.6
300.0	50.0	95.7	96.9	94.9	93.3	94.1	89.7	87.6	84.8	83.7
150.0	25.0	95.0	95.3	93.8	93.1	93.8	89.4	86.8	83.3	80.6

Distance: 23.0 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	86.5	91.5	90.6	85.6	81.2	80.3	78.0	76.7	79.5

450.0	75.0	85.4	90.8	89.3	85.2	81.0	79.4	77.1	75.3	76.1
300.0	50.0	84.3	89.3	87.7	84.6	80.8	78.7	76.0	73.5	71.4
150.0	25.0	83.8	88.0	86.8	84.3	80.7	78.5	75.5	72.4	68.8

Distance: 49.2 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	80.5	85.5	84.6	79.6	75.2	74.3	72.0	70.7	73.5
450.0	75.0	79.4	84.8	83.3	79.2	75.0	73.4	71.1	69.3	70.1
300.0	50.0	78.3	83.3	81.7	78.6	74.8	72.7	70.0	67.5	65.4
150.0	25.0	77.8	82.0	80.8	78.3	74.7	72.5	69.5	66.4	62.8

Open Exhaust Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
600.0	100.0	121.6	107.7	107.7	110.7	110.1	112.5	109.3	108.9	97.1
450.0	75.0	118.4	103.3	102.5	111.1	109.8	109.3	107.1	99.6	83.8
300.0	50.0	114.4	88.4	94.5	113.7	105.0	103.8	102.3	91.7	68.6
150.0	25.0	108.1	87.9	97.5	103.0	98.2	98.3	99.6	83.3	63.1

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PACKAGE DATA [C27DE37]

MARCH 22, 2010

For Help Desk Phone Numbers Click here

Feature Code:	C27DE37	**Rating Type:**	STANDBY	**Sales model Package:**	C27 SR4B
Engine Sales Model:	C27	**Engine Arrangement Number:**	2804140	**Hertz:**	60
EKW W/F:	800.0	**Noise Reduction:**	0 dBA	**Back Pressure:**	0.0 inH2O

Engine Package Information

Engine Package Data

Package Cooling Information

Open Cooling Data

% Load	Airflow Rate scfm			Ambient Capability Sea Level (Deg F)			Ambient Capability 300 m (Deg F)			Ambient Capability 600 m (Deg F)			Ambient Capability 900 m (Deg F)		
	0 inH2O	1/2 inH2O	3/4 inH2O	0 inH2O	1/2 inH2O	3/4 inH2O	0 inH2O	1/2 inH2O	3/4 inH2O	0 inH2O	1/2 inH2O	3/4 inH2O	0 inH2O	1/2 inH2O	3/4 inH
100.0	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	122	134	129

SA Canopy Cooling Data

% Load	Airflow Rate scfm	Ambient Capability Sea Level (Deg F)	Ambient Capability 300 m (Deg F)	Ambient Capability 600 m (Deg F)	Ambient Capability 900 m (Deg F)
100.0	33478	123	120	116	113

WP Canopy - Industrial Cooling Data

% Load	Airflow Rate scfm	Ambient Capability Sea Level (Deg F)	Ambient Capability 300 m (Deg F)	Ambient Capability 600 m (Deg F)	Ambient Capability 900 m (Deg F)
100.0	565	125	122	118	114

WP Canopy - Critical Cooling Data

% Load	Airflow Rate scfm	Ambient Capability Sea Level (Deg F)	Ambient Capability 300 m (Deg F)	Ambient Capability 600 m (Deg F)	Ambient Capability 900 m (Deg F)
100.0	34749	125	122	118	114

Package Sound Information

Open Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	108.0	98.3	107.1	102.5	102.5	104.0	100.8	96.5	97.3

600.0	75.0	107.6	97.2	106.9	101.9	102.4	104.0	100.5	95.3	92.8
400.0	50.0	107.3	96.5	106.6	101.6	102.2	104.0	100.3	94.4	89.9
200.0	25.0	107.2	96.2	106.1	101.7	102.2	104.0	100.2	94.1	88.3

Distance: 23.0 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	98.0	88.3	97.1	92.5	92.6	94.0	90.8	86.5	87.3
600.0	75.0	97.6	87.2	96.9	91.9	92.4	94.0	90.5	85.3	82.8
400.0	50.0	97.3	86.5	96.6	91.6	92.2	94.0	90.3	84.4	79.8
200.0	25.0	97.2	86.2	96.1	91.7	92.2	94.0	90.2	84.1	78.3

Distance: 49.2 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	92.0	82.3	91.1	86.5	86.6	88.0	84.8	80.5	81.3
600.0	75.0	91.6	81.2	90.9	85.9	86.4	88.0	84.5	79.3	76.8
400.0	50.0	91.3	80.5	90.6	85.6	86.2	88.0	84.3	78.4	73.8
200.0	25.0	91.2	80.2	90.1	85.7	86.2	88.0	84.2	78.1	72.3

SA Canopy Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	87.3	94.3	95.1	88.6	84.3	80.2	76.4	76.9	71.9
600.0	75.0	86.1	91.9	93.2	87.4	83.8	79.5	75.5	74.3	69.9
400.0	50.0	85.5	90.1	92.1	86.9	83.6	79.1	75.0	72.2	68.4
200.0	25.0	85.4	88.8	91.8	87.1	83.7	79.3	74.9	70.7	67.2

Distance: 23.0 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	76.3	88.8	86.3	77.0	74.2	67.9	63.1	63.9	57.6
600.0	75.0	75.7	86.9	86.3	76.3	73.5	67.7	61.8	61.1	56.4
400.0	50.0	75.2	85.2	85.9	76.1	73.3	67.6	60.9	58.7	54.6
200.0	25.0	75.1	83.6	85.3	76.2	73.4	67.5	60.6	56.8	52.2

Distance: 49.2 Feet

	OVERALL	OBCF	OBCF	OBCF	OBCF	OBCF	OBCF	OBCF	OBCF

EKW W/F	% LOAD	SOUND DB(A)	63HZ DB	125HZ DB	250HZ DB	500HZ DB	1000HZ DB	2000HZ DB	4000HZ DB	8000HZ DB
800.0	100.0	70.3	82.8	80.3	71.0	68.2	61.9	57.1	57.9	51.6
600.0	75.0	69.7	80.9	80.3	70.3	67.5	61.7	55.8	55.1	50.4
400.0	50.0	69.2	79.2	79.9	70.1	67.3	61.6	54.9	52.7	48.6
200.0	25.0	69.1	77.6	79.3	70.2	67.4	61.5	54.6	50.8	46.2

WP Canopy - Industrial Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	96.3	95.0	97.0	93.5	91.5	90.7	88.6	88.9	83.1
600.0	75.0	95.7	92.6	96.2	93.4	91.7	90.5	88.2	86.6	81.3
400.0	50.0	95.1	90.9	95.5	93.4	91.8	90.3	87.7	84.4	79.4
200.0	25.0	94.6	89.5	94.7	93.6	91.8	89.9	87.1	81.8	76.8

Distance: 23.0 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	85.6	89.9	90.9	82.5	80.0	78.7	78.0	78.6	72.8
600.0	75.0	85.7	86.9	91.3	84.5	81.7	79.5	78.0	76.1	71.2
400.0	50.0	85.4	84.9	91.0	85.3	82.3	79.7	77.7	73.7	69.1
200.0	25.0	84.5	84.0	89.6	84.6	81.7	79.0	77.1	71.1	65.9

Distance: 49.2 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	79.6	83.9	84.9	76.5	74.0	72.7	72.0	72.6	66.8
600.0	75.0	79.7	80.9	85.3	78.5	75.7	73.5	72.0	70.1	65.2
400.0	50.0	79.4	78.9	85.0	79.3	76.3	73.7	71.7	67.7	63.1
200.0	25.0	78.5	78.0	83.6	78.6	75.7	73.0	71.1	65.1	59.9

Open Exhaust Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	112.1	73.8	100.1	109.7	105.9	104.7	104.3	95.0	75.8

Open Mechanical Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	101.6	88.7	95.2	94.6	95.6	96.9	94.7	91.8	90.4

Distance: 23.0 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	91.4	80.2	86.8	85.6	85.7	87.0	84.7	80.5	78.5

Distance: 49.2 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
800.0	100.0	85.0	76.6	81.6	80.7	79.1	81.1	77.7	73.9	68.5

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PACKAGE DATA [C32DE06]

MAY 20, 2010

For Help Desk Phone Numbers Click here

Feature Code:	C32DE06	**Rating Type:**	STANDBY	**Sales model Package:**	C32 SR4B
Engine Sales Model:	C32	**Engine Arrangement Number:**	2537557	**Hertz:**	60
EKW W/F:	1000.0	**Noise Reduction:**	0 dBA	**Back Pressure:**	0.0 inH2O

Engine Package Information

Engine Package Data

Package Cooling Information

Data not available.

Package Sound Information

Open Exhaust Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
1000.0	100.0	117.0	101.3	120.9	122.7	112.0	108.4	107.1	97.0	82.3
750.0	75.0	114.3	99.4	118.4	120.0	108.6	106.1	104.1	93.5	78.3
500.0	50.0	108.5	97.1	111.1	113.5	104.6	101.2	98.3	88.4	69.9
250.0	25.0	108.3	97.3	113.4	115.3	102.7	95.6	94.7	82.0	59.3

Open Mechanical Sound Data

Distance: 3.3 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
1000.0	100.0	107.0	92.8	103.6	101.2	101.2	101.8	101.2	97.0	95.6
750.0	75.0	106.4	93.0	103.4	100.9	101.1	101.5	100.4	96.1	93.6
500.0	50.0	105.4	91.7	102.7	100.4	100.5	100.8	99.1	94.3	91.2
250.0	25.0	105.2	90.3	102.2	100.8	100.5	100.9	99.0	92.9	88.5

Distance: 23.0 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
1000.0	100.0	95.0	82.6	94.6	91.6	88.8	89.5	89.7	83.5	82.4
750.0	75.0	94.2	82.9	92.9	90.3	88.9	89.3	88.4	82.5	80.7
500.0	50.0	93.5	82.3	93.5	90.3	88.7	88.8	87.2	81.2	79.4

250.0	25.0	93.3	81.0	93.7	91.9	88.1	88.6	86.9	80.3	76.6

Distance: 49.2 Feet

EKW W/F	% LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
1000.0	100.0	88.1	77.9	90.5	87.7	82.0	82.9	81.6	76.7	74.6
750.0	75.0	87.8	78.1	89.9	87.3	82.4	82.3	81.0	75.7	72.7
500.0	50.0	87.2	77.0	89.4	87.1	82.0	82.3	80.2	74.3	70.7
250.0	25.0	86.9	75.9	89.0	87.9	81.2	82.1	79.9	73.2	68.6

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EXHAUST Sound Data: 4.92 FEET

GEN W/F EKW	PERCENT LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
1,500	100	117	107	122	118	110	108	109	109	107
1,350	90	116	106	121	117	109	107	108	108	106
1,200	80	115	105	120	116	108	106	107	107	105
1,125	75	114	104	119	115	107	106	107	107	105
1,050	70	114	104	119	115	107	105	106	106	104
900	60	112	103	117	113	105	104	105	105	103
750	50	111	101	116	112	104	103	104	104	102
600	40	110	100	115	111	103	101	103	103	101
450	30	108	99	113	109	101	100	101	101	99
375	25	108	98	113	109	101	99	100	100	98
300	20	107	97	112	108	100	98	99	99	97
150	10	104	95	109	105	97	96	97	97	95

EXHAUST Sound Data: 22.97 FEET

GEN W/F EKW	PERCENT LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
1,500	100	103	95	111	106	97	95	96	96	93
1,350	90	102	94	110	104	96	94	95	95	92
1,200	80	101	93	109	103	95	93	94	94	91
1,125	75	101	92	109	103	94	93	93	93	91
1,050	70	100	92	108	102	94	92	93	93	90
900	60	99	90	107	101	93	91	92	92	89
750	50	98	89	106	100	91	90	91	90	88
600	40	97	88	105	99	90	89	89	89	86
450	30	95	86	103	97	89	87	88	88	85
375	25	94	86	102	96	88	86	87	87	84
300	20	93	85	101	95	87	85	86	86	83
150	10	91	83	99	93	85	83	84	84	81

EXHAUST Sound Data: 49.21 FEET

GEN W/F EKW	PERCENT LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
1,500	100	97	88	105	99	90	89	89	89	86
1,350	90	96	87	104	98	89	88	88	88	85
1,200	80	95	86	103	97	88	87	87	87	84
1,125	75	94	85	102	96	88	86	87	87	84
1,050	70	94	85	102	96	87	86	86	86	83
900	60	92	84	100	95	86	84	85	85	82
750	50	91	83	99	93	85	83	84	84	81
600	40	90	81	98	92	83	82	83	82	80
450	30	88	80	96	91	82	80	81	81	78
375	25	88	79	96	90	81	80	80	80	77
300	20	87	78	95	89	80	79	79	79	76
150	10	84	76	92	87	78	76	77	77	74

MECHANICAL Sound Data: 3.28 FEET

GEN W/F EKW	PERCENT LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
1,500	100	115	118	127	118	109	102	101	98	102
1,350	90	115	118	127	118	109	102	101	98	102
1,200	80	115	118	127	118	109	102	101	98	102
1,125	75	115	118	127	118	109	102	101	98	102
1,050	70	115	118	127	118	109	102	101	98	102
900	60	115	118	127	118	109	102	101	98	102
750	50	115	118	127	118	109	102	101	98	102
600	40	115	118	127	118	109	102	101	98	102
450	30	115	118	127	118	109	102	101	98	102
375	25	115	118	127	118	109	102	101	98	102
300	20	115	118	127	118	109	102	101	98	102
150	10	115	118	127	118	109	102	101	98	102

MECHANICAL Sound Data: 22.97 FEET

GEN W/F EKW	PERCENT LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCJ 8000HZ DB
1,500	100	101	104	113	104	95	89	89	86	90
1,350	90	101	104	113	104	95	89	89	86	90
1,200	80	101	104	113	104	95	89	89	86	90
1,125	75	101	104	113	104	95	89	89	86	90
1,050	70	101	104	113	104	95	89	89	86	90
900	60	101	104	113	104	95	89	89	86	90
750	50	101	104	113	104	95	89	89	86	90
600	40	101	104	113	104	95	89	89	86	90
450	30	101	104	113	104	95	89	89	86	90
375	25	101	104	113	104	95	89	89	86	90
300	20	101	104	113	104	95	89	89	86	90
150	10	101	104	113	104	95	89	89	86	90

MECHANICAL Sound Data: 49.21 FEET

GEN W/F EKW	PERCENT LOAD	OVERALL SOUND DB(A)	OBCF 63HZ DB	OBCF 125HZ DB	OBCF 250HZ DB	OBCF 500HZ DB	OBCF 1000HZ DB	OBCF 2000HZ DB	OBCF 4000HZ DB	OBCF 8000HZ DB
1,500	100	95	98	107	98	89	83	83	81	84
1,350	90	95	98	107	98	89	83	83	81	84
1,200	80	95	98	107	98	89	83	83	81	84
1,125	75	95	98	107	98	89	83	83	81	84
1,050	70	95	98	107	98	89	83	83	81	84
900	60	95	98	107	98	89	83	83	81	84
750	50	95	98	107	98	89	83	83	81	84
600	40	95	98	107	98	89	83	83	81	84
450	30	95	98	107	98	89	83	83	81	84
375	25	95	98	107	98	89	83	83	81	84
300	20	95	98	107	98	89	83	83	81	84
150	10	95	98	107	98	89	83	83	81	84

Mechanical Equipment Sound Level Calculation

Resultant Noise Levels at Receptor Locations [dBA]

	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13
Description	Cooper St	Stillman St	Salem St	Hanover St	Millennium Bostonian	Bowdoin St	The West End Apartments	Proposed Forecaster Bldg	Proposed One Canal	Proposed Trinity	Proposed The Victor	Proposed The Merano	Temporary Home for Women and Children
Noise Monitoring Data [dBA]	**55**	**55**	**55**	**55**	**57**	**57**	**57**	**57**	**55**	**55**	**55**	**55**	**57**
Noise Source [dBA]	47	48	46	45	40	39	38	44	45	47	46	46	47
Calculated Noise Level [dBA]	**56**	**56**	**56**	**55**	**57**	**57**	**57**	**57**	**56**	**56**	**56**	**56**	**57**
Difference	1	1	1	0	0	0	0	0	0	1	1	1	0

Monitoring Data - Ambient Sound Levels (dBA)			
Location		MD1	MD2
Description		M1 - Friend Street	M2 - Stillman Street
Existing Sound Levels	L90	56.5	55.1

Receptor Descriptions

	REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13
Description	Cooper St	Stillman St	Salem St	Hanover St	Millennium Bostonian	Bowdoin St	The West End Apartments	Proposed Forecaster Bldg	Proposed One Canal	Proposed Trinity	Proposed The Victor	Proposed The Merano	Temporary Home for Women and Children
Nearest Reference [#]	2	2	2	2	1	1	1	1	2	2	2	2	1

Noise Source Descriptions

		NS1	NS2	NS3	NS4	NS5	NS6	NS7
	Noise Source Descriptions	West Building 1 (Residential)	West Building 2 (Office)	West Building 3 (Residential)	West Garage	East Building 1 (Hotel/Condo)	East Building 2 (Office)	East Building 3 (Retail)
Noise Sources								
Unit 1	Source Description	900 ton Cooling Tower	2800 ton Cooling Tower	500 ton Cooling Tower	Garage Exhaust	500 ton Cooling Tower	350 ton Cooling Tower	General Exhaust
	Noise Level [dBA]	64	68	61	59	61	61	64
	Reference distance [ft]	50	50	50	50	50	50	50
	# units [#]	1	1	1	2	1	1	1
	Required Attenuation [-dBA]							
		64	68	61	62	61	61	64
Unit 2	Source Description	General Exhaust	Garage Exhaust	Garage Exhaust		General Exhaust	General Exhaust	Retail/Kitchen Exhaust
	Noise Level [dBA]	64	59	59		64	64	59
	Reference distance [ft]	50	50	50		50	50	50
	# units [#]	1	1	1				
	Required Attenuation [-dBA]							
		64	59	59				
Unit 3	Source Description	Retail/Kitchen Exhaust	General Exhaust	General Exhaust		800 kW Emergency Generator	Retail/Kitchen Exhaust	
	Noise Level [dBA]	59	64	64		92	59	
	Reference distance [ft]	50	50	50		49	50	
	# units [#]	1	1	1		1	1	
	Required Attenuation [-dBA]					-30		
		59	64	64		62	59	
Unit 4	Source Description	1000 kW Emergency Generator	Retail/Kitchen Exhaust	Retail/Kitchen Exhaust			600 kW Emergency Generator	
	Noise Level [dBA]	95	59	59			89	
	Reference distance [ft]	49	50	50			49	
	# units [#]	1	1	1			1	
	Required Attenuation [-dBA]	-30					-30	
		65	59	59			59	
Unit 5	Source Description		1500 kW Emergency Generator	800 kW Emergency Generator				
	Noise Level [dBA]		99	92				
	Reference distance [ft]		49	49				
	# units [#]		1	1				
	Noise Source Level Attenuation [-dBA]		-30	-30				
			69	62				
	Total Noise Source Sound Level [dBA]	**69**	**73**	**68**	**62**	**65**	**65**	**64**
	Reference distance [ft]	**50**	**50**	**50**	**50**	**50**	**50**	**50**

Ground Type Between Receptors and Noise Sources

		REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13
		Cooper St	Stillman St	Salem St	Hanover St	Millennium Bostonian	Bowdoin St	The West End Apartments	Proposed Forecaster Bldg	Proposed One Canal	Proposed Trinity	Proposed The Victor	Proposed The Merano	Temporary Home for Women and Children
NS1	West Building 1 (Residential)	H	H	H	H	H	H	H	H	H	H	H	H	H
NS2	West Building 2 (Office)	H	H	H	H	H	H	H	H	H	H	H	H	H
NS3	West Building 3 (Residential)	H	H	H	H	H	H	H	H	H	H	H	H	H
NS4	West Garage	H	H	H	H	H	H	H	H	H	H	H	H	H
NS5	East Building 1 (Hotel/Condo)	H	H	H	H	H	H	H	H	H	H	H	H	H
NS6	East Building 2 (Office)	H	H	H	H	H	H	H	H	H	H	H	H	H
NS7	East Building 3 (Retail)	H	H	H	H	H	H	H	H	H	H	H	H	H

Distances from RECEPTOR TO NOISE SOURCE (in feet)

		REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13
		Cooper St	Stillman St	Salem St	Hanover St	Millennium Bostonian	Bowdoin St	The West End Apartments	Proposed Forecaster Bldg	Proposed One Canal	Proposed Trinity	Proposed The Victor	Proposed The Merano	Temporary Home for Women and Children
NS1	West Building 1 (Residential)	1,078	1,033	1,155	1,255	1,118	1,096	1,362	761	788	985	1,087	1,177	574
NS2	West Building 2 (Office)	1,009	1,013	1,198	1,339	1,288	1,144	1,275	648	727	857	959	1,056	563
NS3	West Building 3 (Residential)	816	737	858	976	915	1,270	1,519	715	573	853	919	991	552
NS4	West Garage	806	781	955	1,105	1,025	1,095	1,319	525	500	742	846	935	172
NS5	East Building 1 (Hotel/Condo)	620	615	835	992	1,062	1,290	1,409	491	325	586	669	747	500
NS6	East Building 2 (Office)	494	419	619	780	932	1,493	1,627	682	332	668	697	736	711
NS7	East Building 3 (Retail)	648	518	613	732	757	1,441	1,656	767	474	817	852	907	693

Receptor Level Attenuation

		REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13
		Cooper St	Stillman St	Salem St	Hanover St	Millennium Bostonian	Bowdoin St	The West End Apartments	Proposed Forecaster Bldg	Proposed One Canal	Proposed Trinity	Proposed The Victor	Proposed The Merano	Temporary Home for Women and Children
NS1	West Building 1 (Residential)	-5	-5	-5	-5	-10	-10	-10	-10	-10	-5	-5	-5	-10
NS2	West Building 2 (Office)	-5	-5	-5	-5	-10	-10	-10	-10	-10	-5	-5	-5	-10
NS3	West Building 3 (Residential)	-5	-5	-5	-5	-10	-10	-10	-10	-10	-5	-5	-5	-10
NS4	West Garage	-5	-5	-5	-5	-10	-10	-10	-10	-10	-5	-5	-5	-10
NS5	East Building 1 (Hotel/Condo)	-5	-5	-5	-5	-10	-10	-10	-10	-10	-5	-5	-5	-10
NS6	East Building 2 (Office)	-5	-5	-5	-5	-10	-10	-10	-10	-10	-5	-5	-5	-10
NS7	East Building 3 (Retail)	-5	-5	-5	-5	-10	-10	-10	-10	-10	-5	-5	-5	-10

Noise Propogation Calculator

		REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13
		Cooper St	Stillman St	Salem St	Hanover St	Millennium Bostonian	Bowdoin St	The West End Apartments	Proposed Forecaster Bldg	Proposed One Canal	Proposed Trinity	Proposed The Victor	Proposed The Merano	Temporary Home for Women and Children
NS1	West Building 1 (Residential)	38	38	37	36	32	33	31	36	35	38	38	37	38
NS2	West Building 2 (Office)	42	42	40	39	34	35	35	40	39	43	42	41	42
NS3	West Building 3 (Residential)	39	40	39	38	33	30	29	35	37	39	38	37	38
NS4	West Garage	33	33	31	30	26	25	24	32	32	34	32	32	41
NS5	East Building 1 (Hotel/Condo)	38	38	35	34	28	26	26	35	38	38	37	36	34
NS6	East Building 2 (Office)	40	41	38	36	29	25	24	32	38	37	37	36	32
NS7	East Building 3 (Retail)	37	39	37	36	30	25	24	30	34	35	34	34	31
	TOTAL	**47**	**48**	**46**	**45**	**40**	**39**	**38**	**44**	**45**	**47**	**46**	**46**	**47**

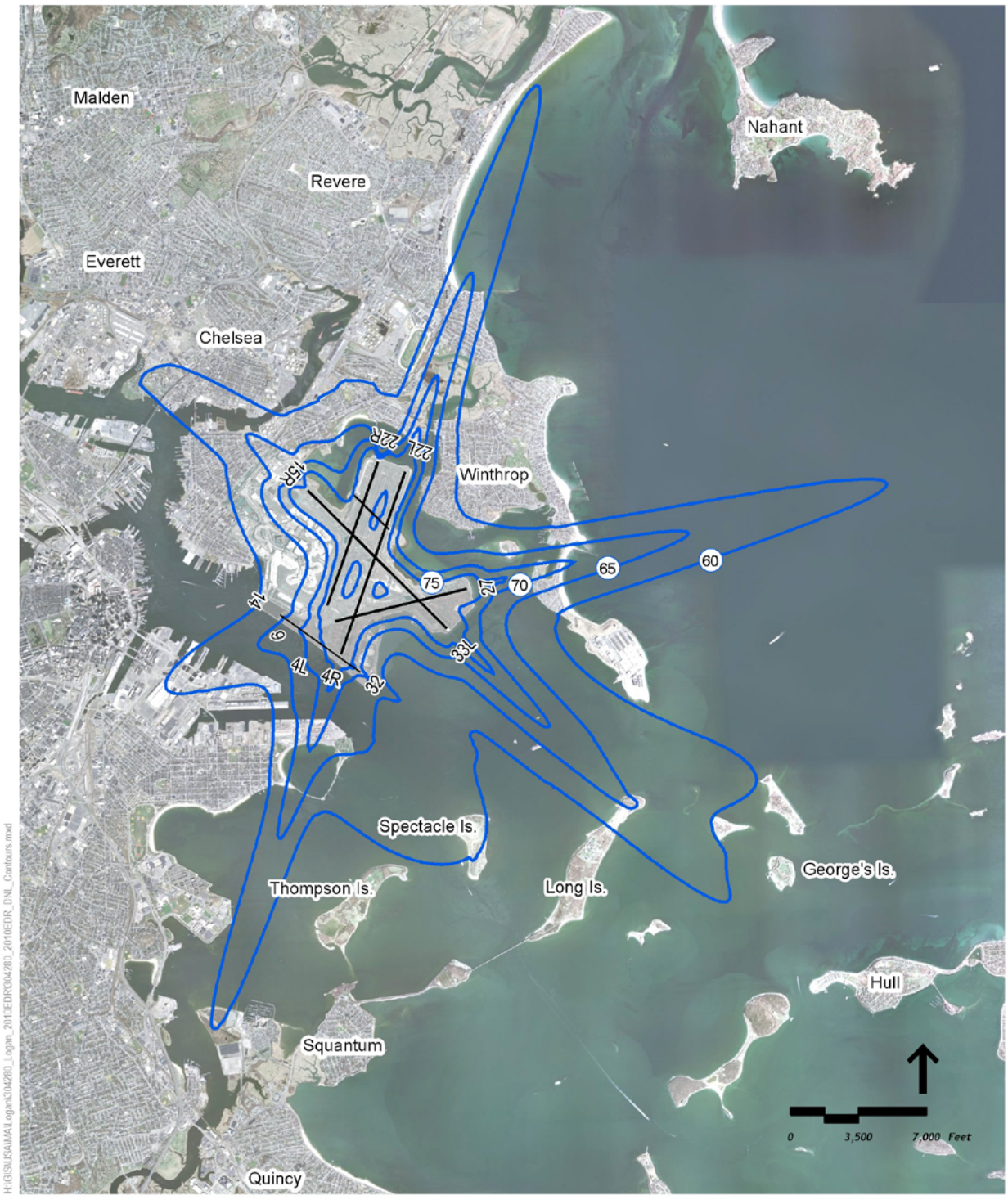
HVAC Types

	Noise Level (dBA)	Ref Distance (ft)
Carrier 50PG CENTURION 3 - 2 ton	75	5
Carrier 50TFQ WEATHERMAKER 4 - 3 ton	84	5
Carrier 50PG CENTURION 5 - 4 ton	72	5
Carrier 50TFF WEATHERMAKER 5 - 4 ton	81	5
Carrier 50PG CENTURION 6 - 5 ton	78	5
Carrier 50TFQ WEATHERMAKER 6 - 5 ton	82	5
Carrier 50PG CENTURION 7 - 6 ton	78	5
Carrier 50TFQ WEATHERMAKER 7 - 6 ton	82	5
Carrier 50PG CENTURION 8 - 7.5 ton	80	5
Carrier 50TFF WEATHERMAKER 8 - 7.5 ton	87	5
Carrier 50PG CENTURION 9 - 8.5 ton	80	5
Carrier 50TFF WEATHERMAKER 9 - 8.5 ton	87	5
Carrier 50HJQ 9 - 8.5 ton	110	5
Carrier 50PG CENTURION 12 - 10 ton	80	5
Carrier 50TFF WEATHERMAKER 12 - 10 ton	88	5
Carrier 50HJ WEATHERMASTER 15 - 12 ton	88	5
Carrier 50PG CENTURION 14 - 12.5 ton	83	5
Carrier 50TFF WEATHERMAKER 14 - 12.5 ton	87	5
Carrier 48HG CENTURION 16 - 15 ton	81.7	5
Carrier 50TJ WEATHERMAKER 16 - 15 ton	88	5
Carrier 48HG CENTURION 20 - 17.5 ton	81.7	5
Carrier 48PG CENTURION 20 - 18 ton	81.7	5
Carrier 50TJ WEATHERMAKER 20 - 18 ton	88	5
Carrier 48PG CENTURION 24 - 20 ton	84.6	5
Carrier 50TJ WEATHERMAKER 24 - 20 ton	94	5
Carrier 48HG CENTURION 28 - 25 ton	84.6	5
Carrier 50TJ WEATHERMAKER 28 - 25 ton	94	5
McQuay Vision 50,000 cfm outdoor air unit	92	5
McQuay Vision 30,000 cfm outdoor air unit	88	5

<--Select this row

	1000 kW Gen		1500 kW Gen	
	feet	dBA	feet	dBA
Exhaust	3.3	117		
	49.2	93.5	49.2	97.0
Mechanical	49.2	88.1	49.2	95.0
Total	49.2	94.6	49.2	99.1

Logan International Airport
DNL Contour



Source: Massport NOMS / ERA Multi-Lat, MassGIS, USDA NAIP 2010

60-75 DNL Contours for 2010 Operations Using INM 7.0b

Figure 6-13

Appendix E
Construction Supporting Documentation

- E.1 – Construction Logistics Plans
- E.2 – Proposed Construction Truck Routes

E.1: Construction Logistics Plans

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One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 1 Construction of WP-B1

General Description of Work/Approach: **Approx. Duration: 42 - 48 Months**

This phase includes constructing Residential Tower No. 1 and minor demolition at the SW corner of the existing garage for the new work. Removal of select area of existing precast concrete in the southwest quadrant of the garage to allow for tower core to pass through existing garage. Demo will be completed with hydraulic processing equipment. The precast concrete tee sections will be removed in one piece at a time from the top to the bottom. The cast in place garage will be processed with hydraulic excavators. New building will be erected with a single tower crane. Assist cranes will be required at periodic times.

Construction Impacts	Mitigation Strategy
General	
Air Quality/Dust Control	Subcontractors will be required to adhere to all applicable regulations regarding control of dust and emissions. Any dust generated from demolition, earthwork and other construction activities will be controlled by spraying with water.
Noise	Equipment will be OSHA noise compliant. Selective sheltering and temporary baffling will be provided as required.
Work Hours	Typically 6:30 to 4:30 Monday through Friday. Off hours and 2nd shift work will likely be required for removal of section of the existing garage. Selective OT and Weekends will be limited for other activities, but may be required.
Hazardous Materials & Solid Waste	Scope of the phase includes selective demolition of the existing garage. We do not anticipate any hazardous materials will be encountered during demolition.
Odor and Rodent Control	A formal Certified Pest Control Plan will be implemented in accordance with the City of Boston's requirements. Other than potential emissions from construction equipment, we do not anticipate any other odor issues during construction.

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One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 1 Construction of WP-B1

Site Logistics

Site Preparation, Construction Staging and Maintenance	The construction area work zone will be confined by jersey barriers and fencing. Construction site access will be from New Sudbury Street. Vehicles will enter from the west and exit heading east. Site fenced area will include the existing police parking area and adjacent travel lane on New Sudbury. Truck track mat will be utilized during below grade construction. Crane picks will be made from New Sudbury Street within the fenced in area.
Erosion Control/Storm Water Management	An erosion and sediment control plan will be developed and maintained in accordance with local, state and federal requirements.

Traffic Impacts

Truck Traffic Management	**Arrivals** – From the South and West, vehicles will travel on I-93 North and take Exit 23 – Aquarium (toward Quincy Market). Merge onto North St and take a right onto Congress St. Pass under Government Center Garage and take a left onto New Chardon. Then left onto Cambridge Street and finally a left onto New Sudbury Street. From the North, Take I-93 Exit 24A Government Center, slight right on Clinton Street, left onto North Street, right onto Congress St and a left onto New Chardon. Then Left onto Cambridge Street and finally a Left onto New Sudbury Street. **Departures** – To go north, continue on New Sudbury Street and take left onto I-93 North ramp. To go south, take a left onto Congress and a take a right onto New Chardon Street and take I-93 South ramp.
Surrounding Streets	Site access will be located on New Sudbury. A detailed CMP and Traffic Control Plan will be developed. It is anticipated that the existing police parking lane and one travel lane on New Sudbury will be utilized for vehicle and site access. No other impacts to surrounding streets are anticipated in this phase, but may be required for some off peak deliveries.

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One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 1 Construction of WP-B1

Public Safety during Construction

Pedestrian Routes	The sidewalk along the north side of New Sudbury will be closed. Pedestrians will be re-routed the south side of New Sudbury at the intersection of Congress Street and at the Police Station.
Temporary Protection	Temporary protection will be afforded by side walk and access walkway overhead protection and routes will be secured by barriers.

MBTA Access Changes/Impacts

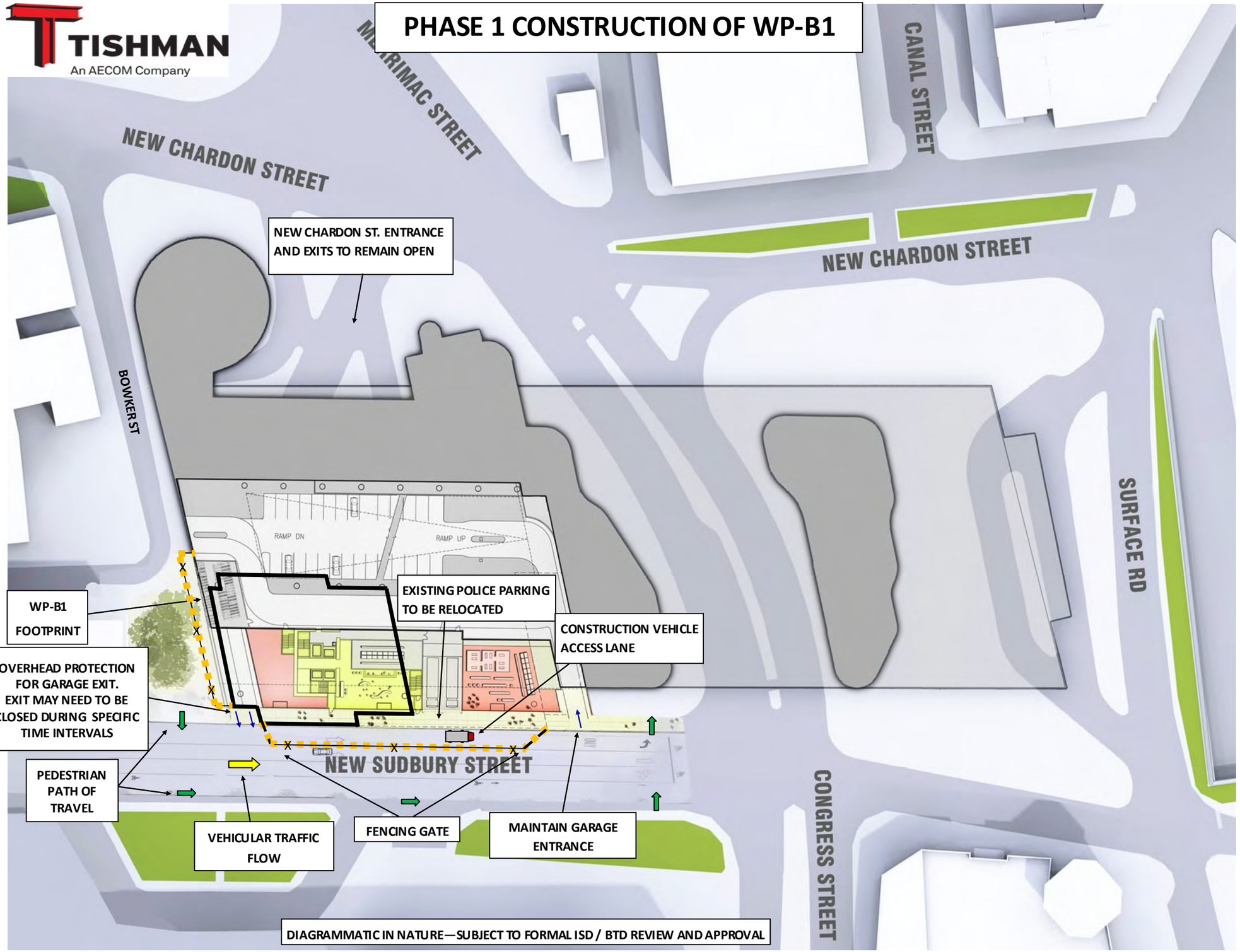
Green Line	No Impacts during this Phase.
Orange Line	No Impacts during this Phase.
Bus Stop	No Impacts during this Phase.

One Congress Street Garage

Garage Access	Overhead shield/temporary protection at the New Sudbury Garage exit will be provided. No other access/egress impacts are anticipated during this phase.

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PHASE 1 CONSTRUCTION OF WP-B1



DIAGRAMMATIC IN NATURE—SUBJECT TO FORMAL ISD / BTD REVIEW AND APPROVAL

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One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 2A Demolition of Existing Garage (East Parcel)

General Description of Work/Approach: **Approx. Duration: 8 to 10 Months**

This phase includes demolition of the existing parking garage spanning Congress and the section located on the East Parcel. The project team intends to utilize a "top-down" and "east-to-west" demolition approach. Construction will be sequenced and phased to always maintain one vehicular corridor and one pedestrian corridor to pass thru Congress St/Surface Rd during demolition of the existing garage.

Construction Impacts	Mitigation Strategy
General	
Air Quality/Dust Control	Subcontractors will be required to adhere to all applicable regulations regarding control of dust and emissions. Any dust generated from demolition, earthwork and other construction activities will be controlled by spraying with water.
Noise	Equipment will be OSHA noise compliant. Selective sheltering and temporary baffling will be provided as required.
Work Hours	Typically 6:30 to 4:30 Monday through Friday. Selective OT and Weekends will be limited, but may be required. Weekend work may be required during demolition of Canopy over-hanging Haymarket Station and other critical work at the East-end location.
Hazardous Materials & Solid Waste	Scope of the phase includes demolition and removal of the eastern portion of the existing garage. We do not anticipate any hazardous materials will be encountered during demolition.
Odor and Rodent Control	A formal Certified Pest Control Plan will be implemented in accordance with the City of Boston's requirements. Other than potential emissions from construction equipment, we do not anticipate any other odor issues during construction.
Site Logistics	
Site Preparation, Construction Staging and Maintenance	The construction area work zone will be confined by jersey barriers and fencing. Construction site access will be through New Sudbury street, New Chardon and Haymarket Square. Truck track

	mat will be utilized during below grade construction. Crane picks will be made from New Sudbury Street, New Chardon & Haymarket Square within the fenced in area.
Erosion Control/Storm Water Management	An erosion and sediment control plan will be developed and maintained in accordance with local, state and federal requirements.

Traffic Impacts

Truck Traffic Management	**Arrivals** – From the South and West, vehicles will travel on I-93 North and take Exit 23 – Aquarium (toward Quincy Market). Merge onto North St and take a Right onto Congress St. Pass under Government Center Garage and take a Left onto New Chardon. Then Left onto Cambridge Street and finally a Left onto New Sudbury Street. From the North, Take I-93 Exit 24A Government Center, slight right on Clinton Street, left onto North Street, right onto Congress St and a left onto New Chardon. Then Left onto Cambridge Street and finally a Left onto New Sudbury Street. **Departures** – To go north, continue on New Sudbury Street and take left onto I-93 North ramp. To go south, take a left onto Congress and a take a right onto New Chardon Street and take I-93 South ramp.
Surrounding Streets	Construction will be sequenced and phased to always maintain one vehicular corridor and one pedestrian corridor to pass thru Congress St/Surface Rd during demolition of the existing garage. Merrimac St. / Congress St. will be closed at certain times during demolition and traffic re-routed around. Site access will be located on New Sudbury. A detailed CMP and Traffic Control Plan will be developed. Sidewalks will be acquired for site laydown area as required and allowed by MBTA/Haymarket Station. Existing Haymarket Bus Station (Route 111 Bus & 400 Series) will be relocated in coordination with the MBTA. No other impacts to surrounding streets are anticipated in this phase, but may be required for some off peak deliveries.

Public Safety during Construction

Pedestrian Routes	Sidewalks along south-side of New Chardon & north-side of New Sudbury will be closed (between Congress St & Surface Road to the extent allowable by MBTA). Pedestrian routes will be

	established on the north-side of New Chardon & south-side of New Sudbury.
Temporary Protection	Temporary protection will be afforded by side walk and access walkway overhead protection and routes will be secured by barriers.

MBTA Access Changes/Impacts

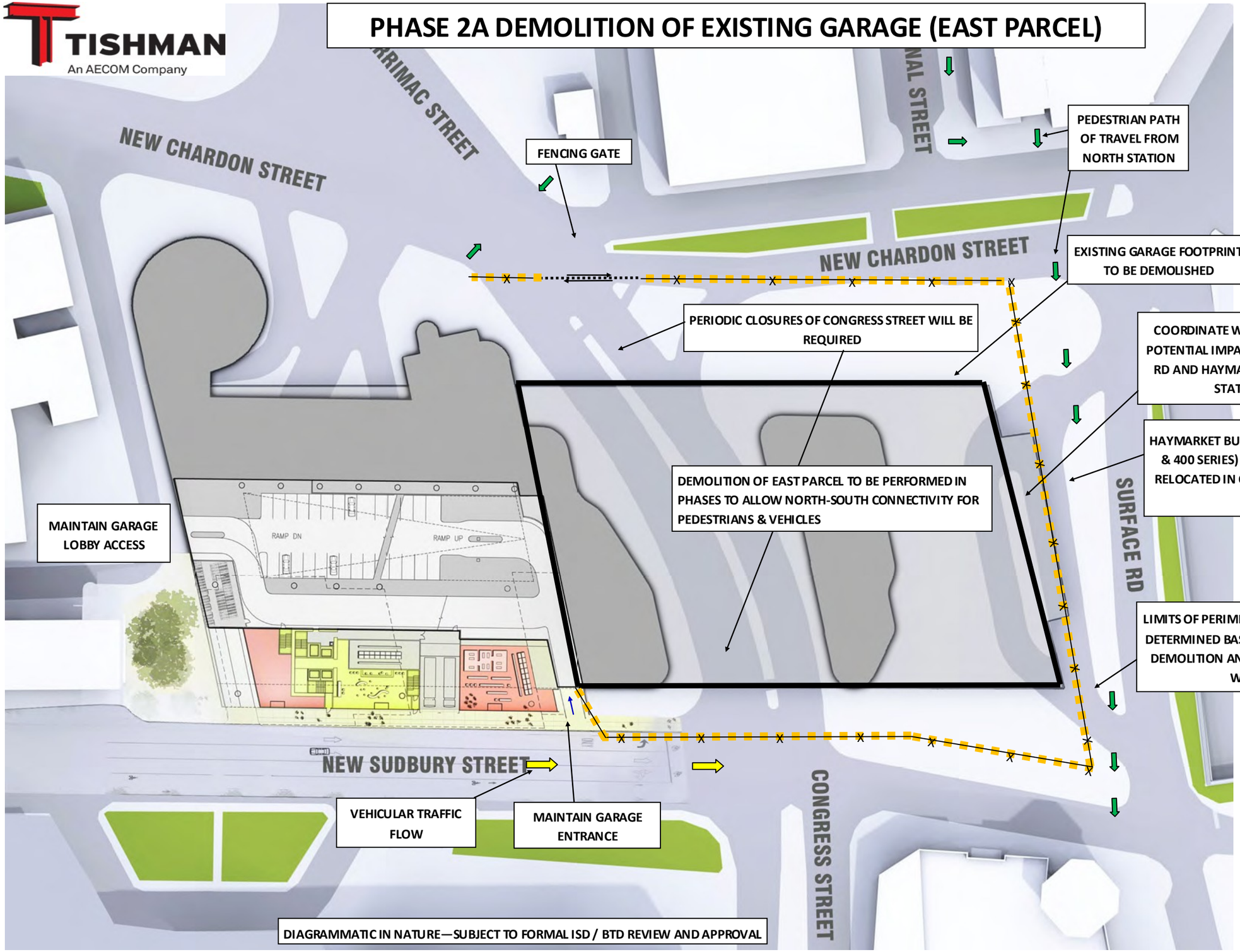
Green Line	Headhouse to Green subway lines will be closed at times. Alternate access will be via headhouse on Parcel 7 garage. Construction activity will be scheduled in accordance with TRA license-agreement and MBTA rules & regulations per right-of-way statute.
Orange Line	Headhouse to Orange subway lines will be closed at times. Alternate access will be via headhouse on Parcel 7 garage. Construction activity will be scheduled in accordance with TRA license-agreement and MBTA rules & regulations per right-of-way statute.
Bus Stop	Construction activity will be scheduled to minimize impact to regular bus stop operations. Existing Haymarket bus stop (Route 111 & 400 Series) will be temporarily relocated in coordination with the MBTA.

One Congress Street Garage

Garage Access	All entrances on West Parcel will be fully functional.

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PHASE 2A DEMOLITION OF EXISTING GARAGE (EAST PARCEL)



DIAGRAMMATIC IN NATURE—SUBJECT TO FORMAL ISD / BTD REVIEW AND APPROVAL

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One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 2B Construction of WP-B2

General Description of Work/Approach: **Approx. Duration: 48 – 54 Months**

This phase includes constructing Office Tower WP-B2 and removal of existing parking garage helix on NW corner of garage and other minor garage modifications. Demo will be completed with hydraulic processing equipment. New building will be erected with a single tower crane. Assist cranes be required at periodic times.

Construction Impacts	Mitigation Strategy
General	
Air Quality/Dust Control	Subcontractors will be required to adhere to all applicable regulations regarding control of dust and emissions. Any dust generated from demolition, earthwork and other construction activities will be controlled by spraying with water.
Noise	Equipment will be OSHA noise compliant. Selective sheltering and temporary baffling will be provided as required.
Work Hours	Typically 6:30 to 4:30 Monday through Friday. Off hours and 2nd shift work will likely be required for removal of section of the existing garage and helix. Selective OT and Weekends will be limited for other activities, but may be required.
Hazardous Materials & Solid Waste	Scope of the phase includes demolition of the existing garage helix. We do not anticipate any hazardous materials will be encountered during demolition.
Odor and Rodent Control	A formal Certified Pest Control Plan will be implemented in accordance with the City of Boston's requirements. Other than potential emissions from construction equipment, we do not anticipate any other odor issues during construction.

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One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 2B Construction of WP-B2

Site Logistics

Site Preparation, Construction Staging and Maintenance	The construction area work zone will be confined by jersey barriers and fencing. Construction site access will be through New Chardon street. Vehicles will enter from the west and exit heading east. Site fenced area will include both east-bound travel lanes on New Chardon. Truck track mat will be utilized during below grade construction. Crane picks will be made from New Chardon Street within the fenced in area.
Erosion Control/Storm Water Management	An erosion and sediment control plan will be developed and maintained in accordance with local, state and federal requirements.

Traffic Impacts

Truck Traffic Management	**Arrivals** – From the South and West, vehicles will travel on I-93 North and take Exit 23 – Aquarium (toward Quincy Market). Merge onto North St and take a left onto Congress St, right on State Street, continue onto Court Street, right on Cambridge Street, take a right onto New Chardon Street. From the North, Take I-93 Exit 24A Government Center, slight right on Clinton Street, left onto North Street and take a left onto Congress St, right on State Street, continue onto Court Street, right on Cambridge Street, take a right onto New Chardon Street. **Departures** – To go north, take a right onto Congress, left onto New Sudbury Street, left onto I-93N ramp. To go south, continue on New Chardon and take a right onto I-93S ramp.
Surrounding Streets	Site access will be located on New Chardon. A detailed CMP and Traffic Control Plan will be developed. It is anticipated both east-bound travel lanes on New Chardon will be utilized for vehicle and site access. No other impacts to surrounding streets are anticipated in this phase, but may be required for some off peak deliveries.

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One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 2B Construction of WP-B2

Public Safety during Construction

Pedestrian Routes	The sidewalk along the south-side of New Chardon St. and east-side of Bowker St will be closed. A new crosswalk/pedestrian signal/handicap ramps at Bowker/New Chardon will be established. Pedestrians will be re-routed the west-side of Bowker St, utilize new crosswalk and then continue on the north-side of New Chardon.
Temporary Protection	Temporary protection will be afforded by side walk and access walkway overhead protection and routes will be secured by barriers.

MBTA Access Changes/Impacts

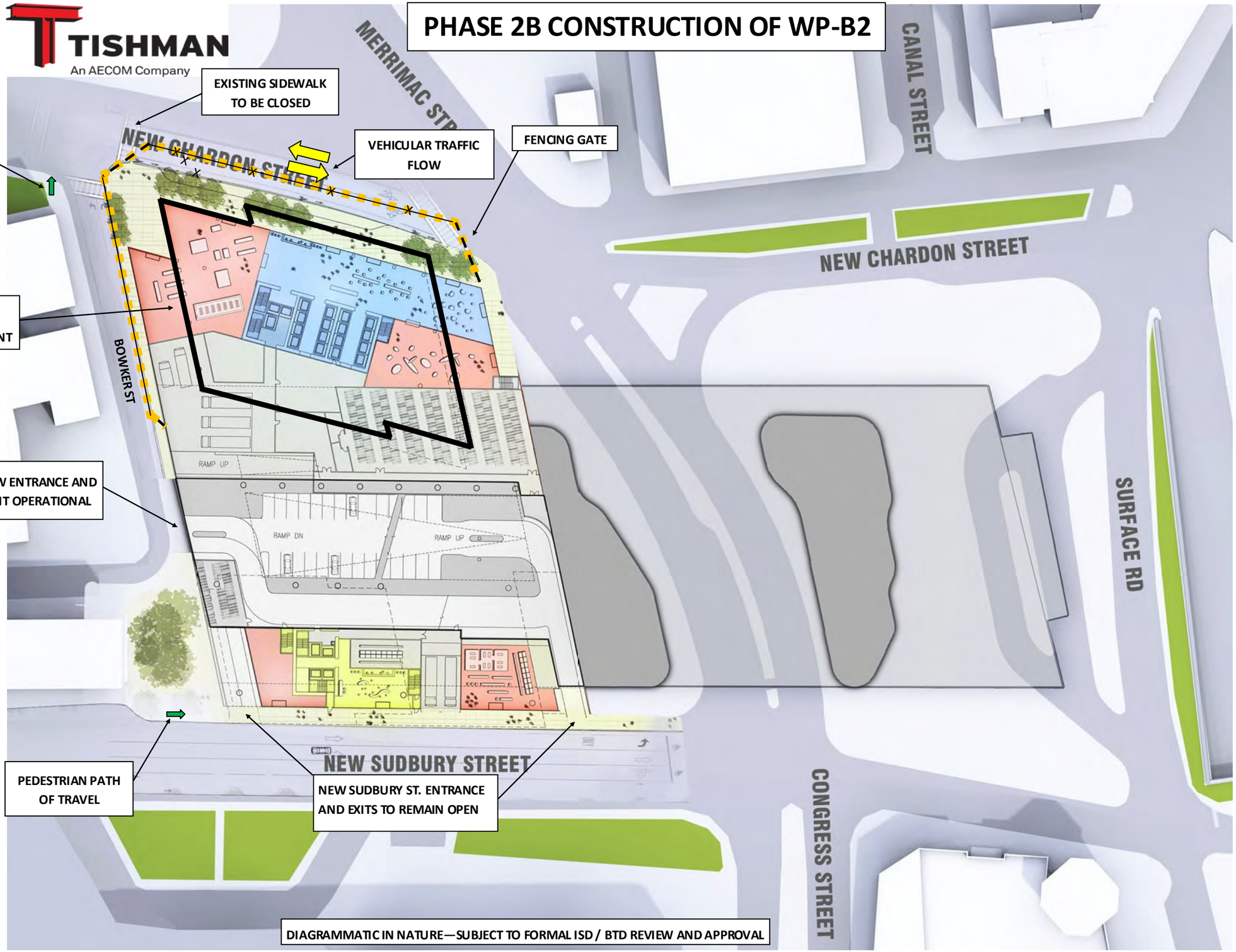
Green Line	No Impacts during this Phase.
Orange Line	No Impacts during this Phase.
Bus Stop	No Impacts during this Phase.

One Congress Street Garage

Garage Access	New Chardon garage entrance will be closed during this phase however the new Bowker Street entrance/exit will be operational at this time.

PHASE 2B CONSTRUCTION OF WP-B2

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DIAGRAMMATIC IN NATURE—SUBJECT TO FORMAL ISD / BTD REVIEW AND APPROVAL

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One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 3A Construction of EP-B1, EP-B2 & EP-B3

General Description of Work/Approach: **Approx. Duration: 42 – 48 Months**

This phase includes constructing of all the East Parcel buildings, including EP-B1, EP-B2 and EP-B3.

Construction Impacts	Mitigation Strategy
General	
Air Quality/Dust Control	Subcontractors will be required to adhere to all applicable regulations regarding control of dust and emissions. Any dust generated from earthwork and other construction activities will be controlled by spraying with water.
Noise	Equipment will be OSHA noise compliant. Selective sheltering and temporary baffling will be provided as required.
Work Hours	Typically 6:30 to 4:30 Monday through Friday. Selective OT and Weekends will be limited, but may be required.
Hazardous Materials & Solid Waste	We do not anticipate any hazardous materials will be encountered during this phase.
Odor and Rodent Control	A formal Certified Pest Control Plan will be implemented in accordance with the City of Boston's requirements. Other than potential emissions from construction equipment, we do not anticipate any other odor issues during construction.

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One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 3A Construction of EP-B1, EP-B2 & EP-B3

Site Logistics

Site Preparation, Construction Staging and Maintenance	The construction area work zone will be confined by jersey barriers and fencing. Construction site access will be through New Sudbury street. Vehicles will enter from the west and exit heading east. Site fenced area will include fencing on all four sides of construction zone including fencing along New Chardon St, Congress St, New Sudbury St & Surface Rd side. Truck track mat will be utilized during below grade construction. Crane picks will be made from New Sudbury Street within the fenced in area.
Erosion Control/Storm Water Management	An erosion and sediment control plan will be developed and maintained in accordance with local, state and federal requirements.

Traffic Impacts

Truck Traffic Management	**Arrivals** – From the South and West, vehicles will travel on I-93 North and take Exit 23 – Aquarium (toward Quincy Market). Merge onto North St and take a Right onto Congress St. Pass under Government Center Garage and take a Left onto New Chardon. Then Left onto Cambridge Street and finally a Left onto New Sudbury Street. From the North, Take I-93 Exit 24A Government Center, slight right on Clinton Street, left onto North Street, right onto Congress St and a left onto New Chardon. Then Left onto Cambridge Street and finally a Left onto New Sudbury Street. **Departures** – To go north, continue on New Sudbury Street and take left onto I-93 North ramp. To go south, take a left onto Congress and a take a right onto New Chardon Street and take I-93 South ramp.
Surrounding Streets	Site access will be located on New Sudbury. A detailed CMP and Traffic Control Plan will be developed. It is anticipated that one travel lane on New Sudbury will be utilized for vehicle and site access. No other impacts to surrounding streets are anticipated in this phase, but may be required for some off peak deliveries.

Public Safety during Construction

TISHMAN
An AECOM Company

One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 3A Construction of EP-B1, EP-B2 & EP-B3

Pedestrian Routes	The sidewalk along the north side of New Sudbury will be closed. Pedestrians will be re-routed the south side of New Sudbury at the intersection of Congress Street and at the Police Station.
Temporary Protection	Temporary protection will be afforded by side walk and access walkway overhead protection and routes will be secured by barriers.

MBTA Access Changes/Impacts

Green Line	Headhouse to Green subway lines will be closed at times. Alternate access will be via headhouse on Parcel 7 garage. Construction activity will be scheduled in accordance with TRA license-agreement and MBTA rules & regulations per right-of-way statute.
Orange Line	Headhouse to Orange subway lines will be closed at times. Alternate access will be via headhouse on Parcel 7 garage. Construction activity will be scheduled in accordance with TRA license-agreement and MBTA rules & regulations per right-of-way statute.
Bus Stop	Construction activity will be scheduled to minimize impact to regular bus stop operations. Existing Haymarket bus stop (Route 111 & 400 Series) will be temporarily relocated in coordination with the MBTA.

One Congress Street Garage

Garage Access	All entrances on West Parcel will be fully functional.

General Description of Work/Approach:

Approx. Duration: 24 – 30 Months

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PHASE 3A CONSTRUCTION OF EP-B1, EP-B2 & EP-B3

EAST PARCEL CONSTRUCTION TO BE COMPLETED IN PHASES TO PROVIDE PEDESTRIAN CONNECTION FROM GOVERNMENT CENTER/ FINANCIAL DISTRICT TO NORTH STATION AND TO MAINTAIN MBTA HAYMARKET BUSES

EP-B1 FOOTPRINT

EP-B2 FOOTPRINT

PEDESTRIAN PATH OF TRAVEL

COORDINATE WITH MBTA FOR POTENTIAL IMPACTS TO SURFACE RD AND HAYMARKET SUBWAY STATION

HAYMARKET BUS STATION (ROUTE 111 & 400 SERIES) TO BE TEMPORARILY RELOCATED IN COORDINATION WITH MBTA

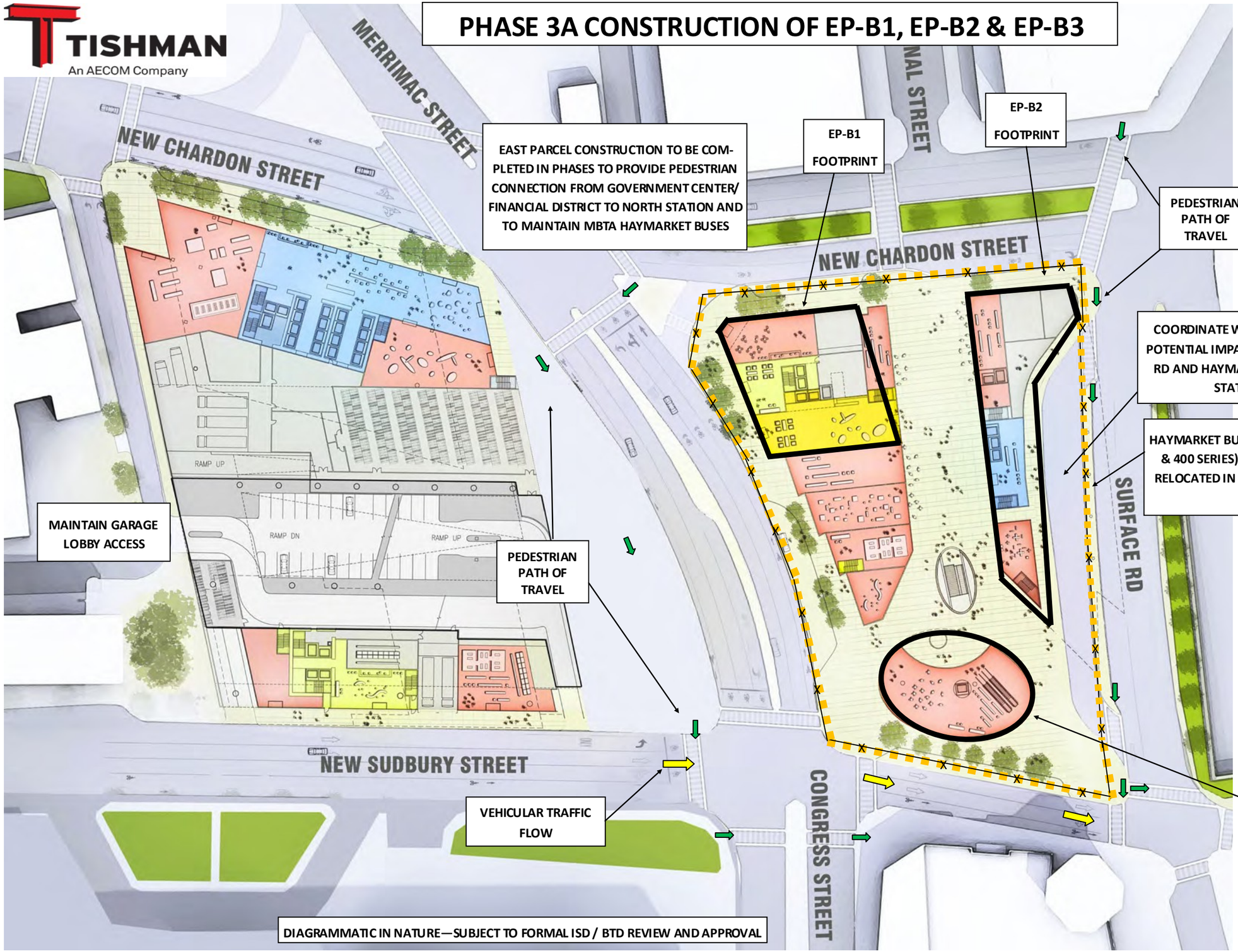
MAINTAIN GARAGE LOBBY ACCESS

PEDESTRIAN PATH OF TRAVEL

VEHICULAR TRAFFIC FLOW

EP-B3 FOOTPRINT

DIAGRAMMATIC IN NATURE—SUBJECT TO FORMAL ISD / BTD REVIEW AND APPROVAL



TISHMAN
An AECOM Company

One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 3B Construction of WP-B3

This phase includes constructing Residential Tower No. 2 (WP-B3) located on the West Parcel. New building will be erected with a single tower crane. Assist cranes be required at periodic times.

Construction Impacts	Mitigation Strategy
General	
Air Quality/Dust Control	Subcontractors will be required to adhere to all applicable regulations regarding control of dust and emissions. Any dust generated from demolition, earthwork and other construction activities will be controlled by spraying with water.
Noise	Equipment will be OSHA noise compliant. Selective sheltering and temporary baffling will be provided as required.
Work Hours	Typically 6:30 to 4:30 Monday through Friday. Selective OT and Weekends will be limited, but may be required.
Hazardous Materials & Solid Waste	Scope of the phase includes selective demolition of the existing garage. We do not anticipate any hazardous materials will be encountered during demolition.
Odor and Rodent Control	A formal Certified Pest Control Plan will be implemented in accordance with the City of Boston's requirements. Other than potential emissions from construction equipment, we do not anticipate any other odor issues during construction.

TISHMAN
An AECOM Company

One Congress Street Redevelopment

Temporary Construction Impacts/Mitigation

Phase 3B Construction of WP-B3

Site Logistics

Site Preparation, Construction Staging and Maintenance	The construction area work zone will be confined by jersey barriers and fencing. Construction site access will be through New Sudbury street. Vehicles will enter from the west and exit heading east. Site fenced area will include the parking area and adjacent travel lane on New Sudbury and fencing will continue along Congress St to delineate work zone. Truck track mat will be utilized during below grade construction. Crane picks will be made from New Sudbury Street within the fenced in area.
Erosion Control/Storm Water Management	An erosion and sediment control plan will be developed and maintained in accordance with local, state and federal requirements.

Traffic Impacts

Truck Traffic Management	**Arrivals** – From the South and West, vehicles will travel on I-93 North and take Exit 23 – Aquarium (toward Quincy Market). Merge onto North St and take a Right onto Congress St. Pass under Government Center Garage and take a Left onto New Chardon. Then Left onto Cambridge Street and finally a Left onto New Sudbury Street. From the North, Take I-93 Exit 24A Government Center, slight right on Clinton Street, left onto North Street, right onto Congress St and a left onto New Chardon. Then Left onto Cambridge Street and finally a Left onto New Sudbury Street. **Departures** – To go north, continue on New Sudbury Street and take left onto I-93 North ramp. To go south, take a left onto Congress and a take a right onto New Chardon Street and take I-93 South ramp.
Surrounding Streets	Site access will be located on New Sudbury. A detailed CMP and Traffic Control Plan will be developed. It is anticipated that the existing parking lane and one travel lane on New Sudbury will be utilized for vehicle and site access. No other impacts to surrounding streets are anticipated in this phase, but may be required for some off peak deliveries.

Public Safety during Construction

Pedestrian Routes	The sidewalk along the north side of New Sudbury will be closed. Pedestrians will be re-routed

	the south side of New Sudbury at the intersection of Congress Street and at the Police Station.
Temporary Protection	Temporary protection will be afforded by side walk and access walkway overhead protection and routes will be secured by barriers.

MBTA Access Changes/Impacts

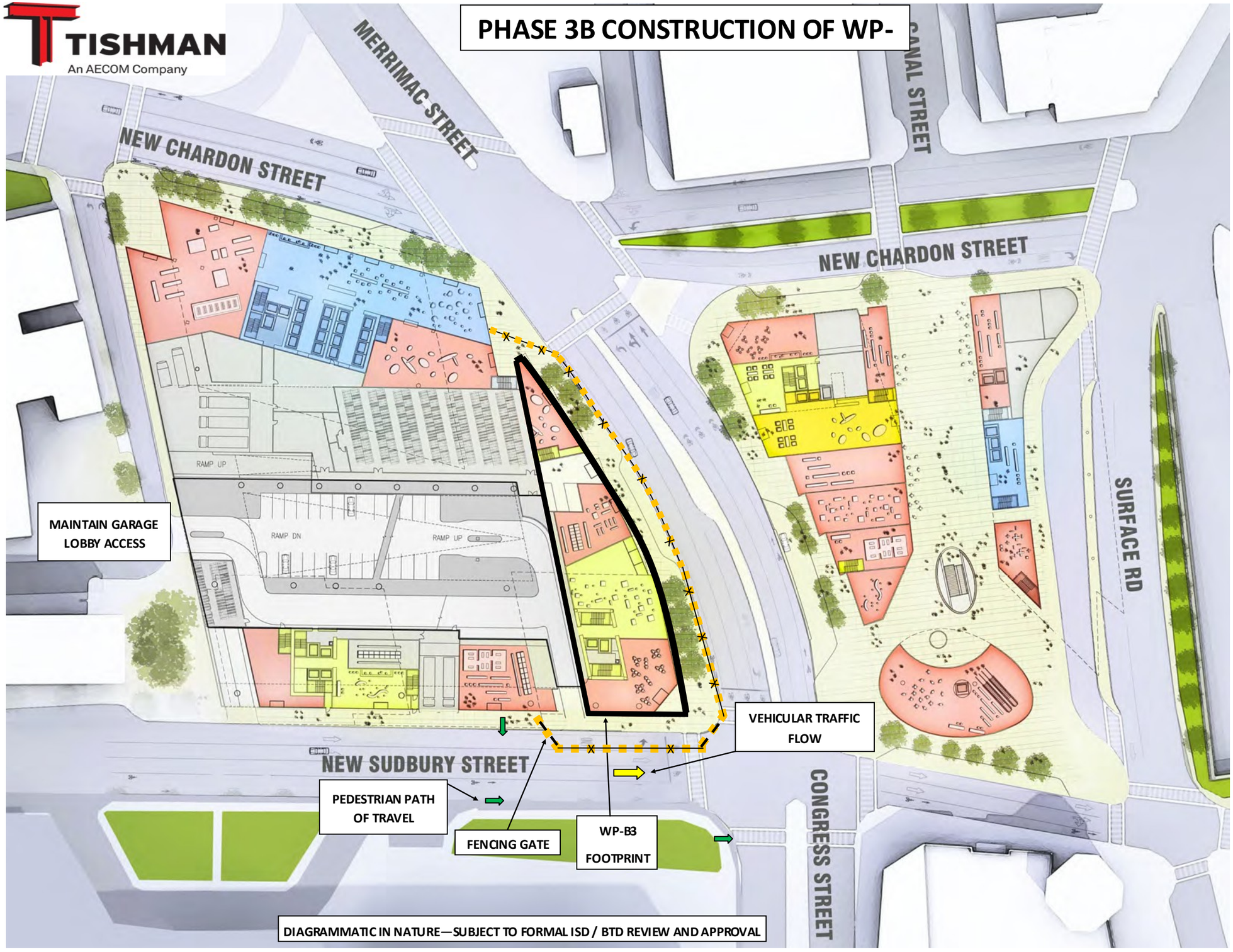
Green Line	No Impacts during this Phase.
Orange Line	No Impacts during this Phase.
Bus Stop	No Impacts during this Phase.

One Congress Street Garage

Garage Access	New Sudbury Garage entrance will have temporary protection.

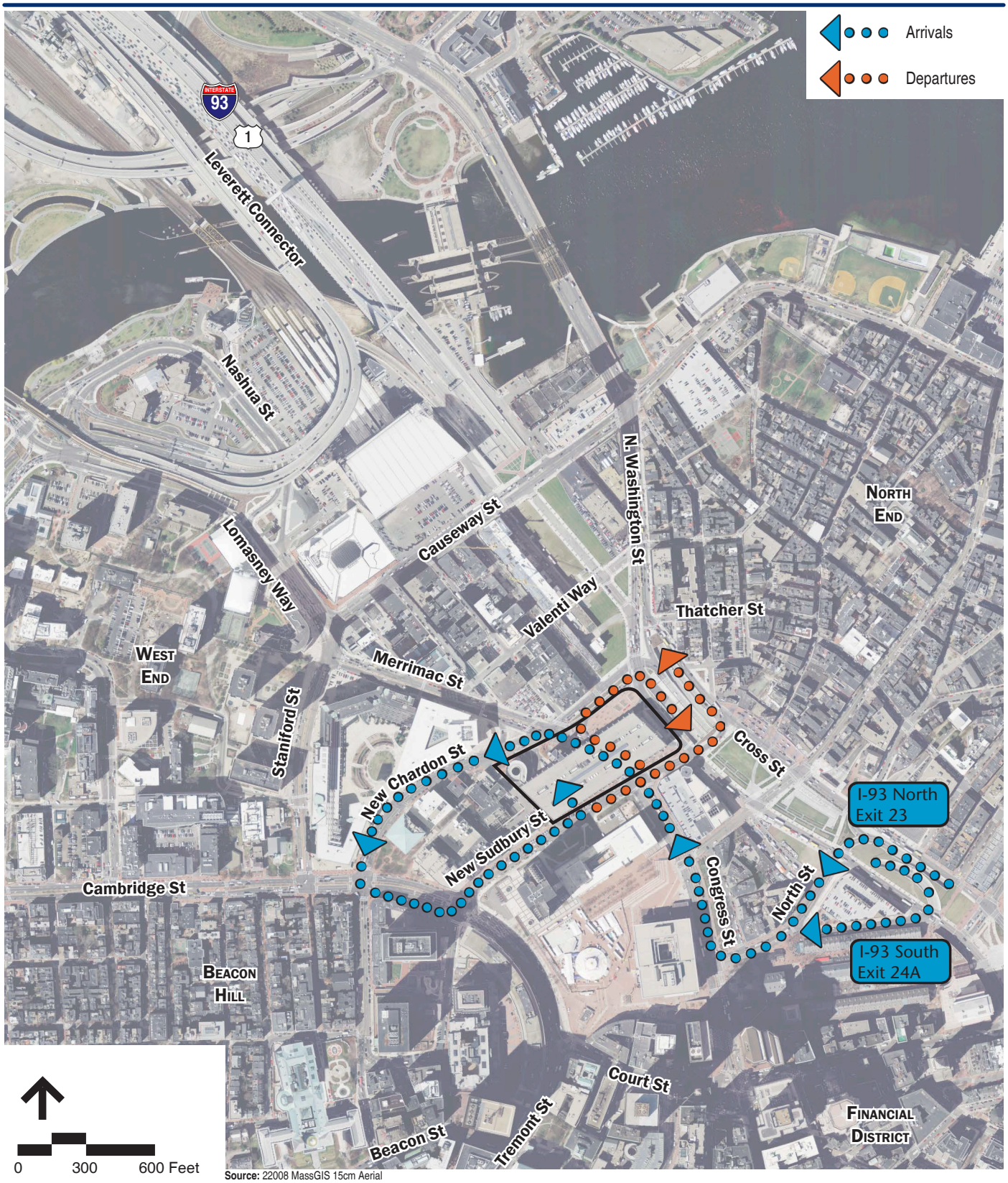
TISHMAN
An AECOM Company

PHASE 3B CONSTRUCTION OF WP-



DIAGRAMMATIC IN NATURE—SUBJECT TO FORMAL ISD / BTD REVIEW AND APPROVAL

E.2: Proposed Construction Truck Routes



Source: 22008 MassGIS 15cm Aerial

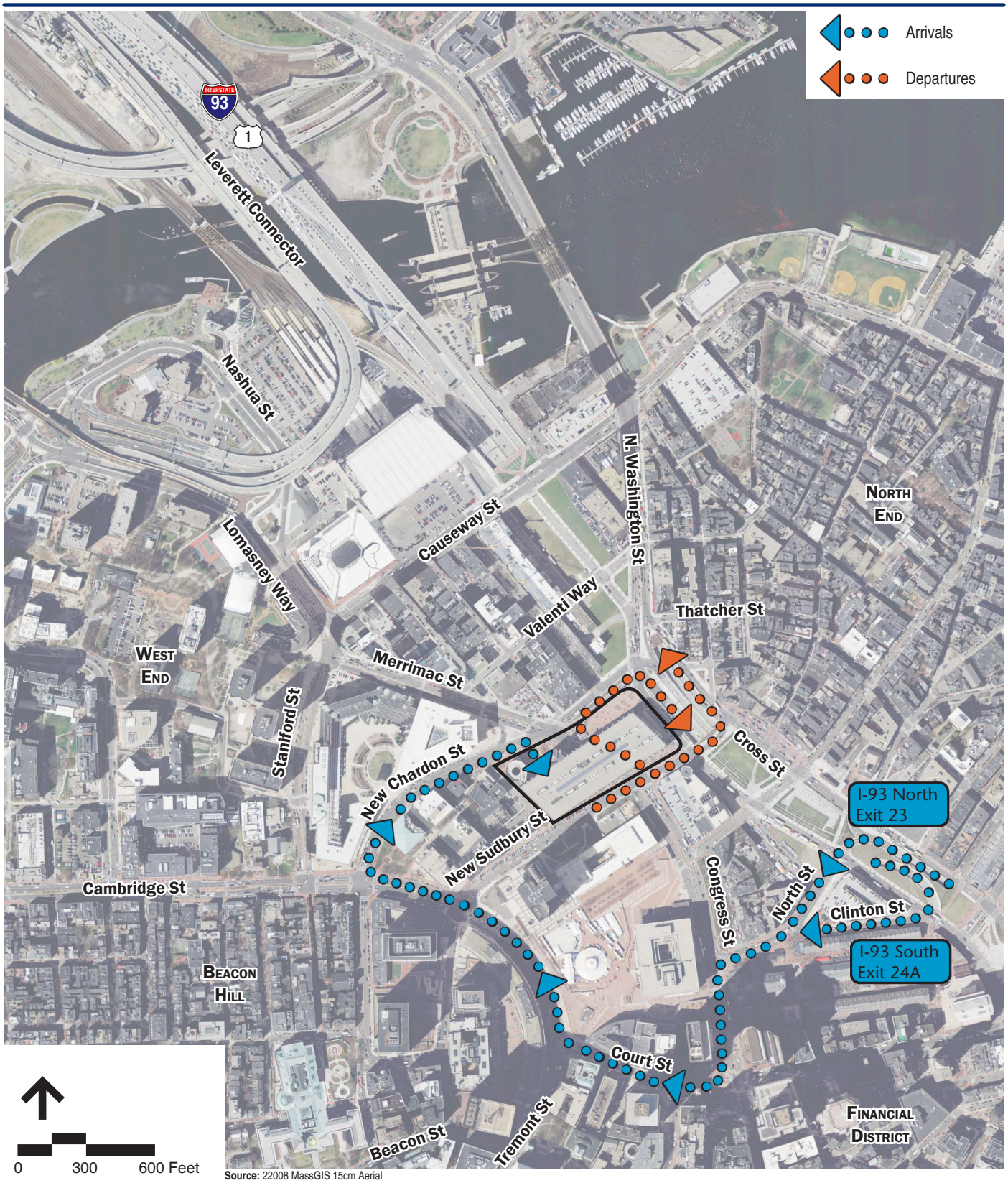
Redevelopment of Government Center Garage
Boston, MA

Figure E-2.1

THE HYM INVESTMENT GROUP, LLC

VHB Vanasse Hangen Brustlin, Inc.

Proposed Construction Truck Routes for WP-B1, Garage Deconstruction, East Parcel and WP-B3



Source: 22008 MassGIS 15cm Aerial

Redevelopment of Government Center Garage
Boston, MA

Figure E-2.2

THE HYM INVESTMENT GROUP, LLC

VHB Vanasse Hangen Brustlin, Inc.

Proposed Construction Truck Routes for WP-B2

Appendix F
List of Property Owners

■

City of Boston - Assessing Department : Abutter List
BOSTON, MA

Account Number	Location	Owner	Care Of	Mailing Address	City	ST	Zip
0301351000	43 COOPER ST	TARANTINO ANTHONY		28 BURBANK RD	MEDFORD	MA	02155
0301498000	34 THATCHER ST	CASA MARIA APARTMENTS LP	C/O COMMUNITY BUILDERS INC	95 BERKELEY ST	BOSTON	MA	02116
0301500000	LYNN ST	MICHELLE HOLDINGS LLC	C/O MICHELLE HOLDINGS LLC	55 HENSHAW ST	BOSTON	MA	02135
0301501000	51 53 COOPER ST	DECRISTOFORO LUCY		53 COOPER ST	BOSTON	MA	02113
0301502000	55 COOPER ST	MICHELLE HOLDINGS LLC	C/O MICHELLE HOLDINGS LLC	55 HENSHAW ST	BOSTON	MA	02135
0301503000	57 59 COOPER ST	MICHELLE HOLDINGS LLC	C/O MICHELLE HOLDINGS LLC	55 HENSHAW ST	BOSTON	MA	02135
0301504000	45 49 N WASHINGTON ST	MICHELLE HOLDINGS LLC	C/O MICHELLE HOLDINGS LLC	55 HENSHAW ST	BOSTON	MA	02135
0301505000	51 53 N WASHINGTON ST	MICHELLE HOLDINGS LLC	C/O MICHELLE HOLDINGS LLC	55 HENSHAW ST	BOSTON	MA	02135
0301506000	55 57 N WASHINGTON ST	MICHELLE HOLDINGS LLC	C/O MICHELLE HOLDINGS LLC	55 HENSHAW ST	BOSTON	MA	02135
0301507000	59 61 N WASHINGTON ST	MICHELLE HOLDINGS LLC	C/O MICHELLE HOLDINGS LLC	55 HENSHAW ST	BOSTON	MA	02135
0301508000	65 63 N WASHINGTON ST	MICHELLE HOLDINGS LLC	C/O MICHELLE HOLDINGS LLC	55 HENSHAW ST	BOSTON	MA	02135
0301560000	HAVERHILL ST	MASS BAY TRANSPORTATION AUTH		10 PARK PLZ	BOSTON	MA	02116
0301564000	ANTHONY R VALENTI WY	COMMWLTH OF MASS		TRAVERSE	BOSTON	MA	02114
0301565000	BEVERLY ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0301566000	N WASHINGTON ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0301567000	N WASHINGTON ST	COMM OF MASS	STATE TRANSP BUILDING	10 PARK PLZ	BOSTON	MA	02116
0301568000	53 85 CANAL ST	CANAL PLAZA LLC	C/O HUNNEMAN MGMT CO	303 CONGRESS ST	BOSTON	MA	02210
0301570010	CANAL ST	MASS BAY TRANSP AUTH		CANAL ST	BOSTON	MA	02114
0301591020	104-108 CANAL ST	WEINREB ROGER L TS	C/O PETER B WEINREB	6509 POZA RICA NW	LOS RANCHOS	NM	87107
0301592000	32 38 ANTHONY R VALENTI WY	GREATER BOSTON LEGAL SERVICE		197 FRIEND ST &	BOSTON	MA	02114
0301610000	54 48 CANAL ST	FIFTY 4 CNL REALTY LLC	C/O HAMLEN & CO/CHARLES MCKENZIE	54 CANAL ST	BOSTON	MA	02114
0301611000	155 FRIEND ST	ANDREW DUTTON CO INC		284 BODWELL ST	AVON	MA	02322
0301612000	157 159 FRIEND ST	BAY COVE HUMAN SERVICES INC	C/O PAUL TONTHAT	66 CANAL ST &	BOSTON	MA	02114
0301613000	165 FRIEND ST	ONE 65 FRIEND ST CONDO ASSN		165 FRIEND	BOSTON	MA	02114
0301613002	165 FRIEND ST #1	IBRAHIM SINOTE ETAL		165 FRIEND	BOSTON	MA	02114
0301613004	165 FRIEND ST #2	GANNETT RICHARD W		165 FRIEND ST #2	BOSTON	MA	02114
0301613006	165 FRIEND ST #3	METCALF JANE E		7110 KITTIWAK RUN	MANLIUS	NY	13104
0301613008	165 FRIEND ST #4	ARCINIEGAS DIEGO A		165 FRIEND ST #4	BOSTON	MA	02114
0301613010	165 FRIEND ST #5	WU DUAN		165 FRIEND ST #5	BOSTON	MA	02114
0301615000	CHAPEL PL	RANELLI LOUIS A		1 HICKORY LANE	SAUGUS	MA	01906
0301616000	CHAPEL PL	RANELLI LOUIS II TS	C/O LOUIS RANELLI II TS	1 HICKORY LN	SAUGUS	MA	01906
0301617000	CHAPEL PL	BAY COVE HUMAN SERVICES INC	C/O PAUL TONTHAT	66 CANAL ST &	BOSTON	MA	02114
0301618000	FRIEND ST	BAY COVE HUMAN SERVICES INC	C/O PAUL TONTHAT	66 CANAL ST &	BOSTON	MA	02114

City of Boston - Assessing Department : Abutter List
BOSTON, MA

Account Number	Location	Owner	Care Of	Mailing Address	City	ST	Zip
0301619000	90 CANAL	CANAL ST LLC 90	C/O VANTAGE REAL ESTATE MGT	90 CANAL ST	BOSTON	MA	02114
0301623000	80 74 CANAL ST	RANELLI LOUIS A		1 HICKORY LANE	SAUGUS	MA	01906
0301626000	NEW CHARDON	CITY OF BOSTON		NEW CHARDON	BOSTON	MA	02114
0301628000	158 150 FRIEND ST	DINOSAUR MERRIMAC LLC	C/O SCOTT ORAN	101 HUNTINGTON AV 9TH FL	BOSTON	MA	20199
0301632000	MERRIMAC ST	NINETY CANAL ST LLC	C/O MECA SAULS, CONTROLLER	HN GORIN INC, 101 HUNTINGTON AV	5TH FL BOSTON	MA	02199
0301633000	121 127 PORTLAND ST	ONE-21 PORTLAND LLC	C/O STATE FINANCIAL SERV INC	197 PORTLAND ST	BOSTON	MA	02114
0301634000	129 131 PORTLAND ST	OLYMPIA GROUP LP		PO BOX 374	WESTPORT	MA	02790
0301635000	ANTHONY R VALENTI WY	MASS GAS * ELECTRIC	C/O M G E HOLDING CO INC	6 MORRILL CIRCLE	WELLESLEY	MA	02482
0301636000	ANTHONY R VALENTI WY	MASS GAS * ELECTRIC	C/O M G E HOLDING CO INC	6 MORRILL CIRCLE	WELLESLEY	MA	02482
0301637000	FRIEND ST	MASS GAS * ELECTRIC	C/O M G E HOLDING CO INC	6 MORRILL CIRCLE	WELLESLEY	MA	02482
0301639000	FRIEND ST	GORIN ROSALIND E TS	C/O H.N. GORIN INC/M SAULS	101 HUNTINGTON AV, 5TH FL	BOSTON	MA	02199
0301639001	FRIEND ST	GORIN ROSALIND E TS	C/O H.N.GORIN INC/ M SAULS	101 HUNTINGTON AV, 5TH FL	BOSTON	MA	02199
0301640000	FRIEND ST	GORIN ROSALIND E TS	C/O H.N. GORIN INC/M SAULS	101 HUNTINGTON AV, 5TH FL	BOSTON	MA	02199
0301641000	FRIEND ST	GORIN ROSALIND E TS	C/O H.N. GORIN INC/M SAULS	101 HUNTINGTON AV, 5TH FL	BOSTON	MA	02199
0301642000	FRIEND ST	MASS GAS * ELECTRIC	C/O M G E HOLDING CO INC	6 MORRILL CIRCLE	WELLESLEY	MA	02482
0301643000	ANTHONY R VALENTI WY	MASS GAS * ELECTRIC	C/O M G E HOLDING CO INC	6 MORRILL CIRCLE	WELLESLEY	MA	02482
0301644000	14 16 ANTHONY R VALENTI WY	PORTLAND STREET HOLDINGS LLC	C/O SYNERGY INVESTMENTS	100 FRANKLIN ST 2ND FLOOR	BOSTON	MA	02110
0301645000	PORTLAND ST	MASS GAS * ELECTRIC	C/O M G E HOLDING CO INC	6 MORRILL CIRCLE	WELLESLEY	MA	02482
0301660000	222 224 FRIEND ST	ONE41 PORTLAND ST LLC	C/O SYNERGY INVESTMENTS	100 FRANKLIN ST, 2ND FLOOR	BOSTON	MA	02110
0301661000	FRIEND ST	MASS GAS * ELECTRIC	C/O M G E HOLDING CO INC	6 MORRILL CIRCLE	WELLESLEY	MA	02482
0301664000	132 130 PORTLAND ST	COUGHLIN JOHN E TS	JOHN E COUGHLIN/GATEWAY RLTY	239 WESTERN AVE	ESSEX	MA	01929
0301665000	142 138 PORTLAND ST	CARLSON CLAIR A	C/O M H MASSEY CO LLC	117 SOUTH 14TH ST SUITE 300	RICHMOND	VA	23219
0301675000	101 MERRIMAC ST	ONE-01 MERRIMAC LLC	C/O H.N GORIN INC	101 HUNTINGTON AVE 5TH FLR	BOSTON	MA	02199
0301686000	115 CAMBRIDGE ST	COMMONWEALTH OF MASS		115 CAMBRIDGE	BOSTON	MA	02114
0301687000	MERRIMAC ST	BOSTON REDEVELOPMNT AUTH		MERRIMAC	BOSTON	MA	02114
0301688000	24 NEW CHARDON ST	COMMONWEALTH OF MASS		ONE ASHBURTON PL	BOSTON	MA	02108
0302396000	198 HANOVER ST	SIXTY CROSS STREET LLC	C/O SIXTY CROSS STREET LLC	975 UNIVERSITY AV	NORWOOD	MA	02062
0302397000	53 55 SALEM ST	SIXTY CROSS STREET LLC	C/O LYNN LIND	975 UNIVERSITY AVENUE	NORWOOD	MA	02062
0302398000	57 61 SALEM ST	FIFTY 7-61 SALEM ST CONDO TR		57 SALEM	BOSTON	MA	02113
0302398002	57 SALEM ST #57F-1	CAPRICORN 24 SERIES LLC	C/O CHRISTOPHER YOUNG MGR	5 FREMONT ST	WINTHROP	MA	02152
0302398004	57 SALEM ST #57F-2	OCONNOR KIMBERLY M	C/O KIMBERLY M. O'CONNOR	44 BOW RD	BELMONT	MA	02478
0302398006	57 SALEM ST #57F-3	KAYNE PATRICIA D	C/O PATRICIA KAYNE SEGEDY	19 DALE ST	SWAMPSCOTT	MA	01907
0302398008	57 SALEM ST #57F-4	DECHRISTOFORO JOHN RYAN	C/O JOHN R DECHRISTOFORO	57 SALEM ST #4F	BOSTON	MA	02113

City of Boston - Assessing Department : Abutter List
BOSTON, MA

Account Number	Location	Owner	Care Of	Mailing Address	City	ST	Zip
0302398010	57R SALEM ST #57R-1	KENT AND ASSOCIATES INC		P O BOX 550218	N WALTHAM	MA	02455
0302398012	57 R SALEM ST #57R-2	BENJAMIN DAVID M ETAL		57R SALEM ST #57R-2	BOSTON	MA	02113
0302398014	57 R SALEM ST #57R-3	CRAIG PATRICIA M		34 TEELE AV	W SOMERVILLE	MA	02144
0302398016	57 R SALEM ST #57R-4	DOOLEY PATRICIA C	C/O PATRICIA CRAIG	32 TEELE AVE	W SOMERVILLE	MA	02144
0302398018	59 R SALEM ST #59R-1	CROWLEY DAVID G		59R SALEM ST #1	BOSTON	MA	02113
0302398020	59 R SALEM ST #59R-2	PANAGIOTOPOULOS VASILIOS	C/O IOANIS PARAGIOTOPOULOS	19 COUNTRY CLUB DR	TEWKSBURY	MA	01876
0302398022	59 R SALEM ST #59R-3	FIFTY-9-3R SALEM STREET	C/O SUSAN PASSACANTILLI	328 POND ST	JAMAICA PLAIN	MA	02130
0302398024	59 R SALEM ST #59R-4	TROIANI LISA L		59 SALEM ST #4R	BOSTON	MA	02113
0302398026	59 SALEM ST #59F-1	IACOVONE LISA	C/O VITO L. IACOVONE	15 ROBIN HILL ROAD	CHELMSFORD	MA	01824
0302398028	59 SALEM ST #59F-2	MCGEE JAMES W		59 SALEM ST #59F-2	BOSTON	MA	02113
0302398030	59 SALEM ST #59F-3	IACOVONE VITO L	C/O VITO IACOVONE	15 ROBIN HILL RD	CHESTNUT HILL	MA	01824
0302398032	59 SALEM ST #59F-4	CACACE JOHN A III	C/O JOHN CACACE	394 RIVERWAY #15	BOSTON	MA	02115
0302398034	61 SALEM ST #61-1	CAPRICORN 24 SERIES LLC	C/O CHRISTOPHER YOUNG MGR	5 FREEMONT ST	WINTHROP	MA	02152
0302398036	61 SALEM ST #61-2	MASTROCOLA GLORIA M	C/O GLORIA M GAVRIS	21 MONADNOCK RD	CHESTNUT HILL	MA	02467
0302398038	61 SALEM ST #61-3	SAMIA CARA	C/O CARA SAMIA	61 SALEM ST #61-3	BOSTON	MA	02113
0302398040	61 SALEM ST #61-4	GARDNER AVRIL					
0302398042	61 SALEM ST #61-5	ONEIL EDWIN R	C/O EDWIN ONEIL	61 SALEM ST #61-5	BOSTON	MA	02113
0302421000	HANOVER ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0302432000	CROSS ST	COMMWLTH OF MASS		CROSS	BOSTON	MA	02113
0302432001	CROSS ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0302456000	52 56 SALEM ST	PACE JOSEPH A TRSTS	C/O JOSEPH A PACE	190 MAIN ST	SAUGUS	MA	01906
0302457000	48 50 SALEM ST	RUGGERIO JOSEPH S		1 NAYATT PT CT	BARRINGTON	RI	02806
0302458000	46 50 CROSS ST	LAFAUCI FELIX TRST	C/O STEPHEN LAFAUCI	969 SALEM ST	MALDEN	MA	02148
0302459000	40 42 CROSS ST	PACE JOSEPH A TRSTS	C/O JOSEPH A PACE	190 MAIN ST	SAUGUS	MA	01906
0302460000	28 32 CROSS ST	PACE JOSEPH A	C/O JOSEPH A PACE	190 MAIN ST	SAUGUS	MA	01906
0302460001	CROSS ST	PACE JOSEPH A TS	C/O JOSEPH PACE	190 MAIN ST	SAUGUS	MA	01906
0302461000	55 57 ENDICOTT ST	PACE JOSEPH A TS	C/O JOSEPH PACE	190 MAIN ST	SAUGUS	MA	01906
0302462000	57 R ENDICOTT ST	PACE JOSEPH A TS	C/O JOSEPH PACE	190 MAIN ST	SAUGUS	MA	01906
0302463000	59 61 ENDICOTT ST	SIXTY ONE ENDICOTT ST LLC	C/O SIXTY ONE ENDICOTT ST LLC	125 BROAD ST	BOSTON	MA	02110
0302463001	MORTON ST	PACE JOSEPH A TRSTS	C/O JOSEPH PACE	190 MAIN ST	SAUGUS	MA	01906
0302464000	MORTON ST	PACE JOSEPH A TS	C/O JOSEPH PACE TS	190 MAIN ST	SAUGUS	MA	01906
0302464001	MORTON ST	PACE JOSEPH A TRSTS	C/O JOSEPH A PACE	190 MAIN ST	SAUGUS	MA	01906
0302464002	MORTON ST	PACE JOSEPH A TRSTS	C/O JOSEPH A PACE	190 MAIN ST	SAUGUS	MA	01906

City of Boston - Assessing Department : Abutter List
BOSTON, MA

Account Number	Location	Owner	Care Of	Mailing Address	City	ST	Zip
0302465000	58 60 SALEM ST	OMAR MOHAMED A TS		58 SALEM ST	BOSTON	MA	02113
0302466000	MORTON ST	CITY OF BOSTON		MORTON	BOSTON	MA	02113
0302469010	26 STILLMAN ST	TWENTY6 STILLMAN ST CONDO TR		26 STILLMAN ST	BOSTON	MA	02113
0302469012	26 STILLMAN #1-1	LAGASSE GLENN A		26 STILLMAN ST #1-1	BOSTON	MA	02113
0302469014	26 STILLMAN #1-2	ABULARACH MARIO		26 STILLMAN ST #1-2	BOSTON	MA	02113
0302469016	26 STILLMAN #1-3	KARNELL JEREMI D		26 STILLMAN ST #1-3	BOSTON	MA	02113
0302469018	26 STILLMAN ST #1-4	SPILLERE ROGGIERO J		26 STILLMAN ST #1-4	BOSTON	MA	02113
0302469020	26 STILLMAN ST #2-1	QUINN STEPHANIE K	C/O STEPHANIE K QUINN	26 STILLMAN ST #2-1	BOSTON	MA	02113
0302469022	26 STILLMAN ST #2-2	WARREN JEREMY		26 STILLMAN ST #2-2	BOSTON	MA	02113
0302469024	26 STILLMAN ST #2-3	CONDELLI MICHAEL C		26 STILLMAN ST # 2-3	BOSTON	MA	02113
0302469026	26 STILLMAN ST #2-4	LUKACS SAMANTHA		26 STILLMAN ST #2-4	BOSTON	MA	02113
0302469028	26 STILLMAN ST #2-5	LAGASSE LISA A		26 STILLMAN ST #2-5	BOSTON	MA	02113
0302469030	26 STILLMAN ST #3-1	BURKE JORDAN M	C/O JORDAN M BURKE	26 STILLMAN ST # 3-1	BOSTON	MA	02113
0302469032	26 STILLMAN ST #3-2	ONEIL JANE R					
0302469034	26 STILLMAN ST #3-3	REISS GARY P	C/O GARY & BRIDGET REISS	324 REEDY MEADOW RD	GROTON	MA	01450
0302469036	26 STILLMAN ST #3-4	HALE ROBIN	C/O ROBIN HALE	26 STILLMAN ST #3-4	BOSTON	MA	02113
0302469038	26 STILLMAN ST #3-5	DURSO STEPHEN F	C/O STEPHEN DURSO	17 SWAN LANE	ANDOVER	MA	01810
0302469040	26 STILLMAN ST #4-1	GIANATASIO FRANK C	C/O FRANK GIANATASIO	26 STILLMAN ST #4-1	BOSTON	MA	02113
0302469042	26 STILLMAN ST #4-2	GAVIN JOHN M	C/O JOHN M GAVIN	26 STILLMAN ST #4-2	BOSTON	MA	02113
0302469044	26 STILLMAN ST #4-3	BALLARIN PETER					
0302469046	26 STILLMAN #4-4	SURAN CAROLINA					
0302469048	26 STILLMAN ST #4-5	LEE CHRISTOPHER B	C/O CHRISTOPHER B LEE	26 STILLMAN ST #4-5	BOSTON	MA	02113
0302469050	26 STILLMAN ST #5-1	SHUR STEVEN E	C/O STEVEN SHUR	26 STILLMAN ST #5-1	BOSTON	MA	02113
0302469052	26 STILLMAN ST #5-2	GEORGE DEIRDRE	C/O DEIRDRE GEORGE	26 STILLMAN ST # 5-2	BOSTON	MA	02113
0302469054	26 STILLMAN ST #5-3	CANGIANO PAUL M		26 STILLMAN ST #5-3	BOSTON	MA	02113
0302469056	26 STILLMAN ST #5-4	SHANBAR MATTHEW					
0302469058	26 STILLMAN ST #5-5	SAMMON JOHN G		26 STILLMAN ST #5-5	BOSTON	MA	02113
0302469060	26 STILLMAN ST #6-1	DEMAGISTRIS NICOLA L		26 STILLMAN ST #6-1	BOSTON	MA	02113
0302469062	26 STILLMAN ST #6-2	HOFFMAN KIRSTEN L	C/O KIRSTEN L HOFFMAN	26 STILLMAN ST #6-2	BOSTON	MA	02113
0302469064	26 STILLMAN ST #6-3	GARCIA ROD R		26 STILLMAN ST # 6-3	BOSTON	MA	02113
0302469066	26 STILLMAN ST #6-4	OCONNOR CORNELIUS J		26 STILLMAN ST #6-4	BOSTON	MA	02113
0302469500	26 STILLMAN ST	INTERCONTINENTAL FUND II 63					
0302470000	24 22 STILLMAN ST	TWENTY4 STILLMAN STREET LLC		334 NORTH ST	BOSTON	MA	02113

City of Boston - Assessing Department : Abutter List
BOSTON, MA

Account Number	Location	Owner	Care Of	Mailing Address	City	ST	Zip
0302471000	20 STILLMAN ST	TWENTY STILLMAN STREET LLC	C/O 20 STILLMAN ST LLC	334 NORTH ST	BOSTON	MA	02113
0302472000	18 STILLMAN ST	EIGHTEEN STILLMAN ST		18 STILLMAN ST	BOSTON	MA	02113
0302472002	18 STILLMAN ST #1	CASTELLUCCI FEDERICO TS		258 W NEWTON ST	BOSTON	MA	02116
0302472004	18 STILLMAN ST #2	CASTELLUCCI FEDERICO TS		258 W NEWTON ST	BOSTON	MA	02116
0302472006	18 STILLMAN ST #3	CASTELLUCCI FEDERICO TS		258 W NEWTON ST	BOSTON	MA	02116
0302472008	18 STILLMAN ST #4	CASTELLUCCI FEDERICO TS		258 W NEWETON ST	BOSTON	MA	02116
0302473000	16 STILLMAN ST	SIXTEEN STILLMAN STREET		16 STILLMAN ST	BOSTON	MA	02113
0302473002	16 STILLMAN ST #1	JENKINS JASON H	C/O JASON H JENKINS	16 STILLMAN ST #1	BOSTON	MA	02113
0302473004	16 STILLMAN ST #2	MITCHEL THOMAS R		16 STILLMAN ST #2	BOSTON	MA	02113
0302473006	16 STILLMAN ST #3	MEZER EDWARD JOSEPH	C/O EDWARD JOSEPH MEZER	16 STILLMAN #3	BOSTON	MA	02113
0302473008	16 STILLMAN ST #4	LYNCH MARCIA T	C/O MARCIA T LYNCH	33 CLINTON AV	S NYACK	NY	10960
0302476000	64 66 SALEM ST	SIXTY 4-66 SALEM ST CONDO TR	C/O RMC DEVELOPMENT CORP	P.O BOX 51182	BOSTON	MA	02205
0302476002	64 66 SALEM ST #C1	CAPRICORN 24 SERIES LLC	C/O CHRISTOPHER YOUNG	5 FREMONT ST	WINTHROP	MA	02152
0302476004	64 66 SALEM ST #2F	SHEEHAN PAMELA A TS	C/O STEPHEN G SHEEHAN	64-66 SALEM ST #2F	BOSTON	MA	02113
0302476006	64 66 SALEM ST #2R	ARRIGG FRED G	C/O FRED G ARRIGG	8 FARNHAM CI	ANDOVER	MA	01810
0302476008	64 66 SALEM ST #3F	SHUMWAY KEVIN A					
0302476010	64 66 SALEM ST #3R	SHUMWAY KEVIN A	C/O KEVIN SHUMWAY	346 CONGRESS ST UNIT 502	BOSTON	MA	02210
0302476012	64 66 SALEM ST #4F	MAMARY MARYCATHERINE TS	C/O MARYCATHERINE MAMARY TS	93 MAIN STREET	HINGHAM	MA	02043
0302476014	64 66 SALEM ST #4R	ARRIGG FRED G	C/O FRED G ARRIGG	8 FARNHAM CI	ANDOVER	MA	01810
0302476016	64 66 SALEM ST #5F	GUIGLI MICHAEL P	C/O MICHAEL P GUIGLI	64-66 SALEM ST #5F	BOSTON	MA	02113
0302476018	64 66 SALEM ST #5R	INGALLS ABIGAIL D	C/O ABIGAIL D INGALLS	64-66 SALEM ST #5R	BOSTON	MA	02113
0302476020	64 66 SALEM ST #PH 1	ARRIGG FRED G JR	C/O FRED G ARRIGG JR	64-66 SALEM ST #PH 1	BOSTON	MA	02113
0302476022	64 66 SALEM ST #PH 2	TUCH STEVEN A	C/O STEVEN A TUCH	64-66 SALEM ST #PH 2	BOSTON	MA	02113
0302477000	62 SALEM ST	OMAR MOHAMED A TS	C/O MOHAMED A OMAR	60 SALEM ST	BOSTON	MA	02113
0302485000	19 STILLMAN ST	BROGNA CARLO					
0302517000	34 COOPER ST	GAMBALE ANTHONY J	C/O GERALD ZYFERS	PO BOX 349	MEDINA	WA	98039
0302518000	73 75A ENDICOTT ST	CAPONE EDWARD TS	C/O JEFF CAPONE	73 ENDICOTT ST	BOSTON	MA	02113
0302519000	77 79 ENDICOTT ST	CAPONE EDWARD TS	C/O JEFF CAPONE	73 ENDICOTT ST	BOSTON	MA	02113
0302520000	83 ENDICOTT ST	EIGHTY1-83 ENDICOTT ST CONDO	C/O SALIL K MIDHA TS	83 ENDICOTT ST	BOSTON	MA	02113
0302520002	81 83 ENDICOTT ST	MIDHA SALIL K TS		17 ST THOMAS MORE DR	WINCHESTER	MA	01890
0302520004	81 83 ENDICOTT ST #2	MIDHA SALIL K TS		17 ST THOMAS MORE DR	WINCHESTER	MA	01890
0302520006	81 83 ENDICOTT ST #3	MIDHA SALIL K TS		17 ST THOMAS MORE DR	WINCHESTER	MA	01890
0302520008	81 83 ENDICOTT ST #4	MIDHA SALIL K TS		17 ST THOMAS MORE DR	WINCHESTER	MA	01890

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Account Number	Location	Owner	Care Of	Mailing Address	City	ST	Zip
0302521000	87 89 ENDICOTT ST	MUCCIO SALVATORE J TS	C/O MARY COLLEAMENO	15 STILLMAN ST	BOSTON	MA	02113
0302522000	93 91 ENDICOTT ST	FARIA JOSE		93 ENDICOTT ST	BOSTON	MA	02113
0302523000	95 97 ENDICOTT ST	RUSSO JENNIE M	C/O JENNIE M RUSSO	97-95 ENDICOTT ST	BOSTON	MA	02113
0302524000	99 ENDICOTT ST	WASNER ANNA		99 ENDICOTT ST	BOSTON	MA	02113
0302525000	101 ENDICOTT ST	DIMAURO JOANNE		4 FARNHAM PT RD	E BOOTHBAY	ME	04544
0302527000	74 76 ENDICOTT ST	DELFAVERO NINA TS	C/O DOMINIC TAVILLA	10 VIKING RD	WINCHESTER	MA	01890
0302528000	STILLMAN ST	ROBERTO FRANK TS		96 ENDICOTT ST	BOSTON	MA	02113
0302528003	STILLMAN ST	CITY OF BOSTON DPW		STILLMAN ST	BOSTON	MA	02113
0302529000	STILLMAN ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0302529003	STILLMAN ST	CITY OF BOSTON		STILLMAN ST	BOSTON	MA	02113
0302529005	STILLMAN ST	ROBERTO FRANK TS		96 ENDICOTT ST	BOSTON	MA	02113
0302530000	2 STILLMAN PL	TWO STILLMAN PL CONDO TR		2 STILLMAN PL	BOSTON	MA	02113
0302530002	2 STILLMAN PL #1	PEANUT TRUST LLC	C/O PEANUT TRUST LLC	114 NORTH ST	STONEHAM	MA	02180
0302530004	2 STILLMAN PL #2	MCMAHON DANIEL	C/O DANIEL MCMAHON	2 STILLMAN PL #2	BOSTON	MA	02113
0302530006	2 STILLMAN PL #3	BRENNAN MICHELLE	C/O MICHELLE BRENNAN	2 STILLMAN PL #3	BOSTON	MA	02113
0302530008	2 STILLMAN PL #4	DAVIS BRIGITTE LINDA	C/O BRIGITTE L DAVIS	2 STILLMAN PL #4	BOSTON	MA	02113
0302531000	3 STILLMAN PL	JEAN ELEANOR M		3 STILLMAN PL	BOSTON	MA	02113
0302532000	4 STILLMAN PL	MENDOZA-ITURRALDE JORGE					
0302533000	5 STILLMAN PL	FIVE STILLMAN PLACE	C/O FRANCIS MONKIEWICZ TS	5 STILLMAN PLACE	BOSTON	MA	02113
0302533002	5 STILLMAN PL #1	DANGELMAIER RALPH A	C/O RALPH A DANGELMAIER	38 SEARS RD	WESTON	MA	02493
0302533004	5 STILLMAN PL #2	ARDINI ANDREW TS	C/O ANDREW ARDINI TS	5 STILLMAN PL # 2	BOSTON	MA	02113
0302533006	5 STILLMAN PL #3	ONSTOTT AINSLEY C					
0302533008	5 STILLMAN PL #4	SAWYER REBECCA		5 STILLMAN PL # 4	BOSTON	MA	02113
0302534000	6 STILLMAN PL	CONLON DAVID L		104 SHERBURN CI	WESTON	MA	02493
0302535000	7 STILLMAN PL	SEVEN STILLMAN PL CONDO TR	C/O SEVEN STILLMAN PLACE LLC	87 TERRACE HALL AV	BURLINGTON	MA	01803
0302535002	7 STILLMAN PL #1	YACCARINO DANIEL M	C/O DNAIEL M YACCARINO	52 COOPER ST #1	BOSTON	MA	02113
0302535004	7 STILLMAN PL #2	ONEIL MARIAN		52 COOPER ST #2	BOSTON	MA	02113
0302535006	7 STILLMAN PL #3	MOSCHOS THOMAS W	C/O ATTY DM MOSCHOS	100 FRONT ST	WORCESTER	MA	01608
0302535008	7 STILLMAN PL #4	MARENGI ARTHUR	C/O ARTHUR MARENGI	52 COOPER ST #4	BOSTON	MA	02113
0302535010	7 STILLMAN PL #5	HATTON COLMAN	C/O COLMAN HATTON	52 COOPER ST #5	BOSTON	MA	02113
0302535012	7 STILLMAN PL #6	COSTELLO JOHN H III		52 COOPER ST #6	BOSTON	MA	02113
0302535014	7 STILLMAN PL #7	LAMONT SCOTT		52 COOPER ST #7	BOSTON	MA	02113
0302535016	7 STILLMAN PL #8	SOKOLOV ILYA	C/O ILYA SOKOLOV	52 COOPER ST # 8	BOSTON	MA	02113

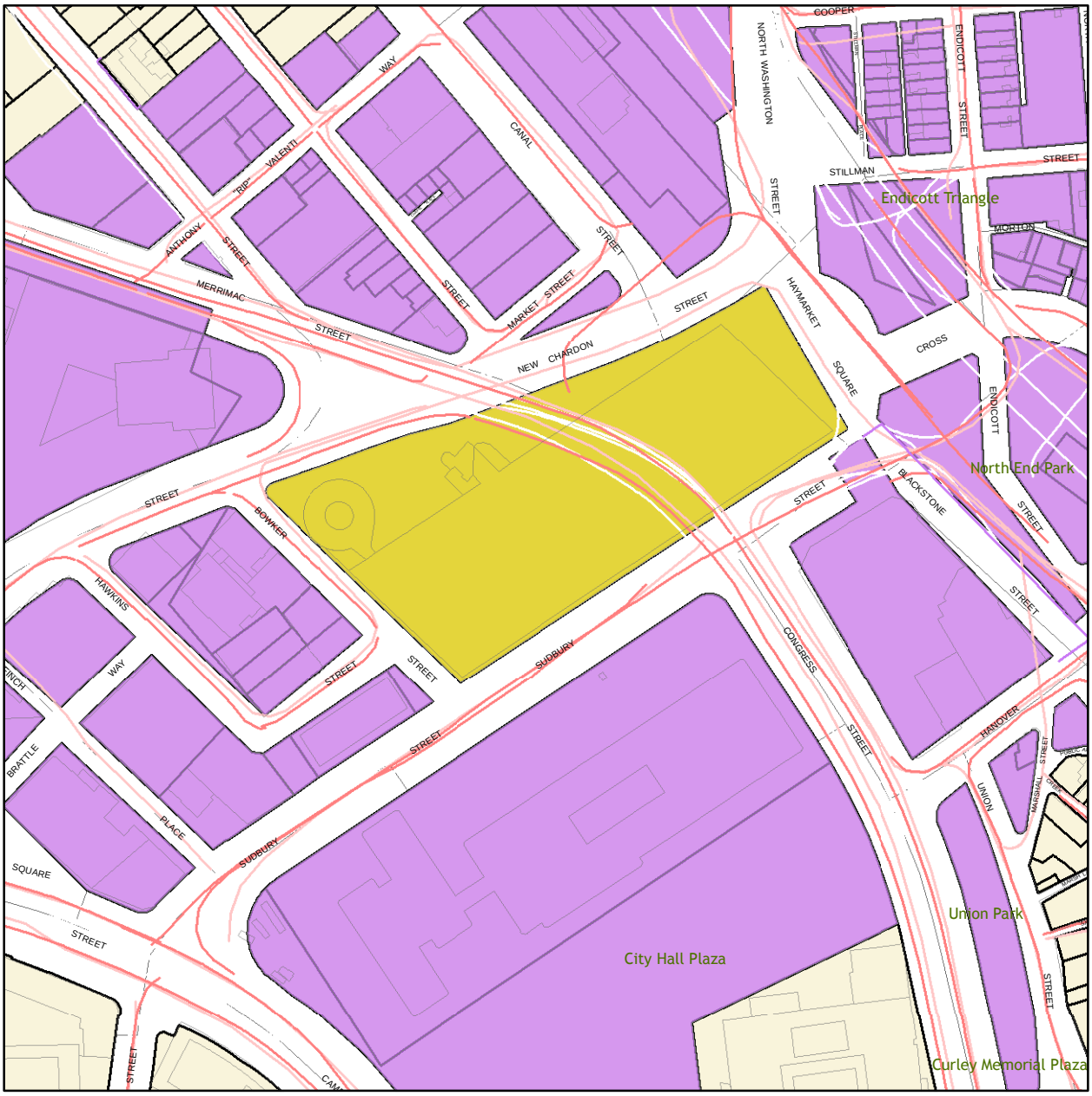
City of Boston - Assessing Department : Abutter List
BOSTON, MA

Account Number	Location	Owner	Care Of	Mailing Address	City	ST	Zip
0302535018	7 STILLMAN PL #9	TALLMAN COLBY S	C/O COLBY S TALLMAN	52 COOPER ST #9	BOSTON	MA	02113
0302535020	7 STILLMAN PL #10	HENDERSON DAVID		52 COOPER ST #10	BOSTON	MA	02113
0302536000	46 COOPER ST	FORTY-SIX COOPER ST CONDO	C/O ANTHONY RANALDI TS	46 COOPER ST	BOSTON	MA	02113
0302536001	44 42 COOPER ST	LUPO KRISTINA T	C/O KRISTINA T LUPO	44 COOPER ST APT 2	BOSTON	MA	02113
0302536002	102 ENDICOTT ST	BUCCIO NOTARO PHYLLIS	C/O MARIA & PHYLLIS BUCCIO	155 WILLIS AVE	MEDFORD	MA	02155
0302536004	46 COOPER ST #1	CORMIER ROBERT		46 COOPER ST # 1	BOSTON	MA	02113
0302536006	46 COOPER ST #2	RUPP KENNETH S		46 COOPER ST # 2	BOSTON	MA	02113
0302536008	46 COOPER ST #3	TIPLADY NATHANIEL D	C/O NATHANIEL D TIPLADY	46 COOPER ST #3	BOSTON	MA	02113
0302536010	46 COOPER ST #4	NAPPI MICHAEL D		46 COOPER ST # 4	BOSTON	MA	02113
0302537000	98 100 ENDICOTT ST	CARUSO NANCY	C/O NANCY J CARUSO	100 ENDICOTT ST APT 2	BOSTON	MA	02113
0302538000	94 96 ENDICOTT ST	ROBERTO FRANK TS		96 ENDICOTT ST	BOSTON	MA	02113
0302539000	90 92 ENDICOTT ST	NINETY- 92 ENDICOTT ST LLC	C/O 90-92 ENDICOTT ST LLC	879 BEACON ST	BOSTON	MA	02115
0302540000	86 88 ENDICOTT ST	CONIARIS THOMAS DUDLEY	C/O THOMAS D CONIARIS	88 ENDICOTT ST	BOSTON	MA	02113
0302541000	84 ENDICOTT ST	EIGHTY-4 ENDICOTT STREET	C/O ALAN L BARNET	28 MONUMENT CT	CHARLESTOWN	MA	02129
0302541002	84 ENDICOTT ST #1	HEALEY BARBARA C	C/O BARBARA C HEALEY	84 ENDICOTT ST #1	BOSTON	MA	02113
0302541004	84 ENDICOTT ST #2	PILIERE HOPE		84 ENDICOTT ST # 2	BOSTON	MA	02113
0302541006	84 ENDICOTT ST #3	WELLS CHRISTOPHER J		84 ENDICOTT ST	BOSTON	MA	02113
0302542000	82 82A ENDICOTT ST	FRENI MARIA		82 ENDICOTT	BOSTON	MA	02113
0302543000	STILLMAN PL	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0302545000	N WASHINGTON ST	MICHELLE HOLDINGS LLC	C/O MICHELLE HOLDINGS	55 HENSHAW ST	BOSTON	MA	02135
0302545010	S COOPER ST	CITY OF BOSTON		COOPER ST	BOSTON	MA	02113
0302546000	CROSS ST	CITY OF BOSTON		CROSS	BOSTON	MA	02113
0302546010	N WASHINGTON ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0302546020	WS ENDICOTT ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0302562000	BLACKSTONE ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0302573000	136 BLACKSTONE	COMMONWEALTH OF MASS	C/O STATE TRANSPORTATION BLDG	10 PARK PLZ #6160	BOSTON	MA	02116
0302604000	CAMBRIDGE ST	BOSTON REDEVELOPMENT AUTH		CAMBRIDGE ST	BOSTON	MA	02114
0302605000	15 55 NEW SUDBURY ST	UNITED STATES OF AMER		15 NEW SUDBURY	BOSTON	MA	02114
0302617000	CONGRESS ST	BOSTON REDEVELOPMNT AUTH		CONGRESS	BOSTON	MA	02109
0302621000	15 NEW CHARDON	BRICKMAN ONE BOWDOIN LLC	C/O BRICKMAN ONE BOWDOIN LLC	712 FIFTH AVENUE	NEW YORK	NY	10019
0302622000	25 NEW CHARDON	TWENTY 5 NEW CHARDON ST LPS		250 FIRST AV #200	NEEDHAM	MA	02494
0302623000	40 HAWKINS ST	NEW ENGLAND TELEVISION CORP	C/O PAT JASPERR	7 BULFINCH PL	BOSTON	MA	02114
0302624000	30 HAWKINS ST	INTERCONTINENTAL I BULFINCH	C/O INTERNATIONAL I BULFINCH	1270 SOLDIERS FIELD RD	BRIGHTON	MA	02135

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BOSTON, MA

Account Number	Location	Owner	Care Of	Mailing Address	City	ST	Zip
0302625000	HAWKINS ST	BOSTON REDVLPMNT AUTH		HAWKINS	BOSTON	MA	02114
0302626000	40 NEW SUDBURY ST	CITY OF BOSTON		40 NEW SUDBURY	BOSTON	MA	02114
0302627000	NEW SUDBURY ST	BOSTON REDVLPMNT AUTH		NEW SUDBURY	BOSTON	MA	02114
0302628000	65 CAMBRIDGE ST	NEW ENGLAND TEL & TEL CO	C/O PROPERTY TAX DEPT	PO BOX 152206	IRVING	TX	75015
0302640000	25 31 HAWKINS ST	BOSTON EDISON CO MASS	NSTAR ELECTRIC CO PROP TAX	PO BOX #567	NORWOOD	MA	02062
0302641000	33 HAWKINS ST	BOSTON EDISON CO	NSTAR ELECTRIC CO PROP TAX	PO BOX #567	NORWOOD	MA	02062
0302642000	35 HAWKINS ST	CITY OF BOSTON		35 HAWKINS	BOSTON	MA	02114
0302643000	HAWKINS ST	BOSTON REDEVLPMNT AUTH		HAWKINS	BOSTON	MA	02114
0302644000	41 43 HAWKINS ST	CITY OF BOSTON		41 HAWKINS	BOSTON	MA	02114
0302645000	31 NEW CHARDON	THIRTY ONE NEW CHARDON STREE	C/O SHELLY L MCPHEE	31 NEW CHARDON ST	BOSTON	MA	02114
0302646000	NEW CHARDON	BOSTON REDEVLPMNT AUTH		NEW CHARDON	BOSTON	MA	02114
0302647000	BOWKER ST	CITY OF BOSTON		BOWKER	BOSTON	MA	02114
0302700000	50 NEW SUDBURY ST	BULFINCH CONGRESS HOLDINGS	C/O HYM INVESTMENT GROUP LLC	ONE CONGRESS ST	BOSTON	MA	02104
0303308000	HANOVER ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0303324000	BLACKSTONE ST	COMMONWEALTH OF MASS	STATE TRANSP BLDG	10 PARK PLZ	BOSTON	MA	02116
0303337000	7 9 MARSHALL ST	IBRAHAM ABDO		120 BLACKSTONE ST	BOSTON	MA	02109
0303347000	45 55 UNION ST	FIFTY FIVE UNION LLC		45 UNION ST	BOSTON	MA	02108
0303350000	145 149 HANOVER ST	BEN SHERI TS	C/O VALERIE POST	142 MARLBOROUGH ST	BOSTON	MA	02116

MAP TITLE



Department 1

Department 2

N
W E
S

Appendix G
Metes and Bounds Description

■

Legal Description – Area 1

A certain parcel of land located between Sudbury Street, New Chardon Street, Bowker Street and John F. Fitzgerald Surface Road in the City of Boston, in the County of Suffolk and the Commonwealth of Massachusetts bounded and described as follows:

Beginning at the intersection of the centerlines of New Chardon Street and Bowker Street, said point being the northwesterly corner of the parcel described herein; thence

N 68°07'48" E	a distance of One Hundred Forty Two and Forty Seven Hundredths feet (142.47') to a point; thence
Easterly	and curving to the right along the arc of a curve having a radius of One Thousand Ninety Six and Fifty Six Hundredths (1096.56'), a length of One Hundred Eight and Ninety Hundredths (108.90') to a point the last two (2) courses by the centerline of New Chardon Street; thence
S 71°04'42" E	a distance of One Hundred Ninety One and Thirty One Hundredths feet (191.31') to a point; thence
Southeasterly	and curving to the right along the arc of a curve having a radius of feet Five Hundred Five and Forty Hundredths (505.40'), a length of Two Hundred Sixty and Sixty Nine Hundredths (260.69') to a point; two (2) courses by the southwesterly line of Merrimac Street; thence
S 56°26'19" W	a distance of Three Hundred Forty Eight and Seventy Five Hundredths feet (348.75') by the centerline of Sudbury Street to a point; thence
N 33°33'41" W	a distance of Forty and No Hundredths feet (40.00') to a point; thence
N 45°58'13" W	a distance of Seventy Seven and Fifty Hundredths feet (77.50') to a point, being the southeasterly corner of Bowker Street; thence
S 41°19'46" W	a distance of Twenty Two and Fifty Three Hundredths feet (22.53') to a point, the last two (2) courses by land now or formerly of the Boston Redevelopment Authority; thence
N 45°58'13" W	a distance of Three Hundred Forty Three and Ninety Two Hundredths feet (343.92') by the centerline of Bowker Street to the point of beginning.

The above described parcel contains 129,744 sq. ft. or 2.979 acres more or less.

Legal Description – Proposed Transfer Parcel

A certain parcel of land located between Sudbury Street, New Chardon Street, Merrimack Street and John F. Fitzgerald Surface Road in the City of Boston, in the County of Suffolk and the Commonwealth of Massachusetts bounded and described as follows:

Beginning at a point on the westerly sideline of the SHLO #7737 and the projected centerline of New Chardon Street, said point being the southeast corner of the parcel described herein; thence

Southwesterly	and curving to the right along the arc of a curve having a radius of One Thousand Two Hundred Forty and No Hundredths feet (1240.00'), a length of Two Hundred Twenty Nine and Eighty Seven Hundredths feet (229.87') and a chord length of Two Hundred Twenty Nine and Fifty Four Hundredths feet (229.54') with a chord bearing of S 61°39'41" W by the centerline of New Chardon Street; thence
N 50°15'51" E	a distance of Two Hundred Thirty One and Sixty Six Hundredths feet (231.66') through New Chardon Street to a point; thence
S 12°10'47" E	a distance of Twenty Four and Forty Two Hundredths feet (24.42') to a point; thence
S 50°50'39" E	a distance of Twenty Four and Sixteen Hundredths feet (24.16') to the point of beginning. The last two (2) courses by the westerly line of State Highway Layout #7737

The above described parcel contains 5,885 sq. ft. or 0.135acres.

Legal Description – Area 2

A certain parcel of land located between Sudbury Street, New Chardon Street, Merrimack Street and John F. Fitzgerald Surface Road in the City of Boston, in the County of Suffolk and the Commonwealth of Massachusetts bounded and described as follows:

Beginning at a stone bound on the westerly line of John F. Fitzgerald Surface Road, being State Highway Layout 7737, and the easterly end of Sudbury Street, said point being the southeast corner of the parcel described herein; thence

S 33°35'08" E	a distance of Twenty Four and Fifteen Hundredths feet (24.15') to a point; thence
S 56°26'19" W	a distance of One Hundred Sixteen and Seventy Hundredths feet (116.70') to a point; thence
N 33°33'41" W	a distance of Twelve and Fifty One Hundredths feet (12.51') to a point; thence
S 56°26'19" W	a distance of Four and Six Hundredths feet (4.06') by the northerly line of Sudbury Street to a point, the last four (4) courses through Sudbury Street;; thence
Northwesterly	and curving to the left along the arc of a curve having a radius of Six Hundred Five and Forty Hundredths feet (605.40'), a length of Three Hundred Seventy Two and Eighty One Hundredths feet (372.81') by the northeasterly line of Merrimac Street to a point; thence
Northeasterly	and curving to the left along the arc of a curve having a radius of One Thousand Two Hundred Forty and No Hundredths feet (1240.00'), a length of One Hundred Four and Thirty Seven Hundredths feet (104.37') and a chord length of One Hundred Four and Thirty Four Hundredths feet (104.34') with a chord bearing of N 69°23'00" E by the centerline of New Chardon Street; thence
N 50°15'51" E	a distance of Two Hundred Thirty One and Sixty Six Hundredths feet (231.66') through New Chardon Street to a point; thence
S 12°10'47" E	a distance of Twenty Four and Forty Two Hundredths feet (24.42') to a point; thence
S 50°50'39" E	a distance of One Hundred Forty Six and Fifty Four Hundredths feet (146.54') to a point; thence
S 26°16'29" E	a distance of Eighty Eight and Eight Hundredths feet (88.08') to a point; thence
S 04°03'21" E	a distance of Eighty Five and Forty Hundredths feet (85.40') to a point; thence
S 56°24'52" W	a distance of Forty One and Seventy Four Hundredths feet (41.74'), to the point of beginning. The last five (5) courses by the westerly line of State Highway Layout 7737

The above described parcel contains 80,205 sq. ft. or 1.841acres more or less.

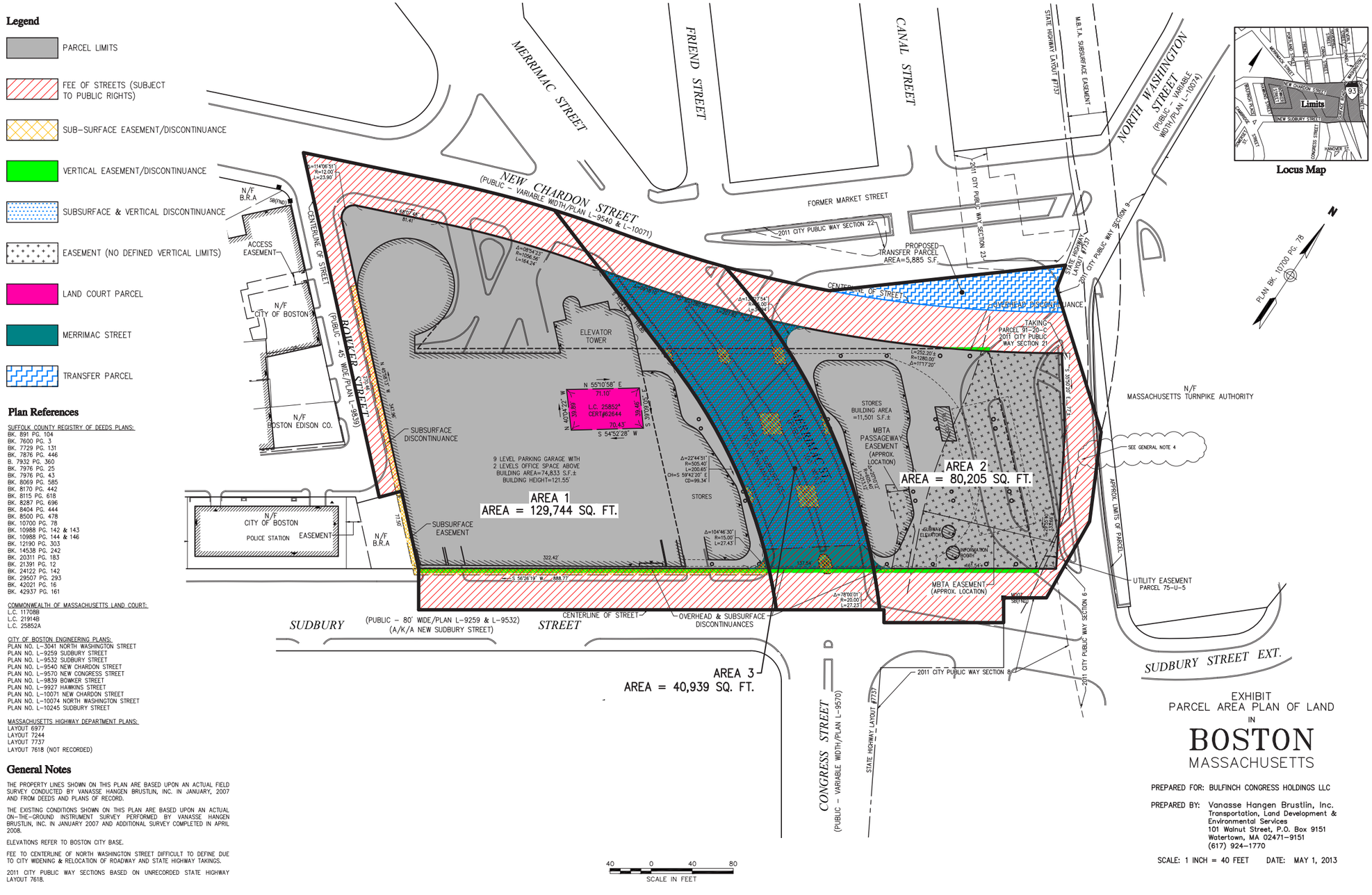
Legal Description – Area 3

A certain parcel of land located between Sudbury Street, New Chardon Street, Merrimack Street and John F. Fitzgerald Surface Road in the City of Boston, in the County of Suffolk and the Commonwealth of Massachusetts bounded and described as follows:

Beginning at a point on the centerline of Sudbury Street, being S 50°55'43" W a tie distance of One Hundred Twenty One and Thirty One Hundredths feet (121.31') from a stone bound on the westerly line of John F. Fitzgerald Surface Road, being State Highway Layout 7737, and the easterly end of Sudbury Street, said point being the southeast corner of the parcel described herein; thence

S 56°26'19" W	a distance of One Hundred and Eighty One Hundredths feet (100.81') by the centerline of Sudbury Street to a point; thence
Northwesterly	and curving to the left along the arc of a curve having a radius of Five Hundred Five and Forty Hundredths feet (505.40'), a length of Two Hundred Sixty and Sixty Nine Hundredths feet (260.69') and a chord length of Two Hundred Fifty Seven and Eighty One Hundredths feet (257.81') with a chord bearing of N 56°18'09" W to a point; thence
N 71°04'42" W	a distance of One Hundred Ninety One and Thirty One Hundredths feet (191.31') to a point, the last two (2) courses by the southwesterly line of Merrimac Street; thence
Easterly	and curving to the right along the arc of a curve having a radius of One Thousand Ninety Six and Fifty Six Hundredths feet (1096.56'), a length of Sixty One and Fifty Six Hundredths feet (61.56') and a chord length of Sixty One and Fifty Five Hundredths feet (61.55') with a chord bearing of N 75°25'42" E to a point; thence
Easterly	and curving to the left along the arc of a curve having a radius of One Thousand Two Hundred Forty and No Hundredths feet (1240.00'), a length of One Hundred Thirteen and Forty Five Hundredths feet (113.45) to a point, the last two (2) courses by the centerline of New Chardon Street; thence
Southeasterly	and curving to the right along the arc of a curve having a radius of Six Hundred Five and Forty Hundredths feet (605.40'), a length of Three Hundred Seventy Two and Eighty One Hundredths feet (372.81') and a chord length of Three Hundred Sixty Six and Ninety Five Hundredths feet (366.95') with a chord bearing of S 57°50'42" E by the northeasterly line of Merrimac Street to the point of beginning.

The above described parcel contains 40,939 sq. ft. or 0.940 acres more or less.



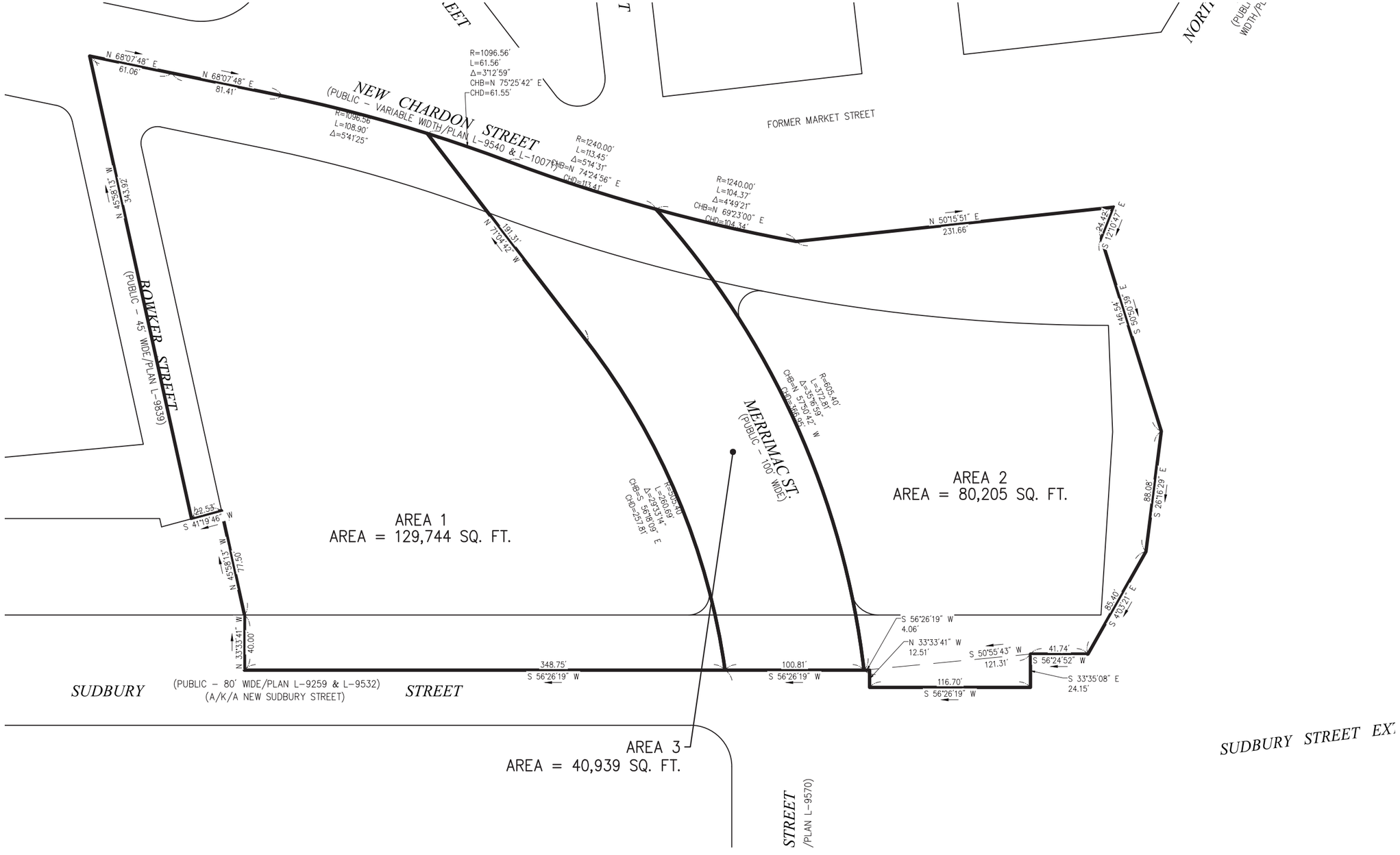
Redevelopment of Government Center Garage
Boston, MA

Figure G-1

Project Development Area

THE HYM INVESTMENT GROUP, LLC

Vanasse Hangen Brustlin, Inc.



Redevelopment of Government Center Garage
Boston, MA

Figure G-2

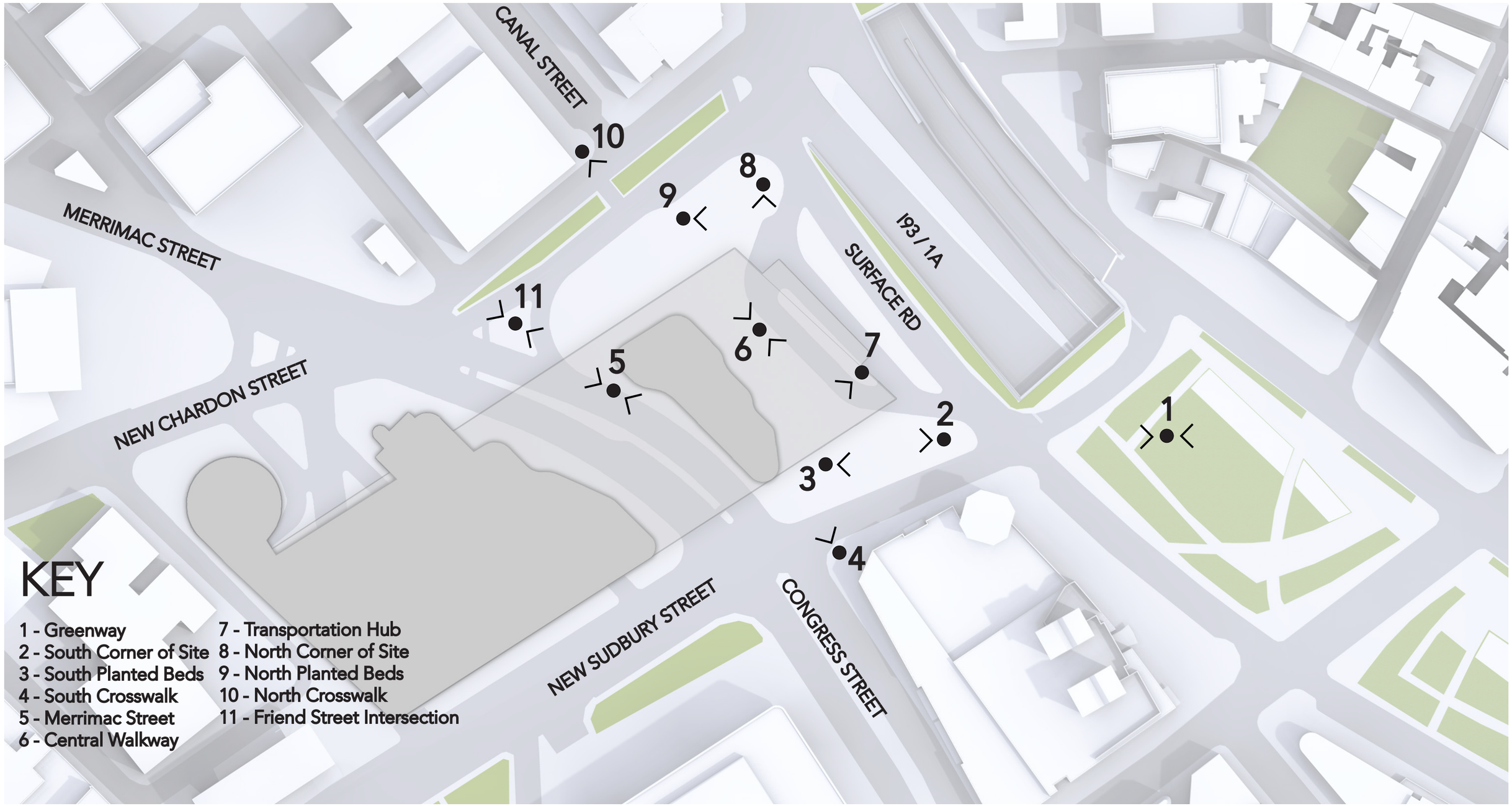
Project Development Area - Metes and Bounds

THE HYM INVESTMENT GROUP, LLC

VHB Vanasse Hangen Brustlin, Inc.

Appendix H
Supplemental Graphics

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Redevelopment of Government Center Garage
Boston, MA

Figure H.1a

Context Photos - Key Plan

THE HYM INVESTMENT GROUP LLC cbt

1.Greenway

Morning



8:00am



9:00am



10:00am



11:00am

Afternoon



1:00pm



2:00pm



3:00pm



4:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1b

Context Photos - Greenway
(August)

2. South Corner of Site

Morning



8:00am



9:00am



10:00am



11:00am

Afternoon



2:00pm



3:00pm



4:00pm



5:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1c

Context Photos - South Corner of Site
(August)

THE HYM INVESTMENT GROUP, LLC cbt

3. South Planted Beds

Morning



8:00am



9:00am



10:00am



11:00am

Afternoon



2:00pm



3:00pm



4:00pm



5:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1d

Context Photos - South Planted Beds
(August)

THE HYM INVESTMENT GROUP LLC cbt

4. South Crosswalk



8:00am



9:00am



11:00am



12:00pm



5:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1e

Context Photos - South Crosswalk
(August)

5. Congress Street



1:00pm



2:00pm



3:00pm



4:00pm



5:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1f

Context Photos - Congress Street
(August)

6. Central Walkway



8:00am



9:00am



12:00pm



2:00pm



4:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1g

Context Photos - Central Walkway
(August)

7. Transportation Hub

Morning



9:00am



10:00am



11:00am



12:00pm

Afternoon



2:00pm



3:00pm



4:00pm



5:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1h

Context Photos - Transportation Hub
(August)

THE HYM INVESTMENT GROUP, LLC cbt

8. North Corner of Site

Morning



8:00am



9:00am



10:00am



11:00am

Afternoon



2:00pm



3:00pm



4:00pm



5:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1i

Context Photos - North Corner of Site
(August)

9. North Planted Beds



10:00am



12:00pm



2:00pm



4:00pm



5:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1j

Context Photos - North Planted Beds
(August)

10. North Crosswalk

Morning



8:00am



9:00am



10:00am



11:00am

Afternoon



2:00pm



3:00pm



4:00pm



5:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1k

Context Photos - North Planted Beds
(August)

THE HYM INVESTMENT GROUP, LLC cbt

11. Friend Street Intersection



1:00pm



2:00pm



3:00pm



4:00pm

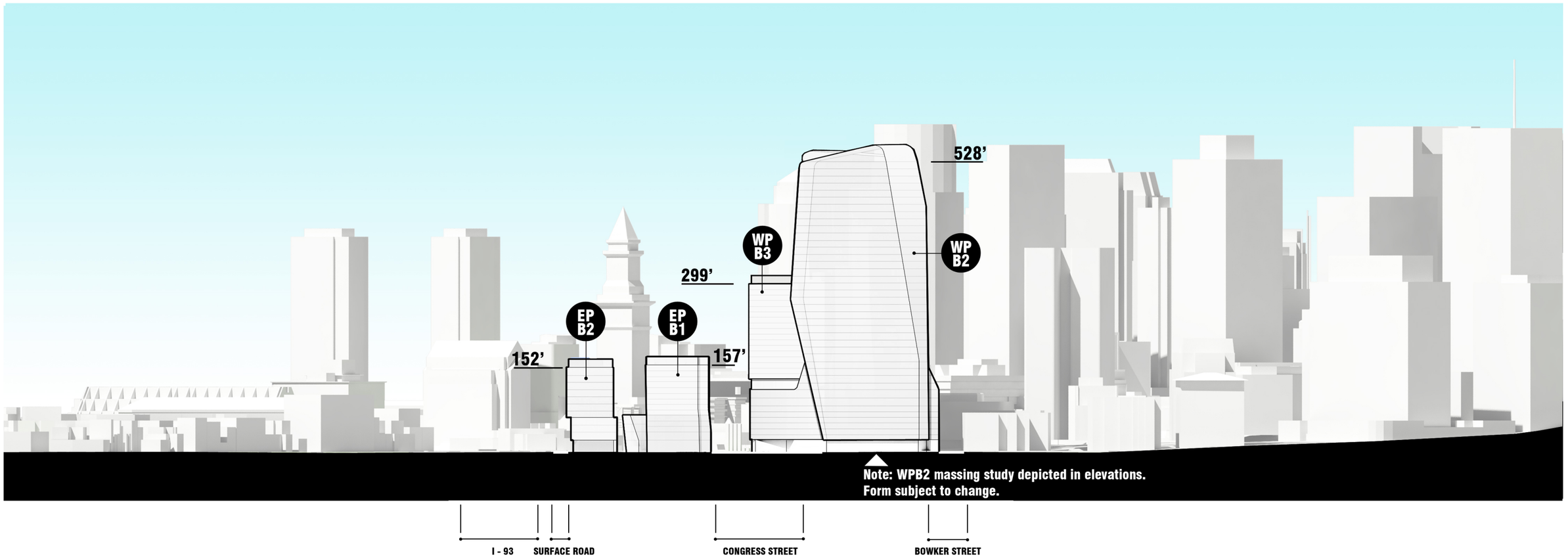


5:00pm

Redevelopment of Government Center Garage
Boston, MA

Figure H.1l

Context Photos - Friend Street Intersection
(August)

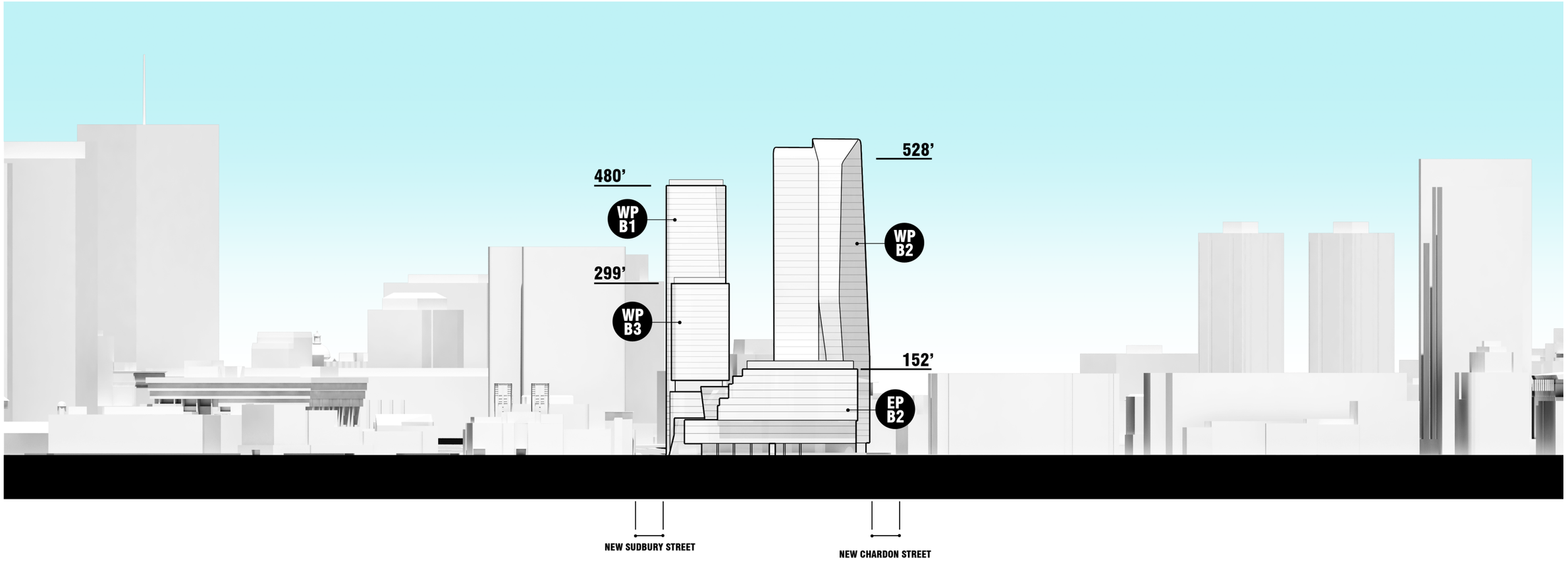


Redevelopment of Government Center Garage
Boston, MA

Figure H.2a

North Elevation

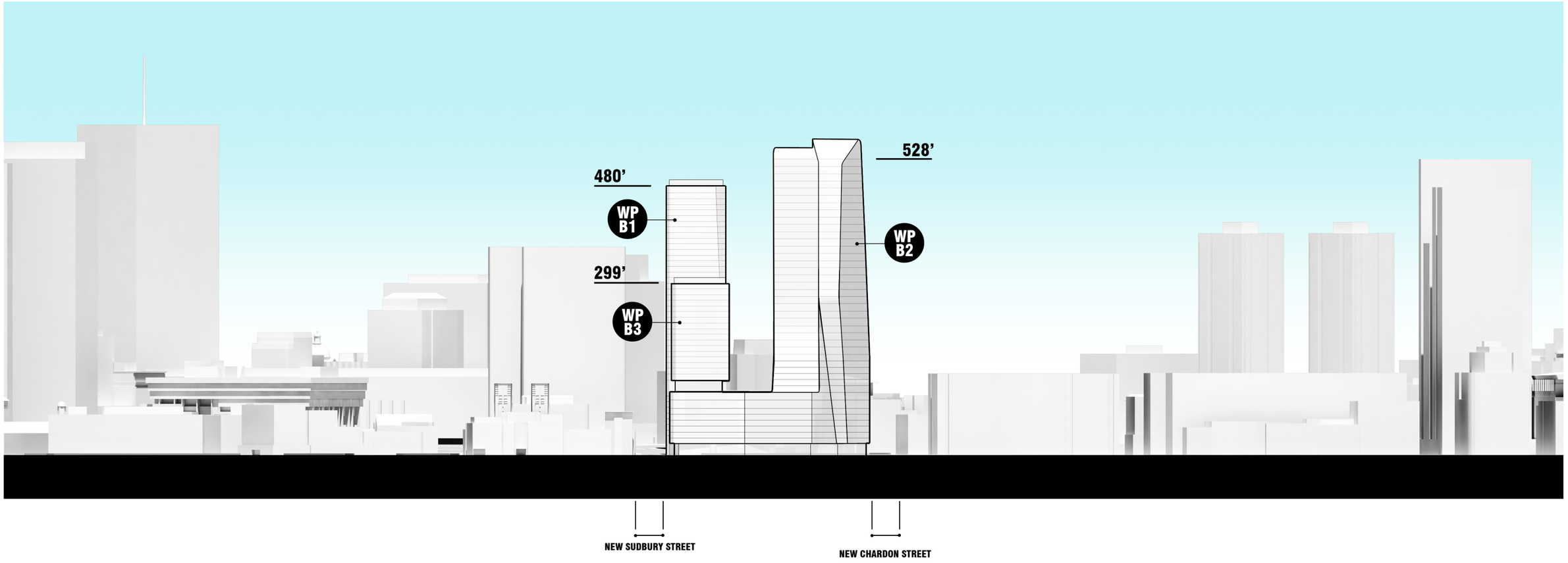
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Redevelopment of Government Center Garage
Boston, MA

Figure H.2b

East Elevation from Rose Kennedy Greenway

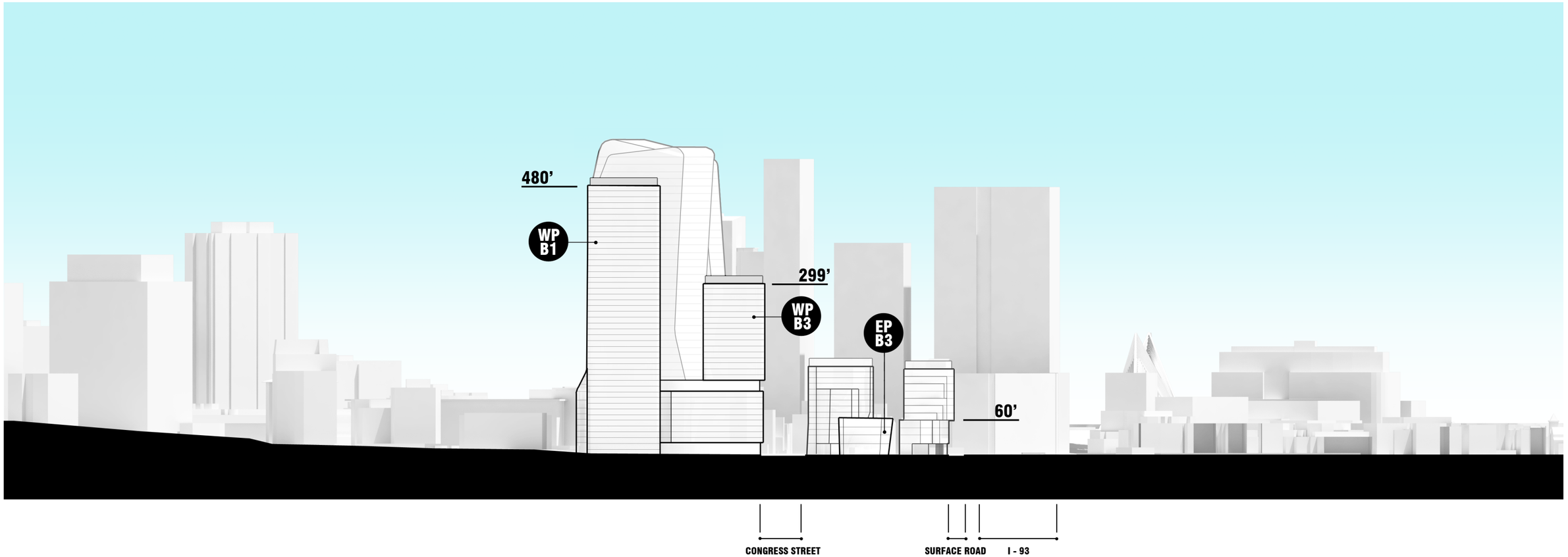


Redevelopment of Government Center Garage
Boston, MA

Figure H.2c

East Elevation from Congress Street

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Redevelopment of Government Center Garage
Boston, MA

Figure H.2d

South Elevation

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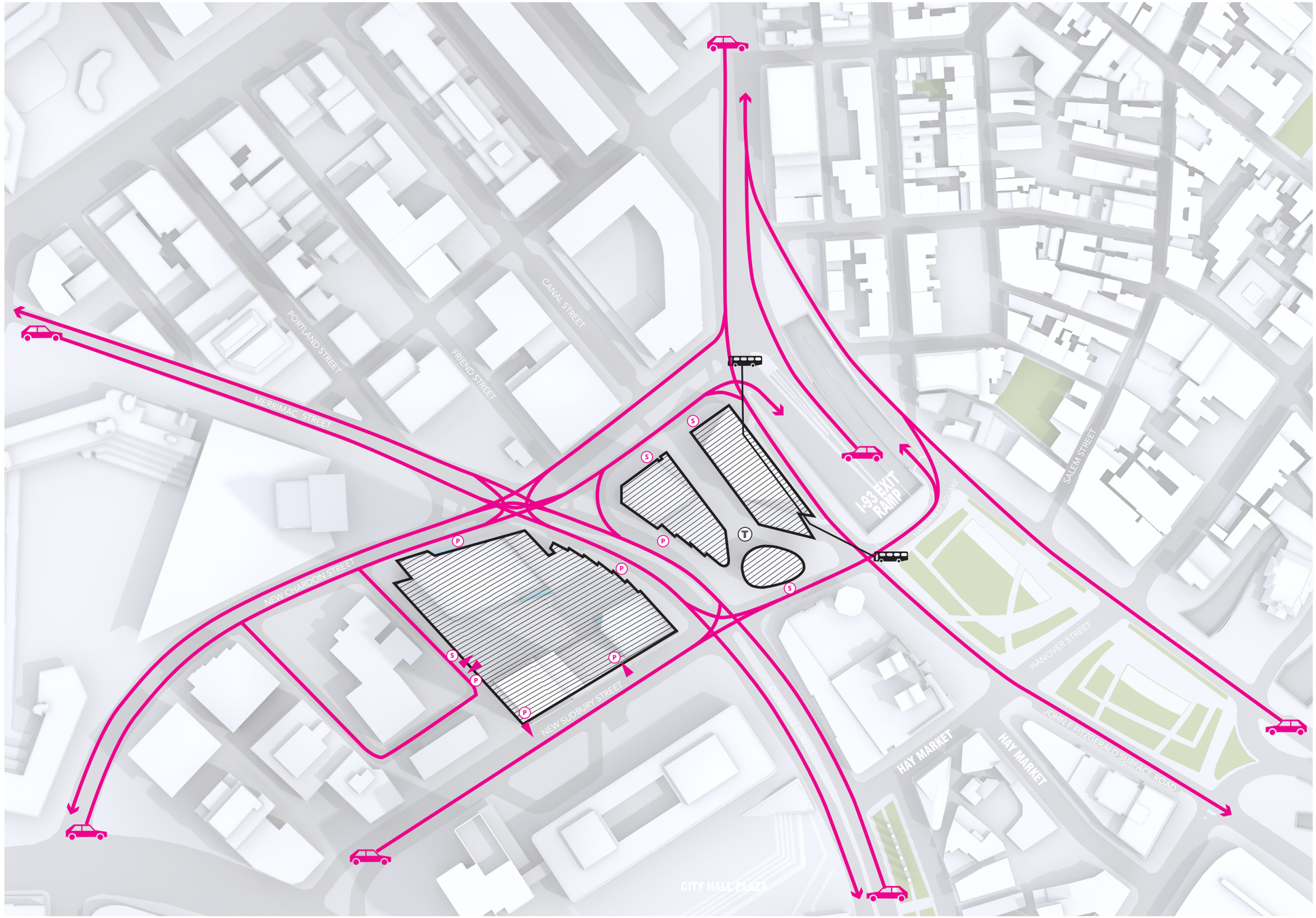
Redevelopment of Government Center Garage
Boston, MA

Figure H.3

Pedestrian Circulation

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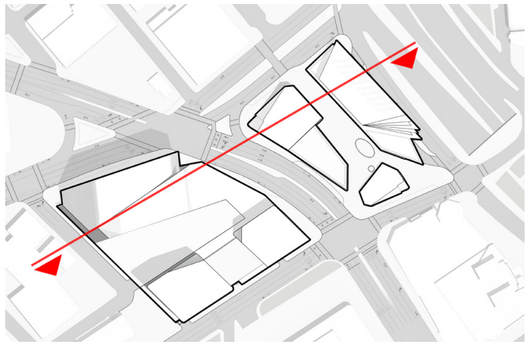
cbt

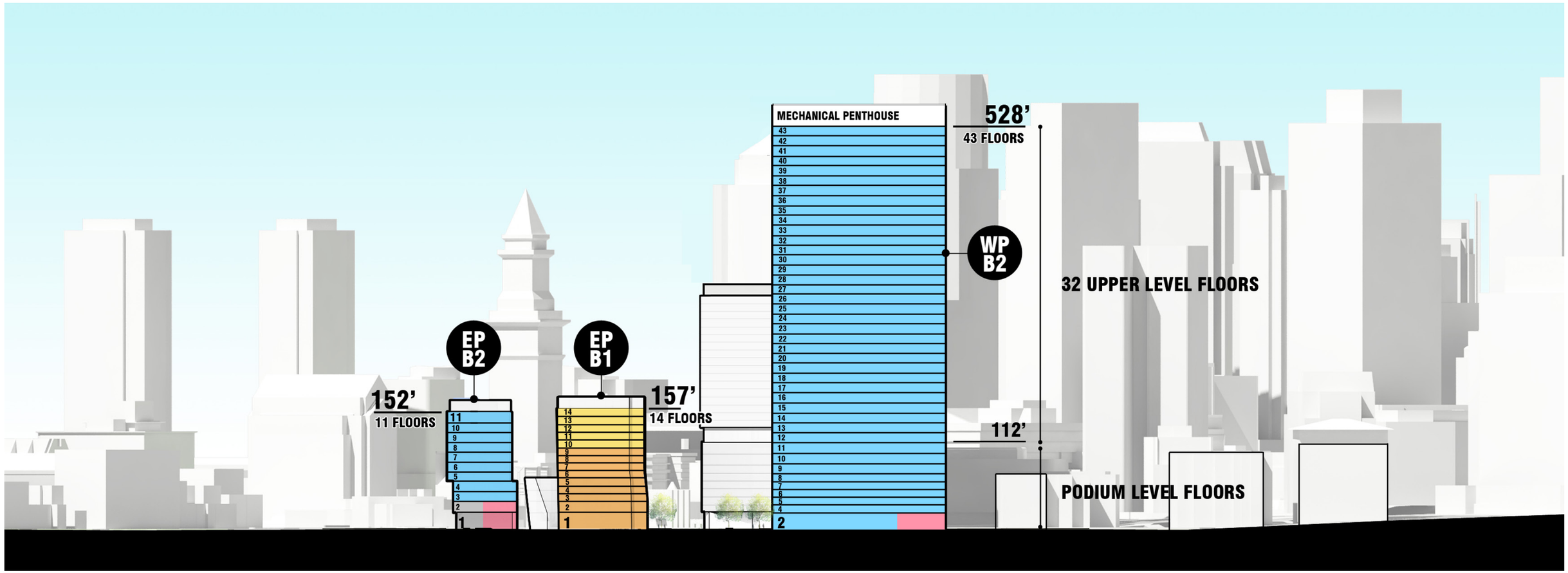


Redevelopment of Government Center Garage
Boston, MA

Figure H.4

Vehicular Circulation





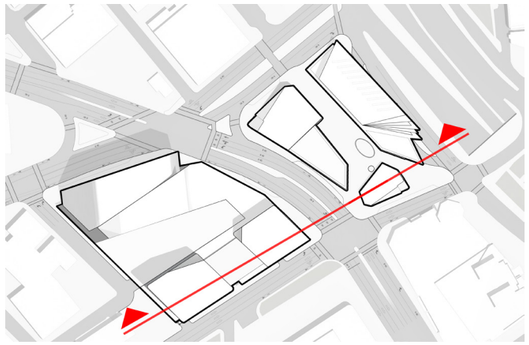
Redevelopment of Government Center Garage
Boston, MA

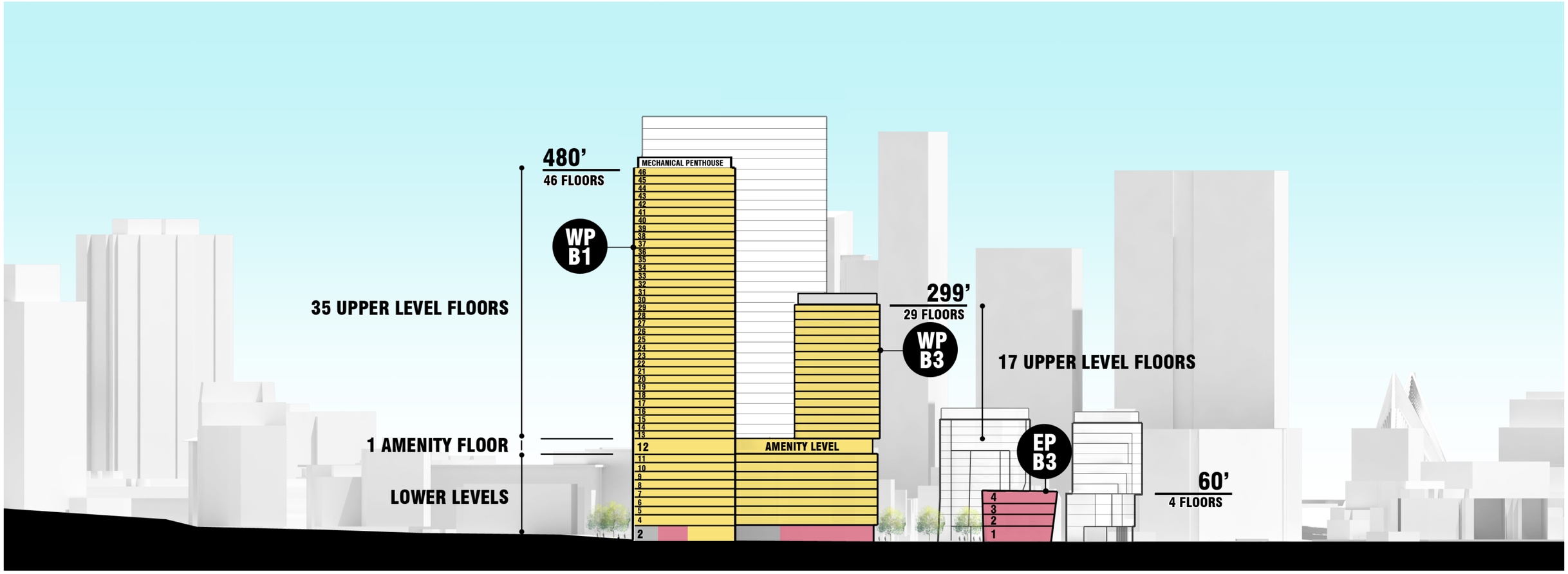
Figure H.5a

Site Section Looking South

THE HYM INVESTMENT GROUP LLC

cbt



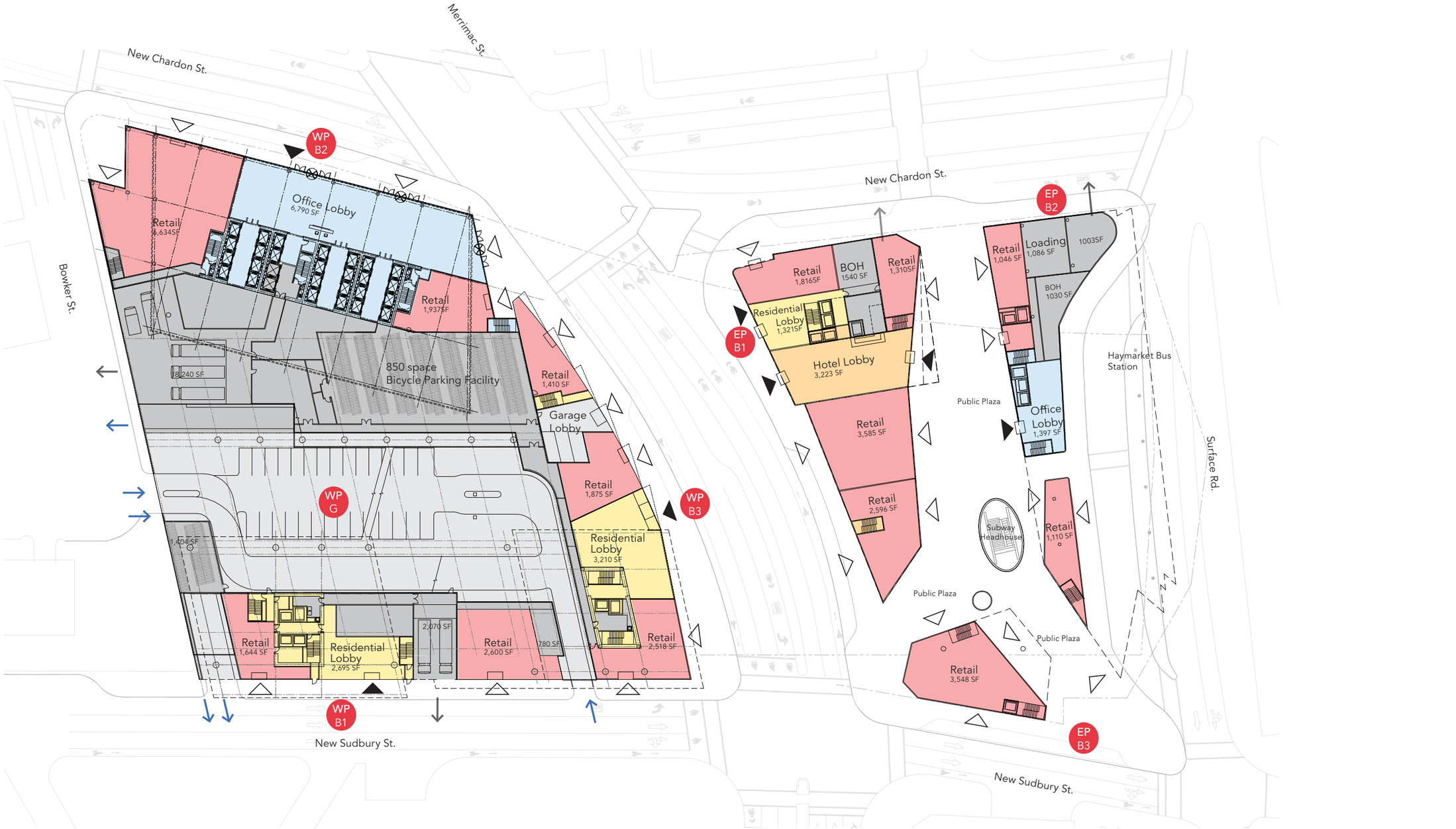


Redevelopment of Government Center Garage
Boston, MA

Figure H.5b

Site Section Looking North

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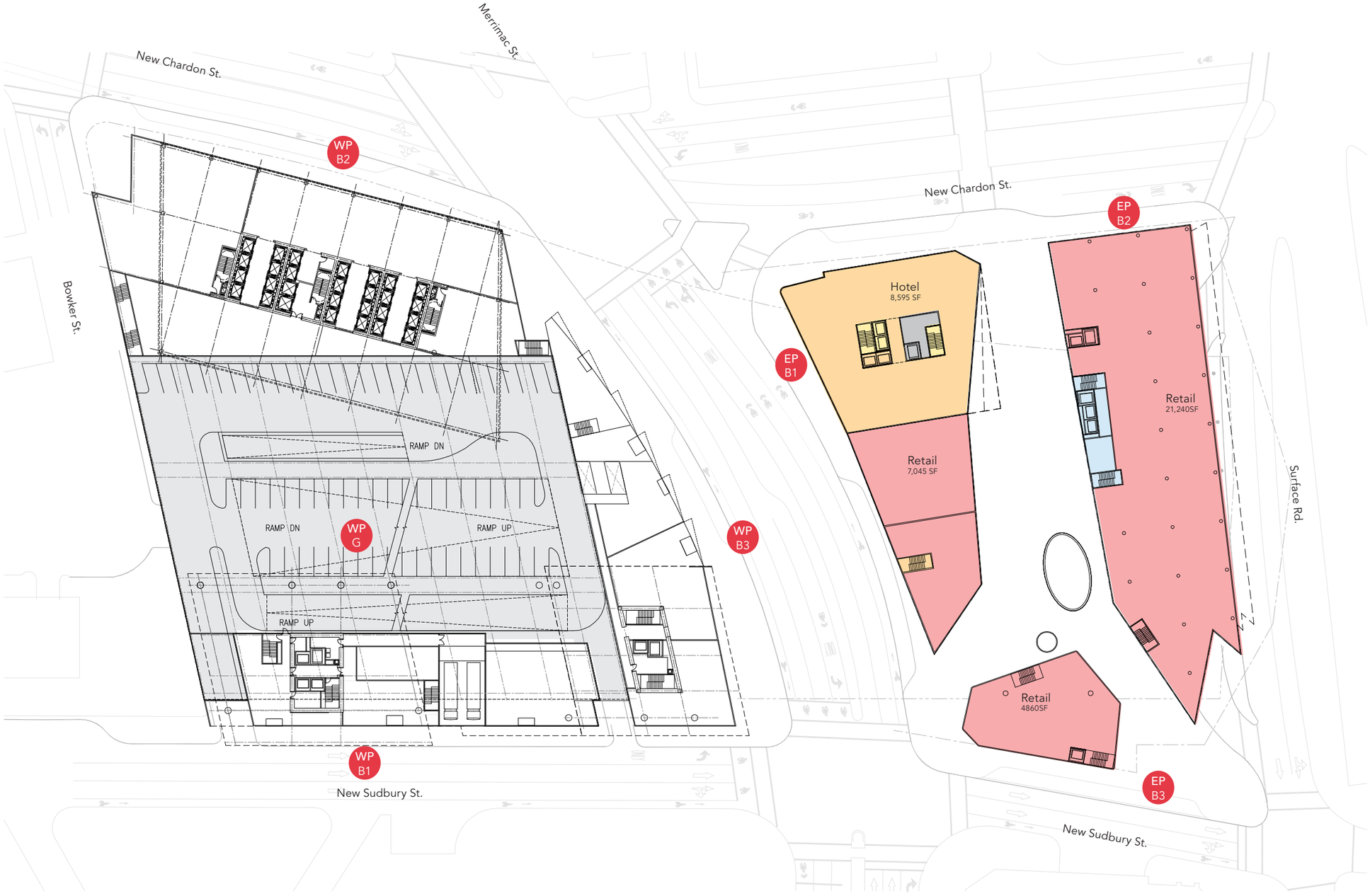
LEGEND: Residential | Hotel | Office | Retail | Parking | Back of House/ Service | Green Roof (Not Occupied) | Landscaped Area | Primary Pedestrian Entry | Secondary Pedestrian Entry | Cars Entry/ Exit | Service Vehicles Entry/Exit | XX YY Parcel ID & Building ID | 0 10' 20' 50' 100' N

Redevelopment of Government Center Garage
Boston, MA

Figure H.6a

Plan - Floor 02

THE HYM INVESTMENT GROUP, LLC cbt



LEGEND

Residential | Hotel | Office | Retail | Parking | Back of House/ Service | Green Roof (Not Occupied) | Landscaped Area | Primary Pedestrian Entry | Secondary Pedestrian Entry | Cars Entry/ Exit | Service Vehicles Entry/Exit | XX YY Parcel ID & Building ID

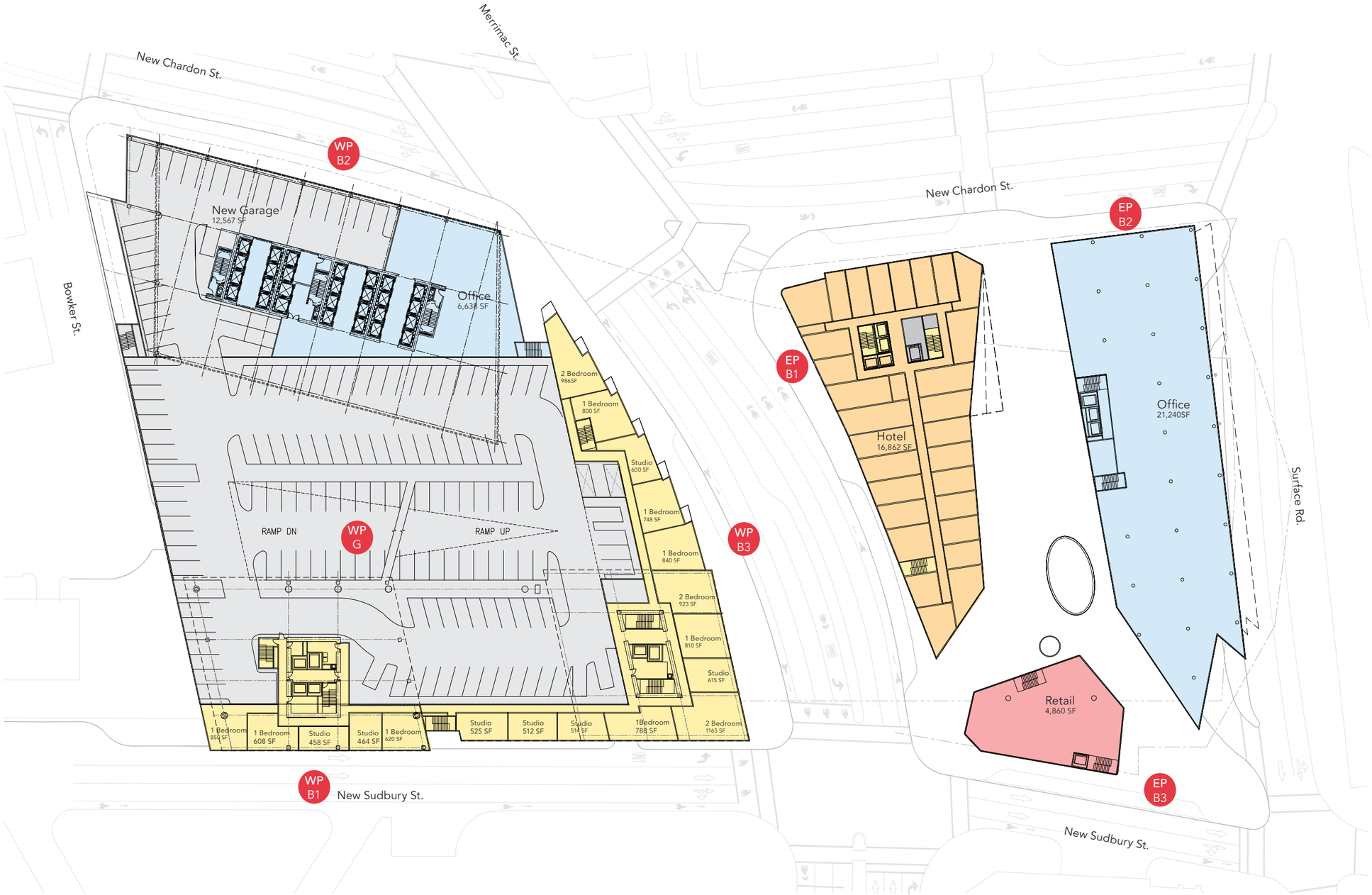
0 10' 20' 50' 100' N

Redevelopment of Government Center Garage
Boston, MA

Figure H.6b

Plan - Floor 03

THE HYM INVESTMENT GROUP LLC cbt



LEGEND

Residential | Hotel | Office | Retail | Parking | Back of House/ Service | Green Roof (Not Occupied) | Landscaped Area | Primary Pedestrian Entry | Secondary Pedestrian Entry | Cars Entry/ Exit | Service Vehicles Entry/Exit | XX YY Parcel ID & Building ID

0 10' 20' 50' 100' N

Redevelopment of Government Center Garage
Boston, MA

Figure H.6c

Plan - Floor 04

THE HYM INVESTMENT GROUP LLC cbt



LEGEND

Residential | Hotel | Office | Retail | Parking | Back of House/ Service | Green Roof (Not Occupied) | Landscaped Area | Primary Pedestrian Entry | Secondary Pedestrian Entry | Cars Entry/ Exit | Service Vehicles Entry/Exit | XX YY Parcel ID & Building ID | 0 10' 20' 50' 100' N

Redevelopment of Government Center Garage
Boston, MA

Figure H.6d

Plan - Floor 05

THE HYM INVESTMENT GROUP LLC cbt



LEGEND Residential · Hotel · Office · Retail · Parking · Back of House/Service · Green Roof (Not Occupied) · Landscaped Area · Primary Pedestrian Entry · Secondary Pedestrian Entry · Cars Entry/Exit · Service Vehicles Entry/Exit · XX YY Parcel ID & Building ID · 0 10' 20' 50' 100' N

Redevelopment of Government Center Garage
Boston, MA

Figure H.6e

Plan - Floor 06-07

THE HYM INVESTMENT GROUP LLC cbt



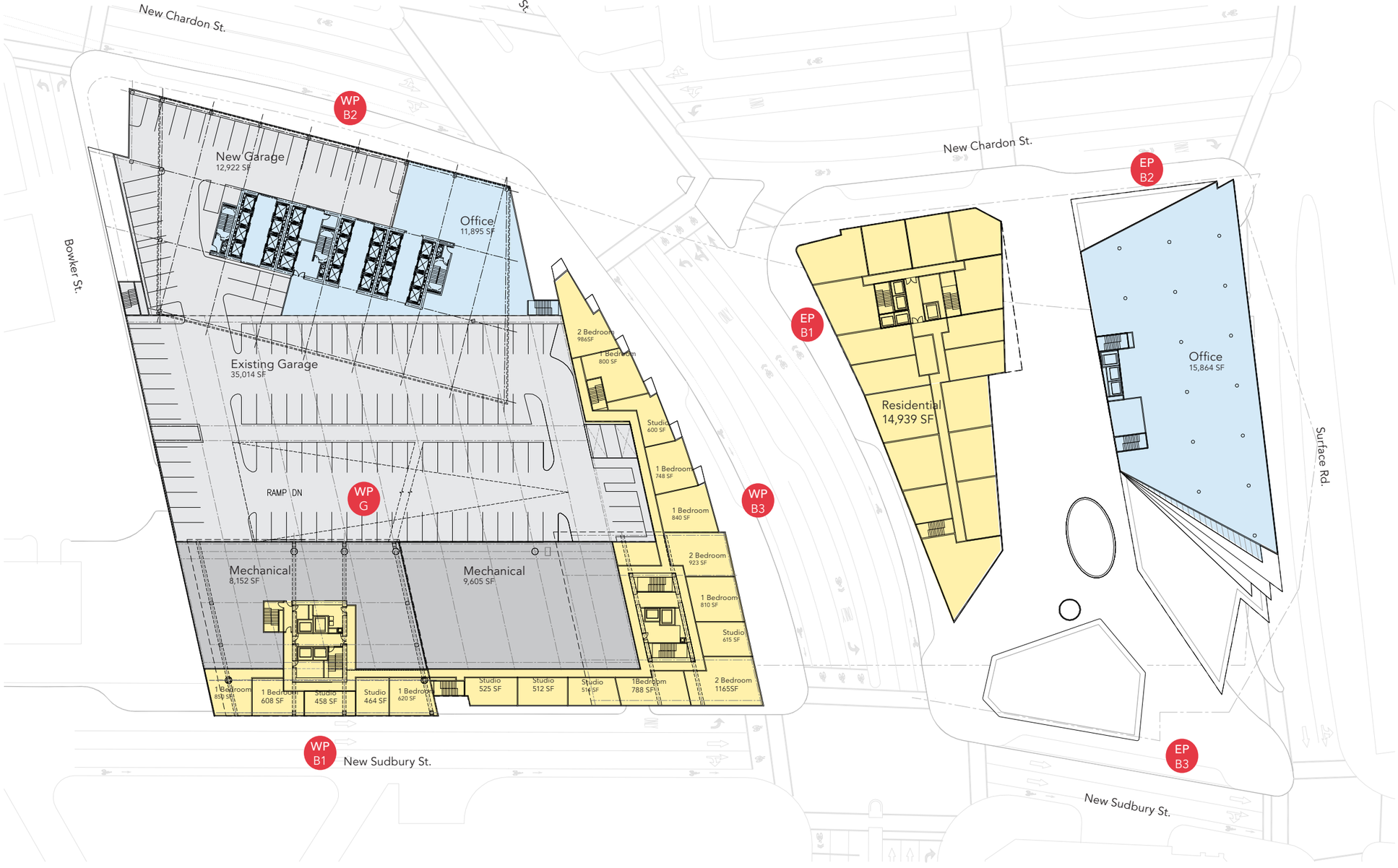
Redevelopment of Government Center Garage
Boston, MA

Figure H.6

Plan - Floor 08-09

THE HYM INVESTMENT GROUP LLC

cbt



LEGEND: Residential; Hotel; Office; Retail; Parking; Back of House/ Service; Green Roof (Not Occupied); Landscaped Area; Primary Pedestrian Entry; Secondary Pedestrian Entry; Cars Entry/ Exit; Service Vehicles Entry/Exit; XX YY Parcel ID & Building ID

0 10' 20' 50' 100' N

Redevelopment of Government Center Garage
Boston, MA

Figure H.6g

Plan - Floor 10

THE HYM INVESTMENT GROUP LLC cbt



LEGEND: Residential; Hotel; Office; Retail; Parking; Back of House/ Service; Green Roof (Not Occupied); Landscaped Area; Primary Pedestrian Entry; Secondary Pedestrian Entry; Cars Entry/ Exit; Service Vehicles Entry/Exit; XX YY Parcel ID & Building ID; 0 10' 20' 50' 100' N

Redevelopment of Government Center Garage
Boston, MA

Figure H.6h

Plan - Floor 11

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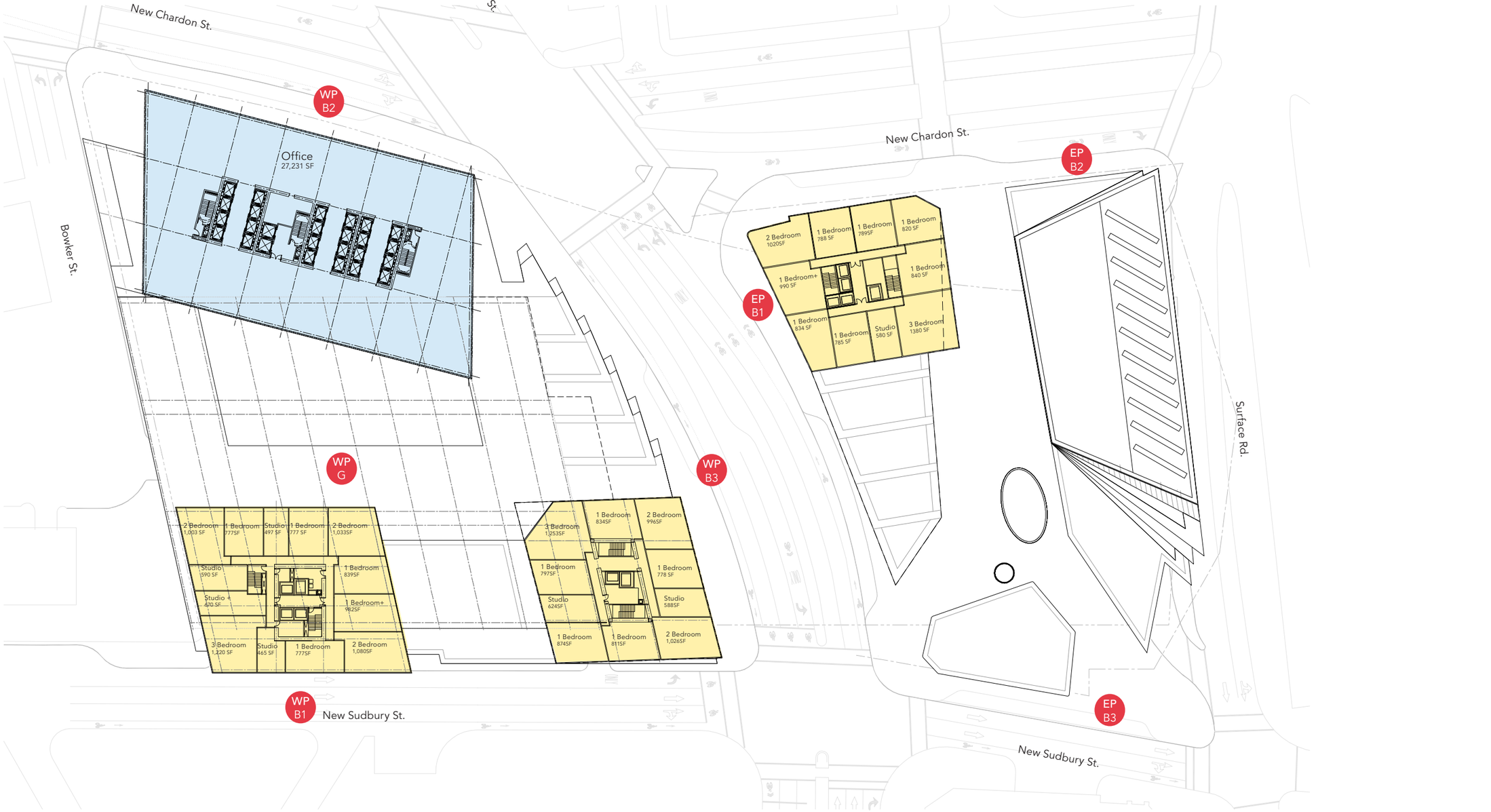


Redevelopment of Government Center Garage
Boston, MA

Figure H.6i

Plan - Floor 12-13

THE HYM INVESTMENT GROUP LLC cbt



LEGEND: Residential; Hotel; Office; Retail; Parking; Back of House/ Service; Green Roof (Not Occupied); Landscaped Area; Primary Pedestrian Entry; Secondary Pedestrian Entry; Cars Entry/ Exit; Service Vehicles Entry/Exit; XX YY Parcel ID & Building ID; 0 10' 20' 50' 100' N

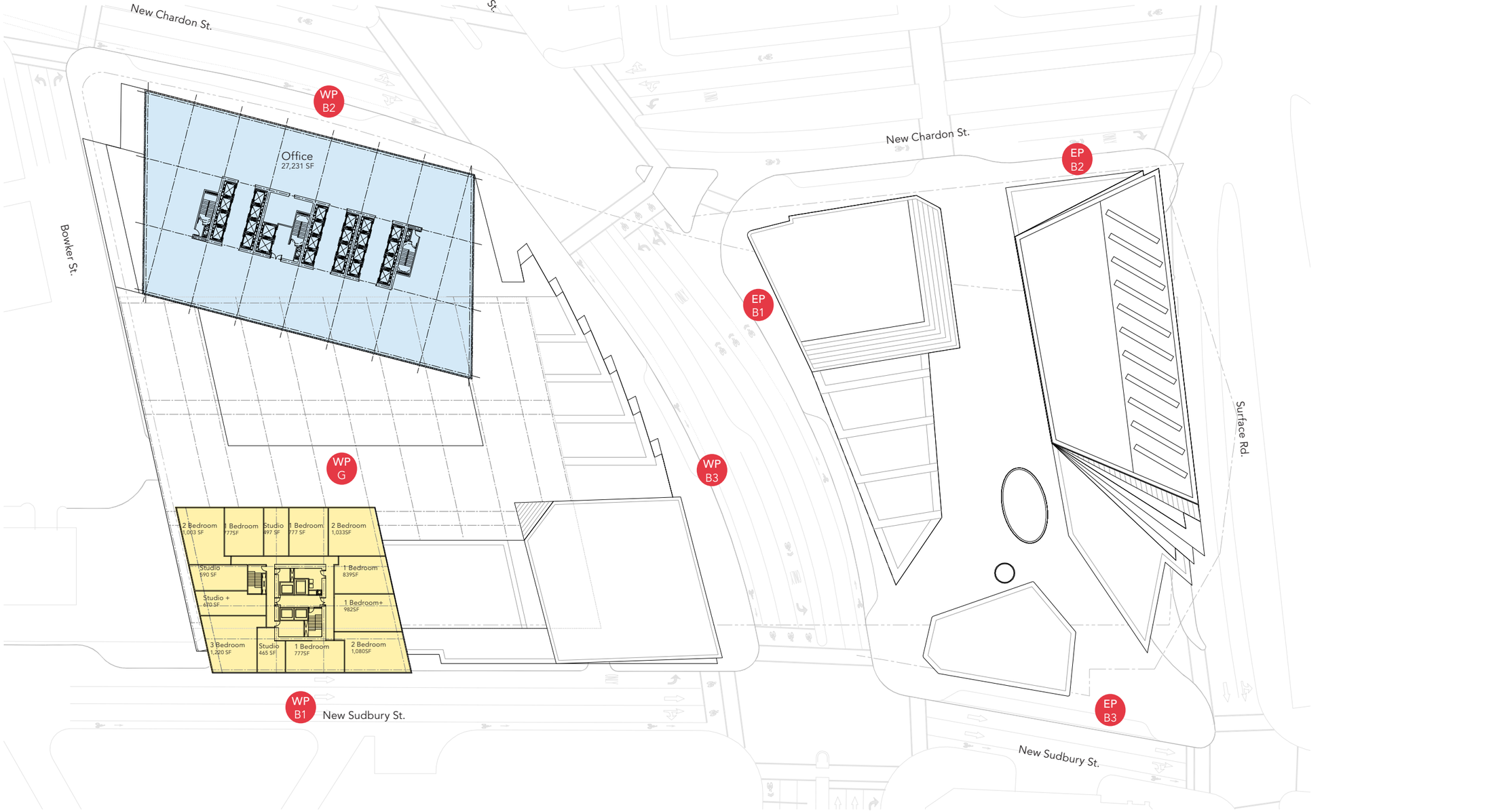
Redevelopment of Government Center Garage
Boston, MA

Figure H.6j

Plan - Floor 14-29

THE HYM INVESTMENT GROUP, LLC

cbt



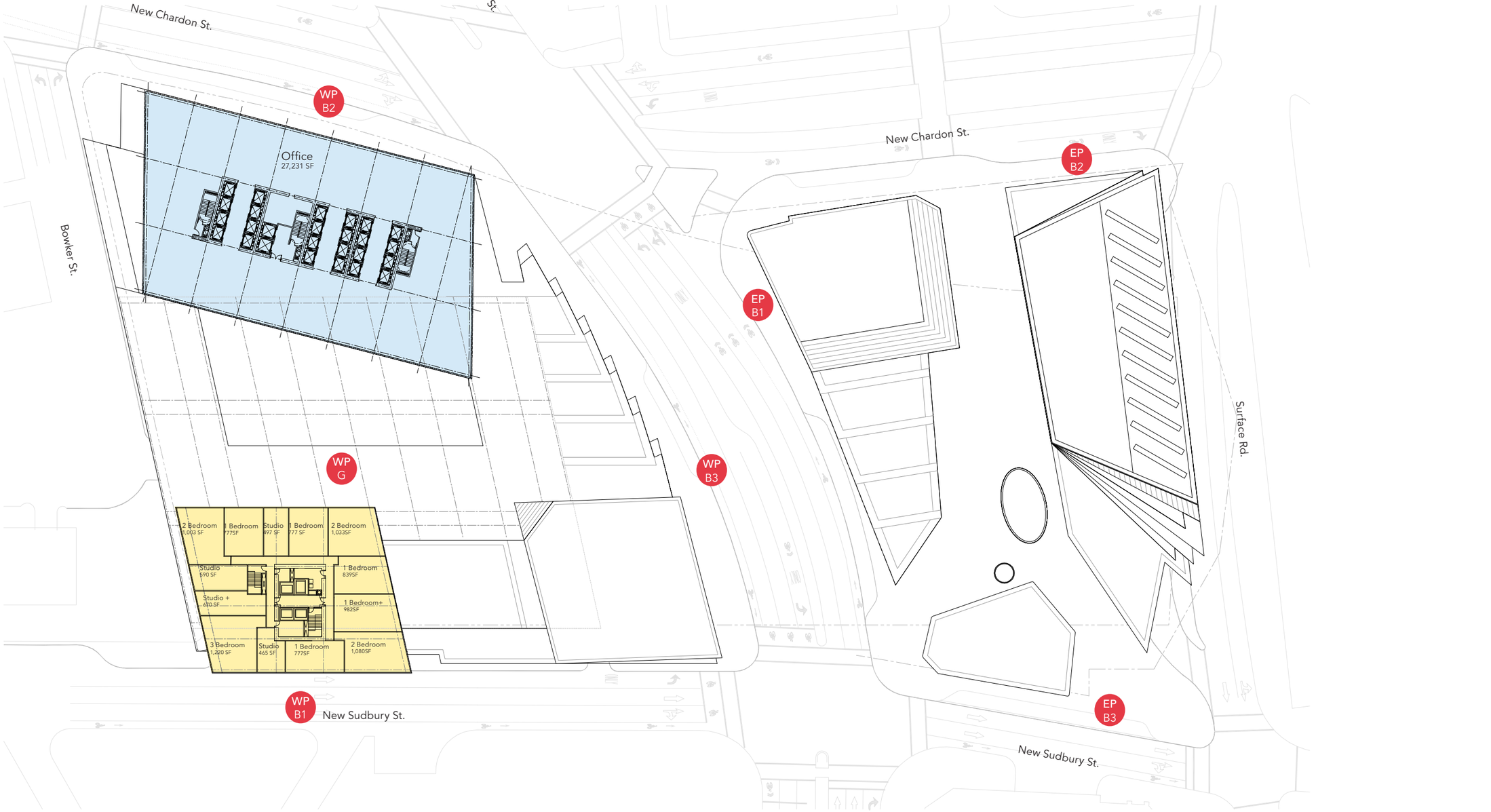
Redevelopment of Government Center Garage
Boston, MA

Figure H.6k

Plan - Floor 30-45

THE HYM INVESTMENT GROUP, LLC

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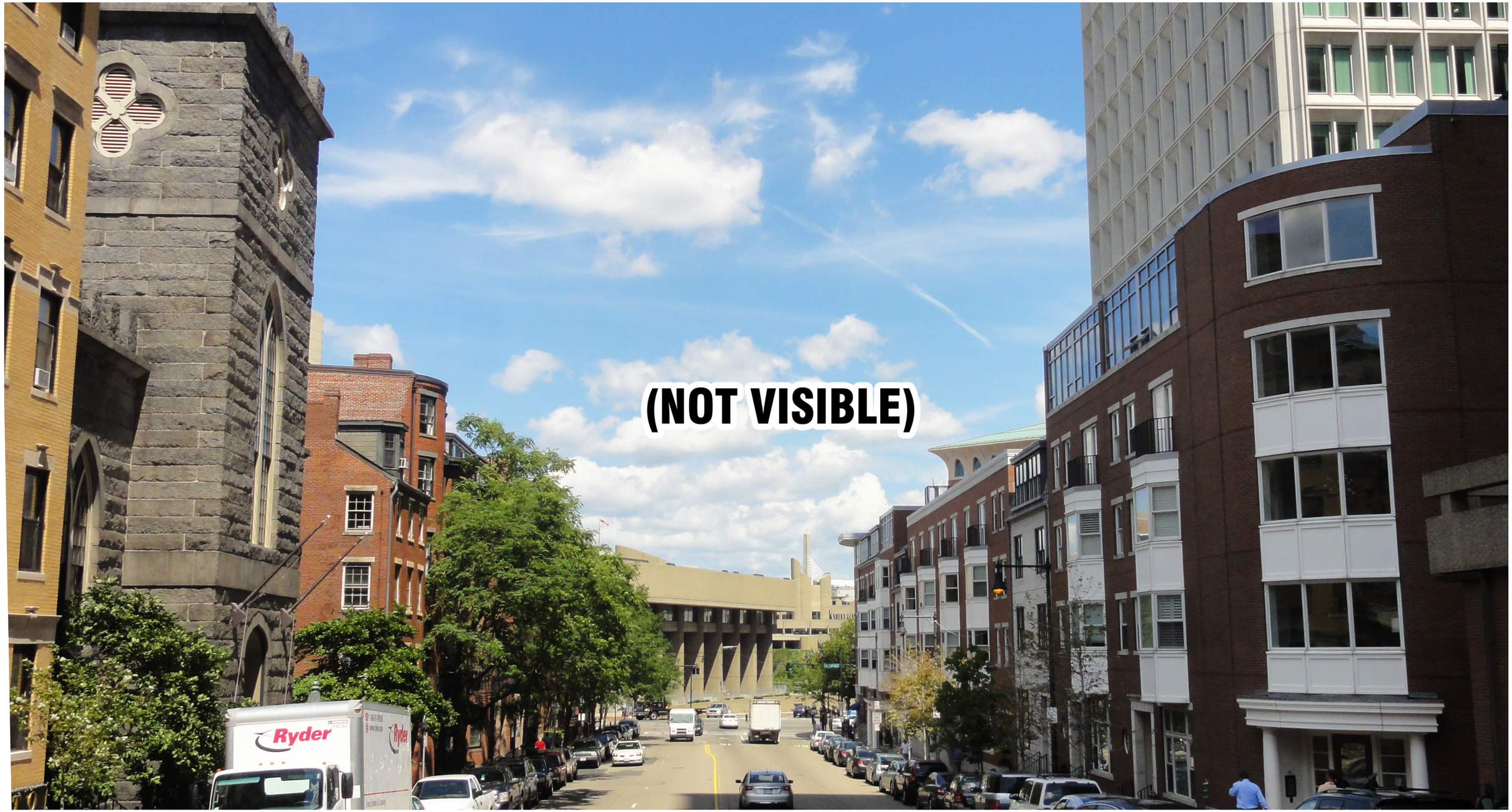
Redevelopment of Government Center Garage
Boston, MA

Figure H.6I

Plan - Floor 46-47

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Redevelopment of Government Center Garage
Boston, MA

Figure H.7a

View from Bowdoin Street

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Redevelopment of Government Center Garage
Boston, MA

Figure H.7b

View from Cambridge Street

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cbt



Redevelopment of Government Center Garage
Boston, MA

Figure H.7c

View from Cambridge-Bowdoin Intersection

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Redevelopment of Government Center Garage
Boston, MA

Figure H.7d

View from Congress Street

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Redevelopment of Government Center Garage
Boston, MA

Figure H.17e

View from Rose Kennedy Greenway

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Redevelopment of Government Center Garage
Boston, MA

Figure H.7f

View from Longfellow Bridge

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Redevelopment of Government Center Garage
Boston, MA

Figure H.17j

View from Martha Road

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Redevelopment of Government Center Garage
Boston, MA

Figure H.7h

View from Memorial Drive

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cbt



Redevelopment of Government Center Garage
Boston, MA

Figure H.7i

View from The Museum of Science

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Redevelopment of Government Center Garage
Boston, MA

Figure H.7j

View from North Washington Street

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Redevelopment of Government Center Garage
Boston, MA

Figure H.7k

View from The Public Gardens



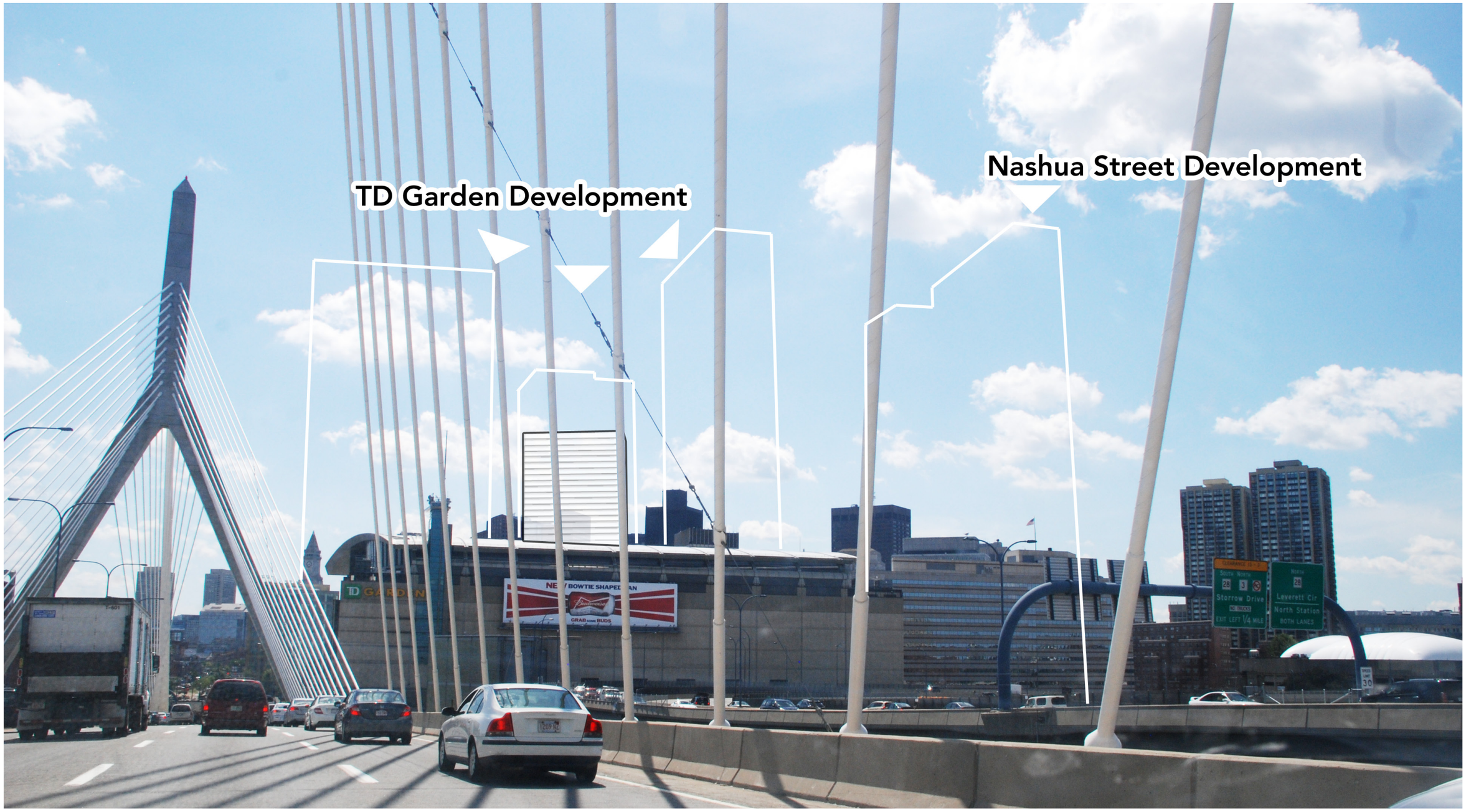
Redevelopment of Government Center Garage
Boston, MA

Figure H.17l

View from Thoreau Path

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Redevelopment of Government Center Garage
Boston, MA

Figure H.7m

View from Zakim Bridge

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