Expanded Project Notification Form

Belvidere/ Dalton Project



Submitted to:

Boston Redevelopment Authority

One City Hall Square Boston, Massachusetts 02201

Submitted by:

CL BD LLC c/o Carpenter and Company, Inc.

Charles Square, 20 University Road Cambridge, Massachusetts 02138

And

PRG BD Investors LLC c/o Pritzker Realty Group

300 North LaSalle, Suite 1500 Chicago, IL 60654 Prepared by:

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In Association with:

Pei Cobb Freed & Partners Cambridge Seven Associates, Inc.

WilmerHale

Vanasse Hangen Brustlin, Inc. Haley & Aldrich, Inc.

WSP

Nitsch Engineering

July 12, 2013



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Project Summary

1.0 PROJECT SUMMARY

1.1 Project Overview

CL BD LLC and PRG BD Investors LLC (the Proponent) propose to construct two new buildings at the intersection of Belvidere and Dalton Streets in the Back Bay. The proposed mixed-use project will include residential units, a hotel, open space, as well as restaurant and retail space.

The Proposed Project was envisioned in The First Church of Christ, Scientist's Plaza Revitalization Plan for the Christian Science Plaza and is included in the Master Plan Planned Development Area No. 80 for the Plaza, which was approved by the Boston Redevelopment Authority (BRA) and the Boston Zoning Commission in 2011 after a lengthy public process. The prior review process included study of potential impacts from the project in a document entitled "Plaza Revitalization Project" dated November, 2010. The public review process also included numerous community meetings and more than 20 Citizens Advisory Committee (CAC) meetings. The Proponent will acquire the project site from the Church and construct the Proposed Project independently.

The Proposed Project includes two buildings: a High-rise of approximately 58 stories and a Mid-rise of approximately 25 stories. Together, the proposed buildings will comprise approximately 950,000 square feet of gross floor area. The High-rise building will be developed by CL BD LLC, and the Mid-rise will be developed by PRG BD Investors LLC. The two buildings are analyzed together in this PNF. Separate Development Plans will be submitted to the BRA and the Zoning Commission for the two buildings.

The High-rise will be constructed on the triangular parcel surrounded by Belvidere Street to the north, 101 Belvidere Street (the former Church Colonnade Building) to the east, and Dalton Street to the west. It is expected to include approximately 290,000 square feet of hotel uses and approximately 422,500 square feet of residential space. Together with the existing tower at 111 Huntington Avenue, located a short distance the east, the new High-rise will provide a step-down transition from the Prudential Building to lower buildings on the Plaza and adjacent neighborhoods.

The Mid-rise building will be constructed opposite the High-rise on the west side of Dalton Street on what is now a surface parking lot adjacent to Belvidere Street. It will include approximately 237,500 square feet of residential space, including approximately 1,800 square feet of retail space. This building will continue the step-down in building height toward the surrounding neighborhoods.

Parking for both buildings will be provided in underground garages primarily via valet service.

The area surrounding the two buildings will be integrated together into an overall coherent site plan that will include the creation of a new approximately 4,400 square foot green open space located on the west side of Dalton Street at the east end of Saint Germain Street. The open space will serve as a buffer to the residences on Saint Germain Street and provide a public amenity for the neighborhood.

The Proponent will work with the BRA and the Boston Transportation Department (BTD) to implement several changes to the streets around the project site in order provide for smooth traffic flow. These changes include making Dalton Street between Belvidere and Saint Germain Street one-way southbound, extending Clearway Street from its current terminus at Dalton Street to connect with Belvidere Street, and making geometric improvements to the Dalton Street/Belvidere Street intersection. Extensive pedestrian improvements around the buildings will also be made.

The Project is described in more detail in Chapter 2. Transportation improvements specifically are presented and analyzed in Chapter 3.

1.2 Development Team

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1.3 Public Benefits

The Proposed Project will provide many benefits to the Christian Science Plaza, the surrounding neighborhood, and the City of Boston in terms of new jobs, tax revenue, infrastructure and public realm improvements, and the addition of beautiful and sustainably designed new buildings to Boston's skyline.

The Project includes new public open space of approximately 4,400 square feet on Saint Germain Street. This space will provide separation between the new buildings and the existing residential buildings on Saint Germain Street and be an attractive amenity for the neighbors and abutters. The design for the open space includes a lawn area, trees, and seating.

The portion of Dalton Street adjacent to the project will be reconstructed as a pedestrian-friendly public way. The new streetwall and retail spaces created by the Project will improve the pedestrian experience in the area. Clearway Street will also be extended to Belvidere Street as part of the project, including new sidewalks.

The Proposed redesign of the Belvidere Street/Dalton Street intersection will improve site access and neighborhood circulation while also improving the overall safety and functioning of the intersection.

In addition to the open space and infrastructure improvements described above, the project will have the following benefits:

- ♦ Creation of an estimated 250-300 permanent jobs;
- ◆ Creation of an estimated 1,000-1,200 construction jobs;
- ♦ Generation of housing and jobs linkage payments of approximately \$1,800,000;

- ◆ Generation of an estimated \$10,000,000 of annual new real estate taxes;
- Generation of approximately \$6,000,000 in annual hotel occupancy and meals tax revenues to the City and to the Commonwealth;
- Addition of distinctive and sustainably designed new architecture;
- Affordable housing commitment pursuant to the Mayor's Executive Order; and
- Creation of additional market-rate housing.

1.4 Preliminary Project Schedule

The Proponent expects to begin construction in early 2014. Construction is expected to take approximately 36 months to complete.

The City of Boston allows construction work from 7:00 a.m. to 6:00 p.m. Monday through Friday. Construction outside of those hours requires a permit. Construction hours will comply with the City's regulations, with no work anticipated on the weekends. In the event that weekend work is necessary, the Proponent will obtain required City approvals.

1.5 Consistency with Zoning

The Belvidere/Dalton Site (the "Site") is included in the Master Plan for Planned Development Area No. 80, Christian Science Plaza, Huntington Avenue/Prudential Center, Boston, dated August 16, 2011 (the "PDA Master Plan"). The Site is located within the Huntington Avenue/Prudential Center District under Article 41 of the Boston Zoning Code (the "Code"), the Restricted Parking District under Article 3-1A.a. of the Code and the Groundwater Protection Overlay District under Article 32 of the Code.

The PDA Master Plan authorizes three new buildings in the PDA containing up to 950,000 square feet of Gross Floor Area between the Huntington Avenue Site and the Belvidere/Dalton Site. The Proponent has submitted a proposed First Amendment to Master Plan, which would increase the permitted Zoning Height of the High-rise Building from 512 feet to 691 feet, and would increase the permitted Zoning Height of the Mid-rise Building from 251 feet to 285 feet. If the First Amendment to Master Plan is adopted, the resulting increase in the permitted height of the High-rise Building and Mid-rise Building could accommodate the allocation of all or substantially all of the 950,000 square feet of Gross Floor Area authorized by the PDA Master Plan. The Proponent also has submitted a Development Plan for the High-rise Building and a Development Plan for the Mid-rise Building for review by the BRA and approval by the Boston Zoning Commission, which would authorize the Project as described herein.

In accordance with Section 41-19 of the Code, off-street parking for the Site will be provided as required in the applicable Development Plan. Parking for new buildings on the Site will be provided primarily by parking spaces in the existing underground Christian Science Center garage and underground parking to be created in the existing Colonnade Building at 101 Belvidere Street, and approximately 21 parking spaces to be constructed under the Mid-rise Building.

The Master Plan requires that the new buildings on the Site will be designed to meet the groundwater standards in Article 32 of the Code for the Groundwater Protection Overlay District, and that upon written determination by the Boston Water and Sewer Commission that such standards are met and such determination is provided to the BRA and the Boston Groundwater Trust, a conditional use permit from the Board of Appeal shall not be required. The PDA Master Plan acknowledges that all buildings subject to Article 80 of the Code, Large Project Review, are subject to Article 37 of the Code, Green Buildings.

1.6 Legal Information

1.6.1 Legal Judgments Adverse to the Proposed Project

The Proponent is not aware of any legal judgments in effect or legal actions pending with respect to the Project.

1.6.2 History of Tax Arrears on Property Owned in Boston by the Proponent

The Proponent does not have a history of tax arrears on property that it owns in the City of Boston.

1.6.3 Site Control

The Proponent has entered into a Purchase and Sale Agreement with the Trustees of Church Realty Trust to acquire the Property.

1.6.4 Legal Description – Site Limits

The site is shown as Lots 1A, 1B and 2 on the Subdivision Plan prepared by Hancock Associates dated August 15, 2012 was recorded at the Suffolk County Registry of Deeds in Plan Book 2013, Page 311 on August 30, 2012. The southeast lot line of the High-rise Site is subject to minor modification. The Subdivision Plan is included in Appendix A.

1.7 Regulatory Controls and Permits

Table 1-1 presents a preliminary list of local, state, and federal permits and approvals that may be required for the Proposed Project. The list is based on current information about the Proposed Project and is subject to change as the design of the Project advances. Some of the permits listed may not be required, while there may be others not listed that will be needed.

Table 1-1 Preliminary List of Permits and Approvals

Agency	Approval
Boston	
Boston Redevelopment Authority	Article 80B Large Project Review
	Article 80C Planned Development Area Review
Boston Zoning Commission	Article 80C Planned Development Area Review
Boston Civic Design Commission	Design Review
Boston Landmarks Commission	Comment During Article 80B Process
Boston Water and Sewer Commission	Site Plan Review/General Service Application/Water
	and Sewer Connection Permits
Public Improvement Commission	Specific Repairs/Discontinuance (if required)
Boston Transportation Department	Construction Management Plan/Transportation
	Access Plan Agreement
Boston Public Works Department	Curb Cut Permit(s)
Boston Air Pollution Control Commission	Parking Freeze Permit/Exemption
Boston Public Safety Commission	Permit to Erect and Maintain a Parking Structure
Joint Committee on Licenses	Flammable Storage License
Boston Inspectional Services Department	Demolition/Building Permits
Licensing Board for the City of Boston	Hotel/ Restaurant Operating Permits
State	
Executive Office of Environmental Affairs	Massachusetts Environmental Policy Act Review
	(Previously obtained, EEA #14828)
Massachusetts Historical Commission	Determination of No Adverse Effect
Department of Environmental Protection	Notice of Demolition/Construction/Fossil Fuel and
	Sewer Connection Permit*
Massachusetts Water Resources Authority	Construction Site Dewatering Discharge Permit (if
	necessary)
Massachusetts Department of Transportation	MGL, C. 40 Sec. 54A, Consent to construction on
	former railroad right-of-way.
Federal	
Federal Aviation Administration	Determination of No Hazard to Air Navigation
Environmental Protection Agency	NPDES Notice of Intent for Construction –
	Stormwater

^{*}Sewer connection permit(s) to be issued by MassDEP and/or BWSC, depending on the outcome of pending regulatory changes.

The Proposed Project has already undergone review pursuant to the Massachusetts Environmental Policy Act (MEPA) as part of the Christian Science Plaza Revitalization Project (EEA Number 14828). The Secretary of Energy and Environmental Affairs issued a Certificate on the Environmental Notification Form for the Plaza Revitalization Project on January 20, 2012 determining that the Project did not require the preparation of an Environmental Impact Report.

Project Description

2.0 PROJECT DESCRIPTION

This Chapter describes the Proposed Project in detail, including its location, Project site plan, and proposed building program. It also discusses how the Project has evolved from the original proposal included in the PDA Master Plan for the Christian Science Plaza.

2.1 Surrounding Neighborhood

The Proposed Project is located along Boston's so-called "High Spine" that generally runs between Boylston Street and Huntington Avenue in the Back Bay. The Project site also sits on the northern edge of the roughly triangular shaped Christian Science Plaza. The Plaza itself is located at the nexus of several neighborhoods, including the Fenway, Back Bay, the South End/St. Botolph, and the Prudential. These neighborhoods include a mix of residential, retail, office, institutional, nonprofit and cultural uses that combine to create a vibrant city fabric. Immediately adjacent to the Plaza are the St. Botolph and Saint Germain residential areas, and Symphony Hall. The proposed new development on this site is designed to blend well with the existing ensemble of buildings and uses and to harmonize with the surrounding area. Figures 2-1 and 2-2 present photos of the existing conditions in the area in and around the project site

2.2 Project Parcels

The Proposed Project site is located at the intersection of Belvidere and Dalton Streets and comprises three separate parcels that will be developed together.

Lot 1A is a triangular vacant parcel surrounded by Belvidere Street to the north, 101 Belvidere Street (the former Church Colonnade Building) to the east, and Dalton Street to the west. This parcel is approximately 28,544 square feet. The proposed High-rise building will be built on this parcel.

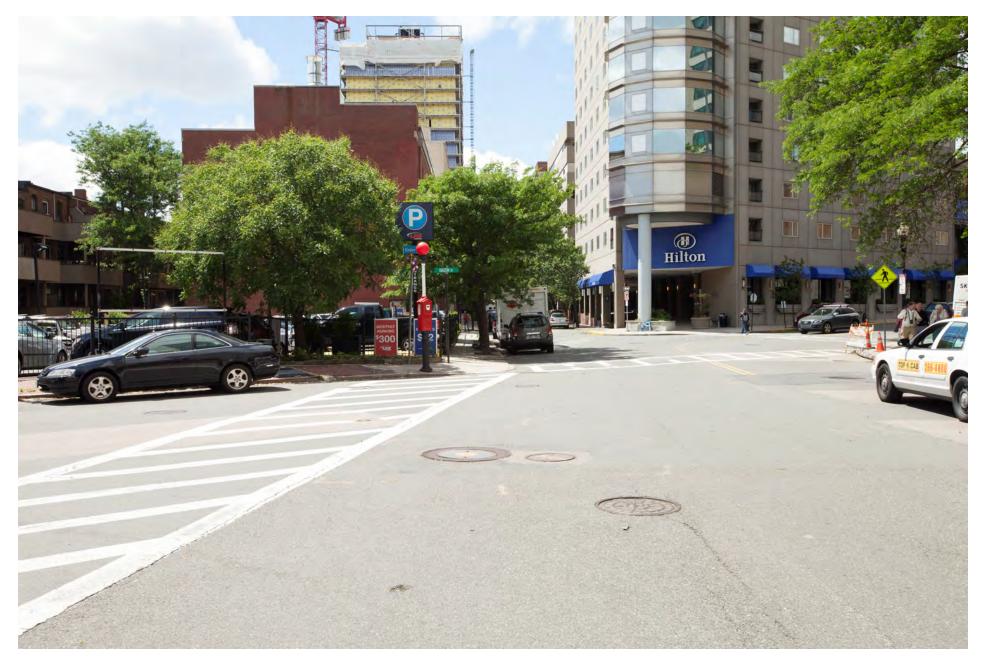
Lot 2 is located west of Dalton Street at its intersection with Belvidere Street. It is currently used as a surface parking lot. It is approximately 12,376 square feet. The proposed Mid-rise building will be built on this parcel.

Lot 1B is located on the west side of Dalton Street at its intersection with Saint Germain Street. It is currently used as a surface parking lot. This parcel is approximately 4,678 square feet. This parcel will be converted to public open space.

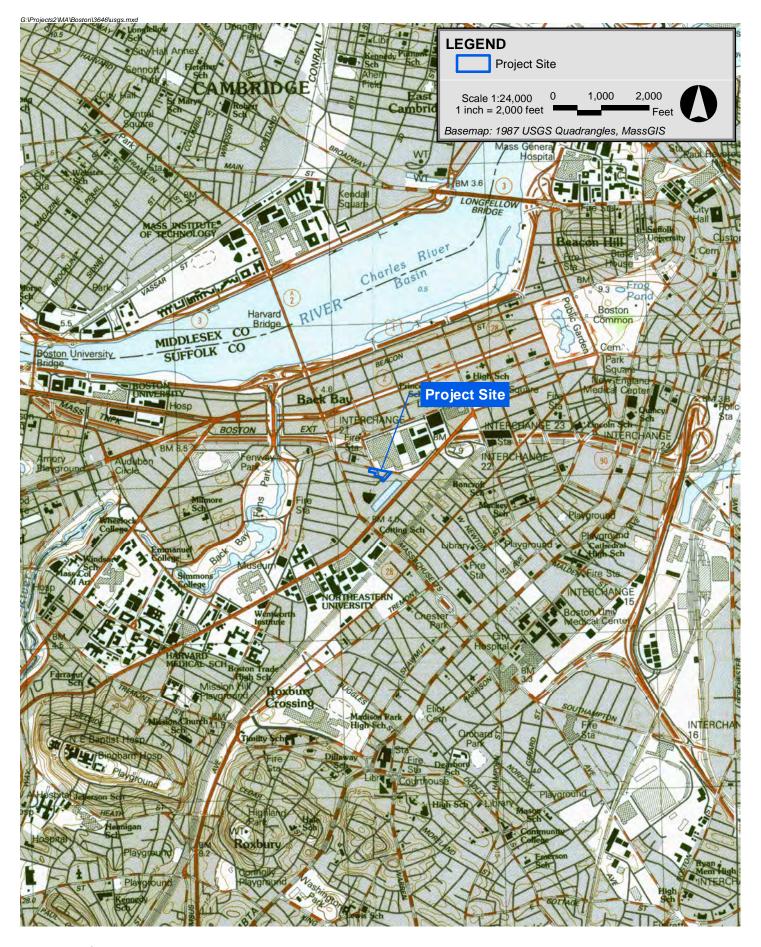
The Project site is shown on a USGS Map in Figure 2-3 and on an aerial photograph base in Figure 2-4. A Subdivision Plan prepared by Hancock Associates dated August 15, 2012 which shows the three parcels is included in Appendix A



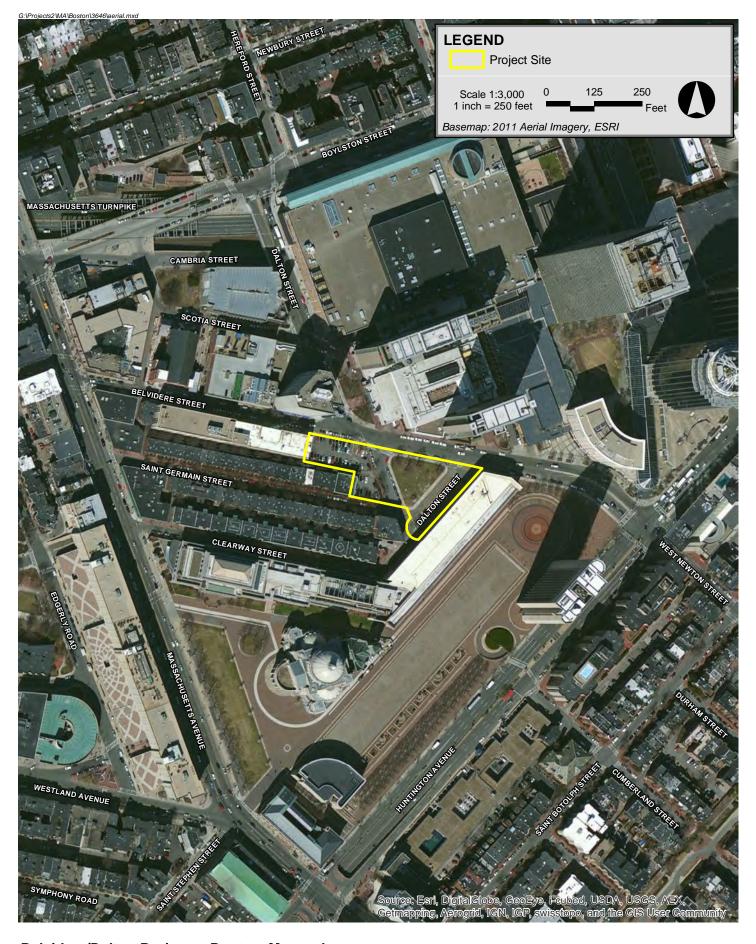














2.3 Previous Planning for the Site

As was briefly described in Section 1.1, the Proposed Project was originally conceived in The First Church of Christ Scientist's Plaza Revitalization Project Plan for the Christian Science Plaza ("Revitalization Plan") and was included in the Master Plan Planned Development Area No. 80 for the Plaza, which was approved by the BRA and the Boston Zoning Commission in 2011 after a lengthy public involvement process that included more than 20 Citizens Advisory Committee meetings.

The Revitalization Plan called for a total of 950,000 square feet of new development to be constructed between two locations, together with 2,000 square feet allocated to a pavilion on the Christian Science Plaza, near the intersection of Huntington Avenue and Belvidere Street, which is not included in the Project studied by this PNF. The first location was the current Proposed Project site described in the preceding section. It was referred to in the Revitalization Plan as the Belvidere/Dalton Site. This site was proposed for approximately 800,000 square feet of development to be divided into an approximately 512-foot high-rise building and an approximately 250-foot high mid-rise building

The second location for development envisioned in the Revitalization Plan was along Huntington Avenue adjacent to the Church's Sunday School Building, where an approximately 291-foot high, 150,000 square-foot building was envisioned. Figure 2-5 includes an image of both locations.

Since the completion of the Revitalization Plan, there has been additional consideration given regarding the suitability of the Huntington Avenue Site for development. While there remains a desire to activate the street edge at that location through the introduction of a new use, there is also concern regarding the impacts a development of the size contemplated in the Revitalization Plan would have on the historic/aesthetic aspects of the Plaza, as well as concerns about wind and shadow impacts of a development of that size on the Huntington Avenue site. Therefore, the Proposed Project has been designed to shift development away from the Huntington Avenue Site by moving its proposed square footage to the Belvidere/Dalton site. Thus, the Proposed Project locates on the Belvidere/Dalton Site, which sits within the High Spine, the 950,000 square feet of development which is all of the new development approved in the PDA Master Plan other than the 2,000 square feet allocated to the pavilion. This approach is in lieu of locating some of the approved density in a tall building on Huntington Avenue, which would sit directly on the Christian Science Plaza. While this will result in taller buildings at the Belvidere/Dalton site, the impacts will be minimized due to the site's location adjacent to taller buildings such as the Prudential and 111 Huntington. Expected impacts are analyzed in detail in the following chapters.

Table 2-1 compares the current Proposed Project with the development scenario that was envisioned in the Revitalization Plan and current PDA Master Plan.

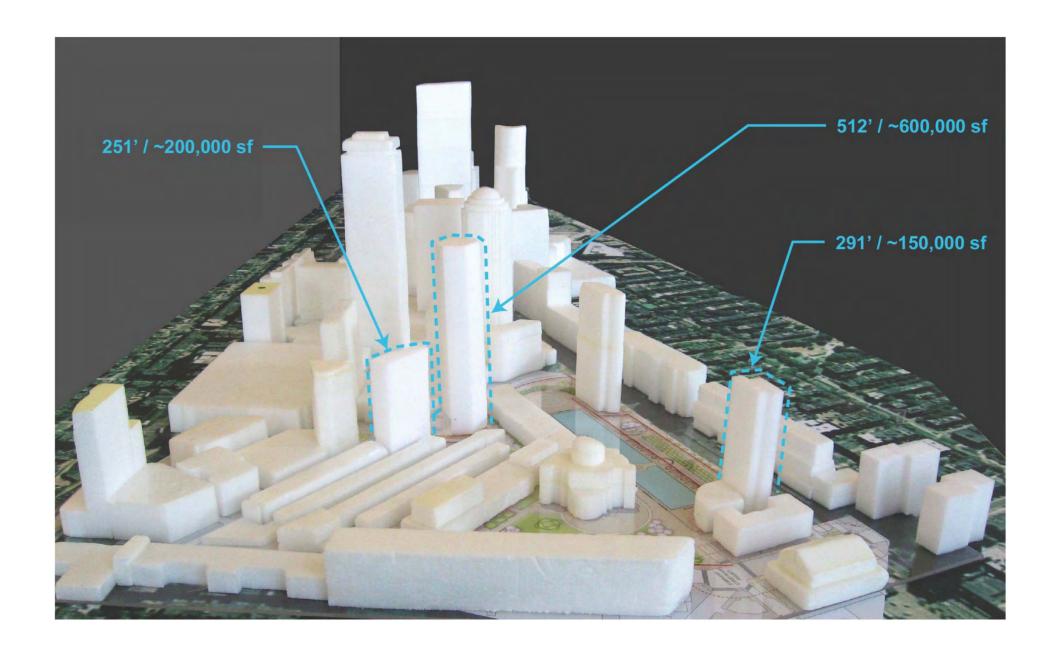




Table 2-1 Proposed Project Compared with Revitalization Plan Development Scenario

Proposed Project	Revitalization Plan Development Scenario
Belvidere/Dalton Site	Belvidere/Dalton Site
High rise Building	High rise Building
Zoning Height – 691 feet	Zoning Height – 512 feet
Gross Floor Area – 712,500	Gross Floor Area – 600,000
Belvidere/Dalton Site	Belvidere/Dalton Site
Mid Rise Building	Mid Rise Building
Zoning Height – 285 feet	Zoning Height – 251 feet
Gross Floor Area – 237,500	Gross Floor Area – 200,000
Huntington Avenue Site	Huntington Avenue Site
N/A – No building proposed at this time	Zoning Height – 291 feet
N/A – No building proposed at this time	Gross Square footage – 150,000
Total Gross Floor Area = 950,000	Total Gross Floor Area = 950,000

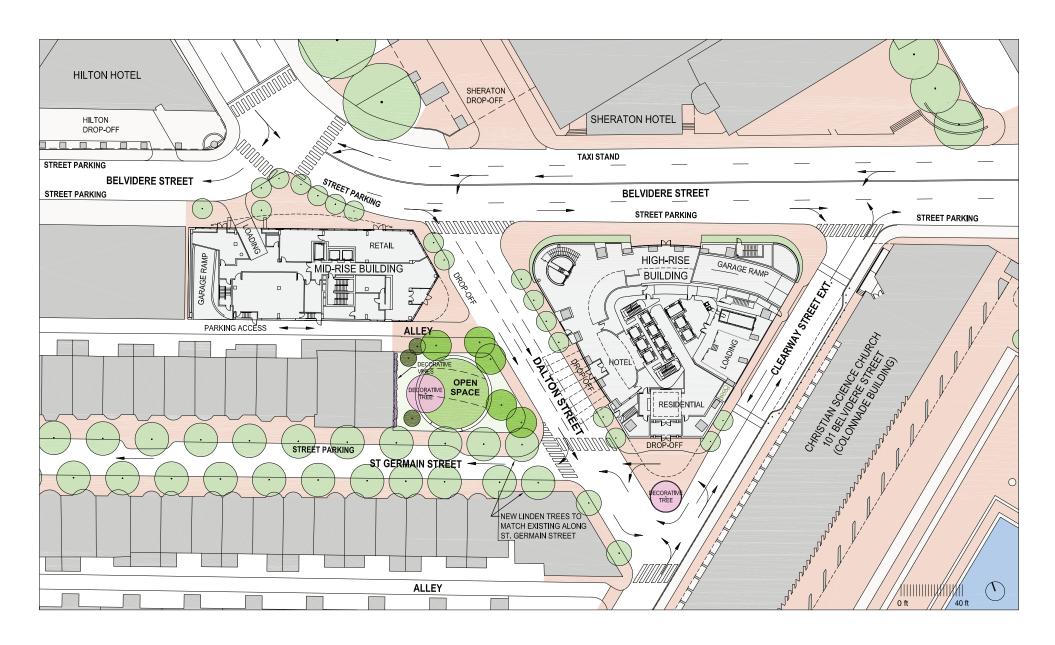
2.4 Project Description

2.4.1 Overall Site Plan

The Proposed Project includes two buildings: a High-rise of approximately 58 stories and a Mid-rise of approximately 25 stories. Together, the proposed buildings will comprise approximately 950,000 square feet of gross floor area. Figure 2-6 presents the overall site plan for the development, depicting the location of the proposed Mid-rise and High rise buildings on opposite sides of Dalton Street, the proposed new open space to be created at the end of Saint Germain Street, and the proposed new traffic improvements which are summarized in Section 2.4.5 and presented in detail in Chapter 3.

2.4.2 High-rise Building

The High-rise will be constructed on the triangular parcel surrounded by Belvidere Street to the north, 101 Belvidere Street (the former Church Colonnade Building) to the east, and Dalton Street to the west. It is expected to include approximately 290,000 square feet of hotel uses and 422,500 square feet of residential units. A number of program elements compose the overall hotel use including guestrooms, meeting rooms, a ballroom, restaurant, café, pool & fitness center. The hotel is expected to have approximately 250 guestrooms, while the residential space is expected to comprise approximately 170 units and up to 425 bedrooms.





The proposed High-rise shape is derived from the equilateral triangle, softened by gently-curved sides and rounded corners. The resulting form complements without competing with the Mother Church, while its eastern face aligns with the orientation of the Reflecting Pool and the buildings that frame it. Thus the new High-rise, results in a smooth transition from the adjoining Prudential Center to the landmarked Christian Science Plaza.

Floor plans, sections, and elevations of the High-rise are included at the end of this chapter as Figures 2-7 through 2-16.

2.4.3 Mid-rise Building

The proposed Mid-rise building will be constructed opposite the High-rise on the west side of Dalton Street on what is now a surface parking lot adjacent to Belvidere Street. It will include approximately 255 residential units (285 bedrooms) totaling approximately 237,500 square feet including approximately 1,800 square of retail space, such as a coffee shop or café, on the ground floor.

The Mid-rise building's exterior has a curved face that closely resembles the curvature of its neighboring High-rise soft sided triangular form. This building is a pivot point for the project, anchoring the development at the intersection of Belvidere and Dalton Streets, and representing the last and furthest development of the Plaza and Christian Science precinct. The scale of the Mid-rise is much reduced from the High-rise component to match that of its adjacent neighbors, notably the Hilton and Sheraton towers. The scale of this building will also respect the surrounding, lower residential blocks comprised of the handsomely scaled buildings on Saint Germain, Clearway and Belvidere Streets.

Floor plans, sections, and elevations of the Mid-rise are included at the end of this chapter as Figures 2-17 through 2-24.

2.4.4 Program Summary

Table 2-2 summarizes the proposed building program.

Table 2-2 Program Summary

High-rise Building	56 occupiable stories	
	691 feet tall per Zoning Code	
Hotel	290,000 square feet	
	250 guestroom keys	
Residential	422,500 square feet	
	170 Units	
	425 Bedrooms	
Parking Up to 400 parking spaces made available in the existing Ch		
	Science Plaza underground garage and in the basement of	
	101 Belvidere Street.	
Mid-rise Building 25 Stories		
	285 feet tall per Zoning Code	
Residential	237,500 square feet	
	255 Units	
	285 Bedrooms	
Parking Approximately 21 spaces below grade on site and up to 60 sp		
	available from the 400 allocated to the High-rise.	

2.4.5 Proposed Changes to Surrounding Roadways

2.4.5.1 Proposed Traffic Patterns

The Proposed Project includes a number of changes to the roadway network surrounding the site. Traffic will circulate counter clockwise around the site. Dalton Street will be made one way southbound between Belvidere and Saint Germain Street. Clearway Street will be extended from its current terminus northward to connect with Belvidere Street. The Belvidere Street/Dalton Street intersection will be realigned to improve sight distances, and will contain only two approaches: Belvidere Street westbound and Dalton Street southbound. The Belvidere Street westbound approach will be striped to include a left/through lane and an exclusive right turn lane.

2.4.5.2 Parking and Loading

High-rise Building

Parking for the High-rise will be handled entirely or almost entirely by valet service at the building's two main entrances on Dalton Street for the hotel, and at the southern apex of the building at the intersection of Dalton and Clearway Streets for the residential units. Parking for the High rise will be provided in the existing First Church of Christ, Scientist's below grade plaza garage and in the basement of the 101 Belvidere Street Building where 60 new spaces will be created. Through the use of valet parking, approximately 113 net

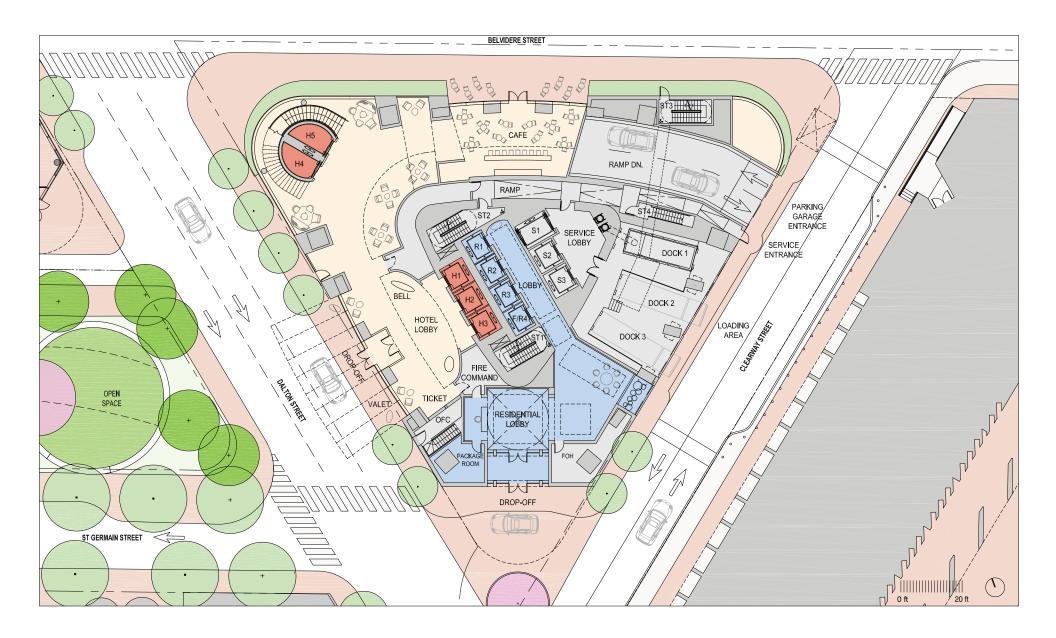
new spaces will be added to the garages after taking into account the relocation of 63 surface parking spaces from the Mid-rise site to the garage. Access to the garages will be via a ramp off of the proposed new Clearway Street Extension on the east side of the High-rise.

The Dalton/Belvidere High-rise loading and service area will be located off of the Clearway Street Extension. As currently planned, the building will be served by three loading bays, two for large trucks and a third intended to house a compactor for the building.

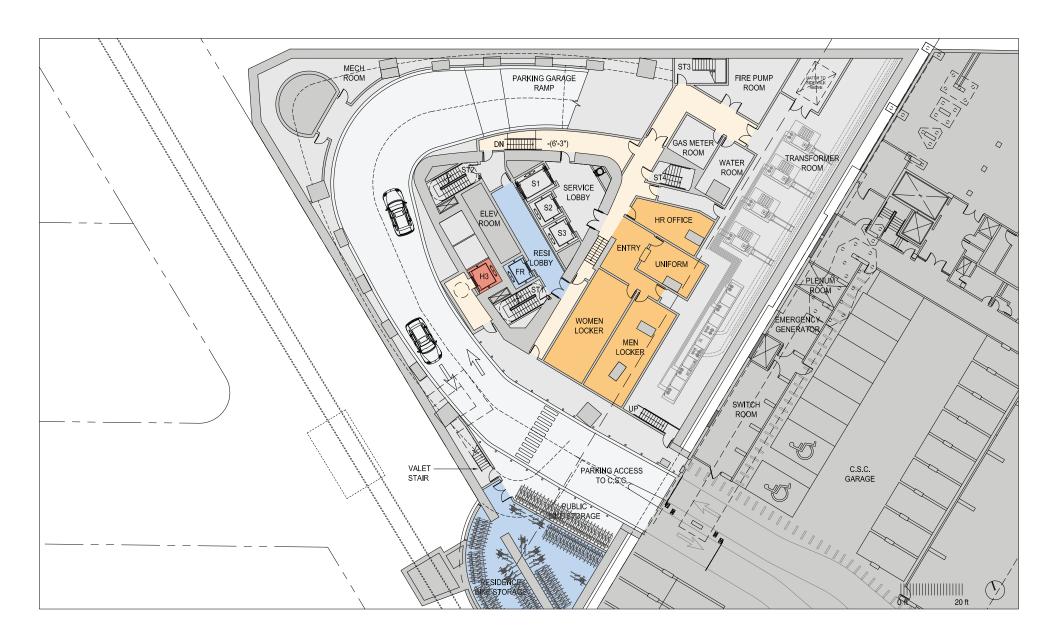
Mid-rise Building

Parking for approximately 21 cars will be provided for the Mid-rise building in a new underground garage accessed from the alley on the south side of the building. Additional parking for the Mid-rise will be provided in the existing First Church of Christ, Scientist's below grade garage for up to 60 cars.

The Mid-rise building's loading dock for trash removal and move in/move out operations will be located off of Belvidere Street.



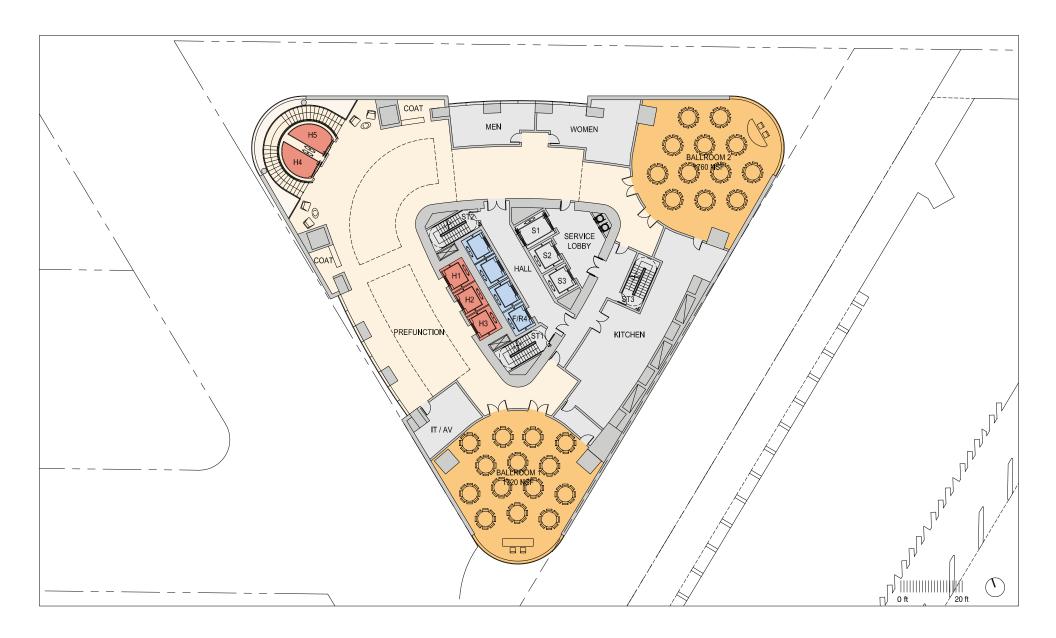








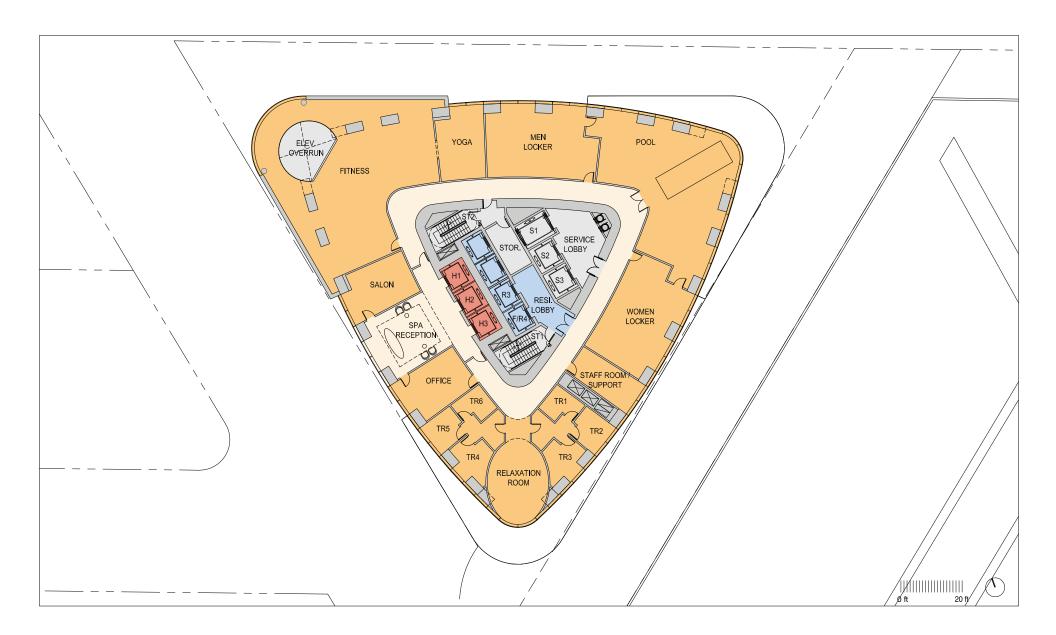




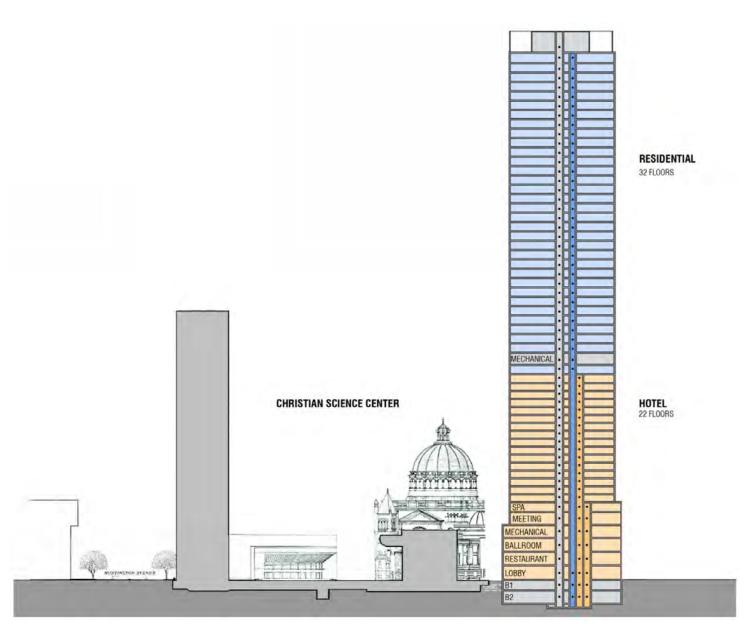




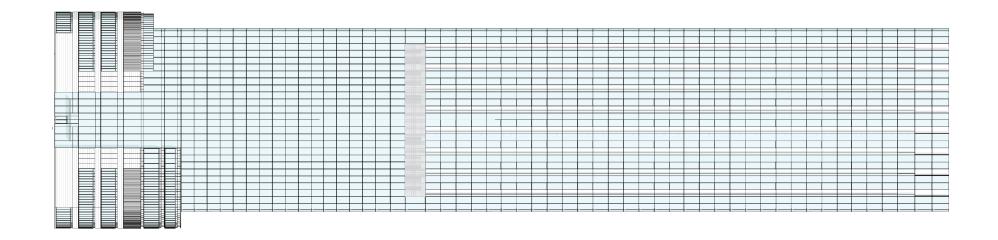




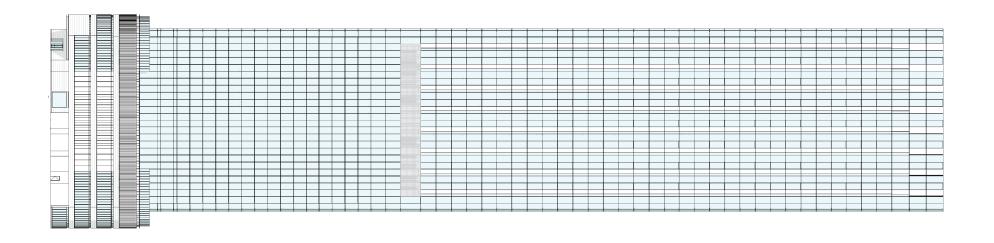




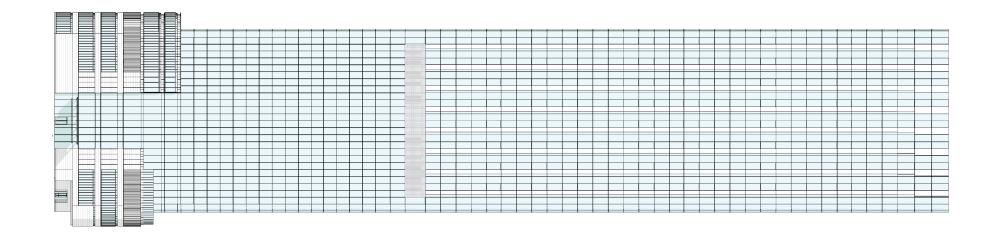




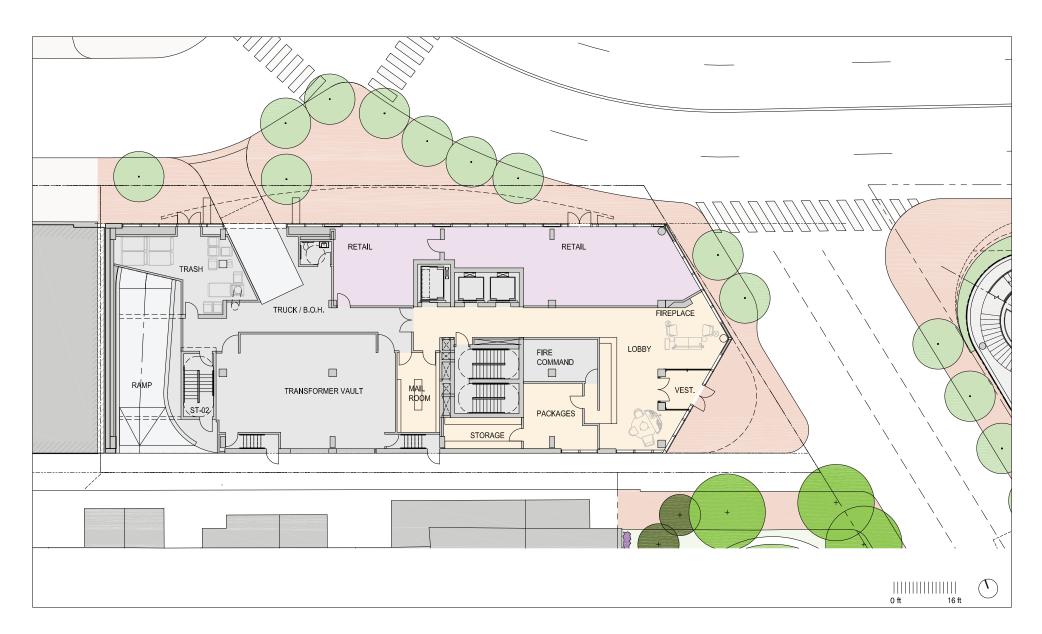




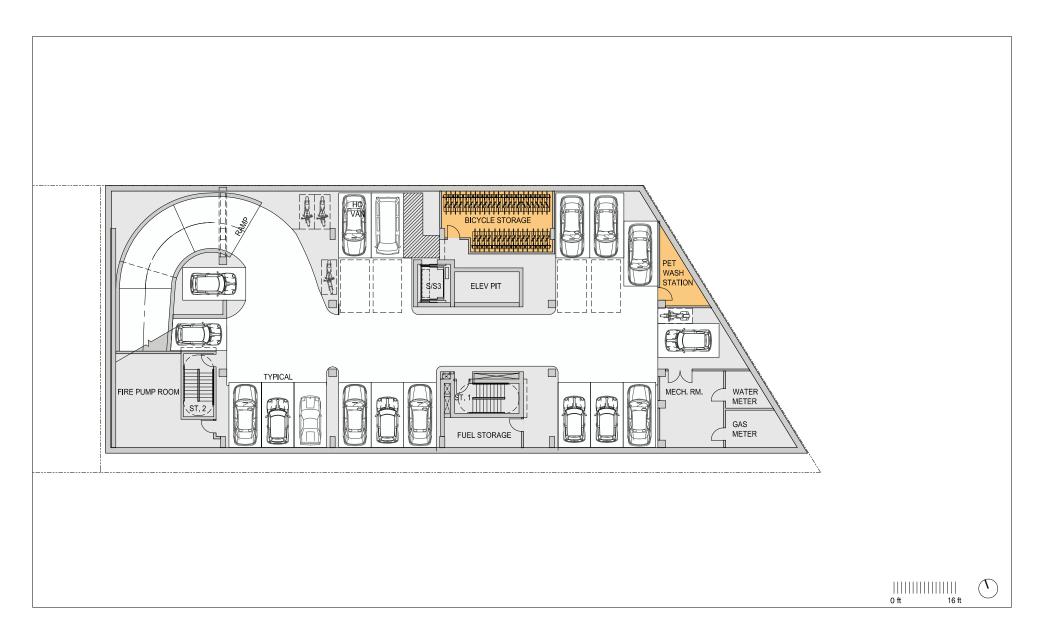




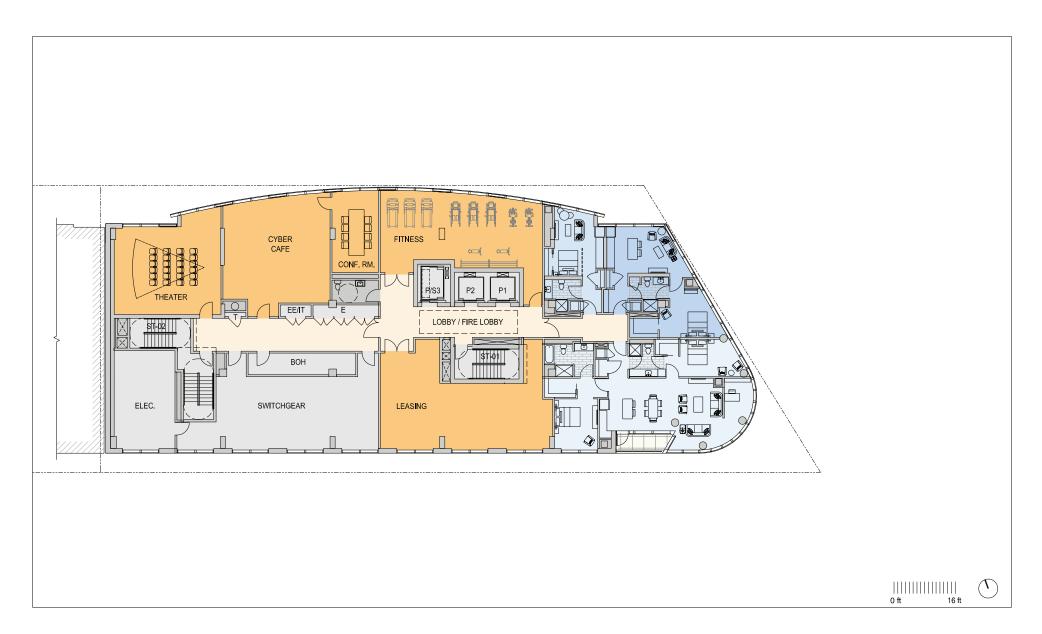




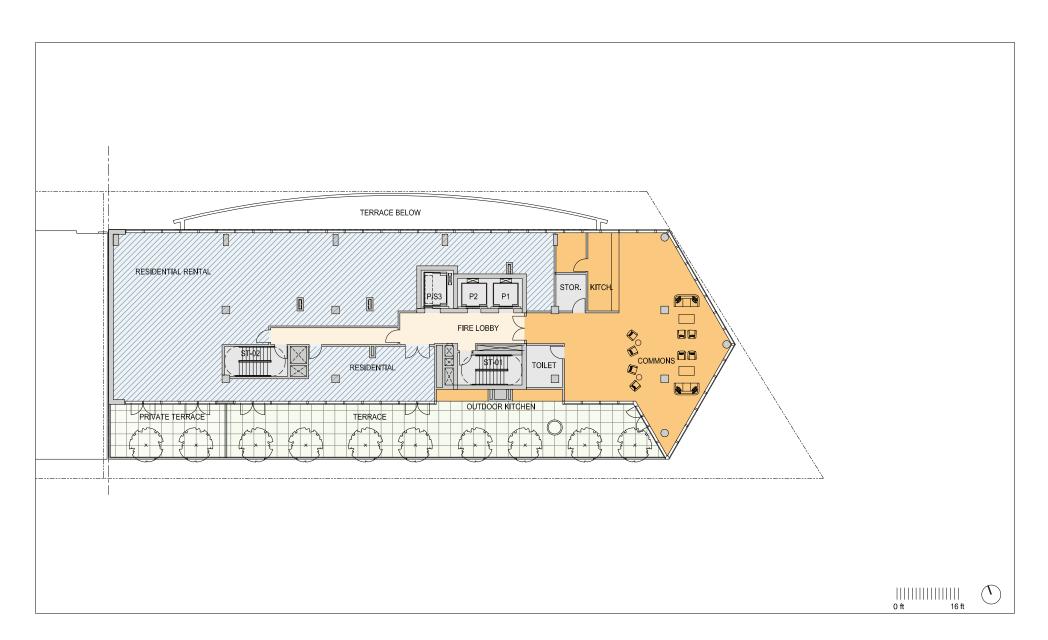




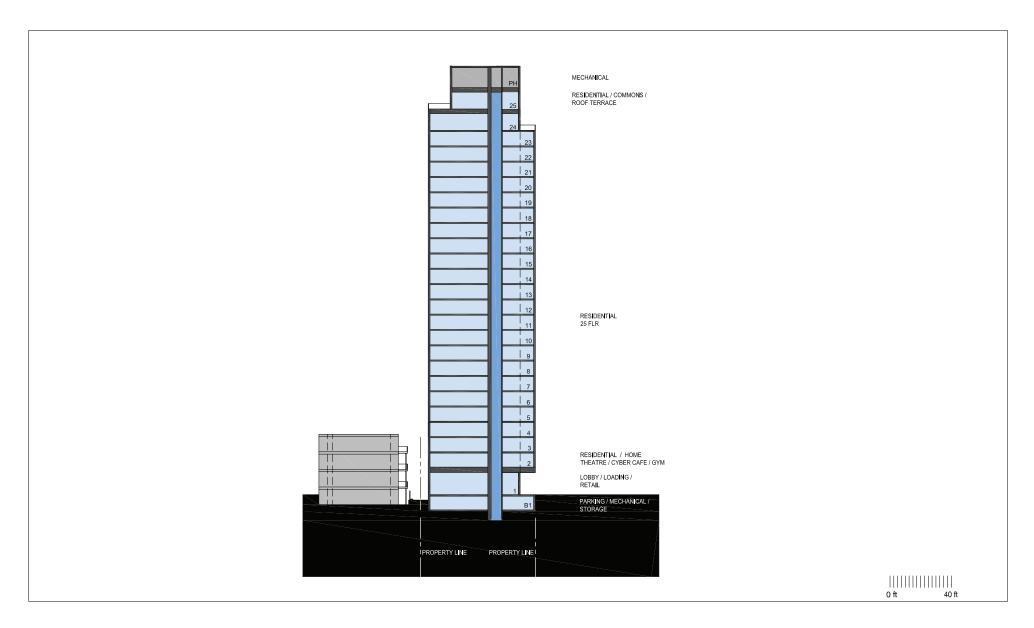




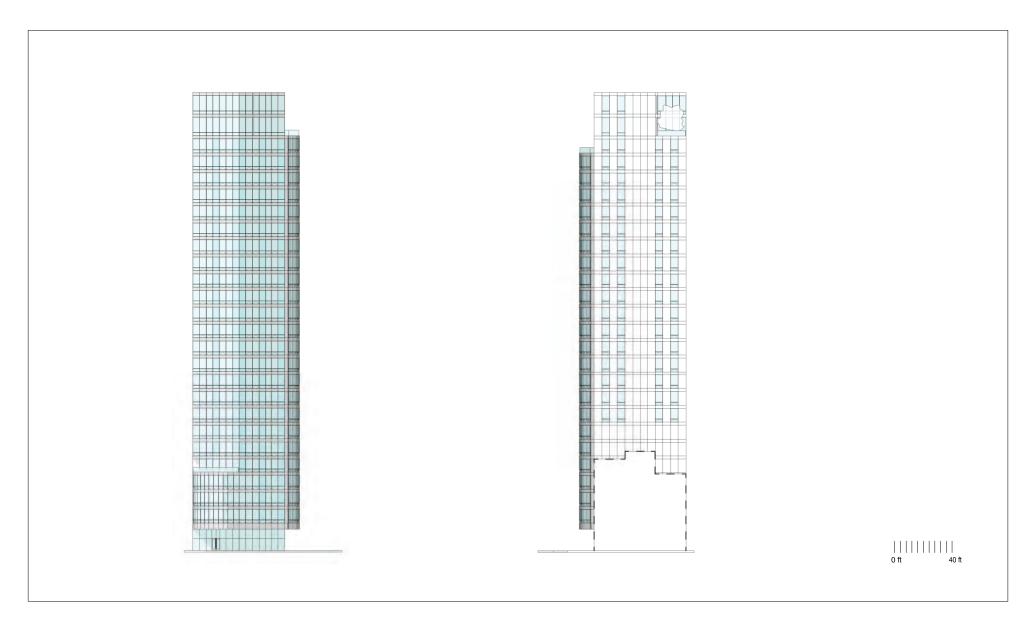




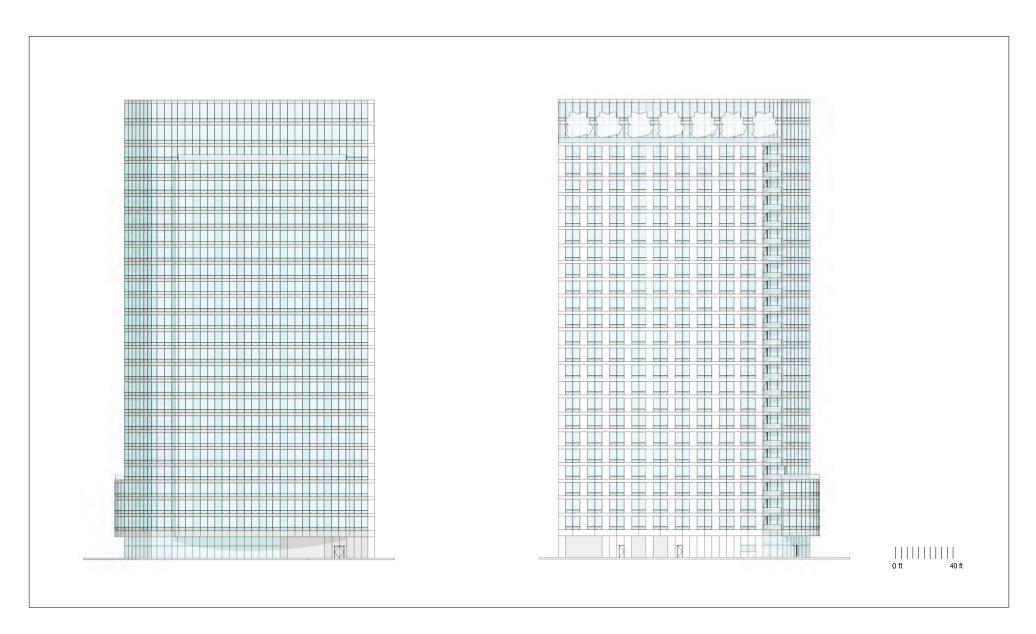




















Transportation Access Plan

3.0 TRANSPORTATION ACCESS PLAN

3.1 Introduction

This chapter presents an evaluation and summary of existing and future transportation infrastructure and operations of the Belvidere/Dalton Project. This transportation study has been developed in order to understand and mitigate the transportation impacts of the Proposed Project.

The Transportation Access Plan includes an analysis of the following:

- Definition and quantification of existing transportation conditions in the Proposed Project Study Area (the "Study Area");
- Projection of future transportation conditions with and without the Proposed Project;
- An assessment of parking conditions in the Study Area;
- ◆ A summary of proposed improvements, including travel demand management (TDM) strategies;
- ♦ An overview of construction-related activities as they pertain to transportation; and
- ♦ Vehicular level of service (LOS) analyses for Study Area intersections.

The transportation analysis considers three specific analysis scenarios as follows:

- 2013 Existing Condition based on traffic volume data collected in May, 2013.
- 2018 No Build Condition including background projects and area growth, and
- 2018 Full Build Condition for a 5-year time horizon assuming completion of the Proposed Project and infrastructure changes to the intersection of Belvidere Street at Dalton Street.

The transportation analysis has been performed in accordance with standard Boston Transportation Department ("BTD") methodologies, including the projection of project trips and the application of local travel characteristics established through the Access Boston 2000-2010 initiative. Synchro 6 software was used to facilitate the evaluation of traffic operations based on Highway Capacity Manual ("HCM") methodologies.

3.1.1 Project Description

The Project is planned to be comprised of approximately 950,000 gross floor area of new development composed of a mix of residential, hotel, and supporting retail uses. The Highrise site is bounded by Dalton Street, Belvidere Street and a private driveway along the First Church of Christ Scientist building and will contain a hotel and residential condominium units. The Mid-rise site is on the corner of Belvidere Street and Dalton Street to the west of Dalton Street and will contain apartment units and some ancillary retail. Parking demand for the High-rise and Mid-rise Buildings will be satisfied as described in Section 3.3.3.7. Figure 3.1-1 depicts the proposed site plan for the Project. The following Table 3-1 summarizes the program by building site.

Table 3-1 Proposed Program

Site:	Hotel	Condominium Units	Net New Parking	Net New Bike Parking
Belvidere/Dalton High-rise	250 units	170 units	113 Spaces	220 spaces
	Retail	Apartment Units	Net New Parking	Net New Bike Parking
Belvidere/Dalton Mid-rise	1,800 SF	255 units	21 spaces	240 spaces

3.1.2 Summary of Findings & Transportation Mitigation

- ◆ The Proposed Project has minimal transportation impacts on nearby intersections due to the Project's predominance of residential and hotel land uses.
- The Proposed Project creates a minimal net increase in parking needs due to the existing on-site parking supply and residential and hotel land-use development program.
- ◆ The Project area currently has a high use of transit, bicycling and walking versus drive-alone commuting which will be encouraged as part of the Project development program.

3.2 Existing Transportation Conditions

This section provides a summary of existing transportation conditions in the study area. Discussions include the following:

- ◆ A description of the existing roadways that provide access to the Project site;
- ♦ A description of the existing traffic volumes in the Study Area;
- ♦ A discussion of nearby public transportation options;



- Summaries of parking in the Study Area; and
- Existing pedestrian and bicycle activity and amenities.

3.2.1 Study Area

The Study Area is located in the Prudential/Back Bay area of downtown Boston, as shown in Figure 3.2-1. The Study Area includes the following ten key intersections:

Signalized Intersections:

- ♦ Boylston Street at Massachusetts Avenue
- ♦ Belvidere Street at Massachusetts Avenue
- ♦ Westland Avenue/Falmouth Avenue at Massachusetts Avenue
- ♦ Huntington Avenue at Massachusetts Avenue
- ♦ Cumberland Street at Huntington Avenue
- Belvidere Street/W. Newton Street at Huntington Avenue
- Boylston Street at Dalton Street/Hereford Street

Un-signalized Intersections:

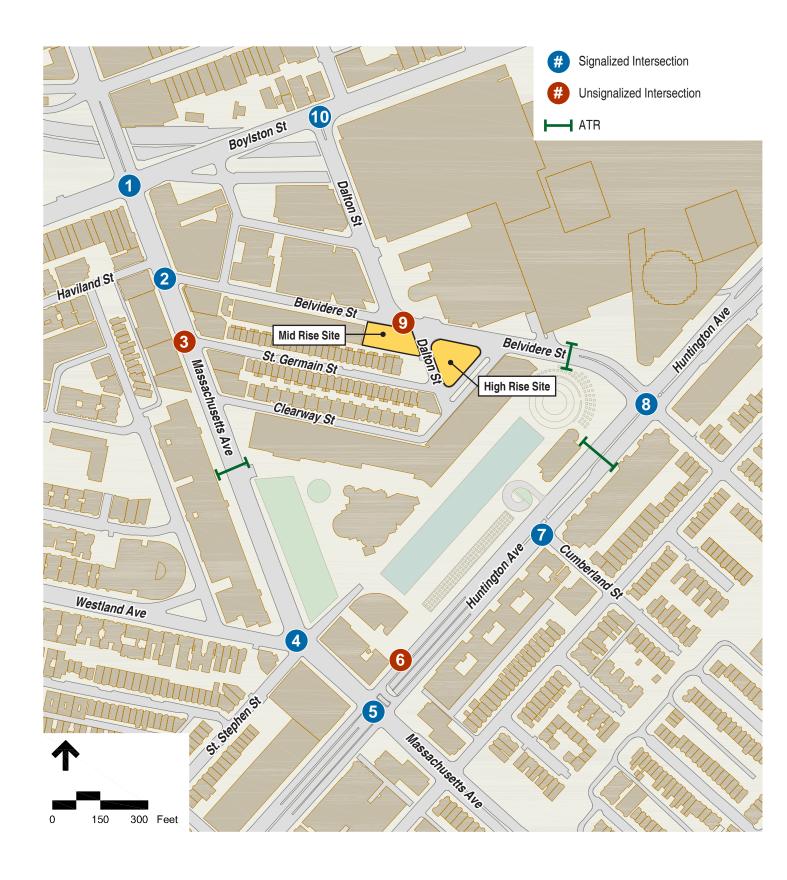
- ♦ Saint Germain Street at Massachusetts Avenue
- Huntington Avenue at The First Church of Christ Scientist (TFCCS) Driveway West
- ◆ Dalton Street at Belvidere Street

3.2.2 Roadway Network

The principal roadways and study intersections in the Study Area are described briefly below. The description of the roadways includes physical characteristics, adjacent land uses, and traffic control devices.

Massachusetts Avenue

Massachusetts Avenue is a two lane roadway in both the north and southbound directions. The roadway, for the most part travels north to south connecting the Boston neighborhood of Dorchester to the City of Cambridge where it becomes Route 2A and travels west through the state of Massachusetts. Parking is located on both sides of the roadway within the study area.



Huntington Avenue

Huntington Avenue is a minor arterial roadway in the northeast/southwest direction, but extends east to west across the state from Boston to Worcester. Within the study area, the roadway is a three lane roadway with metered parking on the east side and tour bus parking on the side adjacent to The First Church of Christ, Scientist site.

Belvidere Street

Belvidere Street is a local roadway that connects Huntington Avenue to Massachusetts Avenue directly north of the High-rise and Mid-rise buildings. The roadway is two lanes in both the east and westbound directions from Huntington Avenue to the east of Dalton Street. To the west of Dalton Street, Belvidere Street is a single lane, one-way roadway in the westbound direction with parking on both sides.

Clearway Street

Clearway Street contains a single travel lane and connects Massachusetts Avenue to Dalton Street. The roadway is one-way in the eastbound direction with parking and loading on the south side of the street.

Dalton Street

Dalton Street is a two-way roadway that runs in the north-south direction between Boylston Street and Clearway Street. The roadway runs between the High-rise and the Mid-rise buildings. Adjacent to the site, the roadway provides on-street parking on both sides.

3.2.3 Study Area Intersections

The study area includes ten intersections listed in section 3.2.1 which provide a basis for determining to what extent, if any, Project traffic is likely to affect the wider transportation network. These intersections are described below, including general physical characteristics, geometric conditions, pedestrian facilities and traffic control measures.

1) Boylston Street/Massachusetts Avenue

The intersection of Boylston Street at Massachusetts Avenue is a four-legged signalized intersection. The northbound approach has two general purpose travel lanes and a bicycle lane. The southbound approach has an exclusive left-turn lane and two general purpose travel lanes. The eastbound direction has two approach lanes and left-turns are not permitted onto Massachusetts Avenue. The westbound approach has two lanes, one of which is an exclusive right-turn lane. Crosswalks with pedestrian signals are provided across all four legs.

2) Belvidere Street/Massachusetts Avenue

The intersection of Belvidere Street at Massachusetts Avenue is a three legged signalized intersection which includes a fourth leg departing the intersection onto Haviland Street slightly offset to the north of the intersection. Belvidere Street is one-way westbound approaching Massachusetts Avenue with a single general purpose lane. Massachusetts Avenue has two lanes in the north and southbound directions with parking on either side of the roadway. Crosswalks with pedestrian signals are provided across Belvidere Street and across Massachusetts Avenue.

3) Saint Germain Street/Massachusetts Avenue

The unsignalized intersection of Saint Germain Street at Massachusetts Avenue is a minor roadway intersecting a free flowing high volume roadway. Saint Germain Street contains a one-way travel lane with parking on the north side and approaches Massachusetts Avenue with a stop control. Massachusetts Avenue has two lanes in the north and southbound directions with metered parking on each side of the roadway. There is a crosswalk for pedestrians to cross Saint Germain Street, but none across Massachusetts Avenue.

4) Westland Street/Massachusetts Avenue/St. Stephen Street

The five-legged intersection of Westland Street/Massachusetts Avenue/St. Stephen Street and Falmouth Avenue (The First Church of Christ Scientist Driveway) is signalized. St. Stephen Street is a one-way roadway departing the intersection and Falmouth Avenue acts as a driveway to the First Church of Christ, Scientist site and is not part of the signal. Massachusetts Avenue in the northbound direction has an exclusive left-turn lane and a general purpose travel lane. The southbound approach on Massachusetts Avenue has two general purpose lanes. Westland Street approaches the intersection with a single general purpose lane that has a restricted left-turn. There is metered parking located on the Westland Street approach.

5) Huntington Avenue/Massachusetts Avenue

Huntington Avenue at Massachusetts Avenue has two signals that run on a coordinated system. The southern signal allows for access to and from the inbound approach/departure of Huntington Avenue; while the northern signal allows access to and from the outbound approach/departure of Huntington Avenue. The Massachusetts Avenue southbound approach has two through lanes and an exclusive right-turn only lane. The northbound approach on Massachusetts Avenue has two general purpose travel lanes. Both the east and westbound approaches on Huntington Avenue provide for a u-turn movement for vehicles to change directions on Huntington Avenue if necessary and two travel lanes. In addition, an underpass allows vehicles to travel along Huntington Avenue without having to travel through the signalized intersection.

6) Huntington Avenue/TFCCS Driveway

The intersection of Huntington Avenue at the First Church of Christ, Scientist driveway is accessed via Huntington Avenue southwest bound. The Driveway approaches the unsignalized intersection with stop control. Vehicles are only permitted to make a right-turn onto Huntington Avenue. Two lanes are provided in the Huntington Avenue southwest bound-approach.

7) Cumberland Street/ Huntington Avenue

The intersection of Huntington Avenue at Cumberland Street is a right-in/right-out movement for Cumberland Avenue due to the median divided Huntington Avenue. The signal is fully actuated and shows either the pedestrian signal or the minor street movement immediately after being called. There is a crosswalk across Cumberland Street.

8) Belvidere Street/ Huntington Avenue/W. Newton Street

The intersection of Belvidere Street/West Newton Street at Huntington Avenue is a four-legged signalized intersection. The eastbound Huntington Avenue approach contains an exclusive left-turn lane and two general purpose travel lanes with adjacent parking. The westbound approaches the intersection with an exclusive left-turn lane, two through lanes and an exclusive right-turn lane. The northbound West Newton Street approach is a single general purpose lane. The southbound Belvidere Street approach has two general purpose travel lanes and an exclusive left-turn lane. There are crosswalks across all four legs of the intersection.

9) Dalton Street/Belvidere Street

The intersection of Dalton Street at Belvidere Street is a four-legged unsignalized intersection with the Dalton Street south leg being offset to the east. Belvidere Street is one-way westbound departing the intersection to the west of Dalton Street. To the east of Dalton Street, Belvidere Street is a two ways with two travel lanes and parking on either side of the roadway. The northbound and southbound approaches are stop controlled while the westbound approach is free-flowing. The northbound approach from Dalton Street is a single general purpose lane with parking on both sides of the roadway. The southbound approach is two general purpose lanes with tour bus and trolley parking on either side of the roadway.

10) Dalton Street/Boylston Street/Hereford Street

The signalized intersection of Dalton Street/Boylston Street/Hereford Street contains two approaches: Dalton Street northbound and Boylston Street eastbound. Two lanes are provided in the Dalton northbound direction, one is a left-turn lane while the other is a right turn lane. Boylston Street approaches the intersection with two general purpose travel lanes. Crosswalks are provided across each leg of the intersection. Hereford Street departs the intersection to the north with two travel lanes. A fire station is located adjacent to the intersection on Boylston Street.

3.2.4 Traffic Volume Data Collection

To better assess existing conditions in the study area, traffic volumes were collected. Manual turning movement counts (TMCs) were conducted during the morning peak hours, 7:00 AM to 9:00 AM, and during the evening peak hours, 4:00 PM to 6:00 PM, on Tuesday May 14, 2013¹. Due to the timing of the counts taking place after local colleges and universities were out of session, the existing conditions traffic counts were increased by 5 percent at the Massachusetts Avenue intersections to account for the additional institutional traffic when local colleges and universities are in session.

In addition to the manual turning movement counts, automatic traffic recorder (ATR) counts were conducted over a 24-hour period in May 2013.

TMC and ATR raw data are attached in Appendix B.

Existing Traffic Volumes

TMC and ATR counts were used to develop the daily 24-hour counts and peak hour turning movement traffic volumes for the 2013 Existing Condition.

Table 3-2 presents a summary of the daily traffic volumes calculated from the ATR counts.

-

Counts that had been originally scheduled for Tuesday April 30, 2013 when the Berklee School of Music, Northeastern University, New England Conservatory and Wentworth Institute of Technology were in session were delayed due to the April 15, 2013 Boston Bombing event.

Table 3-2 Existing Traffic Volumes Summary

		Peak Hour					
	Daily	Weekday Morning		Weekday Evening			
Location	Weekday (vpd)*	Volume (vph)**	"K" Factor***	Directional Distribution	Volume (vph)**	"K" Factor***	Directional Distribution
Massachusetts Avenue south of Clearway Street							
Northbound	10,742	745	6.9%	53%	767	7.1%	50%
Southbound	11,861	650	5.5%	47%	756	6.4%	50%
Total	22,603	1,395	6.2%	-	1,523	6.7%	-
Belvidere Street north of							
Huntington Avenue							
Eastbound	2,871	168	5.9%	21%	250	8.7%	29%
Westbound	8,199	649	7.9%	79%	621	7.6%	71%
Total	11,070	81 <i>7</i>	7.4%	-	8 <i>7</i> 1	7.9%	-
Huntington Avenue west of Belvidere Street							
Eastbound	8,848	560	6.3%	43%	686	7.8%	50%
Westbound	9,904	728	7.4%	57%	689	7.0%	50%
Total	18 <i>,</i> 752	1,288	6.9%	-	1,3 <i>7</i> 5	7.3%	_

Source: Automatic Traffic Recorder (ATR) counts conducted by Precision Data Industries, LLC in May 2013

The intersection turning movement counts were used to establish traffic networks for the 2013 Existing Condition for the Morning and Evening peak hours. The study area's overall morning peak hour was determined to be 7:45 AM to 8:45 AM and the evening peak hour was determined to occur between 5:00 PM and 6:00 PM. Existing Condition (2013) morning and evening peak hour traffic volumes are shown in Figures 3.2-2 and 3.2-3, respectively.

3.2.5 Pedestrian & Bicycle Access

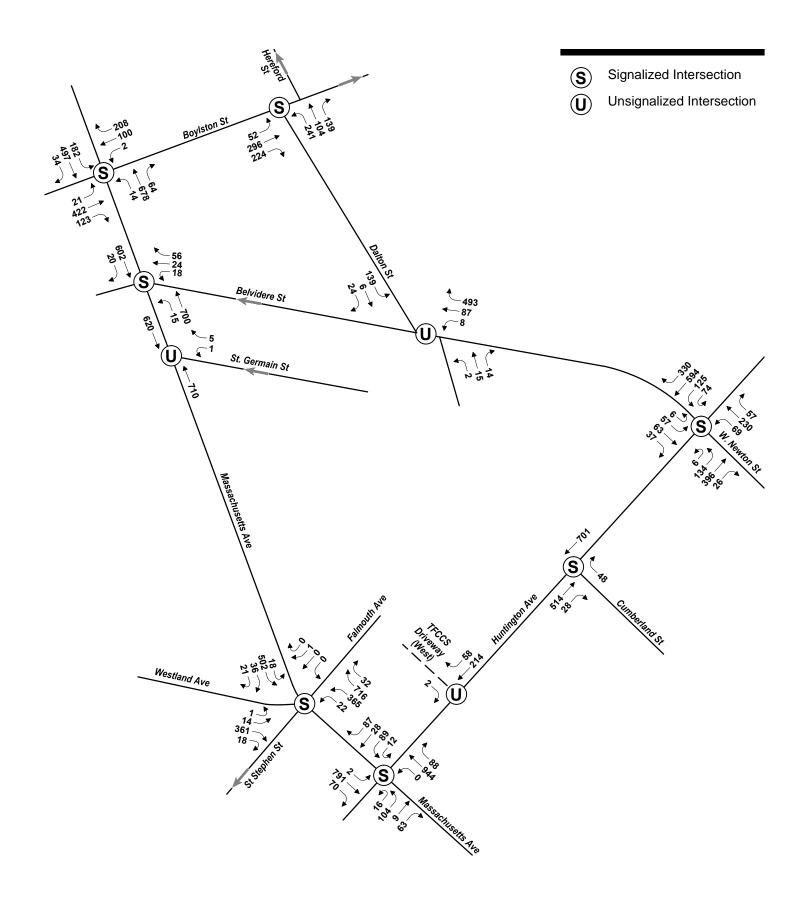
Pedestrian circulation occurs on the sidewalks of streets in and around the site where there is a steady flow of pedestrians throughout the day. Heavily used pedestrian routes are ones that lead to/from train stations and major destinations in the area including the Prudential, Copley, Back Bay and other locations in the area. The area is well served by a sidewalk network that connects it with the rest of the city. Pedestrian facilities in the study area include sidewalks that vary in width, crosswalks at major intersections, and accessible ramps.

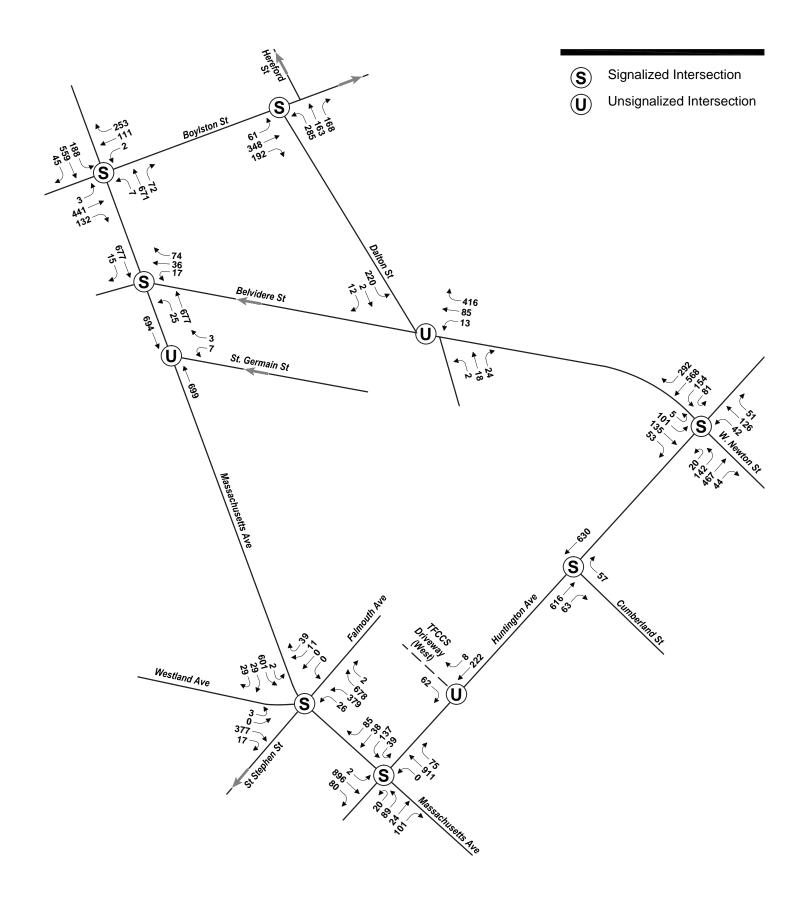
The Southwest Corridor Park is a 4.7 mile linear park stretching from the Back Bay to Forest Hills which provides a roadway separated bicycle and walking path for its length. The corridor is approximately 0.25 mile from the Project. In addition, bicycle

^{*}Daily traffic expressed in vehicles per day.

^{**}Peak hour volumes expressed in vehicles per hour.

^{***}Percent of daily traffic that occurs during the peak hour.





lanes are provided on Massachusetts Avenue and St Stephen Street. The Project Study Area has several bicycle rack locations available, specifically on the TFCCS Plaza area. Enhancing bicycle accommodations is an element of the Project, and will also be a consideration in the design of the new buildings.

Starting in April of 2011, the Hubway bike share system was launched to provide the community with over 1,000 bicycles and 100 stations throughout Boston, Brookline, Cambridge and Somerville. Currently, there is a Hubway station, housing 19 bicycles, located on the Christian Science Plaza. The second closest station is located north of the Project at the Prudential Center; this station provides 25 bicycles. The Hubway system allows bicyclists to either obtain a three-season membership or ride casually with short-term pricing.

Morning and evening peak hour pedestrian and bicycle counts conducted at each of the study area intersections are graphically represented in Figures 3.2-4 through 3.2-7 respectively.

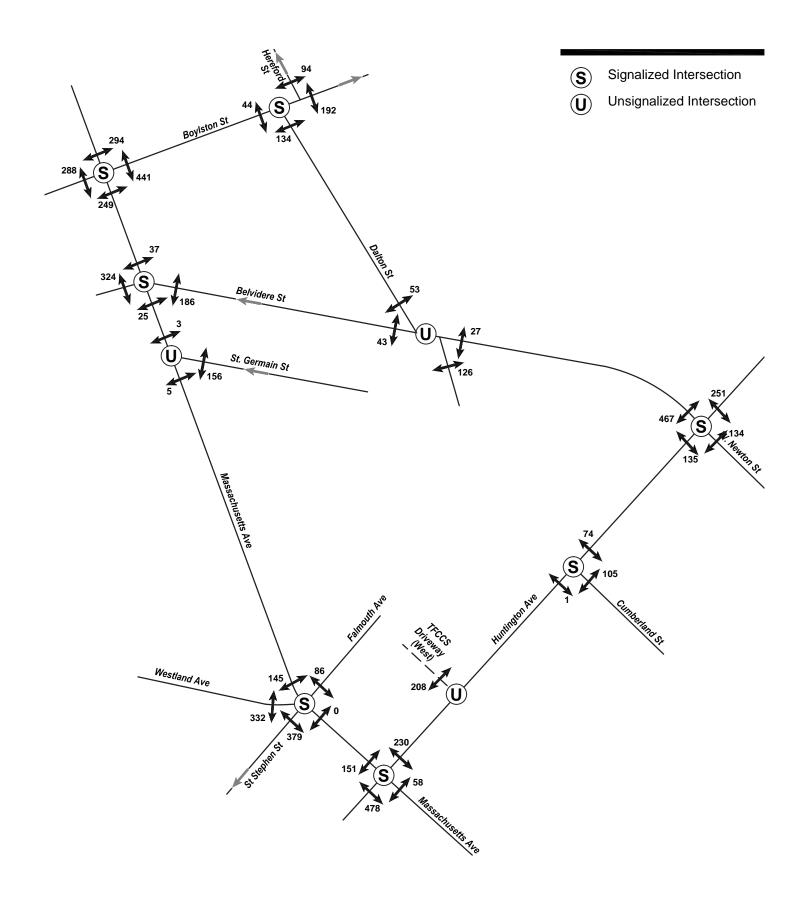
3.2.6 Public Transportation

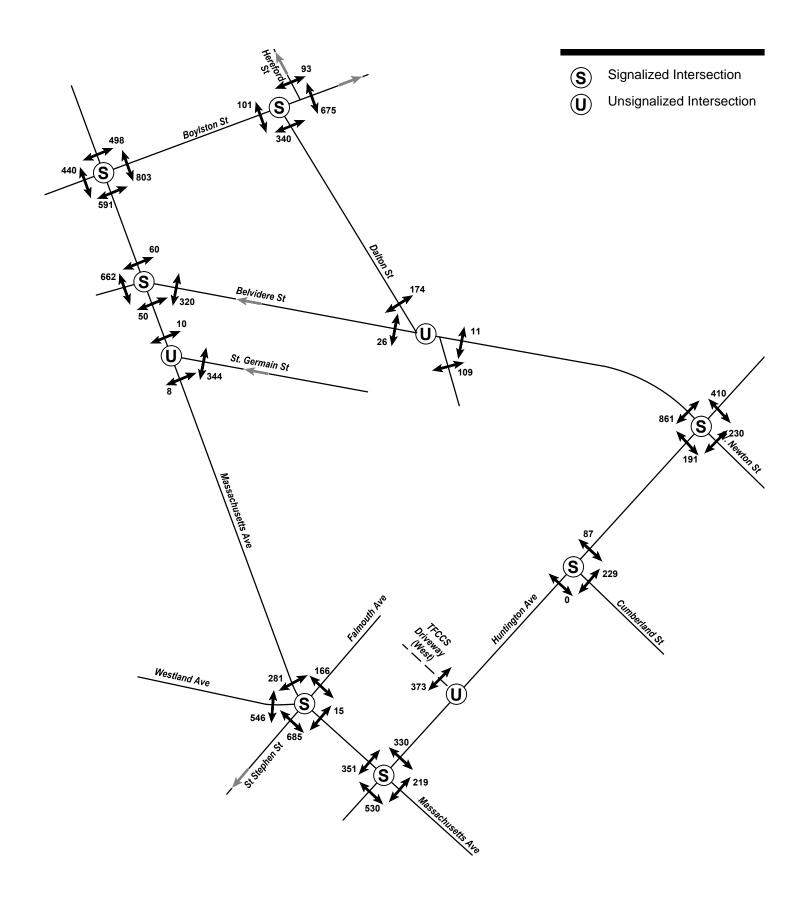
Massachusetts Bay Transportation Authority (MBTA) services in the vicinity of the Project site include multiple bus lines, the Green Line, and four commuter rail lines. These services, illustrated in Figure 3.2-8 are described in further detail below.

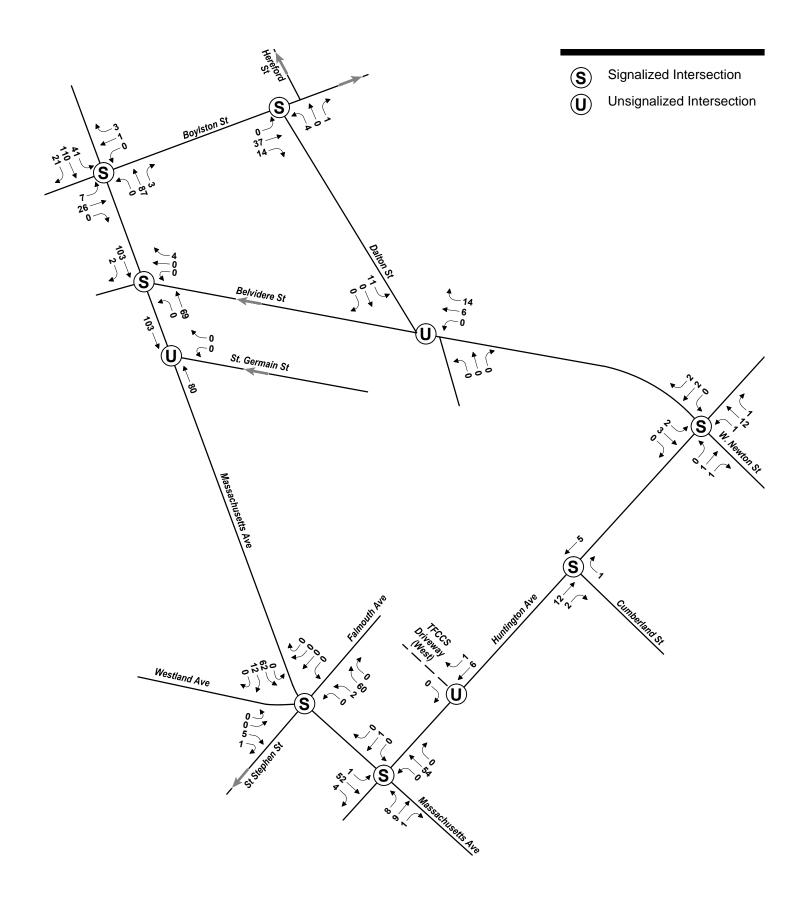
3.2.6.1 MBTA Bus Route Service

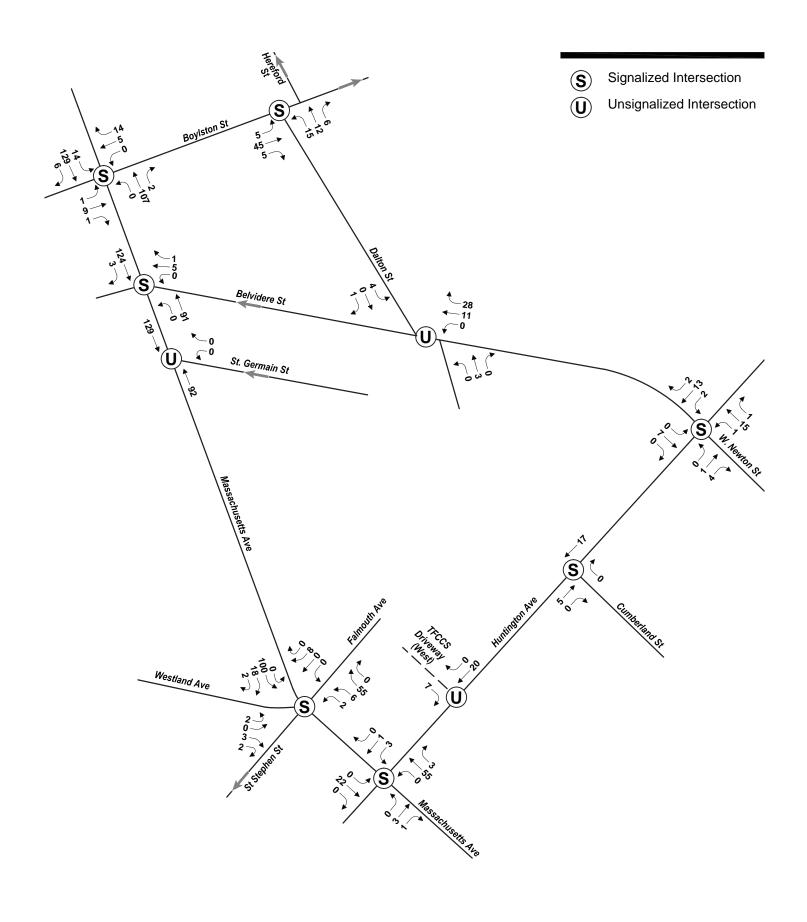
Five bus routes are available in the vicinity of the Project site providing access to/from Somerville, Cambridge, Waltham, Hyde Park, and Watertown.

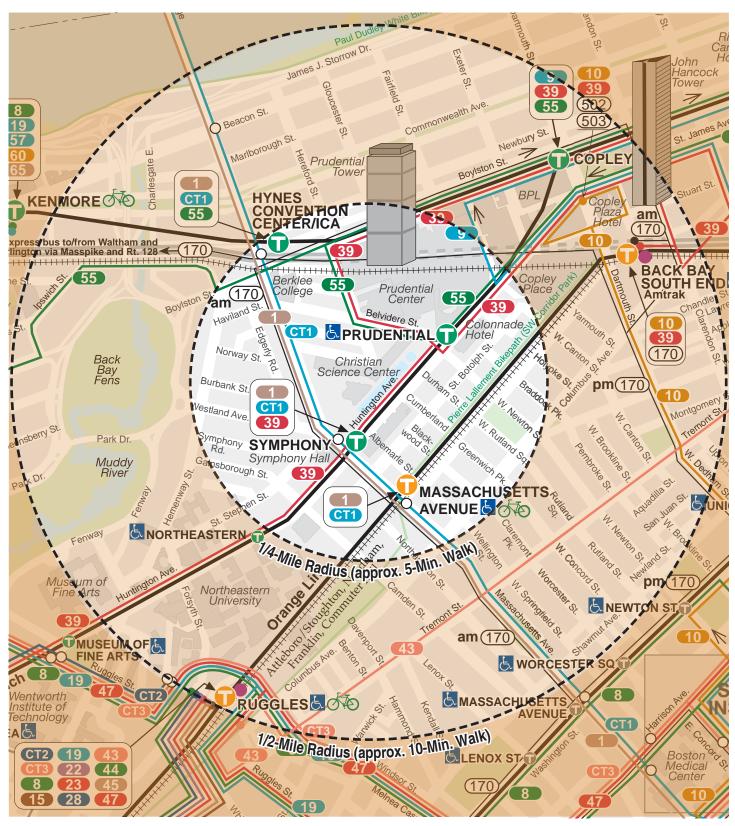
- Route CT1 (Central Square, Cambridge BU Medical Center/Boston Medical Center via M.I.T.) provides stops along Massachusetts Avenue. The route spans north to south from Central Square in Cambridge to the BU Medical Campus in the South End.
- ♦ Route 1 (Harvard/Holyoke Gate Dudley Station via Mass Ave) extends from Harvard Station to Roxbury along Massachusetts Avenue with stops to the west of the site.
- ♦ Route 39 (Forest Hills Station Back Bay Station via Huntington Avenue and Jamaica Plain Center) provides a stop on Huntington Avenue.
- Route 55 (Jersey and Queensbury Copley Square or Park and Tremont Stations via Ipswich Street) provides local access between the Boston Common and the Back Bay Fens.











Source: MBTA

• Route 170 (Central Square, Waltham – Dudley Square) is a limited service bus route only providing two trips in the morning peak in the outbound direction and two trips in the evening peak in the inbound direction. During the morning peak, there are stops along Massachusetts Avenue and one stop on Boylston Street. During the evening peak, the bus route travels directly to Back Bay Station without stopping in the Study Area.

3.2.6.2 MBTA Subway Services

The Project site is centrally located between the Green Line-E Branch and Orange Line to the south and southeast, and the Green Line-B, C, and D branches to the north. The Massachusetts Avenue Orange Line station located to the south of the site provides access from the most southern station of Forest Hills, Hyde Park through Downtown Crossing to Oak Grove, Malden in the north. The Green Line branches provide access from the Cambridge Lechmere Station and Government Center Station to Newton, Brookline and Brighton to the west.

3.2.6.3 MBTA Commuter Rail Services

Four commuter rail lines are accessible in the vicinity of the Project site. The Providence/Stoughton line, the Franklin/Forge Park line, and the Needham Heights line are accessible from Ruggles Station, just over one-half mile away from the site. In addition, Back Bay Station is located less than a mile away from the Project site and provides access to the previously listed lines in addition to the Worcester/Framingham line. All four of these commuter rail lines terminate at South Station in Boston.

Table 3-3 provides a summary of the rush-hour frequencies for MBTA service in the area.

Table 3-3 Available Public Transportation Service

Route	Origin/Destination	Peak Hour Headway (Outbound) ¹	
Framingham/Worcester Commuter Rail Line	South Station to Worcester/Union Station	varies	
Providence/Stoughton Commuter Rail Line	South Station to North Kingston, RI	varies	
Franklin/Forge Park Commuter Rail Line	South Station to Forge Park	varies	
Needham Heights Commuter Rail Line	South Station to Needham Heights	varies	
Green Line – B Branch	Government Center Station to Boston College Station	6 Minutes	
Green Line – C Branch	North Station to Cleveland Circle Station	7 Minutes	
Green Line – D Branch	Government Center Station to Riverside Station	6 Minutes	
Green Line – E Branch	Lechmere Station to Heath Street Station	6 Minutes	

Table 3-3 Available Public Transportation Service (Continued)

Route	Origin/Destination	Peak Hour Headway (Outbound) ¹
Route CT1	Central Square to BU Medical Center	20 Minutes
Route 1	Harvard Gate to Dudley Station	10 Minutes or Less
Route 39	Forest Hills Station to Back Bay Station	10 Minutes or Less
Route 55	Jersey and Queensbury to Copley Square	17-30 Min
Route 170	Central Square, Waltham to Dudley Square	2 Trips Each Peak

¹ Source: Massachusetts Bay Transportation Authority website at www.mbta.com

3.2.7 On-Street Parking

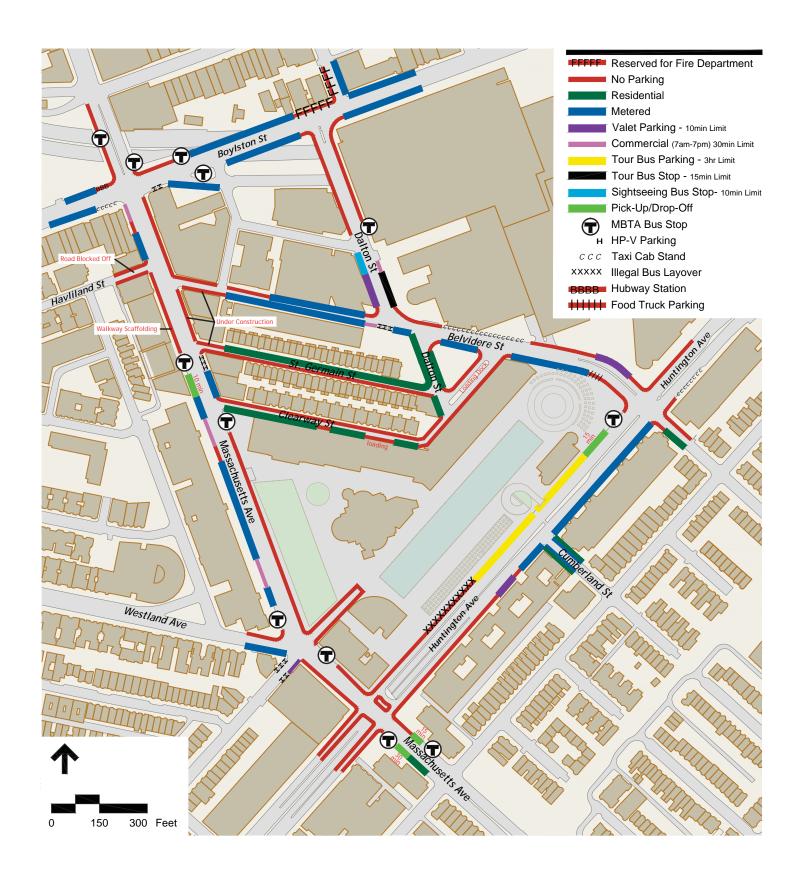
Information regarding curb use within a one-quarter mile walk of the Project site was collected and is graphically shown in Figure 3.2-9. Residential permit parking is permitted along both sides of Dalton Street adjacent to the site and metered parking is provided along Belvidere Street north of the High-rise site.

3.2.8 Public Off-Street Parking

Public Parking is provided at the First Church of Christ, Scientist's Plaza Garage which currently contains approximately 550 parking spaces, 100 of which are available for Commercial use. Access to this garage is provided on Huntington Avenue and Massachusetts Avenue near the southwest corner of the campus. Additional parking is provided on the Mid-rise site which contains approximately 63 public parking spaces that will be transferred to the First Church of Christ, Scientist's Garage.

3.3 Evaluation of Long-Term Transportation Impacts

This section describes the future transportation infrastructure in the study area and the impacts of the Proposed Project. Included is a summary of area transportation infrastructure improvements that are currently planned, are under design, or are under construction by area institutions/developers, the City of Boston, Commonwealth of Massachusetts, and MBTA. Also in this section is a detailed summary of the development of both the future 2018 No-Build and 2018 Build Conditions, including a detailed analysis of morning and evening peak hour traffic activity and operations, parking supply and demands, loading and service accommodations, future pedestrian and bicycle demands, and future transit demands. The development and evaluation of the 2018 No-Build and Build Conditions has been conducted to help identify additional roadway and pedestrian improvements that may be needed to mitigate identified transportation impacts generated by future proposed projects.



3.3.1 No-Build Condition

The 2018 No-Build Condition was developed and analyzed to evaluate future transportation conditions in the Study Area without consideration of the Proposed Project.

This future analysis year represents a 5-year horizon from the 2013 Existing Condition. Under the No-Build Condition, anticipated increases in traffic activity on Study Area roadways due to continued general area-wide traffic growth and approved developments in the area are added to the defined morning and evening peak hour traffic networks.

3.3.1.1 Step 1 – Account for Background Traffic Growth

The first step in projecting No-Build traffic volumes was to estimate general area-wide traffic growth and determine an annualized growth rate that could be applied to existing condition peak hour traffic volumes to reasonably account for future traffic growth in the project Study Area. No-Build Conditions utilize an annual growth rate of 0.5 percent per year from 2013 to 2018. This background growth rate is consistent with rates used to estimate future traffic conditions for other developments planned in the area.

3.3.1.2 Step 2 – Development Projects

There are currently eight approved or planned development projects that are expected to have an influence on future year peak hour traffic volumes on Study Area roadways and intersections. A description of each applicable project and/or master plan is provided below.

- ♦ <u>350 Boylston Street</u>: This approved 9-story office building will include 221,230 square feet of office space, with ground level retail, a health club and 150 underground parking spaces. The project status with the BRA is listed as "Board Approved" and last updated June 2013.
- ♦ 212-222 Stuart Street Development: This project includes the construction of a 10story building containing 65,700 square feet of retail and office space. The project status with the BRA is listed as "Board Approved" and last updated March 2013.
- ◆ <u>Liberty Mutual at 157 Berkeley Street</u>: The project includes the construction of a 590,000 square feet (22-story) office building and renovation to the existing Liberty Mutual sites on Stuart Street, Berkley Street, St. James Avenue and Columbus Avenue. Parking for up to 205 vehicles will be provided in a below grade parking structure (87 net new spaces). The Project is set to open in the coming weeks.

- ♦ Columbus Center: This approved project program includes approximately 1.1 million square feet of development and over 900 parking spaces. The program is comprised of a 199-room hotel, 493 residential units and ground floor retail. The project status with the BRA is listed as "Board Approved" and last updated November 2009.
- Prudential Center Redevelopment: This project includes the construction of a 188-unit residential building (Exeter Residences) as well as development of a 19-story (362,000 square feet) office building, known as 888 Boylston Street. The project status with the BRA is listed as "Board Approved" and last updated June 2013. The Exeter Residences portion of the project is under construction.
- Mass College of Pharmacy- Huntington Avenue Academic Building: The project includes the construction of a 6-story building (49,700 square feet). The proposed structure will provide classroom and auditorium space for approximately 250 students and office space to accommodate approximately 50 employees. Additionally, a 250-seat auditorium will accommodate lectures and guest speakers. No new parking will be provided. The project status with the BRA is listed as "Board Approved" and last updated February 2009.
- ♦ 41 Westland Avenue: The project includes the redevelopment of the site into a 7-story (67,000 square feet) building with up to 48 residential condominiums and up to 31 parking spaces within a street level garage. The project status with the BRA is listed as "Under Construction" and last updated January 2013.
- ◆ Copley Place Residential and Retail Expansion: This project includes approximately 114,000 square feet of new retail (54,000 of Neiman Marcus and 60,000 square feet of restaurant, shops and a garden) as well as a 660,000 square feet residential tower. The project status with the BRA is listed as "Board Approved" and last updated March 2012.

Additional planned or approved projects in the area were not included in this list due to the fact that they are not expected to influence future year peak hour traffic on study area roadways.

3.3.1.3 Infrastructure Changes

The Boston Transportation Department and Department of Public Works is planning and designing streetscape and transportation improvements in the Project Study Area known as the Symphony Streetscape Project. The construction of the streetscape and transportation improvements will commence in the summer of 2013. The final design includes proposed improvements along a portion of Massachusetts Avenue, from St. Botolph Street to Westland Avenue. Primary transportation improvements include the incorporation of the Christian Science Plaza driveway on Massachusetts Avenue into the signal control at the

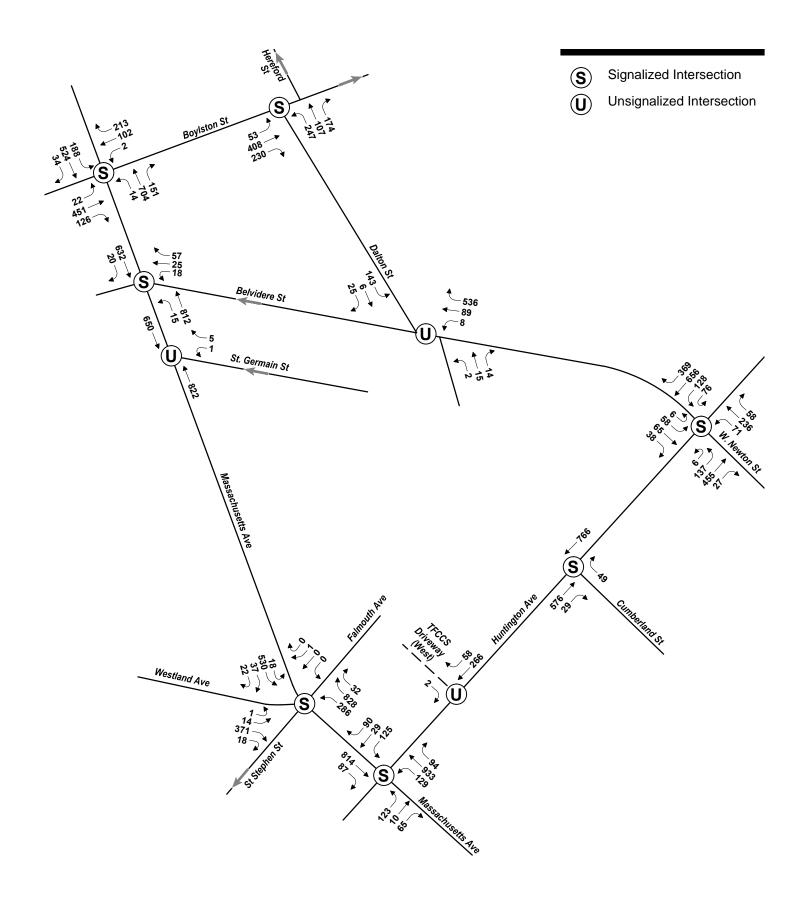
intersection of Massachusetts Ave/Westland Street/ St. Stephen Street with new signal equipment. Signal phasing and timing upgrades as well as a new pedestrian crosswalk, enhancement of handicap accessibility features and the relocation of bus stops greatly improve the pedestrian and vehicular conditions at this key location. The City is also planning bicycle accommodations as part of the overall roadway improvement to this section of Massachusetts Avenue. Signal improvements and streetscape enhancements are also planned for Huntington Avenue at Massachusetts Avenue. All of these changes to the existing roadway and intersection infrastructure have been accounted for and assumed in this future analysis.

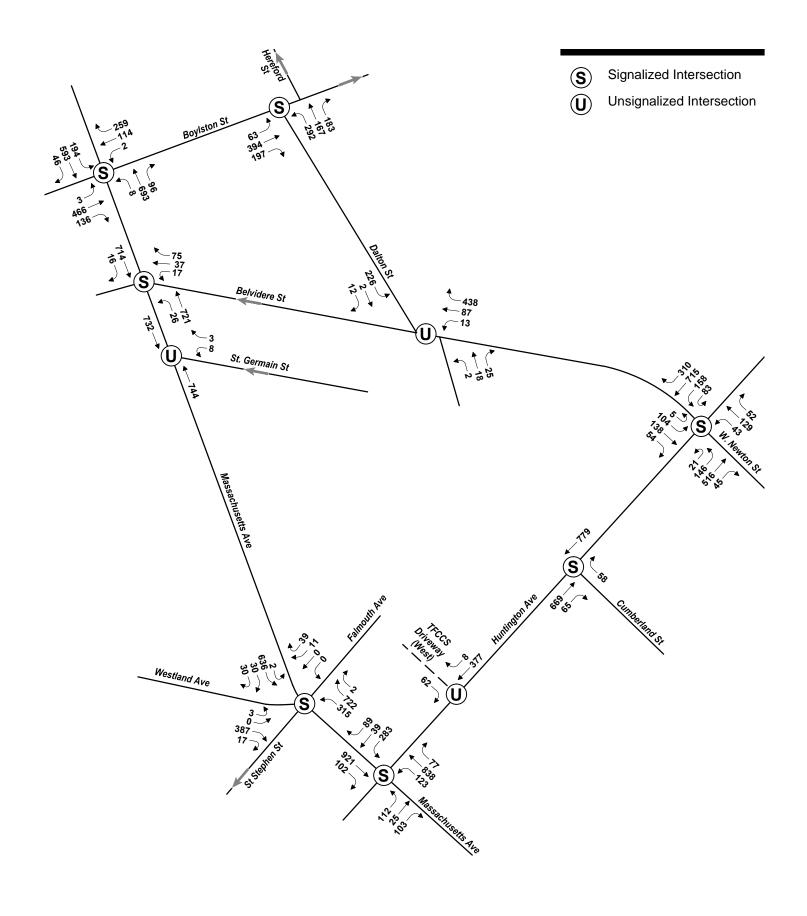
3.3.1.4 2018 No-Build Traffic Volumes

The 2013 Existing Condition volumes were adjusted to 2018 with a growth rate of 0.5 percent per year. The eight area projects that are either planned, approved and/or under construction were added to these adjusted volumes to create the 2018 No-Build Condition weekday morning and evening peak hour traffic volumes. Figures 3.3-1 and 3.3-2 present the 2018 No-Build Condition traffic volume networks for the weekday morning and evening peak hours, respectively.

3.3.2 Build Condition

The 2018 Build Condition was developed in order to evaluate future transportation conditions in the study area with the Belvidere/Dalton Project in place. The 2018 study year represents a five year planning horizon. The Build Condition takes into account the changes and growth established as part of the 2018 No-Build Condition presented previously, and also accounts for the changes that will occur with the Proposed Project. 2018 Build Condition traffic volumes for study area roadways were developed by estimating Project-generated traffic volumes, distributing these volumes, and assigning them to the study area roadways. The traffic volumes expected to be generated by the Proposed Project were added to the 2018 No-Build Condition traffic volumes to create the year 2018 Build Condition traffic volume networks. The following sections describe the procedures used to develop the Build Condition traffic volume networks.





3.3.2.1 Site-Generated Traffic Volumes

Unadjusted Trip Generation

To estimate traffic impacts of the Proposed Project, it is necessary to determine the traffic volumes expected to be generated by the new Belvidere/Dalton Project.

The trip generation for the Residential and Hotel land uses was based on standard Institute of Transportation Engineers (ITE) trip rates published in ITE's Trip Generation manual (8th Edition). ITE's Land Use Codes Condominiums (230), Hotel (310), and Apartments (220) were used to estimate the new trips generated by the Project. Since Hotel (310) is defined as containing retail such as restaurant space within the use in the ITE Trip Generation manual, the restaurant space was not analyzed separately but assumed to be included in the Hotel generated trips. A standard vehicle occupancy rate (VOR) of 1.2 persons per vehicle was applied to determine person-trips rates. These trips are presented in Table 3-4.

Table 3-4 Trip Generation Estimates

		ITE Trip Generation	VOR	Person Trips
Weekday Daily	In	2,402	1.2	2,882
	Out	2,402	1.2	2,882
	Total	4,804	1.2	5,764
Weekday Morning Peak Hour	In	125	1.2	150
	Out	221	1.2	266
	Total	346	1.2	416
Weekday Evening Peak Hour	In	243	1.2	292
	Out	157	1.2	189
	Total	400	1.2	481

Source: Institute of Transportation Engineers, Trip Generation 8h Edition

Adjustments to Trip Generation

Trip generation estimates presented in Table 3-4 do not include any adjustments to reflect public transit, walking trips, or bicycling trips that are characteristic of an urban downtown location.

As previously discussed, the Belvidere/Dalton Project will benefit from MBTA bus and transit services. There will also be a measurable component of walking and bicycling trips to and from the surrounding downtown.

The BTD reference documents published under the Access Boston 2000-2010 (May 2002) initiative were assumed for the mode share splits for the Trip Generation Estimate and are provided in Table 3-5.

Table 3-5 Mode Shares

	Auto	Transit	Walk/Other
Residential			
Daily	24%	19%	57%
AM/PM Peak	21%	15%	64%
Other – Hotel			
Daily	29%	16%	55%
AM/PM Peak	26%	13%	61%

Source: BTD - Access Boston 2000-2010 (May 2002) initiative

The adjusted trip generation estimates are presented in Table 3-6. As shown, the Proposed Project is expected to generate a total of 80 new vehicle trips (31 entering, and 49 exiting) during the weekday morning peak hour, and a total of 92 new vehicle trips (55 entering, and 37 exiting) during the weekday evening peak hour. On a daily basis, the Proposed Project is expected to generate 1,258 new vehicle-trips (629 entering, and 629 exiting) on a weekday.

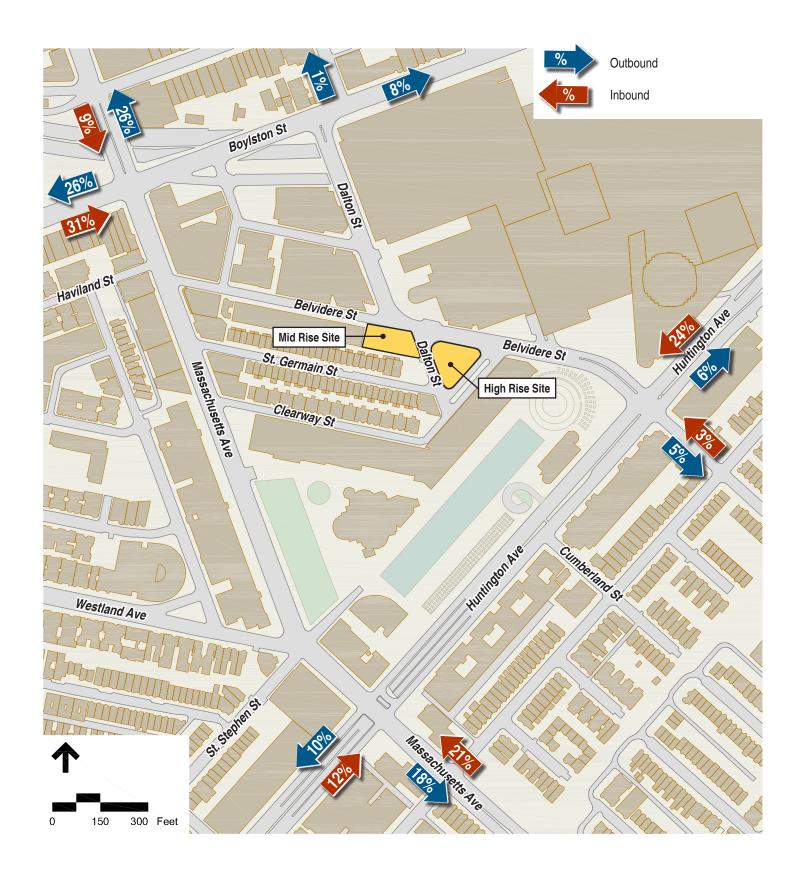
Table 3-6 Trip Generation by Mode

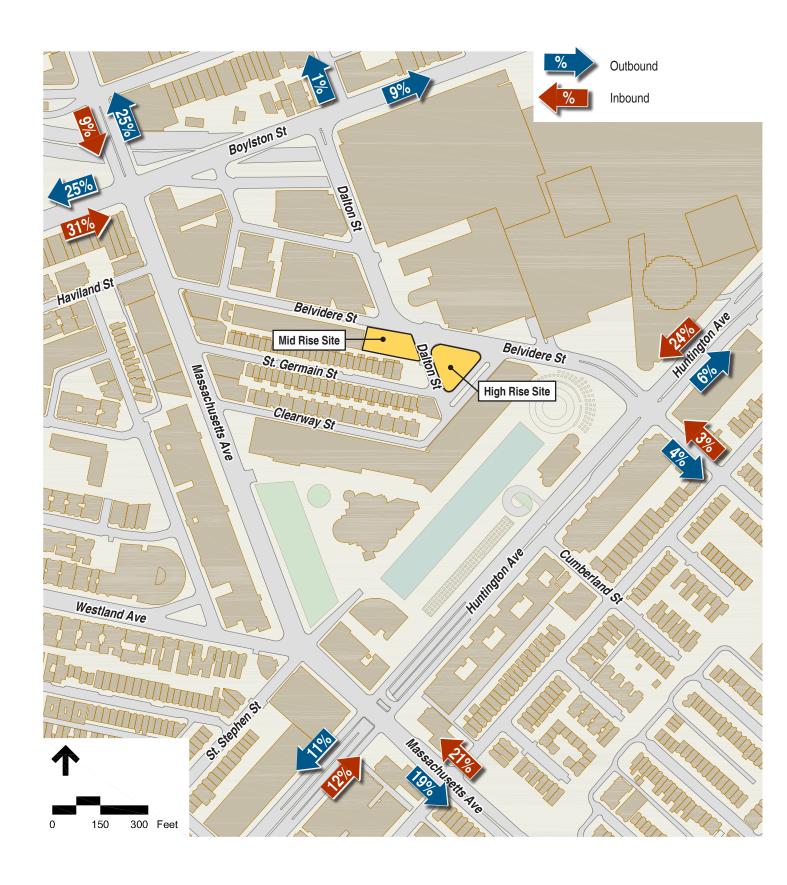
			Person Trips	VO R	Auto Trips	Transit Trips	Walk Trips
Weekday Daily		Enter	2,882	1.2	629	509	1,617
		Exit	2,882	1.2	629	509	1,617
		Total	5,764	1.2	1,258	1,018	3,234
Weekday Mornin	g Peak	Enter	150	1.2	31	20	93
Hour							
		Exit	266	1.2	49	39	168
		Total	416	1.2	80	59	261
Weekday Evening	z Peak	Enter	292	1.2	55	42	184
Hour	, . cur	Lincol			. 55		.51
		Exit	189	1.2	37	27	118
		Total	481	1.2	92	69	302

Trip Distribution and Assignment

Having estimated increases in auto trips associated with the Proposed Project, the next step in the analysis involves the assignment of these trips to the local roadway network based on geographic distribution of Project traffic. The directional distribution of Project traffic is a function of several variables. These include the relative locations and densities of population, competing uses, existing travel patterns, and the efficiency of the roadways leading to the site.

Trip distribution patterns were developed based on Access Boston 2000-2010 (May 2002) trip distribution data. They are summarized in the attached Figures 3.3-3 and 3.3-4.





3.3.2.2 2018 Build Condition Improvements

The 2018 Build Condition includes the following improvements to the existing transportation infrastructure in the study area. The improvements associated with the Project are described in the following bullets:

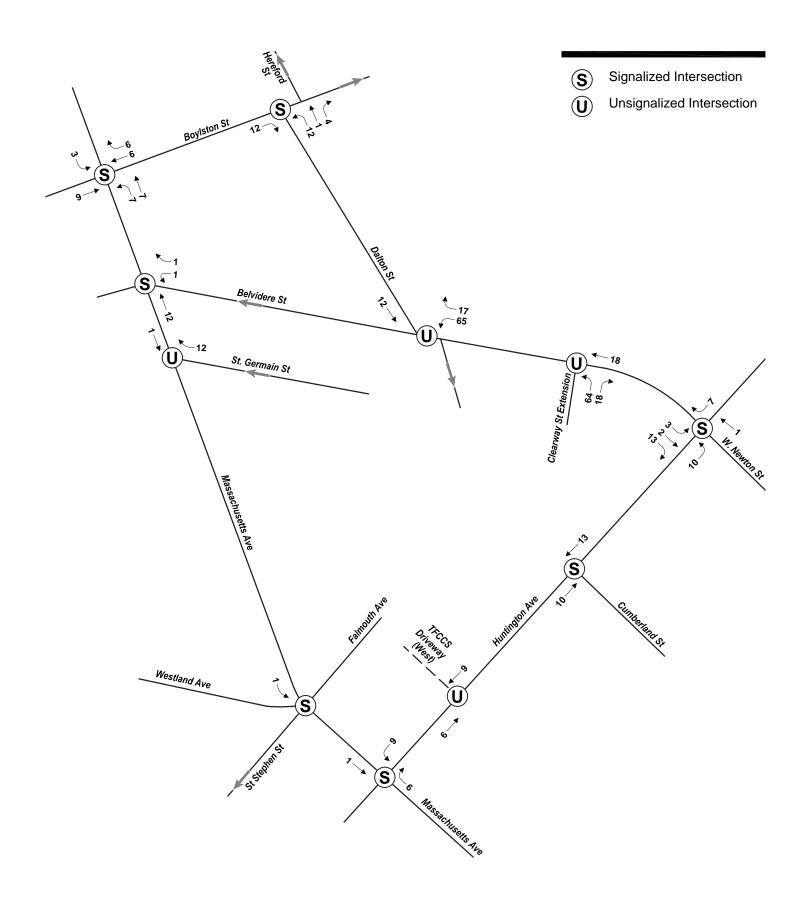
- Modification of Dalton Street between Saint Germain Street and Belvidere Street to provide one-way travel in the south bound direction.
- Creation of a Valet/drop-off/pick-up curb area along the east side of Dalton Street for hotel valet operations.
- Creation of a Valet/drop-off/pick-up curb area along the east side of the Mid-rise site on Dalton Street
- Modification of Clearway Street so it extends from Dalton Street to Belvidere Street to create the Clearway Street Extension. This will provide two-way access to the proposed parking ramp below the High-rise Building and residential drop-off/pickup. Clearway Street Extension will approach Belvidere Street with stop control.
- Redesign of the Belvidere Street/Dalton Street intersection to include a realigned intersection with improved sight distance while maintaining the stop control in the Dalton Street southbound direction. This intersection will contain only two approaches: Belvidere Street westbound and Dalton Street southbound. The Belvidere Street westbound approach will be striped to include a left/through lane and an exclusive right turn lane at the intersection. Crosswalks will be provided at the newly formed intersection to improve pedestrian circulation.

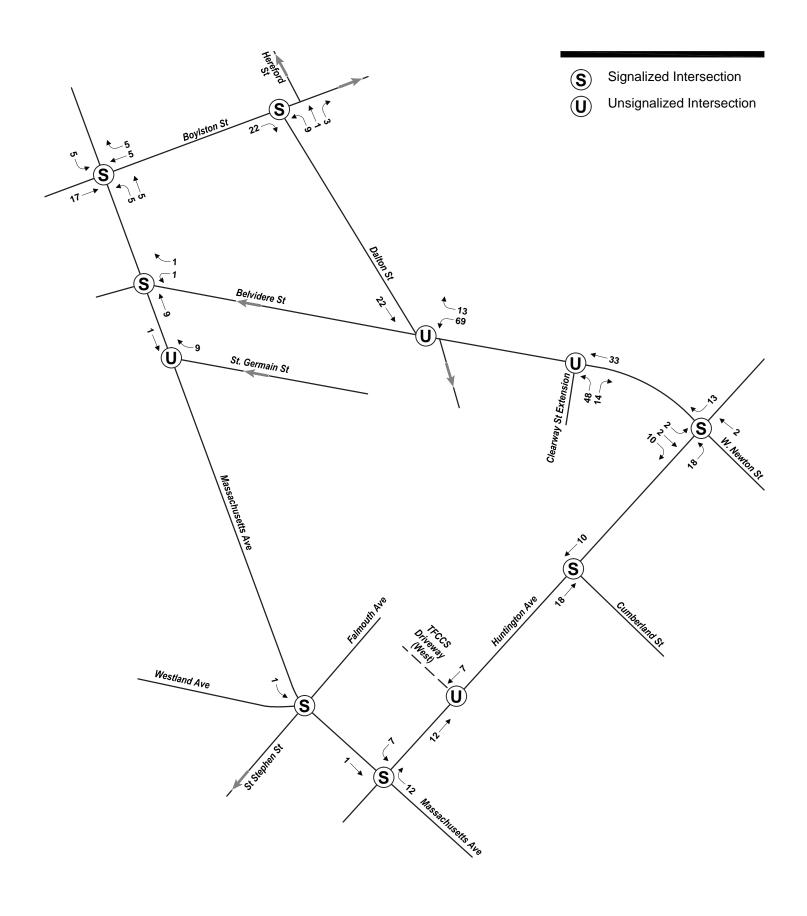
All of these improvements will be designed in consultation with the Boston Transportation Department and Public Improvements Commission. These modifications have been included in the 2018 Build Condition capacity analysis scenarios.

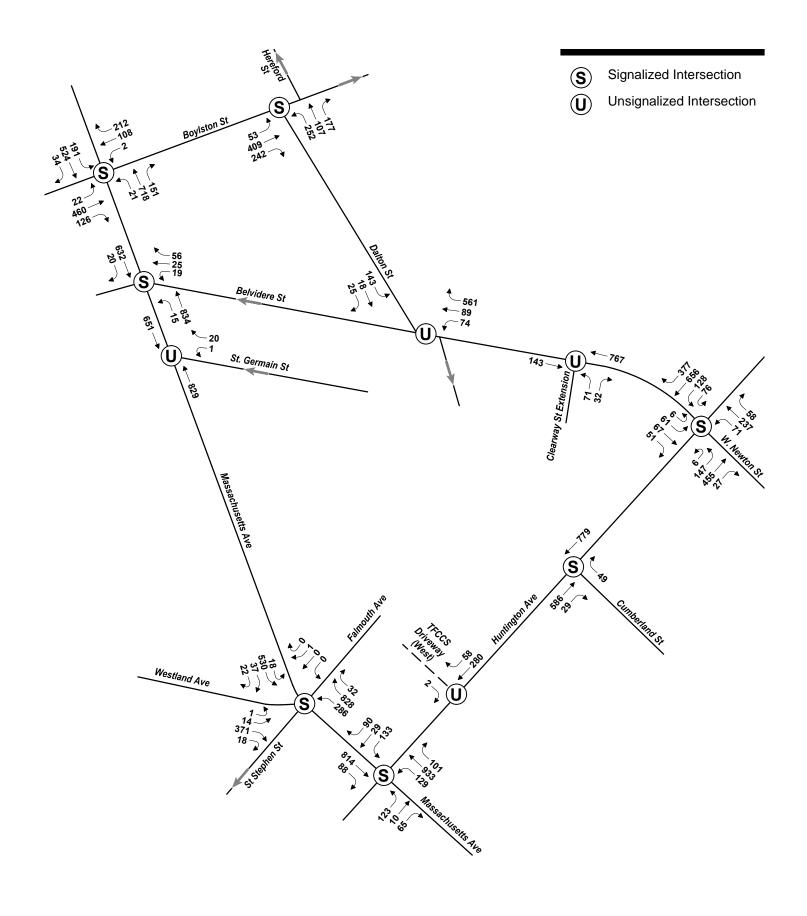
3.3.2.3 2018 Build Condition Traffic Networks

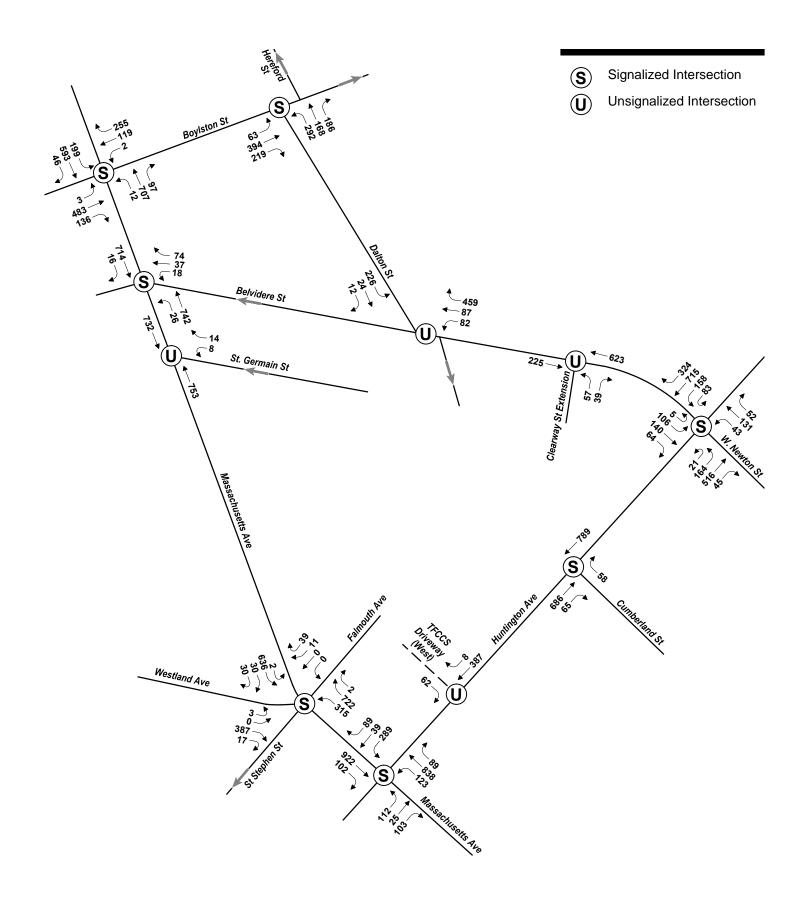
Based upon the trip distribution patterns described above, the new Project-generated traffic volumes were assigned to the roadway network. The Project generated trips are shown graphically in Figures 3.3-5 and 3.3-6. The new trips were combined with the 2018 No-Build Condition traffic volumes to provide the 2018 Build Condition peak hour traffic networks.

The 2018 Build Condition traffic volume networks are presented in Figures 3.3-7 and 3.3-8 for the weekday morning and evening peak hours, respectively.









3.3.2.4 Pedestrians

As shown previously in Table 3-6, the Proposed Project is expected to generate 261 morning peak hour pedestrian trips and 302 evening peak hour pedestrian trips. It is expected that hotel patrons will walk to nearby amenities and destinations within the Back Bay neighborhood.

3.3.2.5 Transit

As shown previously in Table 3-6, the Project is expected to generate a total of 59 transit trips during the morning peak hour and 69 transit trips during the evening peak hour. As discussed in the transit section 5.2.5, this Project site is well served by existing transit infrastructure. The transit trips generated by the Project will be able to easily access the Green Line, Bus Lines and the Commuter Rail.

3.3.2.6 Bicycle Parking

Bicycle parking will be provided for employees of the retail and hotel uses as well as residents of the buildings. In the High-rise Building, 220 bicycle parking spaces will be provided below grade. In the Mid-rise Building, approximately 240 bicycle parking/ storage spaces will be primarily provided below grade in the parking garage.

3.3.2.7 Parking and Valet Operations

High-rise Site

The parking needs of the proposed Belvidere/Dalton High-rise site will be met in The First Church of Christ, Scientist's existing below grade plaza garage that currently contains approximately 550 parking spaces as well as additional parking to be provided in the basement of the 101 Belvidere Street Building containing approximately 50 new spaces. Since valet parking will be provided, this will effectively increase the number of vehicles which can be parked in the garage to a total of approximately 726. This results in a net increase in parking capacity of the Garage of 113 vehicles, after taking into account the elimination of 63 commercial parking spaces from the Mid-rise site and the transfer of those spaces to the garage. The First Church has granted to the High-rise Developer the right to park 400 vehicles in the garage and the High-rise Developer will make available to the Midrise Developer the right to park 60 vehicles (from the 400). The new spaces below the 101 Belvidere Building will connect to the ramp below the High-rise Building (off of the Clearway Street Extension) as well as the existing Plaza garage.

Mid-rise Site

The proposed Belvidere/Dalton Mid-rise site will contain approximately 21 parking spaces, including some tandem spaces, below grade for a portion of the residents to park. The access ramp to this parking will be provided behind the building along the alley accessed off of Dalton Street. Additional parking for up to 60 vehicles will be provided for residents of the Mid-rise Building from the 400 spaces available to the High-rise building under the 101 Belvidere Street Building and in the existing Plaza Garage.

Valet operations for the hotel and the residential uses will be provided along Dalton Street near the south edge of the Belvidere/Dalton High-rise building. Valet operators will meet drivers on the curb and then park their vehicles in the 101 Belvidere Street Building basement or the Plaza Garage. It is expected that all of the hotel patrons and the majority of the residents will utilize the valet parking service.

3.3.2.8 Loading & Service Activity

The First Church of Christ, Scientist Loading and Service

The First Church of Christ, Scientist's existing site currently utilizes the loading and service ramp to an underground service area accessed off of Belvidere Street. This ramp is located along the 101 Belvidere Street building and due to the constrained space, uses a turn table below grade to re-direct the entering and exiting trucks on the ramp. Due to the modification of this driveway and ramp structure in association with the proposed High-rise building, the existing loading and service activity at this location will be relocated to the existing loading docks on Clearway Street. Clearway Street currently contains a curb cut of 36 feet 9 inches and another curb cut of 94 feet 3 inches for loading and service activity with two existing docking areas, which were historically used for both the Christian Science Monitor as well as servicing church administrative offices within the Publishing House Building. As The Christian Science Monitor is no longer printed on site, these docks have the continued capacity to service the Publishing House Building as well as the capacity to service any heavy delivery needs for the 101 Belvidere building.

Clearway Street currently has approximately three trucks per day that utilize the designated loading and service curb. Currently, the below-grade ramp on the private driveway has approximately seven trucks per day. All of these seven trucks will be relocated to Clearway Street for a total of approximately ten trucks per day at the Clearway Street loading area. Trucks make deliveries between 7:30 a.m. and 11:30 a.m., and again between 2:45 p.m. – 3:45 p.m. but predominately between 8:00 a.m. – 10:00 a.m. Trucks will depart the Clearway Street loading area and continue on through to Belvidere Street via the Clearway Street Extension. Saint Germain Street will not be utilized as a truck route for departing loading and service vehicles. The following table summarizes the existing and proposed loading and service activity for The First Church of Christ, Scientist.

Table 3-7 TFCCS Loading and Service Activity During Typical Levels*

	Existing Loading (# of Trucks Per Day)	Future Loading (# of Trucks Per Day)
Below-grade Ramp Loading	7	0
Clearway Street Loading	3	10
Belvidere Street Loading	3	3

^{*}Activity will increase during either Church or Tenant renovation projects.

High-rise Loading and Service

The Dalton/Belvidere High-rise loading and service area will be located off of the Clearway Street Extension. As currently planned, the building will be served by three loading bays, two for large trucks and a third intended to house a compactor for the building.

Mid-rise Loading and Service

The Dalton/Belvidere Mid-rise building will contain a loading dock off of Belvidere Street on the north side of the building. This will provide trash removal and move in/move out operations.

3.4 Level of Service Operations

This section presents the transportation operations analyses for vehicular operations at study area intersections. These operations analyses provide a summary of transportation capacities and overall operations as they relate to delay and congestion.

3.4.1 Intersection Level of Service (LOS) Operations

Vehicle Level of Service (LOS) is a qualitative measure of control delay at an intersection providing an index to the operational qualities of a roadway or intersection. LOS designations range from A to F, with LOS A representing the best operating conditions and LOS F representing the worst operating conditions. LOS A through D are considered acceptable, while LOS E indicates vehicles endure significant delay and LOS F suggests unacceptable delay for the average vehicle. LOS thresholds differ for signalized and unsignalized intersections with longer delays at signalized intersections perceived as acceptable.

Table 3-8 below presents the LOS delay threshold criteria as defined in the 2000 Highway Capacity Manual (HCM). A LOS D is typically considered acceptable in an urban environment.

Table 3-8 Level of Service Criteria

Level of Service (LOS)	Unsignalized Intersection Control Delay (sec/veh)	Signalized Intersection Control Delay (sec/veh)
A	<u><</u> 10	<u><</u> 10
В	> 10 - <u><</u> 15	> 10 - <u><</u> 20
С	> 15 - < 25	> 20 - <u><</u> 35
D	> 25 - <u><</u> 35	> 35 - <u><</u> 55
E	> 35 - <u><</u> 50	> 55- <u><</u> 80
F	> 50	> 80

Source: 2000 HCM

Consistent with BTD's guidelines, Synchro 6 software was used to model LOS operations at the study area intersections. Adjustments were made to the Synchro model to include characteristics of the study area such as heavy vehicles, bus operations, parking activity, and pedestrian crossings.

Signalized Intersection Capacity Analysis

Capacity analyses were conducted for the seven existing signalized intersections identified in the Study Area. A capacity analysis was conducted for 2013 Existing conditions and the 2018 No-Build and Build Conditions. A summary of the signalized capacity analysis is presented in Table 3-9 and Table 3-10.

Table 3-9 Morning Peak Hour Signalized Intersection Capacity Analysis Results

	2013 Existing Condition 2018 No Build Condition		ondition	2018	Build Con	dition			
Approach	v/c ¹	Delay ²	LOS ³	v/c ¹	Delay ²	LOS ³	v/c ¹	Delay ²	LOS ³
Boylston Street at Massachusetts A	venue								
Eastbound – Thru/Right	0.98	70.5	Е	>1.0	>80	F	>1.0	>80	F
Westbound – Left/Thru	0.45	33.4	С	0.46	33.5	C	0.49	33.8	C
Westbound – Right	0.37	32.8	С	0.38	32.9	C	0.37	32.9	C
Northbound – Thru/Right	0.92	27.8	С	>1.0	>80	F	>1.0	>80	F
Southbound – Left	0.59	39.6	D	0.61	40.4	D	0.62	40.8	D
Southbound – Thru/Right	0.33	8.3	A	0.35	8.5	A	0.35	8.5	A
Overall	0.83	35.1	D	0.94	55.5	E	0.96	61.8	E
Belvidere Street at Massachusetts		33.1	D	0.94	33.3	L	0.90	01.0	L
Westbound – Left/Thru/Right	0.58	42.3	D	0.59	42.4	D	0.59	42.7	D
Northbound – Left/Thru	0.50	3.9	A	0.59	6.7	A	0.59	7.1	A
	0.31							8.2	
Southbound – Thru/Right		8.0	A	0.45	8.2	A	0.45		A
Overall	0.53	8.7	Α	0.59	9.9	А	0.61	10.1	В
St. Stephen at Massachusetts Aven				0.00	10.0	Б	0.00	40.0	
Westbound – Left/Thru/Right	-	-	-	0.02	40.9	D	0.02	40.9	D
Northbound – Left	0.90	37.0	D	0.75	45.1	D	0.75	44.6	D
Northbound – Thru/Right	0.41	1.7	A	0.43	1.4	A	0.43	1.4	A
Southbound – Left/Thru/Right	0.98	61.5	E	0.73	26.2	С	0.73	26.3	С
Southeastbound – Thru/Right	0.89	49.7	D	0.67	33.9	С	0.67	33.9	С
Overall	0.93	33.1	С	0.66	20.1	С	0.66	20.1	С
Huntington Avenue at Massachuse		1	1	1	1		1	ı	
Eastbound – Left/Thru/Right	0.38	37.4	D	0.76	50.9	D	0.76	50.9	D
Westbound – Left/Thru/Right	0.42	37.7	D	-	-	-	-	-	-
Westbound – Left/Thru	-	-	-	0.85	67.2	E	0.88	70.5	E
Westbound – Right	-	-	-	0.47	37.8	D	0.46	37.4	D
Northbound – Left	-	-	-	0.68	47.3	D	0.70	48.5	D
Northbound – Thru/Right	>1.0	56.0	E	0.92	34.9	С	0.94	37.4	D
Southbound – Thru/Right	-	-	-	>1.0	>80	F	>1.0	>80	F
Southbound – Thru	0.78	12.7	В	-	-	-	-	-	-
Southbound – Right	0.15	<i>7</i> .1	Α	-	-	1	-	-	-
Overall	0.75	36.8	D	>1.0	>80	F	>1.0	>80	F
Huntington Avenue at Cumberlan	d Street								
Eastbound – Thru/Right	0.19	3.2	Α	0.22	3.3	Α	0.22	3.3	Α
Westbound – Thru	0.16	0.8	А	0.18	0.8	Α	0.18	0.8	Α
Northbound – Right	0.05	39.0	D	0.05	39.0	D	0.05	39.0	D
Overall	0.20	3.8	А	0.21	3.7	Α	0.21	3.7	Α
Huntington Avenue at Belvidere S	treet	•	•	•	•			•	•
Eastbound – Left	0.83	65.6	E	0.84	66.2	E	0.86	69.9	E
Eastbound – Thru/Right	0.53	29.0	С	0.62	31.3	С	0.62	31.5	С
Westbound – Left	0.93	71.9	Е	0.94	77.1	E	0.94	77.1	E
Westbound – Thru	0.61	30.6	С	0.69	32.8	С	0.70	33.9	С
Westbound – Right	0.49	74.7	Е	0.56	79.7	E	0.58	>80	F
Northbound – Left/Thru/Right	0.90	55.4	Е	0.91	57.5	E	0.91	57.8	E
Southbound – Left	0.26	24.3	С	0.26	24.1	С	0.27	24.1	С
Southbound – Thru/Right	0.08	19.4	В	0.08	19.2	В	0.08	19.2	В
Overall	0.70	46.1	D	0.74	48.3	D	0.74	49.5	D
Boylston Street at Dalton Street		1		1	1 2.2			1 2.2	
Eastbound – Thru/Right	0.47	18.0	В	0.65	22.7	С	0.66	23.2	С
Northbound – Left	0.77	39.7	D	0.72	34.7	C	0.72	35.0	C
Northbound – Thru/Right	0.85	49.1	D	0.91	56.5	E	0.91	56.4	E
Overall	0.60	30.2	C	0.75	33.0	C	0.75	33.2	C
Overall	0.00	30.2		0.73	1 : 1	Č	0.73	33.4	

¹ V/C = volume to capacity ratio 3 LOS = Level of Service

2 Delay = Average delay in seconds per vehicle Delay cannot be accurately estimated for v/c ratio greater than 1.0

Table 3-10 Evening Peak Hour Signalized Intersection Capacity Analysis Results

	2013 E	xisting Co	ndition	2018 N	No Build C	ondition	2018	Build Con	dition
Approach	v/c¹	Delay ²	LOS ³	v/c ¹	Delay ²	LOS ³	v/c ¹	Delay ²	LOS ³
Boylston Street at Massachusetts		20.07					.,,,		
			-	0.05	42.4		0.0=	45.0	-
Eastbound – Thru/Right	0.83	41.7	D	0.85	43.4	D	0.87	45.2	D
Westbound – Left/Thru	0.29	29.2	С	0.29	28.8	С	0.30	28.8	С
Westbound – Right	0.33	29.8	С	0.34	29.5	C	0.34	29.5	С
Northbound – Thru/Right	0.83	20.2	С	0.91	32.5	C	0.94	32.7	С
Southbound – Left	0.62	44.9	D	0.64	45.8	D	0.66	46.6	D
Southbound – Thru/Right	0.37	10.4	В	0.40	10.9	В	0.40	11.0	В
Overall	0.78	26.3	С	0.82	30.5	С	0.85	31.1	С
Belvidere Street at Massachusett					1 1		T		
Westbound – Left/Thru/Right	0.66	44.4	D	0.67	44.4	D	0.67	44.5	D
Northbound – Left/Thru	0.55	19.6	В	0.59	25.5	С	0.60	21.8	С
Southbound – Thru/Right	0.48	9.8	Α	0.51	10.0	Α	0.51	9.9	Α
Overall	0.58	17.6	В	0.61	20.3	С	0.62	18.6	В
St. Stephen at Massachusetts Av	enue	ı		1	1		ı		
Westbound – Left/Thru/Right	-	-	-	0.49	46.7	D	0.49	38.8	D
Northbound – Left	0.77	26.2	С	0.82	34.8	С	0.82	55.5	E
Northbound – Thru/Right	0.33	1.4	Α	0.34	8.0	Α	0.34	1.0	Α
Southbound – Left/Thru/Right	>1.0	53.4	D	0.71	16.0	В	0.71	11.9	В
Southeastbound – Thru/Right	0.91	50.9	D	0.70	34.0	С	0.70	36.3	D
Overall	0.91	31.5	С	0.70	18.9	В	0.70	20.5	С
Huntington Avenue at Massach	usetts Ave	enue							
Eastbound – Left/Thru/Right	0.44	37.9	D	0.95	62.1	E	0.96	63.2	E
Westbound – Left/Thru/Right	0.58	39.8	D	-	-	-	-	-	1
Westbound – Left/Thru	-	-	-	>1.0	>80	F	>1.0	>80	F
Westbound- Right	-	-	-	0.38	34.6	C	0.38	34.6	С
Northbound – Left	-	-	-	0.83	70.9	E	0.83	70.9	E
Northbound – Thru/Right	0.87	34.2	С	0.82	28.9	С	0.83	29.7	С
Southbound – Thru/Right	-	-	-	>1.0	>80	F	>1.0	>80	F
Southbound – Thru	0.87	13.7	В	-	-	-	-	-	-
Southbound – Right	0.17	6.2	Α						
Overall	0.72	26.7	С	>1.0	>80	F	>1.0	>80	F
Huntington Avenue at Cumberl	and Stree	t							
Eastbound – Thru/Right	0.23	3.8	Α	0.25	3.9	Α	0.25	3.9	Α
Westbound – Thru	0.15	1.1	Α	0.19	1.1	Α	0.19	1.1	Α
Northbound – Right	0.06	39.1	D	0.06	39.1	D	0.06	39.1	D
Overall	0.22	4.5	Α	0.23	4.2	Α	0.24	4.2	Α
Huntington Avenue at Belvidere	Street								
Eastbound – Left	0.80	62.6	E	0.81	63.3	E	0.84	66.9	E
Eastbound – Thru/Right	0.51	27.5	С	0.57	29.1	С	0.57	29.3	С
Westbound – Left	0.92	78.5	E	0.93	>80	F	0.93	>80	F
Westbound – Thru	0.48	24.4	С	0.62	27.7	С	0.63	28.9	С
Westbound – Right	0.51	30.4	С	0.68	39.9	D	0.72	44.0	D
Northbound – Left/Thru/Right	0.73	48.4	D	0.74	48.8	D	0.74	48.8	D
Southbound – Left	0.45	31.8	С	0.46	31.7	С	0.47	31.7	С
Southbound – Thru/Right	0.18	26.9	С	0.18	26.7	C	0.18	26.7	С
Overall	0.64	37.0	D	0.73	38.9	D	0.72	40.1	D
Boylston Street at Dalton Street			1		<u> </u>				1
Eastbound – Thru/Right	0.49	20.4	С	0.56	22.2	С	0.58	22.8	С
Northbound – Left	0.68	32.0	C	0.67	30.8	C	0.66	30.3	C
Northbound – Thru/Right	0.85	44.6	D	0.87	45.9	D	0.86	45.5	D
Overall	0.63	29.7	C	0.69	30.6	C	0.70	30.6	C
= volume to capacity ratio	2 Delay			conds per			0.70	50.0	

 $^{1 \}text{ V/C} = \text{volume to capacity ratio}$

Delay cannot be accurately estimated for v/c ratio greater than 1.0

³ LOS = Level of Service

² Delay = Average delay in seconds per vehicle

Under existing conditions, all signalized intersections operate at a LOS D or better during both the morning and evening peak hours.

Under 2018 No-Build condition, during the morning peak hour, the intersection of Massachusetts Avenue at Boylston Street will decline from a LOS D to a LOS E and the intersection of Huntington Avenue at Massachusetts Avenue will decline from LOS D to a LOS E.

During the weekday evening peak hour, the intersection of Massachusetts Avenue at Belvidere Street will decline from a LOS B to an acceptable LOS C, the intersection of Massachusetts Avenue at St. Stephen Street is expected to improve in LOS from C to a B due to improvements as part of the Symphony Streetscape project. Huntington Avenue at Massachusetts Avenue will decline from LOS C to a LOS F. These changes to LOS operations are due to background growth as well as changes made to the geometry and signal timing/phasing as part of the Symphony Streetscape Project. All other signalized intersections are expected to operate at a LOS D or better as they do during Existing Conditions.

It is important to note that the timings for the Symphony Street Scape improvements could be adjusted in the field to obtain the most efficient splits once the improvements are implemented. The analysis for the intersection of Huntington Avenue/Massachusetts Avenue in the No-Build scenario is conservative since it assumes the timing plans. This intersection could potentially operate at a better LOS once the timings are implemented. The Synchro analysis also assumes the Central Business District (CBD) which provides a conservative analysis and results.

Under 2018 Build conditions (i.e., with the Proposed Project in place), the intersections will continue to operate at same levels of service grades as under 2018 No-Build conditions, except the intersection of Massachusetts Avenue at Belvidere Street which will decline slightly in level of service during the morning peak hour from LOS A to LOS B and improve in LOS during the evening peak hour from C to B. In addition, the intersection of Massachusetts Avenue at St. Stephen Street will decline from LOS B to LOS C during the 2018 Build condition.

Unsignalized Intersection Capacity Analysis

Capacity analyses were also conducted for the three unsignalized intersections identified in the Study Area including one existing driveway. Capacity analyses were conducted for 2013 Existing, 2018 No-Build and Build Conditions. A summary of the unsignalized capacity analysis is presented in Table 3-11 and Table 3-12.

Table 3-11 Morning Peak Hour Unsignalized Intersection Capacity Analysis Results

	2013 Exis	sting Cond	dition	n 2018 No Build Condition			2018 B	2018 Build Condition		
Approach	Demand ¹	Delay ²	LOS ³	Demand ¹	Delay ²	LOS ³	Demand ¹	Delay ²	LOS ³	
Saint Germain at Massachusetts Avenue										
Westbound – Left/Right	6	17.1	С	6	19.0	С	21	17.7	С	
Northbound – Thru	710	0.0	Α	822	0.0	Α	829	0.0	Α	
Southbound – Thru	620	0.0	Α	650	0.0	Α	651	0.0	Α	
Huntington Avenue at Drivewa	y West									
Westbound – Thru/Right	262	0.0	Α	324	0.0	Α	338	0.0	Α	
Southbound – Right	2	18.1	С	2	18.9	С	2	19.0	С	
Belvidere at Clearway Street Ex	tension									
Eastbound – Thru/Right	-	-	-	-	-	-	143	0.0	Α	
Westbound – Left/Thru	-	-	-	-	-	-	767	0.0	Α	
Northbound – Left/Right	-	-	-	-	-	ı	103	13.3	В	
Belvidere at Dalton Street										
Westbound – Left/Thru/Right	588	28.9	D	633	39.9	E	724	29.4	D	
Northbound – Left/Thru/Right	31	9.4	Α	31	9.6	Α	-	-	-	
Southbound – Left/Thru/Right	169	11.0	В	174	11.3	В	186	11.6	В	

¹ Demand in vehicles per hour for unsignalized Intersections. 2

Table 3-12 Evening Peak Hour Unsignalized Intersection Capacity Analysis Results

	2013 Existing Condition			2018 No	2018 No Build Condition			2018 Build Condition		
Approach	Demand ¹	Delay ²	LOS ³	Demand ¹	Delay ²	LOS ³	Demand ¹	Delay ²	LOS ³	
St. Germain at Massachusetts Avenue										
Westbound – Left/Right	10	>50	F	11	> 50	F	22	45.6	E	
Northbound – Thru	699	0.0	Α	744	0.0	Α	753	0.0	Α	
Southbound – Thru	694	0.0	А	732	0.0	Α	732	0.0	Α	
Huntington Avenue at Drivewa	y West									
Westbound – Thru/Right	230	0.0	Α	383	0.0	Α	393	0.0	Α	
Southbound – Right	62	>50	F	62	>50	F	62	> 50	F	
Belvidere at Clearway Street Ext	tension									
Eastbound – Thru/Right	-	-	-	-	-	-	225	0.0	Α	
Westbound – Left/Thru	-	-	-	-	-	-	623	0.0	Α	
Northbound – Left/Right	-	-	-	-	-	-	96	12.8	В	
Belvidere at Dalton Street										
Westbound – Left/Thru/Right	514	17.1	С	538	19.0	С	628	14.3	В	
Northbound – Left/Thru/Right	44	9.2	Α	45	9.4	Α	-	-	-	
Southbound – Left/Thru/Right	234	13.6	В	240	14.1	В	262	14.5	В	

¹ Demand in vehicles per hour for unsignalized Intersections. The demand applies to only the most critical street approach or lane group.

2 Delay 3 LOS = Level of Service

² Delay 3 LOS = Level of Service

Under existing conditions, all unsignalized intersections operate at LOS D or better during the morning peak hour. During the evening peak hour, the intersection of St Germain Street at Massachusetts Avenue operates at LOS F in the westbound left/right movements and the intersection of Huntington Street at Driveway West operates at LOS F in the southbound-right movement. Both of these LOS F movements are due to heavy traffic along the main roadway and therefore lack of acceptable gaps in traffic. The traffic movements at the intersection of Belvidere Street at Dalton Street operate at LOS C or better.

Under 2018 No-Build Conditions, traffic operation level of service grades will remain the same as under Existing Conditions, with the exception of the intersection of Belvidere Street at Dalton Street which will decline from LOS D to LOS E in the westbound movement during the morning peak hour only.

Under 2018 Build Conditions (i.e., with the Proposed Project in place) traffic operation level of service grades will remain the same as under No-Build Conditions, with the exception of the intersection of Belvidere Street at Dalton Street which will improve from LOS E to LOS D in the westbound movement during the morning peak hour. During the evening peak hour this approach will improve from a LOS C to a LOS B. It is assumed that the Belvidere Street approach will contain a left/through lane and an exclusive right turn lane at the intersection in order to increase capacity at this approach. The newly formed intersection of Clearway Street Extension at Belvidere Street will operate at LOS A and B during both the morning and evening peak hours. During the evening peak hour, the intersection of Massachusetts Avenue at Saint Germain Street will improve from LOS F to LOS E in the westbound movement due a higher demand in the westbound direction.

3.5 Transportation Demand Management

In addition to physical improvements, the Proponent proposes to minimize reliance by hotel and retail employees, patrons and residents on travel by automobile through implementation of on-site Traffic Demand Management (TDM). Generally, TDM strategies are most effective with commuter travel where most trips are made by employees, e.g. in an office development. However, there are a number of measures that will be implemented in an effort to reduce resident and hotel auto trips to the Project as well as retail and hotel employee trips.

The goal of the Transportation Demand Management (TDM) plan is to reduce the project's overall traffic impact through the implementation of TDM measures that are geared toward affecting the demand side of the transportation equation, rather than the supply side. By their very nature, TDM programs attempt to change people's behavior, and, to be successful, they must rely on incentives or disincentives to make these shifts in behavior attractive to the commuter or resident.

TDM programs are designed to maximize the people-moving capability of the existing transportation infrastructure by increasing the number of persons in a vehicle, providing alternate modes of travel, or influencing the time of, or need to, travel.

TDM measures are most often directed at commuter travel, characterized by the day-to-day regularity of this type of trip. Conditions at the workplace, in terms of employer practices such as on-site services, bicycle storage, and shower facilities impact employee commuter choices, and makes this market the most suitable for identifying alternatives.

The term TDM encompasses both alternatives to driving alone and the techniques or supporting strategies that encourage the use of these alternatives. TDM alternatives to driving alone include: carpools and vanpools, public and private transit, and non-motorized travel including bicycling and walking. TDM alternatives can also influence when trips are made. For example, alternative work hours (compressed work weeks, and flex-time) can affect what time of day trips are made, or if trips occur at all on certain days.

TDM strategies are the supporting measures that encourage the use of alternatives to driving alone. TDM strategies include financial incentives, time incentives, provision of new or enhanced commuter services, dissemination of information, and marketing alternative services. TDM strategies include all the incentives and disincentives that increase the likelihood for people to change their existing travel behavior.

A distinction can be drawn between area-wide TDM programs and employer-based TDM programs. Employer-based TDM programs are those run by individual employers or groups of employers, generally located near one another. "Area-wide" usually refers to a region, municipality or corridor. Area-wide programs address a more diverse group of travelers traveling to a wide variety of locations at many different times.

Transportation Demand Management Plan

To implement a TDM program for the proposed site, the Proponent will consider a number of measures that will contribute toward the reduction of vehicular traffic to and from the site.

The following measures could comprise the proposed TDM package.

Ridesharing

The Proponent will promote ridesharing for its retail and hotel employees by carpooling. The Proponent will provide information regarding carpooling and its benefits to new employees. Interested car-pooler names will be posted in the employee area, and a notice of interested car-poolers will be listed in the facility newsletter.

An incentive program will be established to encourage employees to rideshare by providing a financial incentive.

Guaranteed Ride Home

A guaranteed ride home program, in the case of an emergency for registered rideshare participants, will be provided via a local taxi service. Such programs are very effective in eliminating the concern of an employee that they might not be able to respond effectively, for example to an emergency at home, if they have not used their own car to commute to work. The program can also be applied for unexpected overtime or late working.

Transportation Coordinator

An on-site Transportation Coordinator will be identified to ensure that the complete rideshare program, including ride matching, accommodating work shifts, promotion, incentives, and a guaranteed ride home, is consistently promoted and provided.

Transit Incentives

To encourage the use of transit by employees and residents to commute to work, the proposed buildings will provide local bus schedule and route information in the employee and resident areas.

Bicycle and Pedestrian Measures

Bicycling to the site will likely be attractive to some employees and residents due to the proximity of many residential communities and the urban downtown location. To encourage and facilitate use of bicycles by both employees and residents, secure bicycle storage racks will be provided near the front doors to the new buildings and below grade in the parking garage.

Again due to the close proximity of residential areas to the site, walking is, and will continue to be, attractive to many employees and residents. For this reason, the Project site layout has been designed to encourage pedestrian activity to and from the site by making appropriate connections to the existing pedestrian network in the area.

3.6 Construction Management

The Proponent will develop a detailed evaluation of potential short-term construction-related transportation impacts including construction vehicle traffic, parking supply and demand, and pedestrian access. Detailed Construction Management Plans will be developed and submitted to the BTD for their approval. These plans will detail construction vehicle routing and staging.

Construction Vehicle Traffic

Construction vehicles will be necessary to move construction materials to and from the project sites. Every effort will be made to reduce the noise, control fugitive dust, and minimize other disturbances associated with construction traffic. Truck staging and laydown areas for the project will be carefully planned. The need for street occupancy (lane closures) along roadways adjacent to the project site is not known at this time.

Construction Parking Issues

Contractors will be encouraged to devise access plans for their personnel that de-emphasize auto use (such as seeking off-site parking, provide transit subsidies, on-site lockers, etc.) Construction workers will also be encouraged to use public transportation to access the Project site because no new parking will be provided for them. Because of the construction workers early arrival/departure (typically 7:00AM-3:00PM) schedule, a conflict for on-street parking is not anticipated.

Pedestrian Access During Construction

During the construction period, pedestrian activity adjacent to the sites may be impacted by sidewalk closures. A variety of measures will be considered and implemented to protect the safety of pedestrians. Temporary walkways, appropriate lighting, and new directional and informational signage to direct pedestrians around the construction sites will be provided. After construction is complete, finished pedestrian sidewalks will be permanently reconstructed to meet ADA standards around the new facilities. Any damage as a result of construction vehicles or otherwise will be repaired per City standards.

Environmental Protection Component

4.0 ENVIRONMENTAL PROTECTION COMPONENT

4.1 Pedestrian Level Winds

A pedestrian level wind (PLW) study has been performed by RWDI of Guelph, Ontario to assess the effect of the Proposed Project on wind conditions in the pedestrian realm of the Project site and surrounding areas and to provide recommendations for minimizing any potential adverse effects. The results of the wind study are summarized in this section, and the wind study results tables are included in Appendix C.

The wind study involved wind simulations of the Proposed Project on a scale model of the proposed buildings and surroundings in a boundary-layer wind tunnel. A total of 115 wind measurement locations were examined in the wind tunnel under the existing No-Build, the approved Master Plan Build, and the Proposed Project Build Condition for both mean wind speed and effective gust wind speed.

The analysis found that the Proposed Project will not have significant adverse wind impacts. The majority of the locations studied (69 percent) are expected to experience either no change or improved wind conditions under the Proposed Build Condition compared to the No Build Condition. By not constructing at the Huntington Avenue location as was proposed under the approved Master Plan scenario, the Proposed Project avoids creating adverse wind impacts in the vicinity of the Sunday School Building on the Christian Science Plaza.

As design of the Project moves forward, the Proponent will continue to assess the potential for adverse wind impacts and will implement practicable mitigation measures capable of reducing wind impacts adjacent to the Project.

4.1.1 Background

Tall buildings, especially those that protrude above their surroundings, can cause increased local wind speeds at the pedestrian level. Typically, wind speeds increase with elevation above the ground surface, and taller buildings can intercept these faster winds and deflect them down to the pedestrian level. The funneling of wind through gaps between buildings and the acceleration of wind around corners of buildings may also cause increases in wind speed. Conversely, if a building is surrounded by others of equivalent height, it may be protected from the prevailing upper-level winds, resulting in no significant changes to the local pedestrian-level wind environment. The most effective way to assess potential pedestrian-level wind impacts around a proposed new building is to conduct scale model tests in a wind tunnel. The Proponent retained RWDI, one of the foremost international experts in the field of wind modeling, to conduct the wind tunnel modeling for the Proposed Project.

The consideration of wind in planning outdoor activity areas and public sidewalks, entrance locations, and gathering spaces is important since high winds in an area tend to deter pedestrian use. For example, winds should be light or relatively light in areas where people would be sitting, such as outdoor cafes or playgrounds. For bus stops and other locations where people are typically standing, somewhat higher winds can be tolerated. For frequently used sidewalks, where people are primarily walking, stronger winds are acceptable. Similarly, for infrequently used areas, the wind comfort criteria can be relaxed even further. The actual effects of wind can range from pedestrian inconvenience, due to the blowing of dust and other loose material in a moderate breeze, to severe difficulty with walking due to the wind forces on the pedestrian.

4.1.2 Methodology

For its analysis, RWDI gathered information concerning the site and surrounding buildings and topography within an approximately 1,600-foot radius of the Project site from topographic maps, BRA mapping, and site plans and elevations of the proposed development Project provided by the Project design team. The wind tunnel study looked at a No-Build Condition consisting of the current existing site condition without the Proposed Project, the approved Master Plan Build Condition consisting of the Huntington Building, the High-rise and the Mid-rise at the heights approved in the PDA Master Plan, and the Build Condition; specifically, the Proposed Project as it is described in this Expanded PNF. Photographs of the No Build Condition, Approved Master Plan and Proposed Project models tested are included as Figures 4.1-1 through 4.1-3, respectively. All of the figures related to the wind analyses (Figures 4.1-1 through 4.1-14) described herein are included at the end of this section.

The scale model of the Project site and area was equipped with 115 specially designed wind speed sensors which were, in turn, connected to the wind tunnel's data acquisition system.¹ This system is designed to record the mean and fluctuating components of wind speed at a full-scale height of five feet above grade in pedestrian areas throughout the study area. Wind speeds were measured for 36 wind directions, in 10-degree increments, starting from true north. The measurements at each sensor location were recorded in the form of ratios of local mean and gust speeds to the reference wind speed in the free stream above the model. The results were then combined with long-term meteorological data, recorded during the years 1981 to 2011 at Boston's Logan International Airport, in order to predict full scale wind conditions. The analysis was performed separately for each of the four seasons and for the entire year.

Note that only 113 sensors obtained full data during testing.

Figures 4.1-4 through 4.1-6 present "wind roses" that summarize the annual wind climate in the Boston area, based on the data from Logan Airport. On an annual basis, the most common wind directions are those between southwest and northwest. These are also the dominant direction for strong winds. Winds from the east and east-southeast are also relatively common.

4.1.3 Pedestrian Wind Comfort Criteria

The BRA has adopted two standards for assessing the relative wind comfort of pedestrians. First, the BRA wind design guidance criterion states that an effective gust velocity (hourly mean wind speed + 1.5 times the root-mean-square wind speed) of 31 mph should not be exceeded more than one percent of the time. The second standard used by the BRA is based on the work of Melbourne and is used to determine the relative level of pedestrian wind comfort for activities such as sitting, standing, or walking, as shown in Table 4.2-1.² The criteria are shown in terms of benchmarks for the one-hour mean speed exceeded one percent of the time (i.e., the 99-percentile mean wind speed).

Table 4.1-1 Boston Redevelopment Authority Mean Wind Criteria*

Level of Comfort	Wind Speed
Dangerous	> 27 mph
Uncomfortable for Walking	>19 and <27 mph
Comfortable for Walking	>15 and <19 mph
Comfortable for Standing	>12 and <15 mph
Comfortable for Sitting	<12 mph

^{*} Applicable to the hourly mean wind speed exceeded one percent of the time.

4.1.4 Pedestrian Level Wind Test Results

The following sections review the results of the pedestrian level wind tests for the No-Build, the approved Master Plan Build and the Proposed Project Build Conditions. The results for the annualized mean wind speed analyses for the No-Build, the approved Master Plan Build and the Proposed Project Build Conditions are presented in Figures 4.1-7 through 4.1-9. Figure 4.1-10 presents the net change in BRA comfort ratings between the No-Build and the approved Master Plan Condition, and Figure 4.1-11 presents the net change in BRA comfort ratings between the No-Build and the Proposed Project. The results for the annualized

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Melbourne, W.H., 1978, "Criteria for Environmental Wind Conditions," Journal of Industrial Aerodynamics, 3 (1978) 241 – 249.

effective gust wind speed analyses for the No-Build, the approved Master Plan Build and the Proposed Project Build Conditions are presented in Figures 4.1-12, 4.1-13, and 4.1-14, respectively.

4.1.4.1 No-Build

Under the No-Build Condition, the study finds generally good wind conditions using the BRA's annual mean wind criteria. Most sites are suitable sitting (39 percent) or standing (28 percent). There are no locations categorized as Dangerous; however, there are 13 locations (12 percent) considered to be Uncomfortable. A cluster of these uncomfortable locations (Numbers 17, 18 22, 27, are 28) are near the intersection of Dalton and Belvidere Streets. Other uncomfortable areas are at the north end of the Christian Science Plaza (Numbers 75, 79, 80, 85, and 87). Two are at or near 111 Huntington (Numbers 36 and 115).

Under the No-Build Condition, there are six locations that experience unacceptable gusts. Three are near the Dalton/Belvidere Street intersection (Locations 17, 22, and 27). and three are in the north end of the Christian Science Plaza (Locations 79, 80, and 87).

4.1.4.2 Approved Master Plan Build Condition

Under the approved Master Plan Condition, wind conditions would be made somewhat less calm compared to the No-Build Condition, particularly in the vicinity of the proposed Huntington Avenue site, where under the approved Master Plan Condition, a 291-foot tall building was proposed. This building would have created one Dangerous wind location (Number107) just north of the building and two Uncomfortable locations (Numbers 104 and 106) at its northwest and southeast corners (Numbers 108 and 104). These conditions are not found under the Proposed Project. Another Dangerous location (Number 87) is created under the approved Master Plan Condition near the southeast corner of the building at 177 Huntington Avenue. As noted above, this location is also windy under the No-Build Condition (experiencing Uncomfortable mean annual winds and Unacceptable gusts). Although there would be a net increase in the number of Uncomfortable locations near the Belvidere/ Dalton Street intersection, most locations studied would remain suitable for sitting (27 percent), standing (29 percent), or walking (23 percent).

Unacceptable gusts are predicted at ten locations under the approved Master Plan Condition. Four of the locations (Numbers 27, 79, 80, and 87) also occur under the No-Build Condition. Three are associated with the proposed Huntington Avenue building (Numbers 104, 107, and 108), which would not be constructed under the Proposed Project Condition. One location Number 8) is located at the southern apex of the High-rise building. The remaining two are in the vicinity of the north end of the Christian Science Plaza (Locations 36 and 85).

4.1.4.3 Proposed Project Build Condition

Wind impacts under the Proposed Project Condition are very similar to those of the approved Master Plan Condition, with the exception that the Proposed Project does not have any of the impacts associated with the Huntington Avenue Building that was proposed under the Master Plan Condition.

Under the Proposed Project, most locations will be suitable for sitting (27 percent), standing (29 percent), or walking (23 percent). Compared to the No-Build Condition, the Proposed Project results in either no change or improvement to 69 percent of the locations studied. Of those locations expected to experience a downward shift in wind category, 80 percent will shift by only one category, e.g., from comfortable for sitting to comfortable for standing. Four locations, all near the proposed High-rise, are expected to decline by two categories (e.g., comfortable for sitting to comfortable for walking) and two locations, Numbers 7 and 44 near the southern end of the High-rise, will shift from comfortable for sitting to uncomfortable. One dangerous location (Number 85) is expected on the west side of 177 Huntington Avenue. This is a known windy location that is rated Uncomfortable under existing No-Build conditions, and annual mean wind speed at this location is expected to exceed the existing Uncomfortable category by only one mile per hour.

Comparing the Proposed Project to the approved Master Plan shows that 82 locations (73 percent) would be the same. Fifteen locations (13 percent) will be improved (e.g., shifting from comfortable for walking to comfortable for sitting), and 16 locations (14 percent) are expected to experience a decrease.

Unacceptable gusts are predicted at only six locations under the Proposed Project Condition, which is the same number as under the No Build Condition, and four fewer than the Approved Master Plan Condition.

4.1.5 Conclusions

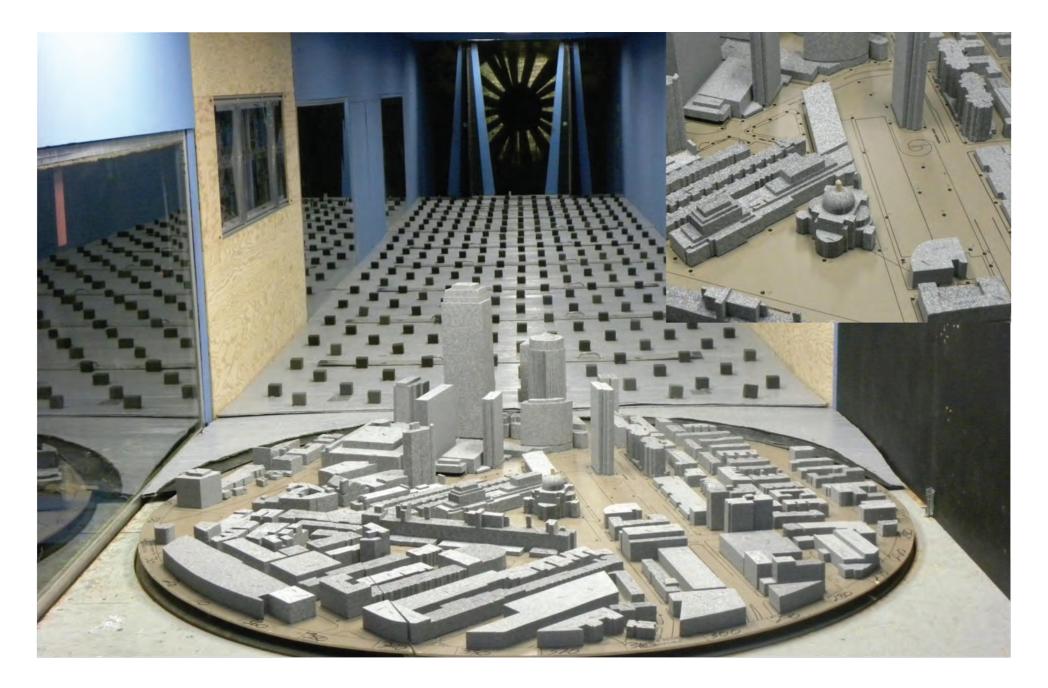
The Proposed Project, as would be expected with any building of substantial size, will result in some increased pedestrian level winds. These increases are not expected to be severe, however, and generally conditions will be similar to the No-Build Condition. At 69 percent of the locations studied, wind conditions under the Proposed Build Condition are expected to be unchanged or improved when compared to the No Build Condition. Compared to the approved Master Plan condition, the Proposed Project will not have any of the adverse wind impacts associated with the Huntington Avenue site that would occur under the approved Master Plan.

Table 4.1-2 summarizes the wind results.

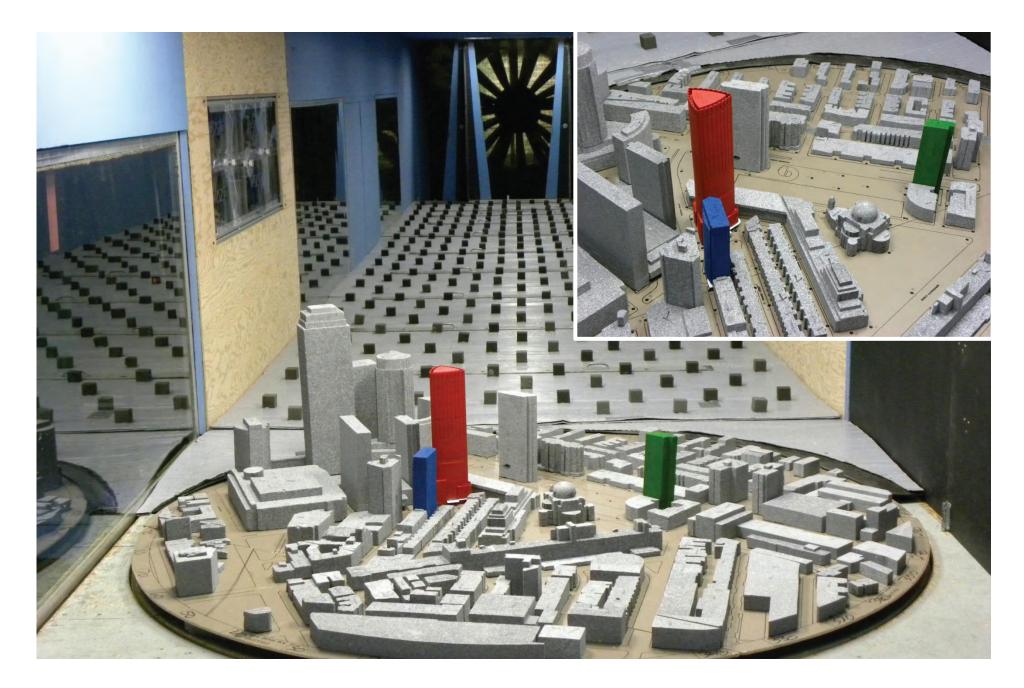
Table 4.1-2 Wind Impacts Summary

BRA Mean Annual Wind Criteria	No-Build		Wind No-Build Approved Master Plan		Approved Master Plan		Proposed	d Project
Number of Locations Comfortable for Sitting	44	39%	30	27%	31	27%		
Number of Locations Comfortable for Standing	32	28%	30	27%	33	29%		
Number of Locations Comfortable for Walking	24	21%	31	27%	26	23%		
Number of Uncomfortable Locations	13	12%	20	18%	22	19%		
Number of Dangerous Locations	0	0%	2	2%	1	1%		
Number of Unacceptable Gust Locations	6	5%	10	9%	6	5%		

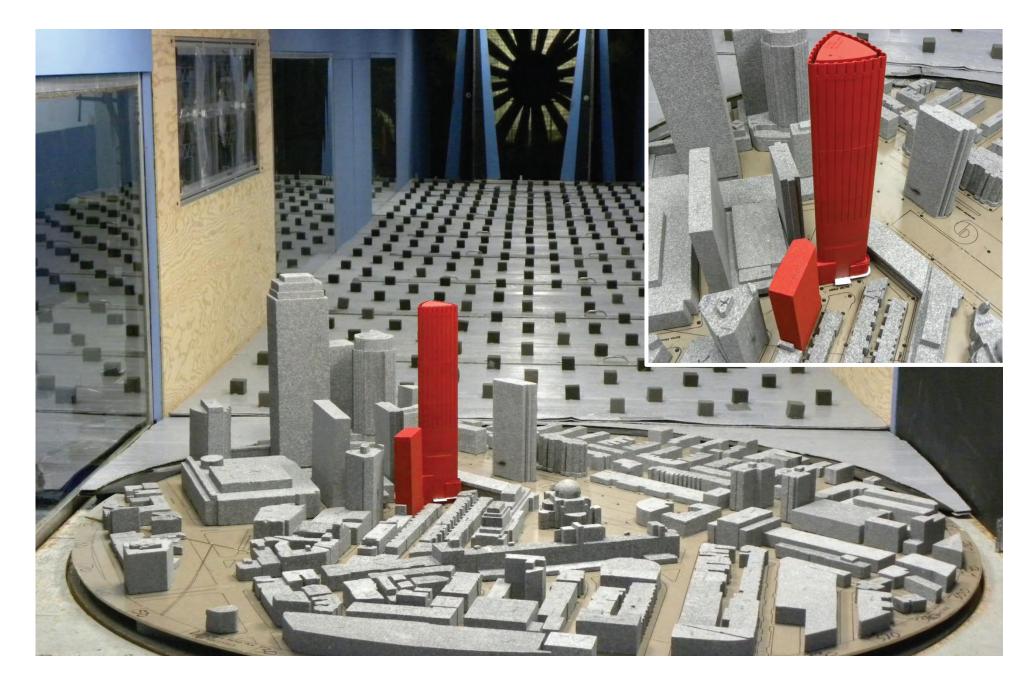
The Proponent will continue to evaluate the need for potential mitigation to minimize the potential for adverse pedestrian level winds. For example, the use of wind screens and a canopy will be employed to protect the south entrance of the High-rise (Location 8) to diffuse westerly winds and a canopy may be used at the entrance to the Mid-rise (Location 16) to protect from wind downwash on the building's façade.



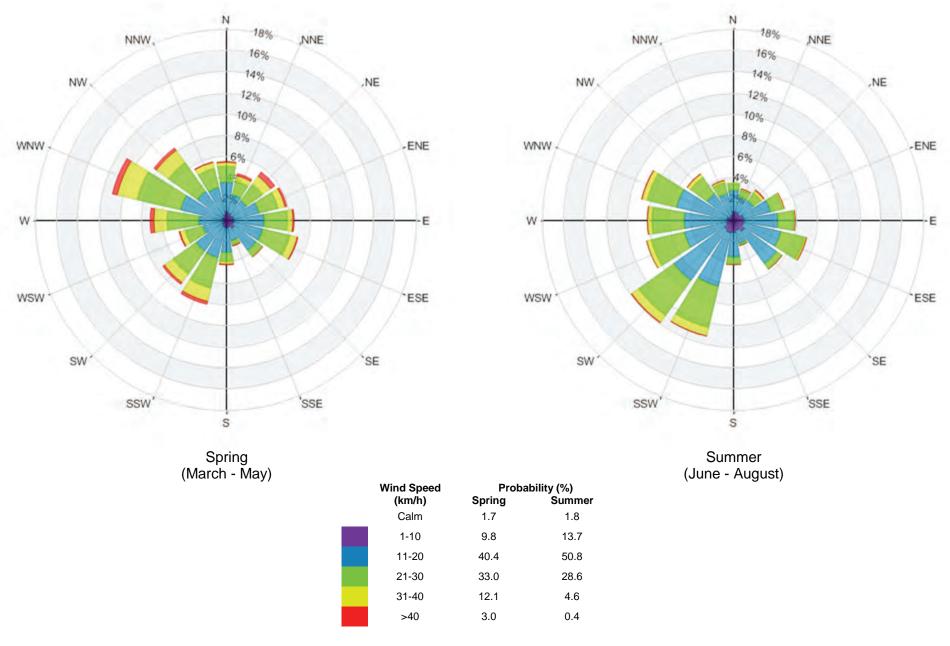




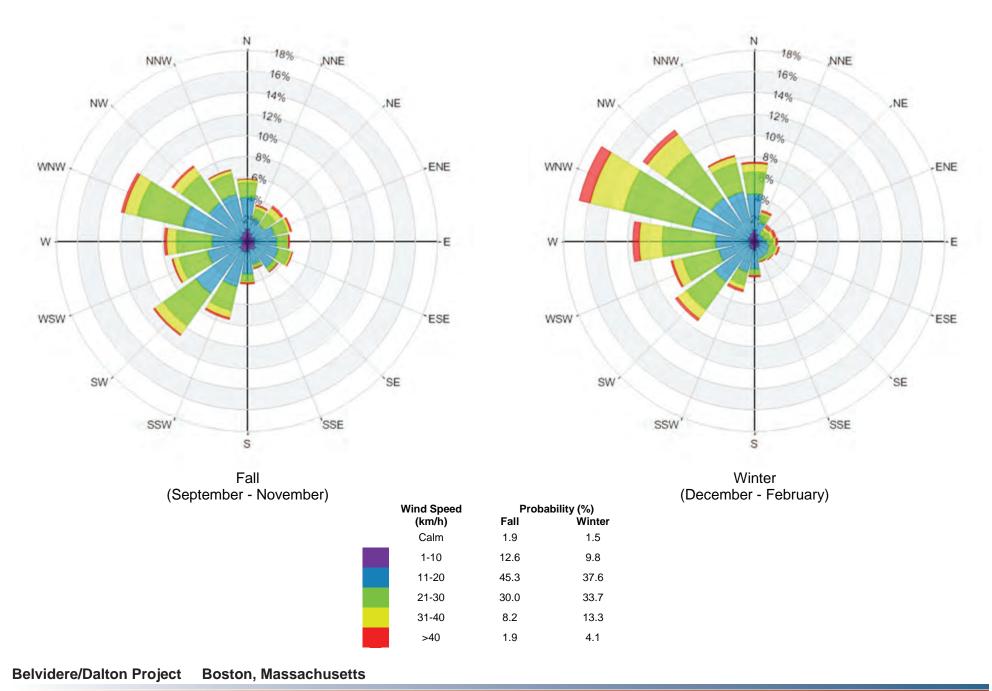










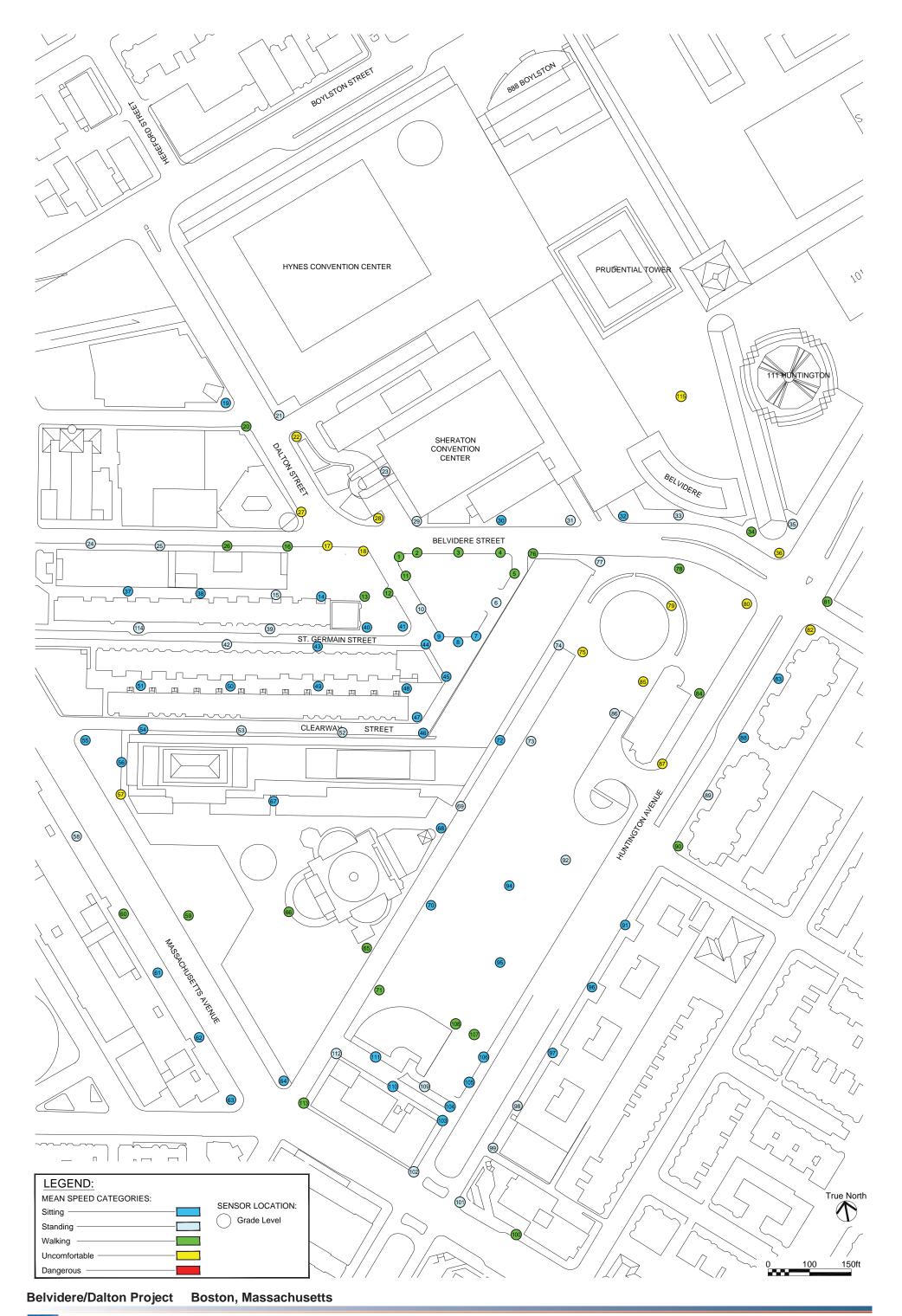




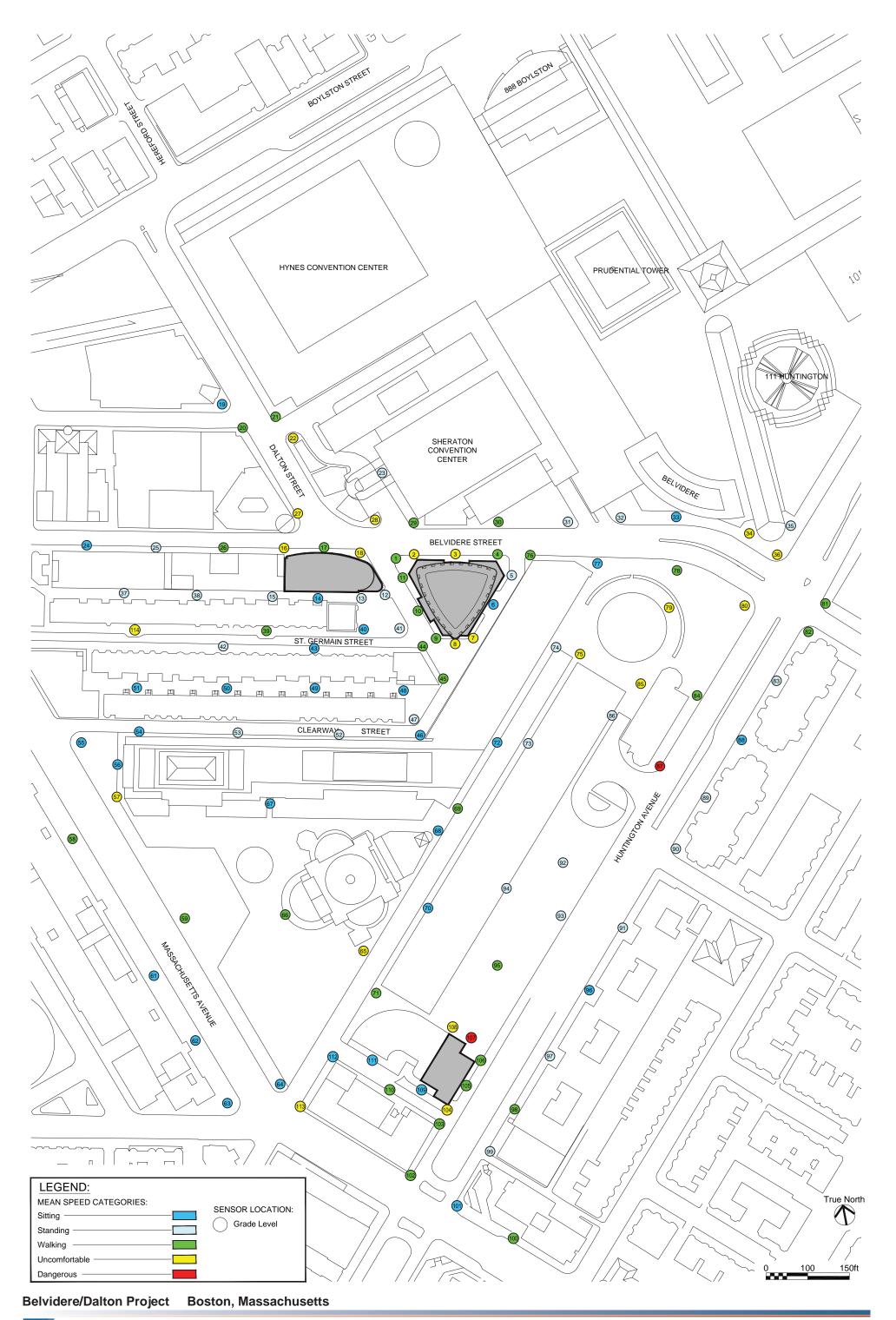


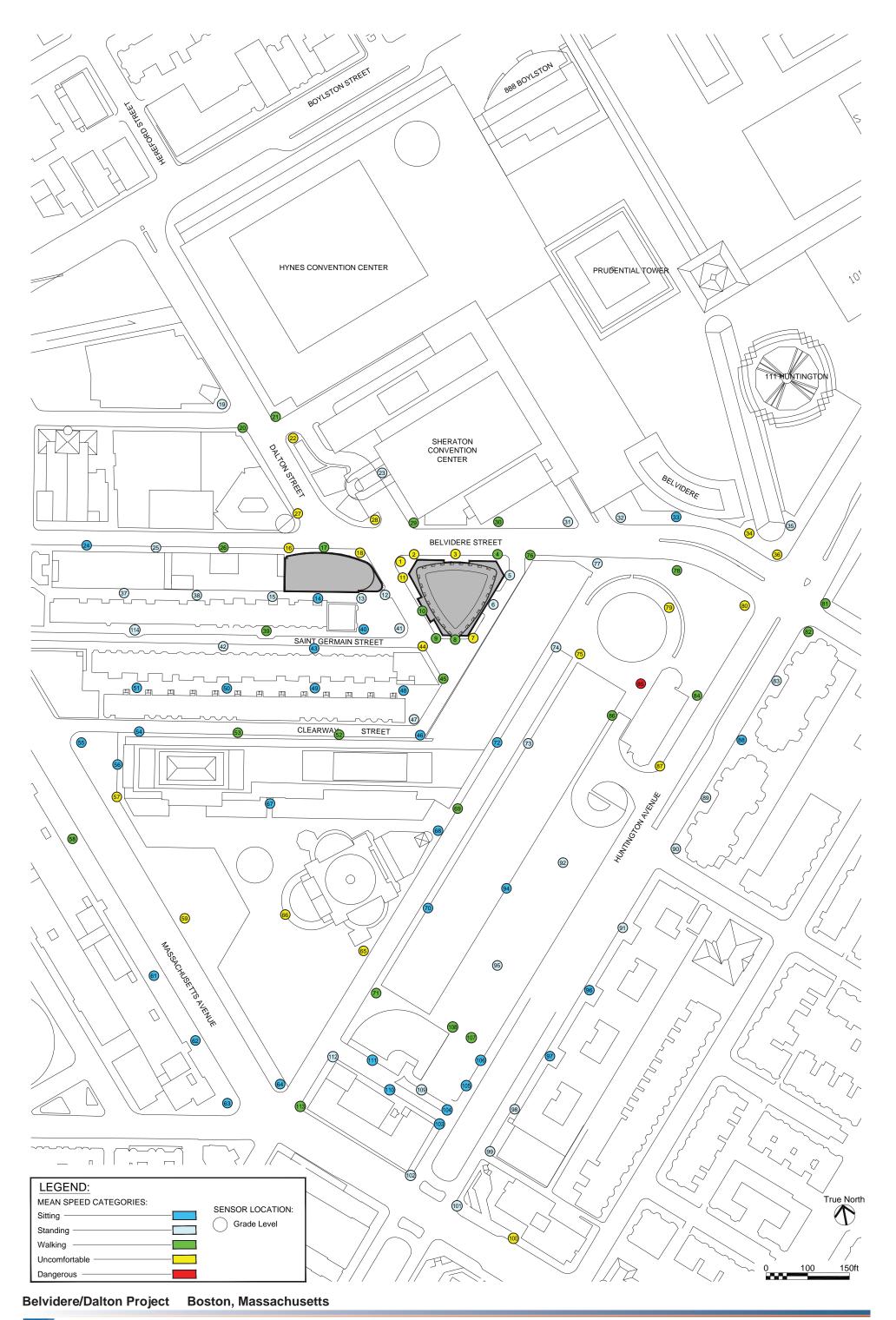
Wind Speed (km/h)	Probability (%)	
Calm	1.7	
1-10	11.5	
11-20	43.5	
21-30	31.3	
31-40	9.5	
>40	2.3	

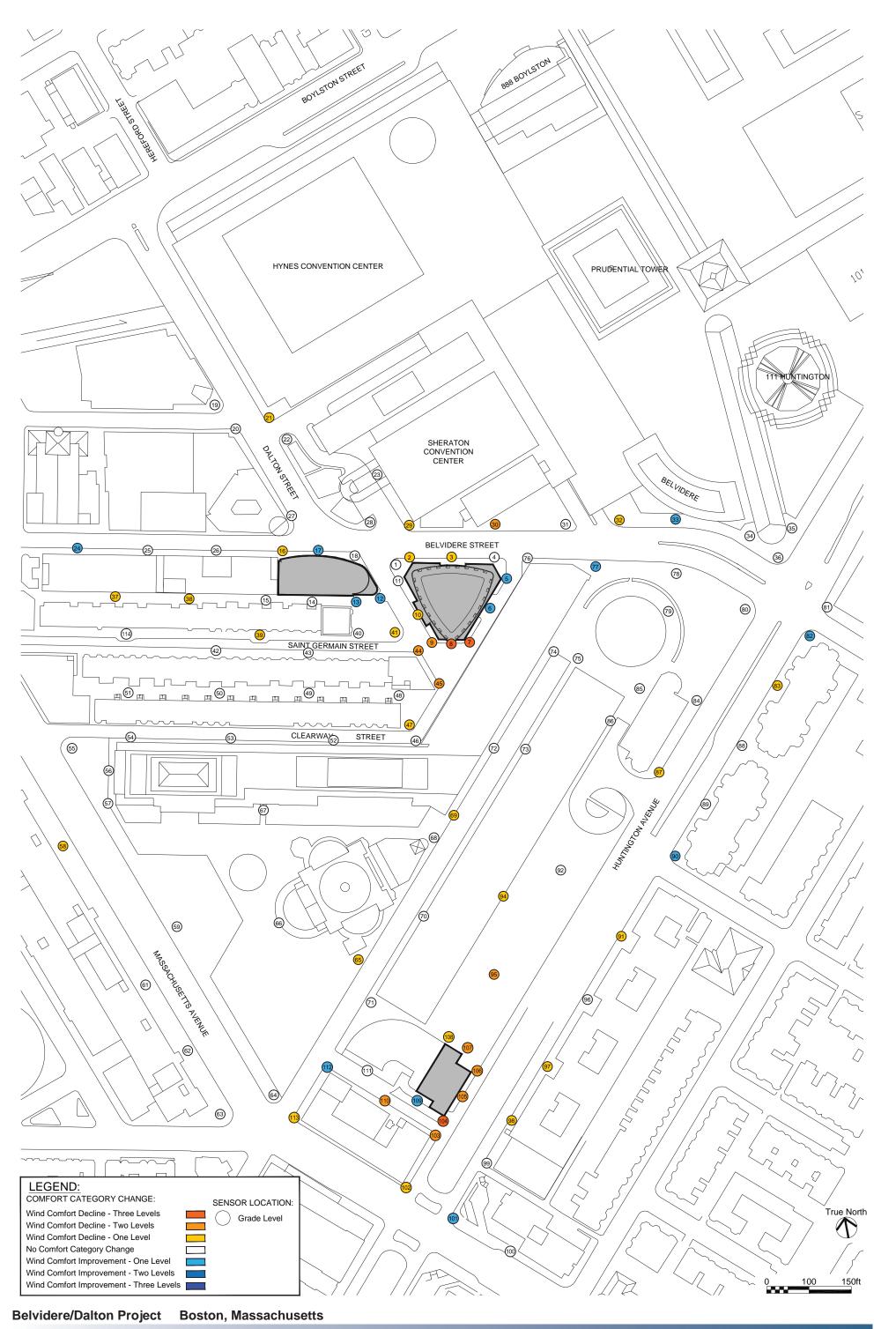


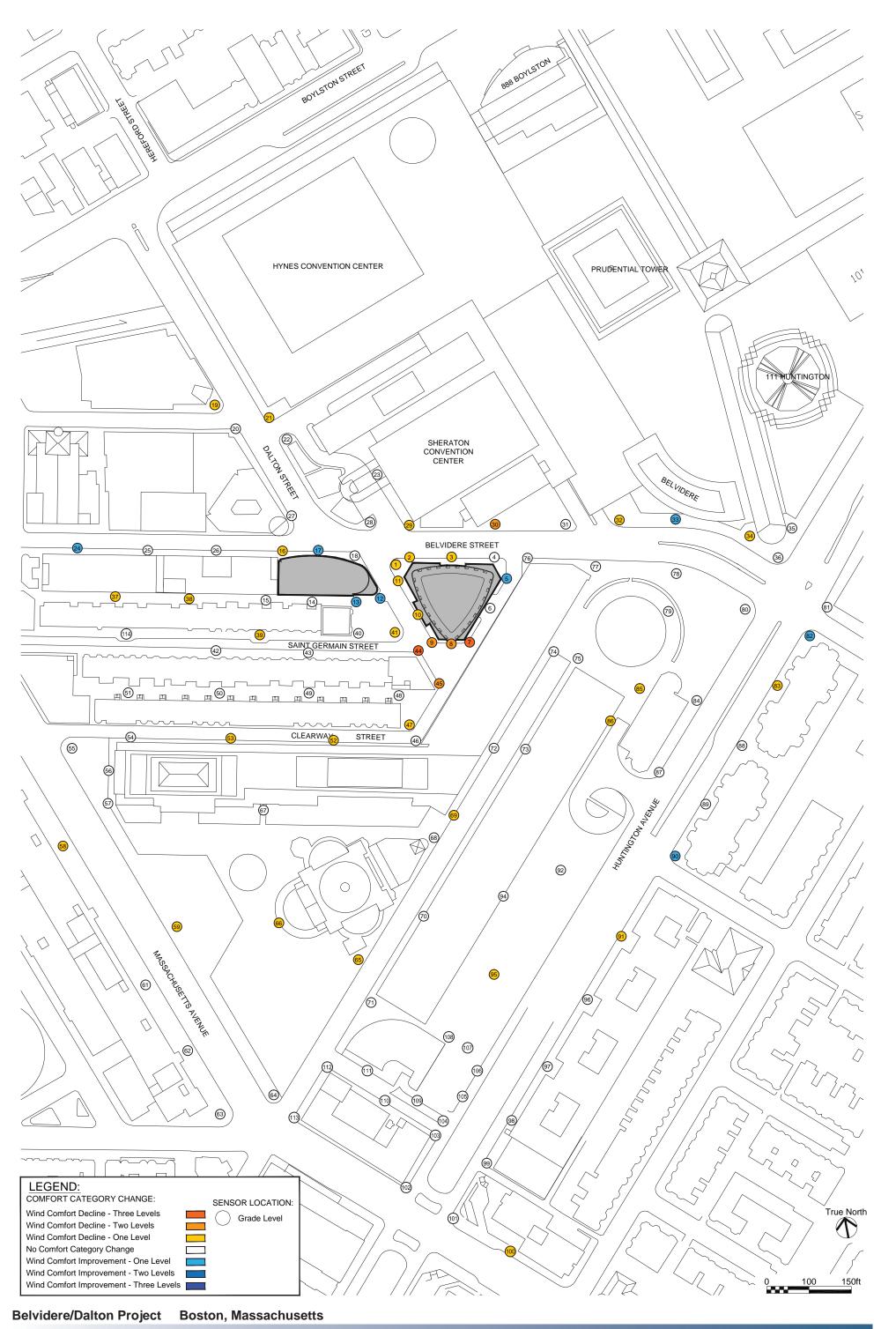


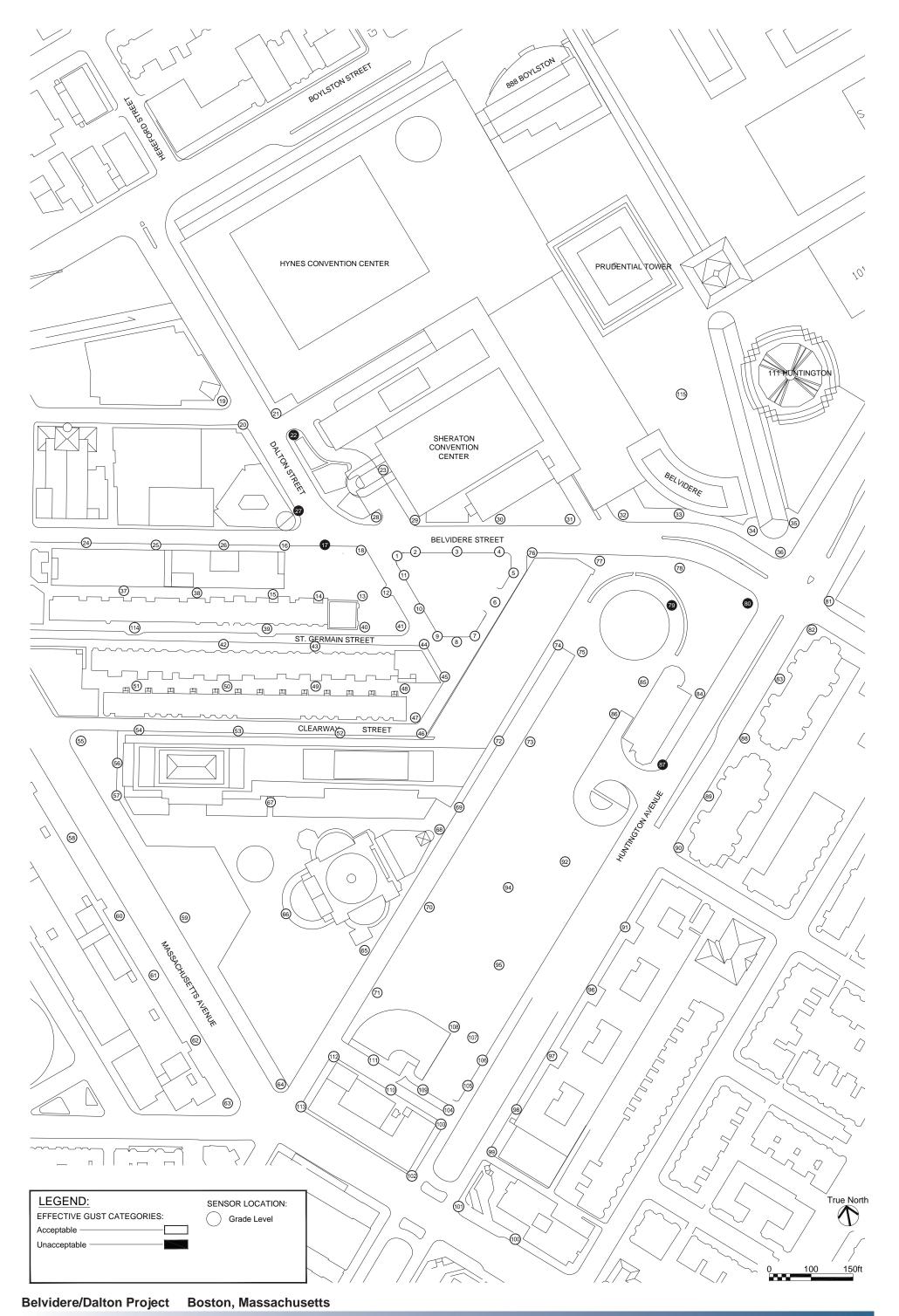




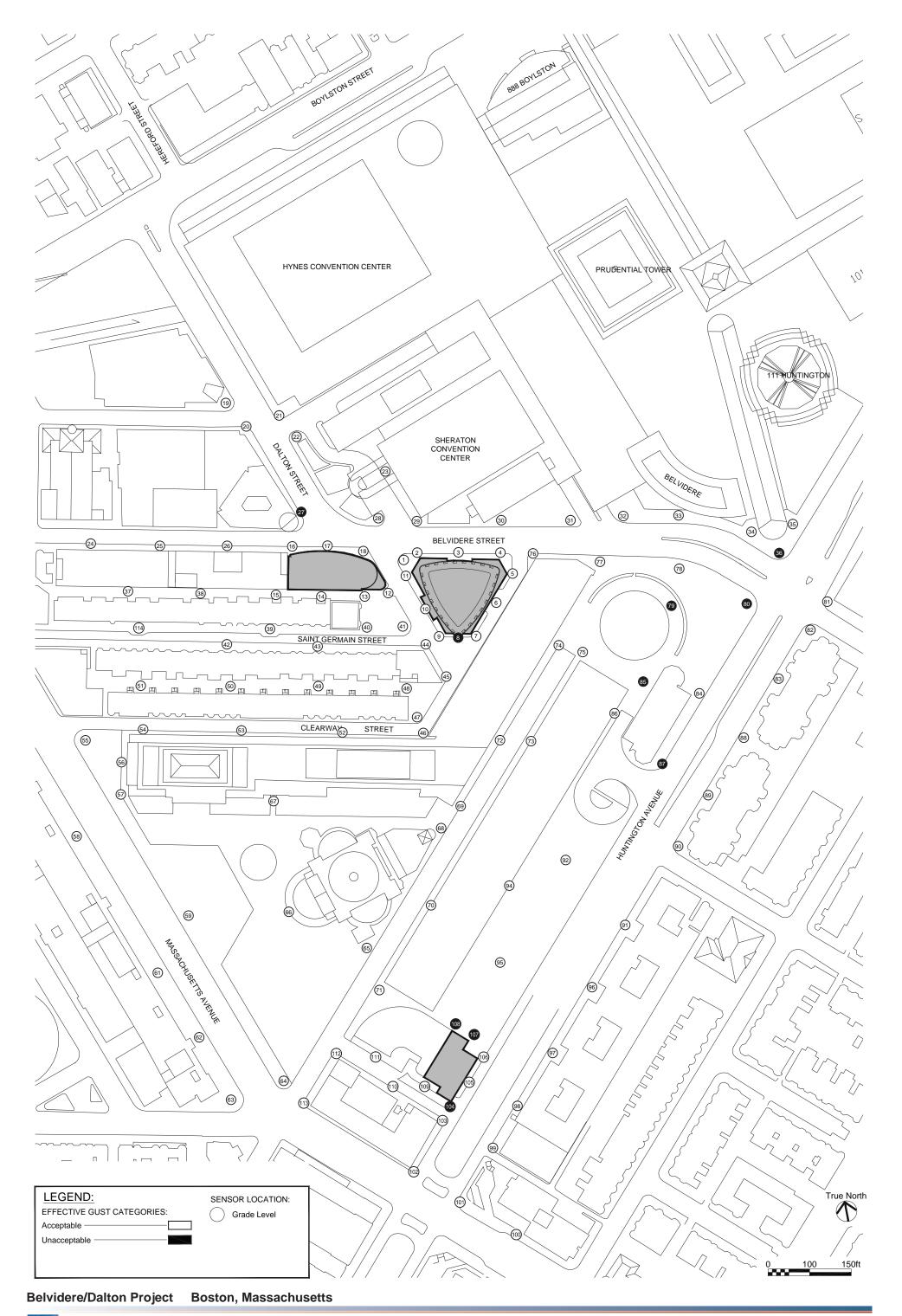




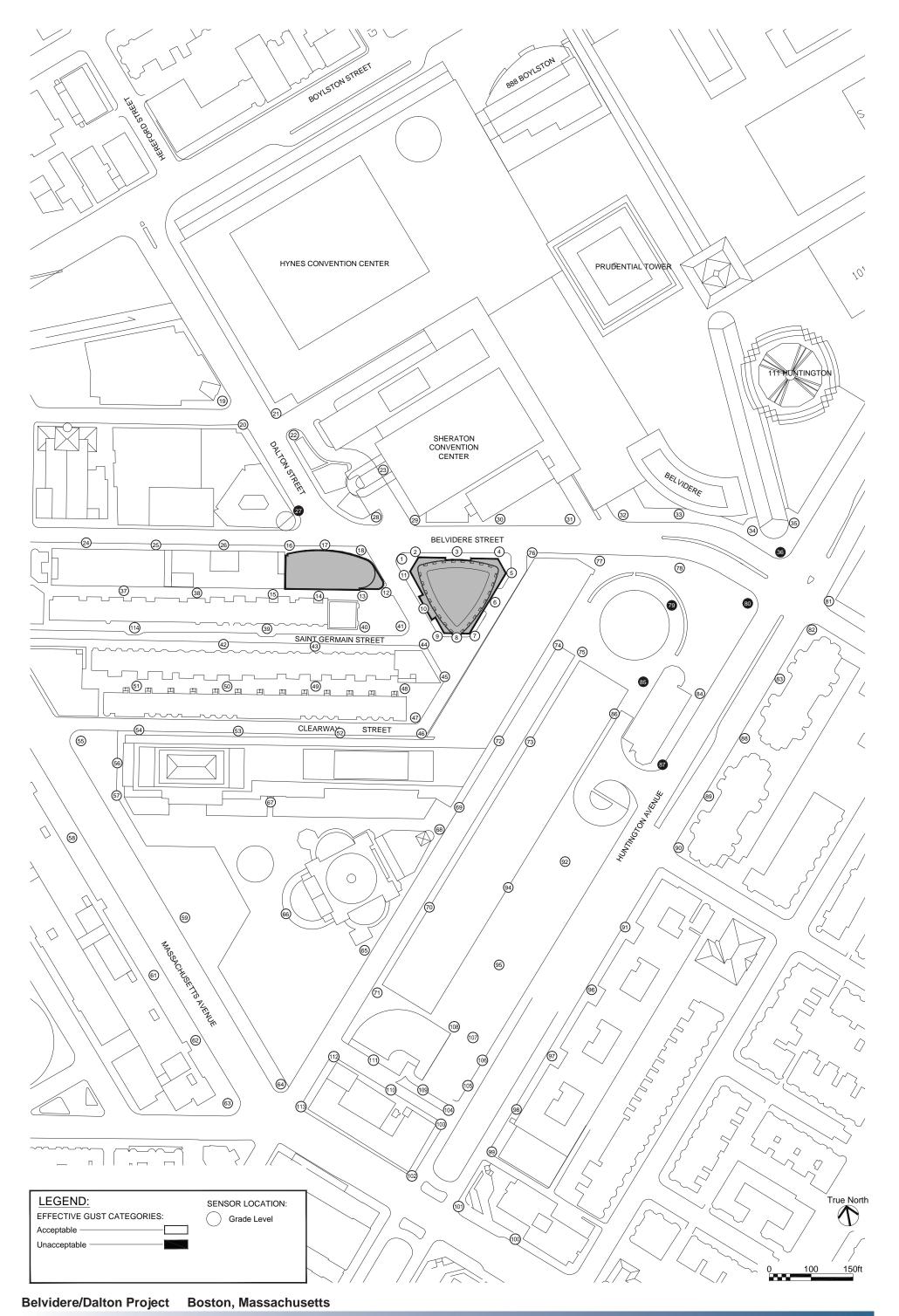














4.2 Shadow Impacts

4.2.1 Introduction and Methodology

A shadow impact analysis was conducted to assess potential shadow impacts from the Project. The study looked at the following four times of the year:

- 1. Spring Equinox (March 21) at 9:00 a.m., 12:00 noon, and 3:00 p.m.
- 2. Summer Solstice (June 21) at 9:00 a.m., 12:00 noon, 3:00 p.m. and 6:00 p.m.
- 3. Autumnal Equinox (September 21) at 9:00 a.m., 12:00 noon, 3:00 p.m. and 6:00 p.m.
- 4. Winter Solstice at 9:00 a.m., 12:00 noon, and 3:00 p.m.

The shadow analysis presents the existing shadow and new shadow that would be created by the Proposed Project, illustrating the incremental impact of the Project. The analysis focuses on nearby open spaces, sidewalks and bus stops adjacent to and in the vicinity of the Project site. It should be noted that the model used for the analysis does not include trees, which can block new shadow from the proposed buildings during much of the year during certain time periods. Shadows have been determined using the applicable Altitude and Azimuth data for Boston. Figures showing the net new shadow from the Project are provided in Figures 4.2-1 to 4.2-14 at the end of this section. Each Figure distinguishes between the approved Master Plan Build condition with shadow shown in green; the Proposed Project Build condition with new shadow shown in blue, and the approved Master Plan Huntington Avenue building shadow with shadow shown in orange.

4.2.2 Vernal Equinox (March 21)

At 9:00 a.m. during the vernal equinox, new shadow from the Project will be cast to the northwest. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto the landmarked Christian Science Plaza, as well as a portion of Massachusetts Avenue and its eastern sidewalk. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Belvidere Street and its northern and southern sidewalks, and a portion of Dalton Street and its eastern and western sidewalks. Additional shadow from the Proposed Project beyond that approved in the Master Plan will be limited to a portion of Boylston Street and the Massachusetts Turnpike, including two bus stops on Boylston Street. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 12:00 p.m., new shadow from the Project will be cast to the north. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto the landmarked Christian Science Plaza. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Dalton Street and its eastern sidewalk, as well as a portion of Belvidere Street and its northern and southern sidewalks. Additional shadow from the

Proposed Project beyond that approved in the Master Plan will be limited to a small portion of the Sheraton Hotel sidewalk and parking garage entrance. By moving to the Belvidere/Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 3:00 p.m., new shadow from the Project will be cast to the northeast. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto a portion of Huntington Avenue and its eastern and western sidewalks. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Belvidere Street and its northern and southern sidewalks, and a small portion of Dalton Street and its eastern and western sidewalks. There will be no additional shadow beyond that approved in the Master Plan as a result of the Proposed Project. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

4.2.3 Summer Solstice (June 21)

At 9:00 a.m. during the summer solstice, new shadow from the Project will be cast to the west. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto the landmarked Christian Science Plaza. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Dalton Street and its eastern and western sidewalks, a small portion of Belvidere Street and its southern sidewalk, and a portion of the alley between the Project and the Saint Germain Street residences. Additional shadow from the Proposed Project beyond that approved in the Master Plan will be cast onto an additional portion of Belvidere Street and its southern sidewalk, as well as an additional portion of the alley between the Project and the Saint Germain Street residences. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 12:00 p.m., new shadow from the Project will be cast to the north. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto the landmarked Christian Science Plaza. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto portions of Belvidere Street and its northern and southern sidewalks, as well as a small portion of Dalton Street and its eastern and western sidewalks. Additional shadow from the Proposed Project beyond that approved in the Master Plan will be minimal, with only a sliver of new shadow on Dalton and Belvidere Streets. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 3:00 p.m., new shadow will be cast to the east. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto a portion of Huntington Avenue and its eastern and western sidewalks. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Dalton Street between the two buildings, and a portion of Belvidere Street and its northern and southern sidewalks, including the bus stop on Belvidere Street. Additional shadow from the Proposed Project beyond that approved in the Master Plan will be limited to a sliver of shadow on the landmarked Christian Science Plaza, as well as onto Belvidere Street. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 6:00 p.m., most of the area is under existing shadow. The shadow from the approved Master Plan Huntington Avenue Building would be cast mostly onto rooftops. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto small portion of Dalton Street, a portion of Huntington Avenue and its eastern and western sidewalks, and slivers of shadow onto nearby residential streets to the east. Additional shadow from the Proposed Project beyond that approved in the Master Plan will mostly be cast onto nearby rooftops. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

4.2.4 Autumnal Equinox (September 21)

At 9:00 a.m. during the autumnal equinox, new shadow from the Project will be cast to the northwest. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto the landmarked Christian Science Plaza, as well as a portion of Massachusetts Avenue and its eastern sidewalk. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Belvidere Street and its northern and southern sidewalks, and a portion of Dalton Street and its eastern and western sidewalks. Additional shadow from the Proposed Project beyond that approved in the Master Plan will be limited to a portion of Boylston Street and the Massachusetts Turnpike, including two bus stations on Boylston Street. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 12:00 p.m., new shadow from the Project will be cast to the north. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto the landmarked Christian Science Plaza. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Dalton Street and its eastern sidewalk, as well as a portion of Belvidere Street and its northern and southern sidewalks. Additional shadow from the Proposed Project beyond that approved in the Master Plan will be limited to a small portion of the Sheraton Hotel sidewalk and parking garage entrance. By moving to the Belvidere/

Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 3:00 p.m., new shadow from the Project will be cast to the northeast. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto a portion of Huntington Avenue and its eastern and western sidewalks. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Belvidere Street and its northern and southern sidewalks, and a small portion of Dalton Street and its eastern and western sidewalks. There will be no additional shadow as a result of the Proposed Project. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 6:00 p.m. (Autumnal Equinox only), most of the area will be under existing shadow. Neither the approved Master Plan Project nor the Proposed Project will cast any new shadow on nearby streets, bus stops, or open space.

4.2.5 Winter Solstice (December 21)

The winter solstice creates the least favorable conditions for sunlight in New England. The sun angle during the winter is lower than in any other season, causing the shadows in urban areas to elongate and be cast onto large portions of the surrounding area.

At 9:00 a.m., new shadow will be cast to the northwest. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto the landmarked Christian Science Plaza, as well as a portion of Massachusetts Avenue and its eastern and western sidewalks, including the bus stop at Massachusetts Avenue and Clearway Street. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Belvidere Street and its northern and southern sidewalks, a portion of Dalton Street and its eastern and western sidewalks, and a small portion of the Massachusetts Turnpike. Additional shadow from the Proposed Project beyond that approved in the Master Plan will limited to a small portion of Beacon Street and a small portion of Storrow Drive. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 12:00 p.m., new shadow will be cast to the north. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto the landmarked Christian Science Plaza. The shadow from the approved Master Plan High-rise and Mid-rise would be cast onto a portion of Belvidere Street and its northern and southern sidewalks, as well as a portion of Dalton Street and its eastern sidewalks. There will be no additional shadow

impact from the Proposed Project. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

At 3:00 p.m., most of the area is under existing shadow. The shadow from the approved Master Plan Huntington Avenue Building would be cast onto the landmarked Christian Science Plaza, as well as a portion of Huntington Avenue. The shadow from the approved Master Plan High-rise and Mid-rise would be limited to a portion of Belvidere Street and its northern and southern sidewalks. There will be no additional shadow impact from the Proposed Project. By moving to the Belvidere/ Dalton sites the square footage previously allocated to the Huntington Avenue Building, the Proposed Project eliminates the shadow impact from the approved Master Plan Huntington Avenue Building.

4.2.6 Conclusions

The shadow impact analysis looked at net new shadow created by the Project during fourteen time periods. In some cases, new shadow from the Proposed Project will extend further than the approved Master Plan High-rise and Mid-rise buildings. However, all shadow from the Master Plan Huntington Avenue Building will be eliminated, as this building is not being constructed a part of the Project, therefor the net effect is a lessened shadow impact from the Proposed Project as compared to the approved Master Plan Project.

Shadow impacts from the Project will be quite minor. During two of the fourteen periods studied, new shadow from the Proposed Project will be cast onto nearby bus stops. Otherwise, shadow impacts are generally limited to small areas of streets and sidewalks, but no other public open spaces.

The Project is also in compliance with the shadow criteria of Section 41-16.1 of the Boston Zoning Code, which limits net new shadows on dedicated public parkland.

4.3 Daylight Analysis

4.3.1 Introduction

The purpose of the daylight analysis is to estimate the extent to which a proposed project will affect the amount of daylight reaching the streets and the sidewalks in the immediate vicinity of a project site. The daylight analysis for the Project considers three conditions: the approved Master Plan conditions, proposed conditions, and typical daylight obstruction values of the surrounding area.

Because the Project site currently consists of a parking lot and undeveloped land, the Proposed Project will inherently result in an increase in daylight obstruction compared to existing conditions. However, the resulting conditions will be a minimal increase compared to the Master Plan Project, and are typical of the area and other urban areas.



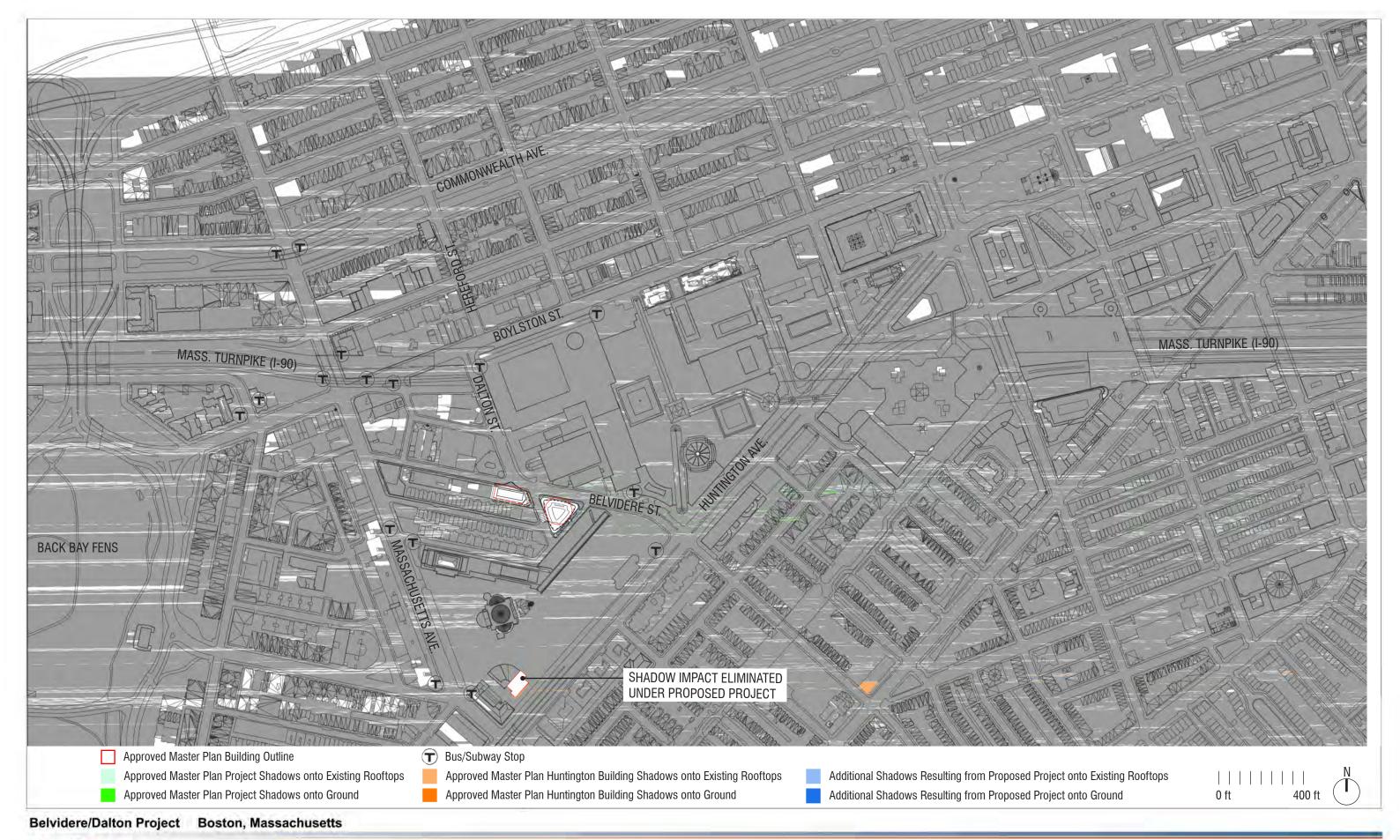
















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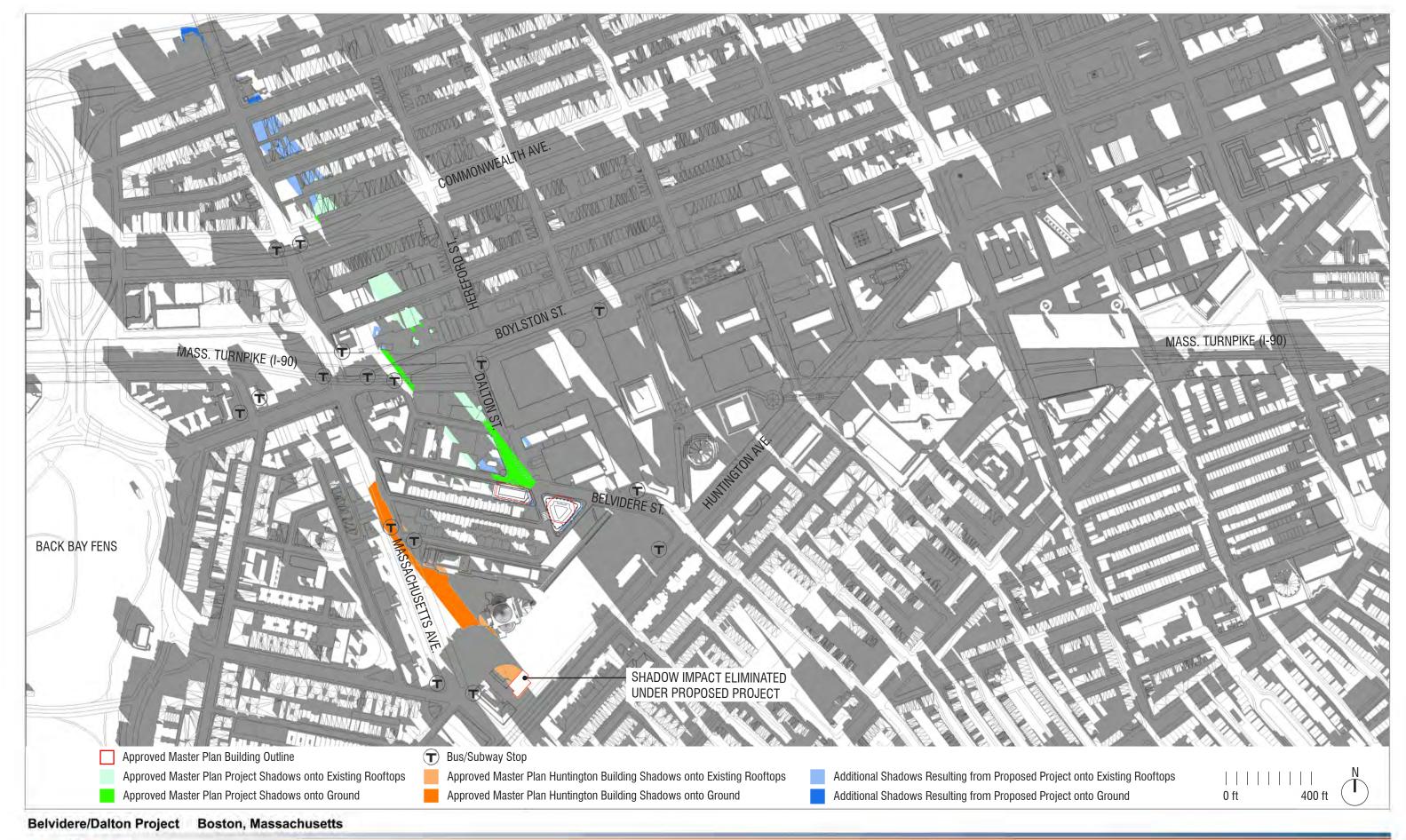




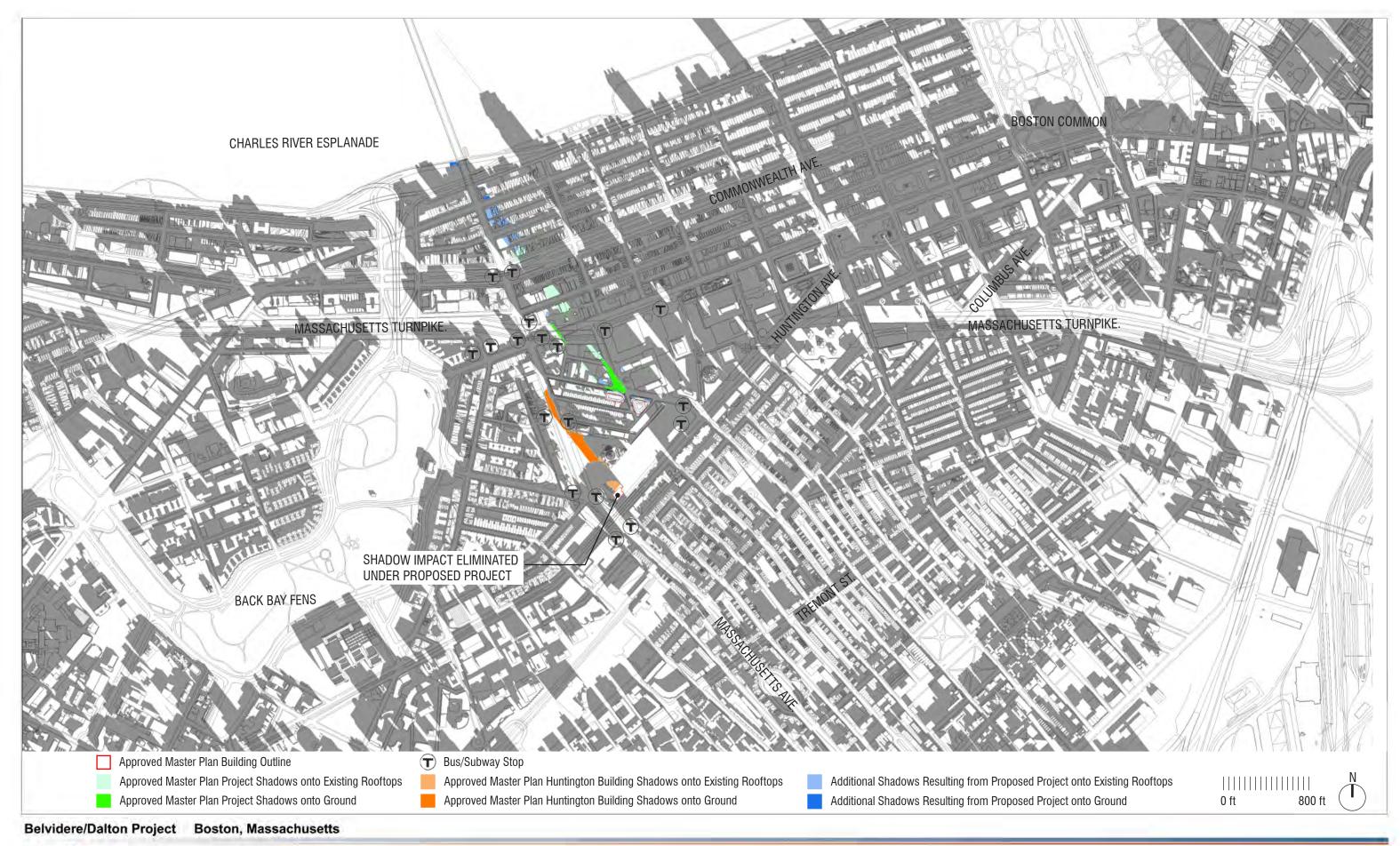












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4.3.2 Methodology

The daylight analysis was performed using the Boston Redevelopment Authority Daylight Analysis (BRADA) computer program³. This program measures the percentage of sky-dome that is obstructed by a project and is a useful tool in evaluating the net change in obstruction from existing to build conditions at a specific site.

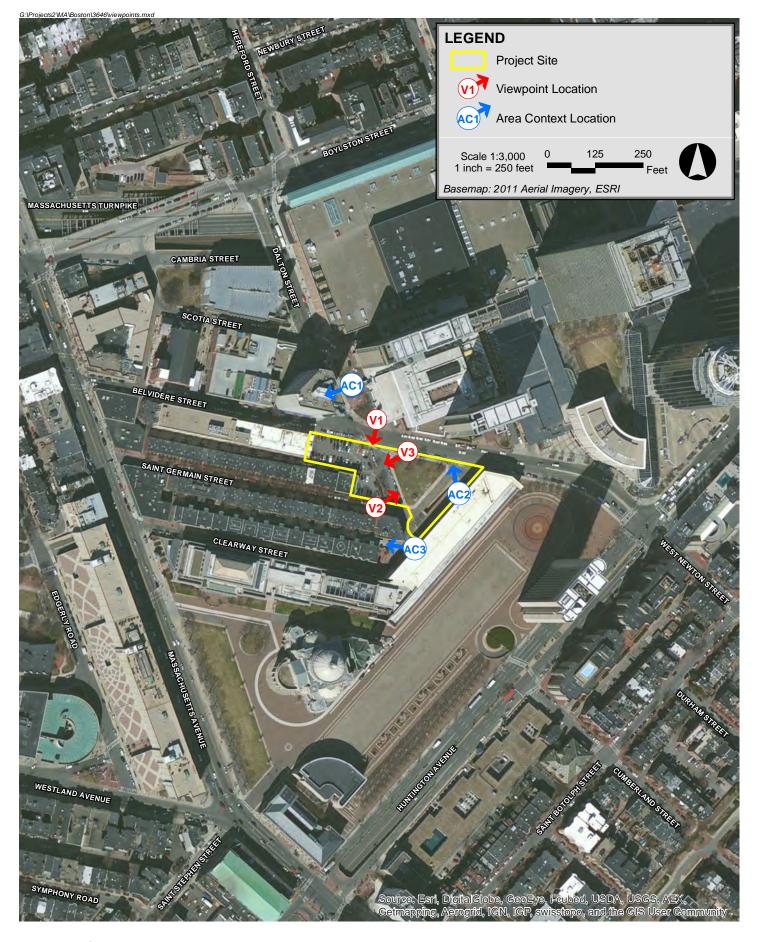
Using BRADA, a silhouette view of the building is taken at ground level from the middle of the adjacent city streets or pedestrian ways centered on the proposed building. The façade of the building facing the viewpoint, including heights, setbacks, corners and other features, is plotted onto a base map using lateral and elevation angles. The two-dimensional base map generated by BRADA represents a figure of the building in the "sky dome" from the viewpoint chosen. The BRADA program calculates the percentage of daylight that will be obstructed on a scale of 0 to 100 percent based on the width of the view, the distance between the viewpoint and the building, and the massing and setbacks incorporated into the design of the building; the lower the number, the lower the percentage of obstruction of daylight from any given viewpoint.

Since the Project site is currently undeveloped, the analysis compares the proposed conditions to the approved Master Plan conditions, as well as the context of the area.

Three viewpoints were chosen to evaluate the daylight obstruction for the Master Plan and proposed conditions; one from Belvidere Street facing both the Mid-rise and the High-rise, one from Dalton Street facing the High-rise, and one from Dalton Street facing the Mid-rise. Three area context points were considered in order to provide a basis of comparison to existing conditions in the surrounding area. The viewpoint and area context viewpoints were taken in the following locations and are shown on Figure 4.3-1.

- ♦ Viewpoint 1: View from Belvidere Street facing south toward the Project site
- ♦ Viewpoint 2: View from Dalton Street facing northeast toward the Project site
- Viewpoint 3: View from Dalton Street facing southwest toward the Project site
- Area Context Viewpoint AC1: View from Dalton Street facing southwest toward the building at 40 Dalton Street
- Area Context Viewpoint AC2: View from Belvidere Street facing northwest toward the building at 39 Dalton Street

Method developed by Harvey Bryan and Susan Stuebing, computer program developed by Ronald Fergle, Massachusetts Institute of Technology, Cambridge, MA, September 1984.





◆ Area Context Viewpoint AC3: View from Dalton Street facing southwest toward the building at 67 Saint Germain Street

4.3.3 Results

The results for each viewpoint are described in Table 4.3-1. Figures 4.3-2 to 4.3-4 illustrates the BRADA results for each analysis.

Table 4.3-1 Daylight Analysis Results

Viewpoint Location	ns	Existing Conditions	Approved Master Plan Conditions	Proposed Conditions
Viewpoint 1	View from Belvidere Street facing south toward the Project site	0%	83.9%	84.6%
Viewpoint 2	View from Dalton Street facing northeast toward the Project site	0%	96.5%	97.7%
Viewpoint 3	View from Dalton Street facing southwest toward the Project site	0%	91.7	92.5%
Area Context Points				
AC1	View from Dalton Street facing southwest toward the building at 40 Dalton Street	94.8%		N/A
AC2	View from Belvidere Street facing northwest toward the building at 39 Dalton Street	93.3%		N/A
AC3	View from Dalton Street facing southwest toward the building at 67 Saint Germain Street	72.5%		N/A

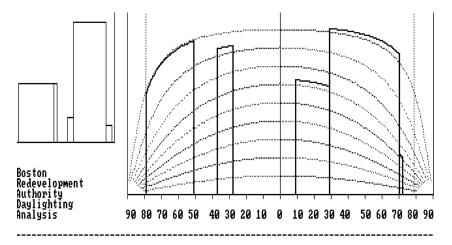
Belvidere Street- Viewpoint 1

Belvidere Street runs along the northern edge of the Project site. Viewpoint 1 was taken from the center of Belvidere Street near the intersection of Dalton Street on the northern side of the site, looking directly south toward the Project site. From this viewpoint, you can see both the High-rise and the Mid-rise buildings. The approved Master Plan would result in a daylight obstruction value of 83.9%. The development of the Proposed Project will result in a minimal increase in the daylight obstruction value over the approved Master Plan to 84.6%.

Dalton Street- Viewpoint 2

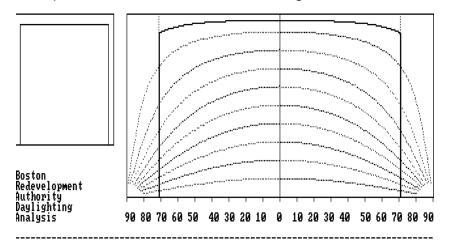
Dalton Street runs through the Project site, between the proposed High-rise and the Midrise buildings. Viewpoint 2 was taken from the center of Dalton Street facing northeast toward the High-rise portion of the Project. The approved Master Plan would result in a

Viewpoint 1: View from Belvidere Street facing south toward the Project Site



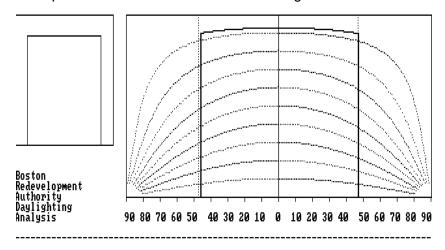
Obstruction of daylight by the building is 83.9 %

Viewpoint 2: View from Dalton Street facing northeast toward the Project Site



Obstruction of daylight by the building is 96.5 %

Viewpoint 3: View from Dalton Street facing southwest toward the Project Site



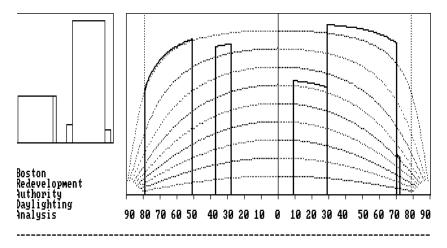
<code>Dbstruction</code> of daylight by the building is 91.7~%

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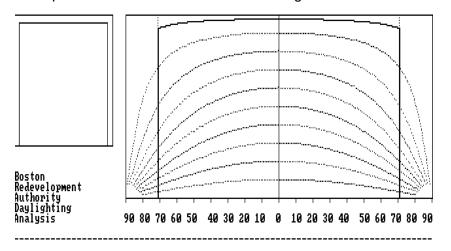


Viewpoint 1: View from Belvidere Street facing south toward the Project Site



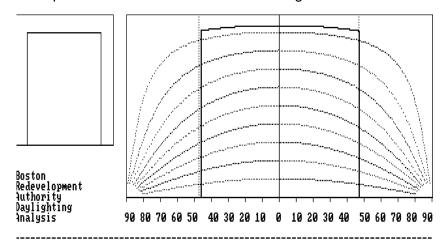
Obstruction of daylight by the building is 84.6 %

Viewpoint 2: View from Dalton Street facing northeast toward the Project Site



Obstruction of daylight by the building is 97.7 %

Viewpoint 3: View from Dalton Street facing southwest toward the Project Site



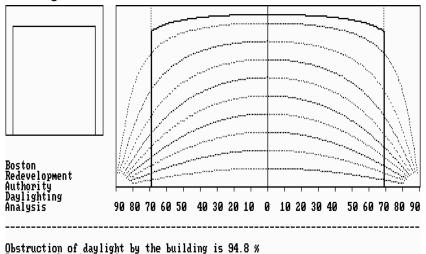
<code>]bstruction</code> of daylight by the building is 92.5 %

Belvidere/Dalton Project

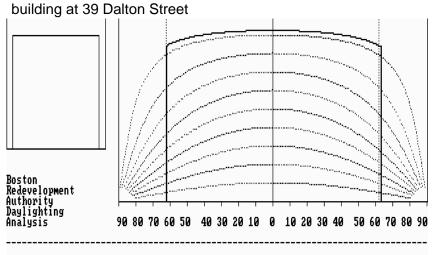
Boston, Massachusetts



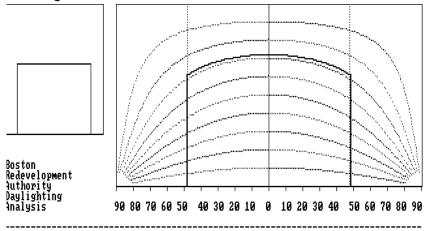
Area Context Viewpoint (AC1): View from Dalton Street facing southwest toward the building at 40 Dalton Street



Area Context Viewpoint (AC2): View from Belvidere Street facing northwest toward the



Area Context Viewpoint (AC3): View from Dalton Street facing southwest toward the building at 67 Saint Germain Street



Obstruction of daylight by the building is 72.5 %

Obstruction of daylight by the building is 93.3 %

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daylight obstruction value of 96.5%. The development of the Proposed Project will result in a slight increase in the daylight obstruction value over the approved Master Plan to 97.7%.

Dalton Street- Viewpoint 3

Viewpoint 3 was taken from the center of Dalton Street facing southwest toward the Midrise portion of the Project. The approved Master Plan would result in a daylight obstruction value of 91.7%. The development of the Proposed Project will result in a minimal increase in the daylight obstruction value over the approved Master Plan to 92.5%.

Area Context Views

The Project area is primarily characterized by mixed-use buildings with commercial, hotel and residential uses, with some retail and restaurant uses on the ground floor. The Project is located in a dense urban area with a number of high-rises in the vicinity. To provide a larger context for comparison of daylight conditions, obstruction values were calculated for the three area context viewpoints described above and shown on Figure 4.3-1. The daylight obstruction values range from 72.5% for AC3 to 94.8% for AC1. Daylight obstruction values for the Project are similar to the Area Context values.

The Approved Master Plan Huntington Building

As discussed in section 1.3.2, the approved Master Plan included a 291-foot tall building along Huntington Avenue that is not being built under the Proposed Project. Therefore, any daylight obstruction impacts that would have resulted from this building will not occur with this Project.

4.3.4 Conclusions

The daylight analysis conducted for the Project describes approved Master Plan and proposed daylight obstruction conditions at the Project site, as well as existing conditions in the surrounding area. The results of the BRADA analysis indicate that the Project will result in minor increases in daylight obstruction values as compared to the approved Master Plan.

4.4 Solar Glare

As currently designed, the majority of the Proposed Project's exterior elevations will be glazed. No reflective glass (such as that used in the new John Hancock Tower, for example) will be used however, and the Proposed Project is not expected to cause any significant solar glare impacts on the surrounding buildings, pedestrian areas, or roadways. Building details and design elements will be presented to the BRA and the Boston Civic Design Commission as the design progresses. Should there be a design change toward using more reflective glass, then a solar glare analysis will be undertaken to evaluate whether the glazing will have any negative impacts on surrounding areas.

4.5 Air Quality Analysis

4.5.1 Introduction

An air quality analysis was conducted to determine the impact of pollutant emissions from mobile sources generated by the Belvidere-Dalton Project. A microscale analysis was performed to evaluate the potential air quality impacts of carbon monoxide (CO) due to traffic flow around the Project area.

4.5.1.1 National Ambient Air Quality Standards

The 1970 Clean Air Act was enacted by the U.S. Congress to protect the health and welfare of the public from the adverse effects of air pollution. As required by the Clean Air Act, the Environmental Protection Agency (EPA) promulgated National Ambient Air Quality Standards (NAAQS) for these criteria pollutants: nitrogen dioxide (NO2), sulfur dioxide (SO2), particulate matter (PM) (PM10 and PM2.5), carbon monoxide (CO), ozone (O3), and lead (Pb). The NAAQS are listed in Table 5-1. Massachusetts Ambient Air Quality Standards (MAAQS) are typically identical to NAAQS.

NAAQS specify concentration levels for various averaging times and include both "primary" and "secondary" standards. Primary standards are intended to protect human health, whereas secondary standards are intended to protect public welfare from any known or anticipated adverse effects associated with the presence of air pollutants, such as damage to vegetation. The more stringent of the primary or secondary standards were applied when comparing to the modeling results for this Project.

A one-hour NO₂ standard was promulgated on January 22, 2010 to protect public health, including the health of sensitive populations (e.g., people with asthma, children, and the elderly). The final rule for the new hourly NO₂ NAAQS was published in the Federal Register on February 9, 2010 and became effective on April 12, 2010. The form of this standard is the three-year average of the 98th percentile of the daily maximum one-hour concentrations.

Similarly, a one-hour SO₂ standard was promulgated on June 2, 2010 to protect public health, including the health of sensitive populations (e.g., people with asthma, children, and the elderly). The final rule for the new hourly SO₂ NAAQS was published in the Federal Register on June 22, 2010 and became effective on August 23, 2010. The form of this standard is the three-year average of the 99th percentile of the daily maximum one-hour concentrations.

Table 4.5-1 National Ambient Air Quality Standards

Pollutant	Averaging Period	National Ambient Air Quality Standards and Massachusetts Ambient Air Quality Standards (micrograms per cubic meter)						
		Primary	Secondary					
NO ₂	Annual 1	100	Same					
1102	1-hour ⁷	188	None					
	Annual ^{1,8}	80	None					
60	24-hour ^{2,8}	365	None					
SO ₂	3-hour ²	None	1,300					
	1-hour ⁷	195	None					
PM10 ⁶	Annual	50	Same					
PMIU	24-hour ³	150	Same					
DM2 F	Annual ⁴	12	15					
PM2.5	24-hour ⁵	35	Same					
60	8-hour ²	10,000	Same					
CO	1-hour ²	40,000	Same					
Ozone	8-hour ³	235	Same					
Pb	3-month 1	1.5	Same					
Notes:								

Not to be exceeded

Source: 40 CFR 50 and 310 CMR 6.00

The NAAQS also reflect various durations of exposure. The short-term periods (24 hours or less) refer to exposure levels not to be exceeded more than once a year. Long-term periods refer to limits that cannot be exceeded for exposure averaged over three months or longer.

The inhalable particulate (PM10) NAAQS were promulgated on July 1, 1987 at the federal level with the intent of replacing the existing standards limiting ambient levels of Total Suspended Particulate (TSP). EPA also promulgated a Fine Particulate (PM2.5) NAAQS, effective July 18, 1997. The PM2.5 standards have since been strengthened to an annual standard of $12 \,\mu\text{g/m}^3$ and a 24-hour standard of $35 \,\mu\text{g/m}^3$.

The standards were developed by EPA to protect human health against adverse health effects with a margin of safety.

² Not to be exceeded more than once per year.

³ Not to be exceeded more than an average of one day per year over three years.

⁴ Not to be exceeded by the arithmetic average of the annual arithmetic averages from 3 successive years.

⁵ Not to be exceeded based on the 98th percentile of data collection.

⁶ Due to a lack of evidence linking health problems to long-term exposure to coarse particle pollution, EPA revoked the annual PM10 standard in 2006 (effective December 17, 2006). However, the annual standard remains codified in 310 CMR 6.00

⁷ Not to be exceeded. Based on the 3-yr average of the 98th (NO2) or 99th (SO2) percentile of the daily maximum 1-hour concentrations.

⁸The Annual and 24-hour SO2 standards were revoked on June 2, 2010. However, these standards remain in effect until one year after an area is designated for the 1-hour standard, unless currently in nonattainment.

4.5.1.2 **Background Concentrations**

To estimate background pollutant levels representative of the area, the most recent air quality monitor data reported by the MassDEP in their Annual Air Quality Reports was obtained for 2007 to 2011. MassDEP guidance specifies the use of the latest three years of available monitoring data from within 10 km of the project site.

The Clean Air Act allows for one exceedance per year of the CO and SO₂ short-term NAAQS. The highest second-high accounts for the one exceedance. Annual NAAQS are never to be exceeded. The 24-hour PM-10 standard is not to be exceeded more than once per year on average over three years. To attain the 24-hour PM-2.5 standard, the three-year average of the 98th percentile of 24-hour concentrations must not exceed 35 μ g/m³. For annual PM-2.5 averages, the average of the highest yearly observations was used as the background concentration. A new 1-hr NO₂ standard was recently promulgated. To attain this standard, the 3-year average of the 98th percentile of the maximum daily 1-hour concentrations must not exceed 188 μ g/m³.

Background concentrations were determined from the closest available monitoring stations to the Project site. The closest monitor is located at Kenmore Square, in Boston. A summary of the background air quality concentrations are presented in Table 4.5-2.

Table 4.5-2 Observed Ambient Air Quality Concentrations and Selected Background Levels

Pollutant	Averaging Time	2009	2010	2011	Background Concentration (µg/m³)	Location
	1-Hour	65.0	69.9	127.4	127.4	Kenmore Sq., Boston
SO ₂ (1)(7)(8)	3-Hour	88.4	62.4	49.4	88.4	Kenmore Sq., Boston
302	24-Hour	23.4	21.8	31.5	31.5	Kenmore Sq., Boston
	Annual	6.5	5.8	6.1	6.5	Kenmore Sq., Boston
PM-10	24-Hour	69.0	40.0	38.0	69.0	Kenmore Sq., Boston
F/VI-10	Annual	20.6	15.5	16.8	20.6	Kenmore Sq., Boston
PM-2.5	24-Hour (4)	19.1	21.9	21.2	20.7	Kenmore Sq., Boston
F/W-2.5	Annual (5)	9.0	9.3	9.4	9.2	Kenmore Sq., Boston
NO ₂ (3)	1-Hour (6)	112.8	119.4	140.8	140.8	Kenmore Sq., Boston
1002**	Annual	37.8	35.9	38.3	38.3	Kenmore Sq., Boston
CO (2)	1-Hour	1596	2166	1710	2166	Kenmore Sq., Boston
	8-Hour	1254	1710	1482	1710	Kenmore Sq., Boston

Notes: From 2007-2011 MA DEP Annual Data Summaries

 $^{^{1}}$ SO₂ reported in ppm or ppb. Converted to μ g/m³ using factor of 1 ppm = 2600 μ g/m³.

² CO reported in ppm or ppb. Converted to μ g/m³ using factor of 1 ppm = 1140 μ g/m³.

 $^{^{3}}$ NO₂ reported in ppm or ppb. Converted to μ g/m³ using factor of 1 ppm = 1880 μ g/m³. 4 Background level for 24-hour PM-2.5 is the average concentration of the 98th percentile for three years

⁵ Background level for annual PM-2.5 is the average for three years.

⁶ Maximum annual 1-hr concentrations.

⁷ The 24-hour and Annual standards were revoked by EPA on June 22, 2010, Federal Register 75-119, p. 35520.

⁸ The 2010 & 2011 SO₂ 3-hr value is not reported. Years 2007-2009 used instead.

Air quality is generally good in the area, with all of the ambient concentrations well below their respective NAAQS. For use in the microscale analysis, background concentrations of CO in ppm were required. The corresponding maximum background concentrations in ppm were 1.9 ppm (2166 μ g/m³) for 1-hour and 1.5 ppm (1710 μ g/m³) for 8-hour CO.

4.5.2 Methodology

4.5.2.1 Microscale Analysis

The BRA requires an analysis of the effects on air quality as a result of any increase in traffic generated by the Project. This "microscale" analysis is required for any intersection (including garage entrances/exits) where the Level of Service (LOS) is expected to deteriorate to D and the proposed Project causes a 10 percent increase in traffic, or where the LOS is E or F and the proposed project contributes to a reduction in LOS. The microscale analysis involves modeling of carbon monoxide (CO) emissions from vehicles idling at and traveling through both signaled and unsignalized intersections. Predicted ambient concentrations of CO for the Build and No-Build cases are compared with federal (and state) ambient air quality standards for CO.

The microscale analysis typically examines ground-level CO impacts due to traffic queues in the immediate vicinity of a project. CO is used in microscale studies to indicate roadway pollutant levels, since it is the most abundant pollutant emitted by motor vehicles and can result in so-called "hot spot" (high concentration) locations around congested intersections. The NAAQS standards do not allow ambient CO concentrations to exceed 35 parts per million (ppm) for a one-hour averaging period and 9 ppm for an eight-hour averaging period, more than once per year at any location. The widespread use of CO catalysts on current vehicles has reduced the occurrences of CO hotspots. Air quality modeling techniques (computer simulation programs) are typically used to predict CO levels for both existing and future conditions to evaluate compliance of the roadways with the standards. The analyses for the Project followed the procedure outlined in U.S. EPA's intersection modeling guidance.⁴

The microscale analysis has been conducted using the latest versions of EPA's MOBILE6.2 and CAL3QHC programs to estimate CO concentrations at sidewalk receptor locations.

Baseline (2013) and future year (2018) emission factor data calculated from the MOBILE6.2 model, along with traffic data, were input into the CAL3QHC program to determine CO concentrations due to traffic flowing through the selected intersections.

U.S. EPA, Guideline for Modeling Carbon Monoxide from Roadway Intersections; EPA-454/R-92-005, November 1992.

Existing background values of CO at the nearest monitor location at Kenmore Square were obtained from the MassDEP. CAL3QHC results were then added to background CO values of 1.9 ppm (one-hour) and 1.5 ppm (eight-hour), as provided by the MassDEP, to determine total air quality impacts due to the Projects. These values were compared to the NAAQS for CO of 35 ppm (one-hour) and 9 ppm (eight-hour).

The modeling methodology was developed in accordance with the latest Massachusetts Department of Environmental Protection (MassDEP) modeling policies and Federal modeling guidelines.⁵

Modeling assumptions and backup data for results presented in this section are provided in the Air Quality Appendix X.

Intersection Selection

A "microscale" analysis is required for the Project at intersections where 1) project traffic would impact intersections or roadway links currently operating at Level of Service ("LOS") D, E, or F or would cause LOS to decline to D, E, or F; 2) Project traffic would increase traffic volumes on nearby roadways by 10% or more (unless the increase in traffic volume is less than 100 vehicles per hour); or, 3) the Project will generate 3,000 or more new average daily trips on roadways providing access to a single location.

The modeling guidance identifies the following steps to determine the intersections to be modeled.

- ♦ Rank the top 20 intersections by traffic volumes
- ◆ Calculate the Level of Service (LOS) for each intersection
- Rank the intersections by volume
- Rank the intersections by LOS
- ◆ Model the top three intersections based on worst LOS and the top three intersections based on the highest traffic volumes

Only three signalized intersections included in the traffic study meet the above conditions (See Section 3, Transportation). The traffic volumes and LOS calculations provided in Section 3 form the basis of evaluating the traffic data versus the microscale thresholds. All three intersections were found to meet the criteria for inclusion in the microscale analysis:

The intersection of Boylston Street and Massachusetts Avenue;

⁵ 40 CFR 51 Appendix W, Guideline on Air Quality Models, 70 FR 68228, Nov. 9, 2005

- ◆ The intersection of Huntington Avenue and Belvidere Street; and,
- The intersection of Huntington and Massachusetts Avenue.

Microscale modeling was performed for the intersections based on the aforementioned methodology. The 2013 existing conditions, and the 2018 No-Build and Build conditions were each evaluated for both morning (AM) and afternoon (PM) peak.

Emissions Calculations (MOBILE6.2)

The EPA MOBILE6.2 computer program was used to estimate motor vehicle emission factors on the roadway network. Emission factors calculated by the MOBILE6.2 model are based on motor vehicle operations typical of daily periods. The Commonwealth's statewide annual Inspection and Maintenance (I&M) program was included, as well as the state specific vehicle age registration distribution. The input files for MOBILE6.2 for the existing (2013) and build year (2018) are provided by MassDEP. As is typical, minor edits to the files were necessary to allow the program to output emission factors for the various speeds used in the analyses.

Idle emission factors are obtained from factors for a vehicle speed of 2.5 mph. The resulting emission rate given in (grams/mile) is then multiplied by 2.5 mph to estimate idle emissions (in grams/hour). Moving emissions are calculated based on actual speeds at which free-flowing vehicles travel through the intersections. A speed of 30 mph is used for all free-flow traffic. Speeds of 10 and 15 mph were used for right (and U-turns, if necessary) and left turns, respectively.

Winter CO emission factors are typically higher than summer for CO. Therefore winter vehicular emission factors were conservatively used in the microscale analyses.

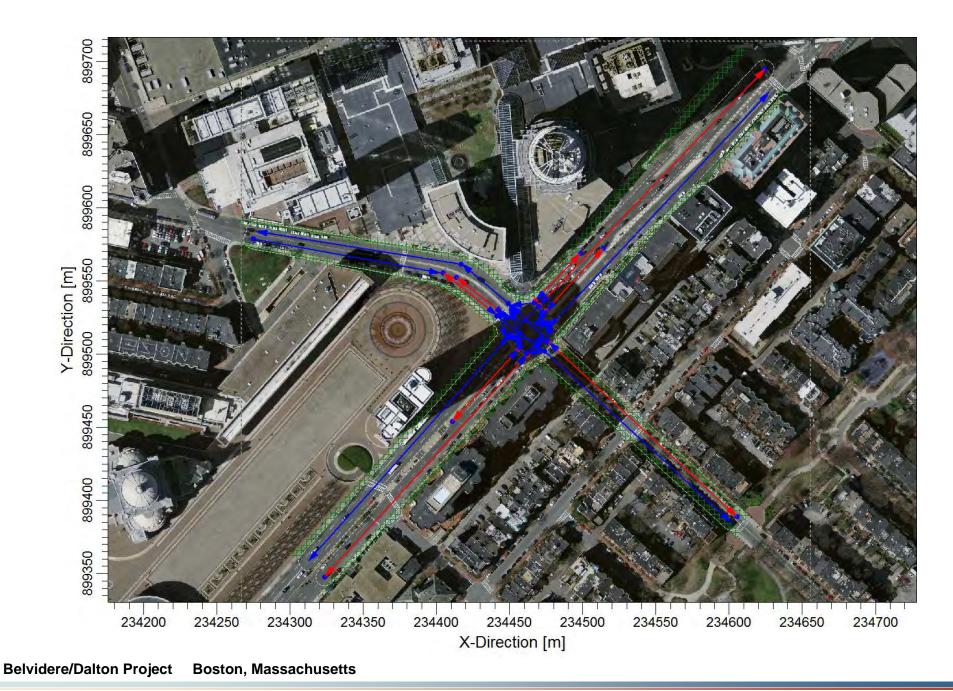
Receptors & Meteorology Inputs

Sets of up to 340 receptors were placed in the vicinity of each of the modeled intersections. Receptors extended approximately 300 feet on the sidewalks along the roadways approaching the intersection. The roadway links and receptor locations of the modeled intersections are presented in Figures 4.5-1 through, 4.5-3.

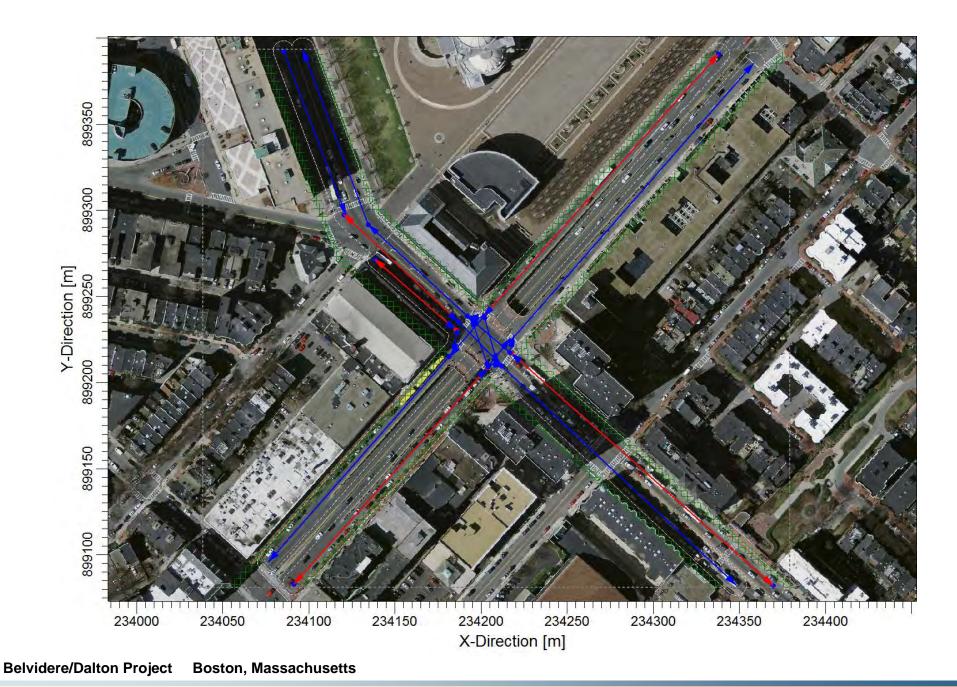


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For the CAL3QHC model, limited meteorological inputs are required. Following EPA guidance⁶, a wind speed of 1 m/s, stability class D (4), and a mixing height of 1000 meters was used. To account for the intersection geometry, wind directions from 0° to 350°, every 10° were selected. A surface roughness length of 175 cm was selected for all three intersections.⁷

Impact Calculations (CAL3QHC)

The CAL3QHC model predicts one-hour concentrations using queue-links at intersections, worst-case meteorological conditions, and traffic input data. The one-hour concentrations were scaled by a factor of 0.7 to estimate 8-hour concentrations. The CAL3QHC methodology was based on EPA CO modeling guidance. Signal timings were provided directly from the traffic modeling outputs. The CAL3QHC input parameters are also described in the Air Quality Appendix.

4.5.3 Air Quality Results

4.5.3.1 Microscale Analysis

The results of the maximum one-hour predicted CO concentrations from CAL3QHC are provided in Tables 4.5-3 through 4.5-5 for the 2013 and 2018 scenarios. Eight-hour average concentrations are calculated by multiplying the maximum one-hour concentrations by a factor of 0.7.9

The results of the one-hour and eight-hour maximum modeled CO ground-level concentrations from CAL3QHC were added to EPA supplied background levels for comparison to the NAAQS. These values represent the highest potential concentrations at the intersection as they are predicted during the simultaneous occurrence of "defined" worst case meteorology. The highest one-hour traffic-related concentration predicted in the area of the Project, for the modeled conditions (2.3 ppm) plus background (1.9 ppm) is 4.2 ppm for the 2018 afternoon peak hour case at the intersection of Huntington Avenue and Massachusetts Avenue for both the No-Build and Build conditions. The highest eight-hour traffic-related concentration predicted in the area of the Project for the modeled conditions (1.6 ppm) plus background (1.5 ppm) is 3.1 ppm for the same locations and scenarios. All

⁶ U.S. EPA, *Guideline for Modeling Carbon Monoxide from Roadway Intersections.* EPA-454/R-92-005, November 1992.

U.S. EPA, User's Guide for CAL3QHC Version 2: A Modeling Methodology for Predicting Pollutant Concentrations Near Roadway Intersections. EPA –454/R-92-006 (Revised), September 1995

U.S. EPA, Screening Procedures for Estimating the Air Quality Impact of Stationary Sources; EPA-454/R-92-019, October 1992

U.S. EPA, Screening Procedures for Estimating the Air Quality Impact of Stationary Sources; EPA-454/R-92-019, October 1992

concentrations are well below the one-hour NAAQS of 35 ppm and the eight-hour NAAQS of 9 ppm. The increase in concentrations from 2013 to 2018 is due to the geometry and signal timing changes attributed to the Symphony Streetscape Project that is starting construction in the summer of 2013.

It would be expected that any future mitigation measures implemented to improve traffic flow at any of the modeled intersections would result in further improved air quality impacts.

4.5.4 Conclusion

4.5.4.1 Microscale Analysis

Results of the microscale analysis show that all predicted CO concentrations are well below 1-hour and 8-hour NAAQS. Therefore, it can be concluded that there are no adverse air quality impacts resulting from increased traffic in the area.

Table 4.5-3 Summary of Microscale Modeling Analysis (Existing 2013)

Intersection	Peak	CAL3QHC Modeled CO Impacts (ppm)	Monitored Background Concentration (ppm)	Total CO Impacts (ppm)	NAAQS (ppm)
1-Hour					
Boylston Street and	AM	1.3	1.9	3.2	35
Massachusetts Avenue	PM	1.3	1.9	3.2	35
Huntington Avenue and	AM	1.5	1.9	3.4	35
Belvidere Street	PM	1.5	1.9	3.4	35
Huntington Avenue and	AM	1.0	1.9	2.9	35
Massachusetts Avenue	PM	1.0	1.9	2.9	35
8-Hour	<u>.</u>				
Boylston Street and	AM	0.9	1.5	2.4	9
Massachusetts Avenue	PM	0.9	1.5	2.4	9
Huntington Avenue and	AM	1.1	1.5	2.6	9
Belvidere Street	PM	1.1	1.5	2.6	9
Huntington Avenue and	AM	0.7	1.5	2.2	9
Massachusetts Avenue	PM	0.7	1.5	2.2	9

Table 4.5-4 Summary of Microscale Modeling Analysis (No-Build 2018)

Intersection	Peak	CAL3QHC Monitored Modeled CO Background Impacts Concentration (ppm) (ppm)		Total CO Impacts (ppm)	NAAQS (ppm)
1-Hour					
Boylston Street and	AM	1.2	1.9	3.1	35
Massachusetts Avenue	PM	1.1	1.9	3.0	35
Huntington Avenue and	AM	1.5	1.9	3.4	35
Belvidere Street	PM	1.4	1.9	3.3	35
Huntington Avenue and	AM	2.2	1.9	4.1	35
Massachusetts Avenue	PM	2.3	1.9	4.2	35
8-Hour					
Boylston Street and	AM	0.8	1.5	2.3	9
Massachusetts Avenue	PM	0.8	1.5	2.3	9
Huntington Avenue and	AM	1.1	1.5	2.6	9
Belvidere Street	PM	1.0	1.5	2.5	9
Huntington Avenue and	AM	1.5	1.5	3.0	9
Massachusetts Avenue	PM	1.6	1.5	3.1	9
Notes:					

CAL3QHC 8-hour impacts were conservatively obtained by multiplying 1-hour impacts by a screening factor of 0.7.

Table 4.5-5 Summary of Microscale Modeling Analysis (Build 2018)

Intersection	Peak	CAL3QHC Modeled CO Impacts (ppm)	Monitored Background Concentration (ppm)	Total CO Impacts (ppm)	NAAQS (ppm)
1-Hour					
Boylston Street and	AM	1.2	1.9	3.1	35
Massachusetts Avenue	PM	1.2	1.9	3.1	35
Huntington Avenue and	AM	1.5	1.9	3.4	35
Belvidere Street	PM	1.4	1.9	3.3	35
Huntington Avenue and	AM	2.2	1.9	4.1	35
Massachusetts Avenue	PM	2.3	1.9	4.2	35

Table 4.5-5 Summary of Microscale Modeling Analysis (Build 2018) (Continued)

Intersection	Peak	CAL3QHC Modeled CO Impacts (ppm)	Monitored Background Concentration (ppm)	Total CO Impacts (ppm)	NAAQS (ppm)
8-Hour					
Boylston Street and	AM	0.8	1.5	2.3	9
Massachusetts Avenue	PM	0.8	1.5	2.3	9
Huntington Avenue and	AM	1.1	1.5	2.6	9
Belvidere Street	PM	1.0	1.5	2.5	9
Huntington Avenue and	AM	1.5	1.5	3.0	9
Massachusetts Avenue	PM	1.6	1.5	3.1	9

Notes:

CAL3QHC 8-hour impacts were conservatively obtained by multiplying 1-hour impacts by a screening factor of 0.7.

4.6 Solid and Hazardous Waste

4.6.1 Hazardous Waste

A Phase I Environmental Site Assessment (Phase I ESA) dated 12 July 2012 was prepared using methods consistent with ASTM E1527-05. The Site Assessment identified two historical releases, of #2 fuel oil that occurred on the property in the 1990s. These releases (101 Belvidere Street (RTN 3-17859) and 103 Belvidere Street (RTN 3-13688)) have achieved regulatory closure.

Additionally, there have been offsite releases of dry cleaning solvents (volatile organic compounds (VOCs)) to the northwest of the property; these offsite releases are subject to the Massachusetts Contingency plan (MCP), Chapter 21E and have not achieved regulatory closure. Finally, an offsite utility release abatement measure (URAM, RTN 3-19708) was issued for work conducted in 2000 in Dalton Street, adjacent to the property. The URAM addressed polycyclic aromatic hydrocarbons (PAHs) and total petroleum hydrocarbon (TPH) concentrations in soil. The URAM achieved regulatory closure.

Recent characterization of the soil and groundwater at the site has not been conducted. If required, management of soil and groundwater will be in accordance with applicable local, state, and federal laws and regulations. Characterization of excess material to be excavated and generated for offsite transport will be undertaken prior to removing any material from the property.

An Asbestos and Hazardous Material Evaluation has not been conducted because there are no existing buildings on the parcels. Should any hazardous materials be encountered during construction, they will handled and disposed of in accordance with all applicable federal, state, and city regulations to protect worker safety and public health.

4.6.2 Operation Solid and Hazardous Waste Generation

The Project will generate solid waste typical of hotel, residential, restaurant and retail uses. Solid waste is expected to include wastepaper, cardboard, glass bottles and food. Recyclable materials will be recycled through a program implemented by building management. The Project will generate approximately 2,500 tons of solid waste per year.

With the exception of household hazardous wastes typical of hotel and residential developments (e.g., cleaning fluids and paint), the Project will not involve the generation, use, transportation, storage, release, or disposal of potentially hazardous materials.

4.6.3 Recycling

A dedicated recyclables storage and collection program will facilitate the reduction of waste generated by building occupants that is hauled to and disposed of in landfills. The recycling program will be fully developed in accordance with LEED standards as described in Chapter 5.

4.7 Noise Impacts

4.7.1 Introduction

A noise analysis was conducted for the Project, including an estimate of future sound levels once the Project is in operation. The analysis was conducted in accordance with the BRA Article 80 requirements to address potential impacts solely from the Project.

Baseline noise levels were measured in the vicinity of the Project and were compared to predicted noise levels based on reference sound data for likely mechanical equipment identified by the Proponent for the Project. These predicted noise levels were compared to the City of Boston Zoning District Noise Standards (City Noise Standards) and the Massachusetts Department of Environmental Protection (MassDEP) Noise Policy. The analysis indicates that predicted noise levels from Project-related mechanical equipment with appropriate noise mitigation will comply with the City Noise Standards, and will result in sound level increases that are below the limit established by the MassDEP Noise Policy.

4.7.2 Noise Terminology

There are several ways in which sound (noise) levels are measured and quantified. All of them use the logarithmic decibel (dB) scale. The following information defines the noise measurement terminology used in this analysis.

The decibel scale is logarithmic to accommodate the wide range of sound intensities found in the environment. One property of the decibel scale is that the sound pressure levels of two separate sounds are not directly additive. For example, if a sound of 50 dB is added to another sound of 50 dB, the total is only a three-decibel increase (to 53 dB), not a doubling to 100 dB. Thus, every three dB change in sound levels represents a doubling or halving of sound energy. Related to this is that a change in sound levels of fewer than three dB is imperceptible to the human ear.

Another property of decibels is that if one source of noise is 10 dB (or more) louder than another source, then the total sound level is simply the sound level of the higher source. For example, a source of sound at 60 dB plus another source of sound at 47 dB is 60 dB.

The sound-level meter used to measure noise is a standardized instrument.¹⁰ It contains "weighting networks" to adjust the frequency response of the instrument to approximate that of the human ear under various circumstances. One network is the A-weighting network (there are also B- and C-weighting networks). The A-weighted scale (dBA) most closely approximates how the human ear responds to sound at various frequencies. Sounds are frequently reported as detected with the A-weighting network of the sound-level meter. A-weighted sound levels emphasize the middle frequency (i.e., middle pitched—around 1,000 Hertz sounds), and de-emphasize lower and higher frequency sounds.

Because the sounds in our environment vary with time, they cannot simply be described with a single number. Two methods are used for describing variable sounds. These are exceedance levels and the equivalent level, both of which are derived from a large number of moment-to-moment, A-weighted sound-level measurements. Exceedance levels are values from the cumulative amplitude distribution of all of the sound levels observed during a measurement period. Exceedance levels are designated Ln, where n can have a value of 0 to 100 percent. Several sound-level metrics that are commonly reported in community noise studies are described below.

- ♦ L₉₀ is the sound level in dBA exceeded 90 percent of the time during the measurement period. The L₉₀ is close to the lowest sound level observed. It is essentially the same as the residual sound level, which is the sound level observed when there are no obvious nearby intermittent noise sources.
- ♦ L₅₀ is the median sound level, the sound level in dBA exceeded 50 percent of the time during the measurement period.

American National Standard Specification for Sound Level Meters, ANSI S1.4-1983, published by the Standards Secretariat of the Acoustical Society of America, Melville, NY.

- ◆ L₁₀ is the sound level in dBA exceeded only 10 percent of the time. It is close to the maximum level observed during the measurement period. The L₁₀ is sometimes called the intrusive sound level because it is caused by occasional louder noises like those from passing motor vehicles.
- ♦ Lmax is the maximum instantaneous sound level observed over a given period.

L_{eq}, the equivalent level, is the level of a hypothetical steady sound that would have the same energy (i.e., the same time-averaged mean square sound pressure) as the actual fluctuating sound observed. The equivalent level is designated L_{eq} and is also A-weighted. The equivalent level represents the time average of the fluctuating sound pressure, but because sound is represented on a logarithmic scale and the averaging is done with linear mean square sound pressure values, the L_{eq} is mostly determined by occasional loud, intrusive noises.

By using various noise metrics, it is possible to separate prevailing, steady sounds (the L₉₀) from occasional, louder sounds (L₁₀) in the noise environment or combined average levels (L_{eq}). This analysis of sounds expected from the Project treats all noises as though they will be steady and continuous, and hence the L₉₀ exceedance level was used. In the design of noise control treatments, it is essential to know something about the frequency spectrum of the noise of interest. Noise control treatments do not function like the human ear, so simple A-weighted levels are not useful for noise-control design. The spectra of noises are usually stated in terms of octave-band sound pressure levels, in dB, with the octave frequency bands being those established by a generally-accepted standard. To facilitate the noise-control design process, the estimates of noise levels in this analysis are also presented in terms of octave-band sound pressure levels.

4.7.3 Noise Regulations and Criteria

The primary set of regulations relating to the potential increase in noise levels is the City Noise Standards (City of Boston Code – Ordinances: Section 16–26 Unreasonable Noise; and City of Boston Air Pollution Control Commission Regulations for the Control of Noise in the City of Boston). Separate regulations within the City Noise Standards provide criteria to control different types of noise. Regulation 2 is applicable to the effects of the proposed building, as completed, and was considered in the noise study for the Project. Table 3.7-1 includes the City Noise Standards.

Additionally, MassDEP regulates community noise by its Noise Policy (DAQC policy 90-001). The MassDEP Noise Policy limits source sound levels to a 10-dBA increase in the ambient measured noise level (L₉₀) at the Project property line and at the nearest residences. The property line evaluation is typically conducted at the property line of existing

residences and/or at the property line of potential future sensitive receptors.¹¹ The policy further prohibits "pure tone" conditions—when any octave-band, center-frequency sound pressure level exceeds that of the two adjacent center-frequency sound pressure levels by three decibels or more.

Table 4.7-1 City Noise Standards, Maximum Allowable Sound Pressure Levels

Octave Band Center	Residenti	al District		l Industrial District	Business Zoning District	Industrial Zoning District
Frequency (HZ)	Daytime (dB)	All Other Times (dB)	Daytime All Other (dB) Times (dB)		Anytime (dB)	Anytime (dB)
32	76	68	79	72	79	83
63	75	67	78	71	78	82
125	69	61	73	65	73	77
250	62	52	68	57	68	73
500	56	46	62	51	62	67
1000	50	40	56 45		56	61
2000	45	33	51	39	51	57
4000	40	28	47	34	47	53
8000	38	26	44	32	44	50
A-Weighted (dBA)	60	50	65	55	65	70
Notes:	"Regulations for All standards app dB and dBA base	the Control of Nois oly at the property ed on a reference p	se in the City of Bo line of the receivin ressure of 20 micro	~ ,	cember 17, 1976.	mmission,

4.7.4 Existing Conditions

4.7.4.1 Baseline Noise Environment

An ambient noise-level survey was conducted to characterize the "baseline" acoustical environment in the vicinity of the Project site. Existing noise sources consisted of: vehicular traffic (including trucks) on the local roadways, MBTA bus traffic, pedestrian traffic, nearby mechanical equipment located in and on surrounding buildings, sidewalk cleaning, and the general din of the city.

[&]quot;Noise levels that exceed the criteria at the source's property line by themselves do not necessarily result in a violation or a condition of air pollution under MassDEP regulations (see 310 CMR 7.10 U)." MassDEP website (http://www.mass.gov/dep/air/laws/noisepol.htm), accessed April 2013.

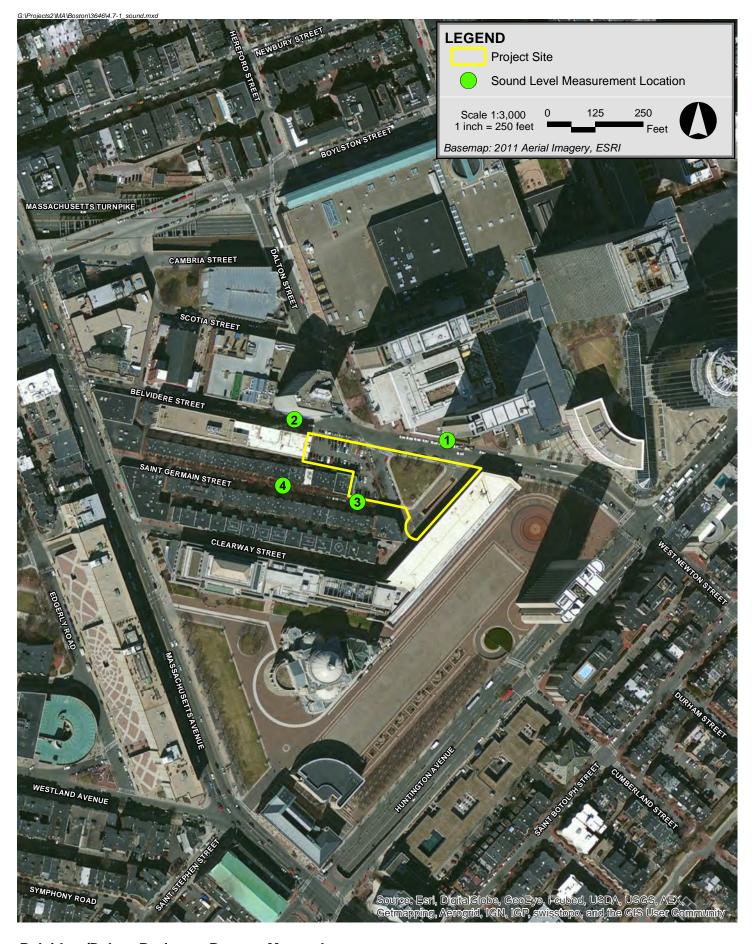
4.7.4.2 Noise Measurement Locations

The selection of the sound-monitoring locations was based upon a review of the current land uses in the Project area. Four noise-monitoring locations were selected as representative in obtaining a sampling of the ambient baseline noise environment. The measurement locations are depicted in Figure 4.7-1 and are described below.

- ◆ Location 1 is located north of the Project site, outside of the Sheraton Hotel building. Noise sources at this location include vehicular, truck, and pedestrian traffic, birds chirping (daytime only), a generator from a nearby food truck (daytime only), a street sweeper (nighttime only), a power-washing operation (nighttime only) and emergency vehicle sirens.
- ◆ Location 2 is located in front of the Hilton Hotel building main entrance north of the Project. Noise sources at this location include vehicular, truck, and pedestrian traffic, birds chirping (daytime only), whistle from nearby hotel cab stand (daytime only), a power-washing operation (nighttime only), leaf rustle (daytime only) and emergency vehicle sirens.
- ◆ Location 3 is across from 65/63 Saint Germain Street, southeast of the Project site outside of the Saint Germain Street apartment complex which is representative of residences located near the Project. Noise sources at this location include vehicular, truck, and pedestrian traffic, birds chirping (daytime only), whistle from nearby hotel cab stand (daytime only), a power-washing operation (nighttime only), a street-sweeping operation (nighttime only), construction activity (nighttime only), and emergency vehicle sirens.
- ◆ Location 4 is outside from 46 Saint Germain Street, southwest of the Project site outside of an apartment complex which is representative of residences located near the Project. Noise sources at this location include vehicular, truck, and pedestrian traffic, birds chirping (daytime only), whistle from nearby hotel cab stand (daytime only), mechanical ventilation from nearby building, dogs barking, construction activity (daytime only), and emergency vehicle sirens.

4.7.4.3 Noise Measurement Methodology

Sound-level measurements were taken for approximately 20 minutes per location during the daytime (11:15 a.m. to 1:00 p.m.) on May 6, 2013, and during nighttime hours (12:00 a.m. to 1:45 a.m.) on May 7, 2013. Since noise impacts are greatest at night when existing noise levels are lowest, the study was designed to measure community noise levels under conditions typical of a "quiet period" for the area. Daytime measurements were scheduled to exclude peak traffic conditions.



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The sound levels were measured at publicly-accessible locations at a height of approximately 1.5 meters above the ground. The measurements were made under low wind conditions, and roadway surfaces were dry. Wind speed measurements were made with a Davis Instruments TurboMeter electronic wind speed indicator, and temperature and humidity measurements were made using a General Tools digital psychrometer. Unofficial observations about meteorology, including wind speed, temperature, and humidity, as well as land use in the community, were made solely to characterize the existing sound levels in the area and to estimate the noise sensitivity at properties near the Proposed Project.

4.7.4.4 Measurement Equipment

A Larson Davis model 831 Sound Level Analyzer, equipped with a Larson Davis model PRM831 Preamplifier, a PCB Piezotronics half-inch microphone, and a four-inch windscreen were used to collect broadband and octave band ambient sound pressure level data. The instrumentation meets the "Type 1 – Precision" requirements set forth in American National Standards Institute (ANSI) S1.4 for acoustical measuring devices. The meter was tripod-mounted at a height of five feet above ground level (AGL). The meter has data logging capability and was programmed to log statistical data for each 20-minute sampling period for the following parameters: L₁₀, L₅₀, L₉₀, L_{max}, L_{min}, and L_{eq}.

All measurement equipment was calibrated in the field before and after the surveys with a LD CAL200 acoustical calibrator, which meets the standards of IEC 942 Class 1L and ANSI S1.40-1984. The meters were calibrated and certified as accurate to standards set by the National Institute of Standards and Technology. These calibrations were conducted by an independent laboratory within the past 12 months.

4.7.4.5 Baseline Ambient Noise Levels

The existing ambient noise environment consists primarily of vehicular traffic on nearby roadways, building mechanical systems, pedestrian activity, and sidewalk cleaning. Baseline noise monitoring results are presented in Table 4.7-2, and summarized below.

- ◆ The daytime residual background (L₉₀) measurements ranged from 52 to 59 dBA;
- The nighttime residual background (L₉₀) measurements ranged from 49 to 59 dBA;
- ♦ The daytime equivalent level (Leq) measurements ranged from 54 to 72 dBA; and
- ◆ The nighttime equivalent level (Leq) measurements ranged from 52 to 63 dBA.

Table 4.7-2 Baseline Ambient Sound Level Measurements

B (15	C . T	L ₁₀	L50	Leq	L90	L _{max}	L90 Sou	nd Leve	l (dB) pe	r Octave	Band C	enter Fre	quency (l	Hz)	
Receptor I.D	Start Time	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	31.5	63	125	250	500	1000	2000	4000	8000
1-Day	11:16 a.m.	69	62	72	59	97	69	65	62	57	54	55	49	43	32
2-Day	11:44 a.m.	59	59	59	59	59	65	67	61	58	56	54	51	47	33
3-Day	12:12 p.m.	61	59	59	57	70	66	64	58	55	53	53	48	41	26
4-Day	12:36 p.m.	55	54	54	52	69	57	57	54	50	49	47	42	38	26
1-Night	12:59 a.m.	67	57	63	56	78	60	59	59	55	51	51	48	41	29
2-Night	1:25 a.m.	61	60	61	59	70	60	64	61	56	54	54	52	47	36
3-Night	12:30 a.m.	59	58	58	53	64	59	59	54	52	50	49	45	35	25
4-Night	12:05 a.m.	51	50	52	49	70	54	54	52	49	47	44	39	31	21

Notes:

- 1. Daytime weather: Temperature = 67.1° F, Relative Humidity = 35%, clear skies, east winds 0-4 miles per hour. Nighttime weather: Temperature = 56.2° F, Relative Humidity = 66%, clear skies, southwest winds 0-1mile per hour.
- 2. All road surfaces were dry during measurements.
- 3. Sampling periods were at least 20 minutes in duration.
- 4. Daytime measurements were collected on May 6, 2013. Nighttime measurements were collected on May 7, 2013.

4.7.5 Overview of Potential Project Noise Sources

The Project will consist of a two buildings, the High-rise and the Mid-rise. The primary sources of continuous sound exterior to the Project will consist of ventilation, cooling, and emergency power noise sources. Multiple noise sources will be located on the roof and there will be various exhaust/intakes along the façades of the buildings on several floors.

4.7.5.1 High-rise

The major sources of sound exterior to the proposed High-rise will be three 500-ton chillers, two 1,000-ton cooling towers, two 38,000 CFM parking corridor exhaust fans, two 38,000 CFM parking corridor intake fans, six 8,500 CFM toilet exhaust fans, two 11,000 CFM kitchen exhaust fans, two 3,500 CFM laundry exhaust fans, two 3,500 CFM trash exhaust fans, 11 15,000 CFM make-up air handling units, two 11,000 CFM make-up air handling units, three 5,000 CFM air handling units, one 3,000 CFM air handling unit, 15 pumps, and one 2,000 kW standby generator. Wall construction and louver selection is assumed to result in insignificant sound pressure level contributions from interior sound levels in the fourth floor mechanical room as compared to sound pressure levels from intakes and exhausts on this level.

The proposed 500-ton chillers are Trane Model CVHF units. These will be located in the fourth floor mechanical room. The proposed rooftop cooling towers for the building are Baltimore Aircoil Company, Inc. Model 31056C 1,000-ton units. They will be located on the roof at a height of approximately 692 feet AGL. The parking corridor intake and exhaust fans are proposed to be Greenheck Model 73-BISW-41-10-I-400 fans. The two exhaust fans will discharge on the western façade of the fourth floor while the two intake fans will draw in air from the northern façade of the fourth floor. The toilet exhaust fans will be Greenheck Model SWB-333-50 fans. The toilet exhaust fans are proposed to exhaust on the northern facade of the 24th floor (2), the southwestern facade of the 24th floor (2) and on the roof (2) at a height of approximately 692 feet AGL. The kitchen exhaust fans will be Greenheck Model SWB-333-75 fans. The kitchen exhaust fans are proposed to exhaust on the southwestern façade of the 24th floor (1) and on the roof (1) at a height of approximately 692 feet AGL. The laundry exhaust fans are proposed to be Greenheck Model SWB-216-30 fans. The laundry exhaust fans are proposed to exhaust on the northern facade of the 24th floor (1) and on the roof (1) at a height of approximately 692 feet AGL. The trash exhaust fans are proposed to be Greenheck Model SWB-216-30 fans. The trash exhaust fans are proposed to exhaust on the southwestern façade of the 24th floor (1) and on the roof (1) at a height of approximately 692 feet AGL. Each 15,000 CFM make-up air handling unit is proposed to be a Johnson Controls Solution Indoor Air Handler 60x96. Six units will be located on the fourth floor with intakes along the eastern facade. An additional four units will be located on the fourth floor with intakes on the northern façade. One 15,000 CFM unit will be located on the 24th floor with the intake along the eastern façade. Each 5,000 CFM air handling unit is proposed to be a Johnson Controls Solution Indoor Air Handler 33x66. Two units will be located on the 24th floor with the intakes and exhausts along the eastern façade. A third unit will be located on the roof at a height of approximately 692 feet AGL. Each 11,000 CFM make-up air handling unit is proposed to be a Johnson Controls Solution Indoor Air Handler 48x84. One unit will be located on the 24th floor and the second on the roof with the intakes along the eastern façade. A 3,000 CFM York Solution Indoor Air Handler 39x42 is proposed to be located on the 24th floor with its intake on the western façade. 15 Bell and Gossett pumps each with a rating of 1800 RPM and 75 HP are proposed to be located in the 24th floor mechanical room. The 2,000 kW Caterpillar standby generator is proposed to be located on the roof at a height of approximately 692 feet AGL.

A tabular summary of the modeled mechanical equipment proposed for the High-rise building is presented below in Table 4.7-3a. Manufacturer specifications indicating the sound power for each piece of equipment, except where noted, are presented in Table 4.7-3b. The Project includes various noise-control measures that are necessary to achieve compliance with the applicable noise regulations. Mitigation will be installed to reduce the sound levels associated with several façade exhausts and intakes. The emergency generator will be controlled using an exhaust silencer and an acoustical enclosure. To further limit impacts from the standby generator, its required periodic, routine testing will be conducted during daytime hours, when background sound levels are highest. A summary of the noise mitigation proposed for the High-rise building is presented below in Table 4.7-3c. Transmission loss assumptions for the 24th floor of the High-rise mitigation are presented below in Table 4.7-3d.

Table 4.7-3a Modeled Noise Sources – High-rise

Noise Source	Quantity	Approximate Location	Size/Capacity
Chiller	3	4 th Floor Mechanical Room	500 Ton
Cooling Tower	2	Roof at 692' AGL	1,000 Ton
Parking Corridor Exhaust Fan	2	4 th Floor Facade	38,000 CFM
Parking Corridor Intake Fan	2	4 th Floor Facade	38,000 CFM
Toilet Exhaust Fan	6	24 th Floor Façade, Roof at 692' AGL	8,500 CFM
Kitchen Exhaust Fan	2	24 th Floor Façade, Roof at 692' AGL	11,000 CFM
Laundry Exhaust Fan	2	24 th Floor Façade, Roof at 692' AGL	3,500 CFM
Trash Exhaust Fan	2	24 th Floor Façade, Roof at 692' AGL	3,500 CFM
Air Handling Make-up Air Unit	11	4 th & 24 th Floor Façade	15,000 CFM
Air Handling Make-up Air Unit	2	24 th Floor Façade, Roof at 692' AGL	11,000 CFM
Air Handling Unit	3	24 th Floor Façade, Roof at 692' AGL	5,000 CFM
Air Handling Unit	1	24 th Floor Façade	3,000 CFM
Pumps	15	4 th Floor Mechanical Room	1800 RPM / 75 HP
Generator	1	Roof at 692' AGL	2,000 kW

Table 4.7-3b Modeled Sound Power Levels per Noise Source – High-rise

	Broadband	Sound	Level (dB) pe	r Octav	/e Band	d Cente	er Frea	uencv	(Hz)
Noise Source	(dBA)	31.5	63	125	250	500	1k	2k	4k	8k
Chiller	80	76¹	76	77	74	73	73	75	74	63
Cooling Tower	100	104 ¹	104	102	103	98	93	86	81	77
Parking Corridor Exhaust Fan – Greenheck – 38,000 CFM	78	92 ¹	92	83	79	77	70	64	61	57
Parking Corridor Intake Fan – Greenheck – 38,000 CFM	74	87¹	87	79	74	74	67	63	58	54
Toilet Exhaust Fan – Greenheck – 8,500 CFM	77	82 ¹	82	82	78	73	73	68	61	55
Kitchen Exhaust Fan – Greenheck – 11,000 CFM	82	84¹	84	87	82	77	77	73	67	61
Laundry Exhaust Fan – Greenheck – 3,500 CFM	81	86¹	86	78	79	79	75	73	68	62
Trash Exhaust Fan – Greenheck – 3,500 CFM	81	86¹	86	78	79	79	75	73	68	62
Air Handling Unit – 5,000 CFM - Exhaust	95	90¹	90	90	89	92	90	88	82	75
Air Handling Unit – 5,000 CFM - Intake	93	89¹	89	89	88	90	88	87	81	74
Air Handling Make-up Air Unit – 11,000 CFM - Intake	94	92¹	92	88	99	88	87	84	77	69
Air Handling Make-up Air Unit – 15,000 CFM - Intake	95	93¹	93	93	99	91	89	84	77	69
Air Handling Unit – 3,000 CFM - Intake	86	871	87	78	80	78	81	80	79	74
Pumps – Bell and Gossett ²	84	73	74	75	77	77	80	77	73	67
2,000 kW Generator – Mechanical – Caterpillar ³	127	130¹	130	139	130	121	11 <i>7</i>	116	114	118
2,000 kW Generator – Exhaust – Caterpillar ³	134	124 ¹	124	139	135	127	125	126	126	124

Notes:

Sound power levels do not include mitigation.

- 1. Sound level assumed to be equal to dB level in 63 Hz band.
- 2. Broadband sound power provided by the client; octave band sound power levels estimated based on procedure in Noise Control for Buildings and Manufacturing Plants, Hoover & Keith Inc.
- 3. The sound power was calculated using sound pressure levels provided at a reference distance.

Table 4.7-3c Attenuation Values Applied to Mitigate Each Noise Source – High-rise

		Sound L	evel (d	B) per	Octave	e Band	Cente	r Frequ	ency (Hz)
Noise Source	Form of Mitigation	31.5	63	125	250	500	1k	2k	4k	8k
All Air Handling Unit Intakes except Rooftop	Silencer	5	10	21	37	55	53	55	36	25
Parking Corridor Intake Fans	Silencer	5	10	21	37	55	53	55	36	25
Parking Corridor Exhaust Fans	Silencer	4	7	17	32	53	54	55	38	27
5,000 CFM Air Handling Unit Exhaust – 24 th Floor	Silencer	4	7	17	32	53	54	55	38	27
Fourth Floor Kitchen Exhaust (western façade), Trash Exhaust (western façade), & Laundry Exhaust (northern façade)	Silencer	2	5	5	19	15	12	11	9	8
8000 kW Generator – Mechanical	Enclosure	4	7	13	25	25	25	25	25	25
800 kW Generator – Exhaust	Silencer	0	1 <i>7</i>	34	32	30	20	20	20	20

Table 4.7-3d Transmission Loss Values Applied to 24th Floor Mechanical Room – High-rise

		Sound Level (dB) per Octave Band Center Frequency (Hz)								
Location	Material	31.5	63	125	250	500	1k	2k	4k	8k
Exterior Facade	Glass	2	8	13	19	23	27	27	27	31

4.7.5.2 Mid-rise

The major sources of sound exterior to the proposed Mid-rise will be two 250-ton open cell cooling towers, two 7,000 cubic-feet-per-minute (CFM) energy-recovery units, one 3,000 CFM exhaust fan for the life safety room, one 3,000 CFM exhaust fan for the mechanical penthouse, two 5,000 CFM garage exhaust fans, one 15,000 CFM garage exhaust fan for the NSTAR vault, and one 800 kW standby generator. Pumps and additional equipment will be located inside the mechanical penthouse. It is anticipated that the mechanical penthouse will be constructed in such a manner that this equipment will result in insignificant sound pressure levels as compared to the previously identified equipment. Therefore, these minor sources in the mechanical penthouse have not been included in the sound level impact assessment.

The proposed rooftop cooling towers for the building are Baltimore Aircoil Company, Inc. Model 15250 250-ton units. They will be located on the roof at a height of approximately 285 feet above ground level (AGL). Each of the two Valent VPRE Series energy-recovery units are proposed to be on the roof as well. One of the two Cook 165QMX exhaust fans is proposed to be located at the mechanical penthouse on Level 25 with the exhaust located on the northern façade of the building. The second fan is proposed to be located in the Life and Safety Room above the mechanical penthouse with the exhaust also located on the northern façade. Each of the garage exhaust fans is proposed to be a Cook 202QMX exhaust fan. Both will exhaust approximate 10 feet above grade on the southern façade of the building. The vault exhaust fan is proposed to be a Cook 270QMX fan. It will also exhaust approximately 10 feet above grade along the southern façade. The 1,000 kW Caterpillar standby generator is proposed to be located on the roof at a height of approximately 285 feet AGL.

A tabular summary of the modeled mechanical equipment proposed for the Mid-rise building is presented below in Table 4.7-4a. Manufacturer specifications indicating the sound power for each piece of equipment, except where noted, are presented in Table 4.7-4b. The Project includes various noise-control measures that are necessary to achieve compliance with the applicable noise regulations. Mitigation will be installed to reduce the sound levels associated with several façade exhausts, the cooling towers, and the emergency generator. The emergency generator will be controlled using an exhaust silencer and an acoustical enclosure. To further limit impacts from the standby generator, its required periodic, routine testing will be conducted during daytime hours, when background sound levels are highest. A summary of the noise mitigation proposed for the Mid-rise building is presented below in Table 4.7-4c.

Table 4.7-4a Modeled Noise Sources – Mid-rise

Noise Source	Quantity	Approximate Location	Size/Capacity
Cooling Tower	2	Roof at 285' AGL	250 Ton
Energy Recovery Unit	2	Roof at 285' AGL	7,000 CFM
Exhaust Fan – Life and Safety Room	1	Above the Mechanical Penthouse	3,000 CFM
Exhaust Fan – Mechanical Penthouse	1	Level 25	3,000 CFM
Garage Exhaust Fan	2	10' AGL, Facade	5,000 CFM
Vault Exhaust Fan	1	10' AGL, Facade	15,000 CFM
Generator	1	Roof at 285' AGL	800 kW

Table 4.7-4b Modeled Sound Power Levels per Noise Source – Mid-rise

	Broadband	Sound	Level (dB) pe	r Octav	/e Band	d Cente	er Freq	uency	(Hz)
Noise Source	(dBA)	31.5	63	125	250	500	1k	2k	4k	8k
Cooling Tower	102	102 ¹	102	105	102	101	98	91	85	80
Energy Recovery Unit – Valent VPRE Series – Exhaust ²	83	87 ¹	87	80	87	79	74	74	66	64
Energy Recovery Unit – Valent VPRE Series – Supply ²	98	102¹	102	95	102	94	89	89	81	79
Exhaust Fan – Cook – 3,000 CFM	73	71¹	71	70	73	73	65	61	56	47
Garage Exhaust Fan – Cook – 5,000 CFM	78	79¹	79	77	78	78	<i>7</i> 1	66	61	54
Vault Exhaust Fan – Cook – 15,000 CFM	88	83 ¹	83	86	89	87	83	79	73	66
800 kW Generator – Mechanical – Caterpillar ³	124	114 ¹	114	123	118	118	120	116	112	113
800 kW Generator – Exhaust – Caterpillar ³	121	85¹	85	111	121	117	116	115	106	87

Notes:

Sound power levels do not include mitigation.

- 1. Sound level assumed to be equal to dB level in 63 Hz band.
- 2. Each energy recovery unit contains two exhaust and two supply fans, each at 3,500 CFM. Sound power presented for 1 fan.
- 3. The sound power was calculated using sound pressure levels provided at a reference distance.

Table 4.7-4c Attenuation Values Applied to Mitigate Each Noise Source – Mid-rise

		Sound Level (dB) per Octave Band Center Frequency (Hz)								
Noise Source	Form of Mitigation	31.5	63	125	250	500	1k	2k	4k	8k
Cooling Towers	Mitigation	0	0	2	4	5	5	5	5	4
Garage and Vault Exhaust	Silencer	4	7	17	32	53	54	55	38	27
8000 kW Generator – Mechanical	Enclosure	4	7	13	25	25	25	25	25	25
800 kW Generator – Exhaust	Silencer	0	1 <i>7</i>	34	32	30	20	20	20	20

4.7.6 Modeling Methodology

The noise impacts associated with the Project were predicted at the nearest receptors using the Cadna/A noise calculation software developed by DataKustik GmbH. This software uses the ISO 9613-2 international standard for sound propagation (Acoustics - Attenuation of sound during propagation outdoors - Part 2: General method of calculation). The benefits of this software are a more refined set of computations due to the inclusion of

topography, ground attenuation, multiple building reflections, drop-off with distance, and atmospheric absorption. The Cadna/A software allows for octave band calculation of noise from multiple noise sources, as well as computation of diffraction around building edges.

4.7.6.1 Future Sound Levels- Nighttime

The analysis of sound levels at night considered all of the mechanical equipment without the emergency generators running, to simulate typical nighttime operating conditions at nearby receptors. Nine modeling locations were included in the analysis. These modeling receptors, which correspond to the closest residential locations, are depicted in Figure 4.7-2. The predicted exterior Project-Only sound levels range from 38 to 45 dBA at nearby receptors. The range at residential modeling locations is 38 to 45 dBA. This analysis conservatively evaluates hotels as residential uses.

Predicted sound levels from Project-related equipment are within the broadband and octave-band nighttime limits under the City Noise Standards at the modeling locations. This evaluation is presented in Table 4.7-5a. In addition, the predicted future total sound levels (Project + Background) are below the MassDEP criteria of 10 dBA over the quietest nighttime sound levels (the L90 level) at sensitive receptors with nighttime use. This evaluation is presented in Table 4.7-5b. Since nighttime sound levels at Locations 1, 2, and 3 were influenced by cleaning activities at the Sheraton Hotel, the ambient nighttime sound levels at Location 4 were conservatively used in this evaluation for all modeling locations. The Project's mechanical equipment is not expected to create any additional "pure-tone" conditions per the MassDEP Noise Policy when combined with existing middle of the night background sound levels at these locations as shown in Table 4.7-5c.

Table 4.7-5a Comparison of Future Predicted Project-Only Nighttime Sound Levels to the City of Boston Limits

Modeling Location	Zoning / Land Use	Broadband										
ID	Zonnig/ Land Ose	(dBA)	31.5	63	125	250	500	1k	2k	4k	8k	
Α	Residential	42	61	57	50	45	38	36	30	22	15	
В	Residential	38	54	50	44	42	34	31	27	1 <i>7</i>	4	
С	Residential	42	58	55	50	46	39	35	29	20	7	
D	Residential	44	57	55	50	49	41	35	29	19	6	
Е	Residential	44	62	58	51	47	41	37	31	22	11	
F	Residential	43	58	55	49	48	39	35	30	21	10	
G	Residential	45	64	61	53	49	40	35	30	21	20	
Н	Residential	42	58	54	49	44	40	36	29	20	5	
I	Residential	42	58	54	48	44	38	36	31	22	10	
City of Boston Limits	Residential	50	68	67	61	52	46	40	33	28	26	

Table 4.7-5b Comparison of Future Predicted Nighttime Sound Levels with Existing Background – MassDEP Noise Policy

Modeling Location ID	Zoning / Land Use	Project- Generated Sound Levels (dBA)	Existing L ₉₀ – Nighttime (dBA) ²	Future L ₉₀ – Nighttime Total (dBA) ¹	Increase (dBA) ¹
Α	Residential	42	49	50	1
В	Residential	38	49	49	0
С	Residential	42	49	50	1
D	Residential	44	49	50	1
Е	Residential	44	49	50	1
F	Residential	43	49	50	1
G	Residential	45	49	50	1
Н	Residential	42	49	50	1
I	Residential	42	49	50	1

Notes:

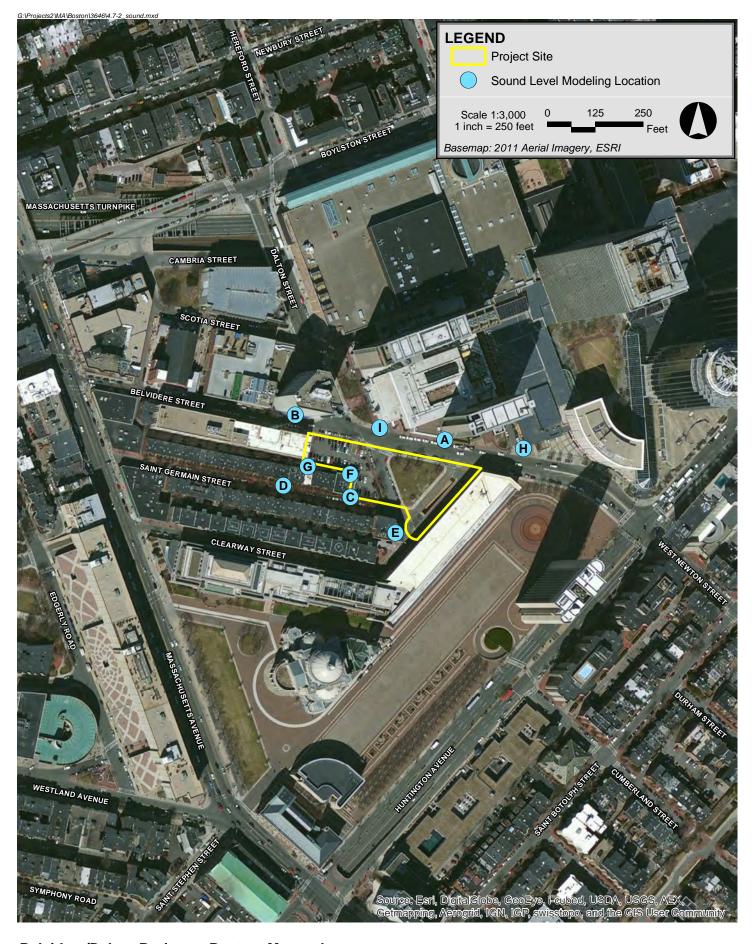
- 1. Calculation performed using existing and Project sound levels rounded to one decimal place.
- 2. Existing sound levels at Modeling ID's A through I correspond to measured sound levels at monitoring Location 4.

Table 4.7-5c MassDEP Noise Policy "Pure-Tone" Evaluation of Future Predicted Nighttime Sound Levels

Modeling	Zoning / Land Use	Sound Level (dB) per Octave Band Center Frequency (Hz) ¹										
Location ID	Zonnig/ Land Ose	31.5	63	125	250	500	1k	2k	4k	8k		
A	Residential	62	59	54	50	47	45	39	31	22		
В	Residential	5 <i>7</i>	56	53	50	47	44	39	31	21		
С	Residential	59	57	54	51	47	45	39	31	21		
D	Residential	58	57	54	52	48	45	39	31	21		
Е	Residential	62	60	55	51	48	45	40	31	22		
F	Residential	59	58	54	51	48	44	39	31	22		
G	Residential	64	62	56	52	48	44	39	31	24		
Н	Residential	59	57	54	50	48	45	39	31	21		
1	Residential	59	57	53	50	47	45	40	31	22		

Notes:

1. Calculation performed using existing and Project sound levels rounded to one decimal place.



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4.7.6.2 Future Sound Levels –Daytime

As noted above, the emergency generator will only operate during the day for brief, routine testing when the background sound levels are high, or during an interruption of power from the electrical grid. A second analysis combined noise from the Project's mechanical equipment and its emergency generator to reflect worst-case daytime conditions. The sound levels were calculated at the same receptors as in the nighttime analysis, and then were evaluated against daytime limits. Daytime ambient sound levels were incorporated where applicable.

The predicted exterior Project-Only daytime sound levels range from 44 to 47 dBA at nearby receptors. The range at residential modeling locations is 44 to 47 dBA. Predicted sound levels from Project-related equipment are within the daytime broadband and octave-band limits under the City Noise Standards at each of the modeling locations. This evaluation is presented in Table 4.7-6a. In addition, the predicted future total sound levels (Project + Background) are below the MassDEP criteria of 10 dBA over the daytime ambient sound levels (the L90 level) at each of the residential locations. That evaluation is presented in Table 4.7-6b. The Project's mechanical equipment is not expected to create any additional "pure-tone" conditions as defined under the MassDEP Noise Policy when combined with existing midday background sound levels. The predicted total sound levels per octave band are shown in Table 3.7-6c.

Table 4.7-6a Comparison of Future Predicted Project-Only Daytime Sound Levels to City Noise Standards

Modeling Location	Zoning / Land Llse	Zoning / Land Use Broadband Sound Level (dB) per Octave Band Center Frequency								uency	(Hz)
ID	Zonnig/ Land Ose	(dBA)	31.5	63	125	250	500	1k	2k	4k	8k
А	Residential	47	68	61	60	46	39	38	33	25	15
В	Residential	46	67	59	60	44	37	36	32	24	9
С	Residential	44	65	58	55	46	39	36	32	24	9
D	Residential	46	65	58	56	49	41	36	32	23	9
E	Residential	45	64	59	55	48	41	38	33	25	12
F	Residential	44	62	5 <i>7</i>	53	48	40	36	33	24	12
G	Residential	45	65	61	55	49	40	36	32	24	21
Н	Residential	47	68	61	60	46	41	39	34	25	7
I	Residential	47	68	61	61	45	39	38	34	26	11
City of Boston Limits	Residential	60	76	<i>7</i> 5	69	62	56	50	45	40	38

Table 4.7-6b Comparison of Future Predicted Daytime Sound Levels with Existing Background – MassDEP Noise Policy

Modeling Location ID	Zoning / Land Use	Project- Generated Sound Levels (dBA)	Existing L ₉₀ – Daytime (dBA)	Future L ₉₀ – Daytime Total (dBA) ¹	Increase (dBA) ¹
A	Residential	47	59 ²	59	0
В	Residential	46	59 ²	59	0
С	Residential	44	57 ²	57	0
D	Residential	46	52 ²	53	1
E	Residential	45	57 ³	57	0
F	Residential	44	57 ³	57	0
G	Residential	45	52 ⁴	53	1
Н	Residential	47	59 ⁵	59	0
1	Residential	47	59 ⁵	59	0

Notes:

- 1. Calculation performed using existing and Project sound levels rounded to one decimal place.
- 2. Sound levels at Modeling ID's A through D correspond to measured sound levels at monitoring locations 1 through 4.
- 3. Ambient sound level assumed to be comparable to Location 3.
- 4. Ambient sound level assumed to be comparable to Location 4.
- 5. Ambient sound level assumed to be comparable to Location 1

Table 4.7-6c MassDEP Noise Policy "Pure-Tone" Evaluation of Future Predicted Daytime Sound Levels

Modeling	Zoning / Land Use	Sound Level (dB) per Octave Band Center Frequency (Hz) ¹										
Location ID	Zoming/ Zama Osc	31.5	63	125	250	500	1k	2k	4k	8k		
A	Residential	71	66	64	58	54	55	50	43	32		
В	Residential	69	67	63	58	56	54	52	48	33		
С	Residential	68	64	60	56	53	53	48	41	26		
D	Residential	66	61	58	53	50	48	43	39	26		
E	Residential	68	65	60	56	53	53	48	41	27		
F	Residential	67	64	59	56	53	53	48	41	27		
G	Residential	66	63	57	53	50	48	43	39	27		
Н	Residential	71	66	64	58	54	55	50	43	32		
I	Residential	71	66	64	58	54	55	50	43	32		

Notes:

1. Calculation performed using existing and Project sound levels rounded to one decimal place.

4.7.7 Conclusions

Baseline noise levels were measured in the vicinity of the Project during the day and at night. These levels were compared to modeled sound levels that were calculated based on information provided by the manufacturers of the expected mechanical equipment. Project-Only and future sound levels (Project + Background) were compared to applicable limits.

Predicted mechanical equipment noise levels from the Project at each receptor location, taking into account attenuation due to distance, structures, and noise-control measures, will be equal to or below the broadband requirements of City Noise Standards. When the aforementioned mitigation efforts are included, the predicted sound levels from Project-related equipment are expected to remain below 50 dBA, within the nighttime residential zoning limits for the City of Boston at the nearest residential receptors. The results indicate that the Project can operate without significant impact on the existing acoustical environment, and will result in a noise experience similar to that of a typical urban setting. In addition, the Project will comply with the MassDEP Noise Policy.

At this time, the mechanical equipment and noise controls are conceptual in nature. During the final design phase of the Project, mechanical equipment and noise controls will be specified and designed to meet the applicable broadband limit and the corresponding octave-band limits of the City Noise Standards, as well as the MassDEP Noise Policy. Additional mitigation may include the selection of quieter mechanical units, and/or the addition of acoustical louvers, screening walls, mufflers, or equipment enclosures, as needed.

4.8 Storm Drainage System

4.8.1 Existing Storm Drainage System

There are BWSC storm drains in Belvidere Street and Saint Germain Street. There are also two combined sewers beneath Dalton Street as described in the Sewer Infrastructure section above. East of Dalton Street, there is a 42-inch BWSC storm drain beneath the north side of Belvidere Street and a 54-inch BWSC storm drain main beneath the south side of Belvidere Street. The 54-inch storm drain is located in an easement which runs through the Project site. West of Dalton Street, there is an 18-inch storm drain on the north side of Belvidere Street. There is a 12-inch BWSC storm drain beneath Saint Germain Street. All of the storm drains described flow into the combined sewer in Dalton Street which flows in the northerly direction.

Stormwater from the existing parking lot is collected in a closed drainage system and directed to the 18-inch BWSC storm drain in Belvidere Street. There is no existing closed drainage system on the High-rise site, stormwater runoff from the site flows to the adjacent properties and the closed drainage system in Belvidere Street and Dalton Street.

4.8.2 Proposed Storm Drainage System

The Project will increase the amount of impervious area at the site compared to the existing condition, but will maintain the existing peak rates and volumes of runoff. No significant stormwater rate or volume mitigation is anticipated.

Stormwater runoff collected from the roof of the Mid-rise will be directed to a subsurface recharge system beneath the new open space which will overflow to the 48-inch x 50-inch combined sewer in Dalton Street. Stormwater runoff collected from the High-rise will be directed across Dalton Street to the recharge system beneath the new open space. The existing BWSC storm drain system is illustrated in Figure 4.8-1

All improvements and connections to BWSC infrastructure will be reviewed as part of the Commission's site plan review process. This process includes a comprehensive design review of the proposed service connections, assessment of project demands and system capacity, and establishment of service accounts.

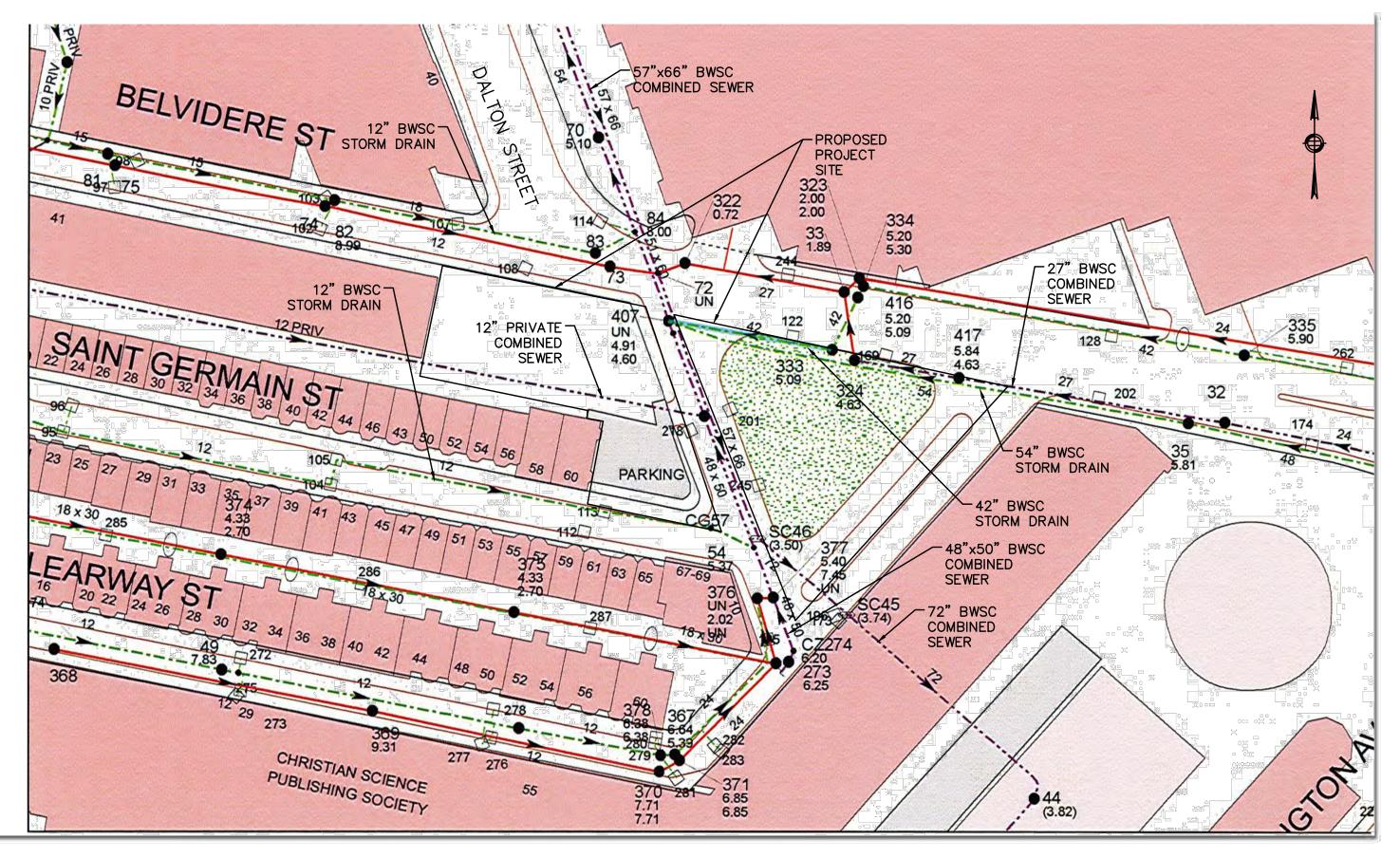
4.8.3 Water Quality Impacts

The Project will not affect the water quality of nearby water bodies. Erosion and sediment control measures will be implemented during construction to minimize the transport of site soils to off-site areas and BWSC storm drain systems. During construction, existing catch basins will be protected with filter fabric, hay bales and/or crushed stone, to provide for sediment removal from runoff. These controls will be inspected and maintained throughout the construction phase until all areas of disturbance have been stabilized through the placement of pavement, structure, or vegetative cover.

All necessary dewatering will be conducted in accordance with applicable MWRA and BWSC discharge permits. Once construction is complete, the Proposed Project will be in compliance with all local and state stormwater management policies. See below for additional information.

4.8.4 DEP Stormwater Management Policy Standards

In March 1997, the Department of Environmental Protection DEP adopted a new Stormwater Management Policy to address non-point source pollution. In 1997, the Massachusetts DEP published the Massachusetts Stormwater Handbook as guidance on the Stormwater Policy, which was revised in February 2008. The Policy prescribes specific stormwater management standards for development projects, including urban pollutant removal criteria for projects that may impact environmental resource areas. Compliance is achieved through the implementation of Best Management Practices (BMPs) in the stormwater management design. The Policy is administered locally pursuant to MGL Ch. 131, s. 40.



A brief explanation of each Policy Standard and the system compliance is provided below:

Standard #1: No new stormwater conveyances (e.g., outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

Compliance: The proposed design will comply with this Standard. No new untreated stormwater will be directly discharged to, nor will erosion be caused to wetlands or waters of the Commonwealth as a result of stormwater discharges related to the Project.

Standard #2: Stormwater management systems must be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates.

Compliance: The proposed design will comply with this Standard. The existing discharge rate will be met or decreased as a result of the improvements associated with the Project.

Standard #3: Loss of annual recharge to groundwater should be minimized through the use of infiltration measures to the maximum extent practicable. The annual recharge from the post development site should approximate the annual recharge from the pre-development or existing site conditions, based on soil types.

Compliance: The Project will comply with this standard to the maximum extent practicable.

Standard #4: For new development, stormwater management systems must be designed to remove 80% of the average annual load (post-development conditions) of Total Suspended Solids (TSS). It is presumed that this standard is met when: Suitable nonstructural practices for source control and pollution prevention are implemented; Stormwater management best management practices (BMPs) are sized to capture the prescribed runoff volume; and Stormwater management BMPs are maintained as designed.

Compliance: The proposed design will comply with this standard. Within the Project's limit of work, there will be mostly roof, landscaping, parking and pedestrian areas. Any paved areas that would contribute unwanted sediments or pollutants to the existing storm drain system will be collected by deep sump, hooded catch basins and conveyed through water quality units before discharging into the BWSC system.

Standard #5: For land uses with higher potential pollutant loads, source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater Handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable. If, through source control and/or pollution prevention, all land uses with higher potential pollutant loads cannot be completely protected from exposure to rain, snow, snow melt, and stormwater runoff, the proponent shall use the specific structural stormwater BMPs determined by the Department to be suitable for such uses as provided in the Massachusetts Stormwater Handbook. Stormwater

discharges from land uses with higher potential pollutant loads shall also comply with the requirements of the Massachusetts Clean Waters Act, M.G.L.c. 21, §§ 26-53 and the regulations promulgated there under at 314 CMR 3.00, 314 CMR 4.00 and 314 CMR 5.00.

Compliance: The proposed design will comply with this standard. The Project is not associated with Higher Potential Pollutant Loads (per the Policy, Volume I, page 1-6). The Project complies with this standard.

Standard #6: Stormwater discharge to critical areas must utilize certain stormwater management BMPs approved for critical areas. Critical areas are Outstanding Resource Waters (ORWs), shellfish beds, swimming beaches, cold-water fisheries and recharge areas for public water supplies.

Compliance: The proposed design will comply with this Standard. The Project will not discharge untreated stormwater to a sensitive area or any other area.

Standard #7: A redevelopment project is required to meet the following Stormwater Management Standards only to the maximum extent practicable: Standard 2, Standard 3, and the pretreatment and structural stormwater best management practice requirements of Standards 4, 5, and 6. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable. A redevelopment project shall also comply with all other requirements of the Stormwater Management Standards and improve existing conditions.

Compliance: The proposed design will comply with this Standard. The Project complies with the Stormwater Management Standards as applicable to the development.

Standard #8: Erosion and sediment controls must be implemented to prevent impacts during construction or land disturbance activities.

Compliance: The Project will comply with this standard. Sedimentation and erosion controls will be incorporated as part of the design of these projects and employed during construction.

Standard 9: A Long-Term Operation and Maintenance (O&M) Plan shall be developed and implemented to ensure that stormwater management systems function as designed.

Compliance: The Project will comply with this standard. An O&M Plan including long-term BMP operation requirements will be prepared for the Project and will assure proper maintenance and functioning of the stormwater management system.

Standard 10: All illicit discharges to the stormwater management system are prohibited.

Compliance: The Project will comply with this standard. There will be no illicit connections associated with the Project.

4.9 Flood Hazard Zones/ Wetlands

The Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) for the site located in the City of Boston - Community Panel Number 25025C0077G.D indicates the FEMA Flood Zone Designations for the site area. The map shows that the Project is located in a Zone X, "Areas determined to be outside the 0.2% annual chance floodplain.".

The site does not contain wetlands.

4.10 Geotechnical Impacts

4.10.1 Subsurface Soil and Bedrock Conditions

Available subsurface data and geologic information was collected for the site to define existing subsurface soil and groundwater conditions. In general, subsurface conditions anticipated in order of increasing depth below ground surface are comprised of approximately 10 ft of miscellaneous fill, over 7 ft of relatively soft organic silt and peat. Naturally deposited sand is present approximately 17 ft below grade and is 18 ft thick. The clay unit is comparatively thick (up to 130 ft) and is underlain by relatively thin (up to 2 ft thick) glacial till deposits. Bedrock is anticipated to be encountered at approximately 155 to 165 ft below the ground surface

4.10.2 Groundwater

Groundwater levels in the project area measured during the past approximately six years from observation wells monitored and published by the Boston Groundwater Trust (BGwT) range from about El. 2.2 to El. 8.2 Boston City Base (BCB) datum.

4.10.3 Project Impacts and Foundation Considerations

Proposed Foundation Construction Methodology

The proposed site development includes construction of a High-rise building on Lot #1A, which will include three levels of below grade space. Lot # 2 will be developed as a Midrise building with two levels of below grade space. Lot #1B will be developed as open space.

Column loads for the High-rise structure are expected to require deep foundations that extend into bedrock. The types of foundations being considered at this time are concrete drill shafts supported in the bedrock. The new foundations would be installed from the ground surface. The proposed Mid-rise building will likely be supported by a reinforced mat foundation bearing in the marine clay stratum or by deep foundations extending to the underlying glacial till or bedrock.

Construction of both buildings will require an excavation extending to the depth required for below grade construction. For the High-rise building depth of excavation will be 45 ft below ground surface (approximately El. -31 BCB). For the Mid-rise building depth of excavation will be in the range of 25 to 30 feet. For both buildings, it is anticipated that the excavation will terminate within the marine clay deposit. A lateral earth support system will be installed prior to excavation to provide excavation support during construction, to limit impacts to adjacent properties, control groundwater seepage, and maintain groundwater levels outside the excavation. Although the wall system has not been selected, it will likely consist of a reinforced concrete diaphragm wall ("slurry wall") installed into the clay stratum. This relatively impervious wall system is commonly used on projects of similar magnitude in the Boston area.

Due to the depth of excavation, temporary lateral bracing of the walls will be required and will probably consist of an internal cross- lot bracing system. Pre-excavation will be required along the building perimeter to remove obstructions prior to installing the excavation support system and foundations. Any penetrations through the temporary support walls and permanent basement walls will be sealed.

Potential Impacts during Excavation and Foundation Construction

Potential impacts during excavation and foundation construction include various impacts to area. The foundation design and construction will be specified and conducted to limit potential adverse impacts, especially to adjacent structures and to groundwater levels.

The Project is located in the Groundwater Conservation Overlay District (GCOD) and will be designed and constructed to comply with the groundwater conservation standards set forth in Article 32 of the City of Boston Zoning Code. In accordance with the approved Master Plan, a written determination from the Boston Water and Sewer Commission will be obtained to evidence compliance with water standards. As described above, the Proponent expects to slurry wall installed into clay to seal the excavation and protect groundwater levels. The lowest floor level for the Proposed Project is planned to be at El. -31 which is about 37 feet below the average measured groundwater level for the area.

4.11 Construction Impacts

4.11.1 Introduction

A Construction Management Plan (CMP) in compliance with the City's Construction Management Program will be submitted to the Boston Transportation Department (BTD) once final plans are developed and the construction schedule is fixed. The construction contractor will be required to comply with the details and conditions of the approved CMP.

Proper pre-planning with the City and neighborhood will be essential to the successful construction of the Project. Construction methodologies, which ensure public safety and protect nearby residences and businesses, will be employed. Techniques such as barricades, walkways and signage will be used. The CMP will include routing plans for trucking and deliveries, plans for the protection of existing utilities, and control of noise and dust.

During the construction phase of the Project, the Proponent will provide the name, telephone number and address of a contact person to communicate with on issues related to the construction.

The Proponent intends to follow the guidelines of the City of Boston and the MassDEP, which direct the evaluation and mitigation of construction impacts.

4.11.2 Construction Methodology/Public Safety

Construction methodologies that ensure public safety and protect nearby tenants will be employed. Techniques such as barricades and signage will be used. Construction management and scheduling will minimize impacts on the surrounding environment and will include plans for construction worker commuting and parking, routing plans for trucking and deliveries, and the control of noise and dust.

As the design of the Project progresses, the Proponent will meet with BTD to discuss the specific location of barricades, the need for lane closures, pedestrian walkways, and truck queuing areas. Secure fencing, signage, and covered walkways may be employed to ensure the safety and efficiency of all pedestrian and vehicular traffic flows. In addition, sidewalk areas and walkways near construction activities will be well marked and lighted to protect pedestrians and ensure their safety. Public safety for pedestrians on abutting sidewalks will also include covered pedestrian walkways when appropriate. If required by BTD and the Boston Police Department, police details will be provided to facilitate traffic flow. These measures will be incorporated into the CMP which will be submitted to BTD for approval prior to the commencement of construction work.

4.11.3 Construction Schedule

The Proponent anticipates that the Project will commence construction in early 2014 and last for approximately 36 months.

Typical construction hours will be from 7:00 am to 6:00 pm, Monday through Friday, with most shifts ordinarily ending at 3:30 pm. No substantial sound-generating activity will occur before 7:00 am. If longer hours, additional shifts, or Saturday work is required, the construction manager will place a work permit request to the Boston Air Pollution Control Commission and BTD in advance. Notification should occur during normal business hours, Monday through Friday. It is noted that some activities such as finishing activities could run

beyond 6:00 pm to ensure the structural integrity of the finished product; certain components must be completed in a single pour, and placement of concrete cannot be interrupted.

4.11.4 Construction Staging/Access

Access to the site and construction staging areas will be provided in the CMP.

Although specific construction and staging details have not been finalized, the Proponent and its construction management consultant will work to ensure that staging areas will be located to minimize impacts to pedestrian and vehicular flow. Secure fencing and barricades will be used to isolate construction areas from pedestrian traffic adjacent to the site. Construction procedures will be designed to meet all Occupational Safety and Health Administration (OSHA) safety standards for specific site construction activities.

4.11.5 Construction Mitigation

The Proponent will follow City and MassDEP guidelines which will direct the evaluation and mitigation of construction impacts. As part of this process, the Proponent and construction team will evaluate the Commonwealth's Clean Air Construction Initiative.

A CMP will be submitted to BTD for review and approval prior to issuance of a Building Permit. The CMP will include detailed information on specific construction mitigation measures and construction methodologies to minimize impacts to abutters and the local community. The CMP will also define truck routes which will help in minimizing the impact of trucks on City and neighborhood streets.

"Don't Dump - Drains to Charles River" plaques will be installed at storm drains that are replaced or installed as part of the Project.

4.11.6 Construction Employment and Worker Transportation

The number of workers required during the construction period will vary. It is anticipated that approximately 1,000- 1,200 construction jobs will be created over the length of construction. The Proponent will make reasonable good-faith efforts to have at least 50% of the total employee work hours be for Boston residents, at least 25% of total employee work hours be for minorities and at least 10% of the total employee work hours be for women. The Proponent will enter into jobs agreements with the City of Boston.

To reduce vehicle trips to and from the construction site, minimal construction worker parking will be available at the site and all workers will be strongly encouraged to use public transportation and ridesharing options. The general contractors will work aggressively to ensure that construction workers are well informed of the public transportation options serving the area. Space on-site will be made available for workers' supplies and tools so they do not have to be brought to the site each day.

4.11.7 Construction Truck Routes and Deliveries

Truck traffic will vary throughout the construction period, depending on the activity. The construction team will manage deliveries to the site during morning and afternoon peak hours in a manner that minimizes disruption to traffic flow on adjacent streets. Construction truck routes to and from the site for contractor personnel, supplies, materials, and removal of excavations required for the development will be coordinated with BTD. Traffic logistics and routing will be planned to minimize community impacts. Truck access during construction will be determined by the BTD as part of the CMP. These routes will be mandated as a part of all subcontractors' contracts for the development. The construction team will provide subcontractors and vendors with Construction Vehicle & Delivery Truck Route Brochures in advance of construction activity.

"No Idling" signs will be included at the loading, delivery, pick-up and drop-off areas.

4.11.8 Construction Air Quality

Short-term air quality impacts from fugitive dust may be expected during demolition, excavation and the early phases of construction. Plans for controlling fugitive dust during demolition, excavation and construction include mechanical street sweeping, wetting portions of the site during periods of high wind, and careful removal of debris by covered trucks. The construction contract will provide for a number of strictly enforced measures to be used by contractors to reduce potential emissions and minimize impacts, pursuant to this Article 80 approval. These measures are expected to include:

- Using wetting agents on areas of exposed soil on a scheduled basis;
- Using covered trucks;
- Minimizing spoils on the construction site;
- Monitoring of actual construction practices to ensure that unnecessary transfers and mechanical disturbances of loose materials are minimized;
- Minimizing storage of debris on the site; and
- Periodic street and sidewalk cleaning with water to minimize dust accumulations.

4.11.9 Construction Noise

The Proponent is committed to mitigating noise impacts from the construction of the Project. Increased community sound levels, however, are an inherent consequence of construction activities. Construction work will comply with the requirements of the City of Boston Noise Ordinance. Every reasonable effort will be made to minimize the noise impact of construction activities.

Mitigation measures are expected to include:

- Instituting a proactive program to ensure compliance with the City of Boston noise limitation policy;
- Using appropriate mufflers on all equipment and ongoing maintenance of intake and exhaust mufflers;
- Muffling enclosures on continuously running equipment, such as air compressors and welding generators;
- Replacing specific construction operations and techniques by less noisy ones where feasible;
- Selecting the quietest of alternative items of equipment where feasible;
- Scheduling equipment operations to keep average noise levels low, to synchronize
 the noisiest operations with times of highest ambient levels, and to maintain
 relatively uniform noise levels;
- Turning off idling equipment; and
- Locating noisy equipment at locations that protect sensitive locations by shielding or distance.

4.11.10 Construction Vibration

All means and methods for performing work at the site will be evaluated for potential vibration impacts on adjoining property, utilities, and adjacent existing structures. Acceptable vibration criteria will be established prior to construction, and vibration will be monitored, if required, during construction to ensure compliance with the agreed-upon standard.

4.11.11 Construction Waste

The Proponent will take an active role with regard to the reprocessing and recycling of construction waste. The disposal contract will include specific requirements that will ensure that construction procedures allow for the necessary segregation, reprocessing, reuse and recycling of materials when possible. For those materials that cannot be recycled, solid waste will be transported in covered trucks to an approved solid waste facility, per MassDEP Regulations for Solid Waste Facilities, 310 CMR 16.00. This requirement will be specified in the disposal contract. Construction will be conducted so that materials that may be recycled are segregated from those materials not recyclable to enable disposal at an approved solid waste facility.

4.11.12 Protection of Utilities

Existing public and private infrastructure located within the public right-of-way will be protected during construction. The installation of proposed utilities within the public way will be in accordance with the MWRA, BWSC, Boston Public Works, Dig Safe, and the governing utility company requirements. All necessary permits will be obtained before the commencement of the specific utility installation. Specific methods for constructing proposed utilities where they are near to, or connect with, existing water, sewer and drain facilities will be reviewed by BWSC as part of its site plan review process.

4.11.13 Rodent Control

A rodent extermination certificate will be filed with each building permit application for the Project. Rodent inspection monitoring and treatment will be carried out before, during, and at the completion of all construction work for each phase of the Project, in compliance with the City's requirements.

4.11.14 Wildlife Habitat

The Project Site is in an established urban neighborhood. There are no wildlife habitats in or adjacent to the Project Site.

Sustainable Design and Climate Change Preparedness

5.0 SUSTAINABLE DESIGN AND CLIMATE CHANGE PREPAREDNESS

5.1 Sustainable Design

To comply with Article 37 of the Code, the Proponent intends to measure the results of their sustainability initiatives using the framework of the Leadership in Energy and Environmental Design (LEED) rating system. As new construction for hotel, residential, retail and restaurant uses, the Project will use the LEED V3 NC 2009 (New Construction) for both the High-rise and the Mid-rise to show compliance with Article 37. The LEED rating system tracks the sustainable features of a project by achieving points in the following categories: Sustainable Sites; Water Efficiency; Energy and Atmosphere; Materials and Resources; Indoor Environmental Quality; and Innovation in Design.

LEED checklists for the High-rise and the Mid-rise are included in Appendix D, and show the credits each building anticipates achieving. The checklists will be updated regularly as the design develops and engineering assumptions are substantiated. Presently, the High-rise is targeted as being of LEED Gold Certified design standards at 64 points, and the Mid-rise is targeted as being of LEED Silver Certified design standards at 58 points.

Sustainable Sites

- <u>SS Prerequisite 1, Construction Activity Pollution Prevention:</u> An erosion and sedimentation control plan will be created and implemented to reduce pollution from construction activity.
- <u>SS Credit 1, Site Selection:</u> The Project site was chosen strategically due to its urban placement. The site is not prime farmland, is not habitat for species on federal or state threatened or endangered lists, not located within 100 feet of wetlands, or public parkland.
- SS Credit 2, Development Density and Community Connectivity: The Project site is in a densely urban area, located within walking distance to cultural, institutional and shopping centers.
- SS Credit 4.1, Alternative Transportation- Public Transportation Access: The Project site is located near several heavily served mass transit stops, including the Prudential Station on the MBTA Green Line, and the Back Bay Commuter Rail Station.
- SS Credit 4.2, Alternative Transportation- Bicycle Storage and Changing Rooms: To encourage bicycle commuting, secure bike racks accommodating a minimum of 5% of occupants are located within 200 feet of the building. In the High-rise building, a shower and changing facility will be available. In the Mid-rise building, there will be staff showers.
- SS Credit 4.4, Alternative Transportation- Parking Capacity: Parking capacity will meet but not exceed minimum local zoning requirements to help in reducing private automobile use.

SS Credits 6.1 and 6.2, Stormwater Design- Quantity Control and Quantity Control: A stormwater management plan will be developed that ensures that the post-development stormwater discharge does not exceed the existing rates and incorporates best management practices for water treatment. The stormwater management plans also addresses the removal of at least 80% of suspended solids in the runoff from the site.

<u>SS Credits 7.1 and 7.2, Heat Island Effect- Non-roof and Roof:</u> The Project will use several strategies for at least 50% of the hardscape and 75% of the roof, including: providing shade from trees, providing shade from architecture features that maximize solar reflectance, using hardscape and roofing materials that maximize solar reflectance, and using pervious pavement systems when appropriate.

SS Credit 8, Light Pollution Reduction: The Project's non-emergency interior lighting visible from the exterior will either be shielded or powered off for the hours of 11:00 p.m. to 5:00 a.m., and exterior lighting will include lighting areas only for safety and comfort. Lighting power densities will not exceed ANSI/ASHRAE/IESNA Standard 90.1-2007.

Water Efficiency

WE Prerequisite 1 and Credit 3, Water Use Reduction: The Project will have a rigorous goal of 30% water use reduction from the LEED calculated baseline through proper fixture selection and procurement, going beyond the industry best practice of 20% below the baseline.

WE Credit 1, Water Efficient Landscaping: Potable water reductions will be achieved through the plant species, density and microclimate factor, and irrigation efficiency opportunities will be explored.

Energy and Atmosphere

EA Prerequisite 1 and Credit 3, Commissioning of Building Energy Systems: In compliance with industry best practices, both prerequisite and enhanced commissioning process will occur with these buildings. An independent commissioning agent with documented commissioning authority experience will conduct a design review of the building energy systems before, during and after the construction process, including the review of contractor submittals in parallel with the design architect and engineer. A commissioning agent will later develop a systems manual that provides future operating staff the information needed to understand and optimally operate the building energy system and will review with staff and occupants within 10 months after the building's substantial completion.

<u>EA Prerequisite 2 and Credit 1, Energy Performance:</u> Through whole building energy model simulation, the Project will demonstrate a percentage improvement in the proposed building performance rating compared with the baseline building performance rating.

<u>EA Prerequisite 3 and Credit 4, Refrigerant Management:</u> Refrigerant management to minimize the negative impacts on ozone depletion and climate change will use all of the following strategies to reduce dangerous refrigerant leakage to the environment:

- Designing buildings that do not rely on chemical refrigerants.
- Designing HVAC&R equipment that uses energy efficiently.
- ◆ Selecting refrigerants with zero or low ozone depleting potential (ODP) and minimal direct global warming potential (GWP).
- Maintaining HVAC&R equipment to reduce refrigerant leakage to the environment.

EA Credit 5, Measurement and Verification: An M&V plan will be developed and implemented consistent with Option D: Calibrated Simulation (Savings Estimation Method 2) as specified by the International Performance Measurement & Verification Protocol (IPMVP).

Materials and Resources

MR Prerequisite 1, Storage and Collection of Recyclables: A dedicated recyclables storage and collection program will facilitate the reduction of waste generated by building occupants that is hauled to and disposed of in landfills.

MR Credit 2, Construction Waste Management: The project will implement a construction waste management plan with a goal to divert at least 75% of construction-related debris by volume from landfills. This plan includes redirecting recyclable recovered resources back to the manufacturing process and reusable materials to appropriate sites.

MR Credit 4, Recycled Content: The Project will aim to use recycled materials for at least 10% of the construction materials by cost.

MR Credit 5, Regional Materials: The Project will aim to include regional materials for at least 40% of the construction materials by cost.

MR Credit 7, Certified Wood: At least 50% of the wood-based materials used for the Project will be wood that is certified in accordance with the Forest Stewardship Council's principles and criteria for wood building components.

Indoor Environmental Quality

IEQ Prerequisite 1 and Credit 2, Indoor Air Quality Performance and Increased Ventilation: All occupied spaces will have increased breathing zone outdoor air ventilation rates by at least 30% above the minimum rates required by ASHRAE Standard 62.1-2007, Ventilation for Acceptable Indoor Air Quality. Mechanical ventilation systems will be designed using the ventilation rate procedure or the applicable local code, whichever is more stringent.

- <u>IEQ Prerequisite 2, Environmental Tobacco Smoke (ETS) Control:</u> The Project will comply with this prerequisite, either by prohibiting smoking or, for the residential units, via the measures laid out in Case 2, which include prohibiting smoking in common areas, the installation of weather-stripping on exterior and windows, and other measures to minimize uncontrolled pathways for ETS.
- <u>IEQ Credit 1, Outdoor Air Delivery Monitoring:</u> CO2 concentrations will be monitored within all densely occupied spaces (those with a design occupant density of 25 people or more per 1,000 square feet). CO2 monitors must be between 3 and 6 feet above the floor.
- IEQ Credits 3.1 and 3.2, Construction IAQ Management Plan- During Construction and Before Occupancy: To reduce the introduction of potentially negative effects of the construction process on indoor air quality, the construction team will meet or exceed the recommended control measures of the Sheet Metal and Air Conditioning National Contractors Association IAQ Guidelines for Occupied Buildings Under Construction. In addition, absorptive materials stored on-site and installed will be protected from moisture damage.
- <u>IEQ Credits 4.1-4.4, Low-Emitting Materials</u>: By using low-emitting materials the Project will significantly reduce odorous, irritating and/or harmful indoor air contaminants.
- <u>IEQ Credit 5, Indoor Chemical and Pollutant Source Control:</u> To reduce or mitigate human contact with airborne chemicals and particles, permanent entryway systems such as walk-off mats will be installed to capture dirt and particulates entering the building. In addition, spaces where hazardous gases or chemicals may be present such as a copying or printing room will be properly exhausted.
- IEQ Credit 6.1, Controllability of Systems-lighting: Providing individual controls for lighting increases occupants' comfort by enabling them to adjust the workspace to their individual needs. Individual controls will allow for multiple lighting possibilities in meeting spaces—lighting for specific tasks, general overhead lighting, and lighting with consideration for A/V needs, and lecture style lighting with emphasis on the learning walls or presentation screens, for example.
- <u>IEQ Credit 6.2, Controllability of Systems- Thermal Comfort:</u> The Project will provide individual comfort controls for at least 50% of the building occupants in workspace locations (e.g. private offices, open plan workstations, reception stations, ticket booths, etc.) to enable adjustments. In multi-occupant spaces where groups congregate, there will be at least one accessible means of control over thermal comfort in the space.
- <u>IEQ Credit 7.1, Thermal Comfort- Design:</u> As a result, the design HVAC systems and the building envelope will meet the requirements of ASHRAE Standard 55-2004, Thermal Environmental Conditions for Human Occupancy, Section 6.1.1.

<u>IEQ Credit 7.2, Thermal Comfort- Verification:</u> To satisfy the LEED requirements, the operating staff will participate in a thermal comfort survey of building occupants within 6 to 18 months after occupancy.

<u>IEQ Credits 8.1 and 8.2, Daylight and Views:</u> To achieve the first credit, the Project may potentially provide building occupants with a connection between indoor spaces and the outdoors through the introduction of daylit views into at least 75% of regularly occupied areas. To achieve the second credit, the Project will provide a direct line of sight to the outdoor environment via vision glazing between 30 inches and 90 inches above the finish floor for building occupants in 90% of all regularly occupied areas.

Innovation in Design

ID Credit 2, LEED Accredited Professional: The Project team includes at least one LEED Accredited Professional.

Regional Priority

The Project anticipates that several points will be achieved in the Regional Priority category.

- Regional Priority SS Credit 6.1, Stormwater Design- Quantity Control and Quality Control
- 2. Regional Priority SS Credit 7.1, Heat Island Effect- Non-roof
- 3. Regional Priority SS Credit 7.2, Heat Island Effect- Roof

5.2 Climate Change Preparedness

The Proponent understands that the City of Boston is especially interested in the adaptability of the city to long-term climate change. This interest has been manifested already by the Mayor's Executive Order Relative to Climate Change in Boston and the recent convening of the Mayor's Climate Action Leadership Committee.

In general, the Proposed Project team examined three areas of concern related to climate change: sea level rise, drought conditions, and increased number of high-heat days and higher cost of energy.

The BRA recently began asking project proponents to complete an on-line questionnaire regarding their project's climate change preparedness. Copies of the completed questionnaire for both the High-rise and the Mid-rise are included in Appendix E. Given the preliminary level of design, the responses are also preliminary and may be updated as the Project design progresses.

5.2.1 Sea Level Rise

According to the Intergovernmental Panel on Climate Change (IPCC), if sea level continues to rise at the current rate, the sea level in Massachusetts as a whole will rise by one foot by the year 2100. However, using a high emissions scenario, sea level rise could reach six feet¹. According to The Boston Harbor Association's Seal-level Rise Maps, the Project site would not be impacted by a rise in sea level of up to five feet. The Proponent has not taken any special precautions to protect against sea level rise.

5.2.2 Drought Conditions

As described in Section 5.1 Water Efficiency, the Proposed Project will employ steps to greatly reduce water consumption and is targeting a 30 percent reduction compared to the baseline case. Further, Project landscaping will be designed to require as little water as practicable. While these measures will not protect against a regional drought, they will incrementally lessen demand on the MWRA system. If similar water conservation measures were to be widely adopted throughout the MWRA's service area, it could potentially make drought conditions more tolerable by making water supplies able to last longer.

5.2.3 High Heat Days and Cost of Energy

The IPCC has predicted that in Massachusetts, the number of days with temperatures greater than 90°F will increase from five to twenty. To prepare for this, when possible the Project will provide shade from trees; provide shade from architecture features that maximize solar reflectance, use hardscape and roofing materials that maximize solar reflectance, and use pervious pavement systems in order to reduce the heat island effect of urban development. In addition all residential units will have operable windows to allow for natural cooling.

Energy modeling for the Project's two buildings has not yet been completed; however, as indicated on the LEED Checklist, the Proponent will strive to reduce the Project's overall energy demand and GHG emissions that contribute to global warming. The Project's proposed TDM program described in Section 3.5 will also help to lessen fossil fuel consumption.

¹ IPCC (Intergovernmental Panel on Climate Change), 2007. Climate Change 2007: The Physical Science Basis. Contribution of Working Group I to the Fourth Assessment Report of the Intergovernmental Panel on Climate Change [Solomon, S., D. Qin, M. Manning, Z. Chen, M. Marquis, K. B. Avery, M. Tignor, and H. L. Miller (eds.)]. Cambridge University Press, Cambridge, UK, and New York, 996 pp.

Urban Design

6.0 URBAN DESIGN

The Project site is located along the "High Spine" that includes both the Hancock Building and the Prudential Center. The Project site also sits on the far northern edge of the Christian Science Plaza, one of Boston's most cherished and venerable landmarks. The Plaza's skillfully-scaled building and plaza elements form a singular composition that is grand in its vision and impressive in its execution, providing the City with a majestic urban experience. Each building within the complex is exquisite in its individual architectural approach, proportions and detailing, resulting in a classically modernist expression of the late twenty century. Pei, Cobb, Freed & Partners, the architects of the Plaza, created for the Church an architectural masterpiece in Boston.

In order to produce a design that compliments the existing Christian Science Plaza, the Proponent has engaged as one of its collaborating architects Henry Cobb of Pei, Cobb, Freed & Partners. Mr. Cobb is a contemporary of, and partners with, Araldo Cosutta, who designed the Plaza. Mr. Cobb is also notable for his past work in Boston, which includes the Hancock Building in the Back Bay and the Moakley Courthouse in the Seaport.

The Proposed Project, which consists of a High-rise and Mid-rise building, has been designed so that these new components will enhance and elevate the Belvidere and Dalton streetscape to a design stature equaling the Christian Science Center itself. The new structures will bring forth architecture that is of "this time", with continued emphasis on architectural proportion and elegance of detail, while combining sustainable design practices and an overall commitment to enhancing the pedestrian experience in this important area of Boston.

The buildings are designed to blend well with the existing ensemble of buildings and open space, and work harmoniously with the surrounding areas. The proposal adds height to the High-rise building (as compared to the Plaza Revitalization Plan), bringing it more into proportion with its high rise environment, addressing not just the Prudential Tower, but even the Hancock Tower, expanding the grouping of tall buildings on the city skyline. See Figure 6-1 for an aerial perspective of the Proposed Project.

At the larger urban scale, the Project represents the harmonization of the Christian Science Center precinct and the Boston high spine. The Christian Science Center precinct is an equilateral triangle formed by Huntington Avenue to the southeast, Massachusetts Avenue to the southwest, and Belvedere Street to the north. The High-rise parcel is also triangular in shape, and thus consistent with the overall geometries of the Christian Science Center precinct. To maintain this geometry, the High-rise has evolved as a "soft" triangular shape that extends up 56 stories. The Mid-rise follows a more rectilinear form for its 25 stories. The Boston high spine includes all of the buildings within the Prudential Center area, which is adjacent to the site, and extends further east to the Hancock Tower and beyond.





The lower register of each building is designed to form a pedestrian-scaled experience that deliberately transforms the scale, materiality and expression of the buildings. Each of the buildings' entries face a new public open space, thus creating a new street experience within the context of the larger urban experience.

The High-rise Building

The proposed High-rise shape is derived from the equilateral triangle, softened by gently-curved sides and rounded corners. The resulting High-rise form complements without competing with the Mother Church, while its eastern face appropriately aligns with the orientation of the Reflecting Pool and the buildings that frame it. Thus the new High-rise, results in a smooth transition from the adjoining Prudential Center to the landmarked Christian Science Plaza.

The High-rise is based in a podium approximating the 67-foot height of the Plaza's Colonnade Building where it faces that building. The podium's volume will be articulated in such a way as to interact vigorously with the High-rise, so that the latter is seen to rise gracefully from the ground rather than awkwardly from the podium roof. The podium's masonry and glass exterior is enlivened by generous street-level entries and upper-level openings that celebrate the quasi-public spaces within, while relating harmoniously to the adjoining residential neighborhood. The new High-rise will be a welcome enrichment of the urban scene. See Figures 6-2 through 6-4 for ground level perspectives of the High-rise.

The Mid-rise Building

The Mid-rise building presents itself within the City as an integral part of the urban fabric on Dalton Street and Belvidere Street. This building is a pivot point for the project, anchoring the development at the intersection of Belvidere and Dalton Streets, and representing the last and furthest development of the Plaza and Christian Science precinct. The scale of the Mid-rise is much reduced from the High-rise component to match that of its adjacent neighbors, notably the Hilton and Sheraton towers. The scale of this building will also respect the surrounding, lower residential blocks comprised of the handsomely scaled buildings on Saint Germain, Clearway and Belvidere Streets.

The ground floor along Belvidere Street nominally aligns with the existing street wall to the west and emphasizes the continuation of the street pedestrian circulation and view corridor. The facades of this building are varied, with the north façade above this level shaped to follow the motion of the curved intersection at Belvidere and Dalton Streets. The curve also resembles, and retains a balance with its neighboring High-rise. The south and west faces of the building are derivative of the rectilinear geometries of the surrounding city blocks, and thus they present themselves as coplanar. This opens the possibility for a change in materials, color and texture of the building facades, which in turn creates interest as the building is viewed from differing points. See Figures 6-5 and 6-6 for ground level perspectives of the Mid-rise.





















Like the High-rise, the Mid-rise residential building is prominently positioned to interact with the new public open space at the intersection of Saint Germain and Dalton Streets. The lobby of the Mid-rise will open directly onto the new open space.

As with all civic minded developments, the Mid-rise and the High-rise buildings both seek to create a harmonious urban environment, one that creates exquisite architecture that engages with pedestrians and invites them to participate, and that establishes a new defined "place" for hospitality, living, and entertaining within the City of Boston.

Development Plan

The proposed Belvidere and Dalton Street buildings will contain new uses combining a hotel, residences and restaurants that will enhance the surrounding streets with increased pedestrian activity and life. A full-service luxury hotel will occupy the High-rise on Belvidere Street, with residential condominium units in the upper floors. The Mid-rise building will contain luxury rental housing.

The High-rise, with its gently curved triangular form includes the Project's hotel component in the lower register of the building and condominium residences above. Restaurants, lobbies and service access are strategically arranged at the base of the building to optimize pedestrian and vehicular access in an effortless and graceful manner. A café along Belvidere Street is designed to spill out onto the sidewalk to enliven the street edge, while the two lobbies, one for the hotel and one for the residences, have their primary entry facing onto Dalton Street, away from the traffic of Belvidere. The ground floor of the building is porous to the extent that it is mostly public, with access to the hotel lobby and the café and restaurant amenities.

The Mid-rise building has also been shaped with a gentle curving façade facing Belvidere Street, in the same spirit as the High-rise geometries. Retail space will be located along Belvidere Street to help in enlivening that streetscape.

The arrival experience to the development will be effortless, with pedestrians, motorists and taxis accommodated in a graceful manner that does not mar the streetscape or become an impediment to pedestrians. Service and parking entries will be discreet.

At the lobby level, the two new buildings present themselves and their front doors graciously to the residential neighborhoods of Saint Germain and Clearwater Streets. The new open space becomes the important centerpiece and focal point for the pedestrian environment created by the surrounding High rise and the Mid-rise buildings and the existing neighborhood, all of which comprise this new development.

The new buildings will not diminish or overwhelm the beautiful residential neighborhoods near the site. The proposed open space is an important element in this transition between old and new. Its design will define the urban character of the development at the ground plane, while respecting the surrounding neighborhoods.

This site is in a pivotal and important location. It calls for an iconic architectural solution that embraces the architecture of the Christian Science Center, while also establishing an architectural character that is forward looking for this century.

Historic and Archaeological Resources

7.0 HISTORIC AND ARCHAEOLOGICAL RESOURCES

This section describes the historic and archaeological resources within and in the vicinity of the Project site.

7.1 Historic Resources

No historic resources are located within the Project site. The Project site is located adjacent to the Christian Science Center Complex, a Boston Landmark that is listed in the State Register of Historic Places. The Project site is also located in the vicinity of several historic resources listed in the State and National Registers of Historic Places and included in the Inventory of Historic and Archaeological Assets of the Commonwealth. Figure 7-1 and Table 7-1 identify historic resources within ½ mile of the Project site.

Table 7-1 Historic Resources in Vicinity of Project Site

Listed in the National Register of Historic Places			
Map No	Name	Address	
Α	Horticultural Hall	300 Massachusetts Avenue	
В	Symphony Hall (also a NHL)	301 Massachusetts Avenue	
С	The New Riding Club	52 Hemenway Street	
D	Fenway-Boylston Historic District	Boylston, Westland and Hemenway Streets	
E	Back Bay Historic District	Arlington, Providence, St. James, Exeter and Boylston Streets, Charlesgate East and the Charles River	
F	Saint Botolph Street Area (NRDOE)	Blackwood, Cumberland, Durham, Follen, Saint Botolph and West Newton Streets	
G	South End District	Penn Central Railroad, Massachusetts and Harrison	
		Avenues and East Berkeley and Tremont Streets	
Listed in the State Register of Historic Places as Local Landmarks			
E	Back Bay Architectural District	Back Street, Embankment Road and Arlington, Boylston	
		and Charlesgate East	
G	South End Landmark District	Penn Central Railroad, Camden Street, Harrison Avenue	
		and East Berkeley and Tremont Streets	
Н	Christian Science Center Complex	Huntington Avenue, Horticultural Hall, Massachusetts	
		Avenue, Clearway, Dalton and Belvidere Streets	
F	Saint Botolph Street Area Architectural	Harcourt Street, Penn Central Railroad. Alley north of	
	Conservation District (LL, NRDOE)	Massachusetts Avenue and alley east of Huntington	
		Avenue	

Table 7-1 Historic Resources in Vicinity of Project Site (Continued)

Included in the Inventory of Historic and Archaeological Assets of the Commonwealth			
1	Saint Germain Street	8, 10, 12, 14-59, 61, 63, 65 St. Germain Street	
2	Henry M Whitney Row House	28-56 St. Stephen Street	
3	Jesse Tirrell Row House	3-22 Symphony Road	
4	David Thomas Apartment Building	25 St. Stephen Street	
5	Hemenway Chambers – Hotel Hemenway	91 Westland Avenue	
6	A.J. Bawford Store	58 Burbank Street	
7	John P. Webber Row Houses	12-30 Edgerly Road	
8	Saint Cecilia Roman Catholic Church	14-18 Belvidere Street	
9	State Street Trust Company Building	130-132 Massachusetts Avenue	
10	Fenway Theater	136 Massachusetts Avenue	
11	William Smith Row House	179-181 Massachusetts Avenue	

A portion of the Project site is identified in the Christian Science Complex Study Report prepared by the Boston Landmarks Commission as "Triangle Park." The site was once a larger triangle of land lined with rowhouses. The site is currently an open turf area with some deciduous trees. Although identified in the Study Report, "Triangle Park" is not part of the Christian Science Center Complex Landmark District. The Study Report also envisioned construction of a new tower on the "Triangle Park" and nearby Belvidere Street parcel.

7.2 Archaeological Resources

The Proposed Project is located on filled land which has been previously disturbed by prior construction. No previously identified archaeological resources are located within the Project site. No impacts to archaeological resources are anticipated.

7.3 Visual Impacts to Historic Resources

The Proposed Project is situated adjacent to the Christian Science Center Complex. Due to their height, the proposed new buildings will be visible from nearby historic resources. The new construction will serve as an intermediately-scaled structure in the context of the taller Prudential and Hancock towers. The base of the buildings both feature strong bases of varied materials. By creating a heavier base, the lower portions of the buildings will relate to the nearby lower-scale masonry structures within the Christian Science Center Complex and the rowhouses on Saint Germain Street. The ground level will also be activated by pedestrian scale entrances and storefronts and sidewalks to connect directly to the pedestrian scale of Belvidere and Saint Germain Streets. It is expected that the taller portions of the High-Rise Building will be largely constructed of glass, giving it a lighter feeling, and will relate directly with the Prudential Building and Hancock towers in the Boston skyline.





7.4 Shadow Impacts to Historic Resources

Limited new shadow from the Project will fall on historic resources in the vicinity of the Project site. Although new shadow will be created by the Project, most impacts are during periods where surrounding properties and districts are already in shadow. As a result, shadow impacts on historic resources are anticipated to be minimal.

New shadow cast by the Project at the Spring and Autumnal Equinox is limited to rooftop shadow on Saint Cecilia's Church and the Fenway Theater at 9:00AM. Minor new shadow will occur on the rooftops in the Saint Botolph Street Area at 6:00PM, however, the area is already largely in shadow. At 9:00AM on the Summer Solstice, new shadow is limited to shadow on the rooftops of buildings on the north side of Saint Germain Street, however, these shadows are fleeting and are gone by 12:00PM. New shadow is also cast on the ground and rooftops of buildings in the Saint Botolph Street Area and in the South End District at 6:00PM, however, most of these areas are already in shadow. During the Winter Solstice, new shadow is cast on the ground and rooftops of buildings in the Back Bay Historic District at 9:00AM when much of the District is already in shadow. By 12:00PM, the shadow is reduced to the rooftops of few buildings on Newbury Street between Fairfield and Gloucester Streets.

7.5 Consistency with State and Federal Regulatory Requirements

The Proposed Project is subject to State Register Review by the Massachusetts Historical Commission (MHC). A MHC Project Notification Form will be submitted to initiate the review. The proponent will coordinate review of the Project with the Boston Landmarks Commission.

Infrastructure

8.0 INFRASTRUCTURE

This chapter outlines the existing utilities surrounding the Project site, the proposed connections required to provide service to the Proposed Project, and any impacts on the existing utility systems that may result from the construction of the Project. Impacts to sewer, water supply, fire protection, electricity, natural gas, and telecommunications are also discussed.

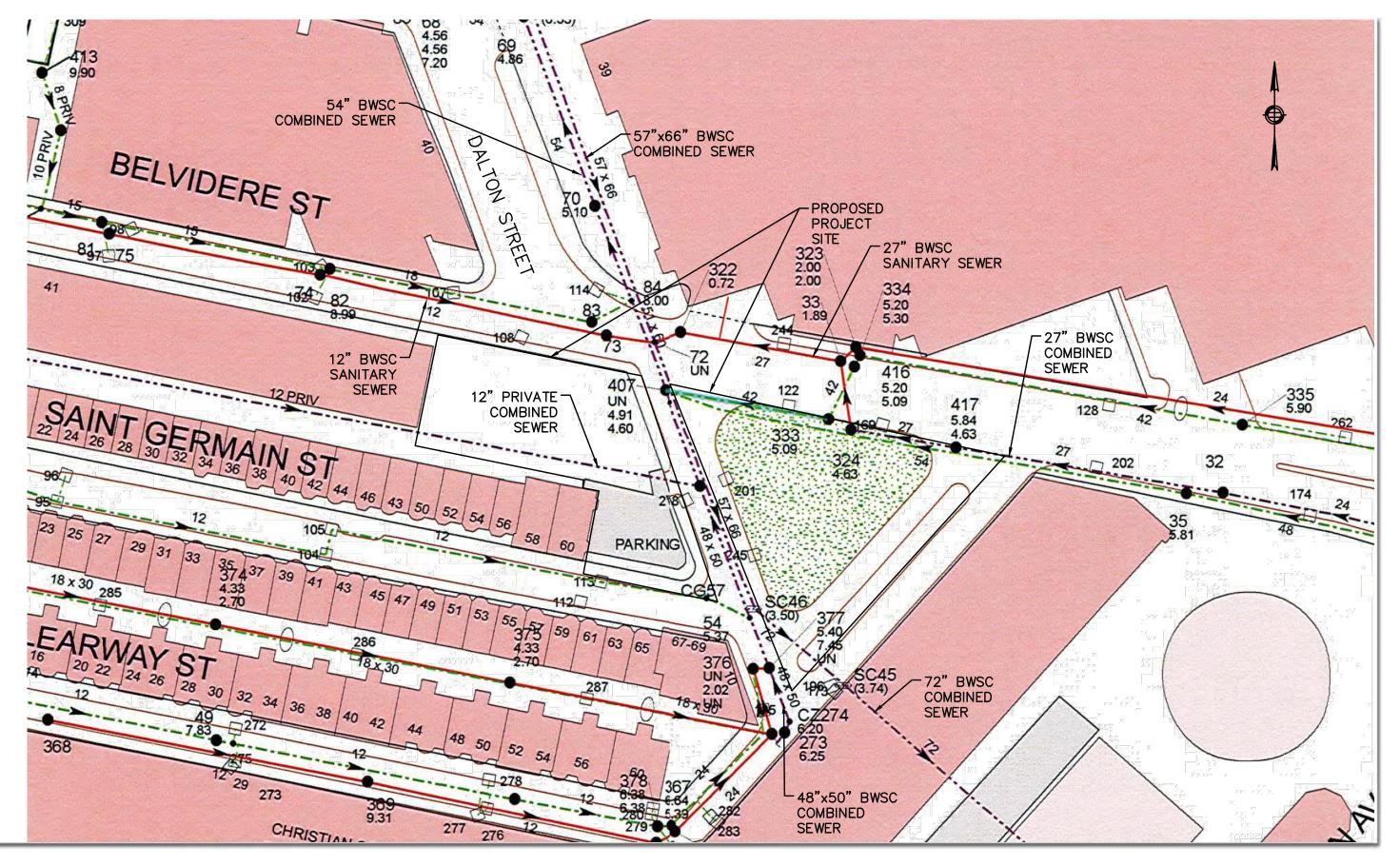
8.1 Wastewater

8.1.1 Existing Sewer System

There are existing Boston Water and Sewer Commission (BWSC) sanitary sewer mains located in Belvidere Street, Dalton Street and Saint Germain Street adjacent to the Project site. There are two BWSC combined sewers beneath Dalton Street. There is a 57-inch x 66-inch combined sewer that transitions into a 72-inch combined sewer and flows in a southerly direction, and a 48-inch x 50-inch which increases to a 51 inch x 60 inch and to a 54 inch diameter round line which flows in a northerly direction. There is a 12-inch BWSC sanitary sewer main beneath Belvidere Street west of Dalton Street. This sanitary sewer main flows into the 51-inch x 60-inch combined sewer beneath Dalton Street. In Belvidere Street east of Dalton Street, there is a 24-inch sanitary sewer beneath the northerly side of the street and a 27-inch combined sewer beneath the southerly side of the Street. Both of these sewers flow into a 27-inch sanitary sewer which flows into the 51-inch x 60-inch combined sewer beneath Dalton Street. There is a 12-inch private combined sewer which runs beneath the alley between Belvidere Street and Saint Germain Street, passing through the Project site and connecting to the 48-inch x 50-inch combined sewer beneath Dalton Street.

The BWSC combined sewer flowing in a southerly direction flows through private property, down Saint Stephen's Street and to the Boston Main Interceptor beneath Gainsborough Street. The Boston Main Interceptor ultimately flows to the MWRA Deer Island Waste Water Treatment Plan for treatment and disposal. The BWSC combined sewer which flows in the northerly direction flows up Dalton Street and Hereford Street. At the intersection of Hereford Street and Beacon Street, the main is directed either into the combined sewer which flows in a southerly direction described above, or, during times of high flow, to a Combined Sewer Overflow that directs flow into the Charles River.

There are currently no sewer services at the Project site. The existing sewer system is illustrated in Figure 8-1.





8.1.2 Project-Generated Sanitary Sewer Flow

The Project's sewage generation rates were estimated using the Massachusetts Division of Water Pollution Control Sewer System Extension and Connection Permit Program at 314 CMR 07.00. 314 CMR 07.00 lists typical generation values for the sources listed in Table 8-1 for the High-rise building, and Table 8-2 for the Mid-rise building. Typical generation values are generally conservative values for estimating the sewage flows from new construction. 314 CMR 07.00 sewage generation values are used to evaluate new sewage flows or the increase in flows to existing connections. Tables 8-1 and 8-2 describe the increased sewage generation due to the Proposed Project.

Table 8-1 Projected Sanitary Sewer Flows: High-rise

Use	Program	Generation Rate	Total Flow (GPD)
Residential	425 bedrooms	110 gpd/ bedroom	46,750
Hotel	250 rooms	110 gpd/ room	27,500
Food Service	320 seats	35 gpd/ room	11,200
o Restaurant	140 seats		
o Cafe	85 seats		
o Breakfast Room	95 seats		
Meeting Rooms	310 seats	3 gpd/ seat	930
Function Areas	225 seats	15 gpd/ seat	3,375
Ballroom	140 seats		
Junior Ballroom	85 seats		
Building Amenities			
o Pool	30 people	10 gpd/ person	300
o Spa	3,021 sf	100 gpd/ 1,000 sf	302
o Fitness Center	2,452 sf	100 gpd/ 1,000 sf	245
Proposed Sewer Flows			90,602

Table 8-2 Projected Sanitary Sewer Flow: Mid-rise

Use	Program	Generation Rate	Total Flow (GPD)
Residential	285 bedrooms	110 gpd/ bedroom	31,350
Retail Space	1,800 sf	50 gpd/ 100 sf	90
Proposed Sewer Flows			31,440

The Project's impact to the existing BWSC systems in Belvidere Street and Dalton Street was analyzed. The existing sewer system capacity calculations are presented in Table 8-3.

Table 8-3 Sewer Hydraulic Capacity Analysis

Manhole	Distance	Invert	Invert	Slope	Diameter	Manning's	Flow	Flow
(BWSC	(feet)	Elevation	Elevation	(%)	(inches)	Number	Capacity	Capacity
Number)		(up)	(down)				(cfs)	(MGD)
417 to 324	72	4.73	4.63	0.1%	27	0.013	11.54	7.46
325 to 33	47	4.63	1.89	5.8%	27	0.013	74.78	48.33
323 to 33	15	5.20	2.00	21.3%	24	0.013	104.49	67.53
33 to 322	113	1.89	0.72	1.0%	27	0.013	31.51	20.37
64 to SC46	464	6.53	3.50	0.7%	57x66	0.013	183.56	118.64

Note: 1. Manhole numbers taken from BWSC Sewer System Map no. 221

8.1.3 Sanitary Sewer Connection

The sewer services for the mid-rise building are proposed to tie into the 12-inch sewer main located in Belvidere Street. The sewer services for the high-rise building are expected to tie into either the 27-inch sanitary sewer in Belvidere Street or the 57-inch x 66-inch combined sewer in Dalton Street.

The adjacent roadway sewer system in Belvidere Street and Dalton Street and potential building service connection to the sewer system was analyzed.

Results shown in Table 8-3 indicate the hydraulic capacity of the 27-inch sanitary sewer system within Belvidere Street and the 57-inch x 66-inch combined sewer system within Dalton Street near the Proposed Project. The minimum hydraulic capacity is 7.46 million gallons per day (MGD) or 11.54 cfs for the 27-inch system in Belvidere Street, and 118.64 MGD or 183.56 cfs for the 57-inch x 66-inch system in Dalton Street. Based on an average daily flow estimate for the Proposed Project of 117,264 GPD or 0.12 MGD; and with a factor of safety of 10 (total estimate = $0.12 \text{ MGD} \times 10 = 1.2 \text{ MGD}$), no capacity problems are expected within either the Belvidere Street or Dalton Street systems.

The Proponent will coordinate with the BWSC on the design and capacity of the proposed connections to the sewer system. The High-rise is expected to generate approximately 90,000 gallons per day, and the Mid-rise is expected to generate approximately 31,000 gallons per day. Because the net sanitary flow for the High-rise is greater than 50,000 gpd, a MassDEP Sewer Connection Permit will be required. MassDEP is currently in the process of eliminating their sewer connection permit program, and depending on the timing, the Project may not be required to submit to MassDEP, in which case approval for the net sanitary flow will come from BWSC.

^{2.} Flow Calculations based on Manning Equation

^{3.} All pipes assumed to be vitrified clay, to be conservative

^{4.} A conservative slope of 0.1% was assumed for Manhole 471 to 325.

All improvements and connections to BWSC infrastructure will be reviewed as part of the BWSC's site plan review process for the Project. This process includes a comprehensive design review of the proposed service connections, an assessment of project demands and system capacity, and the establishment of service accounts.

The Proponent will also coordinate with the BWSC and the MWRA regarding the need to potentially offset the Project's increased wastewater flows via inflow/infiltration (I/I) removal. If required, any net increase in flows will be mitigated in compliance with applicable policies and regulations.

8.2 Water System

8.2.1 Existing Water Service

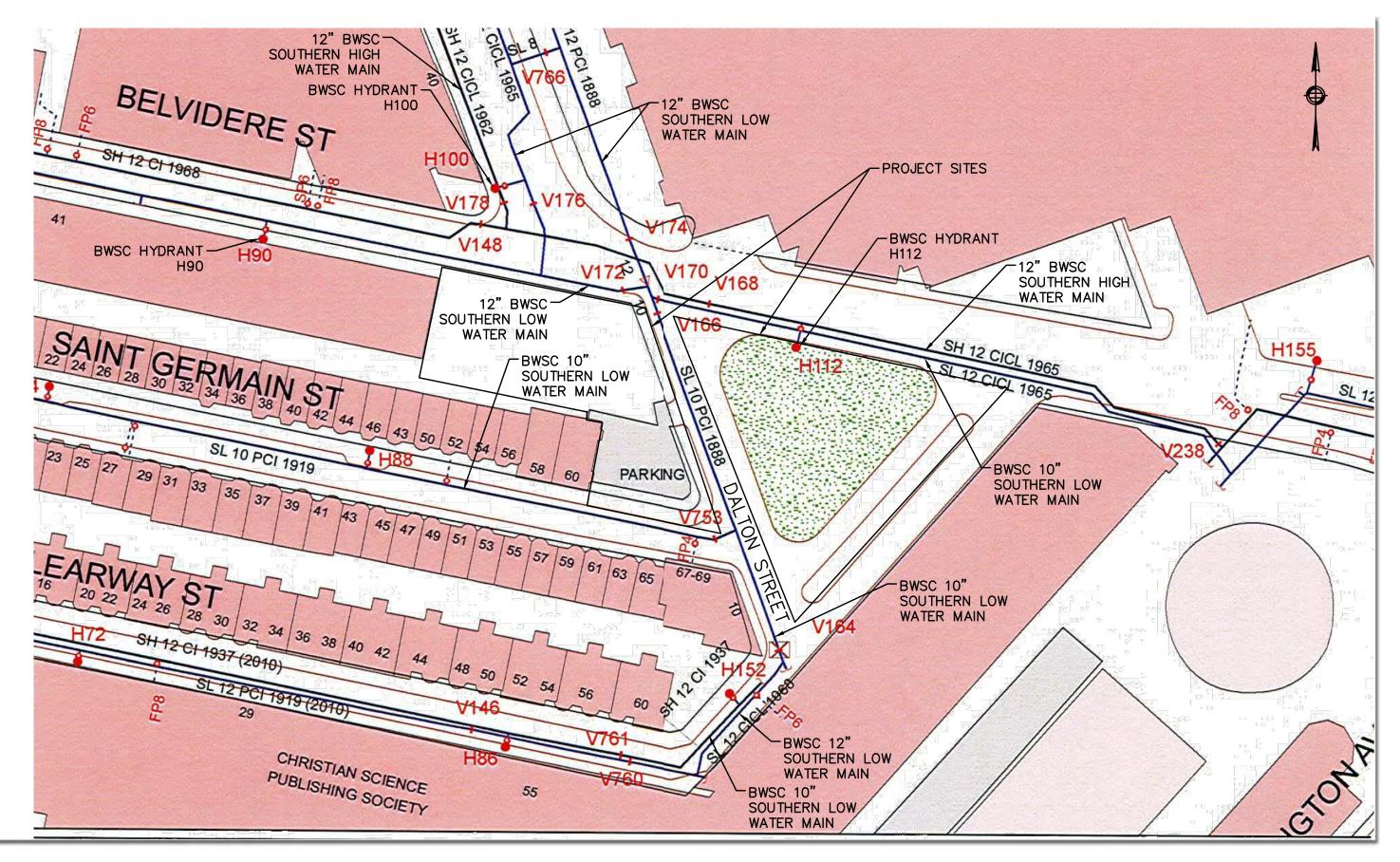
The water mains in the vicinity of the Project site are predominantly owned and maintained by the BWSC. There are five different water systems within the city, and these provide service to portions of the city based on ground surface elevation. The five systems are southern low (commonly known as low service), southern high (commonly known as high service), southern extra high, northern low, and northern high. There is a 12-inch BWSC Southern High main and a 12-inch Southern Low main beneath Belvidere Street, a 10-inch Southern Low main beneath Saint Germain Street. The existing water system is illustrated in Figure 8-2.

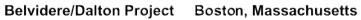
There are currently no domestic or fire services to the Project site.

8.2.2 Anticipated Water Consumption

The Project's water demand estimate for domestic services is based on the Project's estimated sewage generation, described above. A conservative factor of 1.1 (10%) is applied to the estimated average daily wastewater flows calculated with 314 CMR 07.00 values to account for consumption, system losses and other usages to estimate an average daily water demand. The Project, which is being built on an existing parking lot and an undeveloped parcel, will require approximately 122,042 gpd of domestic water. The water for the Project will be supplied by the BWSC system.

All new water services will be installed in accordance with the latest Local, State, and Federal codes and standards. Backflow preventers will be installed at both domestic and fire protection service connections. New meters will be installed with Meter Transmitter Units (MTU's) as part of the Boston Water and Sewer Commission's Automatic Meter Reading (AMR) system.





8.2.3 Proposed Water Service

BWSC record flow test data containing actual flow and pressure for a hydrant within the vicinity of the Project site was available. Additional testing has been requested, as hydrant flow data should be less than a year old to be used as a design tool. The results of the BWSC testing near the Proposed Project site are indicated in Table 8-4.

Table 8-4 Existing Hydrant Flow Data

Flow Hydrant	Date of	Static	Residual	Total Flow	Flow (gpm)	Flow (gpm)
Number	Test	Pressure (psi)	Pressure (psi)	(gpm)	at 20 psi	at 10 psi
H152 12-inch	10/29/2008	108	80	2,456	4,558	4,831
Southern High						

The domestic and fire services for the Mid-rise building are proposed to connect to the 12-inch Southern High service in Belvidere Street west of Dalton Street. The domestic and fire services for the High-rise building will connect to the 12-inch Southern High in Belvidere Street east of Dalton Street.

The domestic and fire protection water service connections required by the Project will meet the applicable City and State codes and standards, including cross-connection backflow prevention. Compliance with the standards for the domestic water system service connection will be reviewed as part of BWSC's Site Plan Review Process. This review includes, but is not limited to, sizing of domestic water and fire protection services, calculation of meter sizing, backflow prevention design, and location of hydrants and siamese connections that conform to BWSC and Boston Fire Department requirements.

8.2.4 Water Supply Conservation and Mitigation Measures

All efforts to reduce water consumption will be made. Aeration fixtures and appliances will be chosen for water conservation qualities. In public areas, sensor operated faucets and toilets will be installed.

The State Building Code requires the use of water-conserving fixtures. Water conservation measures such as low-flow toilets and restricted flow faucets will help reduce the domestic water demand on the existing distribution system. The installation of sensor-operated sinks with water conserving aerators and sensor-operated toilets in all restrooms will be incorporated into the design plans for the Proposed Project.

8.3 Electrical Service

Electrical service for the Project will be provided by NStar. Utility owned switchgear and substation transformers will be installed for each building with underground primary and secondary cables feeding the proposed buildings. Switchgear and substation transformers will be located in electrical rooms within each building. Capacity issues are not anticipated for this project.

8.4 Natural Gas

The Project site is served by low pressure natural gas mains owned by National Grid. Both proposed buildings will have individual services that will provide energy to the building heating, cooling and water heating units. These units will be high efficiency Energy Star compliant units and will be designed to function in accordance with the LEED design criteria.

8.5 Telecommunications Systems

During the final design of the Project, the applicant will work with Verizon to determine the proper sizing and number of pairs for the conduit and cables for each building. As with other utilities, capacity is not anticipated to be an issue.

Cable television and internet services are provided by Comcast in the Project area. Each building will have service connections to these lines that will be designed by the applicant in consultation with Comcast.

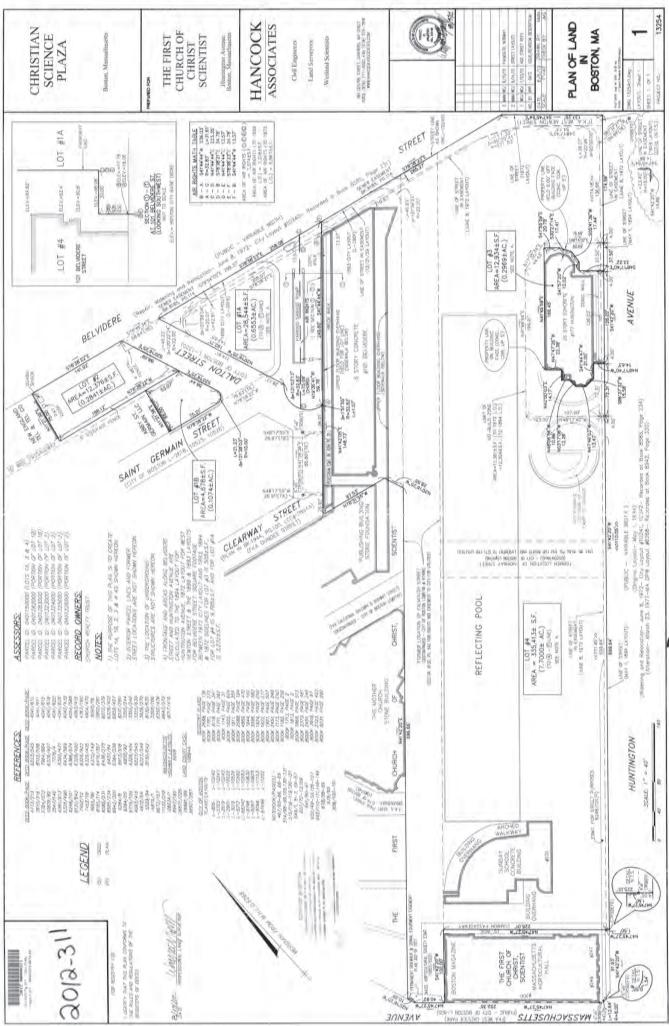
8.6 Utility Protection During Construction

Existing public and private infrastructure located within nearby public rights-of-way will be protected during construction. The installation of proposed utility connections within public ways will be undertaken in accordance with BWSC, the Boston Public Works Department, the Dig-Safe Program, and applicable utility company requirements. Specific methods for constructing proposed utilities where they are near to, or connect with, existing water, sewer, and drain facilities will be reviewed by the BWSC as part of its Site Plan Review process. All necessary permits will be obtained before the commencement of work.

The Proponent will continue to work and coordinate with the BWSC and the utility companies to ensure safe and coordinated utility operations in connection with the Proposed Project.

Appendix A

Subdivision Plan



2012-311

Appendix B

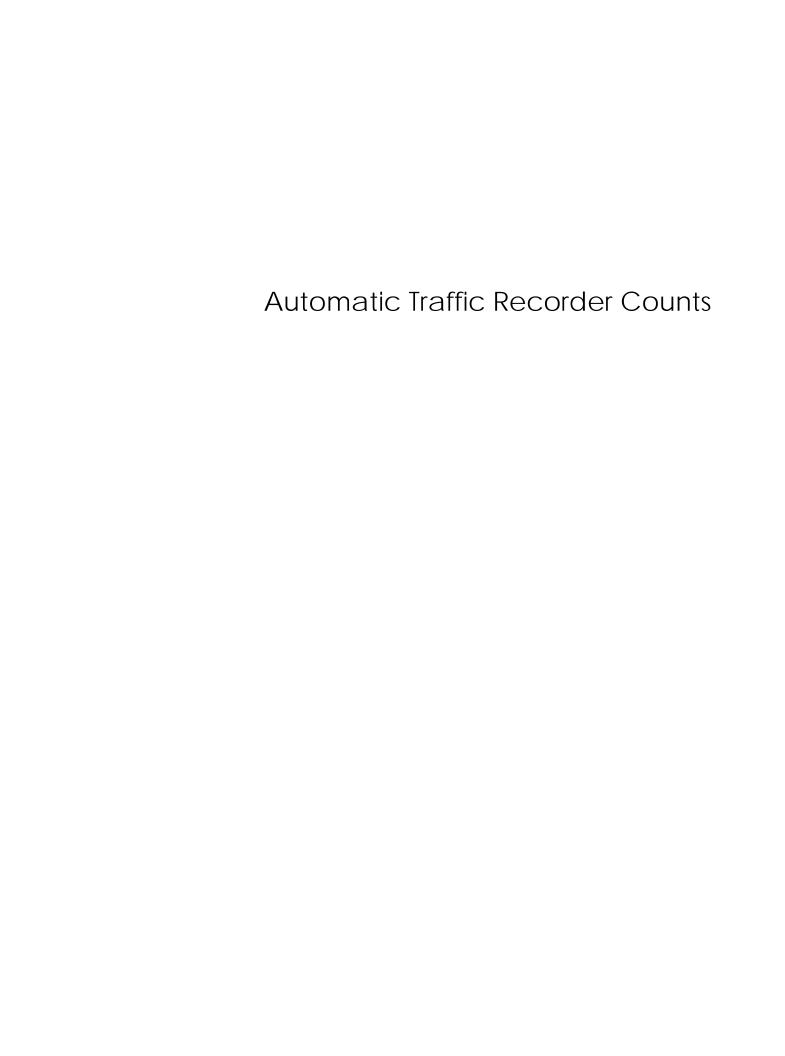
Transportation Appendix

APPENDIX

Transportation

Automatic Traffic Recorder Counts Turning Movement Counts

2013 Existing Condition Synchro Reports 2018 No-Build Condition Synchro Reports 2018 Build Condition Synchro Reports





Massachusetts Avenue south of Clearway Street City, State: Boston, MA Client: VHB/ M. Houdlette

P.O. Box 301 Berlin, MA 01503 Office: 508.481.3999 Fax: 508.545.1234

133307 A Class Site Code: TBA

NB							01 Berlin, MA (1.3999 Fax: 508						Sile Ci	ode: TBA
Start				Heavy			requests@pdil							
Time	Bicylce	Cars	Buses	Vehicle	Total									
05/14/1	Dicylec	Odio	Duscs	VCITICIC	Total									
3	5	129	7	6	0	0	0	0	0	0	0	0	0	147
01:00	0	91	3	1	0	0	0	Ö	0	Ö	0	0	0	95
02:00	2	51	4	0	Ö	Ö	Ö	Ö	Ö	Ö	Ö	Ö	Ö	57
03:00	0	33	10	0	0	0	0	0	0	0	0	0	0	43
04:00	1	58	9	0	0	0	0	0	0	0	0	0	0	68
05:00	8	208	29	9	0	0	0	0	0	0	0	0	0	254
06:00	20	412	62	23	0	0	0	0	0	0	0	0	0	517
07:00	23	554	83	20	0	0	0	0	0	0	0	0	0	680
08:00	91	594	49	19	0	0	0	0	0	0	0	0	0	753
09:00	53	482	49	17	0	0	0	0	0	0	0	0	0	601
10:00	35	430	56	13	0	0	0	0	0	0	0	0	0	534
11:00	23	497	53	9	0	0	0	0	0	0	0	0	0	582
12 PM	23	465	47	9	0	0	0	0	0	0	0	0	0	544
13:00	28	475	39	22	0	0	0	0	0	0	0	0	0	564
14:00	38	487	33	17	0	0	0	0	0	0	0	0	0	575
15:00	46	570	14	16	0	0	0	0	0	0	0	0	0	646
16:00	52	537	29	16	0	0	0	0	0	0	0	0	0	634
17:00	83	648	12	24	0	0	0	0	0	0	0	0	0	767
18:00	77	529	5	15	0	0	0	0	0	0	0	0	0	626
19:00	48	428	8	14	0	0	0	0	0	0	0	0	0	498
20:00	42	396	9	13	0	0	0	0	0	0	0	0	0	460
21:00	20	356	9	7	0	0	0	0	0	0	0	0	0	392
22:00	16	404	12	8	0	0	0	0	0	0	0	0	0	440
23:00	12 746	240 9074	639	<u>5</u> 283	0 0	0	0	0	0	0	0	0	0	265 10742
Total Percent	6.9%	9074 84.5%	5.9%	283 2.6%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	10/42
AM			5.9%		0.0%	0.0%	0.070	0.0%	0.076	0.076	0.076	0.0%	0.070	
Peak	08:00	08:00	07:00	06:00										08:00
Vol.	91	594	83	23										753
Midday							,							
Peak	14:00	11:00	11:00	13:00										11:00
Vol.	38	497	53	22										582
PM		17:00												
Peak	17:00	17:00	16:00	17:00										17:00
Vol.	83	648	29	24										767



Massachusetts Avenue south of Clearway Street City, State: Boston, MA Client: VHB/ M. Houdlette

P.O. Box 301 Berlin, MA 01503 Office: 508.481.3999 Fax: 508.545.1234

133307 A Class Site Code: TBA

SB							01 Berlin, MA (1.3999 Fax: 508						Site C	oue: TBA
Start				Heavy			requests@pdill							
Time	Bicylce	Cars	Buses	Vehicle	Total									
05/14/1	Dioyioc	Ouio	Duoco	VCITICIC	Total									
3	10	211	5	6	0	0	0	0	0	0	0	0	0	232
01:00	4	174	4	2	0	0	0	0	0	0	0	Ö	Ö	184
02:00	4	79	2	3	0	0	0	0	Ō	Ō	Ō	Ö	Ö	88
03:00	0	46	4	0	0	0	0	0	0	0	0	0	0	50
04:00	1	45	8	0	0	0	0	0	0	0	0	0	0	54
05:00	1	105	14	7	0	0	0	0	0	0	0	0	0	127
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07:00	46	476	41	13	0	0	0	0	0	0	0	0	0	576
08:00	93	530	52	16	0	0	0	0	0	0	0	0	0	691
09:00	87	518	59	23	0	0	0	0	0	0	0	0	0	687
10:00	35	469	59	15	0	0	0	0	0	0	0	0	0	578
11:00	40	483	60	10	0	0	0	0	0	0	0	0	0	593
12 PM	22	520	55	6	0	0	0	0	0	0	0	0	0	603
13:00	23	580	56	7	0	0	0	0	0	0	0	0	0	666
14:00	21	647	45	11	0	0	0	0	0	0	0	0	0	724
15:00	43	619	35	10	0	0	0	0	0	0	0	0	0	707
16:00	58	653	17	10	0	0	0	0	0	0	0	0	0	738
17:00	114	612	16	14	0	0	0	0	0	0	0	0	0	756
18:00	79	564	10	16	0	0	0	0	0	0	0	0	0	669
19:00	62	562	14	25	0	0	0	0	0	0	0	0	0	663
20:00	35	510	6	10	0	0	0	0	0	0	0	0	0	561
21:00	39	598	9	8	0	0	0	0	0	0	0	0	0	654
22:00	21	469	8	5	0	0	0	0	0	0	0	0	0	503
23:00	11	375	8	6	0	0	0	0	0	0	0	0	0	400
Total	865	10154	611	231	0	0	0	0	0	0	0	0	0	11861
Percent	7.3%	85.6%	5.2%	1.9%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	
AM	08:00	08:00	09:00	09:00										08:00
Peak														
Vol.	93	530	59	23										691
Midday Peak	11:00	14:00	11:00	14:00										14:00
Vol.	40	647	60	11										724
PM	17:00	16:00	15:00	19:00										
Peak	17.00	10.00	15.00	19.00										17:00
Vol.	114	653	35	25										756

Massachusetts Avenue south of Clearway Street City, State: Boston, MA Client: VHB/ M. Houdlette



P.O. Box 301 Berlin, MA 01503 Office: 508.481.3999 Fax: 508.545.1234 Email: datarequests@pdillc.com 133307 A Volume Site Code: TBA

							arequests@pdil	ic.com		Comb	nin		14-May-	
Start		NB				SB				ed			13	
Time	A.M.		P.M.		A.M.		P.M.		A.M.		P.M.		Tue	
12:00	40		143		77		158		117		301			
12:15	41		129		58 50		160		99		289			
12:30	38	4.47	131	E 4.4	59	222	142	602	97	270	273	4447		
12:45 01:00	28	147	141	544	38	232	143	603	66	379	284	1147		
01:00	39 20		128 152		63 50		166 170		102 70		294 322			
01:13	18		146		43		168		61		314			
01:45	18	95	138	564	28	184	162	666	46	279	300	1230		
02:00	15	90	123	304	27	104	154	000	42	219	277	1230		
02:15	19		150		24		172		43		322			
02:30	14		168		17		205		31		373			
02:45	9	57	134	575	20	88	193	724	29	145	327	1299		
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03:15	9		164		11		171		20		335			
03:30	10		167		13		174		23		341			
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04:00	13		142	0.0	14		176		27		318			
04:15	10		161		13		171		23		332			
04:30	23		172		12		193		35		365			
04:45	22	68	159	634	15	54	198	738	37	122	357	1372		
05:00	29		196		14		190		43		386			
05:15	57		183		37		199		94		382			
05:30	78		196		41		192		119		388			
05:45	90	254	192	767	35	127	175	756	125	381	367	1523		
06:00	108		161		63		181		171		342			
06:15	111		152		93		150		204		302			
06:30	147		160		99		166		246		326			
06:45	151	517	153	626	102	357	172	669	253	874	325	1295		
07:00	161		134		129		167		290		301			
07:15	165		122		127		189		292		311			
07:30	173		125		165		172		338		297			
07:45	181	680	117	498	155	576	135	663	336	1256	252	1161		
08:00	183		111		158		149		341		260			
08:15	174		119		155		141		329		260			
08:30	207		108		182		150		389		258			
08:45	189	753	122	460	196	691	121	561	385	1444	243	1021		
09:00	136		102		179		155		315		257			
09:15	151		95		168		158		319		253			
09:30	174		108		164		194		338		302			
09:45	140	601	87	392	176	687	147	654	316	1288	234	1046		
10:00	134		116		157		137		291		253			
10:15	120		121		142		130		262		251			
10:30	151	F0.4	105	4.40	138	F70	129	500	289	4440	234	0.40		
10:45	129	534	98	440	141	578	107	503	270	1112	205	943		
11:00	149		64		157		113		306		177			
11:15	132		64		145		105		277		169			
11:30	158	E00	81 50	205	139	500	100	400	297	4475	181	CCE		
11:45 Total	143	582	<u>56</u> 6411	265	152 4217	593	82 7644	400	295	1175	138	665		
Percent	4331 50.7%		45.6%		4217		7644 54.4%		8548		14055			
Day Total		107				118				226	03			
Peak	08:00	-	05:00	-	08:30	-	04:30	-	08:00	-	05:00	-	-	-
Vol.	753	-	767	-	725	-	780	-	1444	-	1523	-	-	-
P.H.F.	0.909		0.978		0.925		0.980		0.928		0.981			



Huntington Avenue (Route 9) west of Belvidere Street City, State: Boston, MA Client: VHB/ M. Houdlette

P.O. Box 301 Berlin, MA 01503 Office: 508.481.3999 Fax: 508.545.1234

133307 B Class Site Code: TBA

WB						P.O. Box 30 Office: 508.481	1 Berlin, MA (Site Co	ode: TBA
Start				Heavy			requests@pdill							
Time	Bicylce	Cars	Buses	Vehicle	Total									
05/14/1	Dicyloc	Odis	Duscs	VCITICIC	Total							-		
3	2	96	6	3	0	0	0	0	0	0	0	0	0	107
01:00	1	84	2	2	0	Ő	0	Ö	Ö	0	0	Ö	0	89
02:00	1	55	0	7	0	Ő	0	Ö	0	0	0	0	0	63
03:00	0	23	0	0	0	0	0	Ö	0	0	0	0	0	23
04:00	1	21	0	11	0	0	0	Ö	Ö	0	Ö	Ö	0	33
05:00	2	100	10	20	0	0	0	0	0	0	0	0	0	132
06:00	3	363	19	38	0	0	0	0	0	0	0	0	0	423
07:00	4	575	15	27	0	0	0	0	0	0	0	0	0	621
08:00	9	667	23	26	0	0	0	0	0	0	0	0	0	725
09:00	7	659	24	30	0	0	0	0	0	0	0	0	0	720
10:00	5	523	23	25	0	0	0	0	0	0	0	0	0	576
11:00	3	495	18	23	0	0	0	0	0	0	0	0	0	539
12 PM	11	484	19	30	0	0	0	0	0	0	0	0	0	544
13:00	4	498	21	17	0	0	0	0	0	0	0	0	0	540
14:00	9	501	34	12	0	0	0	0	0	0	0	0	0	556
15:00	5	498	26	8	0	0	0	0	0	0	0	0	0	537
16:00	15	569	25	8	0	0	0	0	0	0	0	0	0	617
17:00	22	635	23	9	0	0	0	0	0	0	0	0	0	689
18:00	18	607	18	4	0	0	0	0	0	0	0	0	0	647
19:00	11	474	19	3	0	0	0	0	0	0	0	0	0	507
20:00	3	365	10	0	0	0	0	0	0	0	0	0	0	378
21:00	3	347	12	4	0	0	0	0	0	0	0	0	0	366
22:00	8	291	5	2	0	0	0	0	0	0	0	0	0	306
23:00	0	158	6	2	0	0	0	0	0	0	0	0	0	166
Total	147	9088	358	311	0	0	0	0	0	0	0	0	0	9904
Percent	1.5%	91.8%	3.6%	3.1%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	
AM	08:00	08:00	09:00	06:00										08:00
Peak		007												
Vol.	9	667	24	38										725
Midday	12:00	14:00	14:00	12:00										14:00
Peak	11	501	24	20										EEC
Vol. PM			34	30										556
Peak	17:00	17:00	15:00	17:00										17:00
Vol.	22	635	26	9										689



Huntington Avenue (Route 9) west of Belvidere Street City, State: Boston, MA Client: VHB/ M. Houdlette

P.O. Box 301 Berlin, MA 01503 Office: 508.481.3999 Fax: 508.545.1234

133307 B Class Site Code: TBA

EB							01 Berlin, MA (1.3999 Fax: 508						Site Co	ode: TBA
Start				Heavy			requests@pdill							
Time	Bicylce	Cars	Buses	Vehicle	Total									
05/14/1	Dicylec	Odio	Duscs	VCITICIC	Total							-		
3	0	105	7	1	0	0	0	0	0	0	0	0	0	113
01:00	0	66	0	1	0	0	0	0	0	0	0	0	0	67
02:00	0	49	0	7	0	0	0	0	0	0	Õ	0	0	56
03:00	0	31	0	4	0	0	0	Ö	0	0	0	0	Ö	35
04:00	0	55	1	10	0	0	0	Ö	0	0	0	0	Ö	66
05:00	3	115	8	8	Ö	Ö	Ö	Ö	Ö	Ö	Ö	Ö	Ö	134
06:00	1	253	13	17	0	0	0	0	0	0	0	0	0	284
07:00	4	469	19	14	0	0	0	0	0	0	0	0	0	506
08:00	14	534	17	26	0	0	0	0	0	0	0	0	0	591
09:00	14	497	26	22	0	0	0	0	0	0	0	0	0	559
10:00	6	423	23	27	0	0	0	0	0	0	0	0	0	479
11:00	14	437	23	22	0	0	0	0	0	0	0	0	0	496
12 PM	0	436	24	24	0	0	0	0	0	0	0	0	0	484
13:00	7	469	25	16	0	0	0	0	0	0	0	0	0	517
14:00	9	460	18	14	0	0	0	0	0	0	0	0	0	501
15:00	12	541	19	9	0	0	0	0	0	0	0	0	0	581
16:00	15	558	18	16	0	0	0	0	0	0	0	0	0	607
17:00	9	646	25	6	0	0	0	0	0	0	0	0	0	686
18:00	15	490	15	6	0	0	0	0	0	0	0	0	0	526
19:00	9	394	13	0	0	0	0	0	0	0	0	0	0	416
20:00	3	350	12	6	0	0	0	0	0	0	0	0	0	371
21:00	6	298	9	1	0	0	0	0	0	0	0	0	0	314
22:00	0	285	9	4	0	0	0	0	0	0	0	0	0	298
23:00	0	156	5	0	0	0	0	0	0	0	0	0	0	161
Total	141	8117	329	261	0	0	0	0	0	0	0	0	0	8848
Percent	1.6%	91.7%	3.7%	2.9%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	
AM Peak	08:00	08:00	09:00	08:00										08:00
Vol.	14	534	26	26										591
Midday Peak	11:00	13:00	13:00	12:00										13:00
Vol.	14	469	25	24										517
PM	16:00	17:00	17:00	16:00									-	17:00
Peak Vol.	15	646	25	16										686

Huntington Avenue (Route 9) west of Belvidere Street City, State: Boston, MA Client: VHB/ M. Houdlette



P.O. Box 301 Berlin, MA 01503 Office: 508.481.3999 Fax: 508.545.1234 Email: datarequests@pdillc.com 133307 B Volume Site Code: TBA

							arequests@pdill	c.com		Comb	in		14-May-	
Start		WB				EB				ed			13	
Time	A.M.		P.M.		A.M.		P.M.		A.M.		P.M.		Tue	
12:00	28		134		37		136		65 50		270			
12:15 12:30	28 24		134 142		30 27		99 126		58 51		233 268			
12:45	2 4 27	107	134	544	19	113	123	484	46	220	257	1028		
01:00	21 24	107	128	344	16	113	142	404	40	220	257 270	1020		
01:15	17		141		20		135		37		276			
01:30	26		130		19		124		45		254			
01:45	22	89	141	540	12	67	116	517	34	156	257	1057		
02:00	14	09	126	340	15	07	122	317	29	130	248	1037		
02:15	15		140		15		114		30		254			
02:13	20		144		15		128		35		272			
02:45	14	63	146	556	11	56	137	501	25	119	283	1057		
03:00	5	00	141	000	8	00	133	001	13	110	274	1001		
03:15	8		137		9		144		17		281			
03:30	6		134		10		164		16		298			
03:45	4	23	125	537	8	35	140	581	12	58	265	1118		
04:00	7		136	•	15		145		22		281			
04:15	10		159		11		193		21		352			
04:30	8		157		20		117		28		274			
04:45	8	33	165	617	20	66	152	607	28	99	317	1224		
05:00	14		156		12		172		26		328			
05:15	30		182		38		176		68		358			
05:30	33		179		45		158		78		337			
05:45	55	132	172	689	39	134	180	686	94	266	352	1375		
06:00	62		163		49		153		111		316			
06:15	98		149		53		126		151		275			
06:30	138		179		90		131		228		310			
06:45	125	423	156	647	92	284	116	526	217	707	272	1173		
07:00	117		140		112		119		229		259			
07:15	164		133		105		115		269		248			
07:30	151		113		141		99		292		212			
07:45	189	621	121	507	148	506	83	416	337	1127	204	923		
08:00	177		105		152		117		329		222			
08:15	183		99		125		88		308		187			
08:30	179		89		135		87		314		176			
08:45	186	725	85	378	179	591	79	371	365	1316	164	749		
09:00	167		99		147		82		314		181			
09:15	193		89		144		80		337		169			
09:30	177		93		141		68		318		161			
09:45	183	720	85	366	127	559	84	314	310	1279	169	680		
10:00	160		108		118		68		278		176			
10:15	140		90		112		98		252		188			
10:30	144		53		122		66		266		119			
10:45	132	576	55	306	127	479	66	298	259	1055	121	604		
11:00	136		51		114		41		250		92			
11:15	113		41		130		46		243		87			
11:30	155	_	45		113		40		268		85			
11:45	135	539	29	166	139	496	34	161	274	1035	63	327		
Total	4051		5853		3386		5462		7437		11315			
Percent	54.5%		51.7%		45.5%		48.3%							
Day Total		990)4			884	48			187	52			
Peak	07:45	-	05:15	-	08:45	-	05:00	-	08:45	-	05:00	-	-	-
Vol.	728	-	696	-	611	-	686	-	1334	-	1375	-	-	-
P.H.F.	0.963		0.956		0.853		0.953		0.914		0.960			



Belvidere Street north of Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

P.O. Box 301 Berlin, MA 01503 Office: 508.481.3999 Fax: 508.545.1234

133307 C Class Site Code: TBA

NB						P.O. Box 30 Office: 508.481	01 Berlin, MA (Site Co	ode: TBA
Start				Heavy			requests@pdll							
Time	Bicylce	Cars	Buses	Vehicle	Total									
05/14/1	Dicyicc	Odis	Duscs	VCITICIC	Total									
3	0	114	8	1	0	0	0	0	0	0	0	0	0	123
01:00	1	64	0	1	0	0	0	Ő	0	Ö	0	Ő	0	66
02:00	2	56	0	4	0	Ö	0	Ö	0	0	0	Ö	0	62
03:00	0	42	0	11	0	0	0	0	0	0	0	0	0	53
04:00	0	49	0	7	0	0	0	0	0	0	0	0	0	56
05:00	Ö	114	10	17	0	0	0	Ö	0	Ö	Ō	Ö	0	141
06:00	4	240	16	26	0	0	0	0	0	0	0	0	0	286
07:00	12	435	20	36	0	0	0	0	0	0	0	0	0	503
08:00	22	535	24	43	0	0	0	0	0	0	0	0	0	624
09:00	8	414	38	36	0	0	0	0	0	0	0	0	0	496
10:00	6	365	29	31	0	0	0	0	0	0	0	0	0	431
11:00	14	354	28	22	0	0	0	0	0	0	0	0	0	418
12 PM	15	340	28	27	0	0	0	0	0	0	0	0	0	410
13:00	8	365	27	29	0	0	0	0	0	0	0	0	0	429
14:00	9	346	29	14	0	0	0	0	0	0	0	0	0	398
15:00	13	365	31	11	0	0	0	0	0	0	0	0	0	420
16:00	12	435	28	11	0	0	0	0	0	0	0	0	0	486
17:00	46	544	26	5	0	0	0	0	0	0	0	0	0	621
18:00	31	545	26	6	0	0	0	0	0	0	0	0	0	608
19:00	19	401	18	1	0	0	0	0	0	0	0	0	0	439
20:00	7	357	14	2	0	0	0	0	0	0	0	0	0	380
21:00	5	291	10	1	0	0	0	0	0	0	0	0	0	307
22:00	8	238	7	3	0	0	0	0	0	0	0	0	0	256
23:00	3	177	5	1_	0	0	0	0	0	0	0	0	0	186
Total	245	7186	422	346	0	0	0	0	0	0	0	0	0	8199
Percent	3.0%	87.6%	5.1%	4.2%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	
AM Peak	08:00	08:00	09:00	08:00										08:00
Vol.	22	535	38	43										624
Midday Peak	12:00	13:00	14:00	13:00										13:00
Vol.	15	365	29	29										429
PM														
Peak	17:00	18:00	15:00	15:00										17:00
Vol.	46	545	31	11										621



Belvidere Street north of Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

P.O. Box 301 Berlin, MA 01503 Office: 508.481.3999 Fax: 508.545.1234

133307 C Class Site Code: TBA

SB							01 Berlin, MA (1.3999 Fax: 508						Site Co	ode: TBA
Start				Heavy			requests@pdll							
Time	Bicylce	Cars	Buses	Vehicle	Total									
05/14/1				7 0										
3	0	46	0	1	0	0	0	0	0	0	0	0	0	47
01:00	0	25	0	0	0	0	0	0	0	0	0	0	0	25
02:00	0	13	0	2	0	0	0	0	0	0	0	0	0	15
03:00	0	12	0	0	0	0	0	0	0	0	0	0	0	12
04:00	0	24	0	0	0	0	0	0	0	0	0	0	0	24
05:00	2	41	1	2	0	0	0	0	0	0	0	0	0	46
06:00	5	73	1	5	0	0	0	0	0	0	0	0	0	84
07:00	8	114	1	7	0	0	0	0	0	0	0	0	0	130
08:00	22	136	3	6	0	0	0	0	0	0	0	0	0	167
09:00	22	124	1	8	0	0	0	0	0	0	0	0	0	155
10:00	9	112	2	6	0	0	0	0	0	0	0	0	0	129
11:00	7	106	1	5	0	0	0	0	0	0	0	0	0	119
12 PM	5	136	1	2	0	0	0	0	0	0	0	0	0	144
13:00	9	145	0	1	0	0	0	0	0	0	0	0	0	155
14:00	1	137	2	5	0	0	0	0	0	0	0	0	0	145
15:00	4	154	2	5	0	0	0	0	0	0	0	0	0	165
16:00	11	179	1	4	0	0	0	0	0	0	0	0	0	195
17:00	10	237	1	2	0	0	0	0	0	0	0	0	0	250
18:00	7	204	1	0	0	0	0	0	0	0	0	0	0	212
19:00	7	164	0	1	0	0	0	0	0	0	0	0	0	172
20:00	5	113	2	0	0	0	0	0	0	0	0	0	0	120
21:00	3	129	1	0	0	0	0	0	0	0	0	0	0	133
22:00	4	139	2	1	0	0	0	0	0	0	0	0	0	146
23:00	1	80	0	0	0	0	0	0	0	0	0	0	0	81
Total	142	2643	23	63	0	0	0	0	0	0	0	0	0	2871
Percent	4.9%	92.1%	0.8%	2.2%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	
AM	08:00	08:00	08:00	09:00										08:00
Peak	00	400	0											
Vol.	22	136	3	8										167
Midday	13:00	13:00	14:00	11:00										13:00
Peak	0	115	2	_										155
Vol. PM	9	145	2	5										155
Pivi	16:00	17:00	15:00	15:00										17:00
Vol.	11	237	2	5										250

Belvidere Street north of Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette



P.O. Box 301 Berlin, MA 01503 Office: 508.481.3999 Fax: 508.545.1234 Email: datarequests@pdillc.com 133307 C Volume Site Code: TBA

						Email: data	arequests@pdill	c.com					44.1.	
Start		NB				SB				Comb ed	in		14-May- 13	
Time	A.M.		P.M.		A.M.		P.M.		A.M.		P.M.		Tue	
12:00	39		102		9		34		48		136			
12:15	34		109		17		33		51		142			
12:30	27		104		8		37		35		141			
12:45	23	123	95	410	13	47	40	144	36	170	135	554		
01:00	16		100		5 6		24		21		124			
01:15	16		125		6		42		22		167			
01:30	16		100		7		39		23		139			
01:45	18	66	104	429	7	25	50	155	25	91	154	584		
02:00	23		94		3		28		26		122			
02:15	19		104		4		34		23		138			
02:30	12		94		2		49		14		143			
02:45	8	62	106	398	6	15	34	145	14	77	140	543		
03:00	12		119		3		48		15		167			
03:15	12		91		4		45		16		136			
03:30	16		98		4		34		20		132			
03:45	13	53	112	420	1	12	38	165	14	65	150	585		
04:00	10	55	106	720	3	12	49	103	13	00	155	303		
04:00	14		125		10		49 44		24		169			
04:30	16	50	135	400	4	0.4	55	405	20	00	190	004		
04:45	16	56	120	486	7	24	47	195	23	80	167	681		
05:00	26		155		8		53		34		208			
05:15	31		144		7		69		38		213			
05:30	44		148		11		60		55		208			
05:45	40	141	174	621	20	46	68	250	60	187	242	871		
06:00	56		166		19		70		75		236			
06:15	57		152		18		49		75		201			
06:30	79		153		20		45		99		198			
06:45	94	286	137	608	27	84	48	212	121	370	185	820		
07:00	91		124		23		50		114		174			
07:15	108		110		30		42		138		152			
07:30	127		122		42		47		169		169			
07:45	177	503	83	439	35	130	33	172	212	633	116	611		
08:00	198		117		38		33		236		150			
08:15	148		87		50		28		198		115			
08:30	126		88		45		34		171		122			
08:45	152	624	88	380	34	167	25	120	186	791	113	500		
09:00	140	024	99	500	42	107	27	120	182	751	126	300		
09:00	118		63		42		32		160		95			
09:13	107		64		40		35		147		99			
09.30		496		307		155		133		651		440		
10:00	131	490	81 72	307	31	155	39 40	133	162 150	651	120	440		
10:00	109		73		41		49		150		122			
10:15	110		60		28		38		138		98			
10:30	103	404	59 64	050	35	400	32	440	138	E00	91	400		
10:45	109	431	64	256	25	129	27	146	134	560	91	402		
11:00	121		40		31		17		152		57			
11:15	98		66		37		26		135		92			
11:30	98		46		21	_	21		119	_	67			
11:45	101	418	34	186	30	119	17	81	131	537	51	267		
Total	3259		4940		953		1918		4212		6858			
Percent	77.4%		72.0%		22.6%		28.0%							
Day Total		819	99			287	71			110	70			
Peak	07:30	-	05:45	-	08:15	_	05:15	-	07:45	-	05:15	-	-	
Vol.	650	-	645	-	171	-	267	-	817	-	899	-	-	
P.H.F.	0.821		0.927		0.855		0.954		0.865		0.929			
г.п.г.	0.021		0.921		0.000		0.904		0.000		0.525			





File Name: 133307 A Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S: Massachusetts Avenue E/W: Boylston Street City, State: Boston, MA Client VHB/ M. Houdlette

File Name: 133307 A Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1



									0								
	Ma	Massachusetts Avenu From North	Avenue			Boylston Street From East	Street.		Ma	Massachusetts Avenu From South	Avenue			Boylston Street From West	Hasel		
Start Time	Right	Then	Left	U-Turn	Right	Then	Left U.	Tom	Right	Thru	Teff	U-Turn	Right	Thru	Left	U-Tum	Int. Total
7:00 AM	3	66	¥	0	19	18	2	0	19	118	-	0	26	72	3	-	415
7:15 AM	v	91	23	0	29	21	0	0	18	127	0	0	25	.59	4	0	400
30 AM	9	93	Z	0	40	17	0	0	11	131	2	0	28	3	2	0	458
7:45 AM	10	101	41	0	39	19	0	0	10	146	5	0	23	88	6	0	485
Total	24	384	132	0	121	75	2	0	88	225	66	0	102	313	10	-	1758
3:00 AM	7	92	32	0	8	23	-	0	15	142	2	0	28	100	4	0	522
3:15 AM	10	117	38	0	42	20	-	0	23	130	8	0	20	8	1	0	505
330 AM	00	124	35	0	26	20	0	0	1	166	1	0	28	68	4	0	508
8:45 AM	4	Ξ	75	0	39	13	0	0	13	110	2	0	35	110	2	0	473
Total	24	444	139	0	188	9/	7	0	27	548	10	0	111	392	17	0	2008
d Total	48	828	271	0	315	151	4	0	1115	1070	18	0	213	705	27	1	3766
pprch %	4.2	72.2	23.6	0	19	32.1	60	0	9.6	6.88	1.5	0	22.5	74.5	2.9	0.1	
Total %	1.3	22	7.2	0	8.4	4	0.1	0	3.1	28.4	0.5	0	5.7	18.7	0.7	0	

	los Total	485	522	505	808	2020		790
ī	Age Total	114	132	120	121	487		000
10 10	U-Tuen	0	0	0	0	0	0	000
ylston Str rom Wes	Left	m	4	1	4	18	3.7	643
Bo	Thru	88	100	93	68	370	26	500
	Right	23	28	20	28	66	20.3	884
	App Test	191	159	157	174	159		935
venue	U-Tum	0	0	0	0	0	0	000
rom Sout	Left	40	7	'n	-	13	2	059
Massach	Thu	146	142	130	166	584	7.68	880
	Night.	10	15	22	1	\$	8.3	614
1	Ago Total	28	105	63	46	272		648
×	U-Tuen	0	0	0	0	0	0	000
rom East	Len	0	-	-	0	2	0.7	200
Boy	Thru	61	23	20	20	82	30.1	801
	Right	39 39	8	42	26	188	1.69	680
i	1 of 1	7:45 A	126	165	167	610		013
- ADDR	U-Tun VM - Pesi	gins at (0	0	0	0	0	900
rom Nort	Left to 08:45/	tion Be	32	38	35	146	23.9	800
Massack	Thru 7:00 AM	Intersec 101	35	117	124	434	71.1	875
	Right is From 0	Entire 10	11	10	00	30	4.9	054
	Start Time Peak Hour Analysi	07:45 AM	08:00 AM	08:15 AM	08:30 AM	Total Volume	% Amp. Total	SHd

101	25	1117	124	434	71.1	. 875	
2	7	10	00	30	4.9	750	
TATE CHICAGO	08:00 AM	08:15 AM 10 117	08:30 AM	Total Volume	% App. Total	PHF	
		1	ht Total			0 128 550	25.4
	٢		Trees.			128	477
	l		an year			0	<
	Change	West	L-T			2	,
	Bardote	From	I mg			95	
	l	ŀ	T			28	
	ŀ		Tout R			681	45
			out Acc			0	
	No. Australia	South	LT U-T			40	
	9000	From	Pro			71	
	W		T			13 1	1 21
	ŀ	- 1	Trees.			9	
	l	Ħ	Area			0	
	Change	East	cf U-T			0	,
	Brudeton Steam	From	T MA			24	,
	l	Ì	T			41	**
	ŀ		Town R.	E E	SAM	89	30
			m Acc	Peak I o	at 07:4	0	
	to Assess	North	off Urro	MY SK	Begin	6	
	the conduction	From	7	AM to 08	section	9 4	
	Maso		ht The	on 67:00	ire Inter	0 10	0
	-	4	Ric	Iysis Fron	or Ent	-	
			Start Time	Peak Hour Ame	Peak Hour f	07:45 AM 10 109 49 0 168 41 24 0 0 65 13 171 5 0 189 28 95 5	A0.00

3766 89.6 33.5 10.1 2.4

20 1.5 0.5 90

337 000

128 128 127 127 1290

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

319 24.7 271 85 45 45 14.1

919 71.1 21.9 828 90.1 68 68 7.4 7.4 23

Grand Total Appreh % Total % Cars % Cars % Cars Heavy Vehicles % Heavy Vehicles % Buses % Buses

88.7 28.8 1070 103 103 34 2.8 34 2.8

\$64 \$51 \$31 \$31

		0	
		24	36
		4	
100	7:45 AM	168	120
	ns at 0	0	4
2000	tion Begi	46	36
WW 00.	Intersec	109	101
S Lumino	Entire	10	•
PORT TO SERVED	Peak Hour for	07:45 AM 10 109 49 0 168	A A 00.00

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					714						
101	107	93	402	74.6	939	370	92.0	25	6.2	7	1.7
			117								
170	171	190	720		746	.651	4.06	53	7.4	16	22
0	0	0	0	0	000	0	0	0	0	0	0
5	S	-	13	1.8	059	13	100	0	0	0	0
152	142	181	949	268	892	584	406	48	7.4	14	2.2
			19								
=	20	49	395		499	272	92.2	14	4.7	6	3.1
0	0	0	0	0	000	0	0	0	0	0	0
-	1	0	2	0.7	200	2	100	0	0	0	0
26	22	23	95	32.2	.913	82	86.3	9	6.3	7	7.4
3	47	26	198	67.1	.589	188	646	00	4.0	N	1.0
138	186	185	119		016	610	1.06	26	8.3	11	1.6
0	0	0	0	0	000	0	0	0	0	0	0
35	47	42	173	25.6	.883	146	84.4	25	14.5	"	1.2
101	128	134	472	2.69	.881	434	616	53	6.1	6	1.9
7	=	6	32	4.7	.727	30	93.8	7	6.3	0	0
08:00 AM	08:15 AM	08:30 AM	Total Volume	% App. Total	PHF	Cars	% Cars	Honry Vehicles	% Heavy Vehicles	Buses	% Buses



File Name: 133307 A Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S: Massachusetts Avenue E/W: Boylston Street City, State: Boston, MA Client VHB/ M. Houdlette



File Name: 133307 A Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

7	PRECISION	INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 01: Office-508.481,3999 Fax: 508.5

							Group	Grouns Printed- B	Supply Street								
	Ma	Massachusetts A venue From North	s A venue			Boylston Street From East	Street		Ma	Massachusetts Avenue From South	Avenue		1	Boylston Street From West	Street		
Start Time	Right	Thru	Left	U-Tum	Right	Then	Teff	U-Tom	Right	Thru	Left	U-Turn	Right	Thru	Left	U-Tum	Int. Total
07:00 AM	0	2	0	0	0	2	0	0	0	7	0	0	0	-	0	0	12
07:15 AM	0	m	0	0	-		0	0	0	4	0	0	0	7	0	0	11
07:30 AM	0	9	0	0	-	0	-	0	0	9	0	0	I	2	0	0	17
07:45 AM	0	-	-	0	0	2	0	0	-	3	0	0	1	2	0	0	11
Total	0	12	-	0	2	5	-	0	-	20	0	0	7	7	0	0	51
08:00 AM	0	m	0	0	0	2	0	0	0	4	0	0	-	-	0	0	11
08:15 AM	0	3	0	0	2	2	0	0	-	3	0	0	0	4	0	0	15
08:30 AM	0	2	-	0	0	-	0	0	0	4	0	0	0	0	0	0	00
08:45 AM	0	3	-	0	0	3	0	0	-	3	-	0	2	2	0	0	16
Total	0	11	2	0	2	00	0	0	5	41	-	0	m	7	0	0	20
imnd Total	0	23	3	0	4	13	-	0	3	34	-	0	'n	14	0	0	101
Appreh %	0	88.5	11.5	0	22.2	72.2	9.6	0	6.7	89.5	2.6	0	26.3	73.7	0	0	
Total %	0	22.8	m	0	4	12.9	-	0	m	33.7	-	0	S	13.9	0	0	

000

38.5

000

0.8

105 86.1 31.3

13.1

23 23

5.4 000

45 13.4

56.7

5.8

Grand Total Appreh % Total %

00000

15 11 22 22 25 66

2

2

123

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

00000

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

35

Groups Brinted-Heavy Vehicles

Right

Left U-Tum

	one for Total			3 17	3 11	2 11	4 15	12 54		750
	En App. Total			0	0	0	0	0	0	ľ
Boylston Street From West	AR U.F			0	0	0	0	0	0	000
Boylste	Thru. I			7	7	_	4	6	75	563
	Right			-	1	1	0	3	25	250
	ton heat			9	4	4	4	81		250
enne	U-Turn A			0	0	0	0	0	0	000
Ausstehnsetts Avenue From South	Lef			0	0	0	0	0	0	1000
Massach	The			9	3	4	3	91	688	667
	Right			0	-	0	-	2	11.1	SOO
1	App. Total			2	2	2	4	10		203
20	Ulten App Total			0	0	0	0	0	0	000
Roylston Street From East	Len			-	0	0	0	-	10	050
Boy	Thru			0	7	7	2	9	8	750
	Right		M	-	0	0	2	3	30	375
	J-Turn App. Total	k lof l	at 07:30 AM	9	7	6	6	14		503
venue	U-Tuen	AM-Pes	gins at	0	0	0	0	0	0	000
fassachusetts A venue From North	Treft	110 08:45	ction Be	0	-	0	0	I	7.1	250
Massac	Thru	07:00 AM	Interse	9	-	6	3	13	92.9	CFS
	Right	sis From	r Entire	0	0	0	0	0	0	9
	StartTime	Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1	Peak Hour for Entire Intersection I	07:30 AM	07:45 AM	08:00 AM	08:15 AM	Total Volume	% App. Total	and

		Massichaeats Av From Nord	hasets Av	venue			Boy	Boylston Street From East	N.			Massachuse	Schusetts Ave From South	one			Boy	Boylston Street From West	M		
Start Time	Right	The	Left	UrTum	Ages Total	Right	The	Let	J-Then A	App. Desi	Right	Thru	Left	Tues	Ages, Total	Right	The	Leff	J-Tuen	Age. Tess	Int. Total
oak Hour Analysis From 07:00 AM	sis From 0	7:00 AM	0 08:45	AM - Peak	kloff																
Peak Hour for Entire Intersection Begins	Entire	Intersec	tion Be	gins at	at 07:00 AM	W															
07:00 AM	-	4	4	0	6	-	0	7	0	10	4	15	0	0	19	1	2	1	0	4	35
07:15 AM	0	=	00	0	19	1	0	0	0	1	e	18	-	0	22	3	4	0	0	7	8
07:30 AM	6	11	m	0	17	0	-	1	0	7	N	=	0	0	13	7	m	0	0	S	37
07:45 AM	0	1	1	0	14	2	*	0	0	S	2	22	0	0	24	4	v	7	0	=	54
Total Volume	4	33	22	0	89	10	4	3	0	17	=	99	-	0	78	10	14	3	0	27	181
% App. Total 6.8		55.9	37.3	0		58.8	23.5	971	0		14.1	84.6	13	0		37	51.9	111	0	H	
CITIC				000	322	250			2000	200				WWW	0.00	200			l		

File Name : 133307 A Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

146 169 169 241 310 866 442 442 442 460 528 1789

78 68 84 33 332

38 12 m

28 8 4 7 5

32 33 38 38

8 125 8 135 135 484

75 77 116 357

∠ 4 2 0 4

28842

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

\$10 89.3 19.2

16 2.8 0.6 452

4 0.7 427 75.8 16.1

133

0.3

28 743

03 0.5

510 66.1 19.2

31-4

180 23.3 6.8 3.6

Grand Total Appreh % Total %

27 27 42 51 58 178

26 26 18 18 18 19 19 19

Thru 10 10 10 10 38

Peds 40 71 71 92 259

4

89 35 9

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

Right

Right

Groups Printed-Peds and Bicycles

N/S: Massachusetts Avenue E/W: Boylston Street City, State: Boston, MA Client VHB/ M. Houdlette

File Name : 133307 A Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

7	PRECISION D A T A INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 01503 Office:508:481.3999 Fax:508.5451234 Emait datarequest@pdillc.com
		Office

		Massac	From Morth	di di			and a	From Fast	ď.			Water B.	From South	Commo .		Ì	DO.	From West			
Start Time		Right Thru	Left	U-Turn	Left U-Tum Americal	Right	Thru	Left	Urben	Left Urben Ass. Total	Right	Tha	Lef	U.Tum	Left U.Turn Age 11cm Right	Right	Thru		Left Urben Age best	Age. Total	
Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1	sis From	07:00 AM	110 08:45	AM-Pe	k lof1																
Peak Hour for Entire Intersection Begins at 07:45 AM	Intire	Interse	ction Be	gms at	07:45	¥.															
07:45 AM	10	100	49	0	168	41	24	0	0	65	13	171	10	0	189	28	95	'n	0	128	
08:00 AM	13	101	35	0	138	84	56	-	0		16	152	7	0	170	34	107	4	0	145	
08:15 AM	=	128	47	0	186	47	22	1	0	20	24	142	S	0	171	25	101	-	0	139	
08:30 AM	6	134	42	0	185	26	23	0	0	49	80	181	-	0	190	30	93	4	0	127	_
Total Volume	32	472	173	0	119	198	95	2	0	295	19	646	13	0	720	117	402	20	0	539	_
% App. Total	4.7	2.69	25.6	0		67.1	32.2	0.7	0		8.5	1.68	1.8	0		21.7	74.6	3.7	0		_
PHF	727	188	883	000	016	685	913	200	000	1999	635	.892	059	000	.947	098	626	714	000	676	
Cars	H	434	146	0	610	_	82	7	0	272	¥	584	13	0	651	66	370	18	0	487	
% Cars	93.8	6.16	84.4	0	90.1	_	863	100	0	92.2	88.5	90.4	100	0	90%	84.6	92.0	0.06	0	90.4	
Beary Vehicles	2	53	25	0	98	00	9	0	0	4	5	48	0	0	53	91	25	4	0	43	
% Honry Vehicles	6.3	6.1	14.5	0	8.3	4.0	6.3	0	0	4.7	8.2	7.4	0	0	7.4	13.7	6.2	10.0	0	8.0	
Buses	0	6	2	0	11	2	1	0	0	6	2	14	0	0	16	7	1	0	0	6	
% Buses	0	1.9	1.2	0	1.6	1.0	7.4	0	0	3.1	3.3	2.2	0	0	2.2	1.7	1.7	0	0	1.7	_
			L	l	l	l	l	L	Mass	Massachusetts Avenue	ts Avenu	91	L	l	l	l	l	_			
									d	=	To	a									
									8 8	2 8	-	3 4									
									16	_	_	27									
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									4			1									
									98	\$ R	25	00	_					_			
									0 8	8 64	220	00									
									Right]_	Left U	U-Tum									
									1	,	•										

550 564 566 551 2231 2230 90.5 166 7.4 45

	Boylston Street Out Total 570 272 842 555 14 69 114 69 188 82 2 0 0 2 7 0 0 198 96 2 0 Rgift Thru Left U-Turn	
730 610 1744 1744 1744 1744 1744 1744 1744 17	Peak Hour Data North Peak Hour Begins at 07.45 AN Cass Heasty Vehicles Busser	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	Page Page	

		Massac	hasets A	lvenue di			Bo	ykton Str	8			Massad	nuscets A	venue			Boy	Iston Str om Wes	¥		
Start Time	Right	Thru	Ireft	Peds	Age. Total	Right	Then	Leff	Peds	App. Des	Right	Thru	Left	Peds	Ages, Total	Right	Three	Left	Peds	Age, Desi	Int. Total
onk Hour Amilys	sis From C	77:00 AM	to 08:45	AM - Pe	ak lof!																
eak Hour for	E	Intersec	ction B	egins at	A 00:80	M															
08:00 AM		22	7	75	109	7	0	0	86		0	15	0	51		0	2	-	78		
08:15 AM		28	4	68	136	-	0	0	126		0	30	0	7		0	00	1	89		
08:30 AM		30	13	17	125	0	-	0	125		7	32	0	74		0	13	4	84		
08:45 AM		41	9	911	165	0	0	0	135		0	8	0	06		4	12	2	102		_
Total Volume	Γ	7 121 40 357 5	40	357	535			0	484	887		98	0	286	383	4	38	6	332	383	1789
% App. Total	m	22.6	7.5	66.7	The second	9.0	0.2	0	99.2		0.5	24.8	0	74.7		-	6.6	2.3	2.98		
PHF	8	738	714	269	811			000	806			742	000	704		250	731	563	814		



File Name: 133307 AA Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S. Massachusetts Avenue E/W: Boylston Street City, State: Boston, MA Client: VHB/ M. Houdlette





Z	PRECISION	DATA	INDUSTRIES, LLC	P.O. Box 301 Berlin, MA. 01503 Office-508-481.3999 Fax: 508.545.1234 Emait desurequest@pdiff.com	

File Name: 133307 AA Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

U-7 cm Right From Fart From Sart		2	Massachusetts Avern	Average			Booken Street	Street,	- Common	Me	Macachinetta Aversa	Aversa			Roderon Stee	Creent		
18 std Then Left V-Tum Relat Then Left V-Tum Relat Then Left Hong Left Left Left Left Left Hong Left Left Then Left Then Left			From N	ionth			From E.	ast.			From So.	uth			From W	- Cal		
15 122 43 2 39 16 3 0 16 119 0 0 0 23 108 7 1135 35 0 44 21 23 0 15 118 1 0 0 23 108 8 142 42 2 0 61 23 0 17 144 0 0 38 107 9 143 125 39 0 61 23 0 0 17 144 0 0 38 107 1 13 125 39 0 62 39 0 0 16 149 0 0 35 103 1 13 43 43 0 55 26 0 13 149 0 0 37 99 1 40 498 176 1 239 100 1 0 67 592 6 0 121 408 1 40 498 176 1 239 100 1 0 67 592 6 0 231 408 1 5 5 7 7 7 7 7 7 7 7	StartTime	Right	Thru	Loft	U-Tum	Right	Thru	Left	Flum	Right	Thru	Left	U-Turn	Right.	Thru		U-Tum	Int Total
1 7 118 38 0 44 23 0 0 17 144 0 38 100 1 8 142 42 0 61 23 0 17 144 0 38 107 1 37 517 158 20 61 23 0 13 126 3 107 415 416 415 415 416 415 416 415 416 415 416 416 416 416 416 416 416 416 416	04:00 PM	15	122	43	2	39	16	3	0	16	119	0	0	32	108	0	0	515
1 8 125 33 0 41 18 3 0 17 144 0 0 29 100 1 37 517 188 2 185 80 6 0 13 126 3 0 127 415 1 1 125 39 0 62 20 0 0 16 145 0 0 35 100 1 1 123 48 0 60 24 0 0 18 151 2 0 37 100 1 40 498 176 1 239 100 1 0 67 592 6 0 121 408 2 47 1015 334 2 424 180 7 0 126 1999 10 0 248 823 3 48 47 47 47 47 47 47 47	04:15 PM	1	118	38	0	44	23	0	0	13	118	-	0	28	100	61	0	492
1 8 442 442 64 51 52 6 6 13 126 3 6 79 100 11 12 13 125 39 6 6 2 30 6 6 13 149 6 127 415 12 12 13 13 43 6 62 30 0 13 149 0 31 100 13 123 43 0 62 20 0 13 149 0 0 31 100 14 15 123 43 0 65 26 1 0 13 149 0 26 106 15 17 1015 334 3 424 180 7 0 126 1099 10 0 248 823 18 233 77 01 237 431 0 0 29 233 0 0 21 189 19 10 10 10 10 10 10 10	04:30 PM	7	135	35	0	41	18	3	0	17	14	0	0	38	107	0	0	545
1 37 517 158 2 185 80 6 0 59 507 4 0 127 415 13 125 39 0 62 20 0 16 145 0 0 35 103 14 18 126 46 1 62 30 0 0 18 145 0 0 37 100 15 11 123 48 0 60 24 0 0 20 147 4 0 26 106 16 17 1015 334 3 424 180 7 0 126 1099 10 0 248 823 18 18 213 77 011 214 012 014 014 014 014 014 014 014 014 014 19 19 19 19 19 19 19	04:45 PM	00	142	42	0	19	23	0	0	13	126	3	0	29	100	0	0	547
1 13 125 39 0 62 20 0 16 145 0 0 35 100 1 123 48 1 62 30 0 16 145 0 0 33 100 1 11 123 48 0 60 26 10 18 15 2 0 27 147 4 0 26 106 1 40 498 176 1 239 100 1 6 7 592 6 121 408 5 44 180 7 0 126 1099 18 823 31 7 94 823 18 823 5 44 180 7 0 126 1099 18 0 23 13 43 18 23 13 43 13 43 43 43 43 43 43	Total	37	517	158	2	185	80	9	0	86	202	4	0	127	415	7	0	2099
1 8 126 46 1 62 39 0 0 13 149 0 0 27 99 1 11 123 48 0 60 24 0 0 18 151 2 0 27 99 1 40 498 176 1 239 100 1 0 67 592 6 0 121 408 1 7 1015 334 3 424 180 7 0 126 1099 10 0 248 823 1 8 233 77 01 97 410 02 02 25 253 02 0 571 186 1 8 125 125 125 125 125 125 125 125 125 125 1 8 125 125 125 125 125 125 125 125 125 125 1 8 125 125 125 125 125 125 125 125 125 125 1 8 125 125 125 125 125 125 125 125 125 125 1 9 125 125 125 125 125 125 125 125 125 125 1 9 125 1	05:00 PM	13	125	39	0	62	20	0	0	91	145	0	0	35	103	0	0	558
1 11 123 48 0 55 26 1 0 18 151 2 0 77 99 1 10 123 48 0 60 24 0 0 20 147 4 0 26 106 1 10 123 124 18 1 239 100 1 0 67 592 6 0 121 408 1 77 1015 334 3 424 180 7 0 126 1099 10 0 248 823 1 8 233 77 01 97 41 0 02 95 253 02 0 57 189	05:15 PM	00	126	46	-	62	30	0	0	13	149	0	0	33	100	-	0	895
11 123 48 0 60 24 0 0 20 147 4 0 26 106 106 106 107 10	05:30 PM	00	124	43	0	55	26	-	0	18	151	2	0	27	8	-	0	555
40 498 176 1 239 100 1 0 67 592 6 0 121 408 1	05:45 PM	11	123	48	0	09	24	0	0	20	147	4	0	56	106	0	0	869
77 1015 334 3 424 180 7 0 126 1099 10 0 248 823 824 824 825	Total	40	498	176	1	239	100	-	0	19	592	9	0	121	408	4	0	2251
5 5.4 71 23.4 0.2 69.4 29.5 1.1 0 10.2 89 0.8 0 23.1 76.6 1.8 23.3 7.7 0.1 9.7 4.1 0.2 0 2.9 25.3 0.2 0 5.7 18.9	Grand Total	11	1015	334	8	424	180	1	0	126	1099	10	0	248	823	4	0	4350
1.8 23.3 7.7 0.1 9.7 4.1 0.2 0 2.9 25.3 0.2 0 5.7 18.9	Appreh %	5.4	7.1	23.4	0.2	69.4	29.5	1.1	0	102	68	8.0	0	23.1	9.9/	0.4	0	
	Total %	1.8	23.3	7.7	0.1	1.6	4.1	0.2	0	2.9	25.3	0.2	0	5.7	18.9	0.1	0	

	Age You			138	134	127	132	531		000
reet	U-Dan			0	0	0	0	0	0	WWW.
cylsten Street From West	Left		-	0	-	-	0	7	0.4	2000
Bo	Thru			103	100	8	901	408	76.8	W.
	Right		-	35	33	27	26	121	22.8	0.00
	Age. Desi			191	162	171	171	665	1	1
emae 1	U-Turn			0	0	0	0	0	0	www
usetts Av	Lef	200	4	0	0	7	*	9	6.0	2000
Massach	The			145	149	151	147	592	68	www
	Right		4	10	13	18	20	19	101	0000
	Age, Total			82	92	82	84	340	1	,00
*	U-Tuen			0	0	0	0	0	0	WWW
Roylston Street From East	Len			0	0	-	0	-	0.3	
Boy	Theu			2	30	56	24	100	29.4	
	Right			9	62	55	09	239	70.3	
	App. Total	k l of 1	1000	171	181	175	182	715		000
enne	U-Tuen	M - Peak	ins ar o	0	-	0	0	1	0.1	000
Assachusetts A v From North	Teff	0 0 5:45 PM - Peak	ion begins at	39	9	43	48	176	24.6	200
Massach	Then	100 PM	ntersoc	125	126	124	123	864	69.7	000
	Right	s From 0	-mure	3	60	00	11	40	5.6	000
Ī	StartTime	Peak Hour Analysis	reak Hour for I	05:00 PM	05:15 PM	05:30 PM	05:45 PM	Total Volume	% App. Total	

4350 95.2 105 2.3 112 2.5

000

126 126 126

201 4.4 180 89.6 431 9.4 424 98.4

8 2 2 4 4 4

5.5

Grand Total Appreh %
Total %
Cars
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595 573 594 594

| Start Time | Sta

591 573 594 594

156 156 156 156 624

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05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

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558 569 555 569 2251



Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

File Name: 133307 AA Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

21 21 14 16 16 69

10 10 36 10 10 10 10

000

- 6 -52.2 11.4 10 43.5 000

23 3 73.2 8 19.5 7.6

33.3 55.6 000

22.9 15 4

1.9

Grand Total Appreh % Total %

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

N/S: Massachusetts Avenue E/W: Boylston Street City, State: Boston, MA Client VHB/ M. Houdlette

File Name: 133307 AA Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

							GROUN PTERC	C- Diagra								
	M	Massachusetts Avenue	8 A venue			Boylston Street	Rred		Massachusetta Avenue	a Avenue			Boylston Street	Street		
		From North	douth			From East	201		From South	outh			From West	/est		
StartTime	Right	Thru	Left	U-Tum	Right	Thru	Left U-Tum	Right	Thru	Left	U-Tura	Ri ght	Thru	Left U-Turn	L-Turn	Int. Total
04:00 PM	0	2	0	0	0	2	0	0 0	5	0	0	0	4	0	0	13
04:15 PM	0	m	0	0	0	3	0	0	2	0	0	0	2	0	0	13
04:30 PM	0	'n	0	0	-	3	0	0	S	0	0	0	4	0	0	18
04:45 PM	0	0	0	0	0	4	0	0	2	0	0	0	2	0	0	80
Total	0	10	0	0	-	12	0	0	17	0	0	0	12	0	0	52
05:00 PM	0	4	-	0	0	2	0	0	6	0	0	-	5	-	0	23
05:15 PM	0	6	0	0	0	7	0	0	4	0	0	-	0	0	0	10
05:30 PM	1	4	0	0	0	-	0	0	4	0	0	0	2	0	0	12
05:45 PM	2	2	2	0	-		0	0	9	0	0	0	-	0	0	15
Total	3	13	3	0	-	9	0 0	0 0	23	0	0	5	8	1	0	09
Grand Total	8	23	3	0	2	18	0	0 0	40	0	0	7	20	-	0	112
Appreh %	10.3	79.3	10.3	0	10	8	0	0	100	0	0	8.7	87	43	0	
Total %	2.7	20.5	2.7	0	8.	16.1	0	0	35.7	0	0	1.8	17.9	6.0	0	

	2	From	Massichusetts Avenue From North			8	Boylston Street From East	10			Massachusetts Avenue From South	thus atts Avenue From South	0		•	Boylston Stree From West	Street					Massac	Massachusetts Avenue From North	venue	Ħ		Boyle	Boylston Street From East			Mas	Ansarchusetts Avenue From South	Avenue			Bo	Boylston Street From West	10	
Start Time Right Thru Left urum Age von Right Thru Left Urum Age took Right Thru	Right	Tru L	eff Linn	To Ago Ton	Right	The	Left	U-Tum As	to lites	Right	Thru	Jeff U-Tu	Left U-Turn Age Town Right	al Right		The Left	U-Turn /	App. Total	Int. Total	Start Time	e Right	Then	Left	U-Turn	App. Total	Right	Theu	Left Urben	T. Age. T.	Rich	il The	u Left	U-Turn	Age, Desi	Right	Thru	Left	Left U.Ten A	Age You!
bak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	1 From 04:0	0 PM to 0.	5:45 PM - 1	Peak I of 1																Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of	bais From	04:00 PM	\$600545	PM - Peak	1 of 1								1000	1000					
Peak Hour for Entire Intersection Begins at 04:00 PM	Entire Int	creection	n Begins	at 04:00	PM															Peak Hour for Entire Intersection	or Entire	Intersec	ction Be	gins at (4:15 PA					į									
04:00 PM	-	8	0	•	0	1	0	0	-	0	7	7	0	6	2	0	0	S	21	04:15 PM	0	3	0	0	m	0	m	0	0	m	0	5 0	0	5	0	2	0	0	71
15 PM	0	7	-		7	0	0	0	7	7	9	0	0	2	1	0	0	4	14	04:30 PM	0	vo	0	0	vo	-	m	0	0	4	0	0 5	0	5	0	4	0	0	4
4:30 PM	0	0	3	6	0	7	0	0	21	10	1	0	0	0	1	0	0	-	91	04:45 PM	0	0	0	0	0	0	4	0	0	4	. 0	2 0	0	2	0	*	0	0	7
04:45 PM	-	2	2		2	0	0	0	2	-	4	0	0	2		-	0	9	81	05:00 PM	0	4	-	0	'n	0	2	0	0	2	0	0 6	0	6	-	*	-	0	7
Potal Volume	2	6	9	1 6	4	3	0	0	1	9	21	2	0	29 7	00	-	0	91	69	Total Volume	0	12	1	0	13	-	12	0	0	13	0 2	1 0	0	21	-	13	-	0	15
% App. Total 11.8 52.9 35.3	11.8 5	2.9 35	3		57.1	42.9	0	0		7 7.02	2.4	6.3	0	43.8	20	6.2	0	3.		% App. Total	0	92.3	7.7	0		7.7	12.3	0	0		0 100	0 (0		6.7	298	6.7	0	
PHF	.500 .450	150 .500	000' 00		.500	375	.708 .500 .375 .000 .000	000	\$78	200	750 .2	.875 .500 .750 .250 .000	0 .72	.725 .583	.500 250	250	000	199	821	PHF	E 000	009	250	000	059	250	750	000 000	8 0	13 000	583	3 ,000	000	583	250	059	050	000	925

		Massack	fassachusetts A venue From North	venue	1		Boy	Boylston Street From East	×	i		Massack	assechusetts Avenue From South	- cons			Boyl	Boylston Street From West	r.	Ħ	
Start Time	Right	Then	Left	U-Tuen	App. Total	Right	There	Len	UrTen	Age. Total	Right	Three	Lef	U-Turn	Ago, Thesi	Right	Thru	Left	J.Turn An	Age You!	In To
Peak Hour Analys	is From 0	4:00 PM	0 0 5 45	PM - Peal	k l of 1																
Peak Hour for	Entire	Intersec	section Be	gins at	04:15 P	×															
04:15 PM	0	m	0	0	6	0	m	0	0	0	0	9	0	0	5	0	7	0	0	71	
04:30 PM	0	w	0	0	80	-	m	0	0	4	0	S	0	0	S	0	4	0	0	4	
04:45 PM	0	0	0	0	0	0	4	0	0	4	0	7	0	0	2	0	N	0	0	7	
05:00 PM	0	4	-	0	2	0	2	0	0	2	0	6	0	0	6	-	*	-	0	7	
Total Volume	0	12	1	0	13	-	12	0	0	13	0	.21	0	0	21	1	13	1	0	15	5
% App. Total	0	92.3	7.7	0		7.7	92.3	0	0		0	100	0	0		6.7	2.98	6.7	0		
PHF	000	009	250	000	059	250	750	000	000	813	000	583	000	000	583	250	059	250	000	985	19

File Name: 133307 AA Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S. Massachusetts Avenue E/W: Boylston Street City, State: Boston, MA Client: VHB/ M. Houdlette



File Name : 133307 AA Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

		Massacl	Massachuseffs A verue From North	verne h			Boy	Boylston Street From East	8			Massac	Asseschusetts Averne From South	- conse			Fi	From West	ž.		
Start Time	Right	Thru	Left	U-Tum	Left U-Tum App. Dots	Right	Thru	Left	Urben	Ago, Total	Right	Than	Left	U-Tum	Ago, Tiess	Right	Thru	Left	U-Tuen	Age, Total	Int. Total
eak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of	is From (4:00 PM	\$6.00	PM - Peal	t lof 1																
eak Hour for	Entire	Intersect	tion Be	ion Begins at	05:00 P	×					į										
05:00 PM	13	131	40	0	182	63	22	0	0	88	14	156	0	0	173	38	110	-	0	140	165
05:15 PM	00	134	46	-	189	62	32	0	0	94	14	156	0	0	170	34	101	-	0	136	589
05:30 PM	6	132	43	0	18	55	27	-	0	83	18	156	5	0	176	27	102	-	0	130	573
05:45 PM	13	129	20	0	192	19	25	1	0	87	20	156	2	0	181	27	107	0	0	134	594
Total Volume	43	526	179	1	749	241	901	2	0	349	69	624	7	0	200	126	420	3	0	549	2347
% App. Total	5.7	70.2	23.9	0.1		1.69	30.4	9.0	0		6.6	89.1	-	0	T	23	76.5	0.5	0		
PHF	827	186	895	.250	576	986	828	200	000	928	863	1.00	350	000	196	829	955	.750	000	.921	886
Cars	9	498	176	-	715	239	100	-	0	340	29	592	9	0	999	121	408	2	0	531	2251
% Cars	93.0	4.7	983	100	95.5	99.2	943	50.0	0	97.4	97.1	6.46	85.7	0	95.0	0.96	97.1	1.99	0	2.96	636
feary Vehicles	0	15	0	0	15	-	0	-	0	2	2	6	-	0	12	m	4	0	0	7	36
N. Honry Vehicles	0	5.9	0	0	2.0	0.4	0	50.0	0	9.0	5.9	1.4	143	0	1.7	2.4	1.0	0	0	13	1.5
Buses	3	13	3	0	19	-	9	0	0	7	0	23	0	0	23	2	00	-	0	Ξ	99
% Buses	7.0	2.5	1.7	0	2.5	0.4	5.7	0	0	2.0	0	3.7	0	0		91	0	33 3	0	00	36

136 173 173 173 173 174 175

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05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

97.7 0.3 1.9

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881 78.1 4 71 2.6

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Peds 123 136 120 67 446

9eds 100 81 188 116 485

10 10 10 39 39

Peds 116 119 91 116 442

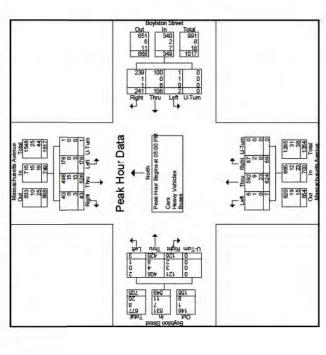
4 2 2 18

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

Right

Right

Groups Printed-Peds and Bicycles Mass





Avenue et/Haviland Street MA

File Name : 133307 B Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

Night The Left L-Tum Right The The		M	Massachusetts A venue From North	Avenue			Belvidere Street From East	Street		Ma	Massachusetts Avenue From South	Avenue			Haviland Street From West	Hasel		
3 122 0 0 15 4 4 0 0 124 6 6 122 0 0 9 8 7 0 0 130 5 17 476 0 0 19 5 5 0 0 129 5 6 122 0 0 19 5 5 0 0 130 5 6 123 0 0 13 2 2 0 0 148 18 6 123 0 0 13 2 4 0 0 149 4 4 141 0 0 13 2 4 0 0 149 4 8 136 0 0 16 4 4 0 0 166 5 12 18 0 0 42 21 14 0 0	StartTime	Right	Thru	Left	U-Tum	Right	Thro	-	U-Tum	Right	Thru		U.Tura	Right	Thru		U-Tum	Int. Total
4 107 0 0 9 8 7 0 0 130 5 4 125 0 0 19 5 5 0 0 130 5 17 476 0 0 19 5 5 0 0 145 2 4 118 0 0 13 2 2 0 0 142 4 4 118 0 0 13 2 2 0 0 149 4 4 141 0 0 6 6 4 0 0 149 4 8 136 0 0 10 4 4 0 0 163 4 22 518 0 0 4 2 1 1 0 0 17 39 994 0 0 94 22 1 1 0 <td>77:00 AM</td> <td>3</td> <td>122</td> <td>0</td> <td>0</td> <td>15</td> <td>4</td> <td>4</td> <td>0</td> <td>0</td> <td>124</td> <td>9</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>278</td>	77:00 AM	3	122	0	0	15	4	4	0	0	124	9	0	0	0	0	0	278
6 122 0 0 7 5 5 0 0 129 5 17 476 0 0 19 5 5 0 0 142 5 4 118 0 0 13 2 4 0 0 142 4 6 123 0 0 13 9 2 0 0 149 4 8 136 0 0 16 4 4 0 0 149 4 22 518 0 0 4 2 1 4 0 0 166 5 33 944 0 0 92 43 33 30 0 0 189 31 17 45 0 94 23 30 0 0 66 31 1 17 45 0 18 15 0	77:15 AM	4	101	0	0	6	00	1	0	0	130	5	0	0	0	0	0	270
4 125 0 0 19 5 5 0 0 145 2 17 476 0 0 50 22 21 0 0 145 2 6 118 0 0 13 2 2 4 0 0 149 4 8 141 0 0 16 6 4 0 0 149 4 22 518 0 0 16 6 4 4 0 0 163 4 22 518 0 0 16 4 4 0 0 163 4 39 994 0 0 42 21 14 0 0 560 17 38 962 0 94 4 18 15 0 668 33 17 42 0 18 15 0 669	77:30 AM	9	122	0	0	1	80	S	0	0	129	8	0	0	0	0	0	279
17 476 0 0 50 22 21 0 528 18 4 118 0 0 13 2 4 0 142 4 6 123 0 0 13 9 2 0 0 142 4 8 136 0 0 6 6 4 0 0 163 4 22 518 0 0 16 4 4 0 0 106 5 39 944 0 0 42 21 14 0 0 560 17 38 962 0 0 42 21 14 0 0 569 31 17 427 0 0 44 18 15 0 0 668 33	77:45 AM	4	125	0	0	19	8	8	0	0	145	2	0	0	0	0	0	305
4 118 0 0 13 2 4 0 0 142 4 6 123 0 0 13 9 2 0 0 149 4 8 136 0 0 6 6 4 0 0 163 4 22 518 0 0 42 21 14 0 0 106 5 39 944 0 0 92 43 35 0 0 17 6 17 17 427 0 0 44 0 0 669 33 1 17 427 0 0 44 0 0 669 31	Total	17	476	0	0	80	22	21	0	0	528	18	0	0	0	0	0	1132
6 123 0 0 13 9 2 0 0 149 4 8 136 0 0 6 6 4 0 0 163 4 22 518 0 0 10 4 4 0 0 163 4 39 994 0 0 42 21 14 0 0 560 17 17 427 0 0 42 21 14 0 0 560 17 13 964 0 0 44 23 35 0 1088 35 17 427 0 0 44 23 35 0 0 969 31 17 427 0 0 4 18 15 0 0 969 31	38:00 AM	4	118	0	0	13	2	4	0	0	142	4	0	0	0	0	0	287
4 141 0 0 6 6 4 0 0 163 4 14 15 14 15 15 15 15	18:15 AM	9	123	0	0	13	6	7	0	0	149	4	0	0	0	0	0	306
8 136 0 0 10 4 4 0 0 106 5 5 1 1 2 5 1 1 4 0 0 106 5 1 1 1 1 1 1 1 1 1	38:30 AM	4	141	0	0	9	9	4	0	0	163	4	0	0	0	0	0	328
22 518 0 0 42 21 14 0 0 560 17 1 1 2 2 3 3 3 3 3 3 3 3	38:45 AM	90	136	0	0	10	4	4	0	0	106	2	0	0	0	0	0	273
39 994 0 0 92 43 35 0 0 1088 35 3.8 96.2 0 0 841 253 20.6 0 96.9 3.1 1.7 42.7 0 0 4 1.8 1.5 0 0 46.8 1.5	Total	22	518	0	0	42	21	14	0	0	260	17	0	0	0	0	0	1194
3.8 96.2 0 0 54.1 25.3 20.6 0 0 96.9 3.1 1.7 42.7 0 0 4 1.8 1.5 0 0 46.8 1.5	and Total	39	56	0	0	92	43	35	0	0	1088	35	0	0	0	0	0	2326
1.7 42.7 0 0 4 1.8 1.5 0 0 46.8 1.5	Appreh %	3.8	96.2	0	0	7	25.3	20.6	0	0	6.96	3.1	0	0	0	0	0	
	Total %	1.7	42.7	0	0	4	1.8	1.5	0	0	8.94	1.5	0	0	0	0	0	

	los Total		305	287	306	328	1226	1	934
	Age Total		0	0	0	0	0		000
200	U-Tern		0	0	0	0	0	0	000
lavland Street From West	Left		0	0	0	0	0	0	000
Hav	Thru		0	0	0	0	0	0	000
	Right		0	0	0	0	0	0	000
	App. Desi		147	146	1.53	167	613		816
reme	U-Turn		0	0	0	0	0	0	000
rom Sout	Leg		7	4	4	4	14	2.3	875
Massach	Thru		145	142	149	163	899	7.76	616
	Right		0	0	0	0	0	0	000
	App. Total		29	19	24	16	88		750
100	Urren		0	0	0	0	0	0	000
Belvidene Street From East	Len		40	4	71	4	15	17	054
Bely	Thru		5	2	6	9	22	25	119
	Right	2	19	13	13	9	SI	28	129
	App. Total	10[1	129	122	129	145	525		506
- Seption	U-Tuen	M. Pest	0	0	0	0	0	0	000
rom North	Treff	to 0845,	0	0	0	0	0	0	000
Massach	Then	7:00 AM	125	118	123	141	207	9.96	800
	Right	Amalysis From 07	4	4	9	4	18	3.4	052
	StartTime	Peak Hour Analysis	07:45 AM	08:00 AM	08:15 AM	08:30 AM	Total Volume	% App. Total	PHF

344 320 339 335 355 355 365 90.3 103 7.6 29 29

172 169 179 681

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serts Av	Street/	f. Houc		Massach	Right T	3 L	4	9	4	17 4	4	9	4	00	22 5	39 9	3.8 96						Massachuset	From
N/S: Massachusetts Av	E/W: Belvidere Street/	City, State: Boston, MA Client: VHB/ M. Houd			StartTime	MA 00:00	07:15 AM	07:30 AM	07:45 AM	Total	08:00 AM	08:15 AM	08:30 AM	08:45 AM	Total	Grand Total	Appreh %	Total %						
File Name : 133307 B	: 10135.00	Start Date : 5/14/2013 Page No : 1			Int. Total	315	312	321	344	1292	320	339	355	318	1332	2624			23.26	988	232	8.8	99	3 6
. 133	101	: 5/1			-Tum	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	<
Name	Site Code	Start Date Page No		1994	Left	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4
File	Site	Star		Havland Street From West	The	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
				H	Right	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
					-Turn	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4
				venue	Loft	9	2	S	2	18	4	4	4	s	11	35	2.7	13	35	100	0	0	0	•
		i	2	Massachusetts Avenue From South	Thru	151	151	151	170	623	157	165	175	126	623	246	97.3	47.5	880	87.3	123	6.6	35	
		01503 8545.1234 Ilc.com	hides - Bu	Mass	Right	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4
PRECISION	D A T A	P.O.Box 301 Berlin, MA 01503 ox:508.4813999 Fax 508.545.1 fmalt:daranequests@pdflc.com	- Heavy Ve		-Lum	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
D D	DON	P.O.Box 301 Berlin, MA 01503 Office: 508 481 3799 Fax 508.545.1234 Email: daranquest signality com	nted-Cass	reed	Loft	4	1	9	S	77	4	10	5	S	17	39	21.4	1.5	35	7.68	4	103	0	
		0	Groups Printed-Cast - Heavy Vehicles - Buses	Betvidere Street From East	Thru	4	00	S	8	22	m	6	9	4	22	4	24.2	1.7	43	7.76	-	2.3	0	4
			Ì	В	Right	16	12	1	10	¥	14	13	1	=	45	66	4.48	3.8	35	92.9	7	7.1	0	
	street				-Tum	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4
	land ?			venue	Left	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4
venue	t/ Hav	A	Т	Massachusetts Avenue From North	Thru	131	125	140	138	534	134	139	154	159	989	120	596	42.7	994	88.88	96	9.8	30	
Setts	Stree	ton, M		Mass	Right	6	4	1	2	16	4	9	4	00	22	14	3.5	971	36		_	2.4	-	
N/S: Massachusetts Avenue	E/W: Belvidere Street/ Haviland Street	City, State: Boston, MA Client: VHB/ M. Houdlette			Start Time	MA 00:00	07:15 AM	07:30 AM	07:45 AM	Total	08:00 AM	08:15 AM	08:30 AM	08:45 AM	Total	Grand Total	Approh %	Total %	Cars	%Cars	Heavy Vehicles	% Heavy Vehicles	Buses	47.00



N/S. Massachusetts Avenue E/W: Belvidere Street/ Haviland Street City, State: Boston, MA Client: VHB/ M. Houdlette

Groups Printed- Heavy Vehicles Street

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

File Name : 133307 B Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Massachusetts Avenue E/W: Belvidere Street/ Haviland Street City, State: Boston, MA Client: VHB/ M. Houdlette

Office:508.481,399 Far;508,5451234 Emait data-request@pdilc.com

File Name: 133307 B Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

Y	PRECISION D A T A	INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 01503

	Ma	Massachusetts Avenue	A venue			Belvidere Street	1990	-	Mas	Massachusens Avenue	Avenue			Havhand Street	Street		
		From North	outh			From East	26.			From South	gh			From West	/est		
StartTime	Right	Thru	Left	Left U-Turn	Right	Thru	Left U-Tum	Com	Right	Thru	Left	Left U-Turn	Right	Thru	Left	Loft U-Turn	Int. Total
07:00 AM	0	2	0	0	0	0	0	0	0	7	0	0	0	0	0	0	
07:15 AM	0	4	0	0	0	0	0	0	0	m	0	0	0	0	0	0	,-
07:30 AM	-	8	0	0	0	0	0	0	0	9	0	0	0	0	0	0	12
07:45 AM	0	4	0	0	0	0	0	0	0	4	0	0	0	0	0	0	~
Total	1	15	0	0	0	0	0	0	0	20	0	0	0	0	0	0	36
08:00 AM	0	4	0	0	0	0	0	0	0	S	0	0	0	0	0	0	
08:15 AM	0	3	0	0	0	0	0	0	0	3	0	0	0	0	0	0	
08:30 AM	0	4	0	0	0	0	0	0	0	2	0	0	0	0	0	0	_
08:45 AM	0	4	0	0	0	0	0	0	0	2	0	0	0	0	0	0	3
Total	0	15	0	0	0	0	0	0	0	15	0	0	0	0	0	0	30
Grand Total	1	30	0	0	0	0	0	0	0	35	0	0	0	0	0	0	99
Appreh %	3.2	8.96	0	0	0	0	0	0	0	100	0	0	0	0	0	0	
Total %	1.5	45.5	0	0	0	0	0	0	0	53	0	0	0	0	0	0	

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884

Grand Total Appreh % Total %

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

Right Thin Lef LiTen Ass load Right Thro Left LiTen Ass load Right Thro Left Lite Li	viand Street					Massach	fassichusetts Avenue From North	enne			Belvi	Belvidene Street From East	Ti di	T		Massach	assichusetts Avenue From South	Store			Havi	Havlind Sreet From West	ĸ
Peak Hour for Battle and May State To Cross AM Peak 1 of 1 Peak Hour for Pattle Intersection Begins at 07.00 AM 0 345 07:15 AM 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Left U-Turn	Age, Desi	Int. Total	Start Time	Right	Thru	Ireft	U-Tuen A	No. Total	Right	Thru	Left		DEC TORI	Right	Three	Left	I-Turn	ton These	Right	Thru	Left	U-Tuen A
Peach Hour for Entire Intersection Begins at 07:00 AM 2 8 07:50 AM 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				Peak Hour Analysi	8 From 07	7:00 AM t	0.089457	M-Pesk	lofl														
0 35 07:150 AM 0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				Peak Hour for	Entire I	ntersect	ion Be	ins at 0	7:00 A														
0 0 35 07:15 AM 0 4 0 0 4 0 0 0 0 0 0 0 3 0 0 3 0 0 3 0 0 0 0	0 0	0	28	07:00 AM	0	7	0	0	7	0	0	0	0	0	0	1	0	0	1	0	0	0	0
0 0 31 07:30 AM 1 5 0 0 6 0 0 0 0 0 0 6 0 0 6 0 0 0 0 0 0	0 0	0	35	07:15 AM	0	4	0	0	4	0	0	0	0	0	0	3	0	0	6	0	0	0	0
0 0 31 07:45 AM 0 4 0 0 4 0 0 0 0 0 0 4 0 0 4 0 0 0 0	0 0	0	30	07:30 AM	-	40	0	0	9	0	0	0	0	0	0	9	0	0	9	0	0	0	0
0 0 124 Total'volamie 1 15 0 0 16 0 0 0 0 0 0 20 0 0 20 0 0 0 0 0 0 0 0	0 0	0	31	07:45 AM	0	4	0	0	4	0	0	0	0	0	0	4	0	0	4	0	0	0	0
0 %Agg, Total 6.2 93.8 0 0 0 0 0 0 100 0 0 0 0 0 0 0 0 0 0 0	0 0	0	124	Total Volume	-	15	0	0	16	0	0	0	0	0	0	20	0	0	20	0	0	0	0
.000 .000 886 PHF 250 .750 .000 .000 .667 .000 .000 .000 .000 .00	0 0			% App. Total	6.2	93.8	0	0		0	0	0	0		0	100	0	0		0	0	0	0
	000 000	000	886	PHF	250	.750	000	000	299	000		000	000	000	000	714		000	714	000	000	000	000

36 .000

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		Massach	nom North	onua			Beh	Belvidere Street From Past	75			Massach	nuscus Av	ongo			Hav	Haviand Street From West	¥.		
tart Time	Right	Thru	Left	UrTum	Ago, Total	Right	The	Left	J-Tuen A	App. Des	Right	Thru	Left	U-Tum	Ages, Total	Right	The	Left	U-Tuen	Age. Desi	Int. Total
Posk Hour Analys	is From 0	7:00 AM	10 08:45 A	AM - Peak 1 of 1	kloff																
Peak Hour for	Entire	Entire Intersec	tion Beg	gins at	107:00 AM	×															
07:00 AM	0	1	0	0	1	-	0	0	0	-	0	20	0	0	20	0	0	0	0	0	28
07:15 AM	0	7	0	0	1	e	0	0	0	0	0	18	0	0	18	0	0	0	0	0	35
07:30 AM	0	13	0	0	13	0	0	-	0	-	0	91	0	0	91	0	0	0	0	0	30
07:45 AM	-	6	0	0	10	0	0	0	0	0	0	21	0	0	21	0	0	0	0	0	31
Total Volume	-	43	0	0	4	4	0	-	0	S	0	75	0	0	75	0	0	0	0	0	124
% App. Total	_	7.79	0	0		80	0	20	0		0	100	0	0	1	0	0	0	0		
CHILL	000	976	9000	000	200	223	500		0000		000	000	000	000	2000	000	000	000	000		

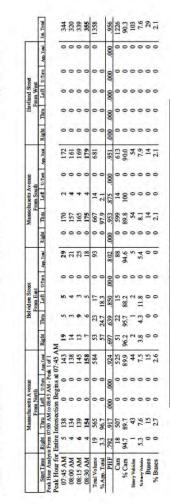
N/S: Massachusetts Avenue E/W: Bebridere Street/ Haviland Street City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 B Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S: Massachusetts Avenue E/W: Belvidere Street/ Haviland Street City, State: Boston, MA Client VHB/ M. Houdlette

PRECISION
D A T A
INDUSTRIES, LLC
P.O. Box 301 Berlin, M. 01503
Office Code, 81, 2009, Prog. 200, 451, 224
Final delayerquesplanelluserum

File Name: 133307 B Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1



115 115 113 138 1463 178 178 178 189 229 224 229 842

100 100 362

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52887

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39 7 11 2 9

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

13 8 8 7 13 8 8 2 6 6

588 99.8 44.8 0.7 000 000

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324

0.3 6 0.5

62 27.1 4.8

165 72.1 12.6

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Grand Total Appreh % Total %

35 64 63 223

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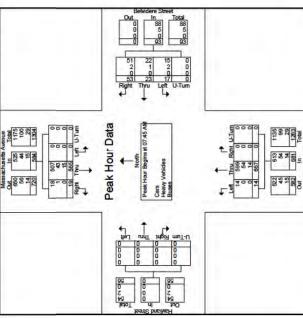
2000

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

Left

Right

Groups Printed-Peds and Bicycles Belvidere Street
Massach



	Total			178	681	246	672	842		958
	test Inc.			75	1 11	110 2	01 2	363 8		825 8
	S App Desi			2	1	1 6		1	-	
Street	Left Peds			0 7	7 0	1 100	0 101	1 362	3 99.7	0 830
Haviand Stre From West				0	0	.0	0	0	0 0.3	0 250
	che Thru			0	0	0	0	0	0	000 00
	on Right			02	22	38	33	811		776 000
	Ago Total							Ē		
s Avenue outh	ft Peds			0	0	0 16	0 16	9 43	36.4	995
tassachusets Avenue From South	Thru Left Peds			3	0	8	4	S	9	000
Mas				0 1	0 2	0 2	0 1	0 7	9'69 0	1
	App. thes Right			25	9	28	52	807		000 268
	Н				4	41				
Street	Thru Leff Peds			0 52	0 45	0 54	0 52	0 204	0 98.1	0 927
Belvidere Street From East	a I.e			0	0	0	0	١	0	000
				0	-	3	0	4	6	3 000
	Right		AM	_	6	0		3	-	0 333
	App. Total	teak 1 of	at 08:00	6	m	4	4	153		800
Avenue	Left Peds	SAM-F	Begins a	6	112	11	7	39	25.5	813
lassichusetts Avenue From North	Left	M to 08 M	ection	0	0	0	0	0	0	000
Mass	Right Thru	n 07:00 A	e Inters	27	0 23	1 28	36	113	73.9	
	Right	ysis From	or Entire	0	9	-	9		0.7	250
	Start Time	Posk Hour Analysis From 07:00 AM to 08:45 AM - Reak 1 of 1	Peak Hour for Entire Intersection Begins at 08:00 AM	08:00 AM	08:15 AM	08:30 AM	08:45 AM	Total Volume	% App. Total	PHF



N/S. Massachusetts Avenue E/W: Belvidere Street/ Haviland Street City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 BB

N/S: Massachusetts Avenue

File Name : 133307 BB Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1



	Ì	Ì					Group	Grouns Printed-	Cars		١						
	Ma	Massachusetts Averue From North	Avenue			Belvidere Street From East	Street		M	Masschusetts Averae From South	Avenue			Haviand Street From West	Hasel		
StartTime	Right	Thru	Left	U-Tum	Right	Thru	Left	U-Tum	Right	Thru	Left	U-Tum	Ri ght	Thru	Loft	U-Tum	Int Total
04:00 PM	7	157	0	0	4	9	2	0	0	117	7	0	0	0	0	0	310
04:15 PM	3	146	0	0	14	00	00	0	0	119	4	-	0	0	0	0	303
04:30 PM	-	171	0	0	15	10	4	0	0	146	2	-	0	0	0	0	350
04:45 PM	4	173	0	0	16	3	0	0	0	142		0	0	0	0	0	339
Total	15	647	0	0	65	27	14	0	0	524	14	2	0	0	0	0	1302
05:00 PM	4	155	0	0	17	7	4	0	0	153	9	0	0	0	0	0	346
05:15 PM	2	155	0	0	6	12	4	0	0	150	4	0	0	0	0	0	336
05:30 PM	4	150	0	0	16	9	9	0	0	147	6	7	0	0	0	0	340
05:45 PM	S	143	0	0	26	6	2	0	0	156	3	0	0	0	0	0	344
Total	15	603	0	0	89	*	16	0	0	909	22	2	0	0	0	0	1366
Grand Total	30	1250	0	0	127	19	30	0	0	1130	36	4	0	0	0	0	2668
Appreh %	2.3	7.76	0	0	58.3	28	13.8	0	0	9.96	3.1	0.3	0	0	0	0	
Total %	1.1	6.94	0	0	8,4	2.3	17	0	0	42.4	1.3	0.1	0	0	0	0	

	in Total		350	339	346	336	1371		626
-	App. Total		0	0	0	0	0	7	000
200	U-Turn		0	0	0	0	0	0	000
aviand Sreet From West	Left		0	0	0	0	0	0	000
Hav	Thru		0	0	0	0	0	0	000
	Right		0	0	0	0	0	0	000
	App. Desi		149	143	159	154	605		156
venue	U-Tum		-	0	0	0	-	0.2	250
rom Sout	Lef		7	-	9	4	13	2.1	542
Massac	Thm		146	142	153	150	165	7.76	996
	Right		0	0	0	0	0	0	000
	App. Total		29	19	28	25	101		871
100	U-Tuen		0	0	0	0	0	0	000
Belvidere Street From East	Len		4	0	4	4	12	6.11	750
Bell	Thru		10	m	1	12	32	31.7	199
	Right	5	15	16	17	6	57	56.4	838
	App. Total	1 of 1	172	177	159	157	999		939
venue	U-Tuen	45 PM - Peak 1 of Regime at 04-2	0	0	0	0	0	0	000
rom Nort	Left	tion Be	0	0	0	0	0	0	000
Massac	Then	MOO PM	171	173	155	155	654	88.3	945
	Right	Pretire	-	4	4	2	=	1.7	889
	StartTime	Peak Hour Analysis From 04:00 PM to 05:4 Peak Hour for Entire Intersection 1	04:30 PM	04:45 PM	05:00 PM	05:15 PM	Total Volume	% App. Total	PHF

369 353 368 368 378 1443 1371 95.0 38 2.6 34 2.4

| Speri Time | Egist | Time | Memory |

	P.O.Bo Office 508. Email of	James L	Left	2	00	4	0	4	4	4	9	"	16
	8	Belvidere Street From East	Then	9	00	10	3	27	7	12	9	6	34
			Right	4	14	15	16	86	11	6	16	26	89
Street			off U-Turn	0	0	0	0	0	0	0	0	0	0
viland	0)	A venue	Left	0	0	0	0	0	0	0	0	0	0
t/Ha	AA udlette	Massachusetts Avenue From North	Then	157	146	171	173	749	155	155	150	143	603
re Stre	ston, N M. Ho	Mas	Right	7	3	1	4	15	4	2	4	S	115
E/W: Belvidere Street/ Haviland Street	City, State: Boston, MA Client: VHB/ M. Houdlette		StartTime	M4:00 PM	04:15 PM	04:30 PM	04:45 PM	Total	05:00 PM	05:15 PM	05:30 PM	05:45 PM	Total
Site Code : 10135.00	Start Date : 5/14/2013 Page No : 1		Int. Total	333	318	369	353	1373	368	353	352	364	1437
: 101			U-Tum	0	0	0	0	0	0	0	0	0	0
Code	Start Date Page No	reed	Tof.	0	0	0	0	0	0	0	0	0	0
Site	Star Pag	Havland Street From West	The	0	0	0	0	0	0	0	0	0	0
			Right	0	0	0	0	0	0	0	0	0	0
			U-Turn	0	-	-	0	2	0	0	7	0	2
		Avenue	Left U-Turn	7	4	2	2	13	9	4	6	3	22

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total



N/S. Massachusetts Avenue E/W: Belvidere Street/ Haviland Street City, State: Boston, MA Client: VHB/ M. Houdlette

Right Thru

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

Grand Total
Appreh %
Total %

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

File Name: 133307 BB Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S: Massachusetts Avenue E/W: Belvidere Street/ Haviland Street City, State: Boston, MA Client VHB/ M. Houdlette

)	PRECISIO	DAT	INDUSTRIES, L	P.O. Box 301 Bedin, M e-508,481,3999 Fax:
				ago.

File Name: 133307 BB Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

							GWD	mount Printed- B	- Supple		١						
	Ma	Massachusens A venue From North	Avenue			Belvidere Street From East	imet		Ma	Massachusetts Averue From South	Avenue		1	Haviland Street From West	Hatel		
StartTime	Right	Thru	Left	U-Tum	Right	Then	Left	U-Tum	Right	Thru	Left	U-Tum	Ri ght	Thro		Left U-Turn	Int. Total
04:00 PM	0	-	0	0	0	0	0	0	0	S	0	0	0	0	0	0	9
04:15 PM	0	4	0	0	0	0	0	0	0	m	0	0	0	0	0	0	1
04:30 PM	0	3	0	0	0	0	0	0	0	8	0	0	0	0	0	0	00
04:45 PM	0	2	0	0	0	0	0	0	0	7	0	0	0	0	0	0	4
Total	0	10	0	0	0	0	0	0	0	15	0	0	0	0	0	0	25
05:00 PM	0	8	0	0	0	0	0	0	0	6	0	0	0	0	0	0	14
05:15 PM	0	6	0	0	0	0	0	0	0	S	0	0	0	0	0	0	00
05:30 PM	0	4	0	0	0	0	0	0	0	60	0	0	0	0	0	0	7
05:45 PM	0	2	0	0	0	0	0	0	0	7	0	0	0	0	0	0	6
Total	0	14	0	0	0	0	0	0	0	24	0	0	0	0	0	0	38
Grand Total	0	24	0	0	0	0	0	0	0	39	0	0	0	0	0	0	63
Appreh %	0	100	0	0	0	0	0	0	0	100	0	0	0	0	0	0	
Total %	0	18.1	0	0	0	0	0	0	0	619	0	0	0	0	0	0	

	to Age York Its Total			0 0	0 0	0 0	0 0	0 0 38	0	000 000
From West	AR U.Te			0	0	0	0	0	0	000
Havliar	Thru			0	0	0	0	0	0	WW WW
	Right			0	0	0	0	0	0	000
	App. Des			6	2	m	7	24		567
as Avenue South	U-Turn			0	0	0	0	0	0	0000
assechusetts / From Soc	Lef			0	0	0	0	0	0	0000
Massa	A Three			6 0	0 5	0 3	7 0	0 24	001 0	1667
	Total Righ			0	0	0	0	0		000
	Tuen Age.			0	0	0	0	0	0	000
Belvidene Street From East	Len			0	0	0	0	0	0	000
Belv	Thru			0	0	0	0	0	0	000
	Right		M	0	0	0	0	0	0	000
	App.Total	ak lof l	t 05:00 1	S	9	4	2	14		200
Avenue	U-Then	S PM - Peak 1 of 1	Begins a	0	0	0	0	0 0	0	000
Assectioners A From Nor	n Left	PM to 05x4	section 1	0 9	3 0	4 0	2 0	4 0	0 0	0000
Mas	ght The	rom 04:00	tire Inter	0	0	0	0	0 1	0 10	000
	Start Time Ri	ak Hour Analysis Fron	eak Hour for En	05:00 PM	05:15 PM	05:30 PM	05:45 PM	Total Volume	% App. Total	O drie

		Massaci	Massichasets Avenue From North	on the			Belv	Belvidere Street From East	8			Massach	Massachusetts Avenue From South	enne			Havi	Haviand Street From West		ī		
Start Time	Right	The	Left	UrTum	Age. Total	Right	The	Leg	U-Tuen	App. Des	Right	Three	Left	J.Tum A	Aces Total	Right	Thro	Leff	Then Age	tee tees	Int. Total	Start Tir
Posk Hour Analysis From 04:00 PM to	sis From C	M:00 PM	ĭŏ	35:45 PM - Peak 1 of 1	l of l																	Peak Hour Analy
Peak Hour for Entire Intersection I	Entire	Intersec	tion Be	gins at C	ns at 04:00 PM	7																Peak Hour fo
04:00 PM	0	90	0	0	90	0	-	0	0	-	0	00	0	0	90	0	0	0	0	0	17	05:00 P
04:15 PM	0	7	0	0	2	0	0	0	0	0	0	9	0	0	9	0	0	0	0	0	00	05:15 PM
04:30 PM	0	2	0	0	2	-	0	0	0	-	0	00	0	0	00	0	0	0	0	0	11	05:30 PM
04:45 PM	0	60	0	0	3	0	0	-	0	1	0	2	-	0	9	0	0	0	0	0	10	05:45 PM
Total Volume	0	15	0	0	15	-	1	1	0	3	0	27	1	0	28	0	0	0	0	0	46	Total Volume
% App. Total	0	100	0	0		333	33.3 33.3	33.3	0		0	96.4	3.6	0		0	0	0	0			% Am. Total
BHIG	000	469	469 000 000	000	050 050 097	050	050		000	050	000	844 250	056	000	875 000	000	000 000	000	000	000	476	d

N/S. Massachusetts Avenue E/W: Bebridere Street/ Haviland Street City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 BB Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Massachusetts Avenue E/W: Belvidere Street/ Haviland Street City, State: Boston, MA Client VHB/ M. Houdlette



File Name : 133307 BB Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

		Massaci	Massachuseffs A verue From North	werne h			Bel	Belvidere Street From East	100			Massel	Massachusetts Averne From South	ome ,	Ī		Fig	From West	×		
Start Time	Right	Thru		Left U-Tum	App. Total	Right	Thru	Left	Urben	Ago, Total	Right	That	Left	U-Tum	Ago, Tiesi	Right	Thru	Left	U-Tuen	Age, Total	Int. Total
eak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of	is From	M 0040	10 0 5:45	PM - Pea	t lof 1																
eak Hour for	Entire	Intersec	tion Be	gins at	ntersection Begins at 04:30 PM	×															
04:30 PM	1	176	0	0	177	16	10	4	0	30	0	159	2	-	162	0	0	0	0	0	369
04:45 PM	7	178	0	0	182	91	m	-	0	20	0	149	7	0	151	0	0	0	0	0	353
05:00 PM	4	165	0	0	169	18	1	4	0	29	0	10	9	0	170	0	0	0	0	0	368
05:15 PM	2	163	0	0	165	10	12	4	0	26	0	158	4	0	162	0	0	0	0	0	353
Total Volume	11	682	0	0	663	09	32	13	0	105	0	630	14	1	645	0	0	0	0	0	1443
% App. Total	1.6	98.4	0	0	1	57.1	30.5	12.4	0		0	7.76	2.2	0.2		0	0	0	0		
PHF	889	856	000	000	.952	.833	199	.813	000	875	000	096	583	.250	646	000	000	000	000	000	876.
Cars	Ξ	654	0	0	999	57	32	12	0	101	0	165	13	-	909	0	0	0	0	0	1371
% Cars	100	686	0	0	0.96	95.0	100	92.3	0	96.2	0	93.8	929	100	93.8	0	0	0	0	0	95.0
Seary Vehicles	0	15	0	0	15	e	0	-	0	4	0	18	-	0	16	0	0	0	0	0	38
N. Honry Vehicles	0	22	0	0	2.2	2.0	0	7.7	0	3.8	0	5.9	7.1	0	2.9	0	0	0	0	0	2.6
Buses	0	13	0	0	13	0	0	0	0	0	0	21	0	0	21	0	0	0	0	0	34
% Buses	0	1.9	0	0	1.9	0	0	0	0	0	0	33	0	0	33	0	0	c	0	0	2.4

261 278 278 237 260 1036 319 331 340 326 1316

161 182 170 170 662

8 2 2 2 2

28882

F 8 8 5 8

84708

28 38 27 27 28 38 8

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

99.8 000 000

0.75 39.9

145 59.7 6.2

S61 23.9 0.5 000 3 0.5

108 35.1 4.6 0.3

194 1.6

Grand Total Appreh % Total %

Peds 135 160 136 134 565

75 39 55 72 741

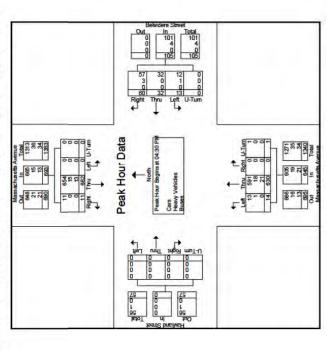
20ds 14 15 15 15 8 8

3 2 8 2 8

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

Right

Groups Printed-Peds and Bicycles Betvidere Street
Massact



	Massichasetts Avenue From North			Belvid	Belvidere Street From East	*			Massachusets Avenue From South	Schusotts Ave From South	venue			Har	Haviand Street From West	1990		
20	× ×	Town R	ingle	Chen	Leff	eds	Age. Desi	Right	Thru	Left	Peds	Ages, Total	Right	Then	Leff	Peds	Age. Desi	Int. Total
PM - Peak I		of 1																
s at 05		05:00 PM																
0		46	0	0	0	11	11	0	19	0	13	32	0	0	0	191		319
4		25	0	4	0	86	8	0	50	0	=	40	0	0	0	149		331
1		45	0	0	0	78	78	0	23	0	12	35	0	0	0	182		340
6		41	-		0	20	81	0	20	0	14	34	0	0	0	170		326
09		187	_	5	0	320	326	0	16	0	80	141	0	0	0	662	662	1316
			0.3	1.5	0	8.2		0	64.5	0	35.5		0	0	0	100		
		000		212	000	000	200	550	204	8	000	100	www	www	www	000	000	070



N/S: Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client: VHB/M. Houdlette

File Name: 133397 C Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

294 293 314 316 1217

157 | 158 | 163 | 167 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 | 164 |

Groups Printed-Cans - Heavy Vehicles - Buses
St. German Street
From East
Left
Left

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

00000

00000

139 165 165 610

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

2486

0.2

000

53.8 85.7

000

Grand Total Appreh % Total %

1172 100 1004 89.1 83 83 31 31 2.6

Cars
% Cars
Heavy Vehicles
% Heavy Vehicles
Buses
% Buses

N/S: Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client VHB/ M. Houdlette

File Name : 133307 C Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

Sheri Time Premisers Avenue St. Germain Steece Absacheers Avenue Absacheers Avenue Premisers Premise					Groups Printed-Cars	ed-Cars					
1760 Left V-Tum Right Left V-Tum Right Thm Thm V-Tum Right Thm Thm Thm V-Tum Right Thm Thm		Massach	om North		St. Ge	rmain Street rom East		Massact	om South		
126 0 0 0 2 0 0 131 131 132 132 132 133 134	Start Time	⊢	Left	U-Tum	L	Left	U-Turn	Н	Thru	U-Turn	Int. Total
117 128 129	07:00 AM	126	0	0	0	2	0	0	131	0	259
129	07:15 AM	117	0	0	0	1	0	0	138	0	256
133	07:30 AM	129	0	0	I	2	0	0	141	0	273
100 30 3 6 0 553 10 145 115	07:45 AM	133	0	0	2	1	0	0	143	. 1	280
124	Total	205	0	0	3	9	0	0	553	1	1068
124	08:00 AM	125	0	0	0	0	0	0	145	0	270
149	08:15 AM	124	0	0	-	0	0	0	149	0	274
141 0 0 0 129 159 0 0 0 3 0 0 0 139 104 0 0 50 50 0 0 139 475 0 0 03 03 03 0 0 599	08:30 AM	149	0	0	1	0	0	0	163	0	313
539	08:45 AM	141	0	0	1	0	0	0	129	0	271
104 0 0 6 6 0 1139 100 0 0 03 50 0 0 99.9 47.5 0 0 03 03 03 0 51.9	Total	539	0	0	3	0	0	0	586	0	1128
100 0 0 50 50 0 0 99,9 47,5 0 0 0,3 0,3 0,3 0 51,9	Grand Total	1044	0	0	9	9	0	0	1139	1	2196
47.5 0 0 0.3 0.3 0 0 51.9	Appreh %	100	0	0	20	20	0	0	6'66	0.1	
	Total %	47.5	0	0	0.3	0.3	0	0	51.9	0	

		Massachusetts Avenue From North	s Avenue			St. Germain Street From East	n Street East			Massachusetts Avenue From South	huseits Avenue rom South		
SartTime	Thro	Leg	U-Tum	App. Total	Right	Left	U-Tum	Are. Total	Right	Thru	UrTurn	Are. Total	Int. Total
eak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1	7:00 AM to 08:	45 AM - Per	de lof1										
eak Hour for Entire Ir	ntersection B	Begins at 07:45 AM	7:45 AM										
07:45 AM	133	0	0	133	2	-	0	3	0	143	1	144	280
08:00 AM	125	0	0	125	0	0	0	0	0	145	0	145	270
08:15 AM	124	0	0	124	,	0	0	-	0	149	0	149	274
08:30 AM	149	0	0	149	,	0	0	-	0	163	0	163	313
Total Volume	531	0	0	531	4	-	0	5	0	009	-	109	1137
% App. Total	100	0	0	3	80	20	0		0	8.66	0.2		
PHF	801	000	000	108	200	050	000	417	000	000	250	600	806

		Massachusetts Avenue	's Avenue			St. Germain Street	n Street			Massachusetts Averna	th Avenue			08:00 AM	125	0	
		From	From North			From East	East		l	From	From South			08:15 AM	124	0	
Start Time	Than		Left U-Tum	App. Total	Right	Left	U-Tum	App. Total	Right	Thru	U-Tum	App. Total	Int. Total	08:30 AM	149	0	J
Peak Hour Analysis From 0700 AM to 0845 AM - Peak 1 of 1	7300 AM to 0	845 AM - Pe	ak 1 of 1											Total Volume	531	0	
Peak Hour for Entire Intersection	ntersection	Begins at 07:45 AM	7:45 AM											% App, Total	100	0	
07:45 AM	145	0	0	145	7	-	0	3	0	167	-	168	316	PHF	168	000	- 1
08:00 AM	142	0	0	142	0	0	0	0	0	163	0	163	305				
08:15 AM	139	0	0	139	7	0	0	2	0	162	1	163	304				
08:30 AM	164	0	0	164	1	0	0	1	0	179	0	179	344				
Total Volume	290	0	0	280	5	1	0	9	0	11.9	2	673	1269				
% App. Total	100	0	0		833	16.7	0		0	266	0.3						
PHF	868	000	000	899	.625	.150	000	.500	000	937	.500	.940	.922				
Cars	531	0	0	531	4	1	0	5	0	009	1	109	1137				
% Cars	0.06	0	0	0.06	80.0	00	0	83.3	0	89.4	50.0	89.3	9'68				
Heavy Vehicles	44	0	0	44	-	0	0	-	0	55	+	26	101				
% Heavy Vehicles	7.5	0	0	7.5	20.0	0	0	16.7	0	8.2	20.0	8.3	8.0				
Buses	15	0	0	15	0	0	0	0	0	16	0	16	31				
% Buses	36	C	0	25	0	0	0	0	c	2.4	0	2.4	2.4				



N/S: Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client: VHB/M. Houdlette

Groups Printed-Heavy Vehicles St. Germain Street From East

2 4 4 8 E4

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

File Name : 133307 C Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

Client VHB/ M. Houdlette N/S: Massachuse E: St. Germain S City, State: Bosto

9			
usetts Avenu	Street	ston, MA	M Umdlott

₽ P	PRECISION	DATA	INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 01503 Office-508:481.3999 Fax: 508.5451234

Boston, MA	main Street e: Boston, MA			D A T A INDUSTRIES, LLC P.O. Box 301 Berlin, MA 01503	D A T A INDUSTRIES, LLC 0x 301 Berlin, MA 01503			Site	e Code :	Site Code : 10135.00 Start Date : 5/14/2013
HB/ M. Houdlette	dlette		8	Office-508.481.3999 Fax: 508.545.1234 Email: desurequest@pdillccom Grouns Printed-Buses	Ppdilccom Ppdilccom			Pag	Page No :	-
	Massach	Massachusetts Avenue From North		St. Gen	St. Germain Street From East		Massach	Massachusetts Avenue From South		
Start Time	Thru	Left	U-Tum	Right	Left	U-Turn	Right	Thru	U-Tum	Int. Total
07:00 AM	2	0	0	0	0	0	0	5	0	7
07:15 AM	n	0	0	0	0	0	0	4	0	8
07:30 AM	S	0	0	0	0	0	0	4	0	6
07:45 AM	4	0	0	0	0	0	0	3	0	7
Total	14	0	0	0	0	0	0	14	0	28
08:00 AM	4	0	0	0	0	0	0	8	0	6
08:15 AM	3	0	0	0	0	0	0	3	0	9
08:30 AM	4	0	0	0	0	0	0	S	0	6
08:45 AM	9	0	0	0	0	0	0	9	0	12
Total	17	0	0	0	0	0	0	19	0	36
Grand Total	31	0	0	0	0	0	0	33	0	3
Appreh %	100	0	0	0	0	0	0	100	0	
Total %	48.4	0	0	0	0	0	0	51.6	0	

E 5 = 5 &

00000

00000

£121 88 7 7 82.9 42.9 42.9

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

127

000

100 4

000

000

Grand Total Appreh % Total %

		Massachusetts Avenue From North	husets Avenue from North			St. German Street From East	Street			Massachusetts Avenue From South	s Avenue		
StartTime	Thru	Leg	U-Turn	App. Total	Right	Left	U-Turn	Are. Total	Right	Thru	UrTurn	Are. Total	Int. Total
Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1	97:00 AM to 08	45 AM - Pe	nk lof!										
Peak Hour for Entire Intersection Begins at 08:00 AM	Intersection	Begins at (38:00 AM										
08:00 AM	4	0	0	4	0	0	0	0	0	8	0	S	6
08:15 AM	m	0	0	3	0	0	0	0	0	3	0	6	9
08:30 AM	4	0	0	4	0	0	0	0	0	v	0	2	6
08:45 AM	9	0	0	9	0	0	0	0	0	9	0	9	12
Total Volume	17	0	0	17	0	0	0	0	0	61	0	61	36
% App. Total	100	0	0		0	0	0	1	0	100	0	3	
PHF	802	000	000	.708	000	000	000	000	000	792	000	792	750

	2	Massachusetts Avenue From North	nusetts Avenue			St. Germain Street From East	in Street			Massachusetts Avenue From South	South South		
Start Time	That	Left	U-Tum	App. Total	Right	Left	U-Turn	App. Total	Right	Then	U-Tam	App. Total	Int. Total
cak Hour Analysis From 07:00		AM to 08:45 AM - Peak of 1	ak l of 1										
eak Hour for Entire Is	ntersection B.	egins at 0	07:00 AM									1	
07:00 AM	7	0	0	7	0	0	0	0	0	21	0	21	28
07:15 AM	14	0	0	14	0	0	0	0	0	18	0	18	32
0730 AM	14	0	0	14	0	0	0	0	0	18	0	18	32
07:45 AM	80	0	0	00	0	0	0	0	0	21	0	21	29
Total Volume	43	0	0	43	0	0	0	0	0	78	0	78	121
% App. Total	100	0	0		0	0	0		0	100	0		
PHF	768	000	000	376	000	900	000	000	000	000	000	000	946

PRECISION
DATA
NODSTRIES,LLC
NO.000-010000
PROCESSER 132000
FOR CONTROL OF THE PROCESSER 1320000
FOR CONTROL OF T

N/S: Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client: VHB/M. Houdlette

Groups Printed-Peds and Bicycles St. Germain Street From East

File Name : 133307 C Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Massachusetts Avenue	E: St. Germain Street	City, State: Boston, MA	Client: VHB/ M. Houdlette

File Name : 133307 C Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

		Massachus etts Avenue From North	la Avenue North			St. German Street From East	in Street			Manageina etta Avanue From South	Is Avenue South		
Start Time	Thru	Lef	U-Turn	App. Total	Right	Treff	U-Turn	App. Total	Right	Thru	UrTurn	App. Total	Int. Total
eak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1	7:00 AM to 08	45 AM - Pa	ak lof!					7					
eak Hour for Entire Intersection Begins at 07:45 AM	ntersection I	Begins at 0	7:45 AM										
07:45 AM	145	0	0	145	*	-	0	3	0	167	-	168	316
08:00 AM	142	0	0	142	0	0	0	0	0	163	0	163	305
08:15 AM	139	0	0	139	7	0	0	2	0	162	-	163	304
08:30 AM	164	0	0	164	•	0	0	-	0	179	0	179	344
Total Volume	890	0	0	968	S	1	0	9	0	1129	2	673	1269
% App. Total	100	0	0		83.3	16.7	0		0	7.66	0.3		
PHF	668	000	000	668	.625	.250	000	.500	000	.937	200	940	922
Cars	531	0	0	531	4	1	0	5	0	009	-	109	1137
% Cars	0.06	0	0	0.06	80.0	100	0	83.3	0	89.4	20.0	89.3	9.68
Heavy Vehicles	4	0	0	4	1	0	0	1	0	55	-	26	101
% Heavy Vehicles	7.5	0	0	7.5	20.0	0	0	16.7	0	8.2	20.0	83	8.0
Buses	15	0	0	15	0	0	0	0	0	16	0	91	31
% Buses	2.5	0	0	2.5	0	0	0	0	0	2.4	0	2.4	2.4

1224

22 32 32 36 36 36 40 40 46 46

0 0 0 - 4

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

0 0 2 L E 0 0 7.1

19 23 27 19 88 128 92.8

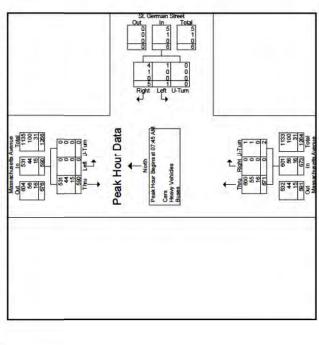
100

23

000

167

Grand Total Approch % Total %



		Massachusett	s Avenue lorth			St. Germain Street From East	Street			Massachusett From S	s Avenue		
Start Time	Thau	Left	Peds	Ann. Total	Right	Left	Peds	App. Total	Right	Then	Reds	App. Total	Int. Total
Hour Analysis From 0	17:00 AM to 08.	MS AM - Peak I of I	k l of 1										
Peak Hour for Entire Is	intersection E	Begins at 01	8:00 AM										
08:00 AM	20	0	0	20	0	0	9	9	0	19	0	16	20
08:15 AM	26	0	*	29	0	0	35	35	0	23	0	23	87
08:30 AM	31	0	0	31	0	0	45	45	0	77	7	29	105
08:45 AM	35	0	-	36	0	0	46	46	0	19	-	20	102
Total Volume	112	0	4	116	0	0	991	991	0	88	3	16	373
% App. Total	9.96	0	3.4	7	0	0	100		0	296.7	3.3		
SHd	800	000	333	808	000	000	600	000	000	818	375	784	888



N/S: Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client: VHB/M. Houdlette

Groups Printed-Casa - Heavy Vehides - Bases
St. German Street
From East
Left
Left

File Name: 133307 CC Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S: Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133397 CC Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

	Massach	Massachus etts Avenue From North		St. Ge	St. Germain Street From East		Massack	Massachusetts Avenue From South		
Start Time	Thru	Left	U-Tum	Right	Left	U-Tum	Right	Thru	U-Tum	Int. Total
04:00 PM	159	0	1	2	1	0	0	119	1	283
04:15 PM	147	0	0	1	61	0	0	124	0	274
04:30 PM	172	0	1	0	1	0	0	150	0	324
04:45 PM	176	0	0	2	61	0	0	142	1	323
Total	654	0	2	\$	9	0	0	535	2	1204
05:00 PM	163	0	0	-	1	0	0	201	0	329
05:15 PM	157	0	0	0	1	0	0	149	0	307
05:30 PM	159	0	0	2	-	0	0	157	0	319
05:45 PM	149	0	0	0	4	0	0	191	0	314
Total	628	0	0	3	7	0	0	631	0	1269
Grand Total	1282	0	7	00	13	0	0	1166	2	2473
Appreh %	8.66	0	0.2	38.1	619	0	0	8.66	0.2	
Total %	51.8	0	0.1	0.3	0.5	0	0	47.1	0.1	

349 323 333 1337 2614

| Prom South | Pro

00000

00000

173 165 156 156

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

000

00000000

2000000

1342 99.9 95.5 35 26 26 27 1.9

Cars
% Cais
Heavy Vehicles
% Heavy Vehicles
Buses
% Buses

15 65.2 0.6 13 86.7

8 8 60

000

Grand Total Appreh % Total %

		Massachusetts Avenue From North	husets Avenue from North			St. Germain Street From East	ormain Street			Massichusetts Averue From South	fram South		
Start Time	Thru	Lef	U-Tum	App. Total	Right	Left	U-Tum	Ann. Total	Right	Thru	U-Turn	App. Total	Int. Total
Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	04:00 PM to 05x	45 PM - Peu	k lof!										
Peak Hour for Entire Intersection	=	Begins at 04:30 PM	M:30 PM										
04:30 PM	172	0	1	173	0	-	0	1	0	150	0	150	324
04:45 PM	176	0	0	176	7	7	0	4	0	142	-	143	323
05:00 PM	163	0	0	163	1	1	0	5	0	164	0	191	329
05:15 PM	157	0	0	157	0	-	0	1	0	149	0	149	307
Total Volume	899	0	,	699	3	5	0	8	0	909	1	909	1283
% App. Total	666	0	0.1		37.5	62.5	0		0	8.66	0.2		
PHF	676	000	056	050	375	369	000	COOS	000	660	050	0.04	940

343 337 349 323 1352

St. Germain Street
From East
Left U-Turn App. Total

368 36 37 37 33 33 2.7

3.0 2.8 2.8 2.0 3.0 3.0 3.0

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| New York | New York



N/S: Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client: VHB/M. Houdlette

File Name: 133397 CC Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

Groups Printed-Heavy Vehicles St. Germain Street From East Right Left

Sart Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

N/S: Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client VHB/ M. Houdlette



Massachusetts Avenue	Germain Street	State: Boston, MA	the same of the same

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File Name: 133397 CC Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

				Course Lineary Disease	COLUMN TO A STATE OF THE PARTY					
	Massach	Massachusotts Avenue From North		St. Gen	St. Germain Street From East		Massach	Massachusetts Avenue From South		
Start Time	Thru	Left	U-Tum	Right	Left	U-Turn	Right	Thru	U-Tum	Int. Total
04:00 PM	1	0	0	0	0	0	0	5	0	
04:15 PM	4	0	0	0	0	0	0	9	0	ĭ
04:30 PM	m	0	0	0	0	0	0	3	0	-
04:45 PM	2	0	0	0	0	0	0	3	0	
Total	10	0	0	0	0	0	0	17	0	77
05:00 PM	5	0	0	0	0	0	0	00	0	1
05:15 PM	4	0	0	0	0	0	0	5	0	
05:30 PM	4	0	0	0	0	0	0	4	0	
05:45 PM	2	0	0	0	0	0	0	9	0	
Total	15	0	0	0	0	0	0	23	0	38
Grand Total	25	0	0	0	0	0	0	40	0	65
Appreh %	100	0	0	0	0	0	0	100	0	
Total %	38.5	0	0	0	0	0	0	61.5	0	

		Massachusetts From N	fassachusetts Avenue From North			St. Germain Street From East	rmain Street rom East			Massichusetts Av From South	Sachasetts Avenue From South		
Start Time	Thru	Lef	U-Turn	App. Total	Right	Left	U-Tum	Arro. Total	Right	Thru	U-Turn	Age. Total	Int. Total
Peak Hour Aradysis From 04:00 PM to 05:45 PM - Peak 1 of 1	om 04:00 PM to	0545 PM - Pe	sak lof!										
Peak Hour for Entire Intersection Begins at 05:00 PM	re Intersection	n Begins at	05:00 PM										
05:00 PM	. S	0	0	v	0	0	0	0	0	00	0	8	1
05:15 PM	4	0	0	4	0	0	0	0	0	2	0	5	-
05:30 PM	4	0	0	4	0	0	0	0	0	4	0	4	
05:45 PM	4 2	0	0	2	0	0	0	0	0	9	0	9	
Total Volume	15	0	0	15	0	0	0	0	0	23	0	23	3
% App. Tota	100	0	0		0	0	0		0	100	0		
PHF	750	000	000	052	000	000	000	000	000	710	000	710	73

		Massachusetts Avenue From North	s Avenue			St. Germain Street From East	Street			Massachusetts Avenue From South	South	Ī	
Start Time	That	Left	U-Tum	App. Total	Right	Teff	U-Turn	App. Total	Right	Thru	U-Tam	App. Total	Int. Total
cak Hour Analysis From (Analysis From 04:00 PM to 05:45 PM - Peak 1 of	45 PM - Peal	cl of l										
eak Hour for Entire Intersection Begins at	Intersection	legins at 0.	4:00 PM										
04:00 PM	6	0	0	6	0	0	0	0	0	10	0	10	19
04:15 PM	-	0	0	1	0	0	0	0	0	4	0	4	S
0430PM	6	0	0	3	0	-	0	1	0	6	0	6	13
04:45 PM	4	0	0	4	0	-	0	1	0	4	0	4	6
Total Volume	17	0	0	11	0	2	0	2	0	27	0	27	94
% App. Total	100	0	0		0	00	0		0	100	0		
PHF	472	000	000	477	000	003	000	005	000	513	900	513	309

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05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

N/S. Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client: VHB/M. Houdlette

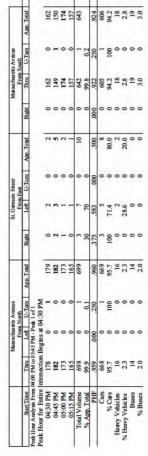
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Groups Printed-Peds and Bicycles St. Germain Street

File Name : 133307 CC Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S. Massachusetts Avenue E: St. Germain Street City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 CC Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1



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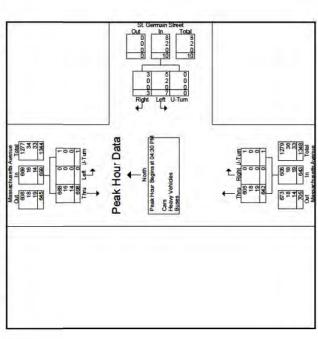
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		Massachusens Avenue	s Avenue			St. Germain Street	n Street			Massachusetts Avenue	s Avenue		
		From North	COLD			From East	180			From South	(E)(C)		
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Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	04:00 PM to 05:	45 PM - Peak	kl of 1										
ak Hour for Entire 1	Intersection	Begins at 0.	S:00 PM										
05:00 PM 30 0 2	30	0	N	32	0	0	11	4	0	19	2	21	130
05:15 PM	36	0	-	40	0	0	28	87	0	25	-	26	153
05:30 PM	38	0	40	43	0	0	92	92	0	24	2	26	191
05:45 PM	22	0	2	24	0	0	88	88	0	24		12	139
Total Volume	129	0	10	139	0	0	344	344	0	35	8	100	583
% App. Total	92.8	0	7.2		0	0	100		0	35	80		
and		OOO	200	808	ww	000	920	320	ww	000	139	900	500



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Gmit clearquesy lept slicks 124 N/S/NW: Massachusetts Ave/ Westland Ave E/W: Christian Science Dr/St. Stephen St

File Name : 133307 D Site Code : 10135.00 Start Date : 5/14/2013 Page No :1

City, State: Boston, MA Client: VHB/ M. Houdlette N/S/NW: Massachus E/W: Christian Science

DRECISION	D A T A	P.O. Box 301 Berlin, MA 01503 Office-508:481,3999 Fox: 506,5451234
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File Name : 133307 D Site Code : 10135.00 Start Date : 5/14/2013

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	*	fassach Fr	Massachusetts Avenue From North	Avenue	-	Ö	histian.	Christian Science Center Driveway From East	Center	1	X	assach Pro	Massachnsets Avenue From South	ven ue			St. Step Fro	St. Stephen Street From West	50			Wester	Wordend Average From Northwest	8 %		
Start	12	Right	Thru	Left	u-bes	Nghi	1 2	Thru	Left	U-Das	Pight	Thru	13	Left	the Character	Mght	Thro	Left	15	to the	11	11	15	15	t-time	Sec Total
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77:15 AM	1	w	103	4	0	-	1	0	0	0	1	136	65	7	0	0	0	0	0	0	6	16	7	0	0	425
7:30 AM	1	4	113	9	0	0	0	0	0	0	-	141	4	-	0	0	0	0	0	0	-	92	-	0	0	446
7:45 AM	6	12	104	2	0	0	0	0	0	0	60	155	92	4	0	0	0	0	0	0	4	75	-	0	0	463
Total	25	25	410	21	0	_	-	0	0	0	21	195	310	14	0	0	0	0	0	0	10	333	S	0	0	1737
08:00 AM	8	9	16	9	0	0	-	0	0	0	8	157	16	1	0	0	0	0	0	0	4	98	2	0	0	467
18:15 AM	7	7	116	4	0	0	0	0	0	0	9	136	75	9	0	0	0	0	0	0	4	8	8	0	0	441
30 AM	4	9	1117	7	0	0	0	0	0	0	10	167	73	N	0	0	0	0	0	0	4	18	8	0	0	477
8:45 AM	7	=	1115	9	0	0	0	0	0	0	=	137	19	7	0	0	0	0	0	0	S	26	4	0	0	461
Total	18	30	445	18	0	0	1	0	0	0	32	265	906	22	0	0	0	0	0	0	17	344	16	0	0	1846
Stand Total	43	55	885		0	_	2	0	0	0	23	8	919	36	0	0	0	0	0	0	12	119	21	0	0	3583
Appreh %	4.3	5.5	862	3.9	0	33.3	66.7	0	0	0	2.8	622	33.1	1.9	0	0	0	0	0	0	3.7	93.4	2.9	0	0	
Total %	1.2	1.5	23.9		0	0	0.1	0	0	0	1.5	323	17.2	-	0	0	0	0	0	0	8.0	18.9	90	0	0	

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Christian Science Center

City, State: Boston, MA Client: VHB/ M. Houdlette

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7:15 AM	es	0	6	0	0	0	0	0	0	0	0	00	6	0	0	0	0	0	0	0	0	0	0	0	0	33
07:30 AM	7	0	14	0	0	0	0	0	0	0	0	17	4	3	0	0	0	0	0	0	0	3	0	0	0	43
7.45 A.M	0	0	9	0	0	0	0	0	0	0	-	23	-	0	0	0	0	0	0	0	-	m	0	0	0	35
Total	9	0	8	0	0	0	0	0	0	0	-	92	17		0	0	0	0	0	0	-	9	0	0	0	139
98:00 AM	7	0	00	0	0	0	0	0	0	0	0	7	-	21	0	0	0	0	0	0	0	2	0	0	0	22
08:15 AM	-	2	00	0	0	0	0	0	0	0	0	6	-	0	0	0	0	0	0	0	0	3	0	-	0	25
38:30 AM	7	0	10	0	0	0	0	0	0	0	0	10	0	0	0	0	0	0	0	0	0	7	0	0	0	24
8:45 AM	-	0	18	0	0	0	0	0	0	0	0	15	2	-	0	0	0	0	0	0	0	0	0	0	0	37
Total	9	2	4	0	0	0	0	0	0	0	0	41	4	0	0	0	0	0	0	0	0	7	0	-	0	108
Grand Total	12	2	78	0	0	0	0	0	0	0	-	1117	16	9	0	0	0	0	0	0	-	13	0	-	0	247
Approb %	13	2.2	848	0	0	0	0	0	0	0	0.7	83.6	11.4	4.3	0	0	0	0	0	0	6.7	6.7	0	6.7	0	
Total %	4.9	8.0	31.6	0	0	0	0	0	0	0	0.4	47.4	6.5	2.4	0	0	0	0	0	0	0.4	5.3	0	0.4	0	

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File Name : 133307 D Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

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File Name : 133307 D Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

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File Name : 133307 D Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

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File Name: 133307 DD Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

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File Name: 133307 DD Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

		Massacl	Massachusetts Avenue From North	on use	1	đ	nistian i	Chiistian Science Center Driveway From East	Center	1	×	Ros	Massachusetts Avenue From South	en ne			St. Step From	St. Stephen Street From West	2			Wesdan From)	Wordend Average From Northwest	9 16		
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04:30 PM	0	0	7	0	0	0	0	0	0	0	0	6	0	0	0	0	0	0	0	0	0	-	0	0	0	9
04:45 PM	0	0	2	0	0	0	0	0	0	0	0	6	2	0	0	0	0	0	0	0	0	2	0	0	0	6
Total	0	0	6	0	0	0	0	0	0	0	0	91	4	0	0	0	0	0	0	0	0	90	0	0	0	37
05:00 PM	0	0	S	0	0	0	0	0	0	0	0	00	7	0	0	0	0	0	0	0	0	0	0	0	0	15
05:15 PM	0	0	4	0	0	0	0	0	0	0	0	9	0	0	0	0	0	0	0	0	0	6	0	0	0	13
05:30 PM	0	0	4	0	0	0	0	0	0	0	0	7	0	0	0	0	0	0	0	0	0	7	0	0	0	00
05:45 PM	0	0	2	0	0	0	0	0	0	0	0	9	0	0	0	0	0	0	0	0	0	0	0	0	0	00
Total	0	0	15	0	0	0	0	0	0	0	0	22	7	0	0	0	0	0	0	0	0	N	0	0	0	4
Grand Total	0	0	24	0	0	0	0	0	0	0	0	38	9	0	0	0	0	0	0	0	0	13	0	0	0	81
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	Start Time		Peak He	01:45 PM	MJ 00:30	05:15 PM	05:30 PM	Total Velicon.	No Age Test	PHI

File Name: 133307 DD Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S/NW: Massachusetts Ave/ Westland Ave E/W: Christian Science Dr/St. Stephen St City, State: Boston, MA Client VHB/ M. Houdlette

)	PRECISION	INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 01 Office-508.481.399 Fac.508.	Email detarequesto0to011c
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File Name: 133307 DD Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

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Start Time 04300 PM 04:15 PM 04:30 PM 04:35 PM Total

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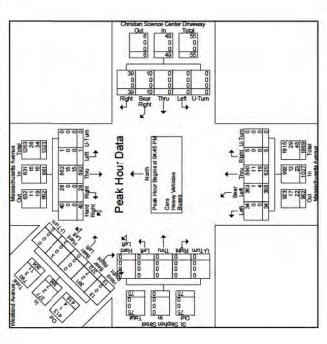
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		Massa	chusets Aw From North	Massachusetts Avenue From North	one			Christian Science Center Driveway From East	Driveway From East	way East	age t		2	nssach Fi	Massachusetts Avenue From South	Avenu			o.	Step	St. Stephen Street From West	ž			F.W	sdand om Ne	Westland Avenue From Northwest			
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N/S: Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

File Name : 133307 E Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette



File Name: 133307 E Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

70	Z	A.	MA 01503
V	RECISION	A T	301 Berlin,
	- 4		P.O. Box

	Ma	Mass achusens A venue From North	Avenue		Huntis	gion Avenue From East	Huntington Avenue (Route 9) From East		Ma	Massachusetts Avenue From South	Avenue		Humin	Hundington Avenue (Route 9)	est (Route 9		
StartTime	Right	Thru	Left	U-Tum	Right	Thru	Left	U-Tum	Right	Thru	Left	U-Tum	Ri ght	Thru	Left	UrTura	Int Total
07:00 AM	22	135	0	0	7	00	=	2	19	187	-	0	19	4	19	0	434
07:15 AM	20	158	0	0	00	9	12	2	13	172	-	0	21	2	18	1	442
07:30 AM	24	173	0	0	00	00	20	2	18	195	0	0	15	0	15	4	482
07:45 AM	12	158	0	0	91	2	14	2	18	218	0	0	6	6	24	4	480
Total	78	624	0	0	39	23	57	00	89	772	2	0	2	12	92	15	1838
08:00 AM	15	171	0	0	18	10	20	m	91	230	0	0	13	-	16	-	520
08:15 AM	17	174	-	0	2.1	00	24	2	16	169	0	0	18	2	25	S	482
08:30 AM	18	180	-	0	18	4	20	9	26	200	0	0	12	0	30	2	514
08:45 AM	26	176	0	0	12	8	11	S	21	176	0	0	6	s	25	00	485
Total	92	707	7	0	69	27	81	13	70	775	0	0	25	90	96	16	2001
Grand Total	154	1331	7	0	108	80	138	21	147	1547	14	0	116	20	172	31	3839
Appreh %	10.4	89.5	0.1	0	7	15.8	43.5	9.9	8.7	91.2	0.1	0	34.2	5.9	50.7	9.1	
Total %	4	34.7	0.1	0	2.8	1.3	3.6	0.5	3.8	40.3	0.1	0	r	0.5	4.5	80	

	In Total		520	482	514	485	2001		796
	Ago Total		31	20	4	47	172	Ī	098
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	App. Thesi		246	185	226	161	854		SYS
venue	U-Tum		0	0	0	0	0	0	000
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Ţ,	App. Total		51	55	45	39	190		864
(Route 9)	UTen		m	7	m	40	13	8.9	059
Avenue rom East	Ive		20	77	20	11	18	42.6	844
mington F	Thru		10	00	4	S	27	14.2	54.9
H	Right	M	18	21	18	12	69	36.3	168
	App Total	t 08:00 AM	192	192	661	202	785		023
venue	U-Tum AM - Pest	gins at	0	0	0	0	0	0	000
rom North	Left to 08:45,	tion Be	0	-	-	0	2	0.3	200
Massack	Thru 77:00 AM	Intersec	177	174	180	176	707	90.1	080
	Right 0	Entire	15	17	18	26	16	1.6	731
	Start Time Peak Hour Analys	Peak Hour for	08:00 AM	08:15 AM	08:30 AM	08:45 AM	Total Volume	% Am. Total	PHF

3839 90.6 290 6.8 108 2.5

191 172 172 191 191 191

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08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

199

Grand Total
Appreh %
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Cars
% Cars
% Cars
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% Busses

		Massac	Massachusetts Avenue From North	on use		H	Huntington Avenue (Route 9) From East	From East	(Rouse 9)			Massad	Massachusetts Averue From South	eme			funithgion Avenue (Route 9) From West	From West	(conte 9)		\neg
Start Time	Right	Thru	Left	Left Urum	Age, Total	Right	Thm	Left	U-Tum	Ago Red	Right	Thra	Left U-Tum		Ago, Your	Right	The	Left	U-Tum	Acr. Total	
r Amily	eak Hour Analysis From 07:00 AM to 08:45 AM - Peak I of I	7:00 AM	80 08 ×45 J	AM - Pea	klofi																
eak Hour for I	Intire	Intersec	tion Be	gins at	Intersection Begins at 08:00 AM	Σ															
08:00 AM	16	193	0	0	209	20	=	22	0	26	18	250	0	0	268	16	7	16	7	36	
18:15 AM	19	193	-	0	213	22	10	22	2	8	18	184	0	0	202	20	7	25	9	8	
08:30 AM	19	195	-	0	215	19	4	20	3	4	28	213	0	0	241	13	-	32	7	8	
08:45 AM	29	661	0	0	228	14	9	17	1	4	24	195	0	0	219	6	9	30	00	23	
Total Volume	83	780	2	0	865	51	31	83	15	204	88	842	0	0	930	88	11	103	18	190	2189
App. Total	9'6	902	0.2	0		36.8	15.2	40.7	7.4		9.5	506	0	0	i	30.5	5.8	542	9.5		- 1
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% Cars	91.6	906	100	0	8.06	920	87.1	9.76	2.98	93.1	8.68	92.0	0	0	8.16	89.7	72.7	93.2	6.88	506	91.4
Heavy Vehicles	5	52	0	0	57	5	4	7	-	12	9	46	0	0	52	9	8	2	7	16	
Sidency Vehicles	0.9	6.7	0	0	9.9	6.7	12.9	2.4	6.7	6.5	8'9	5.5	0	0	5.6	103	27.3	4.9	1.1	8.4	
Buses	2	21	0	0	23	-	0	0	-	N	6	21	0	0	24	0	0	7	0	2	
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N/S: Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 E Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 E Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

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. 2	PREC	A D	P.O. Box 301 B

							Grouns	Groups Printed-Buses	luses.		١						
	Ma	Massachusetts Avenue From North	Avenue		Huntin	Huntington Avenue (Route 9) From East	e (Route 9) st	J	Ma	Massachusetts Averae From South	Avenue		Humin	From West	Humington Avenue (Route 9) From West	6	
StartTime	Right	Thru	Left	U-Tum	Right	Thru	Left	U-Tom	Right	Thru	Left	UrTura	Right	Thro	Left	U-Turn	Int. 1
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07:15 AM	0	4	0	0	0	0	0	0	0	4	0	0	0	0	-	0	
07:30 AM	0	1	0	0	0	-	0	-	0	9	0	0	0	0	-	0	
07:45 AM	0	4	0	0	0	0	0	0	0	8	0	0	-	0	0	0	
Total	0	21	0	0	-	1	0	-	0	59	0	0	7	0	7	0	
08:00 AM	-	1	0	0	0	0	0	0	-	00	0	0	0	0	0	0	
08:15 AM	0	9	0	0	0	0	0	0	0	4	0	0	0	0	0	0	
08:30 AM	1	60	0	0	0	0	0	0	0	4	0	0	0	0	0	0	
08:45 AM	0	8	0	0	-	0	0	-	2	2	0	0	0	0	2	0	
Total	7	21	0	0	-	0	0	1	3	21	0	0	0	0	7	0	
rand Total	7	42	0	0	2		0	7	3	50	0	0	2	0	4	0	
Appreh %	4.5	95.5	0	0	40	20	0	9	5.7	94.3	0	0	33.3	0	66.7	0	
Total %	1.9	38.9	0	0	1.9	6.0	0	1.9	2.8	46.3	0	0	1.9	0	3.7	0	

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08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

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2	Right			1 0	0 0	2 0	0 0	3 0	0	275
funtington Avenue (Route 9) From East	Right Thru Left Urten Age total			0 0	0 0	0 1	0 0	1 0	0 33.3	000
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enne	Left U-Tun App. total	M-Pesk 1 of 1	Peak Hour for Entire Intersection Begins at 07:00 AM	9 0	0 4	0 7	0 4	0 21	0	000 CO
Massachusetts A venue From North	Thru Left U	eak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1	ntersection Beg	0 9	0 4	7 0	4 0	21 0	100 0	750 000
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enae (Route 9)	U-Turn Ago test int. Total	Pea	Pe	2 0 4 37	4 1 5 35	2 0 2 40	2 1 5 41	10 2 16 153	.5 12.5	SAM 900 033
Huntington Avenue (Route 9)	U-Turn Ago test int. Total	Pea	Pe	2 0 2 0 4 37	0 0 4 1 5 35	0 0 2 0 2 40	1 1 2 1 5 41		62 62.5	750 675 500 900 033
	U-Turn Ago test int. Total	Pos	Pe	0 25 2 0 2 0 4 37	0 19 0 0 4 1 5 35	0 19 0 0 2 0 2 40	0 24 1 1 2 1 5 41		62.5	970 375 350 675 500 900 933
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Mustachusetts Avenue From South	U-Turn Ago test int. Total	Pea	Pe	1 0 2 3 22 0 0 25 2 0 2 0 4 37	3 0 3 0 19 0 0 19 0 0 4 1 5 35	1 0 4 0 19 0 0 19 0 0 2 0 2 40	0 1 2 2 22 0 0 24 1 1 2 1 5 41	3 1 10 2 16	9.1 5.7 94.3 0 0 18.8 6.2 6.2.5	250 699 417 037 000 000 076 375 250 625 600 000
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N/S: Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/M. Houdlette

File Name : 133307 E Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette

File Name : 133307 E Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

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Office=508.481.3999 Far Email: desurequesta	ion Avanue (Route 9)

		Massach	Assechasetts Averne From North	werne	1	H	and implican	Avenue	untington Avenue (Route 9) From East			Massaci	Massachusetts Avenue From South	vernie		H	Integion	From West	funtington Avenue (Route 9)		
Start Time	Right	Thru	Left	9	Area Total	Right	Thru	Left	Urben	Age, Total	Right	Tha	Left	U-Tum	Ago, Tiesi	Right	Three	Leg	U-Tuen	Age. Total	Int. Total
eak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of	is From (7500 AM	10 08545	AM-Pea	k lof 1																
eak Hour for	Entire		tion Be	Intersection Begins at	08:00 A	M															
08:00 AM	16	193	0	0	500	20	=	22	m	26	18	250	0	0	897	16	7	16	7	36	269
08:15 AM	19	193	-	0	213	22	10	24	7	28	18	184	0	0	202	20	61	25	9	53	526
08:30 AM	19	195	1	0	215	19	4	20	m	94	28	213	0	0	241	13	-	32	2	48	550
08:45 AM	50	661	0	0	228	14	9	17	7	4	24	195	0	0	219	6	9	30	00	23	24
Total Volume	83	780	23	0	865	75	31	83	15	204	88	842	0	0	930	58	11	103	18	190	2189
% App. Total	9.6	90.2	0.2	0		36.8	15.2	40.7	7.4		9.5	90.5	0	0		30.5	5.8	54.2	9.5		
PHF	.716	086	.500	000	.948	.852	705	865	536	8.79	282	.842	000	000	898	725	458	805	.563	968.	.962
Cars	16	707	2	0	785	69	27	81	13	190	20	775	0	0	854	52	8	96	16	172	2001
% Cars	916	906	100	0	806	92.0	87.1	9.76	1.98	93.1	868	92.0	0	0	8.16	89.7	72.7	93.2	688	90.5	91.4
leavy Vehicles	S	52	0	0	57	S	4	7	-	12	9	46	0	0	52	9	3	2	cı	91	137
S.H.m.ry Vehides	0.9	6.7	0	0	9.9	6.7	129	2.4	6.7	8.9	8.9	5.5	0	0	5.6	10.3	27.3	4.9	11.1	8.4	6.3
Buses	C	21	0	0	23	-	0	0	-	2	6	21	0	0	24	0	0	2	0	61	51
% Buses	2.4	2.7	0	0	27		0	0	67	1.0	3.4	36	0	0	2.6	0	0	0	0	1.1	23

139 1139 1139 1163 1185 247 282 282 333 336 1188

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20 11 6

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

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Grand Total Appreh % Total %

Peds 46 75 79 52 52 252

Peds 10 11 12 80

24 28 26 43 121

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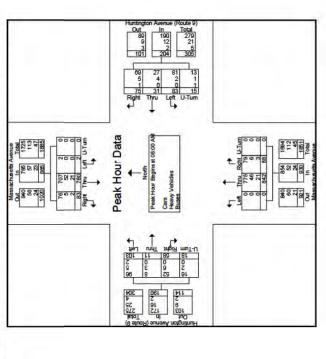
27 23 8

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

Right

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Groups Printed-Peds and Bicycles erue (Route 9) Massach



		Massac	Massachuseuts A. From Nort	wenue		_	Huntington Avenue (Route 9)	Prom East	(Route 9	(Massac	Massachusetts Avenue From South	wenue		2	untington	A venue	Huntington A venue (Route 9) From West		
Start Time	Right	The	Left	Peds	Age. Total	Right	The	Leg	Peds	Are. Des	Right	Thru	Left	Peds	Ages Total	Right	Thro	Left	Peds	Age, Desi	Int. Total
onk Hour Analys	sis From 07:00 AA	7:00 AM	to 08:45	AM - Pes	ik lof!																
ak Hour for	Entire	Intersec	tion B	egins at	08:00 A	W															
08:00 AM	0	6	0	33		0	0	0	9	8	0	12	0	=	23	0	7	11	118	122	247
98:15 AM	-	14	0	4		0	0	0	17	77	0	19	0	13		0	7	-	119	122	282
08:30 AM	-	91	0	39		0	-	0	55	98	0	13	0	10		-	3	m	189	861	333
08:45 AM	0	20	0	80		0	-	0	63	3	0	23	-	14	- 1	0	e	0	142	145	326
otal Volume	2	89	0	172	233	0	2	0	250	252	0	19	-	48	М		10	00	898	587	1188
% App. Total	6.0	253	0	73.8		0	8.0	0	99.2		0	87.8	6.0	41.4		0.2	1.7	1.4	8.96		
DITE	0000	200	5000	000		2000	000		2000						-			,			



N/S. Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 EE Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette



File Name: 133307 EE Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

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e (Route 9	9	TOT	16	20	24	21	81	23	19	15	21	20
Hundington Avenue (Route 9)	The state of	T CELO	1	1	6	10	27	9	S	4	00	22
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i		C-I mu	0	0	0	0	0	0	0	0	0	9
Avenue		Terr	0	0	0	1	1	0	0	0	0	9
Massachusetts Avenue From South	The state of	TDU	171	178	167	174	069	201	504	218	203	900
Mas	77.74	KIER	6	18	13	4	4	19	16	17	16	14
		- Lum	9	0	1	9	28	11	-	9	7	2.1
e (Route 9	11	Tell	16	19	36	19	06	24	32	26	36	110
Huntington Avenue (Route 9)		TIME I	S	00	14	10	37	2	S	18	1	35
Hunting	1000	Kight	15	91	91	22	69	18	17	21	19	36
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	Ago, Total			63	¥	8	55	212		841
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furtington A	Thru		. A	0	2	4	80	23	10.8	219
8	Right		-	28	56	17	22	63	43.9	830
	Ago, Trest		-	220	223	235	219	897		954
eme /	U-Turn		4	0	0	0	0	0	0	000
Assachusetts Averae From South	Lef		4	0	0	0	0	0	0	000
Massach	Thm			201	504	218	203	826	92.1	047
	Right			19	19	11	91	11	7.9	934
SEE	App. Total			28	19	7.1	69	259	-	912
Iuntington Avenue (Route 9) From East	Urven			=	-	9	7	31	12	202
Avenue rom East	Len			24	32	56	36	118	45.6	819
ming ton	Thru			0	v	18	7	35	13.5	486
H	Right		N	×	17	21	10	75	50	863
	App. Total	lofi	0.00	77	232	208	204	865		932
90000	U-Tum	M - Peak	gms ar c	0	0	0	0	0	0	000
Aussichusetts Averue From North	Left	10 0 5 345 P	non Bei	0	0	-	0	-	0.1	050
Massach	Then	4:00 PM	niersoc	200	213	186	184	789	91.2	900
	Right	is From 0	- mure	15	19	21	20	75	8.7	803
	StartTime	eak Hour Analys	eak Hour for	00:00 PM	05:15 PM	05:30 PM	05:45 PM	Total Volume	% App. Total	PHF

ient: VHB/ M. Houdlette	M.H	oudlett	o			_	Email data	ce-508.481.3999 Fac. 508.545. Emait detarequests@pdillccom	pdiliccom	4	
							Grou	Groups Printed-Cars	Cars		
	M	Massachusetts Avenue	Avenue		Huntir	Huntington Avenue (Route 9)	ue (Route 9	0		Massachusetts Avenue	Avenue
Start Time	Richt	Thru	F .	U-Tum	Right	Thru	Left	L-Tue	Riolit	Thru	Left
04:00 PM	36	186	-	0	115	s	16	9	6	171	0
04:15 PM	25	961	-	0	91	00	19	6	18	178	0
04:30 PM	=	3	0	0	16	14	36	1	13	167	0
04:45 PM	28	205	-	0	22	10	19	9	4	174	i.
Total	8	781	3	0	69	37	06	28	4	069	-
05:00 PM	15	206	0	0	18	8	24	=	16	201	0
05:15 PM	19	213	0	0	17	5	32	-	16	204	0
05:30 PM	21	186	-	0	21	18	26	9	17	218	0
05:45 PM	20	18	0	0	10	1	36	7	16	203	0
Total	75	789	-	0	7.5	35	118	31	17	826	0
Grand Total	165	1570	4	0	4	22	208	89	115	1516	-
Appreh %	9.5	90.3	0.2	0	29.8	14.9	43.1	12.2	-	92.9	0.1
Total %	3.9	36.6	0.1	0	3.4	1.7	4.9	4.1	2.7	35.4	0

505 508 548 538 564 2155

82225

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17 6 21 12 38 7 20 11 96 36

Right 17 16 16 17 17 17

From No. 197 203 200 212 812

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

586 596 574 571

82528

203 211 223 212 855

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214 222 197 191 824

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

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37.5 3.7 3.7 159

43.3 43.3 97.4 000

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Huntington Avenue (Route 9)

| Saut Time | Salat | Time | Time | Managera Avenue | Avenue | Managera Managera |
3585 354 354 36 36 39 39 25 25

117 6.9 2.6 115 98.3

151 28 44 48 95 4 000

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1636 90.3 36.5 1570 1570 33 2

Crand Total
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42.7

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0.7			Age Toni			63	¥	40	55	212		.841					
3.7		(Route 9	U-Tuen			9	4	4	4	18	8.5	.750					
2		Huntington Avenue (Route 9) From West	Tirry Left Urten Accress Right Thus Left Urten Accress Right Thru Left Urten			23	19	15	21	78	36.8	.848					
		furning to	Thru			9	2	4	80	23	10.8	617.					
4.4		_	Right			28	26	17	22	93	43.9	830					
0			Age. Then			220	223	235	219	897		954					
0		verse	U-Tum			0	0	0	0	0	0	000					
4.0		Massachusetts Avenue From South	Lef			0	0	0	0	0	0	000					
4.9 1.4 2.7 35.4		Massac	The			201	504	218	203	826	92.1	.947					
-			Right			19	19	17	16	11	7.9	934					
4			Age, You			58	61	7.1	69	259		912					
6.4		Huntington Avenue (Route 9) From East	U.Tven			=	-	9	7	31	12	302					
1.7		From East	Len			24	32	56	36	118	45.6	618					
0 3.4 1.7		unting ton	Thru			2	S	18	7	35	13.5	486					
-		H	Right		×	18	17	21	61	75	53	.893					
			Start Time Right Thru Left U-Tun Ano Total	lofi	5:00 P	221	232	208	204	865		.932					
0.1		9000	U-Tuen	Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of	gins at (0	0	0	0	0	0	000					
		Massachusetts Avenue From North	Left	00545 P	ion Beg	0	0	-	0	-	0.1	250					
Total % 3.9 36.6		Massach	Theo	100 PM	ntersec	206	213	186	184	789	91.2	926					
-			Right	From 04	Entire L	15	19	21	20	75	8.7	893					
Total		П	Time	Ambais	our for	PM	PM.	PM	PM.	otal Volume	Total	PHF					
		L	Start	Peak Hou	Peak Hour for Entire Intersection Begins at 05:00 PM	05:00 PM	05:15 PN	05:30 PM	05:45 PN	V lend V	% App. Total						
T 1																	
4284	2.1	105	-				_		Acc Total Right Thm Left U-Turn Acc Total Int Total			586	965	574	571	2327	
32 7	- m	00	,						Ace. Treat			8	58	42	28	223	
3.7 159 94.6	w w	4 4					10	(ROUNE 9)	U-Tum			9	5	4	4	19	
	2	00						From West	Left			25	21	91	23	85	
94.3	8						1	From West	The			9	8	4	90	23	
189	E 2.	- 2						E .	Right			87	27	18	23	96	
000	00	00						1	New York			228	230	240	228	976	
		3					L		E	-		_	_	_			



N/S: Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 EE Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

Right

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

L = 0 1 4 8

323 3

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30 36.8 32.3

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1.7

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33.5 19

Grand Total Appreh % Total %

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

N/S: Massachusetts Avenu E/W: Huntington Avenue City, State: Boston, MA Client VHB/ M. Houdlett



9	E C	NDO	P.O. Box 301	e-508.481.
				Office

File Name: 133307 EE Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

									500000								
	M	Massachusetts A venue From North	Avenue		Huntin	Huntington Avenue (Route 9)	us (Route	(6	Ma	Massachusetts Avenue From South	Avenue		Humin	Hundington Avenue (Route 9)	ue (Route	(6	
StartTime	Right	Thru	Left	U-Tum	Right	Then	1	Left U-Tum	Right	Thru	Left	UTun	Right	Thru	Left	U-Tum	Int Total
04:00 PM	0	3	0	0	-	0	0	0	0	S	0	0	0	0	0	0	6
04:15 PM	0	9	0	0	0		7	3	-	9	0	0	0	0	-	0	20
04:30 PM	0	S	0	0	0	0	-	0	0	2	0	0	0	0	0	0	6
04:45 PM	-	3	0	0	-	0	1	6	0	4	0	0	-	0	0	0	14
Total	1	17	0	0	2	-	4	9	-	18	0	0	H	0	7	0	52
05:00 PM	-	4	0	0	0	0	7	-	0	7	0	0	0	0	7	0	17
05:15 PM	0	4	0	0	0	0	-	4	0	9	0	0	0	0	0	0	15
05:30 PM	0	9	0	0	0	0	-	1	0	60	0	0	0	0	0	0	11
05:45 PM	0	2	0	0	0	0	-	0	0	8	0	0	-	0	-	0	10
Total	1	16	0	0	0	0	5	9	0	21	0	0	-	0	3	0	53
Grand Total	2	33	0	0	2	-	6	12	-	39	0	0	7	0	4	0	105
Appreh %	5.7	94.3	0	0	8.3	4.2	37.5	8	2.5	97.5	0	0	33.3	0	2.99	0	
Total %	1.9	31.4	0	0	1.9	-	9'8	11.4	-	37.1	0	0	1.9	0	3.8	0	

Masschaest Aveon Masschaest

8 - 5 5 2

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Seat Times	Relat	Times	Left	Liven	Left	Relat
Peak Hour for Finite Intersection	Begins at 04:00 PM					
Peak Hour for Finite Intersection	Begins at 04:00 PM					
04:50 PM	0	1 0 0	1 0 0			
04:30 PM	2	4 0 0	6	2 2		
Total Volume	31	5	824	0 0		
94:45 PM	2	4 0 0	429			
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	000	472	375
94:45 PM	375	838	000	472	375	
94:45 PM	375	838	000	472	375	
94:45 PM	375	838	000	472	375	
94:45 PM	475	838	475	838	475	835
94:45 PM	475	838	475	835		
94:45 PM	475	838	475	835		
94:45 PM	475	838	475	835		
94:45 PM	475	835	475	835		
94:45 PM	475	835	475	835		
94:45 PM	475	835	475	835		
94:45 PM	475	835	475	835		
94:45 PM	475	835	475	835		
94:45 PM	475	835	475	835		
94:45 PM	475	835				
94:45 P						

059 .625

| Hamington Avenue (Route 9) | Massichued's Avenue (Route 9) | Prom South | Prom Host | Pr

PRECISION
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N/S. Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/M. Houdlette

File Name : 133307 EE Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Massachusetts Avenue E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette

PRE	٥	INDO	O. Box 301	-508.481.3	mail datare
				Office	iii

File Name: 133307 EE Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

		Massac	Massachusetts Averne From North	th		Ħ	and grant from	From East	Huntington Avenue (Route 9) From East			Massach	Massachusetts Averne From South	verme		#	untington	From West	Huntington Avenue (Route 9) From West.	
Start Time	Right	Thru	Left	U-Tum	U-Turn App. Dots	Right	Thru	Left	Urben	Ago, Total	Right	Than	Let	U-Tum	Ago, Tiesi	Right	Thru	Left	U-Tuen	Age. Total
eak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	is From	04:00 PM	\$6.500	PM - Pea	k lof l									1					4	
eak Hour for	Entire	Intersection	tion Be	egins at	Begins at 05:00 PM	×				ľ										
05:00 PM	16	214	0	0	230	19	S	27	12	63	19	500	0	0	228	28	9	25	9	65
05:15 PM	19	222	0	0	241	11	5	34	11	67	19	211	0	0	230	27	S	21	45	58
05:30 PM	21	161	-	0	219	21	18	27	-	73	14	223	0	0	240	18	4	16	4	42
05:45 PM	30	161	1	0	212	20	00	38	-	73	16	212	0	0	228	23	90	23	T	58
Total Volume	94	824	2	0	902	11	36	126	37	276	71	855	0	0	926	96	23	85	19	223
% App. Total	8.4	91.4	0.2	0		27.9	13	45.7	13.4		7.7	92.3	0	0		43	10.3	38.1	8.5	H
PHF	506	.928	200	000	.936	716.	200	828	.771	945	934	656	000	000	.965	857	617.	.850	792	.858
Cars	75	789	1	0	865	75	35	118	31	259	11	826	0	0	897	93	23	78	18	212
% Cars	98.7	95.8	200	0	686	97.4	972	93.7	83.8	93.8	100	9.96	0	0	696	6.96	100	8.16	7.76	95.1
Heavy Vehicles	0	19	-	0	20	2	-	m	0	9	0	00	0	0	00	2	0	4	-	7
N. Honry Vehides	0	23	200	0	2.2	2.6	2.8	2.4	0	22	0	6.0	0	0	6.0	2.1	0	4.7	5.3	3.1
Buses	1	91	0	0	17	0	0	5	9	Ξ	0	21	0	0	21	-	0	3	0	4
% Buses		6	0	0	1.9	0	0	4.0	16.2	4.0	0	2.5	0	0	2.3	1.0	0	3.5	0	90

295 297 297 309 380 380 367 390 381 381 381 381 367 367

132 133 133 2 30

23 82 82 82

21178

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05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

986 98.4 36.8

44.0

415 803 15.5

3 0.6

3.6

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28.8

0.0

93.2

Grand Total Appreh % Total %

Peds 1115 1101 1118 122 456

9eds 38 61 55 196

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Thru 10 10 15

\$ 5 X X X X

8 4 4 4 8 E

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

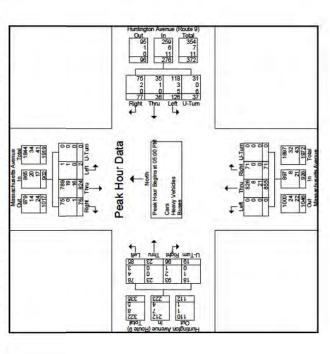
200

Right

Groups Printed-Peds and Bicycles erue (Route 9) Massach

Right

586 574 571 2327 2327 96.0 41 1.8 53 53





File Name : 133307 F Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N: Christian Science Center Driveway E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette

File Name: 133307 F Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

							Group	Groups Printed-Cars	Cars								
	Christian	Christian Science Center Driveway From North	ofer Drive	way	Huntin	Huntington Avenue (Route 9) From East	e (Route 9)			From South	- q		Humin	Humington Avenue (Roule 9)	e (Route)	6	
Start Time	Right	Thru	Left	U-Tum	Right	Then	Left	U-Tum	Right	Thru	ug	U-Turn	Right	Thru	Left	L-Turn	Int. Total
MA 00:70	2	0	0	0	6	26	0	0	0	0	0	0	0	62	0	0	66
07:15 AM	0	0	0	0	00	30	0	0	0	0	0	0	0	72	0	0	110
07:30 AM	0	0	0	0	6	40	0	0	0	0	0	0	0	110	0	0	159
07:45 AM	0	0	0	0	91	36	0	0	0	0	0	0	0	102	0	0	157
Total	2	0	0	0	42	13.5	0	0	0	0	0	0	0	346	0	0	525
08:00 AM	1	0	0	0	19	55	0	0	0	0	0	0	0	111	0	0	186
08:15 AM	0	0	0	0	11	55	0	0	0	0	0	0	0	104	0	0	170
08:30 AM	0	0	0	0	12	48	0	0	0	0	0	0	0	25	0	0	152
08:45 AM	-	0	0	0	13	39	0	0	0	0	0	0	0	122	0	0	175
Total	2	0	0	0	55	197	0	0	0	0	0	0	0	429	0	0	683
Grand Total	4	0	0	0	16	332	0	0	0	0	0	0	0	775	0	0	1208
Appreh %	100	0	0	0	22.6	77.4	0	0	0	0	0	0	0	100	0	0	
Total 9%	0.3	0	0	C	×	375	0	9	0	0	0	9	0	643	0	0	

	Chris	Pristian Scien	om Nort	nce Center Driveway from North	'ay	H	Huntington Avenue (Route 9) From East	Avenue rom East	(Route 9)			Œ.	rom Sout			Ho	intington F	Avenue (furtington Avenue (Roste 9) From West		
Start Time	Right	The	Ireft	U-Tues	App. Total	Right	Thru	Leg	U-Then	Age, Total	Right	Three	Lef	U.Tum	Ago, Thesi	Right	Thru	Left	U-Tuen	Age. Total	los Total
Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1	sis From C	7:00 AM	10 08:45	AM-Pea	k lof l																
Peak Hour for I	Entire	Entire Intersection	tion Be	gins at	08:00 AM	×															
08:00 AM	-	0	0	0	-	19	25	0	0	74	0	0	0	0	0	0	1111	0	0	111	186
08:15 AM	0	0	0	0	0	11	55	0	0	99	0	0	0	0	0	0	2	0	0	2	170
08:30 AM	0	0	0	0	0	12	48	0	0	9	0	0	0	0	0	0	32	0	0	92	152
08:45 AM	1	0	0	0	1	13	39	0	0	52	0	0	0	0	0	0	122	0	0	122	175
Total Volume	2	0	0	0	2	55	161	0	0	252	0	0	0	0	0	0	429	0	0	429	683
% App. Total	100	0	0	0		21.8	782	0	0		0	0	0	0		0	100	0	0	1	
BIIG	COOS	000	000	000	coos	200	508	900	000	158	900	000	000	000	000	000	870	000	000	870	210

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Hundington Avenue (Route 9)

Right Thru Left U-tun

Client: VHB/ M. Houdlette	M. Ho	udlett	e				Small der	oc 508 4513999 Fax 5085453.1 Email: datarequests@pdilc.com	Office: 508-481.3999 Fax: 508.545.1234 Email: decarequests/lipdilic.com	*				Pag	Page No	7.		Clien
						Grouns	Grouns Printed-Cass - Heavy Vehicles - Bases	S - Heavy	Vehides -	lanes.								
	Christian Science Center Driveway From North	Science Center Prom North	orth	eway	Hun	Hundington A venue (Route 9) From East	one (Route 9	6		From South	9		Hunting	From West	Huntington Avenue (Route 9)			
Start Time	Right	Thru	Left	U-Tum	Right	Thru	Left	U-Tum	Right	Thru	Left	U-Tum	Right	Then	Left	U-Tum	Int. Total	L
07:00 AM	2	0	0	0	6	29	0	0	0	0	0	0	0	02	0	0	110	
07:15 AM	0	0	0	0	90	32	0	0	0	0	0	0	0	2	0	0	119	
07:30 AM	0	0	0	0	6	46	0	0	0	0	0	0	0	116	0	0	171	
07:45 AM	0	0	0	0	16	41	0	0	0	0	0	0	0	105	0	0	162	
Total	2	0	0	0	42	148	0	0	0	0	0	0	0	370	0	0	295	
08:00 AM	7	0	0	0	19	56	0	0	0	0	0	0	0	116	0	0	193	
08:15 AM	0	0	0	0	=	28	0	0	0	0	0	0	0	110	0	0	179	
08:30 AM	0	0	0	0	12	49	0	0	0	0	0	0	0	100	0	0	161	
08:45 AM	1	0	0	0	13	44	0	0	0	0	0	0	0	125	0	0	183	1
Total	3	0	0	0	\$5	207	0	0	0	0	0	0	0	451	0	0	216	
Grand Total	8	0	0	0	6	355	0	0	0	0	0	0	0	821	0	0	1278	
Appreh %	100	0	0	0	21.5	78.5	0	0	0	0	0	0	0	100	0	0		
Total %	0.4	0	0	0	7.6	27.8	0	0	0	0	0	0	0	64.2	0	0		
Cars	4	0	0	0	16	332	0	0	0	0	0	0	0	775	0	0	1208	
% Cars	80	0	0	0	100	93.5	0	0	0	0	0	0	0	94.4	0	0	24.5	
Heavy Vehicles	-	0	0	0	0	18	0	0	0	0	0	0	0	20	0	0	36	
% Heavy Vehicles	20	0	0	0	0	5.1	0	0	0	0	0	0	0	2.4	0	0	3.1	
Buses	0	0	0	0	0	S	0	0	0	0	0	0	0	26	0	0	31	
% Ringes	0	0	0	9	0	1.4	9	0	9	0	0	c	0	2.3	•	0	P 6	



Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

File Name : 133307 F Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N: Christian Science Center Drive E/W: Huntington Avenue (Route City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 F Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

J	PRECISION	DATA	INDUSTRIES, LLC	3. Box 301 Berlin, MA 01 508,481,3999 Fax: 508
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oute 9)	A O
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	P.O. Box 301 Be
	Contract of the Contract of th

7	PRECISION D A T A	INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 0 e-508.481.3999 Fax: 508.
			900

							Ground	Groups Printed-Buses	Buses								
	Christian	Christian Science Center Driveway From North	oter Drive	way	Hantin	Huntington Avenue (Route 9) From East	(Route 9)	J		From South	dh dh	П	Humin	Humington Avenue (Route 9) From West	e (Route S		
StartTime	Right	Thru	Left	U-Turn	Right	Thru	Left	Left U-Tum	Right	Thru	Left	U-Turn	Ri ght	Thru	Left	Loft U-Turn	Int. Total
07:00 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	9	0	0	7
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0	0	m
07:30 AM	0	0	0	0	0	-	0	0	0	0	0	0	0	7	0	0	6
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0	0	
Total	0	0	0	0	0	2	0	0	0	0	0	0	0	14	0	0	16
08:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0	0	m
08:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	3	0	0	
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0	0	4
08:45 AM	0	0	0	0	0	10	0	0	0	0	0	0	0	2	0	0	5
Total	0	0	0	0	0	33	0	0	0	0	0	0	0	12	0	0	15
Grand Total	0	0	0	0	0	8	0	0	0	0	0	0	0	56	0	0	31
Appreh %	0	0	0	0	0	100	0	0	0	0	0	0	0	100	0	0	
Total %	0	0	0	0	0	16.1	0	0	0	0	0	0	0	83.9	0	0	

Sear Time Regist The Left through through through the Left through thr	Christian Science Center Driveway From North Left Urban Age 33 roan 07:00 AM to 08:45 AM - Peak 1 of ntire Intersection Begins at 07:07		NA O	Hunt I	From From The I	From East This Left Urbin	var Are	Rea C	The state of	From South	Li-Tum	Age Total	Right	The Fr	0 8	(Route 9)		lst Total	Start Time Peak Hour Analy Peak Hour fo	Start Time Right The From No. Start Fine And Start Fine And Start Fine Transfers & From 07:00 AM to 08:4 Feak Hour Analysis Feak Ho	Right The From 07:00 Entire Inter	From North From North Thru Left O AM to 08.45 A tersection Beg	Christian Science Center Dilveway Start Time Right Then Left Ustra Antion vok Hour Analysis From 07:00 AM to 08:45 AM - Pede 1 of 1 Ceak Hour for Entire Intersection Begins at 07:00	orth U-Tun Anstead R 15 AM - Peak 1 of 1 Begins at 07:00 AM	Right Hu	Huntington F	From East	Route	Total	Right	From	rom South	South Left Urben Age tool	Right H	Huntington	From West Left	Route 9	Age You	Total
00	-		00	00	40	00	00	111	00	00	00	00	00	4 4	00	00	1 4	+ 0	07:15 AM	AM	00	00	00		00	0	00	00	0	00	00	00	00	00	3 0	00	00	m	- 10
00	0 -		00	00	10 C	00	00	10 61	00	00	00	00	00	40	00	00	40	6 6	07:30 AM 07:45 AM	AM AM	00	00	000	0.0	00	0	00	00	-0	00	00	00	00	00	3 2	00	00	(1 m	m m
00	0 -		0	00	- 8	00	00	=	00	00	00	0	00	000	00	00	10	21	Total Volume % App. Total	lume	00	00	00	6.7	0	100	00	00	2	00	00	00	00	0	0 100	00	00	4	16
000 000 000 000 000 000 000 000 000 000 000 000 000 000 000	-	6	000	000	550 08	00	Q.	00	W 000	000	000	000	000	309		9 000	3 309	583			000 000 000	000	000	000	000		000 005	000	800	000	000 000	00	000	000	000 583	000	OOO	583	125

outh	П													
From North	Thru	0	0	0	0	0	0	0	0	0	0	0	0	0
Christian Science Center From North	Right	0	0	0	0	0	0	0	0	0	0	0	0	0
	Start Time	07:00 AM	07:15 AM	07:30 AM	07:45 AM	Total	08:00 AM	08:15 AM	08:30 AM	08:45 AM	Total	Grand Total	Appreh %	Total %
	Int. Total	4	9	6	2	21	4	9	s	3	18	39		
6	U-Tum	0	0	0	0	0	0	0	0	0	0	0	0	0
est (Route 9	Left	0	0	0	0	0	0	0	0	0	0	0	0	0
Huntington Avenue (Route 9) From West	Then	2	4	4	0	10	7	3	4	1	10	20	100	51.3
H untin	Right	0	0	0	0	0	0	0	0	0	0	0	0	0
	U-Turn	0	0	0	0	0	0	0	0	0	0	0	0	0
-6	Left	0	0	0	0	0	0	0	0	0	0	0	0	0
From South	Thru	0	0	0	0	0	0	0	0	0	0	0	0	0
	Right	0	0	0	0	0	0	0	0	0	0	0	0	0
	U-Lum	0	0	0	0	0	0	0	0	0	0	0	0	0
(Route 9)	Loft	0	0	0	0	0	0	0	0	0	0	0	0	0
Hundington A venue (Route 9) From East	Thru	2	2	8	2	=	-	3	-	2	1	18	100	46.2
Honding	Right	0	0	0	0	0	0	0	0	0	0	0	0	0
N.	U-Tum	0	0	0	0	0	0	0	0	0	0	0	0	0
ter Drivew	Left	0	0	0	0	0	0	0	0	0	0	0	0	0
Prom North	Thru	0	0	0	0	0	0	0	0	0	0	0	0	0
Christian Science Center Driveway From North	Right	0	0	0	0	0	-	0	0	0	-	-	100	2.6
_			-	-		-	-	-	-	_	1	-		

Grand Total Appreh % Total %

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

N: Christian Science Center Driveway E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 F Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N: Christian Science Center Driveway E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette

enne (Route 9)

Groups Printed-Peds and Bicycles enue (Route 9)

Right

Orisian Science Center Driveway From North Right Thru Left P

Ped 27 1 19

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

Right

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28228

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

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10 83.3 2.8

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Grand Total Appreh % Total %

File Name: 133307 F Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

.927 683 95.4 18 2.5 15

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1100



	Chris	tian Scien	Christian Science Center Driveway From North	r Driven	ay	#1	uniting ton	Huntington Avenue (Route 9)	Route 9)			į.	ven South			H	Hantington Avenue (Route 9)	From West	Route 9	
Start Time Right Thru Left U-Tum App Total	Right	The	Fell	U-Tum	App Total	Right	Three	Ive	Urben	Ago, Total	Right Thru	Than	Left U	Tim.	Ago Rest Right	Right	Thru	LeR	U-Tuen	\$
Peak Hour Analysis From 0730 AM to 08:45 AM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 08:00 AM	T Entire I	ntersec	tion Be	gins at	08:00 A	M														
08:00 AM	7	0	0	0	7	19	26	0	0	75	0	0	0	0	0	0	116	0	0	
08:15 AM		0	0	0	0	= :	8	0	0	69	0	0	0	0	0 0	0	110	0	0	
08:30 AM		00	0 0	0 0	0 -	7 6	4 4	00	0 0	200	00	00	00	00	0 0	00	125	00	00	
Total Volume	6	0	0	0	m	55	207	0	0	262	0	0	0	0	0	0	451	0	0	4
% App. Total	100	0	0	0		21	62	0	0		0	0	0	0		0	100	0	0	
PHF	-	000	000	000	.375	.724	892	000	000	873	000	000	000	000	000	000	305	000	000	-
Cars	\vdash	0	0	0	2	55	197	0	0	252	0	0	0	0	0	0	429	0	0	1
% Cars	-	0	0	0	2.99	100	952	0	0	96.2	0	0	0	0	0	0	95.1	0	0	6
Henry Vehicles	_	0	0	0	-	0	-	0	0	7	0	0	0	0	0	0	10	0	0	
% Honry Vehicles	33.3	0	0	0	333	0	3.4	0	0	2.7	0	0	0	0	0	0	2.2	0	0	
Buses	-	0	0	0	0	0	3	0	0	6	0	0	0	0	0	0	12	0	0	
% Buses	0	0	0	0	0	0	4.	0	0	7	0	0	0	0	0	0	2.7	0	0	
			(9 shoft) sunsvik notportruH Listo 1 NuO Listo 1 NuO	150 150		1947 1041 105 107-11 10 104 10 10 10 10 10 10 10 10 10 10 10 10 10	D 184 0 10		Peak House, vehicles	T H OOOO P P P P P P P P P P P P P P P P	# ± 100000 ± ± 100000 1	Scooper Community Communit	* + 2	55 203 0 0 Right Thru Left U-Turn	551 197 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	451 262 713	Hurtington Avenue (Houte 9) Out Total 429 252 881 10 7 17 11 3 15 451 262 713	I limited to the second		
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| Christian Science Conner Driveway | Hamington Avenue (Rouse 9) | From Scient | From



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Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

File Name : 133307 FF Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N: Christian Science Center Driveway E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette



File Name: 133307 FF Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

				Crouns Times-Ca	an-Cars					
	Christian Scient	Christian Science Center Driveway From North	way	Huntington	Huntington A venue (Route 9) From East	6	Huntington /	Huntington Avenue (Route 9) From West	6	
Start Time	Right	Left	U-Tum	Right	Thru	U-Turn	Thru	Toff	U-Turn	Int. Total
04:00 PM	10	0	0		35	0	0	0	0	45
04:15 PM	11	0	0	1	48	0	0	0	0	99
04:30 PM	22	0	0	0	55	0	0	0	0	11
04:45 PM	11	0	0	0	20	0	0	0	0	19
Total	35	0	0	2	187	0	0	0	0	243
05:00 PM	17	0	0	0	43	0	0	0	0	99
05:15 PM	13	0	0	4	51	0	0	0	0	89
05:30 PM	22	0	0	m	52	0	0	0	0	11
05:45 PM	10	0	0	1	80	0	0	0	0	02
Total	62	0	0	∞	205	0	0	0	0	275
rand Total	116	0	0	10	392	0	0	0	0	818
Appreh %	100	0	0	2.5	97.5	0	0	0	0	
Total %	22.4	0	0	1.9	75.7	0	0	0	0	

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05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

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Grand Total Appreh % Total %

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Cars
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518 93.2 12 22 26 4.7

	Christin	in Science Center From North	Christian Science Center Driveway From North	ay.	Her	Prom East	funtington A verue (Route 9) From East		Hun	From West	funtington Avanue (Route 9) From West		
Start Time	Right	Lef	U-Tum	App. Total	Right	Thru	U-Tum	Ann. Total	Thru	Left	U-Turn	Age, Total	Int. Total
eak Hour Arralysis From 04:00 PM to 05:45 PM - Peak 1 of 1	M:00 PM to 05x	S PM - Ped	t lof!										
eak Hour for Entire Intersection Begins at 05:00 PM	ntersection B	egins at 0.	S:00 PM										
05:00 PM	17	0	0	17	0	43	0	43	0	0	0	0	09
05:15 PM	13	0	0	13	7	51	0	55	0	0	0	0	89
05:30 PM	22	0	0	22	m	52	0	55	0	0	0	0	11
05:45 PM	10	0	0	10	e	20	0	09	0	0	0	0	10
Total Volume	62	0	0	62	00	205	0	213	0	0	0	0	275
% App. Total	100	0	0		3.8	962	0		0	0	0		
PHF	705	000	000	202	200	698	000	888	000	000	000	000	803

	Consta	in Science Center From North	Christian Science Center Driveway From North	ay.	Han	fington A verue (Huntington A verne (Route 9) From East		Huni	From West	Huntington Avenue (Route 9) From West		
Sart Time	Right	Lef	U-Tum	App. Total	Right	Thru	U-Tum	Arro. Total	Thru	Left	C-Turn	Age. Total	ř
Arabysis From 04:00 PM to 05:45 PM - Peak 1 of 1	4:00 PM to 05×	45 PM - Peak	t lof!										
our for Entire Intersection Begins at 05:00 PM	nersection B	egins at 0.	S:00 PM	Ó									
05:00 PM	17	0	0	17	0	43	0	43	0	0	0	0	
05:15 PM	13	0	0	13	7	51	0	55	0	0	0	0	
05:30 PM	22	0	0	22	3	52	0	55	0	0	0	0	
05:45 PM	10	0	0	10	F	20	0	09	0	0	0	0	
otal Volume	62	0	0	62	80	205	0	213	0	0	0	0	
App. Total	100	0	0		3.8	962	0		0	0	0		
PHF	.705	000	000	.705	200	698	000	888	000	000	000	000	

913 275 942 44 114 13

913 213 213 92.6 1.7 1.7 1.3 5.7

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| Christian Science Center Drivensy | Curisian Science Center Drivensy | Food Hour Anna | Food Hour Center | Center

Hamington A venue (Route 9)

From West
Left U-Turn App. Total

Hantingvn Avenue (Route 9)
From East

Thru U-Turn App. Total



Groups Phintel-Beav Vehicles
Huringen Avenue Route 9)
From East
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File Name: 133307 FF Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

Int Total

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Grand Total Appreh % Total %

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05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

Sart Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

N: Christian Science E/W: Huntington A City, State: Boston, Client: VHB/ M. H

L	RECISIO	A T NUSTRIES, L	101 Berlin, M.
	- 4		P.O. Box

		1	0
ace Center Driveway	Avenue (Route 9)	o. MA	Hondlette

_	PREC	D	INDUS	P.O. Box 301	Ems 6 desse
					No.

File Name : 133307 FF Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

				Chours Present Susce	C- Direct				1	
	Christian Scien	Christian Science Center Driveway From North	ray	Huntington	Huntington A venue (Route 9) From East	6	Huntington Fr	Huntington Avenue (Route 9) From West	6	
Start Time	Right	Left	U-Tum	Right	Thru	U-Turn	Thru	Loft	U-Tum	Int. Total
04:00 PM	0	0	0	0	1	0	0	0	0	1
04:15 PM	0	0	0	0	9	0	0	0	0	9
04:30 PM	0	0	0	0	1	0	0	0	0	1
04:45 PM	0	0	0	0	5	0	0	0	0	S
Total	0	0	0	0	13	0	0	0	0	13
05:00 PM	0	0	0	0	4	0	0	0	0	4
05:15 PM	0	0	0	0	5	0	0	0	0	8
05:30 PM	0	0	0	0	e	0	0	0	0	3
05:45 PM	0	0	0	0	1	0	0	0	0	1
Total	0	0	0	0	13	0	0	0	0	13
Grand Total	0	0	0	0	26	0	0	0	0	26
Appreh %	0	0	0	0	100	0	0	0	0	
Total %	0	0	0	0	100	0	0	0	0	

		Christin	n Science (Christian Science Center Driveway From North	ay.	Her	From From	Huntington A verue (Route 9) From East		Hum	From V	From West		
f. Total	Sart Time	Right	Lef	U-Turn	App. Total	Right	Thru	U-Tum	Ann. Total	Then	Left	U-Turn	Are. Total	Int. Total
	Peak Horr Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	04:00 PM to 05x	SPM-Per	k lof!							1			
	Peak Hour for Entire Intersection Begins at	ntersection B		24:45 PM										
2	04:45 PM	0	0	0	0	0	10	0	40	0	0	0	0	9
_	05:00 PM	0	0	0	0	0	4	0	4	0	0	0	0	4
_	05:15 PM	0	0	0	0	0	S	0	5	0	0	0	0	5
_	05:30 PM	0	0	0	0	0	3	0	6	0	0	0	0	3
l ∞	Total Volume	0	0	0	0	0	17	0	17	0	0	0	0	17
	% App. Total	0	0	0		0	100	0	T	0	0	0		
200	PHF	000	000	000	000	000	.850	000	.850	000	000	000	000	.850

	Christi	Stristian Science Center Driveway	enter Drivew	ry.	Han	ington Avenue (funtington Avenue (Route 9)		Hen	ington A venue (lumington Avenue (Route 9) Hom West		
Start Time	Right	Left	U-Tum	U-Turn App. Total	Right	Thru	C-Turn	App. Total	Thru	Leg	U-Turn	App. Total	Int. Total
cak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	14:00 PM to 05:	45 PM - Peak	1 of 1										
eak Hour for Entire Intersection Begins at 04:00 PM	intersection B	Regins at 04	4:00 PM									Č	
04:00 PM	0	0	0	0	0	2	0	7	0	0	0	0	7
04:15 PM	0	0	0	0	0	1	0	-	0	0	0	0	1
04:30 PM	0	0	0	0	0	-	0	-	0	0	0	0	1
04:45 PM	0	0	0	0	0	*	0	*	0	0	0	0	*
Total Volume	0	0	0	0	0	00	0	8	0	0	0	0	8
% App. Total	0	0	0		0	00	0		0	0	0		
PHF	000	000	000	000	000	003	000	005	000	000	000	000	200



Groups Printed-Pecks and Bicyckes
Hundingkon Avenue (Roate 9)
From East
Right Thru

269 269

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

File Name : 133307 FF Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N: Christian Science Center Dr E/W: Huntington Avenue (Rot City, State: Boston, MA Client: VHB/ M. Houdlette

way	6		
Duve	Route		
e Center Drivew	24	Y	
ence (tington Avenue	on, M	
an Science	ntingt	: Bostor	



File Name : 133307 FF Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

	Christia	an Science Center From North	Christian Science Center Driveway From North	X.	Har	nington A verse (Huntington A venue (Route 9) From East		Hu	Huntington Avenue (Route 9) From West	nue (Route 9 West	6	
Start Time	Right	Leff	U-Turn	App. Total	Right	Thru	U-Tum	App. Total	Thru	Left	U-Turn	App. Total	Int. Total
eak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	04:00 PM to 05:	45 PM - Pest	loft										
eak Hour for Entire Intersection Begins at 05:00 PM	ntersection E	segms at 0.	S CO PM										
05:00 PM	17	0	0	17	0	84	0	48	0	0	0	0	65
05:15 PM	13	0	0	13	7	57	0	19	0	0	0	0	74
05:30 PM	22	0	0	22	60	55	0	58	0	0	0	0	80
05:45 PM	10	0	0	10	-	29	0	63	0	0	0	0	73
Total Volume	62	0	0	62	80	222	0	230	0	0	0	0	292
% App. Total	100	0	0		3.5	596	0		0	0	0		
PHF	.705	000	000	.705	200	868	000	.913	000	000	000	000	.913
Cars	62	0	0	62	000	205	0	213	0	0	0	0	275
% Cars	100	0	0	100	100	923	0	92.6	0	0	0	0	94.2
Heavy Vehicles	0	0	0	0	0	4	0	4	0	0	0	0	4
% Heavy Vehicles	0	0	0	0	0	1.8	0	1.7	0	0	0	0	1.4
Buses	0	0	0	0	0	13	0	13	0	0	0	0	13
% Buses	0	0	0	0	0	5.9	0	5.7	0	0	0	0	4.5

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89 103 107 74 373

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

8 4 4 4 6 5 5.78 S.1.2

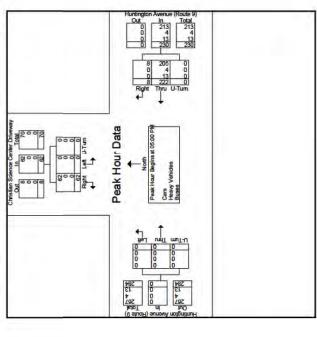
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Grand Total Appreh % Total %



	Christia	n Science Co	Arristian Science Center Driveway From North	'ay	Hum	From F	untington Avenue (Roare 9)		Hon	untington A venue (Route 9) From West	ue (Route 9)		
Start Time	Right	Left	Peds	App. Total	Right	Thru	Peds	App. Total	Thru	Left	Peds	App. Total	Int. Total
eak Bour Analysis From 04:00 PM to 05:45 PM - Peak I of I	4:00 PM a	S PM - Peak	kl of 1										
eak Hour for Entire In	nersecti	on Begins at 05:00 PM	5:00 PM										
05:00 PM	0	0	68	68	0	00	0	30	0	0	0	0	16
05:15 PM	7	0	103	107	0	4	0	4	0	0	0	0	Ш
05:30 PM	0	0	101	107	0	4	0	4	0	0	0	0	111
05:45 PM	9	0	74	11	0	4	0	4	0	0	0	0	81
Total Volume	7	0	373	380	0	20	0	20	0	0	0	0	400
% App. Total	1.8	0	98.2		0	00	0		0	0	0	1	
PRE	438	000	871	888	000	368	000	363	000	000	900	000	100

File Name : 133307 G Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

S: Cumberland Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette

File Name : 133307 G Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1		Int. Total	214	245	258	337	1054	287	300	283	327	1197	2251		
::133 ::101 ::5/1		U-Tum	0	0	0	0	0	0	0	0	0	0	0	0	0
File Name Site Code Start Date Page No	(Route 9)	Left	0	0	0	0	0	0	0	0	0	0	0	0	0
File Site Star Page	Hundington Avenue (Route 9) From West	Thru	16	80	113	147	437	110	115	108	146	479	916	8	40.7
	Huming	Right	3	1	00	00	56	00	6	3	12	32	88	9	5.6
		U-Turn	0	0	0	0	0	0	0	0	0	0	0	0	0
0.03	treet th	Left	0	0	0	0	0	0	0	0	0	0	0	0	0
	Cumberland Street From South	Thru	0	0	0	0	0	0	0	0	0	0	0	0	0
A A C.C. C.C. C.C. C.C. C.C.C.C.C.C.C.C.		Right	9	13	00	10	37	17	6	10	10	94	83	100	3.7
PRECISION D A T A NUDUSTRES,LLC RO, Box 301 Berlin, M. 01503 ces-Goulds 1.3899 Fac. 906.9451 Groups Planted-Cars		U-Tum	0	0	0	0	0	0	0	0	0	0	0	0	0
PRECISION D A T A INDUSTRIES, LLC PO, Box 1399 Feeling, MA 1739 Feel Advance users of Feeling and Feel	(Route 9)	Left	0	0	0	0	0	0	0	0	0	0	0	0	0
8	Huntington Avenue (Route 9) From East	Thru	108	145	129	172	554	152	167	162	159	049	1194	100	53
	Huntin	Right	0	0	0	0	0	0	0	0	0	0	0	0	0
6		U-Tum	0	0	0	0	0	0	0	0	0	0	0	0	0
Route		45	0	0	0	0	0	0	0	0	0	0	0	0	0
t venue (Route 9) AA audlette	From North	Thro	0	0	0	0	0	0	0	0	0	0	0	0	0

Sart Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

230 238 288 280 358 310 310 318 305 325

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

		Œ	om North		Ħ	Hu	ntington Fr	funtington Avenue (Route 9) From East	Route 9)	j		Ound F	Sumberland Street From South	Tod.	ī	£	Intington H	Austrington Avenue (Route 9) From West	Route 9)		
tart Time	Right	Thru	Left	U-Tuen	App. Total	Right	There	Len	U-Tuen A	ten Total	Right	Three	1,48	U-Turn	Ago, Thesi	Right	Thru	Len	U-Turn	ten Toni	los. Total
four Armys	is From 0	7:00 AM	0 08×45 A	AM - Peak	1 of 1																
eak Hour for	Entire	Intersect	ion Beg	gins at 0	D7:45 AM	7															
77:45 AM	0	0	0	0	0	0	172	0	0	172	10	0	0	0	10	00	147	0	0	155	337
08:00 AM	0	0	0	0	0	0	152	0	0	152	11	0	0	0	17	00	110	0	0	811	287
08:15 AM	0	0	0	0	0	0	167	0	0	167	6	0	0	0	6	6	115	0	0	124	300
08:30 AM	0	0	0	0	0	0	162	0	0	162	10	0	0	0	10	3	108	0	0	111	283
Total Volume	0	0	0	0	0	0	653	0	0	653	46	0	0	0	46	28	480	0	0	808	1207
App. Total	0	0	0	0		0	100	0	0		100	0	0	0		5.5	94.5	0	0		
PHF	000	000	000	000	000	000	646	000	000	646	9/9	000	000	000	929	37.78	816	000	000	819	895

Grand Total Approch % Total %

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Grand Total
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08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

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						H	lumington Avenue (Route 9)	Avenue	(Rouge 9)			Cump	Cumberland Street	reet		Ħ	fundington Avenue (Route 9)	A venue (Route 9)		
		F	From North					From East				Ē	From South				Œ	From West			
Start Time	Right	Thru	Left	UTum	Acc. Total	Right	Thin	Lef	U-Tum	App. Real	Right	Thru	Left	U-Tum	Ago, Toni	Right	The	Lef	U-Tum	Ace. These	Int Total
ask Hour Analysis From 07:00 AM to 08:45 AM - Peak I of	is From 0.	2:00 AM	NO 08 345 A	VM - Pea	k l of l																
eak Hour for I	Entire Inte	TSec	tion Begins a	gins at	07:45 A	M															
07:45 AM	0	0	0	0	0	0	185	0	0	22	10	0	0	0	10	00	155	0	0	163	358
08:00 AM	0	0	0	0	0	0	166	0	0	991	18	0	0	0	18	00	118	0	0	126	310
08:15 AM	0	0	0	0	0	0	176	0	0	176	6	0	0	0	6	6	124	0	0	133	318
08:30 AM	0	0	0	0	0	0	174	0	0	174	11	0	0	0	11		117	0	0	120	305
Total Volume	0	0	0	0	0	0	701	0	0	701	48	0	0	0	48	28	514	0	0	542	1291
App. Total	0	0	0	0		0	100	0	0		100	0	0	0		5.2	876	0	0		
PHF	000	000	000	000	000	000	746	000	000	.947	199	000	000	000	199	.778	828	000	000	.831	902
Cars	0	0	0	0	0	0	653	0	0	683	94	0	0	0	46	28	480	0	0	808	1207
% Cars	0	0	0	0	0	0	93.2	0	0	93.2	8.86	0	0	0	95.8	100	93.4	0	0	93.7	93.5
loany Vehicles	0	0	0	0	0	0	50	0	0	29	7	0	0	0	13	0	18	0	0	18	49
4 Heavy Vehicles	0	0	0	0	0	0	4.1	0	0	-	4.2	0	0	0	4.2	0	3.5	0	0	3.3	3.8
Buses	0	0	0	0	0	0	19	0	0	61	0	0	0	0	0	0	91	0	0	16	35
% Buses	0	0	0	0	0	0	2.7	0	0	2.7	0	0	0	0	0	0	3.1	0	0	3.0	2.7



Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

File Name : 133307 G Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

S: Cumberland Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette



File Name: 133307 G Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1



		From North	th.		Huntin	gion Avenue (Huntington Avenue (Route 9) From East		٥	Cumberland Street From South	Street		Huming	Humington Avenue (Route 9) From West	e (Route 9	,	
StartTime	Right	Thru	Left	U-Tum	Right	Thru	Left	U-Tum	Right	Thru	eft	U-Tum	Right	Thro	Left	U-Tum	Int. Total
07:00 AM	0	0	0	0	0	-	0	0	0	0	0	0	0	9	0	0	7
07:15 AM	0	0	0	0	0	2	0	0	0	0	0	0	0	4	0	0	9
07:30 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	8	0	0	12
07:45 AM	0	0	0	0	0	2	0	0	0	0	0	0	0	4	0	0	9
Total	0	0	0	0	0	12	0	0	0	0	0	0	0	61	0	0	31
08:00 AM	0	0	0	0	0	8	0	0	0	0	0	0	0	6	0	0	- 00
08:15 AM	0	0	0	0	0	4	0	0	0	0	0	0	0	S	0	0	6
08:30 AM	0	0	0	0	0	00	0	0	0	0	0	0	0	4	0	0	12
08:45 AM	0	0	0	0	0	9	0	0	0	0	0	0	0	s	0	0	Ξ
Total	0	0	0	0	0	23	0	0	0	0	0	0	0	17	0	0	40
Grand Total	0	0	0	0	0	35	0	0	0	0	0	0	0	36	0	0	7.1
Appreh %	0	0	0	0	0	100	0	0	0	0	0	0	0	100	0	0	
Total %	0	0	0	0	0	403	0	0	0	0	0	0	0	50.7	0	0	

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Grand Total
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		4	Prom North	49	H	Ha	of ing ton	Iuntington Avenue (Route 9) From East	Route 9)	j		Cumb	Cumberland Street From South	red		Ha	mington Fe	Avenue (F	furnington Avenue (Route 9)		
Start Time	Right	Then	Left	U-Tues	App. Total	Right	There		U.Ten	Age. Total	Right	Thru	Lef	U.Tum	Age. Thesi	Right	Thru	Left	U-Turn	Age. Total	Int. Total
Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak	wis From C	07:00 AM	10 08:45	AM-Pea	t lof 1																
Peak Hour for E	r Entire	Entire Intersec	tion Be	Pgins at (08:00 AM	7															
08:00 AM	0	0	0	0	0	0	2	0	0	9	0	0	0	0	0	0	m	0	0	m	80
08:15 AM	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	0	10	0	0	'n	6
08:30 AM	0	0	0	0	0	0	00	0	0	00	0	0	0	0	0	0	4	0	0	4	12
08:45 AM	0	0	0	0	0	0	9	0	0	9	0	0	0	0	0	0	2	0	0	5	11
Total Volume	0	0	0	0	0	0	23	0	0	23	0	0	0	0	0	0	17	0	0	17	40
% App. Total	0	0	0	0		0	100	0	0		0	0	0	0		0	100	0	0		
PHF	000	000	000	000	000	000	617.	000	000	719	000	000	000	000	000	000	850	000	000	.850	.833

Max. Pask Signal Then Leef U.Then Late U.Then U.Then			Pa	From North	1		Æ	mington	Huntington Avenue (Route 9)	(Route 9			Com	Cumberland Street From South	Street		2	Huntington Avenue (Route 9) From West	Prom West	(Route 9)		
Freem 07:00 AN to 865 SAN - Twa.1 of T. Shifter Intersection Begins at 08:00 AM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Start Time	Right	Thru	Left	LTum.	Age. Total	Right	Theo	Teg.	U-Tues	App. Des	Right	Thru	Left	U-Tum	Ages Total	Right	Thro	Leff	U-Tues	Age, Desi	Int. Total
indire Intersection Begins at 08:00 AM 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Hour Analys	is From 07	2:00 AM	to 08:45 A	M - Peak	k lof!																
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Hour for	Entire h	ntersec	ion Beg	ins at C	08:00 AL	V															
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8:00 AM	0	0	0	0	0	0	6	0	0	6	-	0	0	0	-	0	2	0	0	S	15
0 0 0 0 0 0 4 0 0 4 1 0 0 0 1 0 0 0 0 8 0 0 8 0 0 0 0 0 0 0	8:15 AM	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	0	4	0	0	4	6
0 0 0 0 0 0 8 0 0 8 1 0 0 0 1 0 8 0 0 8 0 0 8 0 0 8 0 0 0 0	8:30 AM	0	0	0	0	0	0	4	0	0	4	-	0	0	0	-	0	2	0	0	2	10
0 0 0 0 0 0 0 26 0 0 26 3 0 0 0 3 0 22 0 0 22 0 0 0 0 0 0 100 0 0 100 0 0 0 0 0 0 0 100 0 0	8:45 AM	0	0	0	0	0	0	60	0	0	00	-	0	0	0	-	0	90	0	0	90	17
0 0 0 0 0 0 0 0 100 0 0 100 0 0 0 0 0 0	al Volume	0	0	0	0	0	0	26	0	0	26	6	0	0	0	6	0	22	0	0	22	51
	upp. Total	0	0	0	0		0	100	0	0		100	0	0	0		0	100	0	0		

File Name : 133307 G Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

Right

88 30 77 T 88

Right 0 0 0 0

S 2 2 2 2 2 8

Star Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

Groups Printed-Peds and Bicycles enue (Route 9)

S: Cumberland Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette



File Name : 133307 G Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

		E	From North		ī	1	Huntangion Avenue (Route 9) From East	From East	Kone 9)			Fr	From South	LOG		E	From West	From West	Kome 2)		
Start Time	Right	Thru	Left	U-Turn App. Dots	App. Total	Right	Thru	Left	UTurn	Age, Total	Right	Than	Lef	U-Tum	Ago, Resi	Right	Thru	Left	U-Tuen	Age, Total	Int. Total
tak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1	is From 0	7:00 AM	10 08945	AM-Pesi	k lof1												1	1			
eak Hour for	Entire	ntersec	tion Be	gins at (Entire Intersection Begins at 07:45 AM	×															
07:45 AM	0	0	0	0	0	0	185	0	0	185	10	0	0	0	10	00	155	0	0	163	358
MA 00:80	0	0	0	0	0	0	166	0	0	166	18	0	0	0	18	00	118	0	0	126	310
08:15 AM	0	0	0	0	0	0	176	0	0	176	6	0	0	0	6	6	124	0	0	133	318
08:30 AM	0	0	0	0	0	0	174	0	0	174	11	0	0	0	11	6	117	0	0	120	305
Total Volume	0	0	0	0	0	0	101	0	0	701	48	0	0	0	48	28	514	0	0	545	1291
6 App. Total	0	0	0	0		0	100	0	0		100	0	0	0	1	5.2	876	0	0		
PHF	000	000	000	000	000	000	247	000	000	947	299	000	000	000	199	877.	828	000	000	.831	.902
Cars	0	0	0	0	0	0	653	0	0	653	46	0	0	0	46	28	480	0	0	808	1207
% Cars	0	0	0	0	0	0	93.2	0	0	93.2	8'56	0	0	0	958	100	93.4	0	0	93.7	93.5
Serry Vehicles	0	0	0	0	0	0	50	0	0	29	7	0	0	0	2	0	81	0	0	18	49
N Honry Vehides	0	0	0	0	0	0	4.1	0	0	4.1	4.2	0	0	0	4.2	0	3.5	0	0	33	3.8
Buses	0	0	0	0	0	0	19	0	0	19	0	0	0	0	0	0	91	0	0	91	35
% Buses	0	0	0	0	0	0	27	0	0	27	0	0	0	0	0	0	3.1	c	0	30	27

21 87.5 5.8 15

8.3

197

000

0.5

124 89.9 4.4

10.1 000 000

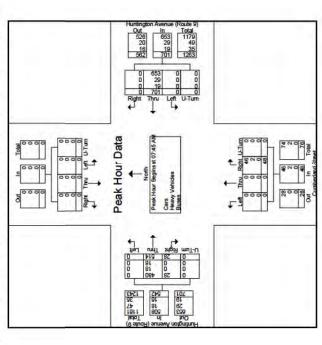
Grand Total Appreh % Total %

244 4 6

0 6 7 2 3

00000

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total



		Po	rom North			H	Huntington Avenue (Route 9)	A venue	(Route 9)			Cumb	Cumberland Street From South	poet		#	Huntington A venue (Route 9) From West	A venue	(Route 9)		
Start Time	Right	Thru	Left	Peds	Ages, Tonal	Right	The	Leg	Peds	Area Dani	Richt	Then	Left	Peds	Ages Total	Right	The	Tell	Peds	Age. Tress	Int. Total
onk Hour Amilys	Amalysis From 0	7:00 AM	to 08 x45 A	AM - Peak 1 of 1	lofi																
ak Hour for	Entire	ntersec	tion Be	gins at 0	A 00:8	×															
08:00 AM	0	0	0	0	0	0	7	0	10	12	0	0	0	21	21	1	v	0	-	7	4
08:15 AM	0	0	0	0	0	0	-	0	19	20	0	0	0	14	14	0	2	0	0	2	36
08:30 AM	0	0	0	0	0	0	-	0	24	25	-	0	0	40	41	0	2	0	0	2	71
08:45 AM	0	0	0	0	0	0	4	0	16	20	0	0	0	34	34	0	3	0	0	3	57
Total Volume	0	0	0	0	0	0	8	0	69	11	1	0	0	109	110	1	15	0	1	17	204
% App. Total	0	0	0	0		0	10.4	0	9.68		60	0	0	99.1		5.9	88.2	0	5.9		
BHB	000	000	000	000	000	000	COUS	000	210	ULL	050	OW)	W	103	144	OSC	USE	8	050	COL	210

Groups Printed-Case - Heavy Vehildes - Biness Cumberland Street Prom South -Turn Right Left

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

File Name: 133307 GG Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

S: Cumberland Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette

7	PRECISION	DATA	INDUSTRIES, LLC	O. Box 301 Berlin, MA 01503
				- 40

File Name: 133397 GG Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

				Groups Printed-Cars	d-Cars					
	Huntington . Fr	Huntington Avenue (Route 9) From East	9	Cumbe	Cumberland Street From South		Huntington F	Huntington Avenue (Route 9) From West	9)	
Start Time	Thru	Left	U-Tum	Right	Left	U-Tum	Right	Thru	U-Tum	Int. Total
04:00 PM	120	0	0	19	0	0	11	117	0	267
04:15 PM	14	0	0	19	0	0	11	148	0	322
04:30 PM	159	0	0	00	0	0	9	101	0	274
04:45 PM	147	0	0	9	0	0	S	133	0	291
Total	570	0	0	25	0	0	33	499	0	1154
05:00 PM	129	0	0	6	0	0	6	148	0	295
05:15 PM	72	0	0	21	0	0	19	142	0	336
05:30 PM	151	0	0	11	0	0	17	135	0	314
05:45 PM	164	0	0	16	0	0	17	147	0	344
Total	865	0	0	57	0	0	62	572	0	1289
Grand Total	1168	0	0	109	0	0	98	1071	0	2443
Appreh %	100	0	0	100	0	0	8.1	91.9	0	
Total %	47.8	0	0	4.5	0	0	3.9	43.8	0	

309 326 339 1353

155 152 141 155 603

00000

00000

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

222 222 222 244.1 247 247 247 3,72 3,73 3,73

00000000

37.88

110 4.3

00000000

1231 100 1168 1949 115 144 44

Grand Total Appreh % Total %

Cars
% Cais
Heavy Vehicles
% Heavy Vehicles
Buses
% Buses

Hamingston A verne (Route 9)

From West

11 128

11 125

11 162

5 138

33 531

	Hun	From	furnington Avenue (Route 9) From East			Cumberland Street From South	rom South		Hus	orington Ave	lumington Avenue (Route 9) From West		
Start Time	Thru	Lef	U-Tum	App. Total	Right	Left	U-Tum	Arro. Total	Right	Thru	U-Turn	Arm. Total	Int. Total
Peak Hour Arralysis From 04:00 PM to 05:45 PM - Peak 1 of 1	94:00 PM to 05x	45 PM - Pea	k lof!										
Peak Hour for Entire I	ntersection	Begins at 05:00 PM	15:00 PM										
05:00 PM	129	0	0	129	6	0	0	6	6	148	0	157	295
05:15 PM	154	0	0	154	2.1	0	0	21	16	142	0	191	336
05:30 PM	151	0	0	151	11	0	0	11	17	135	0	152	314
05:45 PM	164	0	0	164	91	0	0	16	17	147	0	164	75
Total Volume	865	0	0	866	57	0	0	2.2	62	572	0	634	1289
% App. Total	100	0	0		100	0	0		8.6	90.2	0		
PHF	610	000	000	610	670	000	900	029	816	990	000	990	037

	Han	Prom East	Hunington Avenue (Route 9) From East			From	Sumberland Street From South		Han	From West	untington Avenue (Route 9) From West		
StartTime	Thro	Lef	U-Tum	App. Total	Right	Teff	U-Tum	Arro. Total	Right	Thru	U-Turn	Are. Total	Int. To
ak Horr Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	500 PM to 054	S PM - Ped	t lof 1										
ak Hour for Entire Int		1 Begins at 05:00 PM	5:00 PM					3.7					
05:00 PM	129	0	0	129	6	0	0	6	6	148	0	157	53
05:15 PM	154	0	0	154	21	0	0	21	119	142	0	191	3
05:30 PM	151	0	0	151	Π	0	0	11	17	135	0	152	33
05:45 PM	164	0	0	164	91	0	0	16	17	147	0	164	ě
Total Volume	865	0	0	868	57	0	0	57	62	572	0	634	128
% App. Total	100	0	0		100	0	0		8.6	90.2	0		
- PHF	.912	000	000	.912	629	000	000	629	918	996	000	996	93

95.2 7 7 1.1 25 3.8

95.0 10 10 35 35 35

136 157 171 630



Groups Printed-Heavy Vehicles Cumberhard Street From South Right Left

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

File Name : 133307 GG Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

S: Cumberland Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 GG Sire Code : 10135.00 Start Date : 5/14/2013 Page No :1

				Groups Printed-Buses	- Buses					
	Hantington /	Hartington Avenue (Route 9) From East	10	Cumber	Oumberland Street From South		Huntington r	Huntington Avenue (Route 9) From West)	
Start Time	Thru	Left	U-Tum	Right	Let	U-Turn	Right	Thru	U-Turn	Int. Total
04:00 PM	2	0	0	0	0	0	0	4	0	9
04:15 PM	7	0	0	0	0	0	0	7	0	14
04:30 PM	4	0	0	0	0	0	0	3	0	7
04:45 PM	6	0	0	0	0	0	0	3	0	12
Total	22	0	0	0	0	0	0	17	0	39
05:00 PM	9	0	0	0	0	0	0	4	0	13
05:15 PM	1	0	0	0	0	0	0	00	0	15
05:30 PM	9	0	0	0	0	0	0	9	0	12
05:45 PM	3	0	0	0	0	0	0	4	0	7
Total	22	0	0	0	0	0	0	25	0	47
Grand Total	4	0	0	0	0	0	0	42	0	98
Appreh %	100	0	0	0	0	0	0	100	0	
Total %	512	0	0	0	0	0	0	48.8	0	

00000

00000

0 4 0

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

000

100 1

000

100

Grand Total Appreh % Total %

	Hen	Humington Avenue (Route 9)	me (Rome 9	6		Oumberland Street	d Sred		Han	Huntington Avenue (Route 9)	use (Route 9)		
		From Eas	East			From South	contin			From West	Vest		
Start Time	Thru	Lef	U-Tum	App. Total	Right	Left	U-Tum	Arp. Total	Right	Thru	U-Turn	Ago, Total	
Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	4:00 PM to 05x	45 PM - Pesk	ljoli										
Peak Hour for Entire Intersection Begins at 04:45 PM	ntersection B	legins at 0.	4:45 PM										
04:45 PM	6	0	0	6	0	0	0	0	0	6	0	3	
05:00 PM	9	0	0	9	0	0	0	0	0	7	0	7	
05:15 PM	7	0	0	7	0	0	0	0	0	00	0	80	
05:30 PM	9	0	0	9	0	0	0	0	0	9	0	9	
Total Volume	28	0	0	28	0	0	0	0	0	24	0	24	
% App. Total	100	0	0	4	0	0	0		0	100	0		
PHF	778	000	000	778	000	000	000	000	000	750	000	750	

	Hun	From East	Huntington Avenue (Route 9) From East			Cumberland Street From South	id Street		Hun	dington Avenue (I	Hundington A venue (Route 9) From West		
Start Time	That	Left	U-Tum	Ann. Total	Right	Teff	U-Tum	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
bed. Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	4:00 PM to 05:-	45 PM - Pea	k l of l										
Peak Hour for Entire Intersection Begins at 04:00 PM	ntersection E	Regins at 0	14:00 PM									1	
04:00 PM	3	0	0	9	0	0	0	0	0	4	0	4	4
04:15 PM	-	0	0	-	0	0	0	0	0	7	0	7	90
0430PM	2	0	0	2	0	0	0	0	0	2	0	2	4
04:45 PM	m	0	0	6	-	0	0	-	0	2	0	2	9
Total Volume	6	0	0	6	1	0	0	1	0	15	0	15	25
% App. Total	100	0	0		100	0	0		0	100	0		
PHF	750	000	000	250	086	900	000	050	000	983	000	yes	781



Groups Printed-Peds and Bicycles Cumberland Street

File Name: 133307 GG Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

S: Cumberland Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette



	63 51234 om
D A T A	P.O. Box 301 Berlin, MA 015 Office-508.481.3999 Fax: 508.54 Email detarequeste@pdillcc

File Name : 133307 GG Sire Code : 10135.00 Start Date : 5/14/2013 Page No :1

	Har	Hundagion Averae (Route 9) From East	ne (Route 9)			From South	outh outh		nn	From West	Huntagion Avenue (Route 9) From West		
Start Time	Thru	Lef	U-Turn	App. Total	Right	Teff	U-Tum	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
eak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1	4:00 PM to 05:	45 PM - Pest	ljoli										
eak Hour for Entire Intersection	ntersection I	Begins at 05:00 PM	S:00 PM	-									
05:00 PM	136	0	0	136	6	0	0	6	6	155	0	164	309
05:15 PM	166	0	0	166	21	0	0	21	20	152	0	172	359
05:30 PM	157	0	0	157	11	0	0	11	17	141	0	158	326
05:45 PM	171	0	0	171	16	0	0	16	17	155	0	172	359
Total Volume	630	0	0	630	2.2	0	0	ST	63	603	0	999	1353
% App. Total	100	0	0		100	0	0		9.5	90.5	0		
PHF	.921	000	000	.921	629	000	000	629	.788	.973	000	896	942
Cars	865	0	0	865	ST	0	0	57	62	572	0	634	1289
% Cars	94.9	0	0	646	100	0	0	100	98.4	6.46	0	95.2	95.3
Heavy Vehicles	10	0	0	10	0	0	0	0	1	9	0	7	17
% Heavy Vehicles	1.6	0	0	1.6	0	0	0	0	1.6	1.0	0	1.1	13
Buses	22	0	0	22	0	0	0	0	0	25	0	25	47
% Buses	3.5	0	0	3.5	0	0	0	0	0	4.1	0	3.8	3.5

29 31 33 33 33 53 53 53 50 50 50 50 50

Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

21 100 3.6

374

163 86.2 27.9

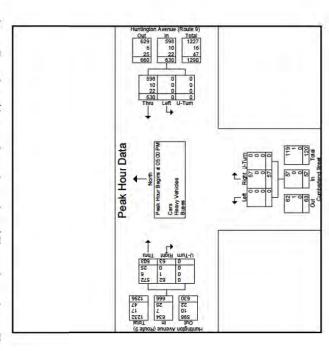
000

26 13.8 4.5

Grand Total Approch % Total %

28282

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total



	Hun	Huntington Aven From E	ne (Route 9)			Cumberland Street From South	Street		Hu	Bom Hom	wenue (Route 9)		
Start Time	That	Left	Peds	App. Total	Right	Left	Peds	App. Total	Right	Thru	Peds	App. Total	Int. Total
esk Hour Analysis From 0	1 04:00 PM to 05:45 PM - Peak 1 of 1	45 PM - Peak	cl of l										
Peak Hour for Entire J	Intersection B	legins at 04	4:45 PM	1									
04:45 PM	2	0	22	24	0	0	53	53	0	9	0	9	83
MG 00:00	w	0	27	32	0	0	23	53	0	2	0	2	87
05:15 PM	S	0	20	25	0	0	20	70	0	1	0	1	96
05:30 PM	m	0	22	25	0	0	20	20	0	-	0	-	92
Total Volume	15	0	16	106	0	0	226	226	0	10	0	10	342
% App. Total	14.2	0	85.8		0	0	100		0	100	0		
200	450	900	0.43	000	0000	NOV.	-00	200	0000	4114	9000	***	100

N/S: Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 H Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette

Office:208.481.399 Far:308.5451234 Emait datarequesta@pdifc.com

File Name: 133307 H Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

Y	PRECISION	DATA	INDUSTRIES, LLC	cx 301 Berlin, MA 01503
	-	_	100	P.O. Be

		Belidere Street	Street		Huntin	Huntington Avenue (Route 9)	se (Route 9	0	*	West Newton Street	n Street		Humin	Humington Avenue (Route 9)	e (Route 9		
		From North	douth			From East	199			From South	outh			From West	lest.		
StartTime	Right	Thru	Left	U-Tum	Right	Thru	Left	U-Tom	Right	Thru	reft	U-Tum	Right	Thru	Left	U-Turn	Int. Total
07:00 AM	2	10	14	0	36	16	24	10	14	33	15	0	9	61	17	0	351
07:15 AM	00	12	7	0	62	124	18	10	13	33	27	0	9	11	1	S	418
07:30 AM	n	13	22	0	44	66	14	13	17	41	26	0	14	20	29	1	417
07:45 AM	6	13	15	2	17	140	25	91	15	63	22	0	13	86	34	3	545
Total	24	48	88	2	219	484	81	88	89	170	06	0	36	333	87	6	1731
08:00 AM	10	13	=	-	100	126	35	13	20	53	12	0	7	100	27	-	524
08:15 AM	4	19	91	2	55	153	30	20	12	64	14	0	2	82	23	1	497
08:30 AM	12	13	13	-	99	131	28	23	6	43	16	0	8	78	30	1	462
08:45 AM	7	18	13	0	92	127	32	19	11	40	16	0	11	108	30	3	514
Total	33	63	53	4	287	537	125	75	25	200	2	0	20	368	110	9	1997
Brand Total	57	П	111	9	908	166	206	133	1111	370	154	0	89	102	197	15	3728
Appreh %	20	38.9	38.9	2.1	27.6	X	11.2	7.2	17.5	58.3	24.3	0	6.1	72.1	20.3	1.5	
Total %	1.5	6	m	0.2	13.6	26.6	5.5	3.6	m	6.6	4.1	0	1.6	18.8	53	0.4	

			om North	From North
ght Thru Left U.T.	Total Right Thru Left U.T.	The Approve Right Thru Left U.T.	Left U-Tun Apartons Right Thru Left U.T.	Thru Left U-Tun Apatons Right Thru Left U.T.
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61

Grand Total Appreh % Total %

Humith glora A venue (Route 9).
From West
Age Yost Right This Left U-Tun Age Yost Int Tool

Huntington A venue (Route 9)

From East S.A.M. - Peak I of 1

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| Peak Hoar Too Entire Information Begin |
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N/S. Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 H Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S: Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 H Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1



		Belidere Street From North	Street		Huntin	gion Avenue (Huntington Avenue (Route 9) From East	Ţ	*	West Newton Street From South	Street		Humbn	Hundington Avenue (Route 9) From West	ue (Route	(6	
Start Time	Right	Thru	Left	Left U-Turn	Right	Thru	Left	Left U-Tum	Right	Thru	Left	U-Turn	Ri ght	Thru	Left	U-Turn	Int. Total
07:00 AM	0	-	0	0	2	s	0	0	0	0	0	0	0	1	3	0	12
07:15 AM	0	0	0	0	-	7	-	0	-	0	0	0	0	8	cı	0	10
07:30 AM	0	0	0	0	0	1	-	0	0	7	0	0	0	3	2	0	15
07:45 AM	0	-	0	0	6	3	-	0	0	0	0	0	0	0	4	0	12
Total	0	2	0	0	9	17	3	0	-	7	0	0	0	7	11	0	49
08:00 AM	0	0	0	0	m	9	-	0	0	0	0	0	0	-	7	0	13
08:15 AM	0	-	0	0	6	7	0	0	0	0	0	0	0	0	5	0	=
08:30 AM	-	0	0	0	7	00	0	0	0	0	0	0	0	0	4	0	15
08:45 AM	-	0	0	0	0	9	-	0	0	0	-	0	0	-	4	0	14
Total	2	T	0	0	00	22	7	0	0	0	1	0	0	2	15	0	53
Grand Total	2	8	0	0	14	39	S	0	-	17	-	0	0	6	26	0	102
Appreh %	9	09	0	0	24.1	67.2	9'8	0	25	20	25	0	0	25.7	74.3	0	
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	4	Belidere Street	Street		1	Auriting ton	untington Avenue (Route 9)	(Ronte 9	(West	West Newton Street	street		B	unting ton	Avenue	furnington Avenue (Route 9)	1 1 1	
		From North	orth				From Bas				4	rom South	4			-	From West	*		
Right Thru	18	Left	U-Tuen	App Total	Right	Thru	Len	U-Tuen	Age, Total	Right	Three	Left	U-Tum	Age, Thesi	Right	Thru	Len	U-Turn	Age. Toni	los Total
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_	0	0	0	-	0	9	-	0	7	0	0	-	0	-	0	-	4	0	5	14
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		Belix	Belidere Street From North			Hunt	ington A	Huntington Avenue (Route 9)	(6 appo			West	West Newton Street From South	pect		£	m tingson	A venue (venue (Route 9)		
Start Time	Right	Thru	Left	Tum Aco	Age, Total	Right	hau	Left U.	Then A	U-Turn App. Deal	Right	Thru	IzeR	U-Turn Age Total Right	Ages Total	Right	The	Tell	U-Tues	Age. Desi	Int. Total
Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1	is From 0.	:00 AM to	0 08 345 A.	M - Peak 1	ofI																
Peak Hour for Entire Intersection Begins at 08:00 AM	Entire L	ntersect	ion Beg	ins at 08.	00 AM																
08:00 AM	0	0	0	0	0	1	7	0	0	14	0	6	7	0	10	0	6	7	0	S	24
08:15 AM	0	-	-	0	2	5	5	6	7	15	0	2	0	0	2	0	2	-	0	2	22
08:30 AM	-	-	-	0	m	00	4	1	0	13	-	1	0	0	2	-	4	11	0	7	25
8:45 AM	-	-	0	0	2	6	1	-	0	17	0	-	0	0	1	-	V.	•	0	6	50
Total Volume	2	6	2	0	7	56	23	S	2	86	-	7	2	0	10	2	14	00	0	24	100
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	2000	200		WWW	500	2000		1		000		****		0000			000		000	-	

N/S: Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 H Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client VHB/ M. Houdlette

File Name : 133307 H Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

U	ECISION	ATA	NUSTRIES, LLC	to1 Berlin, MA 01503	1,3999 Fac. 308,545,1234
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63 16	44 63 16	2 44 63 16	17 2 44 63 16	21 17 2 44 63 16
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		330	6 163 330	6 163 330
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Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

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08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

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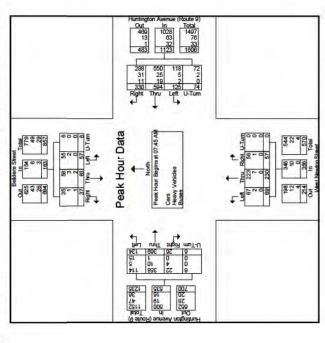
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Grand Total Appreh % Total %



		Beli	Belidere Street From North	*		Ħ	untington	Yrom East	fundington A venue (Route 9) From East	0		Wesk	West Newton Street From South	Street		2	Huntington A venue (Route 9) From West	rom We	(Route	6	
~	seht.	Then	Left	Peds	Ages Total	Right	The	Leg	Peds	App. Des	Right	Thru	Left	Peds	Age, Total	Right	The	Lef	Peds	Age. Desi	Int. Total
VSIS F	10m 07	00 AM 8	0 08:45 A	M - Pea	ik lof!																
FE	ntire In	tersect	ion Beg	zins at	08:00 A	W															
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_	0	-	11	126	129	-	-	0	62	Z	0	m	0	37	40	0	0	0	35	35	268
30 AM	0	0	0	123	123	0	-	0	72	23	-	3	0	37	4	-	-	0	40	42	279
_	0	7	-	134	137	0	2	0	104	100	0	-	0	46	47	0	0	0	37	37	327
Volume	0	4	m	200	207	2	4	0	299	305	-	=	-	154	167	-	-	0	132	134	1113
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N/S: Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 HH Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S: Belidere E/W: Hunting City, State: Bo Client: VHB/

File Name: 133307 HH Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

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	ie (Route S	Loft	19	25	31	17	92	37	32	25	32	126	218	18.3	5.4
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	Humin	Right	13	12	4	00	37	00	12	10	14	4	18	8.9	7
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	Street	Left	10	13	10	17	20	=	91	00	7	42	92	21.1	2.3
	West Newton Street From South	Thru	24	34	34	26	118	30	24	34	36	124	242	55.6	9
680	A	Right	12	11	4	13	80	00	=	18	14	51	101	23.2	2.5
	,	U-Tum	15	12	13	17	22	25	16	23	17	81	138	7.1	3.4
	Huntington Avenue (Route 9) From East	Left	31	27	32	45	135	32	39	33	47	151	286	14.8	1
	gion Avenue From East	Thea	66	114	1117	124	484	134	132	131	140	537	166	513	24.4
	Huntin	Right	89	62	59	09	240	71	63	99	11	277	517	26.8	12.7
		U-Tum	0	2	2	0	4	7	-	0	2	S	6	1.8	0.2
	treet	Left	20	19	21	19	62	17	12	23	32	66	178	35.3	4.4
	Belidere Street From North	Then	23	20	29	22	94	34	39	56	34	133	727	45	5.6
		Right	=	12	11	S	36	=	14	16	10	51	8	17.9	2.2
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Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

Grand Total Appreh % Total %

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05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

246 19.6 5.8 218 88.6

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9 1.7

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23 23 99 93.8

Grand Total
Appreh %
Total %
Cars
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Heavy Vehicles
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888 20.8 852 95.9 1.9 1.7

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05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

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venue (Route 9) n West	U-Turn			e	7	9	4	20	3.1	714
Avenue	Left			37	32	25	32	126	9.61	851
unting too	Thru			811	116	102	116	452	70.4	850
H	Right			00	17	10	14	4	6.9	787
	App. Thes			49	51	9	57	217		OUT
treet h	U-Turn			0	0	0	0	0	0	(MAX)
West Newton Street From South	Lef			11	91	00	1	42	19.4	959
West	Three			30	24	34	36	124	57.1	195
	Right			00	=	18	14	51	23.5	200
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funtington Avenue (Route 9) From East	U-Tuen			25	16	23	11	81	7.7	010
Avenue rom East	Len			32	36	33	47	151	14.4	0003
ming ton	Thru			134	132	131	140	537	513	050
H	Right		7	17	8	99	11	277	26.5	800
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* -	U-Tuen	M - Peak	gins at (7	-	0	2	s	1.7	363
dere Stre	Left	0 0 5 45 P	tion Be	17	27	23	32	66	34.4	472
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	Right	S From 0	Entire 1	11	14	16	10	SI	17.7	TOT
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Huntington Avenue (Route 9)

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	PRE	DON	P.O. Boy 301
	Newton Street	(Route 9)	

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F	PRECIS	D A J
	E	Dage of the state

1	PRECISIO D A T INDUSTRIES,LI
	on Street 9)

Z	PRECISION	DATA	INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 01503
	e Street/ West Newton Street	noton Avenue (Route 9)		oston, MA

F	PRECISI	D A T	P.O. Box 301 Berlin,
	st Newton Street	e (Route 9)	

Z	PRECISION	D A T A	P.O. Box 301 Berlin, MA 01503 Office:508.481.3999 Far: 208.545.1234
	Street/ West Newton Street	gton Avenue (Route 9)	ston, MA M Hondlette



N/S. Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 HH Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

N/S: Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 HH Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

7	PRECISION	DATA	INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 01503
				-

		Belidere Street From North	Street		Huntin	gion Avenue (Huntington Avenue (Route 9) From East	Ti	×	West Newton Street From South	Street		Humi	Hundington Avenue (Route 9) From West	ue (Route Vest	(6	
StartTime	Right	Thru	F	U-Tum	Right	Then	Left	U-Tum	Right	Thru	Left	U-Turn	Right	Thru	Loft	UrTum	Int. Total
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04:15 PM	-	-	0	0	4	50	2	0	0	0	0	0	0	4	4	0	19
04:30 PM	0	0	0	0	4	9	0	0	0	0	0	0	0	0	4	0	17
04:45 PM	0	0	0	0	4	00	-	0	0	-	0	0	-	7	2	0	15
Total	1	-	0	0	16	24	4	0	0	-	0	0	-	00	10	0	9
05:00 PM	0	0	0	0	7	7	-	0	0	0	0	0	0	-	9	0	17
05:15 PM	0	0	0	0	3	00	0	0	0	0	0	0	0	4	4	0	I
05:30 PM	0	0	1	0	2	2	-	0	0	0	0	0	0	3	7	0	14
05:45 PM	0	0	0	0	4	60	0	0	0	0	0	0	0	-	4	0	7
Total	0	0	1	0	=	23	7	0	0	0	0	0	0	6	16	0	9
Grand Total	1	1	1	0	27	4	9	0	0	1	0	0	1	17	26	0	128
Appreh %	33.3	33,3	33.3	0	33.8	58.8	7.5	0	0	100	0	0	2.3	38.6	59.1	0	
Total %	8.0	0.8	80	0	21.1	147	47	0	0	80	0	0	80	13.3	200	0	

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Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

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mington /	Thro	4	0	2	1	7	31.8	4000
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Street	U-Tum	0	0	0	0	0	0	2000
West Newton Street From South	Left	0	0	0	0	0	0	000
West	Thu	0	0	-	0	1	100	000
	Right	0	0	0	0	0	0	000
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Belidere Street From North	Left to 05:45	otton Bk	0	0	0	0	0	WWW
Be	Thru 04:00 PM	Interse	0	0	0	1	20	000
	Right sis From	r Entire	0	0	0	1	20	000
	Start Time Right Thru L. Peak Hour Analysis From 04:00 PM to 0.	Peak Hour for Entire Intersection Begins 04:15 PM 1 1 0	04:30 PM	04:45 PM	05:00 PM	Total Volume	% App. Total	

	Pag Bank	bre Street	w .		Hu	mangron	A venue ((6 anno			West Ne	ration Str	100		Hu	ntington	A venue (Route 9)		
Right		Left	U-Tum A	No. Ton	Right		Leg	-Tues	Dead .	_		Left	Then Ap			The	Tel	J.Turn		Int. Total
om 04:	DO PM to	05:45 P	M - Peak	1 Jo																
ire In	tersect	on Beg	gins at 0	4:00 PA	V															
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Grand Total Appreh % Total %

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

P RECISION
D A T A
NDUSTRIES, LLC
NO. 201 EIN, M. O. 1003
OR. COS. 201 EIN, M. O. 1003

N/S: Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 HH Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Belidere Street/ West Newton Street E/W: Huntington Avenue (Route 9) City, State: Boston, MA Client: VHB/ M. Houdlette

File Name: 133307 HH Sire Code: 10135.00 Start Date: 5/14/2013 Page No: 1

PRECIS	DA	INDUSTRI	P.O. Box 301 Berl e-508.481.3999	mail defaredues
			allo	

		Be	From North	th the		H	and implications	Huntington Avenue (Route 9) From East	(Route 9)			West	West Newton Street From South	leed h		H	inting ton	funtington Avenue (Route 9) From West	(Route 9)		
Start Time	Right	Thru	_	Left U-Turn App Total	Ann Total	Right	Thru	Iseff	Urben	Ago, Total	Right	Than	Left	U-Tum	Ago, Tiesi	Right	Thru	Left	U-Tuen	Age, Total	Int. Total
eak Hour Analysis From 04:00 PM to 05:45 PM - Peak I of	is From C	M-000 PM	50.05:45	PM - Peal	tlofi																
eak Hour for	Entire	Intersec	tion Be	in suize	mersection Begins at 05:00 PM	V															
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05:45 PM	=	34	32	2	2	81	146	47	17	291	14	36	1	0	57	14	120	36	4	174	109
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Buses	0	0	-	0	-	11	23	2	0	36	0	0	0	0	0	0	6	16	0	25	62
% Buses	0	0	1.0	0	0.3	38	40	-	0	33	0	0	0	0	0	0	0 1	11.3	0	37	27

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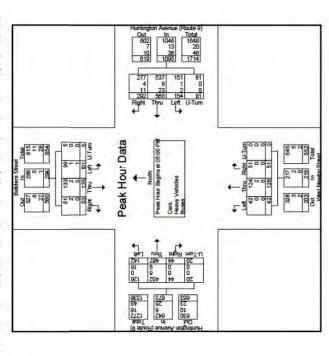
Start Time 04:00 PM 04:15 PM 04:30 PM 04:45 PM Total

mue (Route 9)

Groups Printed-Peds and Bicycles
enue (Route 9) West Newton Street

Right

Right



Hunington Avenue (Route 9) From West	Ago toni Right Thru Left Peds Ago toni Int Ton		_	1 0 0 32 33	43	1 0 0 67 68	247 4 1 0 191 196 1738	
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N/S/NW: Hotel Driveway/ Dalton Street E/W: Behidere Street

Groups Printed-Cass - Heavy Vehides - Buses Dalton Street From South

City, State: Boston, MA Client: VHB/ M. Houdlette

73

The

Then Right

Start Time 0730 AM 07315 AM 0730 AM 0735 AM Total

File Name : 133307 I Site Code : 10135.00 Start Date : 5/14/2013 Page No :1

N/S/NW: Hotel Driveway/ Dalto E/W: Belvidere Street City, State: Boston, MA Client VHB/ M. Houdlette

File Name : 133307 I Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

		Hote	From North	way			Belv	Belvidene Street From East	964			From	Prom South	¥ .			Pro	Belvidere Street From West	9			From	Dalton Street From Northwest	w M		
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7:45 AM	0	0	0	0	0	9	901	29	4	0	m	0	2	0	0	0	0	0	0	0	9	-	30	9	0	193
Total	0	0	0	0	0	28	326	73	4	-	13	0	00	3	0	0	0	0	0	0	115	-	112	20	0	604
MA 00:80	0	0	0	0	0	11	143	16	2	0	4	0	6	-	0	0	0	0	0	0	s	~	28	0	0	215
18:15 AM	0	0	0	0	0	12	6	21	-	Ü	6	0	9	-	0	0	0	0	0	0	9	-	35	61	-	191
18:30 AM	0	0	0	0	0	2	8	17	-	-	ė	0	61	0	0	0	0	0	0	0	S	0	26	4	0	142
8:45 AM	0	0	0	0	0	12	06	22	-	0	2	0	6	0	0	0	0	0	0	0	4	1	27	4	0	166
Total	0	0	0	0	0	37	413	91	S	4	12	0	14	5	0	0	0	0	0	0	20	4	911	10	1	714
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PRECISI
Iton Street



N/S/NW: Hotel Driveway/ Dalton Street E/W: Belvidere Street City, State: Boston, MA Client: VHB/ M. Houdlette

File Name : 133307 I Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

PRECISION D. A. T. A. MOUSTRIES, L.C.

File Name : 133307 I Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

THE PARTY OF THE P	P.O. Box 301 Berlin, MA 01503	Office-508.481,3999 Fac: 908.545.1234	Email datarequests@pdillccom	

		P.C	Office
N/S/NW: Hotel Driveway/ Dalton Street	Belvidere Street	, State: Boston, MA	VHB/ M. Houdlette
/S/N	E/W: Be	City,	Client

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Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

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N/S/NW: Hotel Driveway/ Dalton Street E/W: Belvidere Street

City, State: Boston, MA Client: VHB/ M. Houdlette

From Street

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Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

File Name : 133307 I Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S/NW: Hotel Driveway/ Dalton Street E/W: Belvidere Street City, State: Boston, MA Client: VHB/ M. Houdlette

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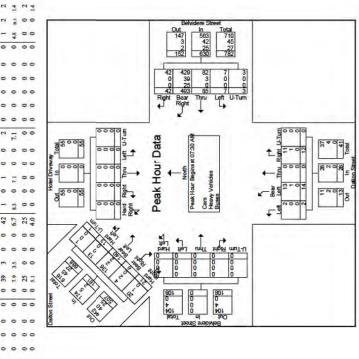
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PRECISION D A T A	P.O. Box 301 Berlin, MA 01503 Office-508.481.3999 Fax: 508-545.1234 Emait datarequest@pdillc.com

File Name : 133307 I Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

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N/S/NW: Hotel Driveway/ Dalton Street E/W: Behvidere Street City, State: Boston, MA Client: VHB/ M. Houdlette

Groups Printed-Cass - Heavy Vehides - Buses Dalton Street From South

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Then Right

File Name : 133307 II Site Code : 10135.00 Start Date : 5/14/2013 Page No :1

N/S/NW: Hotel Drive E/W: Belvidere Street City, State: Boston, MA Client: VHB/ M. Houc

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File Name : 133307 II Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

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Hotel Driveway
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N/S/NW: Hotel Driveway/ Dalton Street E/W: Belvidere Street

City, State: Boston, MA Client: VHB/ M. Houdlette

Let

Right

Start Time 04400 PM 04415 PM 04415 PM 0445 PM Total

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File Name : 133307 II Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S/NW: Hotel Driveway/ Dalton Street E/W: Belvidere Street City, State: Boston, MA Client: VHB/ M. Houdlette



File Name: 133307 II Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

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N/S/NW: Hotel Driveway/ Dalton Street E/W: Belvidere Street City, State: Boston, MA Client: VHB/ M. Houdlette

From Street

From Street

From South

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Log Hotel Driveway From North Then Right

Start Time 04400 PM 04415 PM 0445 PM 0445 PM Total

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File Name : 133307 II Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

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N/S/NW: Hotel Driveway/ Dalton Street E/W: Belvidere Street City, State: Boston, MA Client: VHB/ M. Houdlette

PRECISION	D A T A INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 01503 Te e-508.481.3999 Fax: 508.5451234 Emait datarequests@pdilic.com
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File Name : 133307 II Sire Code : 10135.00 Start Date : 5/14/2013 Page No : 1

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N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA

Client: VHB/ M. Houdlette

File Name : 133307 J Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client VHB/ M. Houdlette

Office-508.481.3999 Far: 508.545.1234

File Name: 133307 J Site Code: 10135.00 Start Date: 5/14/2013 Page No: 1

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7	PRECISION D A T A	INDUSTRIES, LLC	P.O. Box 301 Berlin, MA 01503

		F	Fire Station From North	a ,c			Here	Hereford Street From Northeast	15 26			Boyle	Boylston Sreet From East	*			Prof	Dalton Street From South	*			Boyle	Boylston Street From West	*		
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07:30 AM	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	53	21	0	43	0	57	55	12	0	0	219
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	18	34	0	49	0	52	57	7	-	0	218
Total	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	83	96	0	991	0	193	207	20	-	0	198
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08:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30	30	0	51	0	28	Z	19	0	0	252
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	24	20	0	9	0	52	89	-	-	0	212
08:45 AM	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	31	26	0	36	0	65	9	91	-	0	240
Total	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	611	68	0	210	0	225	253	54	2	0	955
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	Right	23	20	36	25	101	43	38	33	35	149	253	292	12.9	200	366	27	10.7	24	56
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Boylston Street From East	The	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Boyle	Right	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
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	Start	07:00 AM	07:15 AM	07:30 AM	07:45 AM	Total	08:00 AM	08:15 A M	08:30 AM	08:45 AM	Total	Grand Total	Appreh %	Total %	Cars	% Cars	Heavy Vehicles	N Inn o Volution	Buses	% Buses



N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client: VHB/M. Houdlette



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Left Ē

Start Time 07:00 AM 07:15 AM 07:30 AM 07:35 AM Total

08:05 AM 08:15 AM 08:30 AM 08:45 AM Total

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File Name: 133307]
Site Code: 10135.00
Start Date: 5/14/2013
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N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client VHB/ M. Houdlette



File Name : 133307 J Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

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		Fr	Fire Station From North	e .c			From	Hereford Street From Northeast	191			Boyls	Boylston Sreet From East	*			Pron	Dalton Street From South				Boyls	Boylston Street From West	*		
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07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0	0	7	0	0	1	0	0	0	7
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	c	0	0	0	0	7	0	0	0	S
07:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0	0	2	0	-	N	0	0	0	00
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10	2	0	9	0	-	00	0	0	0	27
08:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	8	0	0	2	0	0	-	0	0	0	00
08:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	4	0	-	6	0	0	0	10
08:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9	0	0	-	0	-	0	0	0	0	00
08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-	0	0	3	0	-	2	0	0	0	7
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	14	0	0	10	0	3	9	0	0	0	33
Gmm Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	24	2	0	91	0	4	4	0	0	0	99
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Total %	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	40	3.3	0	26.7	0	6.7	233	0	0	0	

155

Section by Eq. (a) Eq. (b) Eq. (c) Eq.				Fire S	Fire Station From North				Fro	fereford Street from Northeast	Hereford Street From Northeast				Boy	Boylston Street From East	Treed St				Prom	Dalton Street From South	5 4				Boylston Street From West	ylston Street from West			
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North	1 5		ection	0	0	0	0	0	0	9
Fire Station From North	49	1	nters	0	0	0	0	0	0	
EE	The L	BE45 AM	Entire Intersection Begins at 07:45 AM	0	0	0	0	0	0	9
	Rapid	THE AMERICA	Tor En	0	0	0	0	0	0	000
	Start Time R	How Amb to Press 100, Abl to \$545 Abl.	ak Hour	TAS AM	8:00 AM	38:15 AM	30 AM	Total Williams	St. No. Tree	PHF on on on on

N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client: VHB/M. Houdlette

PRECISION
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NODOSTRIBES,LIC
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File Name : 133307 J Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client VHB/ M. Houdlette

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		-	Fire Station From North	North				ž £	Hereford Street From Northeast	Hereford Street From Northeast				Boy	Boylston Sreet From East	Sred	ŀ	-	ŀ	Fro	From South	N G				Boyle Fro	Boylston Street From West	100		
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45 AM	2	0	0	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0	15 2	7	0 42	0 2	01 0	04 67	7 7	17	1	0	156	_
Total Velena	6	0	0	0	0	6	0	0	0	0	0	0	0	0	0	0		0	6 61	8	0 22	0 8	1	2 233	5 299	\$ 62	2	0	866	-
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Buses	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0	0 14	0 6	2	4	m	9	0	0	6	33
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1 6 2 8 2 4

22248

75

Teg. Dalton Street From South Thu 12

75

Right

aroups Printed-Peds and Bicycles Boylston Street

Fire Station From North Left Ē

Start Time 07:00 AM 07:15 AM 07:30 AM 07:45 AM Total

10114 4

76 49.4 7.6

23 23

207

323

162

Grand Total Appreh % Total %

08:00 AM 08:15 AM 08:30 AM 08:45 AM Total

	Out in Total 372 0 372 56 0 56 20 0 20 448 0 448	
	448 0 448 0 448 0 0 0 0 0 0 0 0 0 0 0 0	
000 000 000 000 000 000 000 000 000 00	Peak Hour Data North Peak Hour Begins at 05:00 AM Peak Hour Begins at 05:00 AM Blass	
	1	+
	Boylatin Street Boylatin Boylatin Street Boylatin Boylatin Street Boylatin Boylatin Street Boylatin Boylatin Street	

Boylston Street Boylston Street Boylston Street From South From West	a The Loft nos on age on The Loft nos on the The Loft nos on the Loft nos on the Loft		0 0 37 37 0 0 0 3 35 38 2 8 0 0 7 17 135		0 0 65 65 0 0 0 0 39 39 5 11 0 0 17 33 185) 0 0 215 215 0 0 0 4 M3 147 18 40 0 0 47 105 667	0 0 100 0 0 0 27 503 171 381 0 0 448	
	Pode App News Rapid	1	23 23 0 0	3 23 0 0	7 27 0 0	1 41 0 0	114 0 0	0 0	
Hereford Street From Northeast	111	00 AM	0 0 0 0 2	0 0 0 0 2	0 0 0 0 2	0 0 0 0	0 0 0 0	0 0 0 0	
Fire Station From North	ge the Left lies as Apr	Entire Intersection Begins	0 0 0 0 0 00	0 0 0 0 25 25	0 0 0 0 21 21	0 0 0 0 20 20	98 98 0 0 0 0	0 0 0 0 0	
	Sucr Time R.	Peak Hour for I	MA 00:00	08:15 AM	08:30 AM	08:45 AM	Total Videos	SAME TOR	



N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client: VHB/ M. Houdlette

Right

E

Start Time O4400 PM O4:15 PM O4:15 PM O4:30 PM O4:45 PM Total

File Name : 133307 JJ Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

ulton Street Street/ Hereford St IA
N/S: Fire Station/Dall E/W/NE: Boylston St City, State: Boston, M.



File Name : 133307 JJ Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

		Fr	Fire Station From North	9.5			From	Hereford Street From Northeast	181			Boyl	Boylston Sreet From East	70			From	Dalton Street From South	* -		ď.	Boyle	Boylston Street From West	16		
Start	Pight	E	Loft	1 5	U-Thre	1 2	12	1 5	3 8	U-The	1 2	Right	Thru	Left	U.Da	Paght	12	Thru	Left	ti-Tues	Right	Thru	15	Left	U. Tue.	lar Total
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	25	30	0	37	0	45	103	18	0	0	258
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	36	28	0	57	0	49	2	14	0	0	263
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	31	42	0	47	0	35	16	19	0	0	250
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	42	42	0	62	0	33	11	22	0	0	278
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	134	142	0	203	0	162	335	73	0	0	1049
M4 00:50	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	38	37	0	63	0	42	1	15	0	0	272
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	40	94	0	74	0	20	82	12	0	0	304
05:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	38	28	0	72	0	45	81	21	0	0	285
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30	21	0	65	0	53	93	Ξ	0	0	303
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	146	162	0	274	0	190	333	59	0	0	116
Grand Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	280	304	0	477	0	352	899	132	0	0	22 13
Approch %	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	26.4	28.7	0	45	0	90%	28	11.5	0	0	
Total %	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	12.7	13.7	0	21.6	0	15.9	302	9	0	0	

			Fire St From	Station				出土	Hom Northeast	1 Street				B	From	Boylston Street From East				T	Prom South	South				Bo	rom V	Boylston Street From West			
Start Time	Rade	T)	Left	1 5	8	ė.	1	1	1	1	ń į	*	1	100	F	1.cf	*	4	RES	1	E.	- Series		ŧ,	-	Thru	1	No.	6		In Total
Pout I car Assets & a Pin	and de Penns titte Palis Ch. 43 FB4 -	110.00	1								1		1	1	1	1			1	1	١	ı			١	ı					L
Peak Hou	for	Entire		ntersecti	on Be	Begins at 0	# 05	8	Z																						
M9 00:30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	38	37	0	63	0	138	42	11	2	0	0	34	272
MS:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9	46	0	74	0	99	20	22	2	0	0	44	304
M9 05:30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	38	28	0	72	0	38	45	18	17	0	0	47	285
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30	15	0	9	0	46	8	8	-	0	0	21	303
Total Waters	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-	0	0	146	162	0	274	0	285	061	393	66	0	0 3	582	2
No Age Tree	0	0	0	0	0		0	0	0	0	0		0	0	0	0	0		12	27.8	0	129	0		978	100	10	0	0		
PHF	000	000	000	900	000	000	900	000	000 000	8		000	200 000 000 000	0.00			000	000	91.0	200	000	90.0	4	000	200	200	-	400	9	000	0.00

Boylston Street
From West

Dalton Street

Dalton Street

From South

Tom Tage 1 the Tage 1 to Ann

Tage 1 the Tage

Boylston Street From East The Left

10.00

Herdrind Street
From Northeast
The feet from the
358 298 332 4 4 4 1.1 1.1 0.6

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

0 142 288 0 150 295 0 160 315 0 0 601 177 0 0 808 956 0 808 958 0 808 114 0 0 113 1.1 0 188 33

Seet Time | 14-of | 14



N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client: VHB/ M. Houdlette

Right

Left Ē

Start Right 1.1inc 0450 PM 0 04:15 PM 0 04:30 PM 0 04:45 PM 0 04:45 PM 0 Total 0

Greed Total Appreh % Total %

File Name : 133307 JJ Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client VHB/ M. Houdlette

File Name : 133307 JJ Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

											9		CAUCH LINEAR BUSIN	200												
		F	Fire Station From North	e .c			From	Hereford Street From Northeast	net ret			Boyle	Boylston Sreet From East	*			Prom	Dalton Street From South				Boylett	Boylston Street From West			
Start	Paght	The	Loft	1	U-Thre	12	1 2	15	3 8	U. Day	1 2	Right	Thru	Left	T. Maria	Pight	12	Thru	Left	ti-Thus B	Right	Thru	15	Left	U. Dare.	for Total
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	0	0	6	0	0	6	0	0	0	9
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-	0	0	100	0	-	-	-	0	0	1
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	S	0	0	9	0	0	3	0	0	0	14
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0	0	10	0	-	6	0	0	0	6
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	12	0	0	15	0	13	10	-	0	0	9
M4 00:50	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	4	0	0	m	-	0	0	15
05:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7	0	0	2	0	0	7	0	0	0	9
05:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	S	0	0	-	0	0	1	-	0	0	00
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	-	0	2	0	0	m	0	0	0	=
Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	19	1	0	6	0	0	6	5	0	0	9
Gmmd Total	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	31	4	0	24	0	73	19	m	0	0	80
Approb %	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	55.4	8.1	0 4	67	0	8.3	19.2	12.5	0	0	
Total %	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	38.8	12	0	30	0	2.5	23.8	3.8	0	0	

	In Total		7	4	6	15	45		250
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	R. C.		-	'n	7	7	15	9 89	77.7
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Street	10		0	0	0	0	-	_	
Boylston Street From East	ě		0	0	0	0	0	0	000
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Street	1 5		0	0	0	0	0	0	900
foreford Street from Northeast	1:	V	0	0	0	0	0	0	900
Ho H	11	IS PA	0	0	0	0	0	0	000
	11	8	0	0	0	0	0	0	900
П	ė į	zins	0	0	0	0	0	1	000
	8 3	n Be	0	0	0	0	0	0	000
gon orth	3 5	ntersection	0	0	0	0	0	0	900
ire Station from North	- Up	Inters	0	0	0	0	0	0	900
ш, ш,	The	Entire Inte	0	0	0	0	0	0	000
	100		0	0	0	0	0	0	000
	Start Time	Peak Hour for	04:15 PM	04:30 PM	04:45 PM	05:00 PM	Total Volume	N Ann Teel	PHF

	Then	1164.69	Entire	0	0	0	0	0	0	000
	Rade	marter Pe	rfor	0	0	0	0	0	0	000
	Start Time	Fred Il on Amb de Propi 4th Belack Co.	Peak Hour for Entire	04:15 PM	04:30 PM	04:45 PM	MG 00:50	Total When	No Age Tree	PHF
	- Total	I		5	1	00	9	26		813
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	÷ ;			0	0	0	0	0	0	6
Street	40			0	0	0	0	0	0	000
Boylston Street From West	13			0	0	-	0	-	979	240
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	S age	l		0	-	0	-	7	=	900
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	9 ;	١		0	0	0	0	0	0	000
alton Street from South	Les	١		-	0	-	-	9	375	
Dalton Street From South	The same			0	0	0	0	0	0	000 30
_	1 1			0	-	0	0	-	2.5	240
	-			0	-	7	-	4	20	300
	ŧ ;			0	0	0	0	0	i	000
	3 1			0	0	0	0	0	0	900
Boylston Street From East	Toff	l		0	0	0	0	0	0	000
From	Rade Thes			0	0	0	0	0	0	90
	Right			0	0	0	0	0	0	000
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	*]			0	0	0	0	0		000
25 16	9 1	١		0	0	0	0	0	0	000
Hereford Street From Northeast	13			0	0	0	0	0	0	000
ierefor rom N	1		Σ	0	0	0	0	0	0	000
田匠	11		115 P	0	0	0	0	0	0	000
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	n.		on B	0	0	0	0	0	0	000
ire Station from North	1		rsect	0	0	0	0	0	0	000
Fire Static	Les	1	e Inte	0	0	0	0	0	0	000
	Maga: Then	Second Property lies	Entin	0	0	0	0	0	0	000
	-	Ban 64 52 71	Ir for	0	0	0	0	0	0	900
	Survivae	fred four teadow Free beite bie bet fer fer Free frei e f.	Peak Hour for Entire In	04:15 PM	04:30 PM	04:45 PM	05:00 PM	Test Volume	WAR TOR	PHF

N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client: VHB/M. Houdlette

roups Printed-Peds and Bicycles
Boylston Street

Fire Station From North Left Ē

Start Time 0430 PM 04:15 PM 04:15 PM 04:35 PM Total

File Name : 133307 JJ Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

Pods las Treat 16 325 15 303 22 312 19 311 72 1251

m 9 t

75

Teg. Thu 12

75

Right

21 319 30 319 18 439 32 386 101 1463

62 71 78 78 340

05:00 PM 05:15 PM 05:30 PM 05:45 PM Total

Grand Total Appreh % Total %

68.1 68.1 6.4

944

100

N/S: Fire Station/Dalton Street E/W/NE: Boylston Street/ Hereford Street City, State: Boston, MA Client VHB/ M. Houdlette

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File Name : 133307 JJ Site Code : 10135.00 Start Date : 5/14/2013 Page No : 1

503 451234 com
P.O. Box 301 Berlin, MA 01 fix e-508.481, 3999 Fax; 308.5 Emait dearrequesty@pdillo

			Fire Station From North	North				五座	Hereford Street From Northeast	Stree				Be	ylston Sre From East	Boylston Street From East			Ľ	E H	Dalton Street From South	Arred .	1			Boy	Boylston Street From West	Street		
Start Time	Rade	The s	Inch	1 5	0	-	1 1	1	13	1 5	ė į	ŧ]	1 ;	100	Thu	Let	9 1	4]	Sale.	11	The	Left	8 9	į.	T spin	Thru	13	lel.	-10	And In Test
How Auby de Press Call. Belle Et. 4794 - Park.	and diff. III													1	1	1					1	1				-		1		
eak Hour	for	Entire	Inte	rsect	Intersection Begins at 05:00 PM	suigo	at 05	8	Σ																					
05:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	46	37	0	88	0	151		83	9	0	0 14	_
8:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	42	46	0	94	0	3	51	98	2	0	0 14	_
M4 0E 50	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	28	0	73	0	145	45	83	2	0	0 15	150 295
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	36	25	0	89	0	56	23	96	_	0	91 0	
Total Velence	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	891	163	0 2	285	9 0	919		M8 6	19	0	0 60	-
N App. Tree	0	0	0	0	0		0	0	0	0	0	-	0	0	0	0	0		27.3	290	0	163	0		319	6.5	101	0	0	
PHF	000	000	000	000	000	000	000	000	000	000	000	000	000	000	000	000	000	000	516	100	000	918	6 900	939	906	906		000	6. 000	39 963
Cars	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	346	2	0	274	0 8	_	190 3	133 5	66	0	0 58	582 1164
%Cars	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	698	766	0	19	6 0	94.5	9 06	87 9	23	0	96 0	-
Sawy Vill day	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6	0	0	2	0	S	2	9	0	0	0	8 13
S. Iberg	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.8	0	0	1.7	0	8.0	1.0.1	17	0	0	0	13 1.1
Buses	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	61	-	0	6	0	53	0	6	2	0	0	11 40
% Buses	0	0	c	c	0	0	0	C	C	0	c	0	o	0	0	0	C	c	***	90	0	13	0	4.7	0	1 6 3		0		3

**************************************	Boylston Street Out In Total 479 0 479 9 0 479 9 0 9 28 0 28 516 0 516	
	\$ 0 0 0 0	
100000 0000 0000 0000 0000 0000 0000 0	Peak Hour Data Moth Peak Hour Begins at 05:00 PW Core Heavy vehicles Blass	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	19 186 251 0 0 19 886 251 0 0 0 0 0 0 0 0 0 0 0 0	+ 4[]
	Boylston Street Boylston Stree	

Boylston Street From West	the last we		1 0 21 31	2 0 30 42	2 0 18 39	0 0 32 44	S	32 0 647	2000
	Arr Rage Then		-	-	7	-	73 5 45	3.2	į
Street	Spin Now The Left Ro.		2 2 0 3 62	1 3 0 4 71	1 1 0 6 129	2 6 0 2 78	6 12 0 15 340	16 3.2 0 4 9.2	100 000
Boylston Street	Age that Rage The Left rate Am		0 0 0 0 170	0 0 0 0 146 146	81 0 0 0 0	0 0 0 0 171	0 0 0 0 675 675	0 0 0 0 100	000
fereford Street	11	Me	0 0 18	0 0 16	0 0 27	0 0 0 0 32	0 0 0 0 93 93	0 0 0 0 000	100
Fire Station From North	A	ntire Intersection Begin	0 0 0 31 31	0 0 0 0 36 36	0 0 0 0 48 48	0 0 0 21	0	0 0 0 100	****
	Survivae	Peak Hour	05:00 PM	MS:15 PM	05:30 PM	05:45 PM	Town Videox 0	NAME TOR	CLIE

2013 Existing Condition Synchro Reports

HCM Signalized Intersection Capacity Analysis 1: Boylston Street & Massachusetts Avenue

2013 Existing Conditions Moming Peak Period

EBT 1900 1300 1300 1300 1300 1300 1300 1300	WBL 1900	100							
1900 1900 1900 1900 1900 1900 1900 1900	1 2 -	- MA	WBR	NBL	NBT	NBR	SBL	SBT	SBR
1900 1900 1900 1900 1900 1900 1900 1900		4	*	1	44		*	44	
12 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15		1900	1900	1900	1900	1900	1900	1900	1900
4.0 0.95 0.93 1.00 2745 0.94 2584 2584 2093 0.93 0.93 0.93 0.93 0.93 0.23 0.23 5.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2		12	10	10	10	9	9	9	10
0.95 0.93 1.00 2.15 2.15 0.94 2.21 0.93 0.94 2.00		4.0	4.0		4.0		4.0	4.0	
0.93 1.00 0.94 1.00 0.94 2.84 2.1 422 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93		1.00	1.00		0.95		1.00	0.95	
100 0.97 100 2745 0.94 254 23 454 10% 8% 11 Perm 7 7 7 7 22.0 23.		1.00	0.67		0.97		1.00	96.0	
100 210 221 221 23 454 103 23 454 108 8% 11 Perm 7 7 7 22.0 23.0		1.00	1.00		1.00		1.00	1.00	
1.00 2745 094 2884 093 093 093 093 093 093 094 098 108 8% 11 0023 0023 0023 0023 0023 0023 0023 0		1.00	0.85		0.99		1.00	0.99	
2745 0.94 26.94 26.94 23 454 0 584 0 584 10% 8% 11 Perm 7 7 7 22.0 23.0 0.23 5.0 23.0 0.23 5.0 23		1.00	1.00		1.00		0.95	1.00	
21 284 284 23 454 0.93 0 23 454 1 0 25 0 25 10% 8% 11 Perm 7 7 7 22.0 23.0 0.23 5.0 2.0 23.0 23.0 23.0 23.0 23.0 23.0 23.		1502	860		2626		1307	2679	
21 422 1 23 493 0 23 494 2 10% 8% 11 Perm 7 7 22.0 23.0 0.23 0.23 0.23 0.23 0.23 0.23		0.99	1.00		0.94		0.95	1.00	
21 422 1 23 454 1 0 25 0 0 25 0 0 584 2 10% 8% 11 Perm 7 7 7 7 7 22.0 23.0 0.23 5.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2		1486	860		2469		1307	2679	
23 454 10 0 884 11 10% 8% 11 22.0 23.0 0.23 6.02 88.3 1.00 88.3 1.00 88.3 1.00 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8	2	100	208	14	678	64	182	497	34
23 454 1 0 25 0 25 10% 8% 11 Perm 7 7 22.0 23.0 0.23 5.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 38.3 1.00 38.3 1.00 32.2 70.5 E	99'0	990	990	0.95	0.95	0.95	0.91	0.91	0.91
10% 8% 11 Perm 7 7 7 22.0 23.0 0.23 5.0 0.23 5.0 0.28 38.3 1.00 32.2 7.0 594 50.5 E F 70.5 E		152	315	15	714	67	200	546	37
10% 8% 11 Perm 7 7 7 22.0 23.0 0.23 5.0 2.0 2.0 2.0 2.0 2.0 2.0 3.2.2 7.0.5 E 70.5 Delay 3	0	0	243	0	0	0	0	0	0
10% 8% 11 Perm 7 7 22.0 23.0 0.23 6.023 6.		155	72	0	796	0	200	583	0
10% 8% 11 Perm 7 7 22.0 23.0 23.0 23.0 23.0 23.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2			294	,)	441			288
Perm 7 7 7 7 22.0 23.0 0.23 5.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2			-			87			110
Perm 7 22.0 23.0 0.23 5.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	%0	14%	2%	%0	10%	12%	16%	8%	9%9
7 7 22.0 23.0 0.23 0.23 5.0 2.0 2.0 2.0 594 694 698 38.3 1.00 2.2 2.3 38.3 1.00 2.0 38.3 1.00 2.0 5.9 6.9 8.3 8.3 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	Perm		Perm	Perm			Prot		
7 22.0 23.0 0.23 5.0 2.0 2.0 2.0 2.0 38.4 38.3 1.00 32.2 70.5 E 70.5		1			-		2	15	
22.0 23.0 0.23 0.23 5.0 2.0 2.0 38.4 1.00 1.00 2.0 38.3 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	1		7	-					
23.0 0.23 5.0 2.0 2.0 2.0 38.3 1.00 1.00 2.25 70.5 E		22.0	22.0		34.0		24.0	63.0	
0.23 5.0 2.0 2.0 594 60.23 0.38 38.3 1.00 1.00 7.0.5 E 7.0.5		23.0	23.0		35.0		26.0	65.0	
5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0		0.23	0.23		0.35		0.26	0.65	
(vph) 594 (vph) 594 (vph) 594 (d1 38.3 cdor 1.00 lay, d2 32.2 e E f (s) 70.5 mmany Control Delay		5.0	5.0		5.0		6.0		
(vph) 594 c0.23 d1 38.3 cacor 1.00 lay, d2 32.2 e E y (s) 70.5 mmany Control Delay		2.0	2.0		2.0		2.0		
d1 38.3 co.23 co.2		CVE	108		86.4		340	1741	
c023 d1 88.3 cdor 1.00 lay, d2 32.2 e E E y (s) 70.5 mmany		4	000		8		20 15	0 22	
d1 38.3 cdor 1.00 lay, d2 32.2 70.5 e		010	800		0000		2	1	
d1 38.3 cdor 1.00 lay, d2 32.2 e E E y (s) 70.5 mmany		0.00	0.00		000		0 80	0 33	
at 138.3 lay, d2 32.2 lay, d2 32.2 e E E y (s) 70.5 mmany		0.40	200		0.92		000	200	
cdor 1,000 199, d2 32.2 6 F 70.5 70.5 mmany Control Delay		33.1	32.4		31.2		32.3	. 9	
lay, d2 32.2 70.5 e E E y (s) 70.5 mmary Control Delay		1.00	1.00		0.41		1.00	1.00	
70.5 F 70.5 mmary Control Delay		0.3	4.0		14.9		7.3	0.5	
e E 70.5 mmary Control Delay		33.4	32.8		27.8		39.6	8.3	
y (s) 70.5 mmary Control Delay		O	O		O		۵	A	
mmary Control Delay		33.0			27.8			16.3	
		O			O			8	
	Ī	HCM Level of Service	el of Se	arvice		۵			
ratio									
		Sum of lost time (s)	st time	(s)		16.0			
Utilization 77.		ICU Level of Service	of Ser	NOe		۵			
Analysis Period (min)									

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Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 2: Belvidere Street & Massachusetts Avenue

2013 Existing Conditions Morning Peak Period

	1	1	-	-	ţ	1	-	+	•	•	→	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations					1			114			AT.	
deal Flow (vohol)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
ane Width	12	12	12	12	14	12	10	10	10	10	10	10
otal Lost time (s)		!			4.0		2	4.0	2		4.0	
ane I Hil Factor					100			0 95			0 95	
mh pad/hikas					8			000			100	
The pad hikes					88			88			88	
po, pedicines					3 6			38			3 8	
Tit Drotocted					000			88			8 8	
Sate Flow (prot)					1416			2578			2596	
Elt Demitted					66 0			0 94			100	
Satd. Flow (perm)					1416			2414			2596	
Volume (voh)	0	c	0	18	24	56	15	200	0	c	602	20
Peak-hour factor DHF	0 25	0.25	0.25	080	080	080	0 96	0 95	0 95	0 00	0 92	0 00
Adi Flow (upb)	9	9	9	36	30	200	4 6	737	3	200	BEA	200
OTOP Beduction (unb)	0 0	0	0	1	3 9	2	20	5	0 0	0 0	5	10
Con Croun Flore (unb)	0 0	0	0 0	0 0	200	0 0	0 0	753	0 0	0 0	674	0 0
Conf River (#Arr)	0	>	0	•	7))	3	•	•	1	103
Heavy Vehicles (%)	700	700	700	1004	NOV	707	700	100%	700	700	400%	20%
ing Pleakage (#/hr)	200	200	9 0	2 0	2 0	2 0	200	2 1	9 0	200	2	5 0
Darking (#/hr)	0	>	0	7		7	0		•	•	7	9 +
Calvally (mylli)				-	-	-		-			-	
lum lype				Split	•		Perm				4	
Protected Phases				m	3			-			-	
Permitted Phases					2		-					
Actuated Green, G (s)					12.8			58.8			58.8	
Effective Green, g (s)					14.8			80.8			809	
Actuated g/C Ratio					0.15			0.61			0.61	
Clearance Time (s)					6.0			0.9			6.0	
Vehicle Extension (s)					2.0			2.0			2.0	
ane Grp Cap (vph)					210			1468			1578	
//s Ratio Prot					60.09						0.26	
v/s Ratio Perm								00.31				
v/c Ratio					0.53			0.51			0.43	
Jniform Delay, d1					39.7			112			10.4	
Progression Factor					1.0			0.24			0.70	
ncremental Delay, d2					2.6			12			0.8	
Delay (s)					42.3			3.9			8.0	
evel of Service					٥			V			4	
Approach Delay (s)		0.0			42.3			3.9			8.0	
Approach LOS		×			٥			4			4	
ntersection Summary	ı		ŀ						ì			
HCM Average Control Delay	elay		8.7	-	ICM Lev	HCM Level of Service	ivice		A			
HCM Volume to Capacity ratio	y ratio		0.53									
Actuated Cycle Length (s)	S)		100.0	ב מ	of omn	Sum of lost time (s)	(s)		4.4			
Analysis Period (min)	IIIZation		15	=	O Leve	ICO Level of Service	80		•			
Critical Lane Group												

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VHB, Inc.

2013 Existing Conditions Morning Peak Period HCM Unsignalized Intersection Capacity Analysis 3: Saint Germain Street & Massachusetts Avenue

	-	1	+	1	•	_	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	*		*			**	
Sign Control	Stop		Free			Free	
Grade	%0		%0			%0	
Volume (veh/h)	-	2	710	0	0	620	
Peak Hour Factor	0.50	0.50	0.94	0.94	06.0	0.90	
Hourly flow rate (vph)	2	10	755	0	0	689	
Pedestrians			161			159	
Lane Width (ft)			10.0			10.0	
Walking Speed (fl/s)			4.0			4.0	
Percent Blockage			=			1	
Right turn flare (veh)							
Median type	None						
Median storage veh)							
Upstream signal (ft)			1002			222	
pX, platoon unblocked	0.89						
vC, conflicting volume	1261	537			755		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1173	537			755		
tC, single (s)	8.9	7.3			4.1		
tC, 2 stage (s)							
tF (s)	3.5	3.5			2.2		
bo deene free %	66	16			100		
cM capacity (veh/h)	149	396			864		
Direction, Lane #	WB 1	NB 1	NB 2	SB 1	SB2		
Volume Total	12	378	378	344	344		
Volume Left	2	0	0	0	0		
Volume Right	10	0	0	0	0		
SH	310	1700	1700	1700	1700		
Volume to Capacity	0.04	0.22	0.22	0.20	0.20		
Queue Length 95th (ft)	3	0	0	0	0		
Control Delay (s)	17.1	0.0	0.0	0.0	0.0		
Lane LOS	O						
Approach Delay (s)	17.1	0.0		0.0			
Approach LOS	O						
Intersection Summary							
Average Delay Intersection Capacity Utilization	tilization	ľ	41.8%	ū	ULeve	ICU Level of Service	<
Analysis Period (min)			15				

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Synchro 6 VHB, Inc.

VHB, Inc.

HCM Signalized Intersection Capacity Analysis 4: St. Stephen & Massachusetts Avenue

2013 Existing Conditions
Morning Peak Period

2013 Existing Conditions Moming Peak Period HCM Signalized Intersection Capacity Analysis 5: Huntington Avenue & Massachusetts Avenue

Movement	+ + +	1	+	•	*	→	•
1700 1700 1700 1700 1700 1700 1700 1700							
1700 1700 1700 1700 1700 1700 1700 1700	WBL WBT	SR NBL	NBT	NBR	SBL	SBT	SBR
1700 1700 1700 1700 1700 1700 1700 1700	414		44			++	K_
12 11 12 12	1700 1700	1700 1600	1600	1600	1600	1600	1600
7.5 0.95 0.96 0.96 0.96 0.96 0.97 2269 0.97 2269 0.97 2269 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.9	11 11	11 12	12	16	12	10	10
0.95 0.96 0.96 0.96 0.97 0.97 0.97 0.97 0.97 0.97 0.98 0.88 0.88 0.88 0.88 0.88 0.88 0.88	7.5		7.0			2.0	7.0
0.96 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97	0.95		0.95			0.95	1.00
1.00 0.95 0.95 0.97 2269 0.97 2269 0.86 0.86 0.86 0.86 0.86 0.86 0.87 0 0 143 0 0 143 0 0 143 0 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 0 143 0 0 0 0 0 143 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.89		1.00			1.00	1.00
0.95 2269 0.97 2269 0.86 0.86 0.86 0.86 0.86 0.86 0.86 0.87 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.9	1.00		1.00			1.00	1.00
0.97 2269 0.97 2269 0.86 0.86 0.86 0.86 0.86 0.86 0.87 0.97 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.94		0.99			1.00	0.85
2269 2269 104 2269 0.86 0.86 0.86 0.86 0.86 0.81 10 17 10 17 18 18 2 2 3 18 2 3 18 6 0.16 0.16 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18	860		1 00			100	1 00
269 104 08 63 89 0.86 0.86 0.84 121 10 73 106 0 0 143 0 0 0 0 143 0 0 0 0 143 0 0 0 2% 27% 10% 2% Split Split Split 2 2 3 37.4 0.16 6.0 2.0 2.0 2.0 2.0 37.4 0.38 37.2 10.0 0.38 37.4 0.0 0.3 37.4 0.0 0.3 37.4 0.0 0.3 0.3 0.3 0.3 0.3 0.3 0.3	2179		2489			2343	1058
2269 104 9 63 89 0.86 0.86 0.86 0.86 0 143 0 0 0 0 143 0 0 0 17% 27% 10% 2% 5plit Split Split 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	860		100			100	100
104 9 63 89 0.86 0.86 0.84 0.84 1 1 10 73 106 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 146 0 0 16 0 0 16 0 0 16 0 0 16 0 0 17 0	2179		2489			2343	1058
0.86 0.86 0.86 0.84 121 10 73 106 0 0 143 00 0 143 0 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 16 0 0 0 16 0 0 0 16 0 0 0 174 0	89 28	87 0	944	88	c	791	70
121 10 73 106 0 0 143 0 0 0 143 0 0 0 143 0 0 0 143 0 0 0 145 0 0 16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	084 094	160 76	0 91	0 91	96 0	960	96 0
7% 27% 10% 2% 59lt 59lt 59lt 59lt 59lt 59lt 59lt 50lt 50lt 50lt 50lt 50lt 50lt 50lt 50	106 30		1037	26	0	824	73
Split 2% 2% 2% 58 9 9 7 8 2% 2% 2% 2% 2% 2% 2 3 3 4 6.0 6.0	78		7	0	0	0	0
58 77, 27% 10% 2% Split Spli	0	0	1127	0	0	824	73
9 2% 2% 10% 2% 2% 10% 2% 2% 3% 2% 3% 2% 2% 3% 2% 2% 2% 2% 2% 2% 2% 2% 2% 2% 2% 2% 2%		151					
(e) T% 27% 10% 2% 5plit Split	6	-		25			52
Split Split Split (s)	2% 13%	8% 0%	8%	10%	%0	%6	8%
2 2 3 (s)	Split						Prot
s (e) 18.0 (s) 16.5 0.16 (s) 0.16 (h) 2.0 h) 37.4 h) 0.38 0.38 0.38 0.38 0.2 7.4 37.4 9) 37.4 1.00 b) 37.4 1.00 1.0			-			-	-
18.0 16.5 0.16 6.0 2.0 2.0 37.4 0.2 37.4 0.2 37.4 D D D 37.4 D D 37.4 D D 37.4 D 100.0 O.75 O.75 O.18 37.4 D 100.0 O.75 O.18 O.75 O.18 O.75 O.18 O.75 O.18 O.75 O.18 O.75 O.18 O.75 O.18 O.75 O.18 O.75 O.75 O.75 O.75 O.75 O.75 O.75 O.75							
16.5 0.16 6.0 2.0 37.4 0.38 37.2 1.00 0.2 37.4 37.4 1.00 0.2 37.4 1.00 0.2 0.2 37.4 0.2 0.2 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	18.0		44.0			44.0	44.0
0.16 6.0 2.0 374 c0.06 0.38 37.2 1.00 0.2 37.4 D D 37.4 D D 37.4 D D 37.4 D D 37.4 D D 37.4 D D 100 0.2 37.4 D D 100 0.2 37.4 D D D D D D D D D D D D D	16.5		45.0			45.0	45.0
6.0 2.0 374 c0.06 0.38 37.2 1.00 0.2 37.4 0.2 37.4 0 0.2 37.4 0 0.2 37.4 0 0.2 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1	0.16		0.45			0.45	0.45
2.0 37.4 0.38 37.2 1.00 2 37.4 0.2 37.4 0.2 37.4 0.2 37.4 0.2 37.4 0.2 37.4 0.2 100.0 100.0 100.0	6.0		8.0			8.0	8.0
374 0.06 0.38 37.2 1.00 0.2 37.4 0.2 37.4 0.2 37.4 0.7 0.05 0.7 0.05 0.75 0.05 0.75 0.05 0.75 0.05 0.75 0.05 0.75	2.0		2.0			2.0	2.0
c0.06 0.38 37.2 1.00 0.2 0.2 37.4 0.2 37.4 0.2 37.4 0.7 0.7 0.7 0.75 0.00 0.75 0.00 0.75 0.00 0.75	360		1120			1054	476
0.38 37.2 1.00 0.2 0.2 37.4 D D 37.4 D 37.4 D 37.4 D 37.9 Trol Delay 36.8 pacify ratio 0.75 ogth (s) 100.0 sight (s) 65.2%	20.00		c0.45			0.35	0.07
0.38 37.2 100 0.2 37.4 0.2 37.4 0.37 100 Delay 36.8 100.0 100.0 100.0 100.0							
37.2 1.00 42 0.2 37.4 37.4 57.4 57.4 57.4 57.4 57.4 57.4 57.4 5	0.42		1.01			0.78	0.15
d2 1.00 d2 0.2 37.4 37.4 D D 37.4 D ST.4 D D ST.4 D D ST.4 D ST.7 D ST.7 D D ST.7 D ST	37.5		27.5			23.3	16.2
d2 0.2 37.4 D D 37.4 D 37.4 Trol Delay 36.8 pacify ratio 0.75 gght (s) 100.0 gght (s) 65.2%	1.00		1.00			0.46	0.45
37.4 D 37.4 37.4 any Trol Delay pacify ratio 0.75 gght (s) 100.0 gyth (s) 400.0	0.3		28.5			2.0	0.2
ary 36.8 100.0 100	37.7		56.0			12.7	7.1
37.4 DD	٥		ш			8	4
any any 36.8 rol Delay 36.8 0.75 ggh (s) 100.0 ggh (s) 4.0 hization 65.2%	37.7		56.0			12.3	
36.8 0.75 100.0 65.2%	۵		ш			8	
36.8 0.75 100.0 65.2%							
0.75 100.0 65.2%	Ī	f Service		۵			
100.0							
65.2%		me (s)		22.0			
4		Service		3			
Analysis Period (min)	-						

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Synchro 6 VHB, Inc.

HCM Unsignalized Intersection Capacity Analysis 6: Huntington Avenue & Driveway West

2013 Existing Conditions Morning Peak Period SBR 0.85 554 3.6 554 Stop 0% 0.85 13.0 4.0 4.0 3.5 100 439 None 453 6.8 276 0.95 61 133 61 1700 0.08 0.0 WBR WB 2 0.08 WB 1 ABT Pree 0% 204 0.95 2.15 507 0.92 0 208 11.0 4.0 0.00 Free \$ 260 0.95 0.000000 484 2.2 100 885 **48** Direction, Lane #
Volume Total
Volume Left
Volume Right
cSH
Colume to Capacity
Queue Length 95th (#)
Control Delay (s)
Lane LOS Lane Width (ft)
Walking Speed (ft's)
Walking Speed (ft's)
Percent Biockage
Right turn flare (veh)
Median type
Median storage veh)
Upstream signal (ft)
pX, platoon unblocked
vC, conflicting volume
vC, conflicting volume
vC, stage I conf vol
vCz, stage 2 conf vol Volume (veh/h)
Peak Hour Factor
Hourly flow rate (vph)
Pedestrians Movement
Lane Configurations
Sign Control
Grade tC, single (s)
tC, 2 stage (s)
tF (s)
p0 queue free %
cM capacity (veh/h)

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4

ICU Level of Service

33.3% 15

Average Delay Intersection Capacity Utilization Analysis Period (min)

Intersection Summary Approach Delay (s) Approach LOS

- 50 5 0 - 50 5 0

HCM Signalized Intersection Capacity Analysis 7: Huntington Avenue & Cumberland Street

2013 Existing Conditions Morning Peak Period

	†	-	-	ļ	•	•		
Movement	EBT	EBR	WBL	WBT	NBL	NBR		
ane Configurations	441			#		K		
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
ane Width	=	-	=	-	12	16		
Total Lost time (s)	4.0			4.0		4.0		
ane Util. Factor	0.91			98.0		1.00		
Frpb, ped/bikes	1.00			1.00		1.00		
Flpb, ped/bikes	1.00			1.00		1.00		
E	0.99			1.00		0.86		
Fit Protected	1.00			1.00		1.00		
Satd. Flow (prot)	4047			5208		1443		
Fit Permitted	1.00			1.00		1.00		
Satd. Flow (perm)	4047			5208		1443		
Volume (vph)	514	28	0	701	0	48		
Peak-hour factor, PHF	060	060	0.95	0.95	0.67	790		
Adi Flow (vph)	571	3.1	0	738	C	72		
RTOR Reduction (vph)	6	0	0	0	0	67		
ane Group Flow (vph)	599	0	0	738	0	u		
Confl. Bikes (#/hr)		12				1		
Heavy Vehicles (%)	%4	%0	%0	462	%0	4%		
Bus Blockages (#/hr)	0	0	20	20	0	0		
Parking (#/hr)	-	-						
Tum Type				ľ	Ö	custom		
Protected Phases	9			12		2		
Permitted Phases								
Actuated Green, G (s)	68.4			78.8		6.4		
Effective Green, g (s)	68.4			78.8		6.4		
Actuated g/C Ratio	0.76			0.88		0.07		
Clearance Time (s)	4.0					4.0		
Vehicle Extension (s)	2.0					2.0		
Lane Gro Cap (vph)	3076			4560		103		
v/s Ratio Prot	c0.15			c0.14		0.00		
v/s Ratio Perm								
//c Ratio	0.19			0.16		0.05		
Jniform Delay, d1	3.0			0.8		39.0		
Progression Factor	1.00			1.00		1.00		
ncremental Delay, d2	0.1			0.0		0.1		
Delay (s)	3.2			0.8		39.0		
evel of Service	V			V		٥		
Approach Delay (s)	3.2			0.8	39.0			
Approach LOS	×			4	0			
Intersection Summary								
HCM Average Control Delay)elav		3.8	I	CM Lev	HCM Level of Service	A	
HCM Volume to Capacity ratio	ty ratio		0.20					
Actuated Cycle Length (s) Intersection Capacity Utilization	(s)		90.0	ωS	um of lo	Sum of lost time (s)	15.2 A	
Analysis Period (min)			15					

HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

city Analysis 2013 Existing Conditions
Street Morning Peak Period

	n	1	†	-	•	-		1	-	-	•	1
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBL	NBT	NBR	SBU
Lane Configurations		K	44	7	7	K	**	K		4		
Ideal Flow (vohol)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	1	10	11	10	10	11	11	12	16	12	12
Total Lost time (s)		40	4.0	0		4.0	4.0	4.0		40		ļ.
Lane Util. Factor		1.00	0.95			1.00	0.95	1.00		100		
Frah pad/hikas		100	96 0			1 00	1 00	0.58		1 00		
Elph pad hikes		8	100			100	200	100		000		
Et long beginning		88	000			88	98	0 85		000		
Elt Drotocted		000	000			0 06	88	200		000		
Safe Flour (prot)		1272	2704			1464	2025	200		1810		
Catal Flow (Plot)		200	200			200	100	3 5		200		
Sate Flow (norm)		1272	2704			1464	2026	252		1676		
Volume (mp)	q	424	900	90	1.4	425	200	230	00	200	13	1
Volume (vpn)	0 0	4 6	000	9 9	4 00	071	400	200	000	250	200	0
Peak-hour tactor, PHF	0.92	0.80	0.86	0.86	0.95	0.94	0.94	0.94	0.88	0.88	0.88	0.82
Adj. Flow (vph)	1	156	460	8	78	133	632	351	78	261	92	-
RTOR Reduction (vph)	0	0	2	0	0	0	0	228	0	7	0	0
Lane Group Flow (vph)	0	163	485	0	0	211	632	123	0	397	0	0
Conff. Peds. (#/hr)				134				467				
Confl. Bikes (#/hr)				-				2			12	
Heavy Vehicles (%)	%0	15%	3%	15%	5%	%9	2%	13%	3%	3%	5%	%
Parking (#/hr)			-	-						5		
Tum Type	Prot	Prot			Prot	Prot		Perm	Perm		3	D.P+P
Protected Phases	2	2	2		-	-	9			4		63
Permitted Phases								9	4			4
Actuated Green, G (s)		14.3	32.7			15.7	34.1	34.1		25.4		
Effective Green, g (s)		14.3	33.7			15.7	35.1	35.1		26.4		
Actuated g/C Ratio		0.14	0.34			0.16	0.35	0.35		0.26		
Clearance Time (s)		4.0	5.0			4.0	5.0	5.0		5.0		
Vehicle Extension (s)		2.0	2.0			2.0	2.0	2.0	ĺ	2.0	1	
Lane Grp Cap (vph)		196	910			228	1030	253		442		
v/s Ratio Prot		0.12	0.18			00.15	00.22					
v/s Ratio Perm								0.17		00.24		
v/c Ratio		0.83	0.53			0.93	0.61	0.49		0.90		
Uniform Delay, d1		41.7	26.8			41.6	26.8	25.4		35.5		
Progression Factor		1.00	1.00			0.80	40.	2.68		1.00		
Incremental Delay, d2		23.9	2.2			38.6	2.7	6.5		19.9		
Delay (s)		65.6	29.0			71.9	30.6	74.7		55.4		
Level of Service		ш	O			ш	O	ш		ш		
Approach Delay (s)			38.2				50.9			55.4		
Approach LOS			٥				۵			ш		
Intersection Summary												
HCM Average Control Delay	Delay		46.1	Ť	HCM Level of Service	rel of Se	envice		٥			
HCM Volume to Capacity ratio	ty ratio		0.70									
Actuated Cycle Length (s)	(s)		100.0	0) 2	Sum of lost time (s)	st time	(s)		15.0			
Analysis Period (min)	UIIZATIOLI		15	-	ICO Level of Service	10 IO IO	3		2			

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HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

2013 Existing Conditions Morning Peak Period 37 0.93 0 0 1100 SBR 37.6 38.6 0.39 8% 57 0.93 61 33.6 34.6 0.35 4.0 2.0 0.07 0.07 0.07 1.00 0.2 24.1 24.3 4.0 1.00 1.00 1.00 0.95 0.31 517 4% Total Lost time (s)
Lane Util Factor
Fith, ped/bikes
Fit
Fith Protected
Satd Flow (prot)
Fit Promitted
Satd Flow (prot)
Fit Peas-hour factor, PHF
Adj. Flow (vph)
RTOR Reduction (vph)
RTOR Reduction (vph)
Confl. Bikes (#hrr)
Confl. Bikes (#hrr)
Confl. Bikes (#hrr)
Confl. Bikes (#hrr)
Feavy Vehicles (%)
Parking (#hrr)
Tum Type
Protected Phases
Permitted Phases
Actuated Green, g (s)
Effective Green, g (s)
Actuated Green, G (s)
Lane Gro Cap (vph)
Lane Gro Cap (vph) Movement Lane Configurations Ideal Flow (vphpl) Lane Width

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VHB, Inc.

Synchro 6 VHB, Inc.

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HCM Unsignalized Intersection Capacity Analysis 9: Belvidere Street & Dalton Street

Sign Control

2013 Existing Conditions Morning Peak Period SBR 24 0.90 27 SBT Stop 6 0.90 139 14 0.78 Stop 15 0.78 NBT 0.78 WBR 493 0.81 609 Stop 84 WBT 0.81 282 30 0 27 27 5.8 0.05 593 7.9 0.25 158 154 0 0.55 6.9 0.30 505 11.6 11.0 B 3 41.0-6.0 573 9.4 4 Stop 0.25 NB 1 EBT 0.25 726 10 609 609 609 4.3 6.30 820 28.9 28.9 28.9 WB 1 EBL Volume Left (vph)
Volume Right (vph)
Had (s)
Departure Headway (s)
Degree Utilization, x
Capacity (veh/h) Hourly flow rate (vph) Control Delay (s) Approach Delay (s) Approach LOS Movement Lane Configurations Direction, Lane # Volume Total (vph) Volume (vph) Peak Hour Factor

ICU Level of Service 24.5 C 65.7% HCM Level of Service Intersection Capacity Utilization Analysis Period (min) Intersection Summary

1102

19.4 1.00 19.4 19.4 C

Progression Factor Incremental Delay, d2

Delay (s) Level of Service

Uniform Delay, d1

v/s Ratio Perm

v/c Ratio

Intersection Summary Approach Delay (s) Approach LOS

O

HCM Signalized Intersection Capacity Analysis 10: Boylston Street & Dalton Street

2013 Existing Conditions Morning Peak Period

Configurations	1900 12		NBR	SBL		
1900 1900 1900 1900 1900 1900 1900 1900	12 12 12 12 14 15 15 15 15 15 15 15 15 15 15 15 15 15				195	SBR
Flow (vphp) 1900 1900 1900 1900 1900 1900 1900 19	12 12 15 15 15 15 15 15 15 15 15 15 15 15 15					
wwith the (s) 11 12 12 12 12 12 12 12 12 12 12 12 12	2-	18	1900	1900		1900
Lost time (s) 4.0 UH: Factor 0.95 ped/bikes 1.00 Flow (prot) 2611 Flow (prot) 26	4.0 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1		17	12	77	17
pedfolkes 0.99	1.00 1.00 1.00 1.00 1.00 1.00 1.00					
1000 0.98 1.00 2611 1.00 2611 1.00 2611 2611 286 224 0 0 0 0 0 344 260 0 0 0 0 0 345 260 0 0 0 0 0 346 260 0 0 0 0 0 362 37 0 102 0 0 0 0 0 20 0 102 0 0 0 0 0 20 0 102 0 0 0 0 0 102 0 0 0 0 0 102 0 0 0 0 0 103 0 0 0 0 0 103 0 0 0 0 0 104 0 0 0 0 0 105 0 0 0 0 0 0 105 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 0 0 0 0 0 105 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.00 1.00 1.00 0.95 1504					
1.00 0.094 1.00 2611 1.00 2611 2 296 224 0 0 0 0 0 344 260 0 0 0 0 0 562 0 0 0 0 0 0 562 0 0 0 0 0 0 562 0 0 0 0 0 0 102 0 0 0 0 0 0 102 0 0 0 0 0 102 0 0 0 0 0 102 0 0 0 0 0 102 0 0 0 0 0 103 0 0 0 0 0 0 103 0 0 0 0 0 0 103 0 0 0 0 0 0 103 0 0 0 0 0 0 103 0 0 0 0 0 0 103 0 0 0 0 0 0 103 0 0 0 0 0 0 103 0 0 0 0 0 0 103 0 0 0 0 0 0 103 0 0 0 0 0 0 0 103 0 0 0 0 0 0 0 103 0 0 0 0 0 0 0 103 0 0 0 0 0 0 0 103 0 0 0 0 0 0 0 0 103 0 0 0 0 0 0 0 0 0 103 0 0 0 0 0 0 0 0 0 0 103 0 0 0 0 0 0 0 0 0 0 0 103 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.00 1.00 0.95 1504					
0.94 1.00 2611 1.00 2611 1.00 2611 1.00 2611 2.00 0.344 260 0.00 0.00 0.00 0.00 0.00 0.00 0.00	1.00 0.95 1504					
2611 1.00 2611 1.00 2611 2611 2611 2611 2611 2611 2611 2611 2611 2610	1504	_				
2611 100 2610 2 296 224 0 0 0 6 0.86 0.86 0.92 0.92 0.92 0 0 0 0 0 0 562 0 0 0 0 0 562 0 0 0 0 0 562 0 0 0 0 1 39.4 41.4 0.46 6.0 2.0 1.201 18.0 18.0 18.0 19.0 1	1504	1.00				
2611 2611 2612 2612 266 224 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1371				
2611 2 296 224 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.95					
2 296 224 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1504	-				
6 0.86 0.86 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92	0 0	104	139	0	0	10
20 344 260 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000 000		0.85	0 00		000
102 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0		164	10		10
% 15% 4% 0% 0% 0% 1% 1% 1 1 1 1 1 1 1 1 1 1 1 1				0 0	0	0
7 1 39.4 4% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0%		286	0 0	0 0	0 0	0 0
7 15% 4% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0%	,)	•	•	•
1 39.4 41.4 6.0 6.0 2.0 1201 0.27 0.47 16.7 16.7 1.30 18.0 8 0.0 8 A A B 0.0 90.0 Sum of lost time (8 on 41.0% ICU Level of Servi	%0	%9	20%	%0	%0	%0
39.4 41.4 0.46 6.0 2.0 1201 0.22 0.47 16.7 1.00 1.3 18.0 8 18.0 8 18.0 8 18.0 8 0.0 8 0.0 8 0.0 8 0.0 90.0 Sum of lost time (service) of Service of Service) of Service of Servi		L				
1 39.4 41.4 0.46 6.0 2.0 1201 0.22 0.47 1.00 1.3 18.0 8 0.0 8 0.0 A A A A A A A A A A A A A A A A A A A	-	e				
39.4 41.4 0.46 6.0 2.0 1201 0.22 0.47 1.03 1.30 1.						
0.46 6.0 2.0 1201 0.22 0.47 16.7 16.7 1.00 1.3 18.0 B 18.0 B 0.0 A A A A A A A A A A A A A A A A A A	21.2	21.2				
0.46 6.0 2.0 1201 0.22 0.47 1.00 1.3 18.0 18.0 18.0 18.0 18.0 18.0 19.0 19.0 A A A A A A A A A A A A A A A A A A A	22.2					
6.0 2.0 1201 0.22 0.47 1.00 1.30 1.00 1.30 1.80 1.00 1.30 1.00 1.30 1.00 1.00 1.00 1.0	0.25	0.25				
2.0 0.22 0.47 1.00 1.3 18.0 18.0 18.0 18.0 18.0 18.0 18.0 18.0	5.0	5.0				
1201 0.22 0.47 16.7 1.00 1.3 18.0 8 18.0 8 18.0 8 18.0 8 18.0 9.0 90.0 90.0 90.0 90.0 1.00 41.0% ICU Level of Servi	2.0					
0.22 0.47 16.7 1.00 1.3 18.0 8 B 0.0 8 A A A A A A A A A A A A A A A A A A A	371	338				ľ
0.22 0.47 16.7 1.00 1.3 18.0 B 0.0 B A A 30.2 HDM Level of Sen io 0.60 on 41.0% ICU Level of Servi	0.19	O				
16.7 1.00 1.3 18.0 B 0.0 B 0.0 A A A A A A A A A A A A A A A A 1.0% ICU Level of Servi						
16.7 1.00 1.3 18.0 B 0.0 B A A 30.2 HCM Level of Sen io 0.60 90.0 Sum of lost time (s	77.0	0.85				
1.00 1.3 18.0 B 0.0 B 0.0 A A A A A A A A A A A A A A A A A A 1.0% ICU Level of Servi	31.5					
1.3 18.0 18.0 18.0 18.0 18.0 18.0 18.0 18.0	1 00					
18.0 B 0.0 A 30.2 HCM Level of Service (s) 90.0 Sum of lost time (s) 90.0 to 41.0% ICU Level of Service (s) 90.0 Sum of lost time (s) 90.0 Sum of lo	683					
18.0 A A A 30.2 HCM Level of Sen io 10.0 Sum of lost time (s	39.7	13				
18.0 0.0 A 30.2 HCM Level of Servic 50.0 Sum of lost time (s) on 41.0% ICU Level of Service						
30.2 0 0.60 0 41.0%		44.4			0	
30.2 io 0.60 90.0 on 41.0%	. A					
30.2 io 0.60 90.0 on 41.0%						
on 41.0%	Contract of Contract		(1
90.0	HUM Level of Service		3			
Utilization 41.0%	Sum of lost time (s)		26.4			
	ICU Level of Service		×			
Analysis Penod (min)						

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VHB, Inc.

HCM Signalized Intersection Capacity Analysis 1: Boylston Street & Massachusetts Avenue

2013 Existing Conditions Evening Peak Period

	1	1	-	1	ţ	1	-	←	•	•	-	*
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations		*			4	K		AT		K	4	
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
ane Width	12	13	13	12	12	10	10	10	10	10	10	10
Total Lost time (s)		4.0			4.0	4.0		4.0		4.0	4.0	
Lane Util. Factor		0.95			1.00	1.00		0.95		1.00	0.95	
Frpb, ped/bikes		06.0			1.00	090		0.95		1.00	0.95	
Hpb, ped/bikes		1.00			1.00	1.00		1.00		1.00	1.00	
F		0.97			1.00	0.85		0.99		1.00	0.99	
It Protected		1.00			1.00	1.00		1.00		0.95	1.00	
Satd. Flow (prot)		2832			1601	813		2707		1486	2709	
FIt Permitted		0.95			66.0	1.00		0.95		0.95	1.00	
Satd. Flow (perm)		2703			1589	813	1	2570	ì	1486	2709	Ì
Volume (vph)	6	441	132	2	111	253	7	671	72	188	559	45
Peak-hour factor, PHF	0.92	0.92	0.92	0.93	0.93	0.93	16.0	0.97	0.97	0.97	0.97	0.97
Adj. Flow (vph)	6	479	143	2	119	272	1	692	74	194	576	46
RTOR Reduction (vph)	0	29	0	0	0	199	0	0	0	0	0	0
ane Group Flow (vph)	0	596	0	0	121	73	0	773	0	194	622	0
Confl. Peds. (#/hr)			591			498			803			440
Confl. Bikes (#/hr)			6			2			107			129
Heavy Vehicles (%)	33%	3%	4%	20%	%9	1%	14%	2%	3%	5%	2%	1%
fum Type	Perm	i		Perm	g.	Perm	Perm	10		Prot		
Protected Phases		7			7			-		2	15	
Permitted Phases	7			7		7	-					
Actuated Green, G (s)		25.7			25.7	25.7		35.3		19.0	59.3	
Effective Green, g (s)		26.7			26.7	26.7		36.3		21.0	61.3	
Actuated g/C Ratio		0.27			0.27	0.27		0.36		0.21	0.61	
Clearance Time (s)		5.0			5.0	5.0		5.0		6.0		
Vehicle Extension (s)		2.0			2.0	2.0		2.0		2.0		
ane Gro Cap (vph)		722			424	217		933		312	1661	
//s Ratio Prot										c0.13	0.23	
//s Ratio Perm		c0.22			0.08	0.09		c0.30				
//c Ratio		0.83			0.29	0.33		0.83		0.62	0.37	
Jniform Delay, d1		34.5			29.1	29.5		29.0		35.9	9.7	
Progression Factor		1.00			1.00	1.00		0.45		1.00	1.00	
ncremental Delay, d2		7.3			0.1	0.3		7.1		9.0	9.0	
Delay (s)		41.7			29.2	29.8		20.2		44.9	10.4	
evel of Service		٥			O	O		O		۵	8	
Approach Delay (s)		41.7			29.6			20.2			18.6	
Approach LOS		٥			O			O			00	
Intersection Summary												
HCM Average Control Delay	Delay		26.3	_	CM Lev	HCM Level of Service	arvice		O			
ICM Volume to Capacity ratio	ity ratio		0.78	•								
Actuated Cycle Length (s)	(s)		100.0	S	um of lo	Sum of lost time (s)	(s)		16.0			
Analysis Period (min)	III AUDI		15	2	0.00	5	3		1			
Critical Lane Group												

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HCM Signalized Intersection Capacity Analysis 2: Belvidere Street & Massachusetts Avenue

Analysis 2013 Existing Conditions
Avenue Evening Peak Period

	1	†	*			,	-	-	,		+	•
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					+	-1		44		E	44	1
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	12	12	12	4	12	10	10	10	10	9	9
Total Lost time (s)					4.0			4.0			4.0	
ane Util. Factor					1.00			0.95			0.95	
-rpb, ped/bikes					0.99			3.5			9.0	
Fipb, ped/bikes					1.00			90.			9.0	
-					0.92			90.			00.	
Fit Protected					6.0			0.1			8	
Satd. Flow (prot)					1421			2667			2749	
Fit Permitted					0.99			0.91			1.00	
Satd. Flow (perm)	1				1421			2434			2749	
Volume (vph)	0	0	0	17	36	74	25	677	0	0	677	16
Peak-hour factor, PHF	0.25	0.25	0.25	0.81	0.81	0.81	0.97	0.97	0.97	96.0	96.0	0.96
Adj. Flow (vph)	0	0	0	2	4	91	26	869	0	0	705	17
RTOR Reduction (vph)	0	0	0	0	0	0	0	0	0	0	-	0
ane Group Flow (vph)	0	0	0	0	156	0	0	724	0	0	721	0
Confl. Bikes (#/hr)						2						124
Heavy Vehicles (%)	%0	%0	%0	8%	%0	2%	2%	%9	%0	%0	4%	%0
Bus Blockages (#/hr)	0	0	0	0	0	0	0	7	0	0	0	80
Parking (#/hr)				-	-	-		-			-	-
Tum Type				Split			Perm					
Protected Phases				0	3			-			-	
Permitted Phases							-					
Actuated Green, G (s)					14.6			52.2			52.2	
Effective Green, g (s)					16.6			54.2			54.2	
Actuated g/C Ratio					0.17			0.54			0.54	
Clearance Time (s)					6.0			6.0			6.0	
Vehide Extension (s)					2.0			2.0			2.0	
Lane Grp Cap (vph)					236			1319			1490	
v/s Ratio Prot					8						0.26	
v/s Ratio Perm								00.30				
v/c Ratio					0.66			0.55			0.48	
Uniform Delay, d1					39.1			14.9			14.2	
Progression Factor					1.00			1.21			0.62	
ncremental Delay, d2					5.3			1.6			1.0	
Delay (s)					4.4			19.6			9.8	
evel of Service					٥			m			4	
Approach Delay (s)		0.0			4.4			19.6			9.8	
Approach LOS		4			٥			œ			∢	
Intersection Summary												
HCM Average Control Delay	elay		17.6	I	CM Lev	HCM Level of Service	ivice		æ			
HCM Volume to Capacity ratio	ty ratio		0.58						77.00			
Actuated Cycle Length (s)	s)		100.0	<i>s</i> ⊆	ol o mn	Sum of lost time (s)	(s)		29.2 B			
Analysis Period (min)			15	•			3		1			

	1	1	←	1	•	-	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	*		+			44	
Sign Control	Stop		Free			Free	
Grade	%0		%0			%0	
Volume (veh/h)	7	0	669	0	0	694	
Peak Hour Factor	0.63	0.63	96.0	96.0	96.0	96.0	
Hourly flow rate (vph)	-	2	728	0	0	723	
Pedestrians			352			354	
ane Width (ft)			10.0			10.0	
Walking Speed (fl/s)			4.0			4.0	
Percent Blockage			24			25	
Right turn flare (veh)							
Median type	None						
Median storage veh)							
Jpstream signal (ft)			1002			222	
bX, platoon unblocked	0.86						
vC, conflicting volume	1442	718			728		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1351	718			728		
C, single (s)	7.4	6.9			4.1		
C, 2 stage (s)							
IF (s)	3.8	3.3			2.2		
% eau ene de monte od	85	86			100		
cM capacity (veh/h)	73	284			885		
Direction, Lane #	WB 1	NB 1	NB 2	SB 1	SB 2		
Volume Total	16	364	364	361	361		
Volume Left	-	0	0	0	0		
Volume Right	2	0	0	0	0		
CSH	93	1700	1700	1700	1700		
Volume to Capacity	0.17	0.21	0.21	0.21	0.21		
Queue Lenath 95th (ft)	14	0	0	0	0		
Control Delay (s)	51.3	0.0	0.0	0.0	0.0		
ane LOS	ш						
Approach Delay (s) Approach LOS	51.3 F	0.0		0.0			
Intersection Summary							
Average Delay	1000		9.0	,	1	copies of property	<
mersection capacity offication	IIZAIIOII		200				

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Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 4: St. Stephen & Massachusetts Avenue

2013 Existing Conditions Evening Peak Period

	-	-	-	,			,		•	ł	
Movement	NBL2	NBL	NBT	NBR	SBL	SBT	SBR	SBR2	SER	SER2	
Lane Configurations		¥	44			414		1	W.Z		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Lane Width	10	10	10	10	10	10	10	10	12	12	
lotal Lost time (s)		0.4	4.0			0.4			0.4		
Lane Util. Factor		00.1	0.95			0.95			8.6		
Frpb, ped/bikes		00.1	00.1			0.84			00.0		
Fipp, ped/bikes		3 5	3 5			200			00.0		
700000000000000000000000000000000000000		300	3 8			000			000		
FIT Protected		0.80	00.0			0000			3.5		
Said. Flow (prot)		700	1707			2030			2 5		
Fit Permitted		0.39	00.1			0.0			00.1		
Satd. Flow (perm)	1	020	1797	ľ	1	2181	1	1	1311		
Volume (vph)	28	379	678	7	2	601	58	59	377	17	
Peak-hour factor, PHF	0.98	0.98	0.98	0.98	0.97	0.97	0.97	0.97	0.92	0.92	
Adj. Flow (vph)	27	387	692	2	7	620	30	30	410	18	
RTOR Reduction (vph)	0	0	0	0	0	0	0	0	0	0	
Lane Group Flow (vph)	0	414	694	0	0	682	0	0	428	0	
Confl. Peds. (#/hr)				166	166			546			
Confl. Bikes (#/hr)			7	55			100	18	3		
Heavy Vehicles (%)	%0	1%	2%	%0	%0	2%	%0	%0	1%	%0	
Bus Blockages (#/hr)	0	0	10	10	0	0	12	12	0	0	
Parking (#/hr)	,	,	2	2		,	-	-	-	, -	
	custom	Prot			Perm	ľ		0	custom		
Phasees	2	234	124			-			3.4		
Permitted Phases	34		1		-						
Actuated Green, G (s)		53.0	72.0			29.0			34.0		
Effective Green o (s)		67.0	74.0			310			38.0		
Actional all Datio		2 2 2	27.0			200			900		
Closured go hairo		6.0	1			200			0.00		
Vehicle Extension (s)						0,0					
Verlide Exterision (s)						2.0					
Lane Grp Cap (vph)		539	2092			9/9			472		
V/s Katio Prot		90.16	0.25						00.33		
v/s Ratio Perm		0.28				00.31			2.4		
v/c Ratio		0.77	0.33			1.01			0.91		
Uniform Delay, d1		12.8	4.5			34.5			30.4		
Progression Factor		1.80	0.26			0.54			1.00		
Incremental Delay, d2		3.2	0.2			34.9			20.4		
Delay (s)		26.2	4.1			53.4			50.9		
Level of Service		O	V			٥					
Approach Delay (s)			107			53.4					
Approach LOS			8			٥					
Intersection Summary											
HCM Average Control Delay	Velor		31.5	I	MIN	HCM level of Service	point		C		
HCM Volume to Capacity ratio	ty ratio		0.91			5	3)		
Actuated Cycle Length (s)	(8)		100.0	S	um of lo	Sum of lost time (s)	(8)		12.0		
Intersection Capacity Utilization	ilization	_	85.4%	2	U Leve	ICU Level of Service	100		Ш		
Analysis Period (min)			15								

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VHB, Inc.

HCM Signalized Intersection Capacity Analysis
5: Huntington Avenue & Massachusetts Avenue

Evening Peak Period

Movement El Lane Configurations (17) (deal Flow (vphpl) 177 (and Lost time (s) and Util Factor and Util Factor Frpb, ped/bikes Frt Frotected Satd. Flow (prot) Ft Permitted	EBL	EBT	EBR	OV	WBT		IN	NRT	NBR	SBL	SBT	Cap
suo (s				VVDL	1	WBK	2	1				000
		11			11			AT			**	*
	1700	1700	1700	1700	1700	1700	1600	1600	1600	1600	1600	1600
otal Lost time (s) ane Util. Factor rpb, ped/bikes ripb, ped/bikes rit Protected satd. Flow (prot)	12	11	12	11	11	11	12	12	16	12	10	10
ane Util. Factor Tipb, ped/bikes Tit Protected Satd. Flow (prot)		7.5			7.5			7.0			7.0	7.0
rpb, ped/bikes The ped/bikes The Protected Satd. Flow (prot)		0.95			0.95			0.95			0.95	1.00
ipb, ped/bikes rt It Protected Satd. Flow (prot) It Permitted		0.85			0.88			1.00			1.00	1.00
rt It Protected Satd. Flow (prot) It Permitted		1.00			1.00			1.00			1.00	1.00
It Protected Satd. Flow (prot) It Permitted		0.93			0.95			0.99			1.00	0.85
satd. Flow (prot)		86.0			76.0			1.00			1.00	1.00
It Permitted	***	2080			2195			2624			2455	1131
		86.0			0.97			1.00			1.00	1.00
Satd. Flow (perm)	, 4	2080			2195			2624			2455	1131
Volume (vph)	89	24	101	137	38	85	0	911	75	0	896	80
tor, PHF	98.0	98.0	98.0	0.94	0.94	0.94	96.0	96.0	96.0	0.94	0.94	0.94
	103	28	117	146	40	06	0	949	78	0	953	82
RTOR Reduction (vph)	0	86	0	0	59	0	0	9	0	0	0	0
.ane Group Flow (vph)	0	150	0	0	217	0	0	1021	0	0	953	82
Confl. Peds. (#/hr)			219			351						
			e			-			22			22
icles (%)	2%	8%	3%	%9	3%	3%	%0	3%	%0	20%	4%	1%
	Split			Split								Prot
Protected Phases	N	7		m	n			-			-	-
Permitted Phases		-			1000			200			100	170 000
Actuated Green, G (s)		18.0			18.4			43.6			43.6	43.6
Effective Green, g (s)		16.5			16.9			44.6			44.6	44.6
Actuated g/C Ratio		0.16			0.17			0.45			0.45	0.45
Clearance Time (s)		6.0			6.0			8.0			8.0	8.0
Vehicle Extension (s)		5.0			2.0			2.0			2.0	2.0
ane Grp Cap (vph)	,	343			371			1170			1095	504
//s Ratio Prot	O	c0.07			00.10			c0.39			0.39	0.08
//s Ratio Perm												
//c Ratio		0.44			0.58			0.87			0.87	0.17
Jniform Delay, d1		37.6			38.3			25.1			25.1	16.6
Progression Factor		1.00			1.00			1.00			0.42	0.36
ncremental Delay, d2		0.3			1.5			9.1			3.2	0.2
Delay (s)		37.9			39.8			34.2			13.7	6.2
evel of Service		٥			۵			O			8	4
Approach Delay (s)		37.9			39.8			34.5			13.1	
Approach LOS		٥			۵			O			œ	
ntersection Summary												
HCM Average Control Delay	> 4		26.7	I	CM Lev	HCM Level of Service	ervice		O			
of the capacity is	200		100	0	of go one	Cum of land time (a)	10		000			
ntersection Capacity Utilization	notie	80	84.7%	n ⊆	U Leve	CU Level of Service	(s)		E E			
Analysis Period (min)			13									

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HCM Unsignalized Intersection Capacity Analysis 6: Huntington Avenue & Driveway West

2013 Existing Conditions Evening Peak Period

	1	1	ţ.	1	٠	•	
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		*	44		h	N-	
Sign Control		Free	Free		Stop		
Grade		%0	%0		%0		
Volume (veh/h)	0	0	222	80	0	62	
Peak Hour Factor	0.92	0.92	0.91	0.91	0.70	0.70	
Hourly flow rate (vph)	0	0	244	0	0	89	
Pedestrians		373			373		
Lane Width (ft)		11.0			13.0		
Walking Speed (ft/s)		4.0			4.0		
Percent Blockage		28			8		
Right turn flare (veh)							
Median type					None		
Median storage veh)							
Jpstream signal (ft)		260	202				
oX, platoon unblocked							
VC, conflicting volume	626				621	872	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
VCu, unblocked vol	626				621	872	
C, single (s)	4.1				8.9	6.9	
tC, 2 stage (s)							
tF(s)	2.2				3.5	3.3	
% earl enend oc	100				100	37	
cM capacity (veh/h)	640				281	141	
Direction, Lane #	EB 1	EB 2	WB 1	WB 2	SB1		
Volume Total	0	0	163	06	83		
Volume Left	0	0	0	0	0		
Volume Right	0	0	0	o	68		
cSH	1700	1700	1700	1700	141		
Volume to Capacity	0.00	0.00	0.10	0.05	0.63		
Queue Length 95th (ft)	0	0	0	0	8		
Control Delay (s)	0.0	0.0	0.0	0.0	62.9		
ane LOS					L		
Approach Delay (s)	0.0		0.0		629		
Approach LOS					ıL		
Intersection Summary							
Average Delay			171				
Intersection Capacity Utilization	lization		33.4%	2	C Leve	ICU Level of Service	∢
שואפום ב פווסת לווווויו			2				

HCM Signalized Intersection Capacity Analysis 7: Huntington Avenue & Cumberland Street

2013 Existing Conditions Evening Peak Period

2013 Existing Conditions Evening Peak Period 1900

1900

SBU

1900 12

ABL

	1	-	1	+	1	•	
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
Lane Configurations	441			#		K	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	
Lane Width	=	11	=	-	12	16	
Total Lost time (s)	4.0			4.0		4.0	
Lane Util. Factor	0.91			98'0		1.00	
Frpb, ped/bikes	1.00			1.00		1.00	
Flpb, ped/bikes	1.00			1.00		1.00	
E	0.99			1.00		98.0	
Fit Protected	1.00			1.00		1.00	
Satd. Flow (prot)	4092			5307		1500	
Fit Permitted	1.00			1.00		1.00	
Satd. Flow (perm)	4092	Ì		5307		1500	
Volume (vph)	616	63	0	630	0	22	
Peak-hour factor, PHF	0.97	0.97	0.92	0.92	0.68	0.68	
Adj. Flow (vph)	635	65	0	685	0	84	
RTOR Reduction (vph)	9	0	0	0	0	78	
Lane Group Flow (vph)	694	0	0	685	0	9	
Confl. Bikes (#/hr)		2					
Heavy Vehicles (%)	2%	2%	%0	2%	%0	%0	
Bus Blockages (#/hr)	0	0	20	20	0	0	
Parking (#/hr)	-	۲				-	
Tum Type				ľ	Ö	custom	
Protected Phases	9			12		2	
Permitted Phases							
Actuated Green, G (s)	8.99			77.2		6.4	
Effective Green, g (s)	86.8			77.2		6.4	
Actuated g/C Ratio	0.74			0.86		0.07	
Clearance Time (s)	4.0					4.0	
Vehicle Extension (s)	2.0					2.0	
Lane Grp Cap (vph)	3037			4552		107	ľ
v/s Ratio Prot	c0.17			c0.13		0.00	
v/s Ratio Perm							
v/c Ratio	0.23			0.15		90.0	
Uniform Delay, d1	3.6			1.0		39.0	
Progression Factor	1.00			1.00		1.00	
Incremental Delay, d2	0.2			0.0		0.1	
Delay (s)	3.8			1.1		39.1	
Level of Service	V			4		۵	
Approach Delay (s)	3.8			1.1	39.1		
Approach LOS	4			4	٥		
Intersection Summary							
HCM Average Control Delay	Selav		4.5	I	CM Lev	HCM Level of Service	4
HCM Volume to Capacity ratio	ty ratio		0.22				
Actuated Cycle Length (s)	(8)		90.0	S	um of lo	Sum of lost time (s)	16.8
Intersection Capacity Utilization Analysis Period (min)	ilization		28.1%	Q	ULeve	ICU Level of Service	ď
c Critical Lane Group							

1900 11.00 10.00 1 45.3 46.3 0.42 5.0 2.0 2.0 0.20 0.48 1.00 1.3 24.4 2% 1900 1000 11.00 11 20.0 20.0 0.18 4.0 270 270 270 0.92 2% 0.95 0 0 WBU 1900 Prot 4 5% HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street 46 0 0 0 0 230 EBR 11 0% 5.0 5.0 5.0 5.0 0.20 0.20 0.51 1.00 1.8 27.5 C C C 1100 Prot 16.4 16.4 16.4 2.0 2.0 2.14 0.12 0.80 1.00 17.4 62.6 11% 0 0 2 2 2 0 0 Prot 1900 %0 EBU Total Lost time (s)
Lane Util. Factor
Frpb, ped/bikes
Fit protected
Satt. Flow (prof.)
Fit Permitted
Satt. Flow (prem.)
Volume (vph.)
Peak-nour factor, PHF
Adj. Flow (vph.)
Lane Group Flow (vph.)
Conff. Peds. (#fhr) Uniform Delay, d1 Progression Factor Incremental Delay, d2 Effective Green, g (s)
Actuated g/C Ratio
Clearance Time (s)
Vehicle Extension (s)
Lane Grp Cap (vph)
v/s Ratio Prot Actuated Green, G (s) Movement
Lane Configurations
Ideal Flow (vphpl)
Lane Width Confl. Bikes (#/hr) Heavy Vehicles (%) Parking (#/hr) ntersection Summary Approach Delay (s) Approach LOS Turn Type
Protected Phases
Permitted Phases evel of Service //s Ratio Perm v/c Ratio

0.85

51 0.90 0 0

0.90

%0

15

5%

%0

13

Perm

Perm

21.4 0.19 5.0 2.0 320

6.45.3 46.3 0.42 5.0 2.0 2.0 2.0 0.51 23.5 1.00 7.0 30.4 Synchro 6 6/5/2013
VHB, Inc.

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Synchro 6 VHB, Inc.

16.0 D

HCM Level of Service Sum of lost time (s) ICU Level of Service

37.0 0.64 110.0 75.2%

> Actuated Cyde Length (s) Intersection Capacity Utilization Analysis Period (min) c Critical Lane Group

HCM Average Control Delay HCM Volume to Capacity ratio

HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

2013 Existing Conditions Evening Peak Period 60 60 0 0 1100 SBR 34.3 35.3 0.32 969 26.9 1.00 26.9 26.9 2% 4.0 1.00 1.00 1.00 0.95 1.594 0.37 0.37 0.89 5% Total Lost time (s)
Lane Util Factor
Fath, ped/bikes
Frt
Fit Protected
Satd Flow (prot)
Fit Pown (perm)
Volume (vph)
RTOR Reduction (vph)
RTOR Reduction (vph)
Confl. Blees (#hr)
Fathy Vehicles (%)
Parking (#hr)
Tum Type
Protected Phases
Permitted Green, g (s)
Actuated Green, g (s)
Lane Gro Cap (vph)
Lane Gro Cap (vph) Progression Factor Incremental Delay, d2 Movement Lane Configurations Ideal Flow (vphpl) Uniform Delay, d1 v/s Ratio Perm Lane Width v/c Ratio

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VHB, Inc.

Intersection Summary Approach Delay (s) Approach LOS

Level of Service

Synchro 6 VHB, Inc.

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HCM Unsignalized Intersection Capacity Analysis 9: Belvidere Street & Dalton Street

SBR 0.85 2013 Existing Conditions Evening Peak Period Stop 2 0.85 0.85 24 0.73 33 Stop 18 0.73 25 25 0.73 WBR 416 0.92 452 WBT Sto 4 SB2 15 0.00 5.3 6.33 6.33 7.2 0.92 0.25 280 280 259 0 0 0.53 6.5 6.5 13.9 13.6 Stop 0.25 NB 1 EBT 0.25 WB 1 559 452 0.46 4.5 0.70 779 17.1 17.1 EBL Hourly flow rate (vph) Movement Lane Configurations Direction, Lane # Volume Total (vph) Volume (vph) Peak Hour Factor Sign Control

O ICU Level of Service 15.5 C 67.3% 15 HCM Level of Service Intersection Capacity Utilization Analysis Period (min)

Intersection Summary Control Delay (s) Approach Delay (s) Approach LOS

558 922 922 922 922 922

Volume Left (vph)
Volume Right (vph)
Had (s)
Departure Headway (s)
Degree Utilization, x
Capacity (veh.h)

HCM Signalized Intersection Capacity Analysis 10: Boylston Street & Dalton Street

2013 Existing Conditions Evening Peak Period

	1	†	-	-	,	1	1	-	-	*	+	
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations		4			3		-	4				1
ane Midth	12	11	12	12	12	12	12	12	12	1300	1300	1200
otal lost time (s)		40					4	40				
ane Util. Factor		0.95					1.00	1.00				
Frpb, ped/bikes		96.0					1.00	66.0				
Hpb, ped/bikes		1.00					1.00	1.00				
T.		0.95					1.00	0.92				
FIt Protected		66.0					0.95	1.00				
Satd. Flow (prot)		2835					1562	1459				
It Permitted		0.99					0.95	1.00				
Satd. Flow (perm)	i	2835	Ì		ľ	Ì	1562	1459	1			1
Volume (vph)	61	348	192	0	0	0	285	163	168	0	0	0
Peak-hour factor, PHF	0.94	0.94	0.94	0.92	0.92	0.92	0.94	0.94	0.94	0.92	0.92	0.92
Adj. Flow (vph)	65	370	204	0	0	0	303	173	179	0	0	0
RTOR Reduction (vph)	0	51	0	0	0	0	0	0	0	0	0	0
ane Group Flow (vph)	0	588	0	0	0	0	303	352	0	0	0	0
Confl. Bikes (#/hr)		-	45	1	4		-	-	12			1
icles (%)	3%	4%	1%	%0	%0	%0	4%	1%	13%	%0	%0	%0
	Perm						Split					
Protected Phases		-					e	e				
Permitted Phases	-											
Actuated Green, G (s)		36.0					24.6	24.6				
Effective Green, g (s)		38.0					25.6	25.6				
Actuated g/C Ratio		0.42					0.28	0.28				
Clearance Time (s)		6.0					5.0	2.0				
Vehicle Extension (s)		2.0					2.0	2.0				H
Lane Grp Cap (vph)		1197	l				444	415				ĺ
//s Ratio Prot							0.19	c0.24				
//s Ratio Perm		0.21										
//c Ratio		0.49					0.68	0.85				
Jniform Delay, d1		19.0					28.6	30.4				
Progression Factor		1.00					1.00	1.00				
ncremental Delay, d2		4.1					3.4	14.3				
Delay (s)		20.4					32.0	44.6				
evel of Service		O					O	٥				
Approach Delay (s)		20.4			0.0			38.8			0.0	
Approach LOS		O			×			٥			4	
Intersection Summary												
HCM Average Control Delay	elay		29.7	I	CM Lev	HCM Level of Service	ervice		O			
ACM Volume to Capacity ratio	ratio		0.63	•								
Actuated Cycle Length (s) Intersection Capacity Utilization	(zation		90.0	ωS	um of ic	Sum of lost time (s) ICU Level of Service	(s)		79.4 V			
Analysis Period (min)			15									
() () () () () () () () () ()												

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VHB, Inc.

2018 No-Build Condition Synchro Reports

HCM Signalized Intersection Capacity Analysis 1: Boylston Street & Massachusetts Avenue

2018 NoBuild Conditions Morning Peak Period

	1	1	-	-	ţ	1	-	+	•	*	→	*
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4	*	S	44		K-	44	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	77	2 .	13	17	77	0.	10	0.	2	2	2	OL.
lotal Lost time (s)		4.0			0.4	0.4		0.4		0.4	0.4	
Lane Util. Factor		0.95			1.00	1.00		0.95		1.00	0.95	
Frpb, ped/bikes		0.93			1.00	0.67		0.93		1.00	0.96	
Flpb, ped/bikes		1.00			1.00	1.00		1.00		1.00	1.00	
T.		76.0			1.00	0.85		0.97		1.00	0.99	
Fit Protected		1.00			1.00	1.00		1.00		0.95	1.00	
Satd. Flow (prof)		2762			1502	860		2487		1307	2685	
Elt Permitted		0 94			000	100		0 04		0 95	100	
Satd Flow (perm)		2601			1486	860		2341		1307	26.85	
(chime (mp)	24	451	422	·	402	242	*	707	45.4	400	KCA	24
volume (vpn)	7	0	22	7	701	213	4	40,	0	001	470	5
Peak-hour factor, PHF	0.93	0.93	0.93	99.0	99.0	99.0	0.95	0.95	0.95	0.91	0.91	0.91
Adj. Flow (vph)	23	485	132	m	155	323	15	741	159	207	576	37
RTOR Reduction (vph)	0	23	0	0	0	249	0	0	0	0	0	0
Lane Group Flow (vph)	0	617	0	0	158	74	0	915	0	207	613	0
Confl. Peds. (#/hr)			249			294			441			288
Confl. Bikes (#/hr)			26			-			87			110
Heavy Vehicles (%)	10%	8%	15%	%0	14%	2%	%0	10%	12%	16%	8%	%9
Tum Type	Perm			Perm		Perm	Perm			Prot		
Protected Phases		7			7			-		2	15	
Permitted Phases	7	V		7		7)		
Action of Contract of Co.		220			220	220		340		OFC	620	
Effective Green, 9 (e)		100			000	100		20.00		2000	0 20	
Cilective Green, g (s)		000			200	0.00		0.00		0.00	0.00	
Actuated g/C Ratio		0.23			0.23	0.73		0.35		0.20	0.65	
Clearance Time (s)		2.0			5.0	5.0		2.0		0.9		
Vehicle Extension (s)		2.0			2.0	2.0		5.0		2.0		
Lane Grp Cap (vph)		598			342	198		819		340	1745	
V/s Ratio Prot										c0.16	0.23	
V/s Ratio Perm		c0 24			0.11	0.09		6039				
v/c Ratio		1.03			0.46	0.38		1.12		0.61	0.35	
Iniform Delay d1		38.5			33.2	32 4		30 5		32 5	7 9	
Progression Factor		100			100	100		0 50		100	90	
Portion of the party of		45.5			200	200		000		200	9 9	
inciental Delay, uz		7.00			1 1	4.0		9 6			0 0	
Delay (s)		93.			33.5	32.9		82.5		40.4	0.0	
Level of Service		4			O	O		L		۵	V	
Approach Delay (s)		83.7			33.1			82.5			16.6	
Approach LOS		L			O			L			00	
Intersection Summary												
HCM Average Control Delay	elay		55.5	Ī	ICM Le	HCM Level of Service	arvice		ш			
HCM Volume to Capacity ratio	y ratio		0.94									
Actuated Cycle Length (s)	s)		100.0	()	um of I	Sum of lost time (s)	(s)		16.0			
Intersection Capacity Utilization	ilization		82.9%	2	CULeve	ICU Level of Service	vice		ш			
Analysis Period (min)			15									
c Critical Lane Group												

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Synchro 6 VHB, Inc.

VHB, Inc.

HCM Signalized Intersection Capacity Analysis 2: Belvidere Street & Massachusetts Avenue

2018 NoBuild Conditions Morning Peak Period

1900 1900 125 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1900 1 1900 1 12 0 0.25 0 0 0 0 0	1900 122 0 0.25 0 0.25	1900 12	1900 41	1900 1900	NBL 1900	TBN 1900	NBR oo	SBL 1900	TBS 44	SBR
1900 125 (vph) 0 (vph) 0 0		10.50	1900	1900	1900	1900	1900	000	1900	44	
0.025		C	1200	1400	1900	1900	1900	4000	1900		
0.0000000000000000000000000000000000000		12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5	4 6	42			350		1900	1900
0.25		0.25		40	71	10	10	10	10	9	10
0.25	0.000	0.25		2			4.0			4.0	
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0.25		1.00			0.95			0.95	
0.25 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0.25		1.00			1.00			1.00	
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.900 250 250	0.25		1.00			1.00			1.00	
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0.25		0.92			1.00			1.00	
0.25		0.25		0.99			1.00			1.00	
0.25		0.25		1416			2577			2597	
0.25	110000000000000000000000000000000000000	0.25		0.99			0.94			1.00	
0.25		0.25		1416			2417			2597	
0.00	940000000000000000000000000000000000000	0.25	18	25	25	15	812	0	0	632	20
	000 %0	0	0.80	0.80	0.80	0.95	0.95	0.95	0.92	0.92	0.92
A 20 TO 1	00 %0		22	31	71	16	855	0	0	687	22
	0 %0	0	0	0	0	0	0	0	0	2	0
	%0	0	0	124	0	0	871	0	0	707	0
	%0										103
	0	%0	12%	4%	4%	%0	10%	%0	%0	10%	2%
arking (#/hr) Type Protected Phases		0	0	0	0	0	7	0	0	0	80
rum Type Protected Phases			-	-	-		-			-	
Protected Phases			Split			Perm					
			0	6			-			-	
Permitted Phases						-					
Actuated Green, G (s)				12.9			58.7			58.7	
Effective Green, q (s)				14.9			60.7			60.7	
Actuated o/C Ratio				0.15			0.61			0.61	
Clearance Time (s)				6.0			6.0			6.0	
Vehicle Extension (s)				2.0			2.0			2.0	
Lane Gro Cap (voh)				211			1467			1576	
v/s Ratio Prot				60.00						0.27	
V/s Ratio Perm							98 00				
v/c Ratio				0.59			0.59			0.45	
Uniform Delay, d1				39.7			121			106	
Progression Factor				1.00			0.42			0.70	
Incremental Delay, d2				2.7			1.7			0.8	
Delay (s)				4 6 4			6.7			82	
evel of Service				٥			4			4	
Approach Delay (s)	00			424			67			82	
Approach LOS				0			×			\ \	
Intersection Summary											
HCM Average Control Delay		0	Ĭ	HCM level of Service	of Spile	orivo		A			l
HCM Volume to Capacity ratio		0.59				3					
Actuated Cyde Length (s)	- 05	50 1%	5 C	Sum of lost time (s)	of San	(S)		74.4 A			
Applies Dorod (min)	5	4 4	2	כ רבאפו	10000	3					
Critical Lane Group		2									
											-
Synchro 6										6/11	6/11/2013
Synchro 6										11/0	1/2013

HCM Unsignalized Intersection Capacity Analysis 3: Saint Germain Street & Massachusetts Avenue

2018 NoBuild Conditions Moming Peak Period

	-	1	+	1	•	•	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	*		‡			*	
Grade	0%0		%0			%0	
Volume (veh/h)	-	2	822	0	0	650	
Peak Hour Factor	0.50	0.50	0.94	0.94	0.90	0.90	
Hourly flow rate (vph)	N	10	874	0	0	722	
Pedestrians			161			159	
Lane Width (ft)			10.0			10.0	
Walking Speed (ft/s)			4.0			4.0	
Percent Blockage			1			1	
Right turn flare (veh)							
Median type	None						
Median storage veh)			4000			222	
nX platon unblocked	0.88		700			777	
vC. conflicting volume	1397	596			874		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1317	969			874		
tC, single (s)	8.9	7.3			4.1		
tC, 2 stage (s)							
tF (s)	3.5	3.5			2.2		
% eeu enen bod	86	16			100		
cM capacity (veh/h)	119	360			780		
Direction, Lane #	WB 1	NB 1	NB 2	SB 1	SB2		
Volume Total	12	437	437	361	361		
Volume Left	2	0	0	0	0		
Volume Right	10	0	0	0	0		
SH	269	1700	1700	1700	1700		
Volume to Capacity	0.04	0.26	0.26	0.21	0.21		
Queue Length 95th (ft)	e	0	0	0	0		
Control Delay (s)	19.0	0.0	0.0	0.0	0.0		
Lane LOS	O						
Approach Delay (s)	19.0	0.0		0.0			
Approach LOS	O						
Intersection Summary							
Average Delay			0.1				
Intersection Capacity Utilization	tilization		45.2%	ō	ULeve	ICU Level of Service	∢
Aldiyaia relicu (IIIII)			2				

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VHB, Inc.

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HCM Signalized Intersection Capacity Analysis 4: St. Stephen & Massachusetts Avenue

2018 NoBuild Conditions Morning Peak Period

ions ol) (s)	WBT		-								
Lane Configurations Ideal Flow (vphpl) Lane Width Total Lost time (s)		NBL	NBT	NBR	SBL	SBT	SBR	SBR2	SER	SER2	
Ideal Flow (vphpl) Lane Width Total Lost time (s) Lane Util. Factor	4	K	44			414			N.		
Lane Width Total Lost time (s) Lane Util. Factor	0061	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Total Lost time (s) Lane Util. Factor	16	10	10	10	10	10	10	10	12	12	
Lane Util. Factor	0.4	4.0	4.0			4.0			4.0		
Tank and thilten	1.00	1.00	0.95			0.95			0.88		
ripp, ped/bikes	1.00	1.00	66.0			0.93			1.00		
Flpb, ped/bikes	1.00	1.00	1.00			1.00			1.00		
74	1.00	1.00	0.99			0.99			0.85		
Fit Protected	1.00	0.95	1.00			1.00			1.00		
Satd. Flow (prot) 1	1938	1472	2656			2546			2266		
Fit Permitted	1.00	0.95	1.00			0.68			1.00		
Satd. Flow (perm) 1	1938	1472	2656			1745			2266		
Volume (vph)	-	286	828	32	18	530	37	22	386	18	
tor. PHF	0.38	0.92	0.92	0.92	0.95	0.95	0.95	0.95	0.95	0.95	
	e	311	900	35	19	558	39	23	406	19	
RTOR Reduction (vph)	0	0	0	0	0	0	0	0	0	0	
Lane Group Flow (vph)	e	311	935	0	0	639	0	0	425	0	
Confl. Peds. (#/hr)				86	98			332		E	
Confl. Bikes (#/hr)			2	90				62	2		
Heaw Vehicles (%)	%0	3%	10%	3%	%0	%6	%6	30%	2%	%9	
Bus Blockages (#/hr)	0	0	10	10	0	0	12	12	0	0	
Parking (#/hr)							-	-	-	-	
Tum Type	ľ	Prot	Ì		Perm				Over		
Protected Phases	S	9	16			-			9		
Permitted Phases					-						
Actuated Green, G (s)	9.7	25.1	79.4			47.3			25.1		
Effective Green, g (s)	9.6	28.1	82.4			50.3			28.1		
	0.10	0.28	0.82			0.50			0.28		
	6.0	7.0				7.0			7.0		
Vehicle Extension (s)	2.0	2.0				0.2			2.0		
Lane Gro Cap (voh)	186	414	2189			878			637		
		20 21	0.35						0 19		
						60.37					
	0.02	0.75	0.43			0.73			0.67		
Delay, d1	40.9	32.8	2.4			19.5			31.8		
	1.00	1.30	0.56			1.10			100		
42	0.0	2.6	0.0			8.4			2.1		
	6 04	45.1	1.4			262			33.9		
Service	0	0	4			O			O		
	40.9	1.	12.3			26.2					
Approach LOS	٥		8			0					
Infersection Summan											
HCM Average Control Delay	76		20.1	I	HCM Level of Service	el of Se	vice		C		
HCM Volume to Capacity ratio	ratio		0.66			5	3)		
Actuated Cycle Length (s)			100.0	S	Sum of lost time (s)	st time	(s)		12.0		
Intersection Capacity Utilization	zation		64.9%	≥	ICU Level of Service	l of Sen	100		O		
Analysis Period (min) c Critical Lane Group			5								
		l	l	l		l	l	l	l	l	100

HCM Signalized Intersection Capacity Analysis 5: Huntington Avenue & Massachusetts Avenue

Movement	1700 1700 1700 1700 0.84 149 0 0 0 0 0 0	WBR N 1777 1707 1100 1100 1100 1100 1100 110	NBL NBT NBL NBT 1600 1600 1600 1600 1600 1600 1600 160	1 NBR 1600 1600 1600 1600 1600 1600 1600 160	8BL SBL 1600 1600 1600 1600 1600 1600 1600 1600	↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑ ↑
47b 1700 1700 1700 12 11 12 7.5 0.96 0.95 0.95 0.95 0.97 2274 0.97 2274 0.97 2274 0.97 2274 0.97 2274 0.97 2274 0.97 2274 0.97 2274 0.97 2274 13.9 10.0 0 231 0 0 0 0 231 0 0 0 0 231 0	1700 125 0.84 148 0 0 0 0 Split 5				9 8 9 8 9 9	
1700 1700 1700 1700 1700 1700 1700 1700	1700 125 0.84 149 0 0 0 0 0 0 Split 5				6 . 0 0 1 0 1 22 1 22 1 2 8 0 8 8 8	
7.5 7.5 0.95 0.95 0.95 0.95 0.97 0.97 2274 0.97 2274 0.97 2274 0.97 2274 0.97 0.06 0.06 0.06 0.07 0.	125 126 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			9-	00101212	o "
7.5 0.95 0.96 0.96 1.00 0.95 0.97 2274 123 0.97 2274 143 12 76 0	125 0.84 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				99-9-8-8-8	0
0.95 0.96 1.00 0.95 0.97 2274 0.97 2274 0.97 0.86 0.86 0.86 0.86 0.96 0.97 0.97 0.00	125 0.84 0 0 0 0 0 0 0 0 0 5 pit					o "
0.96 0.96 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.00 0.00	125 0.84 149 0 0 0 0 0 0 5 5					o "
100 0.95 0.97 2274 2274 2274 123 10 65 0.86 0.86 0.86 0.86 143 12 76 0 0 0 0 0 23 1 0 0 3 13.9 13.4 0.13 7.0 2.0 305 0.10 0.76 41.7 1.00 9.2 0.76 0.	125 126 0 0 0 2% Spit 5					9
0.95 0.97 2274 2274 123 0.97 0.97 0.97 0.97 0.97 0.96 0.86 0.86 0.86 0.86 0.86 0.86 0.90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	125 0.084 149 0 0 0 0 2% Spirt					6
2274 0.97 0.97 123 10 65 0.86 0.86 0.86 0	125 0.84 149 0 0 0 0 Spirt 5					6
2274 0.97 2274 123 10 65 0.86 0.86 0.86 143 143 12 76 0 0 0 0 0 0 0 231 0 0 231 0 0 231 0 0 231 0 0 13.9 13.4 0.13 7.0 2.0 305 0.13 7.0 2.0 305 0.16 0.76 41.7 1.00 9.2 80.9 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76	125 0.84 149 0 0 0 0 0 5 pit					0
0.97 2274 123 0 65 0.86 0.86 0.86 0.86 143 12 76 0 0 0 0 0 23 0 50 0 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.0 1	125 0.84 149 0 0 0 0 Spift					o w
2274 123 10 65 0.66 0.86 0.86 143 12 76 0 0 0 23 1 0 0 23 1 0 9 77% 27% 10% 50/13 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	2% 2% 2% Spiit 5					6
123 10 65 0.86 0.86 0.86 0.86 0.86 0.86 0.86 0.86	125 0.84 149 0 0 0 0 Spirt 5					o "
0.86 0.86 0.86 143 12 76 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.84 149 0 0 0 0 Split 5					0
143 112 76 0 0 0 0 0 0 231 58 8 6 8 6 13.9 13.9 13.4 0.13 7.0 2.0	2% Split 55					
Split 58 13.9 17.8 27.8 10.8 58 13.9 13.9 13.4 13.4 13.4 13.4 13.5 10.13 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	2% Spirt 55					
231 0 231 58 9 9 9 7% 27% 10% 9 59lit 6 6 6 13.4 0.13 7.0 2.0 305 0.10 9.2 9.2 9.2 9.2 9.2 9.2 9.2 9.9 9.9 9.9	2% Split 5			10.0		
58 Split 6 6 6 6 6 13.9 13.9 13.4 0.13 7.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	2% Split 5			100		
9 Split 6 13.9 13.4 13.4 13.4 13.4 0.13 7.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	Split 5			5		
Split 6 6 6 6 6 6 6 13.4 0.13 7.0 2.0 2.0 2.0 2.0 0.76 41.7 1.00 9.2 50.9 D 50.9 D D	Split 5			5		
Split 6 6 13.9 13.9 13.4 0.13 7.0 2.0 2.0 2.0 2.0 0.76 0.76 11.00 9.2 50.9 D D D	Split			ш	ш	
6 6 13.9 13.4 13.4 13.4 13.6 2.0 2.0 2.0 0.76 41.7 41.7 100 9.2 50.9 0 D						_
	15.9			7		
	15.9	Ē				
	15.4		12.2 49.2	2	30.0	0
(S)	4	17.4	15.2 49.2	2	30.0	0
d2	0.15	0.17 0	0.15 0.49	6	0.30	0
(S	7.0		7.0		7.0	0
(vph)) d1 cdor lay, d2 e	2.0		2.0		0.2	2
d1 lay, d2 e e y (s)	211	203	208 1223	3	688	8
d1 ccor lay, d2 e e y (s)	00.13	0.08 0	0.10 c0.45	2	c0.41	-
d1 cdor lay, d2 e e y (s)						
d1 Ictor Ilay, d2 e y (s)	0.85	0.47 0	0.68 0.92	2	1.36	9
idy, d2 lay, d2 e y (s)	41.2		40.1 23.6	9	35.0	0
e (s)	1.00	1.00	1.00 1.00	0	1.05	2
e y (s)	26.0	9.0	7.2 11.3	3	170.8	8
e y (s)	67.2	37.8 4	47.3 34.9	6	207.6	9
y (s)	ш	٥		O		ш
	57.0		36.	8	207.6	9
	ш		۵	0		L.
Intersection Summary						ı
Delay 98 9		HOM I avail of Service	90	tu		
112			2	۱		
1000		Sum of lost time (s)		29.0		
ration 82.3%		ICI I evel of Service	a	ш		
15				(
	2					

2018 NoBuild Conditions 7:45 am 6/11/2013 Morning Feak Period VHB, Inc.

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HCM Unsignalized Intersection Capacity Analysis 6: Huntington Avenue & Driveway West

6/14/2013

acity Analysis 2018 NoBuild Conditions
Vest Morning Peak Period

lent EBL EBT WBT WBR SBL configurations		1	1	ţ	1	•	•	
onfigurations	vement	EBL	EBT	WBT	WBR	SBL	SBR	
ontrol Free Free Stop O% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0% 0%	Lane Configurations		*	44			N.	
s (vehrlit) 0 0% 0% 0% 0% 10% 10% 10% 10% 10% 10% 1	Sign Control		Free	Free		Stop		
(a) 0.00 286 58 0.85 0.85 0.85 0.95 0.95 0.95 0.85 0.85 0.85 0.85 0.95 0.95 0.95 0.85 0.85 0.85 0.95 0.95 0.95 0.85 0.85 0.85 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.9	Grade		%0	%0		%0		
h) 0.92 0.92 0.95 0.95 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0	ume (veh/h)	0	0	266	28	0	2	
h) 0 0 280 61 0 2 110 4.0 110 4.0 110 4.0 10 4.0 10 4.0 10 280 507 None S49 519 587 EB 1 EB 2 WE1 WB2 SB 1 0 0 187 154 2 0 0 0 0 0 61 0 0 61 0 0 61 0 0 61 0 0 187 154 2 0 0 0 0 0 0 0 0 0 0 1700 262 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ak Hour Factor	0.92	0.92	0.95	0.95	0.85	0.85	
208 208 13.0 11.0	urly flow rate (vph)	0	0	280	61	0	2	
11.0 13.0 13.0 13.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14	destrians		208			208		
16 4.0 4.0 19 19 19 19 19 19 19 19 19 19 19 19 19	ne Width (ft)		11.0			13.0		
16 19 None See 549 See 507 The see 549 See 507 See	alking Speed (ft/s)		4.0			4.0		
ed 549 507 519 587 618 587 618 587 618 587 618 587 618 587 618 618 7.6	rcent Blockage		16			19		
Hone Sed 507 Sed 507 Sed 508 Sed 507 Sed 508 Sed 507 Sed 507 Sed 508 Sed 50	tht turn flare (veh)							
ed 549 567 619 587 61 619 619 619 619 619 619 619 619 619	dian type					None		
e 549 507 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 587 61 519 519 519 519 519 519 519 519 519 51	Median storage veh)							
ed 549 519 587 ne 549 519 587 4.1 6.8 7.6 2.2 3.5 3.6 100 2.2 3.6 3.6 100 3.3 3.6 100 0 0 187 0 0 0 0 0 1700 1700 1700 1700 262 0.00 0.00 0.11 0.09 0.01 0.00 0.00 0.01 18.3 0.0 0.0 0.0 0.0 18.3 0.0 0.0 0.0 18.3 0.0 0.0 0.0 18.3 0.0 0.0 0.0 18.3 0.0 0.0 0.0 18.3	Jpstream signal (ft)		260	202				
ne 549 519 587 1 549 519 587 4.1 6.8 7.6 2.2 3.6 3.6 100 99 837 EB 1 EB 2 WB 1 WB 2 SB 1 0 0 187 154 2 0 0 0 0 0 0 1700 1700 1700 262 0.0 0.0 0.0 0.0 18.9 0.0 0.0 0.0 18.9 0.0 0.0 0.0 18.9 1	, platoon unblocked							
2.2 3.6 5.87 6.8 7.6 6.8 7.6 100 99 837 837 154 2.2 100 99 92 262 837 154 2 0 0 0 187 154 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	, conflicting volume	549				519	287	
549 4.1 5.2 4.1 5.2 5.2 5.3 5.5 5.6 5.8 5.7 6.8 7.6 6.8 7.6 6.8 7.6 6.8 7.6 6.8 7.6 6.8 7.6 6.8 7.6 9.9 99 99 99 99 99 99 99 99 90 90 90 90 90	VC1, stage 1 conf vol							
### 549 549 549 549 549 549 549 549 549 549	2, stage 2 conf vol							
2.2 3.5 3.6 100 99 837 EB.1 EB.2 WB.1 WB.2 SB.1 0 0 187 154 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	u, unblocked vol	549				519	587	
2.2 3.5 3.6 100 99 837 8837 8837 8837 899 262 899 262 899 262 899 262 899 262 899 899 262 899 899 899 899 899 899 899 899 899 89	single (s)	4.1				6.8	7.6	
22 3.5 3.6 837 899 262 EB 1 EB 2 WB 1 WB 2 SB 1 0 0 187 154 2 0 0 0 0 0 0 1700 1700 1700 262 0.00 0.00 0.11 0.09 0.01 (f) 0 0 0 0 0 18.3 0.0 0.0 0.0 0.0 18.3 0.0 0.0 0.0 18.3	2 stage (s)							
100 99 837 EB 1 EB 2 WB 1 WB 2 SB 1 0 0 187 154 2 0 0 0 0 0 0 1700 1700 1700 262 0.00 0.00 0.11 0.09 0.01 0.0 0.0 0.0 0.0 18.9 0.0 0.0 0.0 0.0 18.9 0.0 0.0 0.0 0.0 18.9 0.0 0.0 0.0 0.0 18.9 0.0 0.0 0.0 0.0 18.9 0.0 0.0 0.0 0.0 18.9	(s)	2.2				3.5	3.6	
EB 1 EB 2 WB 1 WB 2 SB 1 0 0 187 154 2 0 0 0 0 0 0 0 1700 1700 1700 262 0.00 0.00 0.11 0.09 0.01 (#) 0 0 0 0 0 18.3 0.0 0.0 0.0 0.0 18.3 0.0 0.0 0.0 0.0 18.3 vy Utilization 33.3% ICU Level of Service	dnene tree %	100				100	66	
# EB1 EB2 WB1 WB2 SB1 0 0 187 154 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	capacity (veh/h)	837				399	262	
0 0 187 154 2 0 0 0 0 0 0 0 0 0 0 0 61 2 1700 1700 1700 262 95th (\$) 0.00 0.01 10.09 0.01 95th (\$) 0.00 0.01 18.3 7 (\$) 0.0 0.0 0.0 18.3 7 (\$) 0.0 0.0 0.0 18.3 9 0.0 0.0 0.0 18.3 9 0.0 0.0 0.0 18.3 9 0.1 18.3	ection, Lane #	EB 1	EB 2	WB 1	WB 2	SB1		
city 0.00 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	lume Total	0	0	187	154	2		
acty 0.00 1700 1700 262 acty 0.00 0.00 0.11 0.09 0.01 s) 0.0 0.0 0.0 0.18.9 c) (s) 0.0 0.0 0.0 18.9 c mmary 0.11 covel of Service	lume Left	0	0	0	0	0		
acity 0.00 1700 1700 262 95th (#) 0.00 0.01 0.09 0.01 95) 0.0 0.0 0.0 0.0 18.3 7 (s) 0.0 0.0 0.0 18.3	lume Right	0	0	0	61	2		
acity 0.00 0.00 0.11 0.09 0.01 95th (#) 0 0 0 0 1 s) 0.0 0.0 0.0 18.3 (s) 0.0 0.0 0.0 18.3 mmany 0.1 ICU Level of Service		1700	1700	1700	1700	262		
95th (#) 0 0 0 0 1 s) 0.0 0.0 0.0 0.0 18.3 C r(s) 0.0 0.0 0.0 18.3 cmmary 0.1 pacity Utilization 33.3% ICU Level of Service	lume to Capacity	0.00	0.00	0.11	0.09	0.01		
s) 0.0 0.0 0.0 18.3 (s) 0.0 0.0 18.9 c mmary 0.1 pacity Utilization 33.3% ICU Level of Service	ieue Length 95th (ft)	0	0	0	0	-		
(s) 0.0 0.0 18.3 c mmary 0.1 c 10.1 Level of Service	introl Delay (s)	0.0	0.0	0.0	0.0	18.9		
7 (s) 0.0 0.0 18.3 C C mmary 0.1 0.1 ICU Level of Service	neLOS					O		
mmary 0.1 a3.3% ICU Level of Service	proach Delay (s)	0.0		0.0		18.9		
mmary 0.1 pacity Utilization 33.3% ICU Level of Service	proach LOS					O		
0.1 pacity Utilization 33.3% ICU Level of Service	ersection Summary							
Utilization 33.3% ICU Level of Service	erage Delay	7		0.1				-
	Intersection Capacity Ut	ilization		33.3%	_	CU Leve	of Service	ď

Synchro 6 6/11/2013 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 7: Huntington Avenue & Cumberland Street

2018 NoBuild Conditions Morning Peak Period

	†	*		Ą	-			
Movement	EBT	EBR	WBL	WBT	NBL	NBR		
ane Configurations	441			#		K		
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
ane Width	=	11	=	1	12	16		
Total Lost time (s)	4.0			4.0		4.0		
ane Util. Factor	0.91			980		1.00		
Frpb, ped/bikes	1.00			1.00		1.00		
Hpb, ped/bikes	1.00			1.00		1.00		
F	0.99			1.00		0.86		
Fit Protected	1.00			1.00		1.00		
Satd. Flow (prot)	4048			5208		1443		
FIt Permitted	1.00			1.00		1.00		
Satd. Flow (perm)	4048			5208		1443		
Volume (vph)	976	29	0	992	0	49		
Peak-hour factor, PHF	06.0	06.0	0.95	0.95	0.67	29.0		
Adi. Flow (vph)	640	32	0	806	0	73		
REDUCTION (vph)	2	0	0	0	0	68		
ane Group Flow (vph)	670	0	0	806	0	2		
Confl. Bikes (#/hr)		12						
Heavy Vehicles (%)	2%	%0	%0	1%	%0	4%		
Bus Blockages (#/hr)	0	0	20	20	0	0		
Parking (#/hr)	-	٦				-		
Furn Type	1			ľ	0	custom		
Protected Phases	9			12		2		
Permitted Phases								
Actuated Green, G (s)	68.4			78.8		6.4		
Effective Green, g (s)	68.4			78.8		6.4		
Actuated g/C Ratio	0.76			0.88		20.0		
Clearance Time (s)	4.0					4.0		
/ehicle Extension (s)	2.0	١				2.0		
ane Grp Cap (vph)	3076			4560		103		
//s Ratio Prot	c0.17			c0.15		0.00		
//s Ratio Perm								
//c Ratio	0.22			0.18		0.05		
Jniform Delay, d1	3.1			0.8		39.0		
Progression Factor	1.00			1.00		1.00		
ncremental Delay, d2	0.5			0.0		0.1		
Delay (s)	3.3			0.8		39.0		
evel of Service	4			×		٥		
Approach Delay (s)	3.3			0.8	39.0			
Approach LOS	4			4	۵			
ntersection Summary								
HCM Average Control Delay	Delay		3.7	_	ICM Lev	HCM Level of Service	A	
HCM Volume to Capacity ratio	ity ratio		0.21					
Actuated Cycle Length (s)	(s)		90.0	s :	um of lo	Sum of lost time (s)	11.2	
Intersection Capacity Utilization Analysis Period (min)	tilization	2	15	2	OU Leve	ICU Level of Service	∢	

HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

2018 NoBuild Conditions Morning Peak Period

phpl) te (s) tcor es	EBU	EBL	EBT	CBD	100		FO.	000	NBL	NBT	OON	
ne Configurations all Flow (vphpl) all Lost time (s) te Utill. Factor b, ped/bikes b, ped/bikes			1	200	WBD	WBL	WBI	WER			NON	SBU
ar row (vprp) te Width te Width te Ultit (s) te Util Factor b, ped/bikes b, ped/bikes	8	NE COO	44	4000	000	1000	**	1000	4000	400	4000	000
al Lost time (s) te Util. Factor b, ped/bikes b, ped/bikes	12	11	90	11	90	100	11	11	12	16	12	12
ane Util. Factor rpb, ped/bikes ipb, ped/bikes rt		4.0	4.0	0		4.0	4.0	4.0		4.0	!	l),
rpb, ped/bikes lpb, ped/bikes rt		1.00	0.95			1.00	0.95	1.00		1.00		
ipb, ped/bikes		1.00	66.0			1.00	1.00	0.58		1.00		
-		1.00	1.00			1.00	1.00	1.00		1.00		
		1.00	0.99			1.00	1.00	0.85		0.98		
Fit Protected		0.95	1.00			0.95	1.00	1.00		0.99		
Satd. Flow (prot)		1373	2709			1451	2935	722		1820		
Fit Permitted		0.95	1.00			0.95	1.00	1.00		0.91		
Satd. Flow (perm)		1373	2709			1451	2935	722	ľ	1672		
Volume (vph)	9	137	455	27	92	128	929	369	71	236	28	9
or, PHF	0.92	0.86	0.86	0.86	0.95	0.94	0.94	0.94	0.88	0.88	0.88	0.85
Adj. Flow (vph)	1	159	529	31	80	136	869	393	81	268	99	7
RTOR Reduction (vph)	0	0	4	0	0	0	0	252	0	7	0	0
Lane Group Flow (vph)	0	166	556	0	0	216	869	141	0	408	0	0
Confl. Peds. (#/hr)				134				467				
				1				2			12	
Heavy Vehicles (%)	%0	15%	3%	15%	2%	%9	2%	13%	3%	3%	2%	%0
	1000	Drost	1		to-d	Drot		Dorm	Dorm		-	0100
Dhana	5 4	5	c		5 -	5	q	5	5	*		0
Floreded Fliases	0	0	٧		-	-	0	d	*	1		2
Actuated Green G (e)		14.4	22.2			45.8	32 6	33 0	4	9 30		4
Cualculation Order, O (s)			2000			0.0	200	200		0.00		
Activity of Datio		1	7.00			0.00	0.40	0.40		0.00		
Actuated g/C Ratio		4 5	200			0 0	0.50	0.50		0.27		
clearance Time (s)		0.0	0.0			9 0	0.0	0.0		0.0		
Venide Extension (s)		2.0	2.0			2.0	7.0	7.0		2.0		
Lane Grp Cap (vph)		198	899			529	1016	250		448		
v/s Ratio Prot		0.12	0.21			00.15	00.24					
v/s Ratio Perm								0.19		00.24		
v/c Ratio		0.84	0.62			0.94	0.69	0.56		0.91		
Uniform Delay, d1		41.7	28.1			41.7	28.1	26.6		35.4		
Progression Factor		1.00	1.00			0.82	1.04	2.67		1.00		
Incremental Delay, d2		24.5	3.2			43.0	3.8	8.8		22.0		
Delay (s)		66.2	31.3			77.1	32.8	7.67		57.5		
Level of Service		ш	O			ш	O	ш		ш		
Approach Delay (s)			39.2				543			57.5		
Approach LOS			٥				۵			ш		
Intersection Summary												
HCM Average Control Delay	>		48.3	I	CM Lev	HCM Level of Service	arvice		٥			
HCM Volume to Capacity ratio	otto		0.74									
Actuated Cycle Length (s)			100.0	(A)	nm of Ic	Sum of lost time (s)	(s)		12.0			
Intersection Capacity Utilization	tion	~	82.6%	≥ .	CU Leve	ICU Level of Service	vice		ш			
Critical Lane Group			j									

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VHB, Inc.

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Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

2018 NoBuild Conditions Morning Peak Period

	*	+	*	
Movement	SBL	SBT	SBR	
Lane Configurations	K	44		
Ideal Flow (vphpl)	1900	1900	1900	
Lane Width	12	12	=	
Total Lost time (s)	4.0	4.0		
Lane Util. Factor	1.00	0.95		
Frpb, ped/bikes	1.00	0.99		
Flpb, ped/bikes	1.00	1.00		
E	1.00	0.94		
Fit Protected	0.95	1.00		
Satd. Flow (prot)	1568	2857		
FIt Permitted	0.31	1.00		
Satd. Flow (perm)	514	2857		
Volume (vph)	58	65	38	
Peak-hour factor, PHF	0.93	0.93	0.93	
Adj. Flow (vph)	62	20	14	
RTOR Reduction (vph)	0	25	0	
Lane Group Flow (vph)	69	86	0	
Confl. Peds. (#/hr)				
Confl. Bikes (#/hr)			6	
Heavy Vehicles (%)	4%	8%	2%	
Parking (#fhr)				
	D.P+P			
Protected Phases	က	34		
Permitted Phases	4			
Actuated Green, G (s)	34.0	38.0		
Effective Green, g (s)	35.0	39.0		
Actuated g/C Ratio	0.35	0.39		
Clearance Time (s)	4.0			
Vehicle Extension (s)	2.0			
Lane Grp Cap (vph)	266	1114		
v/s Ratio Prot	c0.05	0.03		
v/s Ratio Perm	0.07			
v/c Ratio	0.26	0.08		
Uniform Delay, d1	24.0	19.2		
Progression Factor	1.00	1.00		
Incremental Delay, d2	0.2	0.0		
Delay (s)	24.1	19.2		
Level of Service	O	8		
Approach Delay (s)		21.1		
Approach LOS		O		
Intersection Summary				

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VHB, Inc.

HCM Unsignalized Intersection Capacity Analysis 9: Belvidere Street & Dalton Street

2018 NoBuild Conditions Morning Peak Period

	1	1	-	-	+	1	-	+	•	•	→	+
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					4			4			##	
Sign Control		Stop			Stop			Stop			Stop	
Volume (vph)	0	0	0	80	88	536	2	15	14	143	9	25
Peak Hour Factor	0.25	0.25	0.25	0.81	0.81	0.81	0.78	0.78	0.78	0.90	0.90	0.90
Hourly flow rate (vph)	0	0	0	10	110	662	m	19	18	159	7	28
Direction, Lane #	WB 1	NB 1	SB 1	SB 2								
Volume Total (vph)	781	40	162	31								
Volume Left (vph)	10	en	159	0								
Volume Right (vph)	662	18	0	28								
Hadj (s)	-0.31	-0.14	0.55	-0.49								
Departure Headway (s)	4.4	6.2	7.0	5.9								
Degree Utilization, x	0.95	0.07	0.32	0.05								
Capacity (veh/h)	818	572	505	594								
Control Delay (s)	39.9	9.6	12.0	8.1								
Approach Delay (s)	39.9	9.6	11.4									
Approach LOS	ш	4	œ									
Intersection Summary												
Delay HCM Level of Service			33.3									
Intersection Capacity Utilization Analysis Period (min)	tilization		69.1%	2	OU Leve	ICU Level of Service	vice		O			

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HCM Signalized Intersection Capacity Analysis 10: Boylston Street & Dalton Street

2018 NoBuild Conditions Moming Peak Period

EBL EBT EBR WBL 1900 1900 1900 1900 1900 1900 1900 1900							
900 1900 1900 1900 1900 1900 1900 1900		NBL	NBT	NBR	SBL	SBT	SBR
1900 1900 1900 1900 1900 1900 1900 1900		K	42				
12 11 12 12 12 14 15 15 15 15 15 15 15 15 15 15 15 15 15	1900	900	006	1900	1900	1900	1900
4.0 0.95 0.95 0.96 0.96 0.98 1.00 2628 1.00 2628 1.00 2628 0.96 0.96 0.96 0.96 0.96 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98		12	12	12	12	12	12
9.95 9.98 1.00 9.98 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 1.00 9.95 9.95 9.95 9.95 9.95 9.95 9.95 9	4	4.0	4.0				
9.98 1.00 1.00 1.00 1.00 1.00 2.628 1.00 2.628 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	1.	00.1	1.00				
100 2628 100 2628 100 2628 100 2628 100 62 474 267 0 62 474 267 0 62 474 267 0 62 474 267 0 63 408 0.96 741 0 0 0 741 13% 4% 0% 80 38.3 38.3 38.3 38.3 38.3 38.3 38.3 38	+		00.1				
100 2628 100 2628 100 2628 100 2628 100 262 100 263 100 100 100 100 100 100 100 10	-	00.1	00.1				
100 2628 100 2628 100 2628 100 2628 100 62 408 62 474 267 0 0 00h) 0 741 0 0 0 00h) 0 0 0 0 0 00h) 0 0 0 0 0 00h) 0 0 0 0 0 0 00h) 0 0 0 0 0 0 00h) 0 0 0 0 0 0 0 00h) 0 0 0 0 0 0 0 0 00h) 0 0 0 0 0 0 0 0 0 0 00h) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1	1.00	0.91				
2628 100 2628 100 2628 100 2628 100 262 474 267 0 262 474 267 0 273% 13% 15% 4% 0% 2044 600 208 2028 2027 2037 204 204 205 207 207 207 207 207 207 207 207 207 207	0		1.00				
100 202 202 203 100 1100 1100 1136 1136 1136 1137 1137 1138 1138 1138 1138 1138 1138	15	1504 1	1353				
s) 2628	0		1.00				
F 53 408 230 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	15	-	1353				
HF 0.86 0.86 0.86 0.90 0.90 0.91 0.91 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92		247	107	174	0	0	0
s) 13% 15% 4% 0% 13% 13% 15% 4% 0% 15% 15% 15% 15% 15% 15% 15% 15% 15% 15	2	P	0.85	0.85	0.92	0.92	0.92
ph) 0 62 0 0 13% 15% 4% 0% Perm 1 1 37.3 s) 36.3 s) 2.0 6.0 1148 0.28 0.65 19.9 1.00 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7			126	205	0	0	0
bh) 0 741 0 0 Perm 13% 4% 0% Perm 1 1 13.33.3 s) 39.3 b) 2.0 1148 0.28 0.28 0.65 19.9 12 2.8 22.7 C C C C C C C C C C C C C C C C C C C		0	0	0	0	0	0
37 13% 15% 4% 0% 15% 15% 15% 15% 15% 15% 15% 15% 15% 15		291	331	0	0	0	0
s) 13% 15% 4% 0% 15% 15% 15% 15% 15% 15% 15% 15% 15% 15							
s) 137.3 39.3 39.3 39.3 30.4 6.0 6.0 1148 0.28 0.65 19.9 1.00 1.00 2.7 2.7 C C C C C C C C C C C C C		8%	%9	20%	%0	%0	%0
s) 37.3 9) 34.3 9.44 6.0 1.04 6.0 1.00 1.	Ś	Split	þ	ì	ŀ		
s) 37.3 39.3 0.44 6.0 2.0 2.0 1148 0.28 0.65 19.9 10.0 2.8 22.7 22.7 22.7 22.7 33.0 33.0 33.0 36.0 36.0 36.0 36.0 36.0		0	e				
s) 37.3 9) 38.3 0.44 6.0 1.02 0.28 0.65 1.09 1.00 2.2 2.7 C C C C C C C C C C C C C							
39.3 90.44 6.0 6.0 1148 0.28 0.65 19.9 1.00 1.00 2.2.7 C C C C C C C C C C C C C	23		23.3				
0.44 6.0 2.0 1148 0.28 0.65 19.9 1.00 1.00 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	24		24.3				
20 1148 0.28 0.65 19.9 1.00 2.2.7 2.2.7 2.2.7 C 2.2.7 C 2.2.7 C 33.0 Sackfratio 0.75 sackfratio 0.75	0		0.27				
2.0 1148 0.28 0.65 19.9 1.00 2.2.7 2.7 2.7 C C C C C C C C C C C C C C C C C C C	40	5.0	2.0				
1148 0.28 0.65 19.9 12 2.8 22.7 2.7 2.7 C C C C S S S S S S S S S S S S S S S	C	2.0	2.0				
0.28 0.65 19.9 1.00 12 2.8 22.7 22.7 22.7 C 22.7 C 22.7 C 33.0 sackyratio 0.75 sackyratio 0.75	4	406	365				
0.28 0.65 19.9 1.00 1.02 2.7 2.7 2.7 2.7 2.7 3.0 10 Delay 10 Delay 10.75 10.75 10.75 10.75	0	ō	c0.24				
r 19.9 r 19.9 r 19.9 r 10.0 r 22.7 22.7 22.7 22.7 C S N 22.7 C N 33.0 Trol Delay 33.0 C S S S S S S S S S S S S S S S S S S							
19.9 10.0 10.0 22.7 22.7 C 33.0 rtrol Delay 33.0 outh (y Tatlo	0	0.72	0.91				
1,00 42 2.8 2.7 2.7 C C C S 1,00 2.7 C Hary Atrol Delay 33.0 0.75 0.75 0.00	28		31.8				
lay, d2 2.8 22.7 e C C y (s) 22.7 mmany Control Delay 33.0 c C Gapacity ratio 0.75	7	1.00	1.00				
22.7 (s) C mmany Control Delay 33.0 Control Price 33.0 Control Price 33.0 Control Price 0.75 Control C	40		24.8				
y (s) 22.7 C mmany Control Delay 33.0 C c Capacity ratio 0.75	8	34.7	56.5				
y (s) 22.7 C mmany Control Delay 33.0 C o Capacity ratio 0.75		O	ш				
Control Delay 33.0 Control Delay 33.0 Control Pratio 0.75		,	46.3			0.0	
Control Delay 33.0 c 2 Capacity ratio 0.75			0			4	
33.0							
0.75	vel of Servic	æ		O			
000							
90.06	Sum of lost time (s)			26.4			
Utilization 47.	el of Service			V			
Analysis Period (min) 15							

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> Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 1: Boylston Street & Massachusetts Avenue

2018 No Build Conditions Evening Peak Period

Movement Lane Configurations deal Flow (vphpl) Lane Width Total Lost time (s) Lane Util. Factor Frpb, ped/biles	EBL	EBT	0	I W	-				0014	d		
ane Configurations leal Flow (vphpl) ane Width otal Lost time (s) ane Util. Factor pb, pedbikes			HBY	NON.	WBI	WBR	NBL	NBT	NBK	100	SBT	SBR
eal Flow (vphpl) ane Width otal Lost time (s) ane Util. Factor pb, ped/bikes		*			4	K		AT		K	AT	
ane Width otal Lost time (s) ane Util. Factor rpb, ped/bikes	1900	1900	1900	1900	1900	1900	1900	1000	1900	1900	1900	1900
otal Lost time (s) ane Util. Factor rpb, ped/bikes	12	13	13	12	12	10	10	10	10	10	100	10
ane Util. Factor		40	2		40	40	2	40	2	4.0	40	2
rpb, ped/bikes		900			000	100		000		2	000	
DO DOOLDED		000			200	000		000		3 8	0.00	
The second second		000			200	000		100		3 8	200	
ripp, ped/bikes		0.0			00.	0.0		3.6		3.5	3.6	
-		0.97			1.00	0.85		0.98		9.	0.99	
Fit Protected		1.00			1.00	1.00		1.00		0.95	1.00	
Satd. Flow (prot)		2839			1601	813		2661		1486	2715	
FIt Permitted		0.95			0.99	1.00		0.95		0.95	1.00	
Satd. Flow (perm)		2710			1589	813		2523		1486	2715	
Volume (vph)	3	466	136	2	114	259	80	693	96	194	593	46
Peak-hour factor, PHF	0.92	0.92	0.92	0.93	0.93	0.93	0.97	0.97	0.97	0.97	0.97	0.97
Adi. Flow (vph)	6	507	148	2	123	278	00	714	66	200	611	47
RTOR Reduction (vph)	0	28	0	0	0	202	0	0	0	0	0	0
ane Group Flow (vph)	0	630	0	0	125	76	0	821	0	200	658	0
Confl. Peds. (#/hr)			591			498			803			440
Confl. Bikes (#/hr)			6			2			107			129
Heavy Vehicles (%)	33%	3%	4%	%09	%9	1%	14%	2%	3%	5%	2%	4%
	Perm			Perm		Perm	Perm			Prot		
Protected Phases		7			7			-		2	15	
Permitted Phases	7			1		1	-					
Actuated Green, G (s)		26.3			26.3	26.3		34.7		19.0	58.7	
Effective Green, g (s)		27.3			27.3	27.3		35.7		21.0	60.7	
Actuated g/C Ratio		0.27			0.27	0.27		0.36		0.21	0.61	
Clearance Time (s)		5.0			5.0	5.0		5.0		6.0		
Vehicle Extension (s)		2.0			2.0	2.0		2.0		2.0		
Lane Grp Cap (vph)		740			434	222		901		312	1648	
V/s Ratio Prot										c0.13	0.24	
V/s Ratio Perm	9.	c0.23			0.08	60.0		c0.33				
V/c Ratio		0.85			0.29	0.34		0.91		0.64	0.40	
Uniform Delay, d1		34.4			28.7	29.1		30.6		36.1	10.2	
Progression Factor		1.00			1.00	1.00		0.52		1.00	1.00	
incremental Delay, d2		9.0			0.1	0.3		12.6		9.7	0.7	
Delay (s)		43.4			28.8	29.5		28.6		45.8	10.9	
Level of Service		٥			O	O		O		٥	8	
Approach Delay (s)		43.4			29.3			28.6			19.0	
Approach LOS		٥			O			O			8	
ntersection Summary												
HCM Average Control Delay	slay		29.3	I	CM Lev	HCM Level of Service	ervice		O			
HCM Volume to Capacity ratio	ratio		0.82									
Actuated Cycle Length (s) Intersection Capacity Utilization	s) ization	w	100.0	ωS	um of k	Sum of lost time (s) ICU Level of Service	(s)		16.0 E			
Analysis Period (min)			15									

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Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 2: Belvidere Street & Massachusetts Avenue

2018 No Build Conditions Evening Peak Period

	EBL	EBT		IQ/VI					-	i		
	000,		EBR	VVDL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
	000				4			A.			AT.	
	200	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
ane Util. Factor pb. ped/bikes pb. ped/bikes th treplected ati. Flow (prot) tr Pemitted ati. Flow (pem) olume (vph)	12	12	12	12	14	12	10	10	10	10	10	10
ane Util. Factor pb. ped/bikes pp. ped/bikes tt tt tr tr tr Pemteded att. Flow (prot) att. Flow (perm) olume (vph)					4.0			4.0		g	4.0	
pb, ped/bikes pb, ped/bikes tt Protected atd. Flow (prot) tt Pemitted atd. Flow (pem)					1.00			0.95			0.95	
pb, ped/bikes It Protected and Flow (prot) It Permitted atd. Flow (perm)					0.99			1.00			1.00	
t t Protected atd. Flow (prot) It Permitted atd. Flow (perm) olume (vph)					1.00			1.00			1.00	
t Protected atd. Flow (prot) It Permitted atd. Flow (perm)					0.92			1.00			1.00	
atd. Flow (prot) It Permitted atd. Flow (perm) olume (vph)					0.99			1.00			1.00	
t Permitted atd. Flow (perm) olume (vph)					1422			2667			2749	
atd. Flow (perm) olume (vph)					0.99			0.91			1.00	
olume (vph)					1422			2427			2749	Í
	0	0	0	17	37	75	56	721	0	0	714	16
Peak-hour factor, PHF	0.25	0.25	0.25	0.81	0.81	0.81	0.97	0.97	0.97	96.0	96.0	0.96
Adj. Flow (vph)	0	0	0	21	46	93	27	743	0	0	744	17
RTOR Reduction (vph)	0	0	0	0	0	0	0	0	0	0	-	0
ane Group Flow (vph)	0	0	0	0	160	0	0	770	0	0	260	0
Confl. Bikes (#/hr)						9						124
Heavy Vehicles (%)	%0	%0	%0	8%	%0	2%	2%	%9	%0	%0	4%	%0
Bus Blockages (#/hr)	0	0	0	0	0	0	0	7	0	0	0	۵
Parking (#/hr)				-	-	-		-			-	Ī
rum Type				Split			Perm				4,1	
Protected Phases				3	0			-			-	
Permitted Phases							-					
Actuated Green, G (s)					14.8			52.0			52.0	
Effective Green, g (s)					16.8			54.0			54.0	
Actuated g/C Ratio					0.17			0.54			0.54	
Clearance Time (s)					6.0			0.9			6.0	
Vehicle Extension (s)					2.0			2.0			2.0	
ane Grp Cap (vph)					239			1311			1484	
v/s Ratio Prot					6						0.28	
v/s Ratio Perm								00.35				
v/c Ratio					0.67			0.59			0.51	
Jniform Delay, d1					39.0			15.5			14.6	
Progression Factor					1.00			1.28			0.60	
ncremental Delay, d2					5.4			1.8			1.1	
Delay (s)					4.4			21.7			10.0	
Level of Service					٥			O			4	
Approach Delay (s)		0.0			4.44			21.7			10.0	
Approach LOS		4			٥			O			4	
Intersection Summary												
HCM Average Control Delay	slay		18.6	I	CM Lev	HCM Level of Service	ivice		m			
Actuated Cycle Length (s) Intersection Capacity Utilization	ratio) ization	4,	100.0	S	um of ic	Sum of lost time (s) ICU Level of Service	(s)		29.2 B			
Analysis Period (min)			15									

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HCM Unsignalized Intersection Capacity Analysis 3: Saint Germain Street & Massachusetts Avenue

2018 No Build Conditions Evening Peak Period

Movement Lane Configurations Sign Control Grade Volume (veh.fr) Peak Hour Factor Houry flow rate (vph) Pedesstrans							
Lane Configurations Sign Control Grade Volume (veh.ft) Peak Hour Factor Hourly flow rate (vph) Pedestrians	WBL	WBR	NBT	NBR	SBL	SBT	
Sign Control Grade Volume (veh.ft) Peak Hour Factor Hourly flow rate (vph) Pedestrians	*		**			**	
Grade Volume (veh/h) Peak Hour Factor Hourly flow rate (vph) Pedestrians	Stop		Free			Free	
Volume (veh/h) Peak Hour Factor Hourly flow rate (vph) Pedestrians	%0		%0			%0	
Peak Hour Factor Hourly flow rate (vph) Pedestrians	00	0	744	0	0	732	
Hourly flow rate (vph) Pedestrians	0.63	0.63	96.0	96.0	96.0	0.96	
Pedestrians	13	2	775	0	0	762	
			352			354	
Lane Width (ft)			10.0			10.0	
Walking Speed (fl/s)			4.0			4.0	
Percent Blockage			24			25	
Right turn flare (veh)							
	None						
ge veh)							
Upstream signal (ft)			1002			222	
pX, platoon unblocked	0.85						
vC, conflicting volume	1508	742			775		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1420	742			775		
tC, single (s)	7.4	6.9			4.1		
tC, 2 stage (s)							
tF (s)	3.8	3.3			2.2		
po queue free %	80	86			100		
cM capacity (veh/h)	64	274			850		
Direction, Lane #	WB 1	NB 1	NB 2	SB 1	SB2		
Volume Total	17	388	388	381	381		
Volume Left	13	0	0	0	0		
Volume Right	2	0	0	0	0		
CSH	81	1700	1700	1700	1700		
Volume to Capacity	0.22	0.23	0.23	0.22	0.22		
Queue Length 95th (ft)	19	0	0	0	0		
Control Delay (s)	61.5	0.0	0.0	0.0	0.0		
Lane LOS	ш						
Approach Delay (s)	61.5	0.0		0.0			
Approach LOS	ш						
Intersection Summary							
Average Delay			0.7	ŀ	ŀ		1.
Intersection Capacity Utilization	ization		42.9%	2	ULeve	ICU Level of Service	∢.
Aldiyals relied (IIIII)			2				

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VHB, Inc.

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HCM Signalized Intersection Capacity Analysis 4: St. Stephen & Massachusetts Avenue

2018 No Build Conditions Evening Peak Period

Movement WET WBR WBR2 NBT NBR SBL SBT SBR SBR2 SER SER SBR SBR2 SER						-	-				1	•	
Configurations Conf	Movement	WBT	WBR	WBR2	NBL	NBT	NBR	SBL	SBT	SBR	SBR2	SER	SER2
Fig. 1900 19	Constitution of the Consti	+				**		ŀ	**			2.5	
le Width (with) 150 150 150 150 150 150 150 150 150 150	Lane Comgurations	\$000	1000	1000	1000	1000	1000	1000	100	4000	1000	400	100
al Lost time (a) 10 10 10 10 10 10 10 10 10 10 10 10 10	Ideal Flow (vpripi)	200	200	200	200	000	200	006	200	000	200	200	1300
le Util. Factor (a) 4.0 4.0 4.0 4.0 4.0 4.0 4.0 6.95 0.85 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89	Lane width	0	0	7	2	2 !	2	2	2	2	2	7	7
te official part of the part o	Total Lost time (s)	0.4			4.0	4.0			4.0			4.0	
Depticiples 1.00 1.00 0.93 1.00 1.00 0.99 1.00 0.99 0.85 0.85 0.86 0.86 0.86 0.86 0.86 0.86 0.86 0.86	Lane Util. Factor	9.			00.1	0.95			0.95			0.88	
Protected 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	Frpb, ped/bikes	1.00			9.	1.00			0.93			9	
Protected 0.88 1.00 1.00 0.99 0.88 1.00 1.00 0.99 0.88 1.00 1.00 0.99 1.00 0.98 1.00 1.00 0.99 0.99	Flpb, ped/bikes	9			1.00	1.00			1.00			1.00	
100 0.95 1.00 1	FT	0.86			9.	1.00			0.99			0.85	
6 1501 2825 2401 6 14 39 315 722 2 636 30 390 8 0.38 0.38 0.98 0.97 0.97 0.97 0.92 0 2 0 0 321 737 2 2 656 31 31 424 0 0 0 0 0 0 0 0 0 0 0 0 0 2 0 0 321 739 0 0 0 720 0 0 442 2 56 31 100 18 3 % 0% 0% 1% 5% 0% 0% 5% 0% 0% 1% 0 0 0 0 10 10 0 0 12 12 0 2 56 0 0 321 739 0 0 0 0 0 0 0 2 0 0 321 739 0 0 0 0 0 0 0 0 0 2 0 0 0 0 0 0 0 0 0	Fit Protected	1.00			0.95	1.00			1.00			1.00	
100 0.95 1.00 0.83 1.00 1	Satd. Flow (prot)	1676			1501	2825			2655			2401	
6 1501 2825 2203 2401 0 11 39 315 722 2 636 30 39 39 8 0.38 0.98 0.98 0.98 0.99 0.97 0.98 <td>FIt Permitted</td> <td>1.00</td> <td></td> <td></td> <td>0.95</td> <td>1.00</td> <td></td> <td></td> <td>0.83</td> <td></td> <td></td> <td>1.00</td> <td></td>	FIt Permitted	1.00			0.95	1.00			0.83			1.00	
8 0.38 0.38 0.39 315 722 2 636 30 30 390 0 29 103 31 737 0.97 0.97 0.97 0.97 0.92 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Satd. Flow (perm)	1676			1501	2825			2203			2401	
8 0.38 0.38 0.98 0.98 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97	Volume (vph)	0	=	39	315	722	2	2	636	30	30	390	17
0 29 103 321 737 2 2 656 31 31 424 0 0 0 0 321 739 0 0 720 0 0 0 0 0 0 0 321 739 0 0 720 0 0 442 0 0 0 321 739 0 0 720 0 0 442 0 0 0 10 10 0 0 12 12 12 0 1 0 0 0 10 10 10 0 0 11 1	Peak-hour factor, PHF	0.38	0.38	0.38	0.98	0.98	0.98	0.97	0.97	0.97	0.97	0.92	0.92
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Adi. Flow (vph)	0	29	103	321	737	2	7	656	31	31	424	18
2 0 0 321 739 0 0 720 0 0 442 186 166 166 266 546 2 55 0% 0% 1% 1% 100 18 3 8 0 0 10 10 10 0 0 12 12 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	RTOR Reduction (vph)	0	0	0	0	0	0	0	0	0	0	0	0
2 55 100 18 3 % 0% 0% 1% 5% 0% 0% 0% 0% 1% 0 0 0 10 10 0 0 12 12 12 Frot 10 10 0 0 12 12 12 1 42.8 23.2 26.2 76.0 45.8 26.2 0 28.2 76.0 45.8 23.2 0 28.2 76.0 7.0 0.26 0 0.26 0.76 0.70 0.26 0 0.28 0.34 0.71 0.09 8 0.021 0.25 0.33 0.34 1.41 0.25 0.33 0.37 1.00 5 5.8 1.0 11.9 36.3 1 100.0 Sum of lost time (s) 12.0 10 0.70 Sum of lost time (s) 12.0 10 0.70 Sum of lost time (s) 12.0 10 0.70 Sum of lost time (s) 12.0	Lane Group Flow (vph)	132	0	0	321	739	0	0	720	0	0	442	
% 0% 0% 1% 5% 0% 0% 1% </td <td>Confl. Peds. (#/hr)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>166</td> <td>166</td> <td></td> <td></td> <td>546</td> <td></td> <td></td>	Confl. Peds. (#/hr)						166	166			546		
6 0% 0% 1% 5% 0% 0% 1% 6 0 0 10 10 0 0 12 0 6 16 16 10 0 0 12 1	Confl. Bikes (#/hr)					2	55			100	18	e	
Prot Perm Over	Heaw Vehicles (%)	%0	%0	%0	1%	2%	%0	%0	2%	%0	%0	1%	%0
Frot Prot 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Bus Blockages (#/hr)	0	0	0	0	10	10	0	0	12	12	0	0
Frot Ferm 1 O 6 16 16 1 1 1 1 42.8 22 23.2 73.0 45.8 22 0 0.26 0.76 0.46 0 7.0 7.0 7.0 7.0 2.0 0.33 2147 1009 6 8 0.21 0.25 0.33 0.71 9 0.82 0.34 0.71 9 0.82 0.34 0.71 14.6 0.35 0.3 14.6 0.35 0.7 15.0 0.0 3.8 17.6 0.0 3.8 17.6 HCM Level of Service C 10 0.70 Sum of lost time (s) 12.0 15 10 0.0 Sum of lost time (s) 12.0 16 0.70 Sum of lost time (s) 12.0 17 15 17 18 18 18 18 19 19 19 19 19 19 19 19 19 19 19 19 19	Parking (#/hr)									-	-	-	
5 6 16 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Tum Type	ľ			Prot	Ì		Perm				Over	
23.2 73.0 1 42.8 25.2 76.0 0.26 0.75 0.46 0.00 0.26 0.75 0.46 0.00 0.20 0.20 0.20 0.20 0.20 0.20 0.2	Protected Phases	S			9				-			9	
23.2 73.0 42.8 22 0 28.2 76.0 45.8 22 0 0.28 0.75 0.46 0.46 0 0.28 0.75 0.46 0.0 0 2.0 7.0 7.0 7.0 0 2.0 0.21 0.25 0.33 0 0.82 0.34 0.71 0.0 1.41 0.25 0.37 1.4 0 0.0 0.0 3.8 0.37 1.4 0 0.0 0.0 3.8 0.37 1.4 0 0.0 0.0 0.0 3.8 0.37 1.4 0 0.0 0.0 0.0 0.0 3.8 0 0.0 0.0 0.0 0.0 0.0 0.3 0 0.0 0.0 0.0 0.0 0.0 0.0 0 0.0 0.0 0.0	Permitted Phases							-					
26.2 76.0 45.8 26 6 0.26 0.75 0.46 0. 7 0 0.0 7 7.0 1. 8 393 2147 1009 6 8 60.21 0.25 0.33 0.73 0.71 3 3.46 3.9 21.8 3.9 21.8 8 60.21 0.25 0.33 0.71 1.41 0.25 0.37 1.1 5 5.8 1.0 11.9 3.6 8 55.8 1.0 11.9 3.6 10 0.70 Sum of lost time (s) 12.0 100.0 Sum of lost time (s) 12.0 15 15 15 15 15 15 15 15 15 15 15 15 15 1	Actuated Green, G (s)	14.0			23.2	73.0			42.8			23.2	
6 0.26 0.75 0.46 0.70 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.	Effective Green, g (s)	16.0			26.2	76.0			45.8			26.2	
7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0	Actuated g/C Ratio	0.16			0.26	0.76			0.46			0.26	
2.0 0.2 0.	Clearance Time (s)	6.0			7.0				7.0			7.0	
8 393 2147 1009 6 8 6.0.21 0.25 0.033 0.82 0.34 0.71 3 34.6 3.9 21.8 3.2 0 1.41 0.25 0.37 1.1 5 5.8 1.0 11.9 3.8 8 55.8 1.0 11.9 B A B B A B B 17.5 B B B B 10.0 Sum of lost time (s) 12.0 100.0 Sum of lost time (s) B B	Vehicle Extension (s)	2.0			2.0				0.2			2.0	
8	Lane Grp Cap (vph)	268			393	2147			1009			629	
9 0.82 0.34 0.71 0.71 0.71 0.71 0.72 0.73 0.74 0.71 0.71 0.72 0.72 0.73 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72	v/s Ratio Prot	80.00			00.21	0.26						0.18	
9 0.82 0.34 0.71 0.00 0.71 0.00 0.72 0.00 0.00	v/s Ratio Perm								00.33				
3 34.6 3.9 21.8 33 1.41 0.25 0.37 1.1 5 5.8 1.0 3.8 5.8 1.0 D E A 11.9 36 B 17.5 B B D ACM Level of Service C C 10.0.0 Sum of lost time (s) 12.0 100.0 Sum of lost time (s) 12.0 15 ICU Level of Service B	v/c Ratio	0.49			0.82	0.34			0.71			0.70	
1.41 0.25 0.37 1.70 0.0 3.8 3.8 5.8 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	Uniform Delay, d1	38.3			34.6	3.9			21.8			33.4	
5 7.0 0.3 3.8 3.8 5.8 1.0 11.9 3.8 5.8 1.0 11.9 3.8 5.8 1.0 11.9 3.8 5.8 1.0 11.9 3.8 5.8 1.0 11.9 3.8 5.8 1.0 11.9 3.8 5.8 1.0 1.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	Progression Factor	1.00			1.41	0.28			0.37			1.00	
8 55.8 1.0 11.9 36 8 17.6 B B 8 17.6 11.9 D B HCM Level of Service C 100.0 Sum of lost time (s) 12.0 15 ICU Level of Service B	Incremental Delay, d2	0.5			7.0	0.0			3.8			2.9	
B	Delay (s)	38.8			55.8	1.0			11.9			36.3	
8 17.5 11.9 B B B C 20.6 HCM Level of Service C 100.0 Sum of lost time (s) 12.0 100.1 ICU Level of Service B 15	Level of Service	٥			ш	4			8			٥	
20.6 HCM Level of Service C io 0.70 Sum of lost time (s) 12.0 in 63.2% ICU Level of Service B 15	Approach Delay (s)	38.8				17.6			11.9				
20.6 HCM Level of Service C 0.70 12.0 12.0 10.0 Sum of lost time (s) 12.0 on 63.2% ICU Level of Service B 15	Approach LOS	۵				m			8				
20.6 HCM Level of Service C 0.70 12.0 12.0 100.0 Sum of lost time (s) 12.0 ion 63.2% ICU Level of Service B 15	Intersection Summary												
0.70 100.0 Sum of lost time (s) 12.0 63.2% ICU Level of Service B	HCM Average Control E	Delay		20.6	I	CM Lev	el of Se	rvice		ပ			
100.0 Sum of lost time (s) 12.0 63.2% ICU Level of Service B	HCM Volume to Capaci	ty ratio		0.70			7						
15	Actuated Cycle Length	(s) ilization		100.0	so S	um of lo	st time	(s)		12.0 B			
	Analysis Period (min) c Critical Lane Group			15				3-					
	A. S. S. S. S. S.	l	l	l	l	l	l	l	l	l	l	l	l

HCM Signalized Intersection Capacity Analysis 5: Huntington Avenue & Massachusetts Avenue

## Company Com								-	-	,		+	*
1700 1700 1700 1700 1800	Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
1700 1700 1700 1700 1600 1600 1600 1600 1700 1700 1700 1700 1700 1600 1600 1600 1700	ane Configurations		413			4	K	K	414			413	
12 11 12 11 11 12 12 16 12 10 15	deal Flow (vphpl)	1700	1700	1700	1700	1700	1700	1600	1600	1600	1600	1600	1600
7.5 7.5 7.0	ane Width	12	11	12	11	11	1	12	12	16	12	9	10
0.95	Fotal Lost time (s)		7.5			7.5	5.5	4.0	7.0			7.0	
100	ane Util. Factor		0.95			1.00	1.00	1.00	0.95			0.95	
1,00	-rpb, ped/bikes		0.86			1.00	1.00	1.00	1.00			1.00	
0.94	Ipb, ped/bikes		1.00			1.00	1.00	1.00	1.00			1.00	
0.98	F		0.94			1.00	0.85	1.00	0.99			0.98	
144 121 138 221 2414 100 1098 1.00	It Protected		0.98			96.0	1.00	0.95	1.00			1.00	
0.98 0.96 1.00 0.95 1.00 1.00 112 25 103 283 39 89 123 838 77 0 921 0.86 0.86 0.94 0.94 0.94 0.96 0.96 0.94 0.94 (130 29 120 301 41 95 128 953 0 0 0 1089 0.95 0.96 0.94 0.94 (133 28) 38 38 77 0 921 0 279 0 0 342 995 128 953 0 0 1089 0.95 0.94 0.94 (133 28) 38 38 38 0.96 0.96 0.94 0.94 (198 32) 351 219 0 0 342 995 128 953 0 0 1089 0.95 0.94 0.94 (198 32) 351 219 0 0 342 995 128 953 0 0 1089 0.95 0.94 0.94 0.94 0.94 0.94 0.94 0.94 0.94	Satd. Flow (prot)		2111			1341	1221	1368	2621			2414	
112 25 103 283 39 89 123 888 77 0 921 0.86 0.86 0.84 0.94 0.96 0.96 0.94 0.94 130 29 120 301 41 95 128 953 0 0 0.90 0	It Permitted		0.98			96.0	1.00	0.95	1.00			1.00	
112 25 103 283 39 89 123 838 77 0 921 0.86 0.86 0.86 0.86 0.84 0.94 0.94 0.94 0.95 0.96 0.96 0.96 0.99 0.99 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0	Satd. Flow (perm)		2111			1341	1221	1368	2621			2414	Ī
10.86 0.86 0.86 0.94 0.95	/olume (vph)	112	25	103	283	39	89	123	838	77	0	921	102
130 29 120 301 41 95 128 873 80 0 980 0	Peak-hour factor, PHF	98.0	0.86	98.0	0.94	0.94	0.94	96.0	96.0	96'0	0.94	0.94	0.94
Split Split Prot	Adj. Flow (vph)	130	29	120	301	41	98	128	873	80	0	980	109
0 279 0 0 342 95 128 953 0 0 1089 219	ROR Reduction (vph)	0	0	0	0	0	0	0	0	0	0	0	0
Spit Spit Prot	.ane Group Flow (vph)	0	279	0	0	342	95	128	953	0	0	1089	0
5% 8% 3% 1 55 4% 1 Split For Prot Prot Prot 50% 50% 4% 1 Split For Prot Prot Prot Prot 7 7 1 15.7 19.0 19.0 8.3 44.3 29.0 29.0 15.2 18.5 20.5 11.3 44.3 29.0 29.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 32.1 2.4 4.3 2.4 3.5 4.5 4.1 4.0 3.3 0.3 0.3 0.45 0.23 4.1 4.1 4.0 3.3 4.4 3.5 4.5	Confl. Peds. (#/hr)			219			351						
5% 8% 3% 6% 3% 3% 0% 3% 0% 50% 4% Split Prot Prot Prot Prot 6 6 5 7 17 1 15.7 18.0 18.0 8.3 44.3 29.0 0.15 16.7 18.0 19.0 8.3 44.3 29.0 0.15 16.7 18.0 19.0 8.3 44.3 29.0 0.15 17.0 7.0 7.0 7.0 7.0 29.0 7.0 2.0 2.0 0.11 0.44 7.0 29.0 7.0 2.0	Confl. Bikes (#/hr)			6			-			22			22
Split Split Prot Prot Prot	leavy Vehicles (%)	2%	8%	3%	%9	3%	3%	%0	3%	%0	20%	4%	1%
15.7 19.0 19.0 8.3 44.3 15.2 18.5 20.5 11.3 44.3 15.2 18.5 20.5 11.3 44.3 15.2 18.5 20.5 11.3 44.3 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 321 248 250 155 1161 2.0 2.0 2.0 2.0 321 248 250 155 1161 248 250 155 1161 248 250 155 1161 248 250 153 0.83 0.82 41.4 41.4 40.8 34.3 43.4 24.4 25 27 27 27 2.5 26 19.1 100 100 100 100 27 234.6 34.6 70.9 28.9 28 E	um Type	Split			Split		Prot	Prot					
15.7 19.0 19.0 8.3 44.3 15.2 18.5 20.5 11.3 44.3 0.15 0.18 0.20 0.11 0.44 7.0 7.0 7.0 7.0 2.0 2.0 2.0 2.1 248 250 155 1161 2.0.13 2.2 2.0 2.0 2.0 2.0 8.3 0.82 41.4 40.8 34.3 43.4 24.4 1.00 1.00 1.00 1.00 2.0.6 19.3 80.8 30.8 2 20.6 19.3 80.4 27.5 4.5 20.6 19.3 80.4 27.5 4.5 20.6 19.1 24.6 P. C.	Protected Phases	9	9		vo	2	2	1	17			-	
15.7 19.0 19.0 8.3 44.3 15.2 18.5 20.5 11.3 44.3 15.2 18.5 20.5 11.3 44.3 7.0 7.0 7.0 7.0 2.0 2.0 2.0 2.0 32.1 248 250 155 1161 20.13 20.26 0.08 0.09 20.36 0.95dr 1.38 0.38 0.82 0.82 1.00 1.00 1.00 1.00 1.00 20.6 19.3 8.4.3 24.4 1.00 1.00 1.00 1.00 1.00 20.6 19.3 8.4.5 4.5 20.6 19.3 8.4.6 70.9 29.9 E	Permitted Phases												
15.2 18.5 20.5 11.3 44.3 7.0 7.0 7.0 7.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 1.3 0.82 41.4 40.8 34.3 43.4 24.4 40.8 34.3 43.4 24.4 40.8 34.3 43.4 24.4 40.8 34.3 43.4 24.4 40.0 1.00 1.00 1.00 E F C E C C E C C C C C C C C C C C C C	Actuated Green, G (s)		15.7			19.0	19.0	8.3	44.3			29.0	
0.15 0.18 0.20 0.11 0.44 7.0 7.0 7.0 2.0 2.0 2.0 2.0 2	Effective Green, g (s)		15.2			18.5	20.5	11.3	44.3			29.0	
7.0 7.0 7.0 7.0 7.0 3.2.1 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	Actuated g/C Ratio		0.15			0.18	0.20	0.11	0.44			0.29	
2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	Slearance Time (s)		7.0			7.0	7.0	7.0				7.0	
321 248 250 155 1161 0.013 0.026 0.08 0.09 0.036 0.095dr 1.38 0.38 0.83 0.82 41.4 40.8 34.3 43.4 24.4 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	/ehicle Extension (s)	Ī	2.0			2.0	2.0	2.0				0.2	
Co13	.ane Grp Cap (vph)		321			248	250	155	1161			200	
0.95dr 1.38 0.38 0.83 0.82 41.4 40.8 34.3 43.4 24.4 1.00 1.00 1.00 1.00 1.00 20.6 193.8 0.4 27.5 4.5 62.1 234.6 34.6 70.9 28.9 E F C E C 62.1 154.8 HCM Level of Service F 1.33 100.0 Sum of lost time (s) 29.0 103.9% ICU Level of Service G	//s Ratio Prot		c0.13			00.26	0.08	0.09	c0.36			c0.45	
0.95dr 1.38 0.38 0.83 0.82 41.4 40.8 34.3 43.4 24.4 1.00 1.00 1.00 1.00 20.6 183.8 0.4 27.5 4.5 62.1 234.6 34.6 70.9 28.9 E F C E C E C C E C C C C C 154.8 HCM Level of Service F 13.3 100.0 Sum of lost time (s) C C 103.9% ICU Level of Service G C 13.3 5.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	//s Ratio Perm												
41.4 40.8 34.3 43.4 24.4 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	//c Ratio		0.95dr			1.38	0.38	0.83	0.82			1.56	
100 1.00 1.00 1.00 1.00 1.00 1.00 1.00	Jniform Delay, d1		41.4			8.04	34.3	43.4	24.4			35.5	
20.6 193.8 0.4 27.5 4.5 6.2 6.2 1 234.6 34.6 70.9 28.9 E C C C C C C C C C C C C C C C C C C	Progression Factor		1.00			1.00	1.00	1.00	1.00			0.82	
62.1 234.6 34.6 70.9 28.9 E F C E C 62.1 191.1 33.9 154.8 HCM Level of Service F 13.3 Sum of lost time (s) 29.0 103.9% ICU Level of Service G 155.1 5	ncremental Delay, d2		20.6			193.8	0.4	27.5	4.5			255.0	
62.1 191.1 33.9 E C E C C E C C E C C E C C E C C E C C E C C E C C E C C E C C E C C E C C E C C E C E E E E E E E E E E E E C E	Delay (s)		62.1			234.6	34.6	70.9	28.9			283.9	
62.1 191.1 33.9 E F C C F 154.8 HCM Level of Service F 133 Sum of lost time (s) 29.0 103.9% ICU Level of Service G 13.9% ICU Level of Service G 13.9% ICU Level of Service G 103.9% ICU Le	evel of Service		ш			ıL	O	ш	O			ш	
154.8 HCM Level of Service 1.33 100.0 Sum of lost time (s) 103.9% ICU Level of Service 1.31 103.9%	Approach Delay (s)		62.1			191.1			33.9			283.9	
154.8 HCM Level of Service 1.33 Sum of lost time (s) 100.0 Sum of lost time (s) 103.9% ICU Level of Service 1.05.9%	Approach LOS		ш			L			O			L	
154.8 HCM Level of Service 1.33 Cm of lost time (s) 100.0 Sum of lost time (s) 103.9% ICU Level of Service 1.05.9%	ntersection Summary												
1.33 100.0 Sum of lost time (s) 103.9% ICU Level of Service 15	HCM Average Control D	elay		154.8	I	CM Lev	el of Se	ervice		L			
100.0 Sum of lost time (s) 103.9% ICU Level of Service 15	HCM Volume to Capacit	y ratio		1.33									
103.9% ICU Level of Service	Actuated Cycle Length (s)		100.0	Ø	um of lo	st time	(s)		29.0			
15	ntersection Capacity Uti	ilization	-	03.9%	2	ULeve	of Ser	vice		O			
	Analysis Period (min)			15									

2018 No Build Conditions 5:00 pm 6/11/2013 Evening Peak Period VHB, Inc.

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HCM Unsignalized Intersection Capacity Analysis 6: Huntington Avenue & Driveway West

6/14/2013

2018 No Build Conditions Evening Peak Period

	1	1	ţ	1	٠	`	
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
ane Configurations		**	AT			W	
Sign Control		Free	Free		Stop		
Grade		%0	%0		%0		
Volume (veh/h)	0	0	377	00	0	62	
Peak Hour Factor	0.92	0.92	0.91	0.91	0.70	0.70	
Hourly flow rate (vph)	0	0	414	0	0	89	
Pedestrians		373			373		
Lane Width (ft)		11.0			13.0		
Walking Speed (ft/s)		4.0			4.0		
Percent Blockage		28			3		
Right turn flare (veh)							
Median type					None		
Median storage veh)							
Upstream signal (ft)		260	204				
pX, platoon unblocked							
vC, conflicting volume	286				792	828	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	196				792	928	
tC, single (s)	4.1				8.9	6.9	
tC, 2 stage (s)							
tF(s)	2.2				3.5	3.3	
% and do	100				100	59	
cM capacity (veh/h)	554				219	124	
Direction, Lane #	EB 1	EB 2	WB 1	WB 2	SB1		
Volume Total	0	0	276	147	68		
Volume Left	0	0	0	0	0		
Volume Right	0	0	0	0	68		
CSH	1700	1700	1700	1700	124		
Volume to Capacity	0.00	0.00	0.16	0.09	0.71		
Queue Length 95th (ft)	0	0	0	0	66		
Control Delay (s)	0.0	0.0	0.0	0.0	85.7		
Lane LOS					ш		
Approach Delay (s)	0.0		0.0		85.7		
Approach LOS					ıL		
Intersection Summary							
Andrew Dolon			940				
Intersection Capacity Utilization	ilization		33.4%	2	CU Leve	ICU Level of Service	∢
Analysis Period (min)			0				

6/11/2013 Page 6 Synchro 6

VHB, Inc.

HCM Signalized Intersection Capacity Analysis 7: Huntington Avenue & Cumberland Street

2018 No Build Conditions Evening Peak Period

	†	-	-	ţ	1	•	
Movement	EBT	EBR	WBI	WBT	NBI	NBR	
ane Configurations	AAA			#		*	
Ideal Flow (whini)	1900	1900	1900	1900	1900	1900	
Lane Width	11	11	11	11	12	16	
Total Lost time (s)	4.0	0	8	4.0		4.0	
Lane Util. Factor	0.91			0.86		1.00	
Frpb, ped/bikes	1.00			1.00		1.00	
Flpb, ped/bikes	1.00			1.00		1.00	
Ft	0.99			1.00		98.0	
Fit Protected	1.00			1.00		1.00	
Satd. Flow (prot)	4095			5307		1500	
Fit Permitted	1.00			1.00		1.00	
Satd. Flow (perm)	4095			5307		1500	
Volume (vph)	699	65	0	677	0	58	
Peak-hour factor, PHF	0.97	0.97	0.92	0.92	0.68	0.68	
Adi. Flow (vph)	069	67	0	847	0	85	
RTOR Reduction (vph)	9	0	0	0	0	79	
Lane Group Flow (vph)	751	0	0	847	0	9	
Confl. Bikes (#/hr)		2					
Heavy Vehicles (%)	2%	2%	%0	2%	%0	%0	
Bus Blockages (#/hr)	0	0	20	20	0	0	
Parking (#/hr)	-	٢		7			
Turn Type	1			ť	Ö	custom	
Protected Phases	9			12		2	
Permitted Phases							
Actuated Green, G (s)	8.99			77.2		6.4	
Effective Green, g (s)	86.8			77.2		6.4	
Actuated g/C Ratio	0.74			0.86		20.0	
Clearance Time (s)	4.0					4.0	
Vehicle Extension (s)	2.0	l				2.0	
Lane Grp Cap (vph)	3039			4552		107	
v/s Ratio Prot	c0.18			c0.16		0.00	
v/s Ratio Perm							
v/c Ratio	0.25			0.19		90.0	
Uniform Delay, d1	3.7			1.1		39.0	
Progression Factor	1.00			1.00		1.00	
Incremental Delay, d2	0.5			0.0		0.1	
Delay (s)	3.9			1.1		39.1	
Level of Service	×			4		۵	
Approach Delay (s)	3.9			1.1	39.1		
Approach LOS	V			V	۵		
Intersection Summary							
HCM Average Control Delay	Delay		4.2	I	CM Lev	HCM Level of Service	4
HCM Volume to Capacity ratio	ty ratio		0.23				
Actuated Cycle Length (s)	(s)		90.0	Ø	um of lo	Sum of lost time (s)	12.8
Intersection Capacity Utilization Analysis Period (min)	tilization		29.3%	ō	ULeve	ICU Level of Service	4
c Critical Lane Group							

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Syndhro 6 VHB, Inc.

VHB, Inc.

HCM Signalized Intersection Capacity Analysis
8: Huntington Avenue & Belvidere Street
Evening Peak Period

Movement EBU EBI EBT EBR WBU WBI WBI WBI NBI NBI NBI NBI Later Confideral conversion (1900 1900 1900 1900 1900 1900 1900 190													
1900 1900	Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBL	NBT	NBR	SBU
1900 1900	Lane Configurations		K	414	1		N.	*	K		4		
12	Ideal Flow (vohol)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95	Lane Width	12	11	10	11	10	10	11	11	12	16	12	12
1.00 0.95 1.00 0.96 1.00 0.16 0.100 1.00	Total Lost time (s)		4.0	4.0			4.0	4.0	4.0		4.0		
1.00 0.97	Lane Util. Factor		1.00	0.95			1.00	0.95	1.00		1.00		
1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.85 1.00 1.00 1.00 0.85 1.00 1.00 0.85 1.00 1.00 1.00 0.85 1.00 1.00 0.85 1.00 1.00 0.85 1.00 1.00 0.85 1.00 1.00 0.85 1.00 1.00 0.85 1.00 1.00 0.85 1.00 0.85 1.00 0.85 1.00 0.85 1.00 0.85 1.00 0.85 1.00 0.85 1.00 0.85 1.00 0.85 1.00 0.85 0.80	Frpb. ped/bikes		1.00	0.97			1.00	1.00	0.46		0.99		
1.00	Flpb, ped/bikes		1.00	1.00			1.00	1.00	1.00		1.00		
1433 2688	Fr		1.00	0.99			1.00	1.00	0.85		0.97		
1433 2688	Fit Protected		0.95	1,00			0.95	1.00	1.00		0.99		
1433 2688	Satd. Flow (prot)		1433	2688			1486	2991	613		1826		
1433 2688 1486 2991 613 1643 1643 1643 1644 1451 2688 1486 2991 613 1643 1643 1446 516 45 83 158 715 310 43 129 629 156 625 6295 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.	FIt Permitted		0.95	1.00			0.95	1.00	1.00		0.89		
Color Colo	Satd. Flow (perm)		1433	2688			1486	2991	613		1643		
tor, PHF 0.92 0.95 0.95 0.95 0.94 0.94 0.94 0.94 0.99 0.90 0.90 0.90	Volume (vph)	21	146	516	45	83	158	715	310	43	129	52	2
23 154 543 47 87 168 761 330 48 143 58 0 10 0 0 177 585 0 0 0 255 761 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 239 0 1 172 0 1	Peak-hour factor, PHF	0.92	0.95	0.95	0.95	0.95	0.94	0.94	0.94	0.90	06.0	06.0	0.85
0 177 585 0 0 0 0 156 0 10 0 0 0 0 158 0 10 0 0 0 177 585 0 0 0 255 761 172 0 239 0 0 15 0 177 585 0 0 0 255 761 172 0 239 0 0 0 0 0 118 0 1 1 1 1 1 1 1 1 1 1 1 1	Adj. Flow (vph)	23	154	543	47	87	168	761	330	48	143	28	9
0% 11% 3% 0% 2% 5% 5% 5% 0% 2% 0% 2% 0% 11% 3% 0% 2% 2% 5% 5% 5% 0% 2% 0% 0% 2% 15% 0% 2% 0% 0% 11% 1 1 1 1 1 1 1 1 1 1 1 1 1 1	RTOR Reduction (vph)		0	2	0	0	0	0	158	0	10	0	0
230 861 15 15 15 15 15 15 15 15 15 15 15 15 15	Lane Group Flow (vph)		177	585	0	0	255	761	172	0	239	0	0
0% 11% 3% 0% 2% 5% 5% 0% 2% 0% Frot 1 1 1 6 6 4 0% 2% 0% 2% 0% 2% 0% 2% 0% 2% 0%	Confl. Peds. (#/hr)				230				861				
Prot Prot <th< td=""><td>Confl. Bikes (#/hr)</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td>13</td><td></td><td></td><td>15</td><td></td></th<>	Confl. Bikes (#/hr)				-				13			15	
Prot Prot 1 1 1 1 1 1 1 1 1	Heavy Vehides (%)	%0	11%	3%	%0	5%	5%	2%	2%	%0	5%	%0	%0
Prot Prot Prot Prot Prot Perm Perm 4 5 5 2 1 1 1 6 6 4 4 16.8 41.1 20.2 44.5 44.5 20.7 16.8 42.1 20.2 45.5 45.5 21.7 16.8 42.1 20.2 45.5 45.5 21.7 16.8 42.1 20.2 45.5 45.5 21.7 16.8 42.1 20.2 20.2 45.5 45.5 21.7 16.8 42.1 20.2 20.2 20.0 20.0 2.0	Parking (#/hr)	-	j	-	1						ì		
16.8 41.1 20.2 44.5 44.5 16.8 41.1 1 6 6 4 16.8 41.1 20.2 44.5 44.5 16.8 42.1 20.2 44.5 44.5 16.8 42.1 20.2 45.5 45.5 0.15 0.38 0.18 0.41 0.41 0.41 0.40 0.2 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.	Tum Type	Prot	Prot			Prot	Prot		Perm	Perm	1		D.P+P
16.8 41.1 20.2 44.5 44.5 16.8 42.1 20.2 44.5 44.5 16.8 42.1 20.2 45.5 45.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5	Protected Phases	S	2	7		-	-	9			4		e
16.8 41.1 20.2 44.5 44.5 16.8 41.1 20.2 44.5 44.5 44.5 0.15 0.38 0.15 0.38 0.41 0.41 0.41 0.42 0.30 0.20 0.20 0.20 0.20 0.20 0.20 0.2	Permitted Phases								9	4			4
16.8 42.1 20.2 45.5 45.5 40.5 0.15 0.38 0.18 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41	Actuated Green, G (s)		16.8	41.1			20.2	44.5	44.5		20.7		
0.15 0.38 0.18 0.41 0.41 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.19 1029 273 1237 254 0.12 0.22 0.017 0.25 0.81 0.57 0.93 0.62 0.68 45.0 26.8 44.2 25.4 26.3 1.00 1.00 1.00 1.00 1.00 18.3 2.3 36.6 2.3 13.6 63.3 29.1 80.8 27.7 39.9 F	Effective Green, g (s)		16.8	42.1			20.2	45.5	45.5		21.7		
4.0 5.0 4.0 5.0 5.0 2.0 2.0 2.0 2.0 2.0 219 1029 273 1237 254 0.12 0.22 0.017 0.25 0.28 0.81 0.57 0.93 0.62 0.68 45.0 26.8 44.2 25.4 26.3 1.00 1.00 1.00 1.00 1.00 1.00 18.3 2.3 38.6 2.3 13.6 63.3 29.1 80.8 27 39.9 E	Actuated g/C Ratio		0.15	0.38			0.18	0.41	0.41		0.20		
2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	Clearance Time (s)		4.0	5.0			4.0	5.0	5.0		5.0		
219 1029 273 1237 254 0.12 0.22 0.0.17 0.25 0.81 0.57 0.93 0.62 0.68 45.0 26.8 44.2 25.4 26.3 1.00 1.00 1.00 1.00 1.00 18.3 29.1 80.8 27.7 39.9 E	Vehicle Extension (s)		2.0	2.0			2.0	2.0	2.0	ĺ	2.0	1	
0.12 0.22 0.0.17 0.25 0.028 0.081 0.57 0.59 0.028 0.081 0.57 0.93 0.62 0.68 45.0 26.8 44.2 25.4 26.3 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	Lane Grp Cap (vph)		219	1029			273	1237	254		324		
0.81 0.57 0.93 0.62 0.68 45.0 26.8 44.2 25.4 26.3 1.00 1.00 1.00 1.00 1.00 1.00 18.3 2.3 38.6 2.3 13.6 5.3 29.1 80.8 27.7 39.9 E C F C P C D 37.0 40.7 ay 38.9 HCM Level of Service D ratio 0.73 Sum of lost time (s) 16.0 cation 77.1% ICU Level of Service D	v/s Ratio Prot		0.12	0.22			00.17	0.25					
ay 38.9 HCM Level of Service D action 77.1% ICU Level of Service D	v/s Ratio Perm								00.28		00.15		
45.0 26.8 44.2 25.4 26.3 1.00 1.00 1.00 1.00 1.00 18.3 29.1 80.8 27.7 39.9 E	v/c Ratio		0.81	0.57			0.93	0.62	0.68		0.74		
1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	Uniform Delay, d1		45.0	26.8			44.2	25.4	26.3		41.5		
18.3 2.3 36.6 2.3 13.6 63.3 29.1 80.8 27.7 39.9 E	Progression Factor		1.00	1.00			1.00	1.00	1.00		1.00		
ay 38.9 HCM Level of Service D 110.0 Sum of lost time (s) 16.0 Ed.	Incremental Delay, d2		18.3	2.3			36.6	2.3	13.6		7.3		
ay 38.9 HCM Level of Service D ratio 0.73 Sum of lost time (s) 16.0 zation 77.1% ICU Level of Service D	Delay (s)		63.3	29.1			80.8	27.7	39.9		48.8		
37.0 40.7 D	Level of Service		ш	O			L	O	۵		۵		
ay 38.9 HCM Level of Service D ratio 0.73 HCM Level of Service D cation 77.1% ICU Level of Service D 15 ICU Level of Service D	Approach Delay (s)			37.0				40.7			48.8		
ay 38.9 HCM Level of Service ratio 0.73 Sum of lost time (s) ration 77.1% ICU Level of Service 15	Approach LOS			٥				۵			۵		
ay 38.9 HCM Level of Service ratio 0.73 Sum of lost time (s) ration 77.1% ICU Level of Service 15	Intersection Summary												
ration 110.0 Sum of lost time (s) ration 77.1% ICU Level of Service	HCM Average Control L	Delay		38.9	+	ICM Lev	rel of Se	invice		۵			
cation 77.1% ICU Level of Service	Actuated Cycle Length	(s)		110.0	(i)	of Jo mn	ost time	(8)		16.0			
a	Intersection Capacity U.	filization		77.1%	=	CU Leve	ol of Ser	vice		٥			
c Critical Lane Group	Analysis Period (min)			15									
	c Critical Lane Group												
Outdoor O	O. marken O	l	ı	١	١	1	l	ı	l	l	ı	1	- 1
												6/11	6/11/2013

HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

2018 No Build Conditions Evening Peak Period

Movement SBL SBT SBR (deal Flow (vph) 12 12 11 12 11 12 11 12 12 11 12 12 12		,	→	•	
1900 1900 1900 1900 1900 1900 1900 1900	Movement	SBL	SBT	SBR	
1900 1900 1900 1900 1900 1900 1900 1900	Lane Configurations	KZ	4		
4.0 4.0 1.00 1.00 1.00 1.00 1.00 1.00 1.	ideal Flow (vphpl)	1900	1900	1900	
1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 1.00 0.95 0.95 1.00 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0	Lane Width		7	-	
1,000 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0	lotal Lost time (s)	0.4	0.40		
1,000 1,000	Lane Ottl. Factor	00.	0.00		
1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	Frpb, ped/bikes	0	20.		
(a) 30.7 34.7 35.7 (b) 0.96 0.96 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89	Hpb, ped/bikes	00.	00.1		
0.95 1.00 1.095 1.00 0.37 1.00 0.37 1.00 0.39 0.39 1.00 0.89 0.89 0.89 0.89 0.89 0.89 0.32 0.29 0.32 0.29 0.32 0.09 0.29 0.32 0.09 0.30 0.09 0.09 0.00 0.00 0.00 0.00	H	1.00	96.0		
(s) 30.7 (a) 1.00 (b) 1.00 (c)	Fit Protected	0.95	1.00		
(s) 30.7 34.7 (s) 6.00 0.37 1.00 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0	Satd. Flow (prot)	1594	3019		
(s) 3019 HF 0.089 117 155 ph) 123 175 2% 2% 2 2% 2 34.7 3 37.7 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	Fit Permitted	0.37	1.00		
HF 0.89 0.89 0.89 ph) 0 4 138 ph) 0 4 145 ph) 0 4 145 ph) 0 4 123 175 ph) 0 123 175 ph) 0 123 175 ph) 0 126 ph) 0 12	Satd. Flow (perm)	615	3019		
HF 0.89 0.89 117 155 ph) 123 175 2% 2% 2% 18 30.7 34.7 s) 31.7 35.7 s) 2.0 2.0 0.09 0.09 0.04 0.06 0.09 0.09 0.09 0.00 0.00 0.00 0	Volume (vph)	104	138	54	
ph) 123 175 ph) 123 175 2% 2% 2% 2% 3 3.4 3 3.4 3 3.7 3 3 3.7 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	Peak-hour factor, PHF	0.89	0.89	0.89	
ph) 123 175 2% 2% 2% D.P+P 3 34.7 3 37.7 34.7 s) 30.7 34.7 s) 2.0 c) 28 980 c) 29 0.32 4.0 c) 28 980 c) 29 0.32 d) 20 c) 30 c) 40 c) 60 c) 60 d) 60	Adi. Flow (voh)	117	155	61	
ph) 123 175 2% 2% D.P+P 3 3 4 3 4 3 7 3 17 35.7 S) 30.7 34.7 S) 20.9 20.9 20.0 00.9	RTOR Reduction (vph)	0	4	0	
2% 2% 2% 2% 2% 3.4 3 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	Lane Group Flow (vph)	123	175	0	
2% 2% 2% 2% 2% 2% 3.4 3.4 4.0 6.29 0.32 6.09 0.09 0.09 0.09 0.09 0.00 0.09 0.00 0	Confl Peds (#/hr)				
2% 2% 2% 2% 19 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Confl Bikes (#/hr)			1	
(s) 30.7 34.7 (s) 31.7 35.7 34.7 (s) 30.7 34.7 35.7 34.7 35.7 36.7 36.9 30.0 32 32.0 32.0 32.0 32.0 32.0 32.0 3	Hoavy Vehicles (%)	706	706	701	
(s) 30.7 3 31.7 (s) 30.7 (s) 30.7 (o) 29 4.0 2.0 2.0 0.09 0.09 0.09 0.09 0.09 0.09	Parking (#/hr)	2	6	2	
(s) 30.7 (s) 30.7 (s) 31.7 (s) 31.7 (s) 31.7 (c) 28 (c) 26 (c) 28 (c) 28 (c) 31.2 (c) 31.7 (c) 31.7 (c) 5		D.P+P			
(s) 30.7 s) 31.7 s) 2.0 2.0 2.0 2.0 2.0 2.0 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.046 31.2 1.00 0.05 0	Protected Phases	e	34		
(s) 30.7 s) 31.7 0.29 (c) 4.0 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0	Permitted Phases	4			
s) 31.7 0.29 4.0 0.29 4.0 0.09 0.09 0.09 0.09 0.09 0.09 0.09	Actuated Green, G (s)	30.7	34.7		
0.29 4.0 4.0 2.0 0.09 0.0	Effective Green, q (s)	31.7	35.7		
4.0 5.0 2.0 2.0 2.0 0.03 0.09 0.09 0.09 1.00 4.0 3.12 1.00 4.0 3.12 1.00 4.0 3.12 1.0 4.0 5.0 4.0 5.0 4.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	Actuated q/C Ratio	0.29	0.32		
5) 2.0 286 0.004 0.009 0.46 31.2 1.00 d2 0.5 C	Clearance Time (s)	4.0			
286 0.03 0.09 0.46 31.2 1.00 d2 0.5 C	Vehicle Extension (s)	2.0			
00.09 0.09 0.09 31.2 31.2 31.7 C	Lane Grp Cap (vph)	266	980		
0.09 0.46 33.2 1.00 31.7 C	v/s Ratio Prot	c0.04	90.0		
0.46 1.00 23.1.2 31.7 C	v/s Ratio Perm	60.0			
31.2 1.00 31.7 0.5	v/c Ratio	0.46	0.18		
d2 0.5 31.7 C	Uniform Delay d1	31.2	26.6		
d2 0.5 31.7 C	Progression Factor	1.00	1.00		
31.7	Incremental Delay d2	0.5	0.0		
O	Delay (s)	317	26.7		
	Level of Service	C	C		
	Approach Delay (c)		28 5		
	Approach LOS		0		
			-		

Syndhro 6 6/11/2013 VHB, Inc.

HCM Unsignalized Intersection Capacity Analysis 9: Belvidere Street & Dalton Street

2018 No Build Conditions Evening Peak Period

	1	1	-	-	ţ	1	1	-	•	•	→	*
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					4			4			#	
Sign Control		Stop			Stop			Stop			Stop	
Volume (vph)	0	0	0	13	87	438	7	18	25	226	7	12
Peak Hour Factor	0.25	0.25	0.25	0.92	0.92	0.92	0.73	0.73	0.73	0.85	0.85	0.85
Hourly flow rate (vph)	0	0	0	4	96	476	67	25	34	266	7	4
Direction, Lane #	WB 1	NB 1	SB 1	SB2								
Volume Total (vph)	585	62	267	15								ľ
Volume Left (vph)	14	0	266	0								
Volume Right (vph)	476	8	0	14								
Hadj (s)	-0.46	-0.29	0.53	-0.65								
Departure Headway (s)	4.5	5.7	9.9	5.4								
Degree Utilization, x	0.73	0.10	0.49	0.05								
Capacity (veh/h)	977	547	518	624								
Control Delay (s)	19.0	9.4	14.5	7.3								
Approach Delay (s)	19.0	4.6	14.1									
Approach LOS	O	4	00									
Intersection Summary												
Delay HCM Level of Service Intersection Capacity Utilization	illization		16.9 C 69.3%	2	CU Leve	ICU Level of Service	vice		O			

Synchro 6 6/11/2013 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 10: Boylston Street & Dalton Street

2018 No Build Conditions Evening Peak Period

		t										
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations		*					K	41				
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
ane Width	12	11	12	12	12	12	12	12	12	12	12	12
otal Lost time (s)		4.0					4.0	4.0				
ane Util. Factor		96.0					1.00	1.00				
Frpb, ped/bikes		96.0					1.00	66.0				
Flpb, ped/bikes		1.00					1.00	1.00				
		96.0					1.00	0.92				
Fit Protected		1.00					0.95	1.00				
Satd. Flow (prot)		2844					1562	1453				
FIt Permitted		1.00					0.95	1.00				
Satd. Flow (perm)		2844					1562	1453				
Volume (vph)	63	394	197	0	0	0	292	167	183	0	0	0
Peak-hour factor, PHF	0.94	0.94	0.94	0.92	0.92	0.92	0.94	0.94	0.94	0.92	0.92	0.92
Adi. Flow (vph)	67	419	210	0	0	0	311	178	195	0	0	0
RTOR Reduction (vph)	0	45	0	0	0	0	0	0	0	0	0	0
Lane Group Flow (vph)	0	651	0	0	0	0	311	373	0	0	0	0
Confl. Bikes (#/hr)			45						12			
Heavy Vehicles (%)	3%	4%	1%	%0	%0	%0	4%	1%	13%	%0	%0	%0
fum Type	Perm				ŀ		Split	100		ŀ		
Protected Phases		-					e	e				
Permitted Phases	-											
Actuated Green, G (s)		34.9					25.7	25.7				
Effective Green, g (s)		36.9					26.7	26.7				
Actuated g/C Ratio		0.41					0.30	0.30				
Clearance Time (s)		6.0					5.0	5.0				
Vehicle Extension (s)		2.0					2.0	2.0				
ane Grp Cap (vph)		1166					463	431				ĺ
v/s Ratio Prot							0.20	c0.26				
v/s Ratio Perm		0.23										
v/c Ratio		99.0					0.67	0.87				
Uniform Delay, d1		20.3					27.8	29.9				
Progression Factor		1.00					1.00	1.00				
ncremental Delay, d2		1.9					3.0	15.9				
Delay (s)		22.2					30.8	45.9				
evel of Service		O					O	٥				
Approach Delay (s)		22.2			0.0			39.0			0.0	
Approach LOS		O			4			٥			<	
ntersection Summary												
HCM Average Control Delay	elay		30.6	1	ICM Lev	HCM Level of Service	ervice		O			
HCM Volume to Capacity ratio	y ratio		0.69									
Actuated Cycle Length (s)	(8)		90.0	()	um of lo	Sum of lost time (s)	(s)		26.4			
Intersection Capacity Utilization	Ilzation		50.0%	_	O Leve	ICU Level of Service	MOe		<			

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VHB, Inc.

Synchro 6

2018 Build Condition Synchro Reports

HCM Signalized Intersection Capacity Analysis 1: Boylston Street & Massachusetts Avenue

2018 Build Conditions Morning Peak Period

	1	†	-	1	1	1	-	+	•	*	→	•
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4		-	4	*	1	44		-	44	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	13	13	12	12	10	10	10	9	9	9	9
Total Lost time (s)		4.0			4.0	4.0		4.0		4.0	4.0	
Lane Util. Factor		0.95			1.00	1.00		0.95		1.00	0.95	
Frpb, ped/bikes		0.93			1.00	0.67		0.93		1.00	0.96	
Flpb, ped/bikes		1.00			1.00	1.00		1.00		1.00	1.00	
F		0.97			1.00	0.85		0.97		1.00	0.99	
Fit Protected		1.00			1.00	1.00		1.00		0.95	1.00	
Satd. Flow (prot)		2762			1502	860		2494		1307	2685	
FIt Permitted		0.94			66.0	1.00		0.93		0.95	1.00	
Satd. Flow (perm)		2598			1486	860		2323		1307	2685	
Volume (vph)	22	460	126	2	108	212	21	718	151	191	524	34
Peak-hour factor, PHF	0.93	0.93	0.93	990	990	990	0.95	0.95	0.95	0.91	0.91	0.91
Adj. Flow (vph)	24	495	135	n	164	321	22	756	159	210	576	37
RTOR Reduction (vph)	0	23	0	0	0	247	0	0	0	0	0	0
Lane Group Flow (vph)	0	631	0	0	167	74	0	937	0	210	613	0
Confl. Peds. (#/hr)			249			294			441			288
Confl. Bikes (#/hr)			26			-			87			110
Heavy Vehicles (%)	10%	8%	15%	%0	14%	2%	%0	10%	12%	16%	8%	%9
Tum Type	Perm	ŀ		Perm		Perm	Perm			Prot		
Protected Phases		7			7			-		2	15	
Permitted Phases	7			1		7	-					
Actuated Green, G (s)		22.0			22.0	22.0		34.0		24.0	63.0	
Effective Green, q (s)		23.0			23.0	23.0		35.0		26.0	65.0	
Actuated g/C Ratio		0.23			0.23	0.23		0.35		0.26	0.65	
Clearance Time (s)		5.0			5.0	5.0		5.0		6.0		
Vehicle Extension (s)		2.0			2.0	2.0		2.0		2.0		
Lane Grp Cap (vph)		598			342	198		813		340	1745	
v/s Ratio Prot										c0.16	0.23	
v/s Ratio Perm		c0.24			0.11	0.09		c0.40				
v/c Ratio		1.06			0.49	0.37		1.15		0.62	0.35	
Uniform Delay, d1		38.5			33.4	32.4		32.5		32.6	7.9	
Progression Factor		1.00			1.00	1.00		0.50		1.00	1.00	
Incremental Delay, d2		52.2			4.0	4.0		80.1		8.2	9.0	
Delay (s)		90.7			33.8	32.9		96.3		40.8	8.5	
Level of Service		щ			O	O		L		۵	4	
Approach Delay (s)		206			33.2			96.3			16.7	
Approach LOS		L			O			L			8	
Intersection Summary												
HCM Average Control Delay	Jelay		61.8	I	HCM Level of Service	el of Se	arvice		ш			1
HCM Volume to Capacity ratio	ty ratio		96'0									
Actuated Cycle Length (s)	(s)		100.0	S	Sum of lost time (s)	st time	(s)		16.0 F			
Analysis Period (min)			15						6			
C CIIICAI LAITE GIOUP												

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Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 2: Belvidere Street & Massachusetts Avenue

1900 2018 Build Conditions Morning Peak Period SBR 86.000 58.8 \$81 1900 1000 1000 1.000 58.7 60.7 0.61 6.0 2.0 1576 0.27 0.69 0.69 0.88 8.2 8.2 8.2 8.2 0.92 1900 %0 1900 VBR 0.61 12.3 0.43 1.8 7.1 58.7 60.7 0.61 2.0 2.0 1468 10% 1900 0.95 16 0 %0 1900 0.80 WBR %0 0.41 0.15 0.05 113 0.08 3.0 3.0 3.0 3.0 42.7 1900 0.80 0 0 Split 3 1900 %0 1900 0.25 %0 1900 Total Lost time (s)
Lane Util. Factor
Frpb, ped/bikes
Fipb, ped/bikes
Fit Protected
Satd. Flow (prot)
Fit Permitted
Satd. Flow (perm)
Volume (vph)
Peak-nour factor, PHF
Adj. Flow (vph)
Lane Group Flow (vph)
Canff. Bikes (#/hr) Tum Type
Protected Phases
Permitted Phases
Actuated Green, G (s) Actuated g/C Ratio Clearance Time (s) Vehicle Extension (s) Lane Grp Cap (vph) v/s Ratio Prot Progression Factor Incremental Delay, d2 Movement
Lane Configurations
Ideal Flow (vphpl)
Lane Width Effective Green, g (s) Heavy Vehicles (%) Bus Blockages (#/hr) Jniform Delay, d1 evel of Service //s Ratio Perm Parking (#/hr)

HCM Volume to Capacity ratio 0.61 Actuated Cyde Length (s) 100.0 Sum of lost time (s) 24.4 Intersection Capacity Utilization 50.8% ICU Level of Service A				
100.0			0.61	HCM Volume to Capacity ratio
acity Utilization 50.8%	24.4	Sum of lost time (s)	100.0	Actuated Cycle Length (s)
	4	ICU Level of Service	20.8%	Intersection Capacity Utilization
Analysis Period (min)			15	Analysis Period (min)
c Critical Lane Group				c Critical Lane Group

0.0 A

Approach Delay (s) Approach LOS

v/c Ratio

ntersection Summary

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1B, Inc.	Page 7

2018 Build Conditions Morning Peak Period HCM Unsignalized Intersection Capacity Analysis 3: Saint Germain Street & Massachusetts Avenue

	-	1	+	1	•	-	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	*		*			**	
Sign Control	Stop		Free			Free	
Grade	%0		%0			%0	
Volume (veh/h)	-	20	829	0	0	651	
Peak Hour Factor	0.50	0.50	0.94	0.94	0.90	06.0	
Hourly flow rate (vph)	2	40	882	0	0	723	
Pedestrians			161			159	
Lane Width (ft)			10.0			10.0	
Walking Speed (ft/s)			4.0			4.0	
Percent Blockage			-			1	
Right turn flare (veh)							
Median type	None						
Median storage veh)							
Upstream signal (ft)			1002			222	
pX, platoon unblocked	0.88						
vC, conflicting volume	1405	900			882		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1326	009			882		
tC, single (s)	8.9	7.3			4.1		
tC, 2 stage (s)							
tF (s)	3.5	3.5			2.2		
% eeu enenb od	98	89			100		
cM capacity (veh/h)	117	358			775		
Direction, Lane #	WB 1	NB 1	NB 2	SB 1	SB2		
Volume Total	42	441	441	362	362		
Volume Left	2	0	0	0	0		
Volume Right	40	0	0	0	0		
SH	326	1700	1700	1700	1700		
Volume to Capacity	0.13	0.26	0.26	0.21	0.21		
Queue Length 95th (ft)	11	0	0	0	0		
Control Delay (s)	17.7	0.0	0.0	0.0	0.0		
Lane LOS	O						
Approach Delay (s)	17.7	0.0		0.0			
Approach LOS	O						
Intersection Summary							
Average Delay			0.5				
Intersection Capacity Utilization	tilization		45.4%	Ω	ULeve	ICU Level of Service	4
Andread and annual			2				

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Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 4: St. Stephen & Massachusetts Avenue

2018 Build Conditions Morning Peak Period

Movement WET NBI. NBIT NBIR SBI. SBIT SBR SBR2 SER SER2 Jame Configurations with the series of the		ļ	-	-		٠	•	•	2	*	4	
figurations 4	Movement	WBT	NBL	NBT	NBR	SBL	SBT	SBR	SBR2	SER	SER2	
time (s) 1900 1900 1900 1900 1900 1900 1900 190	Lane Configurations	4	¥-	44	1		414	1	1	N. W.	. 1	
time (s) 4.0 4.0 4.0 4.0 4.0 4.0 10 10 10 12 12 time (s) 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
time (s) 4,0 4,0 4,0 4,0 4,0 6,95	Lane Width	16	10	10	10	10	10	10	10	12	12	
Fedor 1.00 1.00 0.95 0.95 0.95 0.88 0.88 0.88 0.89 0.99 0.99 0.99 0.99	Total Lost time (s)	40	4.0	4.0	1		4.0		3	4.0		
bikes 1.00 1.00 0.98 0.93 1.00 bikes 1.00 1.00 0.99 0.99 0.99 bikes 1.00 1.00 0.99 0.99 0.99 bikes 1.00 1.00 0.99 0.99 0.99 bikes 1.00 0.95 1.00 0.99 0.99 0.89 biked 1.00 0.95 1.00 0.98 1.00 0.88 biked 1.00 0.95 1.00 0.98 0.92 0.92 0.92 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95	Lane Util. Factor	1.00	1.00	0.95			0.95			0.88		
ted 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	Frpb, ped/bikes	1.00	1.00	0.98			0.93			1.00		
ted (100 100 0.99 0.99 0.99 0.85 red (100 0.99 0.99 0.99 0.85 red (100 0.95 1.00 0.99 0.68 1.00 r(prot) 1938 1472 2638 1472 2638 red (100 0.95 1.00 0.95 0.95 0.95 0.95 0.95 red (100 0.95 1.00 0.95 0.92 0.92 0.92 0.95 0.95 0.95 0.95 red (100 0.95 1.00 0.93 11 900 0.93 19 90 0.95 red (100 0.95 0.92 0.92 0.92 0.92 0.95 0.95 0.95 0.95 red (100 0.95 0.92 0.92 0.92 0.93 0.95 0.95 0.95 0.95 red (100 0.95 0.92 0.92 0.93 0.95 0.95 0.95 0.95 red (100 0.95 0.93 0.93 0.95 0.95 0.95 0.95 red (100 0.95 0.93 0.93 0.93 0.93 0.93 0.95 red (100 0.95 0.93 0.93 0.93 0.93 0.93 0.93 red (100 0.95 0.93 0.93 0.93 0.93 0.93 0.93 red (100 0.95 0.93 0.93 0.93 0.93 0.93 0.93 red (100 0.93 0.93 0	Flpb, ped/bikes	1.00	1.00	1.00			1.00			1.00		
100	F	1.00	1.00	0.99			66.0			0.85		
v (prot) 1938 1472 2838 2546 2266 v (pem) 1938 1472 2838 1472 2638 100 v (pem) 1938 1472 2638 1746 2266 100 v (pem) 1938 1472 2638 32 18 530 37 22 386 18 v (ph) 3 1472 263 0.95	Fit Protected	1.00	0.95	1.00			1.00			1.00		
100	Satd. Flow (prot)	1938	1472	2638			2546			2266		
1938 1472 2638 1745 2266 1856	Fit Permitted	1.00	0.95	1.00			0.68			1.00		
Pub	Satd. Flow (perm)	1938	1472	2638	í		1745	1		2266		
(vph) 3 311 935 0.95 0.95 0.95 0.95 0.95 0.95 (vph) 3 311 930 0 35 19 558 39 23 406 19 19 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Volume (vph)	-	286	828	32	18	530	37	22	386	18	
(vph) 3 311 900 35 19 558 39 23 406 19 duction (vph) 3 311 900 35 19 558 39 23 406 19 duction (vph) 3 311 900 35 19 568 39 23 406 19 exequity (vph) 3 311 935 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Peak-hour factor, PHF	0.38	0.92	0.95	0.92	0.95	0.95	0.95	0.95	0.95	0.95	
duction (vph) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Adj. Flow (vph)	က	311	900	35	19	558	39	23	406	19	
bickes (%) 3 311 935 0 0 639 0 0 425 0 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	RTOR Reduction (vph)	0	0	0	0	0	0	0	0	0	0	
### 15	Lane Group Flow (vph)	က	311	935	0	0	639	0	0	425	0	
ses (#hn)	Confl. Peds. (#/hr)				86	88			332			
hiddes (%) 0% 3% 10% 3% 0% 9% 9% 30% 7% 6% ages (#/hr) 0 0 10 10 12 12 0 0 0 1 1 1 1 1 1 1 1 1	Confl. Bikes (#/hr)			7	90				62	2		
ages (#/hr) 0 0 10 10 0 12 12 0 0 #hr) Phases 5 6 6 1 Perm	Heavy Vehicles (%)	%0	3%	10%	3%	%0	%6	%6	30%	1%	%9	
Prot Perm 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Bus Blockages (#/hr)	0	0	10	10	0	0	4	12	0 ,	0 .	
Prote Prot Perm 1 Over Phases 5 6 6 1 1 1 6 6 Phases 1 6 6 6 1 1 1 0 6 Phases 2 6 6 6 1 1 1 1 0 6 Phases 2 6 6 6 1 1 1 1 0 6 Phases 2 6 6 6 1 1 1 1 1 0 1 1 1 1 1 1 1 1 1 1 1	Farking (#/nr)							-		-	-	
Phases 5 6 6 1 1 6 6 6 1 1 1 6 6 6 1 1 1 1 1 1	Tum Type		Prot			Perm				Over		
Phases Green, G(s) 7.5, 25.1, 79.4, 47.3, 25.1 Green, G(s) 8.6, 28.1, 82.4, 50.3, 28.1 Green, G(s) 9.6, 28.1, 82.4, 50.3, 28.1 Green, G(s) 9.6, 28.1, 82.4, 50.3, 28.1 Green, G(s) 6.0, 7.0, 0.2 Cap (vph) 186 414 2174 878 637 Prot co.00 co.21 0.35 co.37 Prot co.00 co.21 0.35 co.37 Fort co.00 co.21 0.35 co.37 Fort do.00 2.4 0.0 4.8 2.1 Fort co.00 2.4 0.0 2.4 0.0 2.4 Green, G(s) 2.4	Protected Phases	o	ø	6			-			9		
Green, G(s) 7, B. 25.1 79.4 47.3 25.1 Green, G(s) 6.0 7.0 0.28 0.82 0.50 0.28 Filme(s) 6.0 7.0 0.28 0.82 0.50 0.28 Filme(s) 6.0 7.0 0.20 0.20 0.20 Kension(s) 2.0 0.2 0.0 0.2 Kension(s) 2.0 0.2 0.0 0.19 Frot control of 0.02 0.75 0.43 0.73 0.67 Frot control of 0.02 0.75 0.43 0.73 0.73 Frot control of 0.02 0.75 0.43 0.73 0.73 Frot control of 0.05 0.75 0.43 0.73 Frot control of 0.05 0.75 0.75 0.75 Frot control of 0.05 0.75 Frot control of 0	Permitted Phases			-		-						
June (s) 9.5 28.1 82.4 50.3 28.1 82.8 34.2 80.3 3.2 82.1 82.8 50.3 3.2 82.1 82.8 50.3 5.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7	Actuated Green, G (s)	9. (729.1	4.67			5.74			70.		
g/C Ratio 0.10 0.28 0.82 0.50 0.28 0.70 0.28 0.70 0.28 0.70 0.70 0.20 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0	Effective Green, g (s)	9.6	28.1	82.4			50.3			28.1		
transic (s) 5.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7	Actuated g/C Ratio	0.10	0.28	0.82			0.50			0.28		
Cap (vph) 186 414 2174 878 6.37 Cap (vph) 186 414 2174 878 6.37 Perm 0.02 0.21 0.35 0.19 Perm 0.02 0.75 0.43 0.73 0.67 Belay, d1 40.9 32.8 2.4 19.5 31.8 Abelay, d2 0.0 2.4 0.0 4.8 2.1 Bervice D A C C C Colorization D A C C C LOS D B C C C Delay (s) D B C C C LOS D B C C C Date (s) 100.0 Sum of lost time (s) C C Cycle (min) 100.0 Sum of lost time (s) C C Osabadiy ratio 0.66 Sum of lost time (s) C C	Clearance Time (s)	0.9	0.7				0.7			0.7		
Cap (vph) 186 414 2174 878 637 Proft c0.00 c0.21 0.35 c0.37 c0.19 Proft c0.00 c0.21 0.35 c0.37 c0.19 Perm c0.00 c0.27 c0.37 c0.67 Perm c0.02 c0.75 c0.43 c0.67 Delay d1.10 1.10 1.00 2.1 Delay d2.6 d.8 2.1 2.0 Delay d2.1 d.6 d.8 2.1 Delay d2.1 d.6 d.8 2.1 Delay d3.2 d.6 d.8 2.1 Delay d4.6 1.4 2.6.3 C C Colsis D A C C C C D D A C C C C C Cycle D B C C C C C Cycle<	Vehicle Extension (s)	2.0	2.0				0.2			2.0		
Prott c0.00 c0.21 0.35 c0.37 0.19 Perm 0.02 0.75 0.43 0.73 0.67 Belay, d1 40.9 32.8 2.4 19.5 31.8 Tabelay, d2 0.0 2.4 0.0 4.8 2.1 Envice D D A C C C Delay (s) 40.9 12.1 26.3 33.9 Envice D D A C C Delay (s) 40.9 12.1 26.3 Tage Control Delay D D A C C Time to Capacity ratio 0.66 Time to Capacity ratio 6.49% ICU Level of Service C Feriod (min) 15 Lane Group 6.66 Envice C C C C C C C C C C C C C C C C C C C	Lane Grp Cap (vph)		414	2174			878			637		
Delay, d1 40.9 2.75 0.43 0.37 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.73 0.67 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.7	v/s Ratio Prot		00.21	0.35						0.19		
0.02 0.75 0.43 0.73 0.67 belay, d1 40.9 32.8 2.4 19.5 31.8 no Factor 1.00 1.29 0.56 1.10 1.00 sal Delay, d2 0.0 2.4 0.0 4.8 2.1 ervice D D A C C C C C C LOS D B B C C me to Capacity ratio 0.06 Sum of lost time (s) 12.0 veriod (min) 15 ICU Level of Service C C lane Group 64.9% ICU Level of Service C C C C C C C C C C C C C C C C C C C	v/s Ratio Perm						00.37					
belay, d1 40,9 32,8 2,4 19,5 31,8 on Factor 1.00 1.29 0.56 1.10 1.00 lervice D D A C C Delay (s) 40,9 12,1 26,3 on Summary age Control Delay 20,1 HCM Level of Service C order Length (s) 0.00 Sum of lost time (s) 12,0 l Lane Group 15 is leaved (min) 15 on Sum of Service C on Capacity at time (s) 12,0 on Capacity at 12,0 on	v/c Ratio	0.05	0.75	0.43			0.73			0.67		
an Factor 1.00 1.29 0.56 1.10 1.00 1.00 1.29 0.56 1.10 1.00 1.00 1.00 1.29 0.56 1.10 1.00 1.00 1.00 1.00 1.00 1.00 1.0	Uniform Delay, d1	40.9	32.8	2.4			19.5			31.8		
Surface Color Co	Progression Factor	1.00	1.29	0.56			1.10			1.00		
40.9 44.6 14 26.3 33.9 ervice D A C C C LOS D B B C C D Summany Tage Control Delay (s) 0.66 Cycle Length (s) 0.00 Sum of lost time (s) 12.0 The Capacity Tation 64.9% ICU Level of Service C C Tene Group 15 I Lane Group 65.9% ICU Level of Service C C Service C C C C C C C C C C C C C C C C C C C	Incremental Delay, d2	0.0	2.4	0.0			8.4			5.1		
Delay (s) A	Delay (s)	40.9	44.6	4.			26.3			33.9		
Delay (s) 40.9 12.1 26.3 LOS I DS	Level of Service	۵	۵	4			O			O		
LOS D B C In Summary Rage Control Delay 20.1 HCM Level of Service C Inner Capacity ratio 0.66 Sum of lost time (s) 12.0 An Capacity Utilization 64.9% ICU Level of Service C Feriod (min) 15 I Lane Group 65.9% ICU Level of Service C 15 15 16 16 17 18 18 18 18 18 18 18 18 18	Approach Delay (s)	40.9		12.1			26.3					
nn Summary rage Control Delay 20.1 HCM Level of Service C ime to Capacity ratio 0.66 Cycle Length (s) 100.0 Sum of lost time (s) 12.0 Cycle Length (s) 12.0 15 I Lane Group 64.9% ICU Level of Service C 15 I Lane Group 65.9%	Approach LOS	۵		m			O					
rage Control Delay 20.1 HCM Level of Service C ime to Capacity ratio 0.66 Sum of lost time (s) 12.0 Cycle Length (s) 100.0 Sum of lost time (s) 12.0 Togacity Utilization 64.9% ICU Level of Service C Period (min) 15 I Lane Group 67.9%	Intersection Summary			1						4		
ime to Capacity ratio 0.86 Sum of lost time (s) 12.0 Cyde Length (s) 100.0 Sum of lost time (s) 12.0 Capacity Utilization 64.9% ICU Level of Service C enicd (min) 15 I Lane Group	HCM Average Control D	Delay		20.1	I	ICM Lev	el of Se	rvice		O		
Cyde Length (s) 100.0 Sum of lost time (s) 12.0 Capacity Utilization 64.9% ICU Level of Service C Feriod (min) I Lane Group	HCM Volume to Capacit	ty ratio		99.0			,					
or Capacity Unitzation 04.3% ICO Level of Service Control 15 I Lane Group 6/1	Actuated Cycle Length ((s)		100.0	ב מי	ol o mn	st time	(s)		12.0		
l Lane Group	Analysis Period (min)	IIIZALIOII		15	4	O Leve	0 0	3)		
./9	c Critical Lane Group											
	Synchro 6											6/11/2013
												Page 4

HCM Signalized Intersection Capacity Analysis 5: Huntington Avenue & Massachusetts Avenue

Movement EBI EBI EBI WBL WBL WBL WBL WBL WBL NBL NB	2	EBL	CRT										
170 170 170 170 170 170 180	8		1	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
1700 1700 1700 1700 1700 1600 1600 1600 1600 1600 1700 1700 1700 1700 1700 1700 1600 1600 1600 1600 1700			414			4	K	K	44			44	
12 11 12 11 11 12 12 16 12 10 0.95	Lane Width Chal Lost Inne (s) Lane Util. Factor Frpb, ped/bikes Frt Frp Protected Satd. Flow (prot)	200	1700	1700	1700	1700	1700	1600	1600	1600	1600	1600	1600
1,00 1,00	Total Lost time (s) Lane Uil. Factor Frpb, ped/bikes Fib., ped/bikes Frt Fit Protected Satd. Flow (prot)	12	11	12	;	11	=	12	12	16	12	10	10
Color Colo	Lane Util. Factor Frpb, ped/bikes Fit Fit Protected Satd. Flow (prot)		7.5			7.5	5.5	4.0	7.0			7.0	
Color Colo	Frpb, ped/bikes Flpb, ped/bikes Frt Ft Protected Satd. Flow (prot)		0.95			1.00	1.00	1.00	0.95			0.95	
100	Fipb, ped/bikes Frt Fit Protected Satd. Flow (prot)		96'0			1.00	1.00	1.00	1.00			0.99	
Color Colo	Frt Fit Protected Satd. Flow (prot)		1.00			1.00	1.00	1.00	1.00			1.00	
Color Colo	Fit Protected Satd. Flow (prot)		96.0			1.00	0.85	1.00	0.99			0.99	
12274 1368 1164 1368 2483 2291 0.957 0.956 1.00 0.95 1.00 12274 1368 1164 1368 2483 2291 123	Satd. Flow (prot)		0.97			96.0	1.00	0.95	1.00			1.00	
Color Colo			2274			1368	1164	1368	2483			2291	
123 10 65 133 29 90 129 933 101 0 814 HF	Fit Permitted		0.97			96.0	1.00	0.95	1.00			1.00	
HF 0.86 0.86 0.84 0.94 0.91 0.91 0.91 0.96 0.96 0.96 0.86 0.86 0.84 0.94 0.91 0.91 0.91 0.96 0.96 0.96 0.80 0.80 0.80 0.80 0.84 0.94 0.91 0.91 0.91 0.96 0.96 0.90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Satd. Flow (perm)		2274			1368	1164	1368	2483			2291	
HF 0.86 0.86 0.86 0.84 0.94 0.91 0.91 0.91 0.96 0.96 0.96 0.90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		123	10	65	133	29	90	129	933	101	0	814	88
14.3 12 76 158 31 96 142 1025 111 0 848 14.3 12 76 158 31 96 142 1025 111 0 848 15		98.0	0.86	0.86	0.84	0.94	0.94	0.91	0.91	0.91	6	96.0	0.96
ph) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		143	12	76	158	31	96	142	1025	111	0	848	92
15		0	0	0	0	0	0	0	0	0	0	0	0
158	Lane Group Flow (vph)	0	231	0	0	189	96	142	1136	0	0	940	0
Split Split Prot Prot Prot Split Split Prot Prot Prot Prot Split Spl	Confl. Peds. (#/hr)			58			151						
Split Split Prot Prot Prot Split Split Prot Prot Prot Prot Split Spl	Confl. Bikes (#/hr)			6			-			54			52
Split Split Prof Prof	Heavy Vehicles (%)	%/	27%	10%	2%	13%	8%	%0	8%	10%	%0	%6	8%
5 (e) 5 5 5 7 17 5 (e) 13.9 16.3 16.3 11.9 48.8 (s) 13.4 15.8 17.8 14.9 48.8 (s) 0.13 15.8 17.8 14.9 48.8 (s) 0.13 0.16 0.18 0.15 0.49 (s) 2.0 2.0 2.0 (s) 2.0 2.0 2.0 10 2.0 2.0 2.0 2.0 2.0 2.0 2.0 305 2.16 2.0 2.0 2.0 2.0 2.0 2.0 305 2.14 0.08 0.46 0.70 0.94 41.7 41.7 36.8 40.4 24.2 1 1.00 1.00 1.00 1.00 1.00 1.00 1.01 1.02 1.00 1.00 1.00 1.00 1.01 1.01.1 HCM Level of Service F 1.02 1.03 Sum of lost time (s) E D 1.02 1.03 Sum of lost time (s)		Solit			Split		Prot	Prot					
(s) 13.9 16.3 16.3 11.9 48.8 (s) 13.4 15.9 17.8 14.9 48.8 (o) 13.4 15.8 17.8 14.9 48.8 (o) 13.4 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0		9	9		10	2	2	7	17				
3(e) 13.9 16.3 16.3 14.9 48.8 (s) 13.4 15.8 17.8 14.9 48.8 (s) 13.4 15.8 17.8 14.9 48.8 (s) 7.0 7.0 7.0 7.0 (s) 2.0 2.0 2.0 2.0 7.0 7.0 7.0 7.0 7.0 h) 30.5 2.0 2.0 2.0 2.0 co.10 0.76 0.8 0.10 0.46 0.7 0.94 rol 41.7 41.1 36.8 0.4 24.2 1.0 rol 1.00 1.00 1.00 1.00 1.00 rol 1.00 1.00 1.00 1.00 1.00 rol 50.9 50.4 38.6 2.0 p D E D D p D E D D sapecily ratio 1.13 HOM	Permitted Phases	,)		×	•	•						
13.4 15.8 17.8 14.9 48.8 0.13 0.13 0.16 0.18 0.15 0.19 0.15 0.19 0.15 0.19 0.15 0.19 0.15 0.19 0.15 0.19 0.15 0.19 0.15 0.19 0.15 0.19 0.10 0.10 0.10 0.10 0.10 0.10 0.10	Actuated Green, G (s)		13.9			16.3	16.3	11.9	48.8			29.9	
0.13 0.16 0.18 0.15 0.49 7.0 7.0 7.0 7.0 3.05 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.16 207 204 1212 0.76 0.88 0.46 0.70 0.94 41.7 41.1 36.8 40.4 24.2 1.00 1.00 1.00 1.00 50.9 70.5 37.4 48.5 37.4 D E D D D D D	Effective Green, q (s)		13.4			15.8	17.8	14.9	48.8			29.9	
7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0	Actuated g/C Ratio		0.13			0.16	0.18	0.15	0.49			0.30	
2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	Clearance Time (s)		7.0			7.0	7.0	7.0				7.0	
305 216 207 204 1212 C0.10 C0.14 0.08 0.10 C0.46 0.76 0.88 0.46 0.70 0.94 41.7 41.1 36.8 40.4 24.2 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	Vehicle Extension (s)		2.0			2.0	2.0	2.0				0.2	
C0.10 C0.14 0.08 0.10 c0.46 0.76 0.88 0.46 0.70 0.94 41.7 41.1 36.8 40.4 24.2 1.00 1.00 1.00 1.00 E D D D E D D D S0.9 50.9 50.4 38.6 D 50.9 50.9 E Colty ratio 1.13 Letter at the co	Lane Gro Cap (vph)		305			216	207	204	1212			685	
0.76 0.88 0.46 0.70 0.94 41.7 41.1 36.8 4.0.4 24.2 41.0 1.00 1.00 1.00 1.00 9.2 29.4 0.6 8.1 13.2 50.9 70.5 37.4 48.5 37.4 50.9 59.4 38.6 D E D D D E D D E D D E D D E D D E D D E D D E D D D D	v/s Ratio Prot		c0.10			c0.14	0.08	0.10	c0.46			c0.41	
0.76 0.88 0.46 0.70 0.94 41.7 41.1 36.8 40.4 24.2 1.00 1.00 1.00 1.00 9.2 29.4 0.6 8.1 13.2 50.9 59.4 0.5 37.4 48.5 37.4 D E D D D E D D D C S9.4 10.1 HCM Level of Service F city ratio 11.03 b (s) 100.0 Sum of lost time (s) 29.0 Utilization 8.26% ICU Level of Service E	Vs Ratio Perm												
1,7	v/c Ratio		0.76			0.88	0.46	0.70	0.94			1.37	
1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	Uniform Delay, d1		41.7			41.1	36.8	40.4	24.2			35.1	
9.2 29.4 0.6 8.1 13.2 50.9 70.5 37.4 48.5 37.4 6.0 50.9 D D D D D D D D D D D D D D D D D D D	Progression Factor		1.00			1.00	1.00	1.00	1.00			1.05	
50.9 70.5 37.4 48.5 37.4 D E D D D C 50.9 59.4 38.6 D E E D D D Location 10.1.1 HCM Level of Service F City ratio 11.3 Sum of lost time (s) 29.0 Utilization 82.6% ICU Level of Service E	Incremental Delay, d2		9.2			29.4	9.0	8.1	13.2			174.1	
50.9 50.4 38.6 50.9 50.4 38.6 D	Delay (s)		50.9			70.5	37.4	48.5	37.4			211.0	
50.9 59.4 38.6	Level of Service		٥			ш	٥	۵	٥			ш	
D E D I Delay 101.1 HCM Level of Service F city ratio 1.13 Sum of lost time (s) 29.0 Utilization 82.6% ICU Level of Service E 15	Approach Delay (s)		50.9			59.4			38.6			211.0	
Delay	Approach LOS		٥			ш			۵			L	
Delay	Interesting Common	ı	1	ı	ı	۱	ı			١	ı	١	
Delay	Illeisealoli sullillaiy	ı			ľ		1	ŀ		ľ			
city ratio 1.1.5 100.0 Sum of lost time (s) 101.0 Sum of lost time (s) Utilization 82.6% ICU Level of Service 15	HCM Average Control Dela	ay		101.1	I	CM Lev	el of Se	arvice		L			
h (s) 100.0 Sum of lost time (s) Utilization 82.6% IGU Level of Service 15	HCM Volume to Capacity i	atto		1.13									
Utilization 82.6% ICU Level of Service	Actuated Cycle Length (s)			100.0	Ø	um of lo	st time	(s)		29.0			
	Intersection Capacity Utiliz	ation	~	32.6%	2	ULeve	of Ser	NIGE		ш			
	Analysis Period (min)			15									

2018 Build Conditions 7:45 am 6/11/2013 Morning Peak Period VHB, Inc.

Synchro 6 Report Page 1

HCM Unsignalized Intersection Capacity Analysis 6: Huntington Avenue & Driveway West

6/14/2013

2018 Build Conditions Morning Peak Period

4 ICU Level of Service SBR 0.85 594 3.6 594 * Stop 0% 0.85 13.0 4.0 4.0 None 3.5 100 391 255 0.01 19.0 19.0 533 533 159 0.09 0.09 WBR 0.95 WB 2 33.3% WB 1 A/BT 0% 0.95 295 295 507 0.92 208 11.0 4.0 0.00 Free \$ 260 Average Delay Intersection Capacity Utilization Analysis Period (min) 2.2 100 827 0.00 564 264 Direction, Lane #
Volume Total
Volume Left
Volume Right
cSH
Volume to Capacity
Queue Length 95th (#)
Control Delay (s)
Lane LOS
Approach Delay (s)
Approach LOS Lane Width (ft)
Walking Speed (ft/s)
Percent Blockage
Right turn flare (veh)
Median type
Median storage veh)
Upstream signal (ft)
px, platoon unblocked
vC, conflicting volume
vC1, stage 1 conf vol
vC2, stage 2 conf vol
vC2, stage (s)
tC, single (s)
tC, single (s)
tC, stage (s)
tF (s)
p0 queue free %
cM capacity (veh/h) Volume (veh/h)
Peak Hour Factor
Hourly flow rate (vph)
Pedestrians Movement
Lane Configurations
Sign Control
Grade Intersection Summary

Synchro 6 6/11/2013 Page 6 Page 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 7: Huntington Avenue & Cumberland Street

2018 Build Conditions Moming Peak Period

Movement Lane Configurations deal Flow (vphpl) Lane Width Otal Lost time (s)	FBT	EBR	WBL	TOW	NBL		
ane Configurations deal Flow (vphpl) ane Width otal Lost time (s)				2		NBK	
deal Flow (vphpl) ane Width otal Lost time (s)	441			Ħ		K	
ane Width otal Lost time (s)	1900	1900	1900	1900	1900	1900	
otal Lost time (s)	11	-	-	11	12	16	
/-/	4.0			4.0		4.0	
ane Util. Factor	0.91			0.86		1.00	
Frpb, ped/bikes	1.00			1.00		1.00	
Hpb, ped/bikes	1.00			1.00		1.00	
T.	66.0			1.00		0.86	
Fit Protected	1.00			1.00		1.00	
Satd. Flow (prot)	4049			5208		1443	
Fit Permitted	1.00			1.00		1.00	
Satd. Flow (perm)	4049			5208		1443	
Volume (vph)	586	29	0	779	0	49	
Peak-hour factor, PHF	060	060	0.95	0.95	0.67	0.67	
Adi Flow (vph)	851	32	0	820		73	
STOR Reduction (voh)	0	0	0	0	0	88	
ane Group Flow (vph)	681	0	0	820	0	ur.	
Confl Rikes (#/hr)	3	120	•	3	•)	
Heavy Vehicles (%)	10%	%0	%0	10%	%0	4%	
Bus Blockages (#/hr)	0	0	20	20	0	0	
Parking (#/hr)	-	-				-	
Turn Type				ľ	0	custom	
Protected Phases	9			12		2	
Permitted Phases							
Actuated Green, G (s)	68.4			78.8		6.4	
Effective Green, g (s)	68.4			78.8		6.4	
Actuated g/C Ratio	0.76			0.88		0.07	
Clearance Time (s)	4.0					4.0	
Vehicle Extension (s)	2.0					2.0	
ane Grp Cap (vph)	3077			4560		103	
	c0.17			c0.16		0.00	
_							
//c Ratio	0.22			0.18		0.05	
Jniform Delay, d1	3.1			0.8		39.0	
Progression Factor	1.00			1.00		1.00	
ncremental Delay, d2	0.2			0.0		0.1	
Delay (s)	3.3			0.8		39.0	
evel of Service	4			V		٥	
Approach Delay (s)	3.3			0.8	39.0		
Approach LOS	4			4	۵		
Intersection Summary							
HCM Average Control Delay	elay		3.7	1	CM Lev	HCM Level of Service	4
HCM Volume to Capacity ratio	y ratio		0.21				
Actuated Cycle Length (s)	(S		90.0	S	um of lo	Sum of lost time (s)	11.2
intersection Capacity Utilization	ization		26.6%	_	ULeve	ICU Level of Service	4
Analysis Period (min)			15				

HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

2018 Build Conditions Morning Peak Period

Movement EBU Lane Configurations 1900 Lane Worlph) 1900 Lane Width 12 Total Lost time (s) Lane Util. Factor Fipb, ped/bikes Fit Fit Protected Sadt. Flow (prot) 6 Sadt. Flow (prot) 7 Adj. Flow (vph) 0 Zadt. Flow (vph) 0 Zane Group Flow (vph) 0 Zane Group Flow (vph) 0	EBL 1900 111 4.0 1.00 1.00 1.00 1.00 1.00 1.373	1900 1000 1000 1.00 1.00 2709		1900	WBL	₩BT	WBR 1900	NBL	₩ ‡	NBR	SBU
PHF (vph)	1900 1.10 1.00 1.00 1.00 1.00 1.00 1.373 1	1900 100 100 1.00 1.00 1.00 1.00 2709	1900	1900	100	1000	1900		4		
PHF (vph)	1900 111 100 1.00 1.00 1.00 1.00 1.373 1.373 1.373 1.47 1.47 1.86 1.71 0.86 1.71 0.86 1.71 0.86 1.71 0.86 1.71 0.86 1.71 0.86 1.71 0.95 1.71 0.05	1900 10 0.95 0.99 1.00 1.00 2709	1900	1900	4000	1000	1900	0000			1
PHF (vph)	4.0 1.00 1.00 1.00 1.00 1.00 1.37 1.37 1.37 1.37 1.37 1.37 1.37 1.37	4.0 0.99 0.99 1.00 2709			200	200		1900	1900	1900	1900
PHF (vph)	4.0 1.00 1.00 1.00 1.373 1.373 1.373 1.47 1.71 1.71 1.71 1.71 1.78	0.95 0.99 1.00 1.00 2709	1	10	10	1	=	12	16	12	12
PHF (vph)	1.00 1.00 1.00 1.00 1.373 1.373 1.373 1.47 1.71 0.86 1.71 0.86	0.99 1.00 0.99 1.00 2709			4.0	4.0	4.0		4.0		
PHF (vph)	1.00 1.00 0.95 1373 0.95 147 147 0.86 171 0 178	0.99 1.00 1.00 2709			1.00	0.95	1.00		1.00		
(vph)	1.00 0.95 1373 1373 147 147 0.86 171 0 171 171 171 178	1.00 0.99 1.00 2709			1.00	1.00	0.58		1.00		
(vph)	0.95 0.95 1373 0.95 147 171 0 0 178 15%	1.00			1.00	1.00	1.00		1.00		
PHF (vph)	0.95 1373 0.95 147 171 0.86 171 0 178	1.00			1.00	1.00	0.85		0.98		
PHF (vph)	1373 0.95 1373 147 0.86 171 0 178	2709			0.95	1.00	1.00		0.99		
PHF (vph)	0.95 1373 147 0.86 171 0 178				1451	2935	722		1820		
PHF (vph)	1373 147 0.86 171 0 178	1.00			0.95	1.00	1.00		0.91		
PHF (vph) (vph)	147 0.86 171 0 178	2709			1451	2935	722		1665		
	0.86 171 0 178 15%	455	27	92	128	656	377	71	237	28	9
	171 0 178 15%	0.86	0.86	0.95	0.94	0.94	0.94	0.88	0.88	0.88	0.85
	0 178 15%	529	31	80	136	869	401	81	269	99	7
	178	4	0	0	0	0	260	0	7	0	0
	15%	556	0	0	216	869	141	0	409	0	0
Conff. Peds. (#/hr)	15%		134				467				
Confl. Bikes (#/hr)	15%		1				2			12	
Heavy Vehicles (%) 0%		3%	15%	5%	%9	%/	13%	3%	3%	5%	%0
		•	٢								
Tum Type Prot	Prot			Prot	Prot		Perm	Perm			D.P+P
Protected Phases 5	2	2		-	-	9			4		e
Permitted Phases							9	4			4
Actuated Green, G (s)	15.0	32.0			15.8	32.8	32.8		25.9		
Effective Green, g (s)	15.0	33.0			15.8	33.8	33.8		26.9		
Actuated g/C Ratio	0.15	0.33			0.16	0.34	0.34		0.27		
Clearance Time (s)	4.0	2.0			4.0	5.0	5.0		5.0		
Vehicle Extension (s)	2.0	2.0			2.0	2.0	2.0		2.0		
Lane Grp Cap (vph)	206	894			529	992	244		448		
v/s Ratio Prot	0.13	0.21			00.15	00.24					
v/s Ratio Perm							0.20		00.25		
v/c Ratio	0.86	0.62			0.94	0.70	0.58		0.91		
Uniform Delay, d1	41.5	28.2			41.7	28.7	27.2		35.4		
Progression Factor	1.00	1.00			0.82	1.04	2.72		1.00		
Incremental Delay, d2	28.4	3.2			43.0	4.1	9.5		22.4		
Delay (s)	669	31.5			77.1	33.9	83.6		8.73		
Level of Service	ш	O			ш	O	L		ш		
Approach Delay (s)		40.8				56.2			57.8		
Approach LOS		٥				ш			ш		
Intersection Summary											
HCM Average Control Delay		49.5	I	CM Lev	HCM Level of Service	ivice		٥			
HCM Volume to Capacity ratio		0.74									
Actuated Cyde Length (s)		100.0	(C)	um of lo	Sum of lost time (s)	(s)		12.0			
Intersection Capacity Utilization Analysis Period (min)	w	83.9%	2	CU Leve	ICU Level of Service	Nice		ш			
Critical Lane Group											

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Synchro 6 VHB, Inc.

2018 Build Conditions Morning Peak Period HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

1900 55 0 0 SBR 1200 1200 1200 0.95 0.95 1.00 2830 2830 2830 38.2 39.2 0.39 SBT 67 72 33 94 1109 0.08 1.00 1.00 19.1 19.1 C 8% 268 0.07 0.27 23.9 1.00 24.1 61 66 66 4% Satd. Flow (perm)
Volume (vph)
Volume (vph)
Pack-hour factor, PHF
Adj. Flow (vph)
RTOR Reduction (vph)
Lane Group Flow (vph)
Confl. Beles (#fm)
Heavy Verlicles (%) Actuated Green, G (s) Effective Green, g (s) Actuated g/C Ratio Uniform Delay, d1 Progression Factor Incremental Delay, d2 Movement
Lane Configurations
Ideal Flow (vphpl)
Lane Width
Total Lost time (s)
Lane Uill. Factor Intersection Summary Lane Grp Cap (vph)

v/s Ratio Prot

v/s Ratio Perm Delay (s) Level of Service Approach Delay (s) Approach LOS Vehicle Extension (s) Parking (#hr)
Turn Type
Protected Phases
Permitted Phases Clearance Time (s) Frpb, ped/bikes Flpb, ped/bikes Frt Fit Protected Satd. Flow (prof) Fit Permitted v/c Ratio

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HCM Unsignalized Intersection Capacity Analysis 9: Belvidere Street & Dalton Street

2018 Mitigated Conditions

SBR 0.90 28 28 Morning Peak Period Stop 18 20 20 SBT 143 0.90 159 SBL NBR 0.78 Stop 0.78 NBT 0.78 NB WBR 561 0.81 693 Yield 89 0.81 WBT 28 0.29 0.06 0.06 560 560 8.4 WBL EBR 169 159 0.55 7.0 0.33 497 12.3 11.6 B Yield 0 0.25 EBT 693 -0.48 4.7 0.91 752 35.2 1 WB2 EBL WB 1 201 91 0 0.26 5.5 0.31 637 29.4 Hadj (s) Departure Headway (s) Degree Utilization, x Hourly flow rate (vph) Direction, Lane #
Volume Total (vph)
Volume Leff (vph) Movement Lane Configurations Volume (vph) Peak Hour Factor Sign Control

26.1 D 47.3% Intersection Capacity Utilization Analysis Period (min) Delay HCM Level of Service

Intersection Summary

Capacity (veh/h)
Control Delay (s)
Approach Delay (s)
Approach LOS

ICU Level of Service

V

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Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 10: Boylston Street & Dalton Street

2018 Build Conditions Moming Peak Period

		†	-	-		1	1	-	-	*	+	*
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations		4	000	000	000	000	-	4	000	000	000	000
deal Flow (vpnpi)	12	11	12	12	12	12	12	12	12	12	1300	12
Total Lost time (e)		4.0			!		40	40	1		!	
ane Util. Factor		0.95					1.00	1.00				
Frpb, ped/bikes		0.98					1.00	1.00				
Hpb, ped/bikes		1.00					1.00	1.00				
		0.95					1.00	0.91				
Fit Protected		1.00					0.95	1.00				
Satd. Flow (prot)		2625					1504	1351				
FIt Permitted		1.00					0.95	1.00				
Satd. Flow (perm)		2625			ł	i	1504	1351	ì	ì		
/olume (vph)	53	409	242	0	0	0	252	107	177	0	0	0
Peak-hour factor, PHF	0.86	0.86	0.86	0.92	0.92	0.92	0.85	0.85	0.85	0.92	0.92	0.92
Adj. Flow (vph)	62	476	281	0	0	0	296	126	208	0	0	0
REDICTION (vph)	0	89	0	0	0	0	0	0	0	0	0	0
ane Group Flow (vph)	0	751	0	0	0	0	296	334	0	0	0	0
Confl. Bikes (#/hr)	1004	704	37	200	200	8	700	100	200	200	200	200
Teavy venices (70)	0,01	0,01	470	020	0.0	020	0.0	0.0	20.70	200	0.0	0.0
lum lype	Lem						Split	•				
Protected Phases	•	-					9	7				
Actuated Phases	-	27.4					22.5	22 5				
cuated Gleen, G(s)		5					200	3 5				
Actuated of Ratio		043					0.27	0.77				
Closmoo Timo (e)		200					200	200				
Jehiole Extension (s)		000					000	000				
Verlicie Exterision (s)		2.5					2.0	2.0				1
Lane Grp Cap (vph)		1140					409	368				
"S Ratio Prot		000					0.20	20.73				
VIS Katio Perm		0.29					-					
//c Katio		0.66					0.72	0.91				
Juiform Delay, d1		20.2					29.7	31.7				
Progression Factor		1.00					1.00	1.00				
ncremental Delay, d2		3.0					5.3	24.7				
Delay (s)		23.2					35.0	56.4				
evel of Service		O					O	ш				
Approach Delay (s)		23.2			0.0			46.3			0.0	
Approach LOS		O			<			٥			4	
ntersection Summary												
HCM Average Control Delay	Delay		33.2	I	ICM Lev	HCM Level of Service	ervice	ŀ	O			
HCM Volume to Capacity ratio	ity ratio		0.75									
Actuated Cycle Length (s)	(s)		90.0	ω :	um of lo	Sum of lost time (s)	(s)		26.4			
Intersection Capacity Utilization Analysis Period (min)	tilization		15,15	2	O Leve	ICU Level of Service	NGe N		X			
DOI DO LO			2									

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> Synchro 6 VHB, Inc.

HCM Unsignalized Intersection Capacity Analysis 11: Belvidere Street & Clearway Street

2018 Build Conditions Morning Peak Period

	1	-	-	1	•	•	
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
ane Configurations	44			44	*		
Sign Control	Free			Free	Stop		
Grade	%0	9	10	%0	%0		
Volume (veh/h)	143	0	0	191	7	32	
Peak Hour Factor	0.95	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	155	0	0	834	11	35	
Pedestrians							
ane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type					None		
Median storage veh)							
Jostream signal (ft)				480			
bX. platoon unblocked							
vC. conflicting volume			155		572	78	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol			155		572	78	
C, single (s)			4.1		8.9	6.9	
tC, 2 stage (s)							
tF(s)			2.2		3.5	3.3	
po queue free %			100		83	96	
cM capacity (veh/h)			1437		455	974	
Direction, Lane #	EB 1	EB 2	WB 1	WB 2	NB TB		
Volume Total	104	52	278	556	112		
Volume Left	0	0	0	0	11		
Volume Right	0	0	0	0	33		
cSH	1700	1700	1437	1700	545		
Volume to Capacity	90.0	0.03	0.00	0.33	0.21		
Queue Length 95th (ft)	0	0	0	0	19		
Control Delay (s)	0.0	0.0	0.0	0.0	13.3		
ane LOS					8		
Approach Delay (s)	0.0		0.0		13.3		
Approach LOS					00		
ntersection Summary							
Average Delay	2		1.4			200	-
Intersection Capacity Utilization Analysis Period (min)	dization		36.8%	_	CO Leve	ICU Level of Service	∢

Synchro 6 6/11/2013 VHB, Inc. Page 12

HCM Signalized Intersection Capacity Analysis 1: Boylston Street & Massachusetts Avenue

2018 Build Conditions Evening Peak Period

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations		*			4	K		474		K	474	
deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
ane Width	12	13	13	12	12	10	10	10	10	10	10	10
otal Lost time (s)		4.0			4.0	4.0		4.0		4.0	4.0	
ane Util. Factor		0.95			1.00	1.00		0.95		1.00	0.95	
-rpb, ped/bikes		0.91			1.00	0.60		0.94		1.00	0.95	
Hpb, ped/bikes		1.00			1.00	1.00		1.00		1.00	1.00	
F		0.97			1.00	0.85		0.98		1.00	0.99	
Fit Protected		1.00			1.00	1.00		1.00		0.95	1.00	
Satd. Flow (prot)		2850			1602	813		2662		1486	2715	
FIt Permitted		0.95			66.0	1.00		0.94		0.95	1.00	
Satd. Flow (perm)		2720			1589	813		2511		1486	2715	
Volume (vph)	6	483	136	2	119	255	12	707	97	199	593	46
Peak-hour factor, PHF	0.92	0.92	0.92	0.93	0.93	0.93	760	0.97	0.97	0.97	0.97	0.97
Adi. Flow (vph)	3	525	148	2	128	274	12	729	100	205	611	47
RTOR Reduction (vph)	0	27	0	0	0	199	0	0	0	0	0	0
ane Group Flow (vph)		649	0	0	130	75	0	841	0	205	658	0
Confl. Peds. (#/hr)			591			498			803			440
Confl. Bikes (#/hr)			6			2			107			129
Heavy Vehicles (%)	33%	3%	4%	20%	%9	1%	14%	2%	3%	5%	2%	1%
Type Type	Perm			Perm		Perm	Perm			Prot		
Protected Phases		1			7			-		2	15	
Permitted Phases	7			1		1	-					
Actuated Green, G (s)		26.4			26.4	26.4		34.6		19.0	58.6	
Effective Green, g (s)		27.4			27.4	27.4		35.6		21.0	9.09	
Actuated o/C Ratio		0.27			0.27	0.27		0.36		0.21	0.61	
Clearance Time (s)		5.0			5.0	5.0		5.0		6.0		
Jehicle Extension (s)		20			2.0	2.0		2.0		2.0		
one Can Con (wh)		745	l		425	222		100		242	16.45	ĺ
de Crip Cap (vpri)		40			420	273		460		2000	040	
Shallorion					000	000				20.75	47.0	
Vs Katio Perm		00.24			0.00	0.03		50.33		000		
VC Katio		0.0			0.30	40.0		50.0		000	0.40	
Juitorm Delay, d1		34.6			28.7	29.0		31.2		36.2	10.2	
Progression Factor		1.00			1.00	1.00		0.54		1.00	9.	
ncremental Delay, d2		10.6			0.1	0.3		15.9		10.4	0.7	
Delay (s)		45.2			28.8	29.4		32.7		46.6	11.0	
evel of Service		۵			O	O		O		۵	8	
Approach Delay (s)		45.2			29.2			32.7			19.4	
Approach LOS		٥			O			O			8	
ntersection Summary												
HCM Average Control Delay	Delay		31.1	I	HCM Level of Service	el of Se	ervice		O			
HCM Volume to Capacity ratio	ity ratio		0.85									
Actuated Cycle Length (s)	(s)		100.0	S	Sum of lost time (s)	st time	(s)		16.0			
ntersection Capacity Utilization	tilization		86.4%	⊆.	CU Level of Service	of Ser	Nice		ш			
Critical Land (min)			2									

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HCM Signalized Intersection Capacity Analysis 2: Belvidere Street & Massachusetts Avenue

2018 Build Conditions Evening Peak Period

Advenment EBL EBT EBR WBL WBT WBR NBL NBT NBR and Configurations (adeal Fow (vphpl)) 1900 1900 1900 1900 1900 1900 1900 19		1	1	-	-		1	-	-	•	•	+	*
1900 1900 1900 1900 1900 1900 1900 1900	Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
1900 1900 1900 1900 1900 1900 1900 1900	ane Configurations	T.				4			44			414	
12 12 12 12 14 12 10 10 10 10 10 10 10 10 10 10 10 10 10	deal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
14.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 6.99 1.00 0.90 1.00 0.99 1.00 0.9	ane Width	12	12	12	12	4	12	10	10	10	9	10	9
1.00 0.99 1.00 0.95 1.00 0.95 1.00 0.99 1.00 0	otal Lost time (s)					4.0			4.0			4.0	
0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.91 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97	ane Util. Factor					1.00			0.95			0.95	
0.992 1.00 1.00 0.992 1.00 0.993 1.00 0.993 1.00 0.994 0.991 27.42 0.09 0.0 0 18 37 74 26 742 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	rpb, ped/bikes					0.99			1.00			9	
0.92 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 1.00 0.99 0.91 0.424 2667 0.99 0.91 0.91 0.81 0.81 0.87 0.97 0.00 0 0 0 16 91 0.97 0.97 0.00 0 0 0 0 0 0 0 0 0 0.00 0 0 0 0 0 0	-Ipb, ped/bikes					1.00			1.00			1.00	
1424 2667 1424 2667 0.99 1.00 1424 2667 0.99 0.91 1424 2667 0.99 0.91 1424 2667 0.99 0.91 1424 2667 0.99 0.91 0.91 0.91 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97	-					0.92			1.00			1.00	
0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09	It Protected					0.99			1.00			1.00	
0.99 0.91 0.25 0.25 0.25 0.81 0.81 0.87 74 26 742 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Satd. Flow (prot)					1424			2667			2749	
1424 2430 0.25 0.25 0.25 0.81 0.81 0.97 0.97 0.00 0 0 0 0 22 46 91 27 765 0.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	It Permitted					0.99			0.91			9	
0 0 0 18 37 74 26 742 0	Satd. Flow (perm)					1424			2430			2749	Û
0.25 0.25 0.81 0.81 0.81 0.97 0.97 0.97 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	/olume (vph)	0	0	0	18	37	74	56	742	0	0	714	16
0 0 0 22 46 91 27 765 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Peak-hour factor, PHF	0.25	0.25	0.25	0.81	0.81	0.81	0.97	0.97	0.97	96.0	96.0	0.96
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(di. Flow (vph)	0	0	0	22	46	91	27	765	0	0	744	17
0 0 0 0 159 0 792 0 0 0 0 0 6% 6% 6% 6% 6% 6% 6% 6% 6% 6% 6% 6% 6%	RTOR Reduction (vph)	0	0	0	0	0	0	0	0	0	0	-	0
5 (s) 0% 0% 8% 0% 5% 7% 6% 7% 6% 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ane Group Flow (vph)	0	0	0	0	159	0	0	792	0	0	760	0
hr) 0% 0% 0% 8% 0% 5% 7% 6% 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Confl. Bikes (#/hr)						2						124
bry 0 0 0 0 0 0 7 7 1 1 1 1 1 1 1 1 1 1 1 1	leaw Vehicles (%)	%0	%0	%0	8%	%0	2%	2%	%9	%0	%0	4%	%0
(s) Split Perm 1 (s) 147 52.1 (s) 167 654.1 (s) 0.07 0.54 (s) 2.0 2.0 (s) 2.0	3us Blockages (#/hr)	0	0	0	0	0	0	0	7	0	0	0	w
Split Perm 1 3 3 1 1 (8) 14.7 52.1 (9) 0.17 0.54 (9) 0.17 0.54 (10) 0.17 0.54 (11) 0.17 0.54 (11) 0.17 0.54 (12) 0.17 0.18 (13) 0.18 (14) 0.19 (15) 0.00 44.5 21.8 (15) 0.00 44.5 21.8 (15) 0.00 44.5 21.8 (16) 0.00 44.5 21.8 (17) 0.00 0.00 0.00 (18.6 HCM Level of Service appacity ratio 0.62 (19) 0.00 Sum of lost time (8) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time (9) or the followed of Service appacity nation 0.62 (10) 0.00 Sum of lost time 0.6	arking (#/hr)				-		-		-			-	Ī
(s) 14.7 52.1 (s) 6.1	um Type				Split			Perm				4,1	
to (s) 14.7 52.1 1.0 (s) 16.7 54.1 atto (s) 0.17 0.54 atto (s) 0.11 0.67 0.60 atto (s) 0.11 0.67 0.60 atto (s) 0.60 atto	Protected Phases				3	3			-			-	
h, G (s) 14.7 52.1 1, g (s) 14.7 52.1 1, g (s) 16.7 54.1 1 (s) 6.0 6.0 6.0 1 (s) 2.0 2.0 2.0 1 (s) 2.0 2.0 2.0 2 (s) 6.0 6.0 6.0 6.0 3 (s) 6.0 6.0 6.0 6.0 6.0 4 (s) 6.0 6.0 6.0 6.0 6.0 6.0 4 (s) 6.0 44.5 2.18 2.18 2.18 8 8 10.0 44.5 2.18 2.18 9 A D A D C 100.0 44.5 10.0 C C 100.0 44.5 10.0 C C 100.0 20.0 44.5 C C 100.0 20.0 20.0 A C C 100.0 20.0 20.0	ermitted Phases							-					
atto (a) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c	Actuated Green, G (s)					14.7			52.1			52.1	
atio 0.17 0.54 e(s) 6.0 0.17 0.54 (vph) 2.0 2.0 2.0 (vph) 2.33 1315 control 0.67 0.63 d1 39.1 15.6 control 0.67 0.60 44.5 21.8 e D C C 44.5 Control Delay 18.6 HCM Level of Service Control Delay 18.6 HCM Level of Service Control 0.62 Sum of lost time (s) control 0.63 Sum of lost time (s) control 0.64 Service	fective Green, g (s)					16.7			54.1			54.1	
e (s) 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0	Actuated g/C Ratio					0.17			0.54			0.54	
(vph) 2.0 2.0 2.0 (vph) 2.0 (vph) 2.0 (vph) 2.0 (vph) 2.3 (33 (33 (44 (44 (54 (44 (54 (44 (54 (44 (54 (44 (54 (5	Searance Time (s)					6.0			6.0			6.0	
(vph) 233 1315 (vph) 0.011 0.033 (d1 0.037 0.67 0.60 d1 0.039 ector 1.00 1.27 exp. 0.0 44.5 2.18 D 0.0 44.5 21.8 Control Delay 18.6 HCM Level of Service	/ehicle Extension (s)					2.0			2.0			2.0	
d1 0.67 0.63 d1 39.1 156 cobr 39.1 156 day, d2 5.4 2.0 y (s) 0.0 44.5 21.8 mmary Control Delay 18.6 HCM Level of Service Control Delay 18.6 HCM Level of Service 10.0 Sum of lost time (s) p. 0.11 p. 0.23 p. 0.24 p. 0.27 p. 0.29 p. 0.20 p. 0.62 p. 0.20 p. 0.	ane Grp Cap (vph)					233			1315			1487	
d1 0.67 0.63 0.66 0.60 0.60 0.60 0.60 0.60 0.60	//s Ratio Prot					8			7			0.28	
Delay, d1 39.1 15.6 10.00 10.0	//s Ratio Perm								00.33				
1.27 1.00 1.27 5.4 4.5 0.0 4.5 0.0 4.5 0.0 4.5 0.0 0.0 0.0 18.6 HCM Level of Service 0.62 10.0 5.8% ICU Level of Service	//c Katio					0.0			0.00			10.0	
1.00 1.00 1.20 1.20 1.20 1.20 1.20 1.20	Dinging Delay, d1					200			0.0			0.4.0	
18.6 HCM Level of Service 0.05.88% ICU Level of Service 0.62.88% ICU Level of Service 0.62.88% ICU Level of Service 0.63.88% I	rogression ractor					3			7			20.00	
0.0 44.5 21.8 A 4.5 C A 5.5 C	nd elliellial Delay, uz								200			- 6	
0.0 44.5 21.8 A D C C A D C C C C C C C C C C C C C C	Jelay (s)					4			0.0			n «	
18.6 HCM Level of Service 58.8% ICU Level of Service 58.8% ICU Level of Service 58.8%	evel of Service		0			3			2			<	
18.6 HCM Level of Service 0.62 0.00 0.00 0.00 0.00 0.00 0.00 0.00	Approach Delay (s)		0.0			4			0. [n .	
18.6 HCM Level of Service 0.62 Sum of lost time (s) 58.8% ICU Level of Service	Approach LOS		<			2			ر			<	
18.6 HCM Level of Service 0.62 Sum of lost time (s) 58.8% ICU Level of Service	ntersection summary												
100.0 Sum of lost time (s) 58.8% ICU Level of Service	HCM Average Control L	belay to making		18.6	I	CM Le	el of Se	ivice		m			
58.8% ICU Level of Service	Actuated Cycle Length	(s)		1000	U,	of Jo min	st time	(8)		29.2			
	ntersection Capacity Ut	ilization		28.8%	_	SU Leve	of Ser	Vice		0			
Analysis Period (min) 15	Analysis Period (min)			15									

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HCM Unsignalized Intersection Capacity Analysis 3: Saint Germain Street & Massachusetts Avenue

2018 Build Conditions Evening Peak Period

	-	1	-	1	*	•	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	*	į	**			**	
Sign Control	Stop		Free			Free	
Grade	%0		%0			%0	
Volume (veh/h)	80	14	753	0	0	732	
Peak Hour Factor	0.63	0.63	96.0	96.0	96.0	96.0	
Hourly flow rate (vph)	13	22	784	0	0	762	
Pedestrians			352			354	
Lane Width (ft)			10.0			10.0	
Walking Speed (fl/s)			4.0			4.0	
Percent Blockage			24			25	
Right turn flare (veh)							
Median type	None						
Median storage veh)							
Upstream signal (ft)			1002			222	
pX, platoon unblocked	0.85						
vC, conflicting volume	1518	746			784		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1431	746			784		
tC, single (s)	7.4	6.9			4.1		
tC, 2 stage (s)							
tF (s)	3.8	3.3			2.2		
% ee y enenb od	80	92			100		
cM capacity (veh/h)	63	272			843		
Direction, Lane #	WB 1	NB 1	NB 2	SB 1	SB2		
Volume Total	35	392	392	381	381		
Volume Left	13	0	0	0	0		
Volume Right	22	0	0	0	0		
SH	123	1700	1700	1700	1700		
Volume to Capacity	0.28	0.23	0.23	0.22	0.22		
Queue Length 95th (ft)	27	0	0	0	0		
Control Delay (s)	45.6	0.0	0.0	0.0	0.0		
Lane LOS	ш						
Approach Delay (s)	45.6	0.0		0.0			
Approach LOS	ш						
Intersection Summary							
Average Delay			1.0				
Intersection Capacity Utilization Analysis Period (min)	tilization		43.1%	⊻	ULeve	ICU Level of Service	∢
THE RESERVE OF THE PARTY OF THE							

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HCM Signalized Intersection Capacity Analysis 4: St. Stephen & Massachusetts Avenue

2018 Build Conditions Evening Peak Period

12.0 B O 00.33 0.37 0.37 0.37 11.9 B HCM Level of Service Sum of lost time (s) ICU Level of Service 0.34 0.26 17.5 17.5 2147 0.82 34.6 1.41 6.7 55.5 20.5 0.70 100.0 63.2% Actuated Cyde Length (s)
Intersection Capacity Utilization
Analysis Period (min)
c Critical Lane Group 0.49 1.00 0.5 38.8 0 0 0 HCM Average Control Delay HCM Volume to Capacity ratio Incremental Delay, d2 Intersection Summary Level of Service Approach Delay (s) Approach LOS Lane Grp Cap (vph) v/s Ratio Prot Progression Factor v/c Ratio Uniform Delay, d1 //s Ratio Perm Delay (s)

0.70 33.4 1.00 2.9 36.3

6/11/2013 Page 4 Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 5: Huntington Avenue & Massachusetts Avenue

The color of the	Movement ane Configurations deal Flow (vphpl) ane Width fotal Lost time (s)	EBL	-										
100 1700 1700 1700 1700 1800 1	deal Flow (vphpl) Lane Width Total Lost time (s)		EBI	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
1700 1700 1700 1700 1600 1600 1600 1600 1700 1700 1700 1700 1600 1600 1600 1700	deal Flow (vphpl) ane Width Total Lost time (s)		414			4	K	K	414			44	
7.5 7.7 7.5 5.5 4.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7	cotal Lost time (s)	1700	1700	1700	1700	1700	1700	1600	1600	1600	1600	1600	1600
75 75 55 40 70 70 0.95 1.00 1.00 1.00 1.00 1.00 0.84 1.00 1.00 1.00 1.00 1.00 0.94 1.00 0.85 1.00 0.89 0.96 0.94 1.00 0.85 1.00 0.99 1.00 0.98 0.96 1.00 0.95 1.00 1.00 0.98 0.96 1.00 0.95 1.00 1.00 2099 1.341 1.221 1368 2615 2414 25 1.03 289 1.96 1.96 0.96 0.94 0.94 2099 1.03 289 1.24 1.221 1368 2615 2414 2099 1.03 2.94 0.94 0.94 0.96 0.96 0.94 0.94 279 0 0 0 0 0 0 0 0 0 0 0	Total Lost time (s)	12	11	12	-	11	=	12	12	16	12	10	10
0.95			7.5			7.5	5.5	4.0	7.0			7.0	
0.85 1.00 1.00 1.00 1.00 1.00 1.00 0.095 0.098 0.098 0.098 0.098 0.098 0.098 0.098 0.098 0.098 0.098 0.098 0.098 0.098 0.098 0.096 1.00 0.099 0.098 0.098 0.096 0.	ane Util. Factor		0.95			1.00	1.00	1.00	0.95			0.95	
1.00	rpb, ped/bikes		0.85			1.00	1.00	1.00	1.00			1.00	
0.94	-lpb, ped/bikes		1.00			1.00	1.00	1.00	1.00			1.00	
0.98	F		0.94			1.00	0.85	1.00	0.99			0.98	
2099 1341 1221 1368 2615 2414 2098 0.96 1.00 0.95 1.00 1.00 2099 0.96 1.00 0.95 1.00 1.00 2099 0.96 1.00 0.95 1.00 1.00 209 0.96 1.00 0.95 1.00 1.00 29 120 307 41 95 128 873 93 0 981 0 29 120 307 41 95 128 873 93 0 981 0 279 0 0 348 95 128 966 0 0 0 1090 279 0 0 348 95 128 966 0 0 0 1090 279 0 0 348 95 128 966 0 0 0 1090 279 0 0 348 95 128 966 0 0 0 0 0 279 0 0 0 0 0 0 0 0 0 0 270 0 0 0 0 0 0 0 0 0 0 270 0 0 0 0 0 0 0 0 0 270 0 0 0 0 0 0 0 0 0 270 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 280 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Fit Protected		0.98			96.0	1.00	0.95	1.00			1.00	
0.98	Satd. Flow (prot)		2099			1341	1221	1368	2615			2414	
299 134 1221 1368 2615 2414 25 103 289 39 89 123 888 89 0 922 29 086 0.94 0.94 0.96 0.96 0.94 0.94 29 120 307 41 95 128 966 0 0 1090 279 0 0 348 95 128 966 0 0 1090 279 0 0 348 95 128 966 0 0 1090 279 0 0 348 95 128 966 0 0 1090 279 0 0 348 95 128 966 0 0 0 1090 279 0 0 348 95 128 966 0 0 0 0 0 279 0 0 100 0 0 0 0 0 279 0 0 248 95 128 966 0 0 0 1090 0.15	It Permitted		0.98			96.0	1.00	0.95	1.00			1.00	
25 103 289 39 89 123 838 89 0 922 0.86 0.86 0.86 0.86 0.89 0.99 0.99 0.90 0.90 0.90 0.90 0.90	Satd. Flow (perm)		2099	ì		1341	1221	1368	2615		ì	2414	Ī
086 086 094 094 096 096 096 094 094 099 0 0 0 0 0 0 0 0 0 0 0 0 0 0	/olume (vph)	112	25	103	289	39	89	123	838	89	0	922	102
29 120 307 41 95 128 873 93 0 981 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Peak-hour factor, PHF	98.0	98.0	98.0	0.94	0.94	0.94	96.0	96.0	96.0	0.94	0.94	0.94
279 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 2 2 2	Adj. Flow (vph)	130	29	120	307	41	98	128	873	93	0	981	109
279 0 0 348 95 128 966 0 0 0 3 1 1 25 3 1 1 55 3 1 1 55 3 1 1 55 3 1 1 55 3 1 1 55 3 1 1 55 3 1 1 55 3 1 1 1 55 3 1 1 1 55 3 1 1 1 1	RTOR Reduction (vph)	0	0	0	0	0	0	0	0	0	0	0	0
219 351 55 8% 3% 3% 1% 0% 3% 0% 56% 5 5 5 5 7 17 7 7 17 15.2 18.5 20.5 11.3 44.3 15.2 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	.ane Group Flow (vph)	0	279	0	0	348	95	128	996	0	0	1090	0
8% 3% 6% 3% 3% 0% 3% 0% 55% 5 5 5 7 17 7 17 15.2 18.5 20.5 11.3 44.3 15.2 18.5 20.5 11.3 44.3 15.2 18.5 20.5 11.3 44.3 15.2 18.5 20.5 11.3 44.3 21.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	Confl. Peds. (#/hr)			219			351						
8% 3% 6% 3% 9% 3% 0% 3% 0% 50% 50% 50% 50% 50% 50% 50% 50% 50%	Confl. Bikes (#/hr)			က			-			55			22
Split custom Prot 1 15.7 19.0 19.0 18.3 44.3 15.2 18.5 20.5 11.3 44.3 15.2 18.5 20.5 11.3 44.3 7.0 7.0 7.0 7.0 2.0 2.0 2.0 2.0 2.	leavy Vehicles (%)	2%	%8	3%	%9	3%	3%	%0	3%	%0	20%	4%	1%
15.7 19.0 19.0 8.3 44.3 15.2 18.5 20.5 11.3 44.3 0.15 2.0 18.5 20.5 11.3 44.3 0.15 0.18 0.20 0.11 0.44 7.0 7.0 7.0 7.0 7.0 7.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	um Type	Split			Split	0	ustom	Prot					
15.7 19.0 19.0 8.3 44.3 15.2 15.2 18.5 20.5 11.3 44.3 0.15 7.0 7.0 7.0 7.0 7.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	Protected Phases	9	9		2	2	2	1	17			-	
15.7 19.0 19.0 8.3 44.3 15.2 18.5 20.5 11.3 44.3 16.5 20.5 11.3 44.3 16.5 20.5 11.3 44.3 16.5 20.5 11.3 44.3 16.5 20.5 11.3 44.3 16.5 20.5 11.3 44.3 16.5 20.5 11.3 44.3 16.5 20.5 11.3 44.3 16.5 11.5 16.5 16	Permitted Phases						2						
15.2 18.5 20.5 11.3 44.3 0.15 0.15 0.18 0.20 0.11 0.44 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	Actuated Green, G (s)		15.7			19.0	19.0	8.3	44.3			29.0	
7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0	ffective Green, g (s)		15.2			18.5	20.5	11.3	44.3			29.0	
7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0	Actuated g/C Ratio		0.15			0.18	0.20	0.11	0.44			0.29	
20 2.0 2.0 319 248 250 155 1158 c0.13 c0.26 0.08 c0.09 c0.37 c0.96dr 1.40 0.38 0.83 0.83 1.00 1.00 1.00 1.00 1.00 21.8 24.7 34.6 7.9 29.7 63.2 244.7 34.6 70.9 29.7 63.2 HCM Level of Service F 1.34 CUL Level of Service G	Clearance Time (s)		7.0			7.0	7.0	7.0				7.0	
319 248 250 155 1158 0.06dr 0.026 0.08 0.09 0.37 0.96dr 1.40 0.38 0.83 0.83 41.5 40.8 34.3 43.4 24.6 1.00 1.00 1.00 1.00 1.01 1.02 244.7 34.6 27.5 5.1 2 E 53.2 244.7 34.6 70.9 29.7 E 63.2 199.6 E C 63.2 HCM Level of Service F 1.34 100.0 Sum of lost time (s) 100.0 Sum of lost time (s) 29.0	Vehicle Extension (s)	1	2.0	l	Ì	2.0	2.0	2.0		Ì	ĺ	0.2	
Co.13	Lane Grp Cap (vph)		319			248	250	155	1158			200	
0.96dr 140 0.38 0.83 0.83 4.15 4.15 40.8 34.3 43.4 24.6 1.00 1.00 1.00 1.00 1.00 1.00 21.8 20.3.9 0.4 27.5 5.1 2 24.7 34.6 70.9 29.7 2 E E 199.6 E C E 3.2 HCM Level of Service F 1.34 100.0 Sum of lost time (s) 29.0 15.3	//s Ratio Prot		c0.13			00.26	0.08	0.09	c0.37			c0.45	
0.96dr 140 0.38 0.83 0.83 41.5 40.8 3.4.3 43.4 24.6 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	//s Ratio Perm												
41.5 40.8 34.3 43.4 24.6 1.00 1.00 1.00 1.00 1.00 63.2 244.7 34.6 70.9 29.7 E	//c Ratio		196dr			1.40	0.38	0.83	0.83			1.56	
1,00 1,00 1,00 1,00 1,00 1,00 1,00 1,00	Jniform Delay, d1		41.5			40.8	34.3	43.4	24.6			35.5	
21.8 203.9 0.4 27.5 5.1 63.2 24.7 34.6 70.9 29.7 63.2 199.6 34.5 E F C E 34.5 E 156.2 HCM Level of Service F 1.34 100.0 Sum of lost time (s) 29.0 153.4% ICU Level of Service G 34.5 15.4 C E F C E C C E C C C C C C C C C C C C	Progression Factor		1.00			1.00	1.00	1.00	1.00			0.81	
63.2 244.7 34.6 70.9 29.7 E F C E C 63.2 199.6 34.5 E F F C 156.2 HCM Level of Service F 13.4 100.0 Sum of lost time (s) 29.0 103.4% ICU Level of Service G	ncremental Delay, d2		21.8			203.9	0.4	27.5	5.1			255.6	
63.2 199.6 34.5 284 63.2 199.6 34.5 284 156.2 HCM Level of Service F 1.34 100.0 Sum of lost time (s) 29.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15	Delay (s)		63.2			244.7	34.6	6.07	29.7			284.5	
63.2 199.6 34.5 284 E F C C 284 156.2 HCM Level of Service F 1.34 100.0 Sum of lost time (s) 29.0 15.0 15.0 Level of Service G G 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0	evel of Service		ш			ш	O	ш	O			ш	
156.2 HCM Level of Service 1.34 100.0 Sum of lost time (s) 1.03.4% ICU Level of Service 1.03.4% ICU Level of Service	Approach Delay (s)		63.2			199.6			34.5			284.5	
156.2 HCM Level of Service 1.34 100.0 Sum of lost time (s) 103.4% ICU Level of Service 1.54 15	Approach LOS		ш			ш			O			L	
156.2 HCM Level of Service 1.34 100.0 Sum of lost time (s) 1 103.4% ICU Level of Service 1 5	ntersection Summary												
1.34 100.0 Sum of lost time (s) 103.4% ICU Level of Service 15	HCM Average Control De	elay	Ĩ	156.2	I	CM Lev	el of Se	ervice		L			
h (s) 100.0 Sum of lost time (s) Utilization 103.4% ICU Level of Service 15	HCM Volume to Capacity	/ ratio		134									
Utilization 103.4% ICU Level of Service	Actuated Cycle Length (s	(6		100.0	S	um of lo	st time	(s)		29.0			
15	ntersection Capacity Utili	ization	¥	3.4%	2	ULeve	I of Ser	vice		O			
	Analysis Period (min)			15									

2018 Build Conditions 5:00 pm 6/11/2013 Evening Peax Period VHB, Inc.

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HCM Unsignalized Intersection Capacity Analysis 6: Huntington Avenue & Driveway West

6/14/2013

2018 Build Conditions Evening Peak Period

4 ICU Level of Service 3.3 0.70 962 962 3.5 100 216 None 800 89 0.723 400 7 57.0 7 67.0 87.0 SB1 WBR WB 2 0.09 282 0 0.17 0.00 14.8 33.4% 15 ABT 0.91 0.91 423 WB 1 507 Free 0% 0 0.92 0 373 11.0 4.0 4.0 0.00 260 Average Delay Intersection Capacity Utilization Analysis Period (min) 0.00 4.1 100 549 Direction, Lane #
Volume Total
Volume Left
Volume Right
cSH
Colume to Capacity
Queue Length 95th (#)
Control Delay (s)
Lane LOS Lane Width (ft)
Walking Speed (ft's)
Walking Speed (ft's)
Percent Biockage
Right turn flare (veh)
Median type
Median storage veh)
Upstream signal (ft)
pX, platoon unblocked
vC, conflicting volume
vC, conflicting volume
vC, stage I conf vol
vCz, stage 2 conf vol Volume (veh/h)
Peak Hour Factor
Hourly flow rate (vph)
Pedestrians Movement
Lane Configurations
Sign Control
Grade tC, single (s)
tC, 2 stage (s)
tF (s)
p0 queue free %
cM capacity (veh/h) Intersection Summary Approach Delay (s) Approach LOS

6/11/2013 Page 6 Synchro 6

VHB, Inc.

2018 Build Conditions Evening Peak Period

Movement Lane Configurations deal Flow (vphpl) Lane Width	EBT	EBR	WBI	TAW	NBL	5014	
ane Configurations deal Flow (vphpl) ane Width			1	2		NBK	
leal Flow (vphpl) ane Width	441	3		Ш		K	
ane Width	1900	1900	1900	1900	1900	1900	
	1	-	=	11	12	16	
Total Lost time (s)	4.0			4.0		4.0	
ane Util. Factor	0.91			98.0		1.00	
Frpb, ped/bikes	1.00			1.00		1.00	
-1pb, ped/bikes	1.00			1.00		1.00	
Į.	0.99			1.00		0.86	
Fit Protected	1.00			1.00		1.00	
Satd. Flow (prot)	4096			5307		1500	
Elt Permitted	1.00			1.00		1.00	
Satd. Flow (perm)	4096			5307		1500	
Volume (vph)	686	65	0	789	0	58	
Peak-hour factor PHF	0.97	260	0 92	0 82	0.68	0.68	
Adi Flow (voh)	707	67	0	858	0	85	
STOR Reduction (vph)	10	0	0	0	0	62	
ane Group Flow (vph)	769	0	0	858	0	· · ·	
Confl. Bikes (#/hr)	2	2	•				
Heavy Vehicles (%)	2%	2%	%0	2%	%0	%0	
Bus Blockages (#/hr)	0	0	20	20	0	0	
Parking (#/hr)	-	-				-	
fum Type				1	0	custom	
Protected Phases	9			12		2	
Permitted Phases							
Actuated Green, G (s)	8.99			77.2		6.4	
Effective Green, g (s)	8.99			77.2		6.4	
Actuated g/C Ratio	0.74			0.86		20.0	
Clearance Time (s)	4.0					4.0	
Vehicle Extension (s)	2.0					2.0	
ane Grp Cap (vph)	3040			4552		107	
//s Ratio Prot	60.19			c0.16		0.00	
//s Ratio Perm							
//c Ratio	0.25			0.19		90.0	
Uniform Delay, d1	3.7			1.1		39.0	
Progression Factor	1.00			1.00		1.00	
ncremental Delay, d2	0.2			0.0		0.1	
Delay (s)	3.9			1.1		39.1	
evel of Service	V			4		۵	
Approach Delay (s)	3.9			1.1	39.1		
Approach LOS	<			V	٥		
Intersection Summary							
HCM Average Control Delay	elay		4.2	I	CM Lev	HCM Level of Service	¥
HCM Volume to Capacity ratio	by ratio		0.24				
Actuated Cycle Length (s) intersection Capacity Utilization	s) ilization		90.0	ω⊆	um of lo	Sum of lost time (s) ICU Level of Service	12.8 A
Analysis Period (min)			15				

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Synchro 6 VHB, Inc.

HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

2018 Build Conditions Evening Peak Period

Movement												
	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBL	NBT	NBR	SBU
Lane Configurations		K	44	7		K	**	K		4		
	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	11	10	11	10	10	11	11	12	16	12	-
Total Lost time (s)		4.0	4.0			4.0	4.0	4.0		4.0		
Lane Util. Factor		1.00	0.95			1.00	0.95	1.00		1.00		
Frpb, ped/bikes		1.00	0.97			1.00	1.00	0.46		0.99		
Flpb, ped/bikes		1.00	1.00			1.00	1.00	1.00		1.00		
Frt		90.1	0.99			1.00	1.00	0.85		0.97		
Fit Protected		0.95	1.00			0.95	1.00	1.00		0.99		
Satd. Flow (prot)		1431	2688			1486	2991	613		1827		
Fit Permitted		0.95	1.00			0.95	1.00	1.00		0.89		
Satd. Flow (perm)	Ì	1431	2688	ì		1486	2991	613		1640	Ì	n
	51	164	516	45	83	158	715	324	43	131	52	1
Dr, PHF	0.92	0.95	0.95	0.95	0.95	0.94	0.94	0.94	0.90	0.90	0.90	0.85
Adj. Flow (vph)	23	173	543	47	87	168	761	345	48	146	28	9
RTOR Reduction (vph)	0	0	2	0	0	0	0	169	0	9	0	0
Lane Group Flow (vph)	0	196	585	0	0	255	761	176	0	242	0	0
Confl. Peds. (#/hr)				230				861				
Confl. Bikes (#/hr)				-				13			15	
Heavy Vehicles (%)	%0	11%	3%	%0	5%	2%	2%	2%	%0	5%	%0	%0
Parking (#/hr)			-	-								
	Prot	Prot			Prot	Prot		Perm	Perm			D.P+P
Protected Phases	S	2	7		-	-	9			4		3
Permitted Phases								9	4			
Actuated Green, G (s)		17.9	40.9			20.2	43.2	43.2		20.9		
Effective Green, g (s)		17.9	41.9			20.2	44.2	44.2		21.9		
Actuated g/C Ratio		0.16	0.38			0.18	0.40	0.40		0.20		
Clearance Time (s)		4.0	5.0			4.0	5.0	5.0		5.0		
Vehicle Extension (s)		2.0	2.0			2.0	2.0	2.0		2.0		
Lane Grp Cap (vph)		233	1024			273	1202	246		327		
v/s Ratio Prot		0.14	0.22			00.17	0.25					
v/s Ratio Perm								60.29		60.15		
v/c Ratio		0.84	0.57			0.93	0.63	0.72		0.74		
Uniform Delay, d1		44.7	26.9			44.2	26.4	27.6		4.14		
Progression Factor		1.00	1.00			1.00	1.00	1.00		1.00		
Incremental Delay, d2		22.2	2.3			36.6	2.5	16.4		7.3		
Delay (s)		6.99	29.3			80.8	28.9	4.0		48.7		
Level of Service		ш	O			u.	O	۵		۵		
Approach Delay (s)			38.6				42.5			48.7		
Approach LOS			۵				۵			۵		
Intersection Summary												
HCM Average Control Delay	ay		40.1	†	HCM Level of Service	el of Se	arvice	h	٥			
HCM Volume to Capacity ratio	atio		0.72	. !								
Actuated Cycle Length (s)			110.0	(C)	Sum of lost time (s)	st time	(s)		15.0			
Intersection Capacity Utilization	ation		79.4%	=	ICU Level of Service	of Ser	VICE		۵			
Analysis Period (min)			15									

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HCM Signalized Intersection Capacity Analysis 8: Huntington Avenue & Belvidere Street

2018 Build Conditions Evening Peak Period 1900 0.89 SBR 1900 12 4.0 6.95 0.95 1.00 1.00 3001 3001 SBT 140 0.89 157 49 180 2% 4.0 1.00 1.00 1.00 1.594 0.36 106 0.89 125 2% Satd. Flow (perm)
Volume (vph)
Volume (vph)
Pack-hour factor, PHF
Adj. Flow (vph)
RTOR Reduction (vph)
Lane Group Flow (vph)
Confl. Beles (#fm)
Heavy Verlicles (%) Movement
Lane Configurations
Ideal Flow (vphpl)
Lane Width
Total Lost time (s)
Lane Uill. Factor Frpb, ped/bikes Flpb, ped/bikes Frt Fit Protected Satd. Flow (prof) Fit Permitted

34.9 35.9 0.33 0.18 1.00 0.0 26.6 C 28.4 979 30.9 267 0.09 0.09 0.47 31.1 1.00 0.5 31.6 Actuated Green, G (s) Effective Green, g (s) Actuated g/C Ratio Uniform Delay, d1 Progression Factor Incremental Delay, d2 Intersection Summary Lane Grp Cap (vph)

v/s Ratio Prot

v/s Ratio Perm Delay (s) Level of Service Approach Delay (s) Approach LOS Vehicle Extension (s) Parking (#hr)
Turn Type
Protected Phases
Permitted Phases Clearance Time (s) v/c Ratio

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VHB, Inc. Synchro 6

HCM Unsignalized Intersection Capacity Analysis

12 0.85 14 SBR 2018 Mitigated Conditions **Evening Peak Period** SBT Stop 24 0.85 28 28 226 0.85 266 NBR 0.73 V Stop 0.73 NBT 0.73 图 ICU Level of Service WBR 459 0.92 499 WBT Yield 87 0.92 95 82 0.92 89 28 0 14 -0.35 5.8 0.05 586 7.8 WBL 14.4 B 42.5% 15 EBR 280 266 0.51 0.51 6.6 0.51 517 15.2 14.5 B 9: Belvidere Street & Dalton Street 0.25 EBT 4.8 0.67 731 15.8 **Yield** 1 WB 2 499 Intersection Capacity Utilization Analysis Period (min) EBL 0.25 WB 1 0.31 5.8 0.30 594 10.1 14.3 \$ 8 Hadj (s) Departure Headway (s) Delay HCM Level of Service Hourly flow rate (vph) Intersection Summary Capacity (veh/h)
Control Delay (s)
Approach Delay (s)
Approach LOS Direction, Lane #
Volume Total (vph)
Volume Leff (vph) Degree Utilization, x Movement Lane Configurations Volume (vph) Peak Hour Factor Sign Control

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HCM Signalized Intersection Capacity Analysis 10: Boylston Street & Dalton Street

2018 Build Conditions Evening Peak Period

	1	†	-	-		1	-	-	-	*	+	*
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
ane Configurations	000	4	000	000	000,	0007	F-000	45	000,	0007	000	000
deal Flow (vpnpi)	1300	11	12	12	120	12	12	12	12	1300	12	12
Total Lost time (e)		4.0			!		4	40				1
ane Util. Factor		0.95					1.00	1.00				
-rpb. ped/bikes		0.98					1.00	0.99				
Hpb, ped/bikes		1.00					1.00	1.00				
F		0.95					1.00	0.92				
It Protected		1.00					0.95	1.00				
Satd. Flow (prot)		2832					1562	1452				
It Permitted		1.00					0.95	1.00				
Satd. Flow (perm)		2832					1562	1452				
Volume (vph)	63	394	219	0	0	0	292	168	186	0	0	0
Peak-hour factor, PHF	0.94	0.94	0.94	0.92	0.92	0.92	0.94	0.94	0.94	0.92	0.92	0.92
Adj. Flow (vph)	67	419	233	0	0	0	311	179	198	0	0	0
RTOR Reduction (vph)	0	55	0	0	0	0	0	0	0	0	0	0
.ane Group Flow (vph)	0	664	0	0	0	0	311	377	0	0	0	0
Confl. Bikes (#/hr)			45		4				12			
Heavy Vehicles (%)	3%	4%	1%	%0	%0	%0	4%	1%	13%	%0	%0	%0
fum Type	Perm						Split					
Protected Phases		-					m	e				
Permitted Phases	-	Ì						T				
Actuated Green, G(s)		34.6					26.0	26.0				
Effective Green, g (s)		36.6					27.0	27.0				
Actuated g/C Ratio		0.41					0.30	0.30				
Clearance Time (s)		6.0					5.0	2.0				
Vehicle Extension (s)		2.0					2.0	2.0				
ane Grp Cap (vph)		1152					469	436	l.			ĺ
//s Ratio Prot							0.20	c0.26				
//s Ratio Perm		0.23										
//c Ratio		0.58					99.0	0.86				
Jniform Delay, d1		20.7					27.5	29.8				
Progression Factor		1.00					1.00	1.00				
ncremental Delay, d2		2.1					2.7	15.7				
Delay (s)		22.8					30.3	45.5				
evel of Service		O					O	٥				
Approach Delay (s)		22.8			0.0			38.6			0.0	
Approach LOS		O			4			٥			4	
ntersection Summary												
HCM Average Control Delay	Delay		30.5	I	ICM Lev	HCM Level of Service	ervice		O			
HCM Volume to Capacity ratio Actuated Cycle Length (s)	ity ratio		90.0	(C)	um of lo	Sum of lost time (s)	(8)		26.4			
Intersection Capacity Utilization	tilization		51.1%	_	ULeve	ICU Level of Service	Nice Nice		<			
() (

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HCM Unsignalized Intersection Capacity Analysis 11: Belvidere Street & Clearway Street

2018 Build Conditions Evening Peak Period

ICU Level of Service 39 0.92 42 122 3.3 95 912 122 None 3.5 583 0.27 44 Free 0% 623 0.92 480 WB 2 0.92 100 1333 0.00 1.3 32.0% 15 245 245 0.92 82 0 1700 0.05 0.0 Average Delay Intersection Capacity Utilization Analysis Period (min) 163 0.00 0.00 0.00 EB 1 EBT Free 0% 225 0.92 245 Direction, Lane # E Volume Total Volume Total Volume Right CSH Volume to Capacity Queue Length 95th (ft) Control Delay (s) Lane LOS Approach Delay (s) Lane Width (ft)
Walking Speed (ft's)
Walking Speed (ft's)
Percent Blockage
Right turn flare (veh)
Median type
Median type
Median storage veh)
Upstream signal (ft)
pX, platoon unblocked
vC, conflicting volume
vC, stage I conf vol
vCz, stage 2 conf vol
vCu, unblocked vol Volume (veh/h)
Peak Hour Factor
Hourly flow rate (vph)
Pedestrians Intersection Summary Movement
Lane Configurations
Sign Control
Grade tC, single (s)
tC, 2 stage (s)
tF (s)
p0 queue free %
cM capacity (veh/h) Approach LOS

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Appendix C

Air Quality Appendix

AIR QUALITY APPENDIX

Introduction

This Air Quality Appendix provides modeling assumptions and backup for results presented in Section 4.5 of the report. Included within this documentation is a brief description of the methodology employed along with pertinent calculations and data used in the emissions and dispersion calculations supporting the microscale air quality analysis.

Motor Vehicle Emissions

The EPA MOBILE6.2 computer program generated motor vehicle emissions used in the garage stationary source analysis along with the mobile source CAL3QHC modeling and mesoscale analysis. The model input parameters were provided by MassDEP. Emission rates were derived for 2013 and 2018 for speed limits of 2.5, 10, 15, and 30 mph for use in the microscale analyses. The 10 mph rate was used to estimate parking garage emissions.

CAL3QHC

For the intersections studied, the CAL3QHC model was applied to calculate CO concentrations at sensitive receptor locations using emission rates derived in MOBILE6.2. The intersection's queue links and free flow links were input to the model along with sensitive receptors at all locations nearby each intersection. The meteorological assumptions input into the model were a 1.0 meter per second wind speed, Pasquill-Gifford Class D stability combined with a mixing height of 1000 meters. For each direction, the full range of wind directions at 10 degree intervals was examined. In addition, a surface roughness (z₀) of 175 cm was used for all intersections. Idle emission rates for queue links were based on 2.5 mph emission rates derived in MOBILE6.2 and converted from grams per mile to grams per hour. Emission rates for speeds of 10, 15, and 30 mph were used for right turn, left turn, and free flow links, respectively.

Belvedere Dalton - Christian Science Center - Boston, MA Calculation of Microscale Modeling Emission Factors Summary of MOBILE6 Output

Carbon Monoxide Only

Winter	2013	2018	
Left Turns		15 mph	
Right Turns		10 mph	
Free Flow		30 mph	
Queues		ldle	

Winter	2013	2018	Units
ldle	46.840	42.335	g/hr
2.5 mph	18.736	16.934	g/mile
10 mph	10.195	9.284	g/mile
15 mph	9.193	8.380	g/mile
30 mph	8.237	7.521	g/mile

Note: Winter CO emission factors are higher than Summer and are conservatively used

Model Input/Output Files

Due to excessive size CAL3QHC, and MOBILE6.2 input and output files are available on digital media upon request.

Appendix D

LEED Checklists

0 5 1 Susta	ect Checklist ainable Sites Possible Point	ts: 26	Materials and Resources, Continued	
/ N ?			Y N ?	
Prereq 1	,		3	to 2
Credit 1	Site Selection	1	ů – v – v – v – v – v – v – v – v – v –	to 2
Credit 2	, , ,	5	1 Credit 6 Rapidly Renewable Materials 1	
1 Credit 3		1	Credit 7 Certified Wood 1	
Credit 4.		6 5 1	13 2 Indoor Environmental Quality Possible Points: 1	15
3 Credit 4.:			13 2 Indoor Environmental Quality Possible Points.	S
Credit 4.		2	Y Prereq 1 Minimum Indoor Air Quality Performance	
1 Credit 5.		1	Y Prereg 2 Environmental Tobacco Smoke (ETS) Control	
1 Credit 5.	•	1	1 Credit 1 Outdoor Air Delivery Monitoring	
Credit 6.		1	1 Credit 2 Increased Ventilation 1	
Credit 6	3	1	1 Credit 3.1 Construction IAQ Management Plan—During Construction 1	
Credit 7.	3	1	Credit 3.2 Construction IAQ Management Plan—Before Occupancy	
Credit 7.	2 Heat Island Effect—Roof	1	1 Credit 4.1 Low-Emitting Materials—Adhesives and Sealants 1	
Credit 8	Light Pollution Reduction	1	1 Credit 4.2 Low-Emitting Materials—Paints and Coatings 1	
			1 Credit 4.3 Low-Emitting Materials—Flooring Systems 1	
2 2 Wate	er Efficiency Possible Point	ts: 10	1 Credit 4.4 Low-Emitting Materials—Composite Wood and Agrifiber Products 1	
_			1 Credit 5 Indoor Chemical and Pollutant Source Control 1	
Prereq 1	Water Use Reduction—20% Reduction		1 Credit 6.1 Controllability of Systems—Lighting	
Credit 1	Water Efficient Landscaping	2 to 4		
Credit 2	g	2	1 Credit 7.1 Thermal Comfort—Design	
2 Credit 3	Water Use Reduction	2 to 4		
las s Enor	au and Atmacahara Descible Deini	to. 25	1 Credit 8.1 Daylight and Views—Daylight 1 Credit 8.1 Daylight and Views—Views	
ol 12 2 Ellerí	gy and Atmosphere Possible Point	ts: 35	Credit 8.2 Daylight and Views—Views 1	
Prereq 1 Prereq 2	3 3 3, 3		2 4 Innovation and Design Process Possible Points: 6)
Prereq 2	33		5 1 5 6 2011	
Prereq 3	3 3	4 1 40	1 Credit 1.1 Exemplary Performance SSc4.1 1	
6 5 Credit 1	1 03	1 to 19		
7 Credit 2	3,	1 to 7 2	7 1 1 Credit 1.3 Pilot Credit 14: Walkable Streets 1 1 Credit 1.4 Pilot Credit 48: Discovery—Analysis to Support Integrative Process 1	
Credit 3		2	1 credit 1.4 Pilot Credit 48: Discovery—Analysis to support integrative Process 1 Credit 1.5 Pilot Credit 49: Implementing Strategies—Analysis to Support Integrat 1	
Credit 4	5	3	1 credit 2 LEED Accredited Professional	
Cradit 5		3 2	ocult 2 LEED hoof cultod 11010331011d1	
	Green Power	_	3 1 Regional Priority Credits Possible Points: 4	ļ
2 Credit 6				
2 Credit 6	rials and Resources Possible Point	ts: 14	00445 D. J. J. D. J. J. C. C. C. J. C. J. D. J.	
2 Credit 6	rials and Resources Possible Point	ts: 14	1 Credit 1.1 02115 Regional Priority: SSc3, Brownfield Redevelopment 1	
2 Credit 6 7 2 Mate	rials and Resources Possible Point Storage and Collection of Recyclables		1 Credit 1.2 02115 Regional Priority: SSc7.1, Stormwater Design, Quantity Control 1	
2 Credit 6 7 2 Mater Prereq 1 3 Credit 1.	rials and Resources Possible Point Storage and Collection of Recyclables Building Reuse—Maintain Existing Walls, Floors, and Roof	1 to 3	1 Credit 1.2 O2115 Regional Priority: SSc7.1, Stormwater Design, Quantity Control 1 3 1 Credit 1.3 O2115 Regional Priority: SSc7.1, Heat Island Effect—Non-Roof 1	
7 2 Mater Prereq 1 3 Credit 1. Credit 1.	rials and Resources Possible Point Storage and Collection of Recyclables Building Reuse—Maintain Existing Walls, Floors, and Roof Building Reuse—Maintain 50% of Interior Non-Structural Elements	1 to 3	1 Credit 1.2 O2115 Regional Priority: SSc7.1, Stormwater Design, Quantity Control 1 1 Credit 1.3 O2115 Regional Priority: SSc7.1, Heat Island Effect—Non-Roof 1 1 Credit 1.4 O2115 Regional Priority: SSc7.2, Heat Island Effect—Roof 1	
2 Credit 6 7 2 Mater Prereq 1 3 Credit 1.	rials and Resources Storage and Collection of Recyclables Building Reuse—Maintain Existing Walls, Floors, and Roof Building Reuse—Maintain 50% of Interior Non-Structural Elements Construction Waste Management	1 to 3	1 Credit 1.2 02115 Regional Priority: SSc7.1, Stormwater Design, Quantity Control 1 1 Credit 1.3 02115 Regional Priority: SSc7.1, Heat Island Effect—Non-Roof 1 1 Credit 1.4 02115 Regional Priority: SSc7.2, Heat Island Effect—Roof 1	

N ?	inable Sites Possible	Points: 26	Materials and Resources, Continued Y N ?	
Prereq 1	Construction Activity Pollution Prevention		1 1 Credit 4 Recycled Content	1 t
Credit 1	Site Selection	1	1 1 Credit 5 Regional Materials	1 t
Credit 2	Development Density and Community Connectivity	5	1 Credit 6 Rapidly Renewable Materials	1
Credit 3	Brownfield Redevelopment	1	Credit 7 Certified Wood	1
	Alternative Transportation—Public Transportation Access		to large English and Coultry	
	2 Alternative Transportation—Bicycle Storage and Changing		12 3 Indoor Environmental Quality Possible Poin	ts: 15
	Alternative Transportation—Low-Emitting and Fuel-Efficient		Minimum Indoor Air Quality Denfarmance	
Credit 4.4		2	Y Prereq 1 Minimum Indoor Air Quality Performance	
Credit 5.1	· · · · · · · · · · · · · · · · · · ·	1	Y Prereq 2 Environmental Tobacco Smoke (ETS) Control	
	2 Site Development—Maximize Open Space	1	1 Oredit 1 Outdoor Air Delivery Monitoring	1
_	Stormwater Design—Quantity Control	1	1 Credit 2 Increased Ventilation	1
	2 Stormwater Design—Quality Control	1	1 Credit 3.1 Construction IAQ Management Plan—During Construction	1
	Heat Island Effect—Non-roof	1	1 Credit 3.2 Construction IAQ Management Plan—Before Occupancy	1
	Heat Island Effect—Roof	1	1 Credit 4.1 Low-Emitting Materials—Adhesives and Sealants	1
Credit 8	Light Pollution Reduction	I	1 Credit 4.2 Low-Emitting Materials—Paints and Coatings	1
2 Moto	r Efficiency Descible	Doints: 10	1 Credit 4.3 Low-Emitting Materials—Flooring Systems 1 Credit 4.4 Low-Emitting Materials—Composite Wood and Agrifiber Products	. 1
2 Wate	r Efficiency Possible	Points: 10	3) I
Prereg 1	Water Use Reduction—20% Reduction			1
Credit 1		2 to 4	1 Credit 6.1 Controllability of Systems—Lighting 1 Credit 6.2 Controllability of Systems—Thermal Comfort	1
Credit 1	Water Efficient Landscaping Innovative Wastewater Technologies	2 10 4	1 Credit 7.1 Thermal Comfort—Design	1
2 Credit 3	Water Use Reduction	2 to 4	1 Credit 7.2 Thermal Comfort—Verification	1
Z Credit 3	water ose reduction	2 10 4	1 Credit 8.1 Daylight and Views—Daylight	1
10 Energ	y and Atmosphere Possible	Points: 35	1 Credit 8.2 Daylight and Views—Views	1
Prereq 1	Fundamental Commissioning of Building Energy Systems		2 4 Innovation and Design Process Possible Poin	tc· 6
Prereq 2	Minimum Energy Performance		2 4 minovation and besign 1 rocess	ts. U
Prereq 3	Fundamental Refrigerant Management		1 Credit 1.1 Exemplary Performance SSc4.1	1
	Optimize Energy Performance	1 to 19	1 Credit 1.2 Exemplary Performance MRc5	1
	On-Site Renewable Energy	1 to 7	1 Credit 1.3 Pilot Credit 14: Walkable Streets	1
			1 Credit 1.4 Pilot Credit 48: Discovery—Analysis to Support Integrative Proce	ss 1
Credit 2	Enhanced Commissioning	2		
	Enhanced Commissioning Enhanced Refrigerant Management	2 2	1 Credit 1.5 Pilot Credit 49: Implementing Strategies—Analysis to Support In	
Credit 2 Credit 3 Credit 4	Enhanced Refrigerant Management	2	1 Credit 1.5 Pilot Credit 49: Implementing Strategies—Analysis to Support In	1
Credit 2 Credit 3 Credit 4 Credit 5	Enhanced Refrigerant Management Measurement and Verification	2 3	1 Credit 1.5 Pilot Credit 49: Implementing Strategies—Analysis to Support In Credit 2 LEED Accredited Professional	
Credit 2 Credit 3 Credit 4 Credit 5	Enhanced Refrigerant Management	2	1 Credit 2 LEED Accredited Professional	1
Credit 2 Credit 3 Credit 4 Credit 5 Credit 6	Enhanced Refrigerant Management Measurement and Verification Green Power	2 3 2		1
Credit 3 Credit 4 Credit 5 Credit 6	Enhanced Refrigerant Management Measurement and Verification Green Power	2 3 2	1 Credit 2 LEED Accredited Professional	1
Credit 2 Credit 3 Credit 4 Credit 5 Credit 6	Enhanced Refrigerant Management Measurement and Verification Green Power	2 3 2	1	1 nts: 4
Credit 2 Credit 3 Credit 4 Credit 5 Credit 6	Enhanced Refrigerant Management Measurement and Verification Green Power Tials and Resources Storage and Collection of Recyclables	2 3 2 e Points: 14	1 Credit 2 LEED Accredited Professional 3 1 Regional Priority Credits Possible Poir 1 Credit 1.1 02115 Regional Priority: SSc3, Brownfield Redevelopment	1 nts: 4
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Credit 2 Credit 3 Credit 4 Credit 5 Credit 6 2 Mater Prereq 1 Credit 1.1	Enhanced Refrigerant Management Measurement and Verification Green Power Possible Storage and Collection of Recyclables Building Reuse—Maintain Existing Walls, Floors, and Roof	2 3 2 Points: 14	1 Regional Priority Credits Possible Poir 1 Credit 1.1 02115 Regional Priority: SSc3, Brownfield Redevelopment Credit 1.2 02115 Regional Priority: SSc7.1, Stormwater Design, Quantity Cordit 1.3 02115 Regional Priority: SSc7.1, Heat Island Effect—Non-Roof	1 nts: 4 ntrol 1 1

Appendix E

Climate Change Preparedness Questionnaire

APPENDIX E CLIMATE CHANGE PREPAREDNESS QUESTIONNAIRE

In conformance with Mayor Menino's 2011 Climate Action Leadership Committee's recommendations, the Proponent has preliminarily completed a Climate Change Preparedness Questionnaire for both the High-rise and Mid-rise buildings. Given the preliminary level of design, the responses are also preliminary and may be changed as the Project design advances.

Climate Change Preparedness Questionnaire – High-rise Building

Boston Climate Change Preparedness Questionnaire

1. Project Type

1. Is this project a:

Single building

2. At what phase is this project?

PNF Submitted

2. Phased, multi-building project

Project Identification

3. Single building project

3. Project Identification:

Project Name : Belvidere/ Dalton Project High-rise Primary Project Address : Dalton Street, Boston, MA

4. Master Plan

Project Identification

5. Institutional Master Plan

Project Identification

6. Project Information

4. Project Contact:

Name: David Hewett Title: Associate

Company: Epsilon Associates, Inc.

Email Address: dhewett@epsilonassociates.com

Phone Number: (978) 461-6215

Email Address to send completed question naire:

5. Team Description:

Owner / Developer : CL BD LLC do Carpenter and Company Inc Architect : Cambridge Seven Associates/ Pei Cobb Freed & Partners

Engineer (building systems): WSP

Sustainability / LEED: Cambridge Seven Associates

Permitting: Epsilon Associates, Inc.

Construction Management: Tishman Construction Climate Change Expert: Epsilon Associates, Inc.

7. Building Classification and Description

6. Building Uses - check all appropriate uses:

Assembly

Residential - Multi-unit, Four plus

7. Building First Floor Uses - list all:

Restaurant, hotel lobby, residential lobby

8. Construction Type - select most appropriate type:

Concrete Frame

9. Building Size: do not include commas

Site Area (Square Feet) : 28,544 Building Area (Square Feet) : 712,500

Building Height (Feet): 691 Number of Stories (Floors): 56

First Floor Elevation (Feet above sea level): 18 ft

Number of below grade levels: 2

8. Green Building

10. Which LEED Rating System(s) has or will your project use (by area for projects using multiple rating systems):

	Rating System
Primary Use	LEED 2009 for New Construction
Secondary Use	
Additional Uses	

11. What are the projected LEED Rating System Outcome(s):

	Rating System
Primary Use	Gold
Secondary Use	
Additional Uses	

12. Is or will the Project Register with the US Green Building Council

No

13. Is or will the Project Seek US Green Building Council Certification:

No

9. Higher Temperatures and Heat Waves - Analysis and General Strategies

14. Analysis Sources:

List Climate Change information sources: http://www.dimatechoices.org/ne/

15. What time span of Climate Change was considered:

None

16. Analysis Conditions:

What Low Temperature will be used for project planning (degrees): 0 What High Temperature will be used for project planning (degrees): 100

17. What Extreme Heat Event characteristics will be used for project planning:

Peak High (degrees): 100

Duration (days): 4

Number of events per year: 2

18. What measures will the project employ to reduce urban heat-island effect:

Shade trees

High reflective roof materials

Vegetated roof materials

Other: Grass

19. Will the project be able to manage hotter and more humid summers without increasing its electrical load; if so how?

No

20. Will the building remain operable without utility power for an extended period; if so for how long and by what strategies?

If Yes, for how long (days) and describe strategies: 1 day using an emergency power generator

10. High Temperatures and Heat Waves - Active and Passive Strategies

21. What will be the overall energy performance of the project or building (percentage above code)

20%

22. How will project energy performance be determined

Whole Building Energy Model

23. What specific measures will the project employ to reduce building energy consumption

High performance lighting

Automatic lighting controls

EnergyStar equipment / appliances

High performance HVAC equipment

Energy recovery ventilation

Describe any added measures: Variable frequency drives/ High efficiency domestic water heating equipment

24. What specific measures will the project employ to reduce building energy demands on the utilities and infrastructure

None

25. Will the project employ Smart Grid Infrastructure and I or Systems

No

26. Describe any non-mechanical strategies that will support building functionality and use during an extended interruption(s) of utility services and infrastructure

Operable windows (including emergency only)

Natural ventilation

Potable water storage for drinking / food preparation

Potable water for sinks / sanitary systems

High performance building envelop

27. List the R values for building envelope elements:

Roof: 21 Walls: 27

Floors / Slab : 18

Foundation / Basement: 16

Windows: 2.6 Doors: 3.6

11. Sea-Level Rise and Storms – location analysis and description

28. Location Description:

Site Elevation - low point (feet above sea level) : 16 Site Elevation - high point (feet above sea level) : 18

29. Location Classification - is the site or building located in any of the following:

	Yes	No
Coastal Zone		Ø
Velocity Zone		Ø
Flood Zone		Ø
Area Prone to Flooding		0

30. Are updates in the floodplain delineation due to climate change likely to change the classification of the site or building location:

No

31. What is the project or building proximity to nearest Coastal, Velocity or Flood Zone or Area Prone to Flooding (horizontal distance in feet)

1,700 feet

12. Sea-Level Rise and Storms – analysis and general strategies

Analysis Sources:

What time span of Climate Change and Rising Sea-Levels was considered:

How were impacts from higher sea levels and more frequent and extreme storm events analyzed:

13. Sea-Level Rise and Storms - Building Flood Proofing

Will the building remain occupiable without utility power during a period of extended inundation:

Will the proposed ground floor be raised in response to Sea Level Rise:

Will the proposed ground floor be raised in response to Sea Level Rise:

Will lower building levels be constructed in a manner to prevent water penetration:

Describe measures and strategies intended to ensure the integrity of critical building systems during a flood or severe storm event:

Were the differing effects of fresh water and salt water flooding considered:

Will the project site and building(s) be accessible during periods of inundation or limited circulation and *l* or access to transportation:

Describe any additional Building Floor Proofing strategies?

14. Sea-Level Rise and Storms - Building Resiliency and Adaptability

Will the building be able to withstand severe storm impacts and endure temporary inundation

Will the building include additional structural capacity and or building systems to accommodate future on-site renewable and or clean energy sources; if so what:

Can the site and building be reasonably modified to increase Building Flood Proofing; if so how:

Describe any additional Building Resiliency and Adaptability strategies:

Climate Change Preparedness Questionnaire – Mid-rise Building

Boston Climate Change Preparedness Questionnaire

1. Project Type

1. Is this project a:

Single building

2. At what phase is this project?

PNF Submitted

2. Phased, multi-building project

Project Identification

3. Single building project

3. Project Identification:

Project Name : Belvidere/ Dalton Project Mid-rise Primary Project Address : Belvidere Street, Boston, MA

4. Master Plan

Project Identification

5. Institutional Master Plan

Project Identification

6. Project Information

4. Project Contact:

Name: David Hewett Title: Associate

Company: Epsilon Associates, Inc.

Email Address: dhewett@epsilonassociates.com

Phone Number: (978) 461-6215

Email Address to send completed question naire:

5. Team Description:

Owner / Developer : PRG BD Investors LCC do Pritzker Realty Group Architect : Cambridge Seven Associates/ Pei Cobb Freed & Partners

Engineer (building systems): WSP

Sustainability / LEED: Cambridge Seven Associates

Permitting: Epsilon Associates, Inc. Construction Management: TBD

Climate Change Expert: Epsilon Associates, Inc.

7. Building Classification and Description

6. Building Uses - check all appropriate uses:

Retail

Residential - Multi-unit, Four plus

7. Building First Floor Uses - list all:

Retail, Lobby

8. Construction Type - select most appropriate type:

Steel Frame

Concrete Frame

9. Building Size: do not include commas

Site Area (Square Feet) : 12,376 Building Area (Square Feet) : 237,500

Building Height (Feet): 285 Number of Stories (Floors): 25

First Floor Elevation (Feet above sea level): 17

Number of below grade levels: 1

8. Green Building

10. Which LEED Rating System(s) has or will your project use (by area for projects using multiple rating systems):

	Rating System
Primary Use	LEED 2009 for New Construction
Secondary Use	
Additional Uses	

11. What are the projected LEED Rating System Outcome(s):

	Rating System
Primary Use	Silver
Secondary Use	
Additional Uses	

12. Is or will the Project Register with the US Green Building Council

No

13. Is or will the Project Seek US Green Building Council Certification:

No

9. Higher Temperatures and Heat Waves - Analysis and General Strategies

14. Analysis Sources:

List Climate Change information sources: http://www.climatechoices.org/ne/

Was there information you were unable to find: no

15. What time span of Climate Change was considered:

None

16. Analysis Conditions:

What Low Temperature will be used for project planning (degrees): 0 What High Temperature will be used for project planning (degrees): 100

17. What Extreme Heat Event characteristics will be used for project planning:

Peak High (degrees): 100

Duration (days): 4

Number of events per year: 2

18. What measures will the project employ to reduce urban heat-island effect:

Shade trees

High reflective roof materials

Vegetated roof materials

19. Will the project be able to manage hotter and more humid summers without increasing its electrical load; if so how?

Nο

20. Will the building remain operable without utility power for an extended period; if so for how long and by what strategies?

If Yes, for how long (days) and describe strategies: 1 day using an emergency power generator

10. High Temperatures and Heat Waves - Active and Passive Strategies

21. What will be the overall energy performance of the project or building (percentage above code)

20%

22. How will project energy performance be determined

Whole Building Energy Model

23. What specific measures will the project employ to reduce building energy consumption

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Automatic lighting controls

EnergyStar equipment / appliances

High performance HVAC equipment

Energy recovery ventilation

Describe any added measures: Variable frequency drives/ High efficiency domestic water heating equipment

24. What specific measures will the project employ to reduce building energy demands on the utilities and infrastructure

None

25. Will the project employ Smart Grid Infrastructure and / or Systems

26. Describe any non-mechanical strategies that will support building functionality and use during an extended interruption(s) of utility services and infrastructure

Operable windows (including emergency only)

Natural ventilation

Potable water storage for drinking / food preparation

High performance building envelop

27. List the R values for building envelope elements:

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11. Sea-Level Rise and Storms – location analysis and description

28. Location Description:

Site Elevation - low point (feet above sea level) : 16 Site Elevation - high point (feet above sea level) : 18

29. Location Classification - is the site or building located in any of the following:

	Yes	No
Coastal Zone		Ø
Velocity Zone		Ø
Flood Zone		Ø
Area Prone to Flooding		Ø

30. Are updates in the floodplain delineation due to climate change likely to change the classification of the site or building location:

No

31. What is the project or building proximity to nearest Coastal, Velocity or Flood Zone or Area Prone to Flooding (horizontal distance in feet)

1,700 feet

12. Sea-Level Rise and Storms – analysis and general strategies

Analysis Sources:

What time span of Climate Change and Rising Sea-Levels was considered:

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Describe measures and strategies intended to ensure the integrity of critical building systems during a flood or severe storm event:

Were the differing effects of fresh water and salt water flooding considered:

Will the project site and building(s) be accessible during periods of inundation or limited circulation and *l* or access to transportation:

Describe any additional Building Floor Proofing strategies?

14. Sea-Level Rise and Storms - Building Resiliency and Adaptability

Will the building be able to withstand severe storm impacts and endure temporary inundation

Will the building include additional structural capacity and or building systems to accommodate future on-site renewable and or clean energy sources; if so what:

Can the site and building be reasonably modified to increase Building Flood Proofing; if so how:

Describe any additional Building Resiliency and Adaptability strategies: