PROJECT NOTIFICATION FORM

1120-1132 Washington Street



Submitted to: Boston Planning and Development Agency One City Hall Square Boston, MA 02201

Submitted by: City Point Center LLC 1 Gateway Center, Suite #613 Newton, MA 02458 Prepared by: Epsilon Associates, Inc. 3 Mill & Main Place, Suite 250 Maynard, MA 01754

In Association with: RCA, LLC R. Jon Henson Landscape Architects Rudolph Friedmann LLP Howard Stein Hudson New Ecology, Inc.

August 25, 2017



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Table of Contents

Table of Contents

1.0	GENERAL INFORMATION			1-1
	1.1	Introduction		
	1.2	Development Team		
	1.3	Public B	lenefits	1-3
	1.4	Legal Inf	formation	1-4
		1.4.1	Legal Judgments Adverse to the Proposed Project	1-4
		1.4.2	History of Tax Arrears on Property Owned in Boston by the P	roponent1-4
		1.4.3	Site Control/ Public Easements	1-4
	1.5	Public P	Participation	1-4
2.0	PROJ	ECT DESC	RIPTION	2-1
	2.1	Project [Description	2-1
		2.1.1	Project Site	2-1
		2.1.2	Area Context	2-1
		2.1.3	Proposed Project	2-1
	2.2	City of Boston Zoning		2-10
	2.3	Anticipated Permits and Approvals		2-10
	2.4	Schedule	e	2-11
3.0	TRAN	NSPORTAT	ION	3-1
	3.1	Introduc	tion	3-1
		3.1.1	Project Description	3-1
		3.1.2	Study Methodology	3-1
		3.1.3	Study Area	3-2
	3.2	Existing	(2017) Condition	3-2
		3.2.1	Existing Roadway Conditions	3-2
		3.2.2	Existing Intersection Conditions	3-4
		3.2.3	Existing Parking and Curb Use	3-5
		3.2.4	Car and Bicycle Sharing Services	3-5
		3.2.5	Existing Bicycle Conditions	3-7
		3.2.6	Existing Pedestrian Conditions	3-7
		3.2.7	Existing Public Transportation	3-9
		3.2.8	Existing Traffic Conditions	3-9
			3.2.8.1 Turning Movement Counts	3-9
			3.2.8.2 Seasonal Adjustment	3-12
		3.2.9	Traffic Operations Analysis	3-12
		3.2.10	Existing (2017) Condition Traffic Operations Analysis	3-15

Table of Contents (Continued)

	3.3	No-Buil	d (2024) Condition	3-18
		3.3.1	Background Traffic Growth	3-18
		3.3.2	Specific Development Traffic Growth	3-18
		3.3.3	Proposed Infrastructure Improvements and Planning Initiatives	3-20
		3.3.4	No-Build (2024) Condition Traffic Volumes	3-20
		3.3.5	No-Build (2024) Condition Traffic Operations Analysis	3-20
	3.4	Build (2	024) Condition	3-25
		3.4.1	Site Access and Vehicle Circulation	3-25
		3.4.2	Parking	3-25
		3.4.3	Loading and Service Accommodations	3-25
		3.4.4	Bicycle Accommodations	3-27
		3.4.5	Trip Generation Methodology	3-27
		3.4.6	Mode Share	3-28
		3.4.7	Project Trip Generation	3-28
		3.4.8	Trip Distribution	3-29
		3.4.9	Build (2024) Traffic Volumes	3-29
		3.4.10	Build (2024) Condition Traffic Operations Analysis	3-35
	3.5	Transportation Demand Management		3-37
	3.6	Transpo	ortation Mitigation Measures	3-38
	3.7	Evaluati	on of Short-term Construction Impacts	3-39
4.0	ENVI	RONMEN	TAL PROTECTION COMPONENT	4-1
	4.1	Wind		4-1
	4.2	Shadow	/ Impacts	4-1
	4.3	Davligh	Analysis	
		4.3.1	Introduction	4-1
		4.3.2	Methodology	4-2
		4.3.3	Results	4-2
		4.3.4	Conclusions	4-4
	4.4	Solar Glare		4-7
	4.5	Air Qua	llity Analysis	4-7
		4.5.1	Introduction	4-7
		4.5.2	National Ambient Air Quality Standards and Background	
			Concentrations	4-7
			4.5.2.1 National Ambient Air Quality Standards	4-7
			4.5.2.2 Background Concentrations	4-9
		4.5.3	Methodology	4-10
		-	4.5.3.1 Microscale Analysis	4-10
			4.5.3.2 Air Quality Results	4-15
			4.5.3.3 Conclusions	4-17

Table of Contents (Continued)

	4.6	Solid and	d Hazardous Waste	4-17
		4.6.1	Hazardous Waste	4-17
		4.6.2	Operation Solid and Hazardous Waste Generation	4-18
		4.6.3	Recycling	4-18
	4.7	Noise Im	apacts	4-18
	4.8	Stormwa	ter/Water Quality	4-20
	4.9	Flood Ha	azard Zones/ Wetlands	4-20
	4.10	Geotech	nical Impacts	4-20
		4.10.1	Site Conditions	4-20
		4.10.2	Groundwater	4-20
	4.11	Construc	tion Impacts	4-21
		4.11.1	Introduction	4-21
		4.11.2	Construction Methodology/Public Safety	4-21
		4.11.3	Construction Schedule	4-22
		4.11.4	Construction Staging/Access	4-22
		4.11.5	Construction Mitigation	4-22
		4.11.6	Construction Employment and Worker Transportation	4-22
		4.11.7	Construction Truck Routes and Deliveries	4-23
		4.11.8	Construction Air Quality	4-23
		4.11.9	Construction Noise	4-24
		4.11.10	Construction Waste	4-24
		4.11.11	Protection of Utilities	4-25
	4.12	Rodent C	Control	4-25
	4.13	Wildlife	Habitat	4-25
5.0	SUST	AINABLE E	DESIGN AND CLIMATE CHANGE	5-1
	5.1	Sustainat	ole Design	5-1
	5.2	Climate (Change Resilience	5-7
		5.2.1	Introduction	5-7
		5.2.2	Extreme Heat Events	5-7
		5.2.3	Rain Events	5-8
		5.2.4	Drought Conditions	5-8
	5.3	Renewab	ble Energy	5-8
6.0	URBA		١	6-1
	6.1	6.1 Architecture and Landscape Design		
	6.2	Evolutior	n of Design	6-7

Table of Contents (Continued)

7.0	HISTORIC AND ARCHAEOLOGICAL RESOURCES		7-1	
	7.1	.1 Project Site		
	7.2	Historic Resources Within the Vicinity of the Project Site		
	7.3	Archaeological Resources Within the Project Site		
	7.4	Potentia	al Impacts to Historic Resources	7-4
		7.4.1	Demolition of Existing Buildings	7-4
		7.4.2	Urban Design	7-4
		7.4.3	Visual Impacts to Historic Resources	7-4
	7.5	Consist	ency with Other Historic Reviews	7-5
		7.5.1	Boston Landmarks Commission Article 80 Review	7-5
		7.5.2	Boston Landmarks Commission Article 85 Review	7-5
		7.5.3	Massachusetts Historical Commission	7-5
8.0	INFR	ASTRUCT	URE	8-1
	8.1	Wastew	vater	8-1
		8.1.1	Existing Sanitary Sewer System	8-1
		8.1.2	Project-Generated Wastewater Generation	8-3
		8.1.3	Sanitary Sewer Connection	8-3
	8.2	Water S	System	8-4
		8.2.1	Existing Water Service	8-4
		8.2.2	Proposed Water Service	8-4
		8.2.3	Anticipated Water Consumption	8-4
		8.2.4	Water Supply Conservation and Mitigation Measures	8-4
	8.3	Storm E	Drainage System	8-6
		8.3.1	Existing Storm Drainage System	8-6
		8.3.2	Proposed Storm Drainage System	8-6
		8.3.3	Water Quality and Construction Stormwater Management	8-6
		8.3.4	City of Boston Groundwater Overlay District	8-6
	8.4	Electrical Service		8-7
	8.5	Natural	Gas	8-7
	8.6	Telecommunications Systems		8-7
	8.7	Utility I	Protection During Construction	8-7
9.0	COORDINATION WITH OTHER GOVERNMENTAL AGENCIES			9-1
	9.1	Archite	ctural Access Board Requirements	9-1
	9.2	Massac	husetts Environmental Policy Act (MEPA)	9-1
	9.3	Massachusetts Historical Commission		9-1
	9.4	Boston Civic Design Commission		9-1

List of Appendices

- Appendix A Site Survey
- Appendix B Transportation
- Appendix C Air Quality
- Appendix D Climate Change Checklist
- Appendix E Accessibility Checklist

List of Figures

Figure 2-1	Aerial Locus Map	2-2
Figure 2-2	Existing Conditions	2-3
Figure 2-3	Site Plan	2-5
Figure 2-4	Second, Third and Fourth Floor Plan	2-6
Figure 2-5	Parking Plan	2-7
Figure 2-6	Elevations	2-8
Figure 2-7	Elevations	2-9
Figure 3-1	Study Area Intersections	3-3
Figure 3-2	On-Street Parking	3-6
Figure 3-3	Existing (2017) Condition Bicycle Volumes, Weekday a.m. and p.m. Peak Hours	3-8
Figure 3-4	Existing (2017) Condition Pedestrian Volumes, Weekday a.m. and p.m.	
-	Peak Hours	3-10
Figure 3-5	Public Transportation	3-11
Figure 3-6	Existing (2017) Condition Traffic Volumes, Weekday a.m. Peak Hour	3-13
Figure 3-7	Existing (2017) Condition Traffic Volumes, Weekday p.m. Peak Hour	3-14
Figure 3-8	Area Development Projects	3-19
Figure 3-10	No-Build (2024) Condition Traffic Volumes, p.m. Peak Hour	3-22
Figure 3-11	Site Access Plan	3-26
Figure 3-12	Vehicle Trip Distribution	3-30
Figure 3-13	Project-Generated Vehicle Trip Assignment, a.m. Peak Hour	3-31
Figure 3-14	Project-Generated Vehicle Trip Assignment, p.m. Peak Hour	3-32
Figure 3-15	Build (2024) Condition Traffic Volumes, a.m. Peak Hour	3-33
Figure 3-16	Build (2024) Condition Traffic Volumes, p.m. Peak Hour	3-34
Figure 4.3-1	Viewpoint Map	4-3
Figure 4.3-2	Existing and Proposed Conditions	4-5
Figure 4.3-3	Area Context	4-6
Figure 4.5-1	Intersection of Washington Street, Morton Street, and Richmond Street	4-13
Figure 4.5-2	Intersection of Washington Street, Adams Street, and Dorchester Avenue	4-14
Figure 6-1	View facing Northeast onto Washington Street	6-2
Figure 6-2	Landscape Plan	6-3
Figure 6-3	View facing Southeast on Washington Street	6-4
Figure 6-4	View facing South toward the Project Site	6-6

List of Figures (Continued)

Figure 7-1	Historic Resources	7-3
Figure 8-1	Existing Sewer System	8-2
Figure 8-2	Existing Water System	8-5

List of Tables

Table 2-1	Project Program	2-4
Table 2-2	Anticipated Permits and Approvals	2-10
Table 3-1	Vehicle Sharing Locations	3-7
Table 3-2	Existing Public Transportation	3-9
Table 3-3	Vehicle Level of Service Criteria	3-12
Table 3-4	Existing (2017) Condition Capacity Analysis Summary, Weekday a.m. Peak Hour	3-15
Table 3-5	Existing (2017) Condition Capacity Analysis Summary, Weekday p.m. Peak Hour	3-16
Table 3-6	No-Build (2024) Condition Capacity Analysis Summary, Weekday a.m. Peak	2 7 2
Table 3-7	No-Build (2024) Condition Capacity Analysis Summary, Weekday p.m. Peak	5-25
	Hour	3-24
Table 3-8	I ravel Mode Shares	3-28
Table 3-9	Project Trip Generation	3-29
Table 3-10	Build (2024) Condition Capacity Analysis Summary, Weekday a.m. Peak Hour	3-35
Table 3-11	Build (2024) Condition Capacity Analysis Summary, Weekday p.m. Peak Hour	3-36
Table 4.3-1	Daylight Analysis Results	4-4
Table 4.5-1	National (NAAQS) and Massachusetts (MAAQS) Ambient Air Quality Standards	4-8
Table 4.5-2	Observed Ambient Air Quality Concentrations and Selected Background Levels	4-9
Table 4.5-3	Summary of Microscale Modeling Analysis (Existing 2017)	4-15
Table 4.5-4	Summary of Microscale Modeling Analysis (No-Build 2024)	4-16
Table 4.5-5	Summary of Microscale Modeling Analysis (Build 2024)	4-16
Table 4.7-1	City of Boston Zoning District Noise Standards, Maximum Allowable Sound	
	Pressure Levels	4-19
Table 7-1	Historic Resources in the Vicinity of the Project Site	7-2
Table 8-1	Estimated Existing Wastewater Flows	8-3
Table 8-2	Project Wastewater Generation	8-3

Chapter 1.0

General Information

1.0 GENERAL INFORMATION

1.1 Introduction

City Point Center, LLC (the Proponent) proposes to redevelop the approximately 48,303 square foot site located at 1120-1132 Washington Street in the Lower Mills neighborhood of Dorchester. The Project site, located on the eastern side of Washington Street south of Richmond Street, currently contains the former Molloy Funeral Home, a vacant lot behind the funeral home building, and residential buildings on each side of the funeral home. The site will be redeveloped into a four-story, approximately 67,000 square foot (sf) building with approximately 57 residential units and ground floor commercial space. The Project will include approximately 86 residential parking spaces and eight parking spaces for the commercial space.

The Project will redevelop an underutilized site with a design that will complement and respect the existing buildings surrounding the site. The ground floor commercial spaces, envisioned as professional offices and/or a locally owned and operated store, will have large aluminum glass storefront windows and doors along Washington Street to create an inviting pedestrian experience. The sidewalk along Washington Street will be improved with a combination of bollards, lighting, and street trees. In addition to the benefits to the public realm, and a design that complements the existing architecture of the area, the Project also provides new housing units, including new affordable housing, construction and permanent jobs, and improved tax revenues for the City of Boston.

This Expanded Project Notification Form (PNF) is being submitted to the Boston Redevelopment Authority (BRA) doing business as Boston Planning and Development Agency (herein, the BPDA), to initiate review of the Project under Article 80B, Large Project Review, of the Boston Zoning Code. The PNF offers a description of the Project, its minimal impacts, and its benefits to the City of Boston.

1.2 Development Team

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	Boston, MA 02108
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	Lauren Baumann
	Paul Eddows

1.3 Public Benefits

The Project will generate many public benefits for the surrounding neighborhood and the City of Boston as a whole, both during construction and on an ongoing basis upon its completion.

Smart Growth/Transit-Oriented Development

The Project is consistent with smart-growth and transit-oriented development principles. The Project site is well served by existing public transportation, including major regional rapid transit and bus lines that provide easy access to the Project site from the Greater Boston region.

Improved Pedestrian Environment

The streetscape and the pedestrian experience will be improved though the use of lighting and landscaping.

Inclusionary Affordable Housing

The Project is subject to the Mayor's Executive Order regarding inclusionary affordable housing, dated February 29, 2000, as amended, as well as the Inclusionary Development Policy (IDP). Thirteen percent (13%) of the approximately 57 dwelling units in the Project will be IDP units.

Sustainable Design/Green Building

Energy conservation and other sustainable design measures are an integral component of the proposed Project. The Project will employ energy and water efficient features for mechanical, electrical, architectural, and structural systems, assemblies, and materials, where feasible. Sustainable design elements relating to building energy management systems, lighting, recycling, conservation measures, local building materials, and clean construction vehicles will be included, to the greatest extent practicable. The Proponent is committed to building a LEED certifiable project with a target of the Silver level, incorporating sustainable design features into the Project to preserve and protect the environment.

Increased Employment

The Project will create approximately 50 construction jobs and approximately 10 permanent jobs upon stabilization.

New Property Tax

The Project will result in increased tax revenues compared to the existing condition.

1.4 Legal Information

1.4.1 Legal Judgments Adverse to the Proposed Project

There are no legal judgements adverse to the proposed Project.

1.4.2 History of Tax Arrears on Property Owned in Boston by the Proponent

There is no current or past history of tax arrears on property owned in Boston by the Proponent.

1.4.3 Site Control/ Public Easements

The Proponent acquired the site by deed dated August 4, 2014, and recorded with the Suffolk County Registry of Deeds in Book 53327, Page 44. The site is bounded by utility easements within Washington Street for sewer (sanitary and storm), water, electric, communications, and gas. In addition, there are overhead electric lines that cross the site and run into and along the side property lines of the site.

A site survey is provided in Appendix A.

1.5 Public Participation

As part of its planning efforts, the Proponent has engaged with nearby residents and representatives of numerous neighborhood groups, elected officials, and public agencies since 2014. The Proponent revised its plans for the Project as a result of several meetings, including a meeting with representatives of the BPDA and other City officials on January 26, 2015, and meetings with the Executive Board of the Dorchester Lower Mills Civic Association beginning on May 27, 2015.

The Proponent is committed to a comprehensive and effective community outreach and will continue to engage the community to ensure public input on the Project. The Proponent looks forward to working with the BPDA and city agencies, local officials, neighbors, and others as the design and review processes move forward.

Chapter 2.0

Project Description

2.0 PROJECT DESCRIPTION

2.1 Project Description

2.1.1 Project Site

The Project site comprises six contiguous parcels of land with a total of approximately 48,303 sf located on the eastern side of Washington Street south of Richmond Street (see Figure 2-1). The Project site contains the former Molloy Funeral Home, a vacant lot behind the funeral home building, and residential buildings on each side of the funeral home. To the south of the funeral home is a building containing one two-family and one three-family dwelling, and to the north of funeral home is another two-family dwelling. Existing conditions are presented in Figure 2-2.

2.1.2 Area Context

The Project site is located in the Lower Mills neighborhood at the southeastern edge of Dorchester. Immediately to the west of the site is the Mattapan neighborhood of Boston, and to the south just across the Neponset River is the town of Milton. The area surrounding the Project site contains a mix of uses, including two to three-story residential buildings, as well as some commercial uses. A Star Market is located to the south of the Project site on River Street, and there are a variety of locally owned and operated eateries along Dorchester Avenue to the east of the Project site. Within a quarter-mile from the Project site are several public open spaces, including the William G. Walsh Playground, Dorchester Park, and the Neponset River Greenway.

The Project site is located just steps away from several Massachusetts Bay Transportation Authority (MBTA) bus stops serviced by multiple bus routes, and is just over a quarter-mile from the MBTA Milton Station, providing access to the Mattapan Trolley section of the Red Line. The proximity to the bus stops, train station and a variety of basic services makes the area an ideal location for a pedestrian-oriented residential development.

2.1.3 Proposed Project

The Project, as shown in Table 2-1, includes approximately 67,000 sf anticipated to contain approximately 3,600 sf of ground floor commercial space, and approximately 57 residential units. The residential units are anticipated to be condominiums, however, they could be developed as rental units should market conditions, financing, or other factors make a condominium development unfeasible. The commercial space is envisioned to consist of two professional offices and/or a locally owned and operated store. Approximately 86 residential parking spaces will be included in a combination of at-grade and below-grade facilities, and eight at-grade parking spaces will be provided for the commercial space.









The residential units will be a variety of sizes, including one bedroom, two bedroom and three bedroom units. Secure bicycle storage for residents (one per residential unit) will be included within the building. Figures 2-3 to 2-7 present a site plan, floor plans, and elevations.

Project Element	Approximate Dimension
Residential	57 units
1-bedroom	12 units
2-bedroom	39 units
3-bedroom	6 units
Commercial	3,600 sf
Total Square Footage	67,000 sf
Parking	94 spaces
Height	40 feet

Table 2-1Project Program

The Project includes five open space components, including a private open space in the northwest corner of the site consisting of a lawn for small scale informal play, a play area for toddlers, and a patio with benches where the residents can sit in the shade of the proposed trees; perhaps while tending to their toddler on the play sculpture. The parking for the Project is divided up into a series of bays which are visually separated by building components and proposed natural features. The proposed landscaping in each area helps to provide a spatial context for the building. The proposed shrub foundation plantings provide scale transition from the vertical building walls to the horizontal ground plane. All proposed plantings will be selected to generate seasonal interest and to minimize maintenance.

The Project front is along Washington Street, and is designed to maintain a consistent streetwall with the existing surrounding buildings. The main entrances to both commercial spaces and to the residential lobby are on Washington Street. The building footprint has the longest leg of the structure pulled back along the southerly property line, adjoining the former Funeral Home parking lot to the south, and a small, off site, wooded cluster. This creates a substantial open space buffer between the building and the three adjoining residences fronting on Richmond Street to the north.

Vehicular access and egress is on Washington Street, located at the northwesterly edge of the Project site farthest from the Washington Street/River Street intersection, allowing for more favorable entry and exit to the site with minimal impacts from the intersection. Parking has been divided up into a series of smaller scaled lot areas, to the side and rear of the proposed building, leaving the front for open space streetscape amenities.





Figure 2-3 Site Plan

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Figure 2-4 Second, Third and Fourth Floor Plan





Figure 2-5 Parking Plan

10

<u>05</u> 11

76'-0"













Figure 2-7 Elevations

2.2 City of Boston Zoning

The Project site is located within the Neighborhood Shopping Subdistrict (NS) of the Dorchester Neighborhood District, Article 65 of the Boston Zoning Code. The Project also lies within a Neighborhood Design Overlay District (NDOD). The Project as presently contemplated requires a conditional use approval from the City of Boston Board of Appeal for the proposed first floor multi-family dwelling use (multi-family dwelling use on the second, third, and fourth floors is allowed) and dimensional relief to exceed the allowed maximum floor area ratio. The Project is subject to review by the Boston Landmarks Commission pursuant to the requirements of the NDOD and Article 85 (demolition delay), with the associated BPDA design review requirements of the NDOD addressed pursuant to the pending Large Project Review.

The Project's uses for Boston Zoning Code purposes will consist of a multi-family dwelling and ground-floor commercial uses, most likely local retail, restaurant, professional offices, and/or services uses, as well as accessory parking for both the residential and commercial uses.

2.3 Anticipated Permits and Approvals

Table 2-2 presents a preliminary list of permits and approvals from governmental agencies that are expected to be required for the Project, based on currently available information. It is possible that only some of these permits or actions will be required, or that additional permits or actions will be required.

Agency	Approval
Local	
Board of Appeal or Boston Zoning Commission	Zoning relief
Boston Civic Design Commission	Design Review
Boston Public Safety Commission Committee on	Parking Garage Permit and Fuel Storage License
Licenses	
Boston Employment Commission	Construction Employment Plan
Boston Fire Department	Approval of Fire Safety Equipment;
	Fuel Oil Storage Permit (if required)
Boston Inspectional Services Department	Demolition/Building Permit;
	Other construction-related permits;
	Certificates of Occupancy
Boston Landmarks Commission	Article 85 Demolition Delay Review;
	Design Review
Boston Public Works Department	Curb Cut Permit(s);
	Sidewalk Occupancy Permit (as required)
Boston Planning and Development Agency	Article 80B Large Project Review
Boston Transportation Department	Transportation Access Plan Agreement;
	Construction Management Agreement

Table 2-2Anticipated Permits and Approvals

Table 2-2 Anticipated Permits and Approvals (Continued)

Agency	Approval
Local	
Boston Water and Sewer Commission	Site Plan Review;
	Water and Sewer connection permits;
	Storm Drainage
Office of Jobs and Community Services	Permanent Employment Agreement (as required)
Public Improvement Commission	Specific Repair Plan and Sidewalk Improvements
	(as required)
State	
Department of Environmental Protection	Notification of Demolition and Construction
Massachusetts Historical Commission	Determination of No Adverse Effect on Historic
	Properties
Massachusetts Water Resources Authority	8(m) Permit
Federal	
U.S. Environmental Protection Agency	NPDES Notice of Intent for Construction (if required)

2.4 Schedule

It is anticipated that construction will commence in the first quarter of 2018. Once begun, construction is expected to last approximately 18-24 months.

Chapter 3.0

Transportation

3.0 TRANSPORTATION

3.1 Introduction

Howard Stein Hudson (HSH) has conducted an evaluation of the transportation impacts of the proposed Project. This transportation study adheres to the Boston Transportation Department (BTD) *Transportation Access Plan Guidelines* and the BPDA Article 80 Large Project Review process. This study includes an evaluation of the existing conditions, future conditions with and without the Project, projected parking demand, loading operations, transit services, and pedestrian and bicycle activity. The Project will have minimal impact on the study area intersections and the pedestrian and public transportation facilities in the area.

3.1.1 Project Description

The Project is located at 1120-1132 Washington Street in the Lower Mills neighborhood of Dorchester. The Project consists of the demolition of the existing buildings to construct a new, approximately 67,000 square foot building containing approximately 57 residential units, 3,600 sf of ground floor commercial/office space, and a total of 94 parking spaces. Approximately 43 parking spaces will be located in a surface lot and the remaining 51 spaces will be located in a below-grade garage. A total of eight parking spaces in a surface lot will be designated for the commercial uses, with the remainder for the residential uses. Access to the parking will be provided by a curb cut located along the east side of Washington Street, just south of Richmond Street. All loading, trash/recycling, service, and delivery activity will also take place on the site in the surface parking lot. The Project will include a bicycle storage room on site that will store approximately 57 bicycles.

3.1.2 Study Methodology

This transportation study and its supporting analyses were conducted in accordance with BTD guidelines, and are described below.

The Existing (2017) Condition analysis includes an inventory of the existing transportation conditions such as traffic characteristics, parking, curb usage, transit, pedestrian circulation, bicycle facilities, loading, and site conditions. Existing counts for vehicles, bicycles, and pedestrians were collected at the study area intersections. A traffic data collection effort forms the basis for the transportation analysis conducted as part of this evaluation.

The future transportation conditions analyses evaluate potential transportation impacts associated with the Project. The long-term transportation impacts are evaluated for the year 2024, based on a seven-year horizon from the year of the filing of this traffic study.

The No-Build (2024) Condition analysis includes general background traffic growth, traffic growth associated with specific developments (not including this Project), and transportation improvements that are planned in the vicinity of the Project site.

The Build (2024) Condition analysis includes a net increase in traffic volume due to the addition of Project-generated trip estimates to the traffic volumes developed as part of the No-Build (2024) Condition analysis. The transportation study identifies expected roadway, parking, transit, pedestrian, and bicycle accommodations, as well as loading capabilities and deficiencies.

The final part of the transportation study identifies measures to mitigate Project-related impacts and to address any traffic, pedestrian, bicycle, transit, safety, or construction related issues that are necessary to accommodate the Project.

An evaluation of short-term traffic impacts associated with construction activities is also provided.

3.1.3 Study Area

The transportation study area consists of intersections surrounding the Project site along Washington Street, Dorchester Avenue, Richmond Street and Adams Street. The study area includes the following four signalized intersections, also shown in Figure 3-1:

- Washington Street/River Street;
- Washington Street/Morton Street/Richmond Street;
- Dorchester Avenue/Richmond Street; and
- Dorchester Avenue/Washington Street/Adams Street.

3.2 Existing (2017) Condition

This section includes descriptions of existing study area roadway geometries, intersection geometry and traffic control, parking and curbs usage, public transportation services, peak-hour traffic volumes for vehicles, bicycles, and pedestrians, and intersection traffic operations.

3.2.1 Existing Roadway Conditions

The study area includes the following major roadways, which are categorized according to the Massachusetts Department of Transportation (MassDOT) Office of Transportation Planning functional classifications:

Washington Street is a two-way, two-lane roadway adjacent to the western edge of the Project site and runs in a north-south direction between Blue Hill Avenue to the north and Adams Street to the south. Washington Street is classified as an urban minor arterial roadway under BTD Jurisdiction. In the vicinity of the site, on-street parking is restricted on both sides of Washington Street. Sidewalks are provided on both sides of the roadway.





Dorchester Avenue is a two-way, two-lane roadway located east of the Project site. Dorchester Avenue generally runs in a north-south direction between Broadway in South Boston to the north and the Milton Town Line to the south. Dorchester Avenue is classified as an urban principal arterial roadway under BTD jurisdiction. In the vicinity of the site, twohour parking is available on both sides of the road. Sidewalks are provided on both sides of Dorchester Avenue.

Richmond Street is a two-way, two lane roadway located north of the Project site. Richmond Street generally runs in an east-west direction between Dorchester Avenue to the east and Washington Street to the west. Richmond Street is classified as a local roadway under BTD jurisdiction. In the vicinity of the site, unrestricted parking is available on the south side of the roadway only. Sidewalks are provided on both sides of Richmond Street.

Adams Street is a two-way, two-lane roadway located south of the Project site. Adams Street generally runs in a north-south direction between Gallivan Boulevard to the north and Dorchester Avenue to the south. Adams Street is classified as an urban minor arterial roadway under BTD jurisdiction. In the vicinity of the site, parking is generally prohibited on both sides of the roadway. Sidewalks are provided on both sides of Adams Street.

River Street is a two-way, two lane roadway located to south of the Project site that generally runs in an east-west direction between Washington Street to the east and Cedar Street in Dedham to the west. River Street is classified as an urban minor arterial roadway under BTD jurisdiction. In the vicinity of the site, parking is restricted along both sides of the roadway. Sidewalks are provided on both sides of the roadway.

Morton Street is a two-way, two lane roadway located north of the Project site that generally runs in an east-west direction between Washington Street to the east and Arborway to the west. Morton Street is classified as an urban minor arterial roadway under BTD jurisdiction. In the vicinity of the site, parking is provided on both sides of Morton Street. Sidewalks are provided on both sides of the roadway.

3.2.2 Existing Intersection Conditions

The existing study area intersections are described below. Intersection characteristics such as traffic control, lane usage, pedestrian facilities, pavement markings, and adjacent land use are described.

Washington Street/River Street is a four-legged, signalized intersection with four approaches. The River Street eastbound approach consists of an exclusive left-turn lane and an exclusive right-turn lane. The Washington Street northbound approach consists of an exclusive left-turn lane and a through lane. The Washington Street southbound approach consists of a through lane and an exclusive right-turn lane. A driveway that provides access to the Star

Market loading dock serves as the fourth and northbound leg of the intersection. Sidewalks are provided along all approaches. Crosswalks, wheelchair ramps, and pedestrian signal equipment are provided across all approaches to the intersection.

Washington Street/Morton Street/Richmond Street is a four-legged, signalized intersection with four approaches. The Morton Street eastbound approach consists of two undesignated travel lanes. The Richmond Street westbound approach consists of a single travel lane. The Washington Street northbound and southbound approaches each consist of a single travel lane. Sidewalks are provided along all approaches. Crosswalks, wheelchair ramps, and pedestrian signal equipment are provided across all approaches to the intersection.

Dorchester Avenue/Richmond Street is a four-legged, signalized intersection with four approaches. The Richmond Street eastbound and westbound approaches each consist of a single lane. The Richmond Street westbound approach consists of one shared left-turn/through/right-turn. The Dorchester Avenue northbound and southbound approaches also each consist of a single travel lane. Sidewalks are provided along all approaches. Crosswalks, wheelchair ramps, and pedestrian signal equipment are provided across all approaches to the intersection.

Dorchester Avenue/Washington Street/Adams Street is a four-legged, signalized intersection with four approaches. The Washington Street eastbound approach consists of one shared left-turn/through lane and one shared through/right-turn lane. The Adams Street westbound approach consists of a single lane that operates as two lanes (one left-turn lane and one shared through/right-turn lane). The Adams Street northbound approach consists of an exclusive left-turn lane, a through travel lane, and an exclusive right-turn lane. The Dorchester Avenue southbound approach consist of one shared left-turn/through lane and one shared through/right-turn lane. Sidewalks are provided along all approaches. Crosswalks, wheelchair ramps, and pedestrian signal equipment are provided across all approaches to the intersection.

3.2.3 Existing Parking and Curb Use

On-street parking surrounding the Project site generally consists of residential, metered, and commercial parking. The on-street parking regulations within the study area are shown in Figure 3-2. Parking is not provided on either side of Washington Street adjacent to the site.

3.2.4 Car and Bicycle Sharing Services

Car sharing services enable easy access to short-term vehicular transportation. Vehicles are rented on an hourly or daily basis, and all vehicle costs (gas, maintenance, insurance, and parking) are included in the rental fee. Vehicles are checked out for a specific time period and returned to their designated location. Pick-up/drop-off locations are typically in existing





parking lots or other parking areas throughout neighborhoods as a convenience to users of the services. Nearby car sharing services provide an important transportation option and reduce the need for private vehicle ownership.

One major car sharing service with vehicle locations near the Project site is Zipcar Car Share. The nearest car sharing location to the Project site is at 209 Ashmont Street north of the Project site.

Boston's major bicycle sharing service, Hubway, launched in 2011 and currently consists of more than 1,600 shared bicycles at more than 160 stations throughout Boston, Brookline, Cambridge, and Somerville. However, there are currently no Hubway stations in the immediate Project area. The car and bicycle sharing locations within more than a mile of the Project site are described in Table 3-1.

Description	Location	Distance	
Zipcar ¹			
All Saints Church	209 Ashmont Street	0.9 miles	
Mattapan Train Station	500 River Street	1.25 miles	
River Street Lot	451 River Street	1.25 miles	
Dorchester Ave/Wrentham St Lot	1859 Dorchester Avenue	1.0 miles	
Dorchester Ave/Banton St Rear Lot	1815 Dorchester Avenue	1.1 miles	

Table 3-1Vehicle Sharing Locations

1. Source: <u>www.zipcar.com</u>, March 2017.

3.2.5 Existing Bicycle Conditions

In recent years, bicycle use has increased dramatically throughout the City of Boston. Several streets in the vicinity of the Project site are designated in the City of Boston's 2013 "Bike Routes of Boston" map. Dorchester Avenue currently has bicycle lanes and is designated as a route for advanced riders. Adams Street, Washington Street, and River Street are all designated as intermediate routes. Morton Street is designated as an advanced route.

Bicycle counts were conducted concurrent with the vehicular Turning Movement Counts (TMCs) and are presented in Figure 3-3. As shown in the figure, bicycle activity in the area was generally light during the data collection period. It is expected that bicycle activity is higher during the warmer months.

3.2.6 Existing Pedestrian Conditions

Sidewalks are provided along all roadways in the study area and are generally in good condition. Crosswalks and pedestrian signal equipment are provided at all study area intersections.





Figure 3-3

To determine the amount of pedestrian activity within the study area, pedestrian counts were conducted concurrent with the TMCs at the study area intersections and are presented in Figure 3-4. The heaviest pedestrian volumes occurred at the intersection of Dorchester Avenue/Washington Street/Adams Street.

3.2.7 Existing Public Transportation

The Project site area is well-served by public transportation. The MBTA's Red Line Mattapan Trolley and several bus lines are located in proximity to the site. The closest Mattapan Trolley Station, Milton Station, is a quarter mile away. The Mattapan Trolley runs between Mattapan Station and Ashmont Station, connecting passengers to the MBTA's Red Line.

The MBTA Route 15 and Route 27 buses travel along Dorchester Avenue and River Street with bus stops located at the intersections of Washington Street/River Street and Washington Street/Adams Street/ Dorchester Avenue. The MBTA Route 217 bus travels along Dorchester Avenue with a bus stop at the intersection of Dorchester Avenue/Washington Street. The MBTA Route 240 bus travels along Dorchester Avenue, River Street, and Central Avenue with bus stops at the intersection of Dorchester Avenue, River Street.

The nearby public transit services are shown in Figure 3-5 and summarized in Table 3-2.

Transit	Description	Peak-Hour Headway	
Subway Lines			
Red Line	Mattapan Trolley –Mattapan Station- Ashmont Station	5-12	
Bus Routes			
15	Kane Square or Fields Corner Station –Ruggles Station via Uphams Corner	3-20	
27	Mattapan Station –Ashmont Station via River Street	15-35	
217	Quincy Center Station –Ashmont Station via Beale St, Wollaston, & E. Milton Square	30	
240	Avon Square or Holbrook/Randolph Commuter Rail Station –Ashmont Station via Crawford Square, Randolph	10-45	

Table 3-2Existing Public Transportation

1 Headway is the scheduled time between trains or buses. Headways are approximate. Source: www.mbta.com, March 2017.

3.2.8 Existing Traffic Conditions

3.2.8.1 Turning Movement Counts

Traffic volume data was collected at the study area intersections on March 21, 2017. Traffic Turning Movement Counts and vehicle classification counts were conducted during the weekday a.m. and weekday p.m. peak periods (7:00 – 9:00 a.m. and 4:00 – 6:00 p.m., respectively). The traffic classification counts included car, heavy vehicle, pedestrian, and bicycle movements. Detailed traffic counts are provided in Appendix B.




Figure 3-4





3.2.8.2 Seasonal Adjustment

In order to account for seasonal variation in traffic volumes throughout the year, data provided by MassDOT were reviewed. The most recent (2011) MassDOT Weekday Seasonal Factors were used to determine the need for seasonal adjustments to the March 2017 TMCs. The seasonal adjustment factor for roadways similar to the study area (Group 6) indicates that average month traffic volumes are approximately four percent less than the traffic volumes that were collected. The traffic counts were not adjusted downward to reflect average month conditions in order to provide a conservatively high analysis.

Existing traffic volumes were collected to develop the 2017 Existing Condition vehicular traffic volumes. The Existing (2017) Condition weekday a.m. peak hour and weekday p.m. peak hour traffic volumes are shown in Figure 3-6 and Figure 3-7, respectively.

3.2.9 Traffic Operations Analysis

Trafficware's Synchro (version 9) software package was used to calculate average delay and associated Level of Service (LOS) at the study area intersections. This software is based on the traffic operational analysis methodology of the Transportation Research Board's 2000 Highway Capacity Manual (HCM).

LOS designations are based on average delay per vehicle for all vehicles entering an intersection. Table 3-3 displays the intersection LOS criteria. LOS A indicates the most favorable condition, with minimum traffic delay, while LOS F represents the worst condition, with significant traffic delay. LOS D or better is typically considered acceptable in an urban area. However, LOS E or F is often typical for a stop controlled minor street that intersects a major roadway.

Level of	Average Stopped Delay (sec/veh)					
Service	Signalized Intersection	Unsignalized Intersection				
А	≤10	≤10				
В	>10 and ≤ 20	> 10 and ≤ 15				
С	>20 and ≤ 35	> 15 and ≤ 25				
D	>35 and ≤ 55	>25 and ≤ 35				
E	>55 and ≤ 80	> 35 and ≤ 50				
F	>80	> 50				

Table 3-3 Vehicle Level of Service Criteria

Source: 2000 Highway Capacity Manual, Transportation Research Board.

In addition to delay and LOS, the operational capacity and vehicular queues are calculated and used to further quantify traffic operations at intersections. The following describes these other calculated measures.









The volume-to-capacity (v/c) ratio is a measure of congestion at an intersection approach. A v/c ratio below one indicates that the intersection approach has adequate capacity to process the arriving traffic volumes over the course of an hour. A v/c ratio of one or greater indicates that the traffic volume on the intersection approach exceeds capacity.

The 50th percentile queue length, measured in feet, represents the maximum queue length during a cycle of the traffic signal with typical (or median) entering traffic volumes.

The 95th percentile queue length, measured in feet, represents the farthest extent of the vehicle queue (to the last stopped vehicle) upstream from the stop line during five percent of all signal cycles. The 95th percentile queue will not be seen during each cycle. The queue would be this long only five percent of the time and would typically not occur during off-peak hours. Since volumes fluctuate throughout the hour, the 95th percentile queue represents what can be considered a "worst case" scenario. Queues at the intersection are generally below the 95th percentile queue throughout the course of the peak hour. It is also unlikely that the 95th percentile queues for each approach to the intersection will occur simultaneously.

3.2.10 Existing (2017) Condition Traffic Operations Analysis

Table 3-4 and Table 3-5 summarize the Existing (2017) Condition capacity analysis for the study area intersection during the weekday a.m. peak hour and the weekday p.m. peak hour. The detailed analysis sheets are provided in Appendix B.

Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)
Sign	alized				
Washington Street/Morton Street/Richmond Street	D	47.6	-	-	-
Morton Street EB left/thru	D	40.9	0.27	74	170
Morton Street EB right	А	0.9	0.23	0	0
Richmond Street WB left/thru thru/right	F	>80.0	0.89	130	#246
Washington Street NB bear left	E	61.8	0.85	187	m#299
Washington Street NB thru/right	D	37.4	0.56	166	m#251
Washington Street SB bear left	D	53.5	0.40	28	68
Washington Street SB thru/right	D	42.4	0.45	117	190
Washington Street/River Street	С	24.1	-	-	-
River Street EB left	E	70.3	0.83	191	#337
River Street EB right	А	7.7	0.22	49	101
Washington Street NB left	В	10.7	0.23	43	148
Washington Street NB thru	А	2.9	0.31	4	113
Washington Street SB thru	D	52.7	0.51	123	m171
Washington Street SB right	В	15.8	0.37	25	m70

Table 3-4 Existing (2017) Condition Capacity Analysis Summary, Weekday a.m. Peak Hour

Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)
Sign	alized				
Dorchester Avenue/Washington Street/Adams Street	C	34.8	-	-	-
Washington Street EB left/thru	E	68.6	0.87	138	298
Washington Street EB right	А	8.7	0.22	10	57
Adams Street WB left	F	>80.0	0.86	102	#195
Adams Street WB thru/right	D	43.0	0.46	121	183
Adams Street NB left	D	36.0	0.67	217	#404
Adams Street NB thru	С	27.5	0.35	165	259
Adams Street NB right	А	4.2	0.40	0	65
Dorchester Avenue SB left/thru thru/right	С	32.8	0.30	67	109
Dorchester Avenue/Richmond Street	В	13.5	-	-	-
Richmond Street EB left/thru/right	С	23.7	0.54	24	#131
Richmond Street WB left/thru/right	В	14.5	0.29	10	58
Dorchester Avenue NB left/thru/right	В	11.8	0.45	44	#222
Dorchester Avenue SB left/thru/right	А	9.0	0.26	22	117

Table 3-4Existing (2017) Condition Capacity Analysis Summary, Weekday a.m. Peak Hour
(Continued)

95th percentile volume exceeds capacity.

m = Queue is metered from upstream signal.

Grey shading indicates LOS E or F.

Table 3-5Existing (2017) Condition Capacity Analysis Summary, Weekday p.m. Peak Hour

Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)
Sign	alized				
Washington Street/Morton Street/Richmond Street	D	41.9	-	-	-
Morton Street EB left/thru	С	34.8	0.22	70	162
Morton Street EB right	А	3.2	0.27	0	27
Richmond Street WB left/thru thru/right	F	>80.0	0.94	152	#290
Washington Street NB bear left	С	34.4	0.56	72	m110
Washington Street NB thru/right	С	26.4	0.39	163	162
Washington Street SB bear left	D	41.3	0.16	20	49
Washington Street SB thru/right	D	48.2	0.62	165	255
Washington Street/River Street	C	27.3	-	-	-
River Street EB left	E	72.5	0.75	121	#197
River Street EB right	A	8.9	0.23	50	102
Washington Street NB left	С	22.6	0.30	56	240

Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)
Sign	alized				
Washington Street NB thru	А	9.2	0.16	40	103
Washington Street SB thru	D	50.7	0.62	153	m163
Washington Street SB right	В	14.3	0.48	54	m22
Dorchester Avenue/Washington Street/Adams Street	D	36.9	-	-	-
Washington Street EB left/thru	E	62.2	0.83	162	250
Washington Street EB right	А	6.7	0.34	73	43
Adams Street WB left	F	>80.0	0.88	128	#217
Adams Street WB thru/right	D	48.0	0.59	153	222
Adams Street NB left	С	30.8	0.50	116	193
Adams Street NB thru	С	25.8	0.27	124	204
Adams Street NB right	А	4.6	0.21	0	49
Dorchester Avenue SB left/thru thru/right	D	38.2	0.43	151	206
Dorchester Avenue/Richmond Street	В	19.8	-	-	-
Richmond Street EB left/thru/right	С	27.6	0.56	44	92
Richmond Street WB left/thru/right	D	36.2	0.69	65	121
Dorchester Avenue NB left/thru/right	В	13.2	0.30	36	167
Dorchester Avenue SB left/thru/right	В	13.3	0.34	45	201

Table 3-5	Existing (2017)	Condition	Capacity	Analysis	Summary,	Weekday	p.m.	Peak	Hour
	(Continued)								

95th percentile volume exceeds capacity.

m = Queue is metered from upstream signal.

Grey shading indicates LOS E or F.

The signalized intersection of **Washington Street/ Morton Street/ Richmond Street** currently operates at LOS D during both the weekday a.m. and p.m. peak hour. During the a.m. and p.m. peak hour, the Richmond Street westbound approach operates at LOS F, but under capacity (v/c is less than 1.0). The Washington Street northbound approach operates at LOS E during the a.m. peak hour. The longer delays at the intersection are a result of a long cycle length (120 seconds) at the traffic signal. The longest queues at the intersection occur along the Washington Street northbound approach.

The signalized intersection of **Washington Street/ River Street** currently operates at LOS C during both the a.m. and p.m. peak hours. The River Street eastbound left lane operates at LOS E during both the a.m. and p.m. peak hours. The longest queues at the intersection occur along the River Street eastbound approach during the a.m. peak hour and along the Washington Street northbound approach during the p.m. peak hour.

The signalized intersection of **Dorchester Avenue/ Washington Street/ Adams Street** currently operates at LOS C during the a.m. peak hour and LOS D during the p.m. peak hour. The Washington Street eastbound left/thru lane operates at LOS E during both the a.m. and p.m.

peak hours. The Adams Street westbound left operates at LOS F during both the a.m. and p.m. peak hours. The longest queues at the intersection occur along the Adams Street northbound approach during the a.m. peak hour and at the Washington Street eastbound approach during the p.m. peak hour.

The signalized intersection of **Dorchester Avenue/ Richmond Street** operates under capacity with acceptable levels of service.

All movements at the study area intersections currently operate under capacity (v/c less than 1.0) during the weekday peak hours.

3.3 No-Build (2024) Condition

The No-Build (2024) Condition reflects a future scenario that incorporates anticipated traffic volume changes associated with background traffic growth independent of any specific project, traffic associated with other planned specific developments, and planned infrastructure improvements that will affect travel patterns throughout the study area. These infrastructure improvements include roadway, public transportation, pedestrian and bicycle improvements. The No-Build (2024) Condition does not include the Project-related impacts.

3.3.1 Background Traffic Growth

The methodology to account for future background traffic growth, independent of large development projects, may be affected by changes in demographics, smaller scale development projects, or projects unforeseen at this time. Based on a review of recent traffic studies conducted for nearby projects and historic traffic data, to account for any additional unforeseen traffic growth, a one percent per year annual traffic growth rate was used.

3.3.2 Specific Development Traffic Growth

Traffic volumes associated with known, larger or adjacent development projects can affect traffic patterns throughout the study area within the future analysis time horizon. The following nearby development projects were identified in the vicinity of the Project and are shown in Figure 3-8:

- Lower Mills Apartments This project is located to the east of the Project site and consists of the renovation of the existing Lower Mills Apartments at 2262 Dorchester Avenue. The renovation will update the existing building, which contains 177 residential units. This project has completed construction.
- 73 River Street This project is located to the west of the Project site and consists of the demolition of two single story structures and the construction of a new four-story retail/residential building. This project will consist of approximately 33,942 gross square feet of space.





These projects are expected to generate minimal vehicular activity. Traffic volumes related to these projects were assumed to be included in the general background growth rate.

3.3.3 Proposed Infrastructure Improvements and Planning Initiatives

A review of planned improvements to roadway, transit, bicycle, and pedestrian facilities was conducted to determine if there are any nearby improvement projects or planning initiatives in the vicinity of the study area. Based on this review, the following projects are in the vicinity of the Project:

Harborwalk – The Harborwalk project is located to the east of the Project site and consists of a continuous public walkway along the water's edge that is mostly re-established shoreline. The Harborwalk System connects the City's neighborhoods to its Harbor, linking recreational, cultural and historic attractions, as well as access to public transit, including water transportation facilities. Currently 38 miles of Harborwalk have been constructed and when completed, the walkway system will stretch over 47 miles from Dorchester to East Boston. Access to the planned extension of the Harborwalk will be provided east of the site at the Neponset Trail.

Mattapan Economic Development Initiative – This project, located to the west of the Project site, focuses on improving the business districts of Mattapan Square, Blue Hill Avenue Center and the Morton Street Village Corridor, creating job opportunities within the neighborhood, and increasing capital investment in commercial areas and properties. This project includes the creation of the "Fast Track" Rapid Rail along the Fairmont Commuter Rail line. The project may also include improving the maintenance of existing pedestrian infrastructure and upgrading the alleyway between Blue Hill Avenue northbound and River Street to provide a more direct connection between Mattapan Square and the River Street and MBTA parking lots.

3.3.4 No-Build (2024) Condition Traffic Volumes

The one percent per year annual growth rate was applied to the Existing (2017) Condition traffic volumes to develop the No-Build (2024) Condition traffic volumes. The No-Build (2024) weekday a.m. peak hour and weekday p.m. peak hour traffic volumes are shown on Figure 3-9 and Figure 3-10, respectively.

3.3.5 No-Build (2024) Condition Traffic Operations Analysis

The No-Build (2024) Condition capacity analysis uses the same methodology as the Existing (2017) Condition capacity analysis. Table 3-6 and Table 3-7 present the No-Build (2024) Condition capacity analysis for the a.m. and p.m. peak hours, respectively. The detailed analysis sheets are provided in Appendix B.









Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)
Sign	alized				
Washington Street/Morton Street/Richmond Street	D	53.4	-	-	-
Morton Street EB left/thru	D	41.2	0.29	79	180
Morton Street EB right	А	1.1	0.25	0	1
Richmond Street WB left/thru thru/right	F	>80.0	0.95	140	#267
Washington Street NB bear left	E	76.9	0.95	183	m#340
Washington Street NB thru/right	D	38.3	0.60	178	m173
Washington Street SB bear left	E	68.7	0.55	32	#87
Washington Street SB thru/right	D	43.3	0.48	127	203
Washington Street/River Street	C	24.1	-	-	-
River Street EB left	E	68.2	0.83	202	#369
River Street EB right	А	8.2	0.24	58	109
Washington Street NB left	В	11.5	0.26	46	m149
Washington Street NB thru	А	3.1	0.34	4	120
Washington Street SB thru	D	52.6	0.52	131	m181
Washington Street SB right	В	16.9	0.39	32	m77
Dorchester Avenue/Washington Street/Adams Street	D	37.0	-	-	-
Washington Street EB left/thru	E	71.6	0.90	147	#347
Washington Street EB right	А	9.5	0.23	14	66
Adams Street WB left	F	>80.0	0.90	108	#221
Adams Street WB thru/right	D	42.0	0.47	125	195
Adams Street NB left	D	41.5	0.75	249	#346
Adams Street NB thru	С	29.0	0.39	188	278
Adams Street NB right	А	4.3	0.43	0	67
Dorchester Avenue SB left/thru thru/right	С	33.9	0.34	73	117
Dorchester Avenue/Richmond Street	В	14.2	-	-	-
Richmond Street EB left/thru/right	С	24.9	0.57	26	#141
Richmond Street WB left/thru/right	В	14.7	0.31	11	61
Dorchester Avenue NB left/thru/right	В	12.8	0.49	48	#267
Dorchester Avenue SB left/thru/right	А	9.2	0.28	24	126

Table 3-6No-Build (2024) Condition Capacity Analysis Summary, Weekday a.m. Peak Hour

95th percentile volume exceeds capacity.

Grey shading indicates a decrease to LOS E or F from Existing (2017) Condition.

m = Queue is metered from upstream signal.

Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)
Sign	alized				
Washington Street/Morton Street/Richmond Street	D	52.9	-	-	-
Morton Street EB left/thru	D	35.0	0.24	76	175
Morton Street EB right	А	4.3	0.30	0	42
Richmond Street WB left/thru thru/right	F	>80.0	>1.00	~ 188	#324
Washington Street NB bear left	D	46.1	0.63	97	151
Washington Street NB thru/right	С	34.7	0.42	175	244
Washington Street SB bear left	D	41.5	0.19	22	53
Washington Street SB thru/right	D	49.0	0.66	182	277
Washington Street/River Street	С	26.8	-	-	-
River Street EB left	E	67.8	0.73	127	195
River Street EB right	В	10.0	0.25	60	103
Washington Street NB left	В	20.0	0.36	94	287
Washington Street NB thru	А	3.6	0.19	1	112
Washington Street SB thru	D	53.4	0.63	178	m231
Washington Street SB right	С	21.3	0.50	72	m104
Dorchester Avenue/Washington Street/Adams Street	D	41.1	-	-	-
Washington Street EB left/thru	E	76.9	0.86	98	#275
Washington Street EB right	В	11.4	0.33	4	96
Adams Street WB left	F	>80.0	0.92	136	#249
Adams Street WB thru/right	D	47.1	0.59	161	238
Adams Street NB left	С	31.4	0.55	130	206
Adams Street NB thru	С	27.0	0.29	138	216
Adams Street NB right	А	4.6	0.23	0	50
Dorchester Avenue SB left/thru thru/right	D	44.3	0.53	174	#256
Dorchester Avenue/Richmond Street	В	19.5	-	-	-
Richmond Street EB left/thru/right	С	25.7	0.52	21	#118
Richmond Street WB left/thru/right	С	32.6	0.65	32	#168
Dorchester Avenue NB left/thru/right	В	14.2	0.43	32	163
Dorchester Avenue SB left/thru/right	В	14.2	0.46	38	188

Table 3-7	No-Build (2024) Condition Capacity Analysis Summary, Weekday p.m. Peak Hour
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95th percentile volume exceeds capacity.

 \sim 50th percentile volume exceeds capacity. Queue may be longer. Queue shown is the maximum after two cycles.

m = Queue is metered from upstream signal.

As shown in Table 3-6 and Table 3-7, the study area intersections are expected to operate at the same LOS as Existing Conditions. At the **Washington Street/Morton Street/Richmond Street** intersection, the Washington Street southbound bear left decreases from LOS D to LOS E during the a.m. peak hour.

3.4 Build (2024) Condition

As previously summarized, the Project site is located at 1120-1132 Washington Street in the Lower Mills neighborhood of Dorchester. The Project consists of the construction of approximately 57 residential units, 3,600 sf of ground floor commercial/office space, and a total of 94 parking spaces

3.4.1 Site Access and Vehicle Circulation

Vehicular access to the site will be provided by a curb cut along the east side of Washington Street, south of Richmond Street. As part of the Project, the two curb cuts that serve the existing uses will be closed. The new curb cut will provide access to approximately 43 parking spaces in a surface lot and 51 spaces in a below-grade garage. A total of eight parking spaces in a surface lot will be designated for the commercial uses, with the remainder for the residential uses. All loading, trash/recycling, service, and delivery activity will also take place on the site in the surface parking lot. The Project will include a bicycle storage room on site that will store approximately 57 bicycles.

Primary pedestrian access to the site will be from Washington Street. The site plan is shown in Figure 3-11.

3.4.2 Parking

The parking goals developed by the BTD for this section of Dorchester are a maximum of 1.0 to 1.5 parking spaces per residential unit. The Project is proposing to construct a total of 94 parking spaces – 43 spaces in a surface lot and 51 spaces in a below-grade garage. Of the 94 parking spaces, eight spaces will be designated for commercial uses and the remaining 86 spaces will be designated for residential uses, resulting in a parking ratio of 1.5 parking spaces per residential unit.

Approximately 57 secure, covered bicycle parking spaces will also be provided as part of the Project.

3.4.3 Loading and Service Accommodations

Loading and service operations for the Project will occur on the site and will accommodate up to an SU-36 box truck, which is expected to be the largest vehicle traveling to the site. Trash pick-up will also occur on the site without impacting pedestrian and vehicular movements along Washington Street.





Figure 3-11 Site Plan

10

Delivery estimates for the residential element of the Project are based on data provided in the Truck Trip Generation Rates by Land Use in the Central Artery/Tunnel Project Study Area report¹. Deliveries to the Project site will likely be SU-36 trucks and smaller delivery vehicles. Residential units primarily generate delivery trips related to small packages and prepared food. Based on the CTPS report, the Project is expected to generate one light truck trip per day to the site.

3.4.4 Bicycle Accommodations

BTD has established guidelines requiring projects subject to Transportation Access Plan Agreements to provide secure bicycle parking for residents and short-term bicycle racks for visitors. Based on BTD guidelines, the Project will supply a minimum of 57 secure bicycle parking/storage spaces within the site, as well as short-term bicycle spaces.

3.4.5 Trip Generation Methodology

Determining the future trip generation of the Project is a complex, multi-step process that produces an estimate of vehicle trips, transit trips, walk trips, and bicycle trips associated with a proposed development and a specific land use program. A project's location and proximity to different travel modes determines how people will travel to and from a project site.

To estimate the number of trips expected to be generated by the Project, data published by the Institute of Transportation Engineers (ITE) in the *Trip Generation Manual*² were used. ITE provides data to estimate the total number of unadjusted vehicular trips associated with the Project. In an urban setting well-served by transit, adjustments are necessary to account for other travel mode shares such as walking, bicycling, and transit.

To estimate the trip generation for the Project, the following ITE land use code (LUCs) were used:

Land Use Code 220 –Apartment. The apartment land use includes rental dwelling units located within the same building with at least three other dwelling units. Calculations of the number of trips use ITE's average rate per residential unit. The Apartment land use code has slightly higher trip generation rates than condominiums based on the ITE data and was used in this analysis to provide a more conservative (higher) estimate.

¹ Truck Trip Generation Rates by Land Use in the Central Artery/Tunnel Project Study Area; Central Transportation Planning Staff; September 1993.

² Trip Generation Manual, 9th Edition; Institute of Transportation Engineers; Washington, D.C.; 2012.

Land Use Code 710 –General Office Building. The General Office Building land use code is defined as a building with multiple tenants where affairs of business, industrial organizations, professional persons, or firms are conducted. Calculations of the number of trips use ITE's average rate per 1,000 sf.

3.4.6 Mode Share

BTD provides vehicle, transit, and walking mode split rates for different areas of Boston. The Project is located within designated Area 9 – Outer Red Line, Mattapan. The unadjusted vehicular trips were converted to person trips by using vehicle occupancy rates published by the Federal Highway Administration (FHWA)³. The person trips were then distributed to different modes according to the mode shares shown in Table 3-8.

Time Period		Land Use	Vehicle Occupancy Rate ¹	Walk/Bike Share ²	Transit Share ²	Vehicle Share²
	In	Apartmont	1.13	18%	16%	66%
Daily	Out	дрантнени	1.13	18%	16%	66%
Dally	In	Office	1.13	10%	15%	75%
	Out	Building	1.13	10%	15%	75%
	In	A	1.13	28%	18%	54%
a ma Daali Llaur	Out	Apartment	1.13	13%	31%	56%
a.m. Peak Hour	In	Office	1.13	17%	19%	64%
	Out	Building	1.13	8%	29%	63%
	In	A in a state a set	1.13	13%	31%	56%
p.m. Peak Hour	Out	Apartment	1.13	28%	18%	54%
	In	Office	1.13	8%	29%	63%
	Out	Building	1.13	17%	19%	64%

Table 3-8Travel Mode Shares

1. 2009 National Household Travel Survey.

2. Based on rates published by the Boston Transportation Department for Area 9.

3.4.7 Project Trip Generation

The mode share percentages shown in Table 3-8 were applied to the number of person trips to develop walk/bicycle, transit, and vehicle trip generation estimates. The trip generation for the Project by mode is shown in Table 3-9. The detailed trip generation information is provided in Appendix B.

³ Summary of Travel Trends: 2009 National Household Travel Survey; FHWA; Washington, D.C.; June 2011.

Time Period		Walk/Bike Trips	Transit Trips	Primary Vehicle Trips
		Daily		
Apartment ¹		78	68	252
Office Building ²		4	6	32
Total	Daily Trips	82	74	284
		a.m. Peak H	our	
	In	2	1	4
Apartment ¹	Out	<u>3</u>	<u>8</u>	<u>13</u>
	Total	5	9	17
	In	1	1	4
Office Building ²	Out	<u>0</u>	<u>0</u>	<u>1</u>
	Total	1	1	5
Total a.m. Peak	Hour Trips	6	10	22
	-	p.m. Peak H	our	
	In	3	3	13
Apartment ¹	Out	4	8	6
	Total	7	11	19
	In	0	1	1
Office Building ²	Out	1	0	3
	Total	1	1	4
Total p.m. Peak	Hour Trips	8	12	23

Table 3-9Project Trip Generation

1. Based on ITE LUC 220- Apartment, average rate per unit

2. Based on ITE LUC 710 –1,000 sf General Office Building, average rate

As shown in Table 3-9, the Project is expected to generate approximately 284 vehicular trips on a daily basis, with 22 trips during the weekday a.m. peak hour and 23 trips during the weekday p.m. peak hour. The transit trips will be accommodated by the MBTA buses that run along Dorchester Avenue and by the nearby Mattapan Trolley portion of the Red Line.

3.4.8 Trip Distribution

The trip distribution identifies the various travel paths for vehicles arriving and leaving the Project site. Trip distribution patterns for the Project were based on BTD's origin-destination data and trip distribution patterns presented in traffic studies for nearby projects. The vehicle trips associated with the Project were assigned to the proposed parking garage on site. The trip distribution patterns for the Project are illustrated in Figure 3-12.

3.4.9 Build (2024) Traffic Volumes

The vehicle trips were distributed through the study area. The Project-generated trips for the weekday a.m. peak hour and weekday p.m. peak hour are shown in Figure 3-13 and Figure 3-14, respectively. The trip assignments were added to the No-Build (2024) Condition vehicular traffic volumes to develop the Build (2024) Condition vehicular traffic volumes. The Build (2024) weekday a.m. peak hour and weekday p.m. peak hour traffic volumes are shown on Figure 3-15 and Figure 3-16, respectively.





















3.4.10 Build (2024) Condition Traffic Operations Analysis

The Build (2024) Condition capacity analysis uses the same methodology as the Existing (2017) Condition capacity analysis and the No-Build (2024) Condition capacity analysis. Table 3-10 and Table 3-11 present the Build (2024) Condition capacity analysis for the weekday a.m. peak hour and weekday p.m. peak hour, respectively. The detailed analysis sheets are provided in Appendix B.

Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)
Sign	alized				
Washington Street/Morton Street/Richmond Street	D	55.0	-	-	-
Morton Street EB left/thru	D	41.2	0.29	79	180
Morton Street EB right	А	1.3	0.25	0	2
Richmond Street WB left/thru thru/right	F	>80.0	0.95	140	#267
Washington Street NB bear left	F	>80.0	0.97	186	m#354
Washington Street NB thru/right	D	38.7	0.62	238	m324
Washington Street SB bear left	E	75.1	0.60	32	#92
Washington Street SB thru/right	D	43.8	0.49	131	207
Washington Street/River Street	С	24.1	-	-	-
River Street EB left	E	67.9	0.83	203	#370
River Street EB right	А	8.2	0.24	58	109
Washington Street NB left	В	11.6	0.26	46	m149
Washington Street NB thru	А	2.7	0.34	4	120
Washington Street SB thru	D	52.5	0.52	131	m182
Washington Street SB right	В	16.8	0.39	33	m78
Dorchester Avenue/Washington Street/Adams Street	D	37.1	-	-	-
Washington Street EB left/thru	E	72.1	0.90	151	#347
Washington Street EB right	А	9.6	0.23	14	66
Adams Street WB left	F	>80.0	0.90	108	#221
Adams Street WB thru/right	D	42.0	0.47	125	195
Adams Street NB left	D	41.6	0.76	250	#348
Adams Street NB thru	С	29.0	0.39	188	278
Adams Street NB right	А	4.3	0.43	0	67
Dorchester Avenue SB left/thru thru/right	С	33.9	0.34	73	117
Dorchester Avenue/Richmond Street	В	14.2	-	-	-
Richmond Street EB left/thru/right	С	25.0	0.58	27	#143
Richmond Street WB left/thru/right	В	14.7	0.31	11	61
Dorchester Avenue NB left/thru/right	В	12.8	0.49	48	#267
Dorchester Avenue SB left/thru/right	А	9.2	0.28	24	126

Table 3-10Build (2024) Condition Capacity Analysis Summary, Weekday a.m. Peak Hour

Table 3-10Build (2024) Condition Capacity Analysis Summary, Weekday a.m. Peak Hour
(Continued)

Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)
Unsig	gnalized				
Washington Street/ Site Driveway	-	-	-	-	-
Site Driveway WB left/right	В	14.9	0.04	-	2.5
Washington Street NB thru/right	А	0.0	0.00	-	0
Washington Street SB left/thru	А	9.2	0.07	-	0

95th percentile volume exceeds capacity.

m = Queue is metered from upstream signal.

Table 3-11Build (2024) Condition Capacity Analysis Summary, Weekday p.m. Peak Hour

Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)	
Signalized						
Washington Street/Morton Street/Richmond Street	D	46.4	-	-	-	
Morton Street EB left/thru	С	34.9	0.24	75	171	
Morton Street EB right	А	4.2	0.30	0	41	
Richmond Street WB left/thru thru/right	F	>80.0	1.01	~166	#318	
Washington Street NB bear left/thru/right	D	40.8	0.67	82	m117	
Washington Street NB thru/right	С	27.2	0.44	182	m176	
Washington Street SB bear left/thru/right	D	42.6	0.20	21	52	
Washington Street SB thru/right	D	51.4	0.69	186	282	
Washington Street/River Street	С	27.8	-	-	-	
River Street EB left	E	73.8	0.78	131	#229	
River Street EB right	А	9.7	0.25	58	116	
Washington Street NB left	С	24.1	0.33	60	254	
Washington Street NB thru	А	9.3	0.18	45	107	
Washington Street SB thru		49.2	0.62	153	m173	
Washington Street SB right	В	14.8	0.49	50	m29	
Dorchester Avenue/Washington Street/Adams Street	D	38.5	-	-	-	
Washington Street EB left/thru	E	65.2	0.87	173	#276	
Washington Street EB right		7.6	0.36	77	53	
Adams Street WB left		>80.0	0.91	136	#247	
Adams Street WB thru/right		47.0	0.59	161	237	
Adams Street NB left		34.8	0.59	132	#237	
Adams Street NB thru		27.0	0.30	140	219	
Adams Street NB right		4.5	0.23	0	50	
Dorchester Avenue SB left/thru thru/right	D	39.6	0.48	164	222	

Table 3-11Build (2024) Condition Capacity Analysis Summary, Weekday p.m. Peak Hour
(Continued)

Intersection/Approach	LOS	Delay (s)	V/C Ratio	50th Percentile Queue (ft)	95th Percentile Queue (ft)	
Signalized						
Dorchester Avenue/Richmond Street	С	20.8	-	-	-	
Richmond Street EB left/thru/right	С	29.6	0.60	49	100	
Richmond Street WB left/thru/right		38.1	0.72	70	130	
Dorchester Avenue NB left/thru/right		13.7	0.33	41	181	
Dorchester Avenue SB left/thru/right	В	13.8	0.36	52	219	
Unsignalized						
Washington Street/Site Driveway	-	-	-	-	-	
Site Driveway WB left/right		12.5	0.04	-	2.5	
Washington Street NB thru/right		0	0.00	-	0	
Washington Street SB left/thru	А	8.2	0.01	-	0	

95th percentile volume exceeds capacity.

 \sim 50th percentile volume exceeds capacity. Queue may be longer. Queue shown is the maximum after two cycles.

m = Queue is metered from upstream signal.

As shown in Table 3-10 and Table 3-11, the study area intersections are expected to continue to operate at LOS D or better during the peak hours. The site driveway will operate at LOS B, with minimal delay and queueing.

The Project is expected to have minimal impact on traffic operations throughout the study area. Based on this analysis, no additional mitigation is required to accommodate the Project.

3.5 Transportation Demand Management

The Proponent is committed to implementing Transportation Demand Management (TDM) measures to minimize automobile usage and Project related traffic impacts. TDM will be facilitated by the nature of the Project (which does not generate significant peak hour trips) and its proximity to numerous public transit alternatives.

On-site management will keep a supply of transit information (schedules, maps, and fare information) to be made available to the residents and patrons of the site. The Proponent will work with the City to develop a TDM program appropriate to the Project and consistent with its level of impact.

The Proponent is prepared to take advantage of good transit access in marketing the site to future residents by working with them to implement the following TDM measures to encourage the use of non-vehicular modes of travel.

The TDM measures for the Project may include, but are not limited, to the following:

- The Proponent will designate a transportation coordinator to oversee transportation issues, including parking, service and loading, and deliveries, and will work with tenants as they move in to the retail/commercial spaces to raise awareness of public transportation, bicycling, and walking opportunities;
- The Proponent will provide orientation packets to new tenants containing information on available transportation choices, including transit routes/schedules and nearby vehicle sharing and bicycle sharing locations. On-site management will work with residents and tenants as they move in to help facilitate transportation for new arrivals;
- The Proponent will provide an annual (or more frequent) newsletter or bulletin summarizing transit, ridesharing, bicycling, alternative work schedules, and other travel options;
- The Proponent will provide two electric vehicle charging stations on the site;
- The Proponent will provide information on travel alternatives for employees and visitors via the Internet and in the building lobby; and
- The Proponent will explore the feasibility of providing spaces on-site for a car sharing service.

3.6 Transportation Mitigation Measures

Although the traffic impacts associated with the new trips are minimal (generating less than three vehicle trips per minute during the peak hours), the Proponent will continue to work with the City of Boston so that the Project efficiently serves vehicle trips, improves the pedestrian environment, and encourages transit and bicycle use.

The Proponent is responsible for preparation of the Transportation Access Plan Agreement (TAPA), a formal legal agreement between the Proponent and the BTD. The TAPA formalizes the findings of the transportation study, mitigation commitments, elements of access and physical design, travel demand management measures, and any other responsibilities that are agreed to by both the Proponent and the BTD. Because the TAPA must incorporate the results of the technical analysis, it must be executed after these other processes have been completed. The proposed measures listed above and any additional transportation improvements to be undertaken as part of this Project, will be defined and documented in the TAPA.

The Proponent will also produce a Construction Management Plan (CMP) for review and approval by BTD. The CMP will detail the schedule, staging, parking, delivery, and other associated impacts of the construction of the Project.

3.7 Evaluation of Short-term Construction Impacts

Most construction activities will be accommodated within the current site boundaries. Details of the overall construction schedule, working hours, number of construction workers, worker transportation and parking, number of construction vehicles, and routes will be addressed in detail in a CMP to be filed with BTD in accordance with the City's transportation maintenance plan requirements.

To minimize transportation impacts during the construction period, the following measures will be considered for the CMP:

- Limited construction worker parking on-site;
- Encouragement of worker carpooling;
- Consideration of a subsidy for MBTA passes for full-time employees; and
- Providing secure spaces on-site for workers' supplies and tools so they do not have to be brought to the site each day.

The CMP to be executed with the City prior to commencement of construction will document all committed measures.

Chapter 4.0

Environmental Review Component

4.1 Wind

Major buildings, especially those that protrude above their surroundings, often cause increased local wind speeds at the pedestrian level. Typically, wind speeds increase with elevation above the ground surface, and taller buildings intercept these faster winds and deflect them down to the pedestrian level. The funneling of wind through gaps between buildings and the acceleration of wind around corners of buildings may also cause increases in wind speed. Conversely, if a building is surrounded by others of equivalent height, it may be protected from the prevailing upper-level winds, resulting in no significant changes to the local pedestrian-level wind environment.

The proposed Project is four stories and approximately 40 feet tall at its highest point. The other buildings surrounding the Project site are primarily two to three-story buildings and are similar in height. In addition, the Project will include new trees on the sidewalks surrounding the Project, which serve to reduce wind speeds. Due to the Project's low height, along with significant landscaping included in the Project, wind impacts are not anticipated.

4.2 Shadow Impacts

The proposed Project consists of the demolition of three existing, two to three-story buildings, and the construction of one four-story building. Due to the minimal new height being proposed, new shadow from the Project will be limited to Washington Street and its sidewalks. In the mornings, shadow is cast to the northwest, and the Project will cast new shadow onto Washington Street. In the afternoons, the shadow moves north, and most of the shadow cast by the Project will be within the Project site. In the afternoons shadow swings east, onto areas adjacent to the Lower Mills Branch library. No new shadow will be cast onto nearby public open spaces or bus stops.

4.3 Daylight Analysis

4.3.1 Introduction

The purpose of the daylight analysis is to estimate the extent to which a proposed project will affect the amount of daylight reaching the streets and the sidewalks in the immediate vicinity of a project site. The daylight analysis for the Project considers the existing and proposed conditions, as well as daylight obstruction values of the surrounding area.

Because the Project site currently consists of several two to three-story buildings with space between each, the proposed Project will inherently increase daylight obstruction; however, resulting conditions will be similar to the daylight obstruction values within the surrounding area due to the height of the building and open areas on each side of the building, which is consistent with the development pattern in the neighborhood.

4.3.2 Methodology

The daylight analysis was performed using the Boston Redevelopment Authority Daylight Analysis (BRADA) computer program¹. This program measures the percentage of sky-dome that is obstructed by a project and is a useful tool in evaluating the net change in obstruction from existing to build conditions at a specific site.

Using BRADA, a silhouette view of the building is taken at ground level from the middle of the adjacent city streets or pedestrian ways centered on the proposed building. The façade of the building facing the viewpoint, including heights, setbacks, corners and other features, is plotted onto a base map using lateral and elevation angles. The two-dimensional base map generated by BRADA represents a figure of the building in the "sky dome" from the viewpoint chosen. The BRADA program calculates the percentage of daylight that will be obstructed on a scale of 0 to 100 percent based on the width of the view, the distance between the viewpoint and the building, and the massing and setbacks incorporated into the design of the building; the lower the number, the lower the percentage of obstruction of daylight from any given viewpoint.

The analysis compares three conditions: Existing Conditions; Proposed Conditions; and the context of the area.

One viewpoint was chosen to evaluate the daylight obstruction for the Existing and Proposed Conditions, since the Project site is adjacent to only one public way. Three area context points were considered to provide a basis of comparison to existing conditions in the surrounding area. The viewpoint and area context viewpoints were taken in the following locations and are shown in Figure 4.3-1.

- Viewpoint 1: View from Washington Street facing northeast toward the Project site.
- Area Context Viewpoint AC1: View from Washington Street facing northeast toward 1110 Washington Street.
- Area Context Viewpoint AC2: View from Richmond Street facing south toward a residence on Richmond Street.
- Area Context Viewpoint AC3: View from Dorchester Avenue facing west toward 2269 Dorchester Avenue.

4.3.3 Results

The results for each viewpoint are described in Table 4.3-1. Figures 4.3-2 and 4.3-3 illustrate the BRADA results for each analysis.

¹ Method developed by Harvey Bryan and Susan Stuebing, computer program developed by Ronald Fergle, Massachusetts Institute of Technology, Cambridge, MA, September 1984.







Viewpoint Locat	ions	Existing Conditions	Proposed Conditions			
Viewpoint 1	View from Washington Street facing northeast toward the Project site	21.8%	40.7%			
Area Context Points						
AC1	View from Washington Street facing northeast toward 1110 Washington Street	29.6%	N/A			
AC2	View from Richmond Street facing south toward a residence on Richmond Street	56.2%	N/A			
AC3	View from Dorchester Avenue facing west toward 2269 Dorchester Avenue	27.8%	N/A			

Table 4.3-1Daylight Analysis Results

Washington Street – Viewpoint 1

Washington Street runs along the southwestern edge of the Project site. Viewpoint 1 was taken from the center of Washington Street facing northeast toward the Project site. The Project site has an existing daylight obstruction of 21.8% due to the spaces between the buildings and the low heights of the existing buildings. The development of the Project will increase the daylight obstruction to 40.7%. Daylight obstruction is minimized by the spaces next to the building which allow for views of the sky, as well as the height of the building, which is similar to heights of other buildings in the neighborhood. The daylight obstruction value is consistent with the daylight obstruction value of other buildings in the area, including the Area Context buildings.

Area Context Viewpoints

The Project site is located in an area with a mix of one to three-story buildings with a mix of residential and commercial uses. To provide a larger context for comparison of daylight conditions, obstruction values were calculated for the three Area Context Viewpoints described above and shown on Figure 4.3-1. The daylight obstruction values ranged from 27.8% for AC3 to 56.2% for AC2. Daylight obstruction values for the Project are consistent with the Area Context values.

4.3.4 Conclusions

The daylight analysis conducted for the Project describes existing and proposed daylight obstruction conditions at the Project site and in the surrounding area. The results of the BRADA analysis indicate that while the development of the Project will result in increased daylight obstruction over existing conditions, the resulting conditions will be similar to the daylight obstruction values within the surrounding area. **Existing Conditions:** View from Washington Street facing northeast toward the Project site



Obstruction of daylight by the building is 21.8 %

Proposed Conditions: View from Washington Street facing northeast toward the Project site



Obstruction of daylight by the building is 40.7 %




Obstruction of daylight by the building is 29.6 %

Area Context Viewpoint AC1: View from Washington Street facing northeast toward 1110 Washington Street



Obstruction of daulight by the building is 27.8 % Area Context Viewpoint AC3: View from Dorchester Avenue facing west toward 2269 Dorchester Avenue

1120-1132 Washington Street Boston, Massachusetts





Obstruction of daylight by the building is 56.2 %

Area Context Viewpoint AC2: View from Richmond Street facing south toward 17 Richmond Street

4.4 Solar Glare

The Project materials are still being studied and glazing of the windows will be determined as the design progresses. Due to the type of potential glass and glazing proposed, solar glare impacts are not currently anticipated.

4.5 Air Quality Analysis

4.5.1 Introduction

The BPDA requires that proposed projects evaluate the air quality in the local area, and assess any adverse air quality impacts attributable to a project.

The Project doesn't generate enough traffic to require a mesoscale vehicle emissions quantification analysis. However, the Project creates new trips to local intersections operating at LOS D or worse. Therefore, a microscale analysis of carbon monoxide has been completed to provide information on the Project's impact to air quality from mobile sources. Results of the microscale analysis show that all predicted CO concentrations are well below one-hour and eight-hour National Ambient Air Quality Standards (NAAQS).

Any new stationary sources will be reviewed by the Massachusetts Department of Environmental Protection (MassDEP) during permitting under the Environmental Results Program, as required. It is expected that all stationary sources will be small, and any impacts from stationary sources would be minimal.

4.5.2 National Ambient Air Quality Standards and Background Concentrations

Background air quality concentrations and federal air quality standards were utilized to conduct the above air quality impact analyses. Federal NAAQS were developed by the U.S. Environmental Protection Agency (EPA) to protect the human health against adverse health effects with a margin of safety. The modeling methodologies were developed in accordance with the latest MassDEP modeling policies and Federal modeling guidelines.² The following sections outline the NAAQS standards and detail the sources of background air quality data.

4.5.2.1 National Ambient Air Quality Standards

The 1970 Clean Air Act was enacted by the U.S. Congress to protect the health and welfare of the public from the adverse effects of air pollution. As required by the Clean Air Act, EPA promulgated NAAQS for the following criteria pollutants: nitrogen dioxide (NO₂), sulfur dioxide (SO₂), particulate matter (PM) (PM-10 and PM-2.5), carbon monoxide (CO),

² 40 CFR 51 Appendix W, Guideline on Air Quality Models, 70 FR 68228, Nov. 9, 2005

ozone (O₃), and lead (Pb). The NAAQS are listed in Table 4.5-1. Massachusetts Ambient Air Quality Standards (MAAQS) are typically identical to NAAQS (differences are highlighted in **bold** in Table 4.5-1).

NAAQS specify concentration levels for various averaging times and include both "primary" and "secondary" standards. Primary standards are intended to protect human health, whereas secondary standards are intended to protect public welfare from any known or anticipated adverse effects associated with the presence of air pollutants, such as damage to vegetation. The more stringent of the primary or secondary standards were applied when comparing to the modeling results for this Project.

The NAAQS also reflect various durations of exposure. The non-probabilistic short-term periods (24 hours or less) refer to exposure levels not to be exceeded more than once a year. Long-term periods refer to limits that cannot be exceeded for exposure averaged over three months or longer.

	Averaging	NA/ (µg	AQS /m³)	MA (µg	MAAQS (µg/m³)		
Pollutant	Period	Primary Secondary		Primary	Secondary		
NO	Annual (1)	100	Same	100	Same		
INO2	1-hour (2)	188	None	None	None		
	Annual (1)(9)	80	None	80	None		
50.	24-hour (3)(9) 365		None	365	None		
302	3-hour (3)	None	1300	None	1300		
	1-hour (4)	196	None	None	None		
DAADE	Annual (1)	12	15	None	None		
F/W-2.5	24-hour (5)	35	Same	None	None		
DM 10	Annual (1)(6)	None	None	50	Same		
P/W-10	24-hour (3)(7)	150	Same	150	Same		
60	8-hour (3)	10,000	Same	10,000	Same		
	1-hour (3)	40,000	Same	40,000	Same		
Ozone	8-hour (8)	147	Same	235	Same		
Pb	3-month (1) 1.5		Same	1.5	Same		

lable 4.5-1 National (NAAOS) and Massachusetts (MAAOS) Ambient Air Quality Sta
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(1) Not to be exceeded.

(2) 98th percentile of one-hour daily maximum concentrations, averaged over three years.

(3) Not to be exceeded more than once per year.

(4) 99th percentile of one-hour daily maximum concentrations, averaged over three years.

(5) 98th percentile, averaged over three years.

(6) EPA revoked the annual PM-10 NAAQS in 2006.

(7) Not to be exceeded more than once per year on average over three years.

(8) Annual fourth-highest daily maximum eight-hour concentration, averaged over three years.

(9) EPA revoked the annual and 24-hour SO₂ NAAQS in 2010. However, they remain in effect until one year after the area's initial attainment designation, unless designated as "nonattainment".

Source: http://www.epa.gov/ttn/naaqs/criteria.html and 310 CMR 6.04

4.5.2.2 Background Concentrations

To estimate background pollutant levels representative of the area, the most recent air quality monitor data reported by the MassDEP to EPA was obtained for 2013 to 2015. Data for the pollutant and averaging time combinations were obtained from the EPA's AirData website.

The Clean Air Act allows for one exceedance per year of the CO and SO₂ short-term NAAQS per year. The highest second-high accounts for the one exceedance. Annual NAAQS are never to be exceeded. The 24-hour PM-10 standard is not to be exceeded more than once per year on average over three years. To attain the 24-hour PM-2.5 standard, the three-year average of the 98th percentile of 24-hour concentrations must not exceed 35 μ g/m³. For annual PM-2.5 averages, the average of the highest yearly observations was used as the background concentration. To attain the one-hour NO₂ standard, the three-year average of the 98th percentile of the maximum daily one-hour concentrations must not exceed 188 μ g/m³.

Background concentrations were determined from the closest available monitoring stations to the Project site. All pollutants are not monitored at every station, so data from multiple locations are necessary. The closest monitor is at Harrison Avenue in Boston, roughly 3.9 miles north of the Project site. A summary of the background air quality concentrations are presented in Table 4.5-2.

Pollutant	Averaging Time	2013	2014	2015	Background Concentration (µg/m³)	NAAQS	Percent of NAAQS
	1-Hour (5)	28.6	32.2	24.6	28.5	196.0	15%
SO ₂ (1)(6)(7)	3-Hour	25.4	56.3	22.8	56.3	1300.0	4%
302	24-Hour	13.1	13.4	11.3	13.4	365.0	4%
	Annual	2.8	2.8	2.1	2.8	80.0	4%
DNA 10	24-Hour	34.0	61.0	28.0	61.0	150.0	41%
F/M-10	Annual	15.1	13.9	12.4	15.1	50.0	30%
	24-Hour (5)	15.9	12.7	19.0	15.9	35.0	45%
F/W-2.3	Annual (5)	7.3	6.0	8.8	7.4	12.0	61%
	1-Hour (5)	94.0	95.9	99.6	96.5	188.0	51%
NO_2	Annual	32.8	29.6	28.1	32.8	100.0	33%
	1-Hour	2145.3	1963.1	1560.9	2145.3	40000.0	5%
	8-Hour	1375.2	1489.8	1031.4	1489.8	10000.0	15%

Table 4.5-2Observed Ambient Air Quality Concentrations and Selected Background Levels
(Continued)

Pollutant	Averaging Time	2013 2014 2015		2015	Background Concentration (µg/m³)	NAAQS	Percent of NAAQS	
Ozone (4)	8-Hour	115.8	106.0	109.9	115.8	147.0	79%	
Lead	Rolling 3- Month	0.006	0.014	0.016	0.016	0.15	10%	

Notes:

From 2013-2015 EPA's AirData Website

⁽¹⁾ SO₂ reported ppb. Converted to μ g/m³ using factor of 1 ppm = 2.62 μ g/m³.

⁽²⁾ CO reported in ppm. Converted to μ g/m³ using factor of 1 ppm = 1146 μ g/m³.

⁽³⁾ NO₂ reported in ppb. Converted to μ g/m³ using factor of 1 ppm = 1.88 μ g/m³.

⁽⁴⁾ O₃ reported in ppm. Converted to $\mu g/m^3$ using factor of 1 ppm = 1963 $\mu g/m^3$.

⁽⁵⁾ Background level is the average concentration of the three years.

⁽⁶⁾ The 24-hour and Annual standards were revoked by EPA on June 22, 2010, Federal Register 75-119, p. 35520.

⁽⁷⁾ The E. 1st St. monitor was closed in 2014. Harrison Avenue data used for 2015 SO₂ and NO₂.

Air quality in the vicinity of the Project site is generally good, with all local background concentrations found to be well below the NAAQS.

4.5.3 Methodology

Mobile sources of air pollution include emissions from gasoline, diesel, and natural gas fueled vehicle traffic. Emissions from mobile sources have continually decreased as engine technology and efficiency have been improved.

4.5.3.1 Microscale Analysis

The BPDA typically requests an analysis of the effect on air quality of the increase in traffic generated by projects subject to Large Project Review. This "microscale" analysis is typically required for any intersection where 1) Project traffic would impact intersections or roadway links currently operating at LOS D, E, or F or would cause LOS to decline to D, E, or F; 2) Project traffic would increase traffic volumes on nearby roadways by 10% or more (unless the increase in traffic volume is less than 100 vehicles per hour); or, 3) the Project will generate 3,000 or more new average daily trips on roadways providing access to a single location. The microscale analysis involves modeling of CO emissions from vehicles idling at and traveling through signaled intersections. Predicted ambient concentrations of CO for the Build and No-Build cases are compared with federal (and state) ambient air quality standards for CO.

The microscale analysis typically examines ground-level CO impacts due to traffic queues in the immediate vicinity of a project. CO is used in microscale studies to indicate roadway pollutant levels since it is the most abundant pollutant emitted by motor vehicles and can result in so-called "hot spot" (high concentration) locations around congested intersections. The NAAQS standards do not allow ambient CO concentrations to exceed 35 parts per million (ppm) for a one-hour averaging period, and 9 ppm for an eight-hour averaging period, more than once per year at any location. The widespread use of CO catalysts on current vehicles has reduced the occurrences of CO hotspots. Air quality modeling techniques (computer simulation programs) are typically used to predict CO levels for both existing and future conditions to evaluate compliance of the roadways with the standards. The microscale analysis has been conducted using the latest versions of EPA's MOVES and CAL3QHC programs to estimate CO concentrations at sidewalk receptor locations. Baseline (2017) and future year (2024) emission factor data calculated from the MOVES model, along with traffic data, were input into the CAL3QHC program to determine CO concentrations due to traffic flowing through the selected intersections. The modeling methodology was developed in accordance with the latest MassDEP modeling policies and Federal modeling guidelines.³

Existing background values of CO at the nearest monitor location at Harrison Avenue were obtained from MassDEP. CAL3QHC results were then added to background CO values of 1.9 ppm (one-hour) and 1.3 ppm (eight-hour), as provided by MassDEP, to determine total air quality impacts due to the Project. These values were compared to the NAAQS for CO of 35 ppm (one-hour) and 9 ppm (eight-hour).

Modeling assumptions and backup data for results presented in this section are provided in Appendix C.

Intersection Selection

Two signalized intersections included in the traffic study meet the above conditions described at the beginning of this section (see Chapter 3). The traffic volumes and LOS calculations provided in Chapter 3 form the basis of evaluating the traffic data versus the microscale thresholds. The intersections found to meet the criteria are:

- Washington Street, Morton Street, and Richmond Street, and
- Washington Street, Adams Street, Dorchester Avenue.

Microscale modeling was performed for the intersections based on the aforementioned methodology. The 2017 Existing Condition and the 2024 No-Build and Build conditions were each evaluated for both morning (a.m.) and afternoon (p.m.) peak.

Emissions Calculations (MOVES)

The EPA MOVES computer program was used to estimate motor vehicle emission factors on the roadway network. Emission factors calculated by the MOVES model are based on motor vehicle operations typical of daily periods. The Commonwealth's statewide annual

³ 40 CFR 51 Appendix W, Guideline on Air Quality Models, 70 FR 68228, Nov. 9, 2005

Inspection and Maintenance (I&M) program was included, as well as the county specific vehicle age registration distribution, fleet mix, meteorology, and other inputs. The inputs for MOVES for the existing (2017) and future year (2024) are provided by MassDEP.

All link types for the modeled intersections were input into MOVES. Idle emission factors are obtained from factors for a link average speed of 0 miles per hour (mph). Moving emissions are calculated based on speeds at which free-flowing vehicles travel through the intersection as stated in traffic modeling (Synchro) reports. A speed of 25 mph is used for all free-flow traffic, consistent with the City of Boston speed limit. Speeds of 10 and 15 mph were used for right (and U-turns, if necessary) and left turns, respectively. Roadway emissions factors were obtained from MOVES using EPA guidance.⁴

Winter CO emission factors are typically higher than summer. Therefore, January weekday emission factors were conservatively used in the microscale analysis.

Receptors & Meteorology Inputs

Sets of up to 200 receptors were placed in the vicinity of the modeled intersections. Receptors extended approximately 300 feet on the sidewalks along the roadways approaching the intersections. The roadway links and receptor locations of the modeled intersections are presented in Figures 4.5-1 and 4.5-2.

For the CAL3QHC model, limited meteorological inputs are required. Following EPA guidance⁵, a wind speed of one meter per second, stability class D (4), and a mixing height of 1,000 meters were used. To account for the intersection geometry, wind directions from 0° to 350°, every 10° were selected. A surface roughness length of 321 centimeters was selected.⁶

Impact Calculations (CAL3QHC)

The CAL3QHC model predicts one-hour concentrations using queue-links at signalized intersections, worst-case meteorological conditions, and traffic input data. The one-hour concentrations were scaled by a factor of 0.9 to estimate eight-hour concentrations.⁷ The CAL3QHC methodology was based on EPA CO modeling guidance. Signal timings were provided directly from the traffic modeling outputs.

⁴ U.S. EPA, 2010. Using MOVES in Project-Level Carbon Monoxide Analyses. EPA-420-B-10-041

⁵ U.S. EPA, *Guideline for Modeling Carbon Monoxide from Roadway Intersections.* EPA-454/R-92-005, November 1992.

⁶ U.S. EPA, User's Guide for CAL3QHC Version 2: A Modeling Methodology for Predicting Pollutant Concentrations Near Roadway Intersections. EPA –454/R-92-006 (Revised), September 1995.

⁷ U.S. EPA, AERSCREEN User's Guide; EPA-454/B-11-001, March 2011.



1120-1132 Washington Street Boston, Massachusetts





¹¹²⁰⁻¹¹³² Washington Street Boston, Massachusetts



For use in the microscale analysis, background concentrations of CO in ppm were required. The corresponding maximum background concentrations in ppm were 1.9 ppm (2,145 μ g/m³) for one-hour and 1.3 ppm (1,490 μ g/m³) for eight-hour CO.

4.5.3.2 Air Quality Results

The results of the maximum one-hour predicted CO concentrations from CAL3QHC are provided in Tables 4.5-3 through 4.5-5 for the 2017 and 2024 scenarios. Eight-hour average concentrations are calculated by multiplying the maximum one-hour concentrations by a factor of 0.9.⁸

Intersection	Peak	CAL3QHC Modeled CO Impacts (ppm)	Monitored Background Concentration (ppm)	Total CO Impacts (ppm)	NAAQS (ppm)
1-Hour					
Washington Street, Morton	AM	0.2	1.9	2.1	35
Street, and Richmond Street	PM	0.2	1.9	2.1	35
Washington Street, Adams Street,	AM	0.3	1.9	2.2	35
Dorchester Avenue	PM	0.3	1.9	2.2	35
8-Hour					
Washington Street, Morton	AM	0.2	1.3	1.5	9
Street, and Richmond Street	PM	0.2	1.3	1.5	9
Washington Street, Adams Street,	AM	0.3	1.3	1.6	9
Dorchester Avenue	PM	0.3	1.3	1.6	9

Table 4.5-3 Summary of Microscale Modeling Analysis (Existing 2017)

Notes: CAL3QHC eight-hour impacts were conservatively obtained by multiplying one-hour impacts by a screening factor of 0.9.

⁸ U.S. EPA, AERSCREEN User's Guide; EPA-454/B-11-001, March 2011.

Intersection	Peak	CAL3QHC Modeled CO Impacts (ppm)	Monitored Background Concentration (ppm)	Total CO Impacts (ppm)	NAAQS (ppm)
1-Hour					
Washington Street, Morton	AM	0.1	1.9	2.0	35
Street, and Richmond Street	PM	0.1	1.9	2.0	35
Washington Street, Adams Street,	AM	0.2	1.9	2.1	35
Dorchester Avenue	PM	0.2	1.9	2.1	35
8-Hour					
Washington Street, Morton	AM	0.1	1.3	1.4	9
Street, and Richmond Street	PM	0.1	1.3	1.4	9
Washington Street, Adams Street,	AM	0.2	1.3	1.5	9
Dorchester Avenue	PM	0.2	1.3	1.5	9

Table 4.5-4Summary of Microscale Modeling Analysis (No-Build 2024)

Notes: CAL3QHC eight-hour impacts were conservatively obtained by multiplying one-hour impacts by a screening factor of 0.9.

Table 4.5-5 Summary of Microscale Modeling Analysis (B
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Intersection	CAL3QHC Monit Modeled CO Backgr Peak Impacts Concen (ppm) (pp		Monitored Background Concentration (ppm)	Total CO Impacts (ppm)	NAAQS (ppm)
1-Hour					
Washington Street, Morton	AM	0.1	1.9	2.0	35
Street, and Richmond Street	PM	0.1	1.9	2.0	35
Washington Street, Adams Street,	AM	0.2	1.9	2.1	35
Dorchester Avenue	PM	0.2	1.9	2.1	35
8-Hour					
Washington Street, Morton	AM	0.1	1.3	1.4	9
Street, and Richmond Street	PM	0.1	1.3	1.4	9
Washington Street, Adams Street,	AM	0.2	1.3	1.5	9
Dorchester Avenue	PM	0.2	1.3	1.5	9

Notes: CAL3QHC eight-hour impacts were conservatively obtained by multiplying one-hour impacts by a screening factor of 0.9.

The results of the one-hour and eight-hour maximum modeled CO ground-level concentrations from CAL3QHC were added to EPA supplied background levels for comparison to the NAAQS. These values represent the highest potential concentrations at the intersection as they are predicted during the simultaneous occurrence of "defined" worst case meteorology. The highest one-hour traffic-related concentration predicted in the area of the Project for the modeled conditions (0.3 ppm) plus background (1.9 ppm) is 2.2 ppm. The highest eight-hour traffic-related concentration predicted in the area of the Project for the modeled conditions (0.3 ppm) plus background (1.3 ppm) is 1.6 ppm. Both maximum concentrations occur under Existing Conditions.

Under future No-Build and Build cases, the highest one-hour traffic-related concentration predicted in the area of the Project for the modeled conditions (0.2 ppm) plus background (1.9 ppm) is 2.1 ppm. The highest eight-hour traffic-related concentration predicted in the area of the Project for the modeled conditions (0.2 ppm) plus background (1.3 ppm) is 1.5 ppm.

All concentrations are well below the one-hour NAAQS of 35 ppm and the eight-hour NAAQS of 9 ppm.

4.5.3.3 Conclusions

Results of the microscale analysis show that all predicted CO concentrations are well below one-hour and eight-hour NAAQS. Therefore, it can be concluded that there are no anticipated adverse air quality impacts resulting from increased traffic in the area.

4.6 Solid and Hazardous Waste

4.6.1 Hazardous Waste

A Phase I Environmental Site Assessment was conducted at the Project site by Penney Engineering, Inc. using methods consistent with ASTM E1527-105. No recognized environmental conditions were identified at the Project site.

Characterization of the environmental soil and groundwater quality at the Project site has not been conducted to date. Chemical testing of soil and groundwater to be generated as a result of construction activity will be conducted at the appropriate stage of the design process to further evaluate site environmental conditions. Management, transport and disposal of soil and groundwater will be in accordance with all applicable local, state, and federal laws and regulations

4.6.2 Operation Solid and Hazardous Waste Generation

The Project will generate solid waste typical of residential and commercial uses. Solid waste is expected to include wastepaper, cardboard, glass bottles and food. Recyclable materials will be recycled through a program implemented by building management. The Project will generate approximately 98 tons of solid waste per year.

With the exception of household hazardous wastes typical of residential and commercial developments (e.g., cleaning fluids), the Project will not involve the generation, use, transportation, storage, release, or disposal of potentially hazardous materials.

4.6.3 Recycling

A dedicated recyclables storage and collection program will facilitate the reduction of waste generated by building occupants that is hauled to and disposed of in landfills. Each floor of the residential building will provide a separate recycling bay, and individual units will include dedicated space in the kitchen for two bins in order to encourage recycling.

4.7 Noise Impacts

The City of Boston has both a noise ordinance and noise regulations. Chapter 16 §26 of the Boston Municipal Code sets the general standard for noise that is unreasonable or excessive: louder than 50 decibels between the hours of 11:00 p.m. and 7:00 a.m., or louder than 70 decibels at all other hours. The Boston Air Pollution Control Commission (APCC) has adopted regulations based on the city's ordinance - "Regulations for the Control of Noise in the City of Boston", which distinguish among residential, business, and industrial districts in the city. In particular, APCC Regulation 2 is applicable to the sounds from the proposed Project.

Table 4.7-1 below presents the "Zoning District Noise Standards" contained in Regulation 2.5 of the APCC "Regulations for the Control of Noise in the City of Boston," adopted December 17, 1976. These maximum allowable sound pressure levels apply at the property line of the receiving property. Zoning District Standards are presented below in Table 4.7-1.

Octave-band Center	Resid Zoning	dential g District	Residenti Zonin	al-Industrial g District	Business Zoning District	Industrial Zoning District
Frequency	Daytime	All Other Times	Daytime	All Other Times	Anytime	Anytime
(Hz)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)
32	76	68	79	72	79	83
63	75	67	78	71	78	82
125	69	61	73	65	73	77
250	62	52	68	57	68 62	73
500	56	46	62	51		67
1000	50	40	56 45 56		56	61
2000	45	33	51	39	51 47	57
4000	40	28	47	34		53
8000	38	26	44	32	44	50
A-Weighted	60	50	65	55	65	70
(dBA)						
Notes: Noise standards are extracted from Regulation 2.5, City of Boston Air Pollution Control Commission, "Regulations for the Control of Noise in the City of Boston", adopted Decembe 1976.						
All stand	lards apply at	the property li	ne of the rece	iving property.		
dB and c	BA based on	a reference so	und pressure o	of 20 micropasc	als.	
'Daytime	e' refers to the	e period betwee	en 7:00 a.m. a	and 6:00 p.m. da	aily, excluding Su	unday.

Table 4.7-1	City	of	Boston	Zoning	District	Noise	Standards,	Maximum	Allowable	Sound
	Press	ure	Levels							

Additionally, the MassDEP has the authority to regulate noise under 310 CMR 7.10, which is part of the Commonwealth's air pollution control regulations. According to MassDEP, "unnecessary" noise is considered an air contaminant and thus prohibited by 310 CMR 7.10. The MassDEP administers this regulation through Noise Policy DAQC 90-001 which limits a source to a 10-dBA increase above the L₉₀ ambient sound level measured at the Project property line and at the nearest residences. The MassDEP policy further prohibits "pure tone" conditions where the sound pressure level in one octave-band is 3 dB or more than the sound levels in each of two adjacent bands.

While the details of the mechanical equipment associated with the Project have not yet been precisely determined, steady operational noise from stationary sources will primarily involve heating, cooling, and ventilation equipment for the commercial spaces and residential units. During the final design phase of the Project, mechanical equipment will be specified to meet the applicable City of Boston and MassDEP noise limits. Reasonable efforts will be made, if necessary, to minimize noise impacts from the Project using routinely employed methods of noise control. With appropriate noise control, the Project is not expected to result in any adverse noise impacts at nearby sensitive receptors. Short-term, intermittent increases in noise levels will occur during Project construction. However, every reasonable effort will be made to minimize the noise impacts and ensure the project complies with the requirements of the City of Boston noise ordinance.

4.8 Stormwater/Water Quality

Chapter 8 includes a discussion of stormwater and water quality.

4.9 Flood Hazard Zones/ Wetlands

The Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) for the site located in the City of Boston - Community Panel Number 25025C0089J, effective March 16, 2016, indicates the FEMA Flood Zone Designations for the site area. The map shows that the Project is located in a Zone X, "Areas determined to be outside the 0.2% annual chance floodplain."

The site does not contain wetlands.

4.10 Geotechnical Impacts

4.10.1 Site Conditions

The Project site, as described in Section 2.1.1, comprises six parcels of land with a total of approximately 48,303 sf located on the easterly side of Washington Street south of Richmond Street. The site currently contains the former Molloy Funeral Home, a parking lot, and residential building on each side of the funeral home. The site is relatively flat, with a high point and bedrock outcroppings in the southeastern corner of the site. Soil boring to determine the generalized subsurface conditions at the Project site have not yet been conducted, but will be conducted prior to determining the appropriate foundation approach.

4.10.2 Groundwater

Based on Massachusetts Geographic Information System mapping and field observations of the local topography, the local groundwater flow direction is assumed to be to the east toward Dorchester Bay and in the same flow direction as the Neponset River.

The Project is not located in the Groundwater Conservation Overlay District and will therefore not need to comply with the requirements of Article 32 of the City of Boston Zoning Code.

4.11 Construction Impacts

4.11.1 Introduction

A Construction Management Plan (CMP) in compliance with the City's Construction Management Program will be submitted to the BTD once final plans are developed and the construction schedule is fixed. The construction contractor will be required to comply with the details and conditions of the approved CMP.

Proper pre-planning with the City and neighborhood will be essential to the successful construction of the Project. Construction methodologies, which ensure public safety and protect nearby residences and businesses, will be employed. Techniques such as barricades, walkways and signage will be used as appropriate. The CMP will include routing plans for trucking and deliveries, plans for the protection of existing utilities, and control of noise and dust.

During the construction phase of the Project, the Proponent will provide the name, telephone number and address of a contact person to communicate with on issues related to the construction.

The Proponent intends to follow the guidelines of the City of Boston and the MassDEP, which direct the evaluation and mitigation of construction impacts.

4.11.2 Construction Methodology/Public Safety

Construction methodologies that ensure public safety and protect nearby businesses and residents will be employed. Techniques such as barricades and signage will be used. Construction management and scheduling will minimize impacts on the surrounding environment, and will include plans for construction worker commuting and parking, routing plans for trucking and deliveries, and the control of noise and dust.

As the design of the Project progresses, the Proponent will meet with BTD to discuss the specific location of barricades, the need for lane closures, pedestrian walkways, and truck queuing areas. Secure fencing, signage, and covered walkways may be employed to ensure the safety and efficiency of all pedestrian and vehicular traffic flows. In addition, sidewalk areas and walkways near construction activities will be well marked and lighted to protect pedestrians and ensure their safety. Public safety for pedestrians on abutting sidewalks will also include covered pedestrian walkways when appropriate. If required by BTD and the Boston Police Department, police details will be provided to facilitate traffic flow. These measures will be incorporated into the CMP which will be submitted to BTD for approval prior to the commencement of construction work.

4.11.3 Construction Schedule

The Proponent anticipates that the Project will commence construction in the first quarter of 2018 and last for approximately 18-24 months.

Typical construction hours will be from 7:00 a.m. to 6:00 p.m., Monday through Friday, with most shifts ordinarily ending at 3:30 p.m. No substantial sound-generating activity will occur before 7:00 a.m. If longer hours, additional shifts, or Saturday work is required, the construction manager will place a work permit request to the Boston Air Pollution Control Commission in advance. It is noted that some activities such as finishing activities could run beyond 6:00 p.m. to ensure the structural integrity of the finished product; certain components must be completed in a single pour, and placement of concrete cannot be interrupted.

4.11.4 Construction Staging/Access

Access to the site and construction staging areas will be described in the CMP.

Although specific construction and staging details have not been finalized, the Proponent and its construction management consultant will work to ensure that staging areas will be located to minimize impacts to pedestrian and vehicular flow. Secure fencing and barricades will be used to isolate construction areas from pedestrian traffic adjacent to the site. Construction procedures will be designed to meet all Occupational Safety and Health Administration (OSHA) safety standards for specific site construction activities.

4.11.5 Construction Mitigation

The Proponent will follow City of Boston and MassDEP guidelines which will direct the evaluation and mitigation of construction impacts. As part of this process, the Proponent and construction team will evaluate the Commonwealth's Clean Air Construction Initiative.

A CMP will be submitted to BTD for review and approval prior to issuance of a Building Permit. The CMP will include detailed information on specific construction mitigation measures and construction methodologies to minimize impacts to abutters and the local community. The CMP will also define truck routes which will help in minimizing the impact of trucks on City and neighborhood streets.

"Don't Dump - Drains to Neponset River" plaques will be installed at storm drains that are replaced or installed as part of the Project.

4.11.6 Construction Employment and Worker Transportation

The number of workers required during the construction period will vary. It is anticipated that approximately 50 construction jobs will be created over the length of construction. The Proponent will make reasonable good-faith efforts to have at least 51% of the total

employee work hours be for Boston residents, at least 40% of total employee work hours be for minorities and at least 12% of the total employee work hours be for women. The Proponent will enter into jobs agreements with the City of Boston.

To reduce vehicle trips to and from the construction site, minimal construction worker parking will be available at the site, and all workers will be strongly encouraged to use public transportation and ridesharing options. The general contractors will work aggressively to ensure that construction workers are well informed of the public transportation options serving the area. Space on-site will be made available for workers' supplies and tools so they do not have to be brought to the site each day.

4.11.7 Construction Truck Routes and Deliveries

Truck traffic will vary throughout the construction period, depending on the activity. The construction team will manage deliveries to the site during morning and afternoon peak hours in a manner that minimizes disruption to traffic flow on adjacent streets. Construction truck routes to and from the site for contractor personnel, supplies, materials, and removal of excavations required for the development will be coordinated with BTD. Traffic logistics and routing will be planned to minimize community impacts. Truck access during construction will be determined by the BTD as part of the CMP. These routes will be mandated as a part of all subcontractors' contracts for the development. The construction team will provide subcontractors and vendors with Construction Vehicle & Delivery Truck Route Brochures in advance of construction activity.

"No Idling" signs will be included at the loading, delivery, pick-up and drop-off areas.

4.11.8 Construction Air Quality

Short-term air quality impacts from fugitive dust may be expected during demolition, excavation and the early phases of construction. Plans for controlling fugitive dust during demolition, excavation and construction are anticipated to include mechanical street sweeping, wetting portions of the site during periods of high wind, and careful removal of debris by covered trucks. The construction contract will provide for a number of strictly enforced measures to be used by contractors to reduce potential emissions and minimize impacts. These measures are expected to include:

- Using wetting agents on areas of exposed soil on a scheduled basis;
- Using covered trucks;
- Minimizing spoils on the construction site;
- Monitoring of actual construction practices to ensure that unnecessary transfers and mechanical disturbances of loose materials are minimized;

- Minimizing storage of debris on the site; and
- Periodic street and sidewalk cleaning with water to minimize dust accumulations.

4.11.9 Construction Noise

The Proponent is committed to mitigating noise impacts from the construction of the Project. Increased community sound levels, however, are an inherent consequence of construction activities. Construction work will comply with the requirements of the City of Boston Noise Ordinance. Every reasonable effort will be made to minimize the noise impact of construction activities.

Mitigation measures are expected to include:

- Instituting a proactive program to ensure compliance with the City of Boston noise limitation policy;
- Using appropriate mufflers on all equipment and ongoing maintenance of intake and exhaust mufflers;
- Muffling enclosures on continuously running equipment, such as air compressors and welding generators;
- Replacing specific construction operations and techniques by less noisy ones where feasible;
- Selecting the quietest of alternative items of equipment where feasible;
- Scheduling equipment operations to keep average noise levels low, to synchronize the noisiest operations with times of highest ambient levels, and to maintain relatively uniform noise levels;
- Turning off idling equipment; and
- Locating noisy equipment at locations that protect sensitive locations by shielding or distance.

4.11.10 Construction Waste

The Proponent will take an active role with regard to the reprocessing and recycling of construction waste. The disposal contract will include specific requirements that will ensure that construction procedures allow for the necessary segregation, reprocessing, reuse and recycling of materials when possible. For those materials that cannot be recycled, solid waste will be transported in covered trucks to an approved solid waste facility, per

MassDEP Regulations for Solid Waste Facilities, 310 CMR 16.00. This requirement will be specified in the disposal contract. Construction will be conducted so that materials that may be recycled are segregated from those materials not recyclable to enable disposal at an approved solid waste facility.

4.11.11 Protection of Utilities

Existing public and private infrastructure located within the public right-of-way will be protected during construction. The installation of proposed utilities within the public way will be in accordance with the Massachusetts Water Resources Authority, Boston Water and Sewer Commission (BWSC), Boston Public Works, Dig Safe, and the governing utility company requirements. All necessary permits will be obtained before the commencement of the specific utility installation. Specific methods for constructing proposed utilities where they are near to, or connect with, existing water, sewer and drain facilities will be reviewed by BWSC as part of its Site Plan Review process.

4.12 Rodent Control

A rodent extermination certificate will be filed with the building permit application for the Project. Rodent inspection monitoring and treatment will be carried out before, during, and at the completion of all construction work for each phase of the Project, in compliance with the City's requirements.

4.13 Wildlife Habitat

The Project site is in an established urban neighborhood. There are no wildlife habitats in or adjacent to the Project site.

Chapter 5.0

Sustainable Design and Climate Change

5.0 SUSTAINABLE DESIGN AND CLIMATE CHANGE

5.1 Sustainable Design

To comply with Article 37 of the Boston Zoning Code, the Project will be designed and constructed under the guidelines of U.S. Green Building Council's (USGBC) Leadership in Energy and Environmental Design (LEED) for Building Design and Construction (BD+C): Homes (H) Version 4 (V4). The Project is currently targeting to be LEED certifiable at the Silver level.

In the case of four-story multifamily buildings, LEED has a specific set of guidelines to determine whether the project should utilize the LEED for Homes or the LEED for Homes Midrise pathway. New Ecology, the Project's sustainability consultant, reviewed those guidelines and determined that the Project qualifies for use of the LEED for Homes low rise pathway, which corresponds well with the requirement for a Home Energy Rating System (HERS) score necessary to demonstrate compliance with the Massachusetts Stretch Code.

The preliminary LEED for Homes checklist is included at the end of this chapter, and illustrates an overview of the credits the Project anticipates achieving within each LEED category. This is a preliminary evaluation of the LEED checklist, and applicable credits may change as the building design advances.

The following is a detailed credit-by-credit analysis of the Project team's approach to achieving LEED certifiability at the Silver level. Points that are still being studied and marked as "maybe" on the LEED checklist are italicized below.

Integrative Process

<u>IP Integrative Process:</u> The Project includes a comprehensive design team that is composed of the skilled professionals required to comply with this Credit, including architecture, mechanical, electrical, plumbing, building science and performance testing, green building, civil, and landscape architecture specialists. The team is committed to close coordination during the future design development, final design, and construction phases of Project execution.

Location and Transportation

<u>LT Prerequisite – Floodplain Avoidance:</u> The Project site is not located within the FEMA 100-year floodplain.

<u>LT Site Selection:</u> The Project meets the requirements for several of the options provided under this credit

- Option 1 Path 1 Previously Developed: The entire Project site is previously developed, exceeding the 75% requirement. The Project site currently consists of three buildings and surface parking.
- Option 2 Infill Development: The Project site is located within a one-half mile from previously developed land. The Project site is located in a densely populated area of Boston.
- Option 3 Open Space: The Project site is located within a half-mile of Dorchester Park.
- Option 5 Bicycle Network and Storage: The Project will comply with City of Boston bicycle storage requirements. It will include 57 covered and protected bicycle spaces, as well as three short term bicycle parking spots. Residents will be within a 176-yard walk/bike of Dorchester Avenue, which is a bike friendly roadway and connects to a large variety of biking paths, services, and amenities.

<u>LT Compact Development:</u> The Project has a density of 51 units per acre, exceeding the 20 unit per acre requirement.

<u>LT Community Resources</u>: The Project site has significant access to community resources. The Project easily meets the credit requirement of 12 uses and qualifies for one exemplary performance credit. The nearby resources include, but are not limited to:

- Star Market Grocery 0.1 mile
- RTN Federal Credit Union 0.2 miles
- Meeting House Bank 0.2 miles
- CVS 0.2 miles
- Rite-Aid 0.3 miles
- Harbor Health Services 0.3 miles
- Carney Hospital 0.4 miles
- A large number of restaurants (over 15) in a 0.5-mile radius
- Dorchester Park 0.4 miles
- Willian G. Walsh Playground 0.3 miles
- Milton Hill Sport and Spa Health Club 0.3 miles
- US Post Office 0.3 miles
- Eclipse Salon 0.3 miles
- Milton Village Hardware 0.3 miles
- St. Gregory Grammar School 0.2 miles
- Conservatory Lab Charter School 0.4 miles
- Boston Youth Sanctuary 0.2 miles
- St. Gregory Parish 0.2 miles
- Wesley United Methodist Church 436 feet

<u>LT Access to Transit</u>: The Project site is located within a seven-minute walk (0.3 miles) of the Mattapan High-Speed line at the Milton Station as well as multiple bus routes that will meet the ride frequency requirement of this credit.

Sustainable Sites

<u>SS Prerequisite – Construction Activity Pollution Prevention:</u> The construction documents will include a Soil Erosion Sedimentation Control Plan to be developed in accordance with the EPA Construction General Permit of the National Pollutant Discharge Elimination System (NPDES). A Stormwater Pollution Prevention Plan (SWPPP) will also be developed for the site in accordance with the requirements for the EPA's NPDES Construction General Permit. These documents will be used to show compliance with this prerequisite.

<u>SS Prerequisite – No Invasive Plants:</u> The Project team is committed to meeting this prerequisite and complying with United States Department of Agriculture's Germplasm Resources Information Network (GRIN) Taxonomy for Plants database, the National Association of Exotic Pest Plant Council, or the UMass Extension school invasive plant list. The Project team includes a Massachusetts licensed landscape architect that will adhere to these guidelines during design.

<u>SS Nontoxic Pest Control</u>: The Project will comply with this credit by using solid concrete foundation walls and sealing all external cracks, joints, penetrations and entry points. *The Project team will investigate incorporating additional features as the design progresses.*

Water Efficiency

<u>WE Prerequisite – Water Metering:</u> The Project will comply with the requirements of this credit by installing a water meter for each unit within the development.

<u>WE Indoor Water Use:</u> The Project will reduce demand for water through high efficiency fixtures and efficient landscaping practices. The design will specify fixtures that will achieve the following flow rates:

- Shower: 1.5 GPM
- Bath Lavatory: 1.0 GPM
- Toilet: 0.8 GPF
- Clothes washers: Energy Star certified

<u>WE Outdoor Water Use:</u> The Project will reduce demand for water through water conserving landscape design. Less than 40% of the vegetated site area will be composed of turf, which includes the planted roof areas, and more than 50% of the planted areas will be planted with native/adaptive species.

Energy and Atmosphere

<u>EA Prerequisite – Minimum Energy Performance:</u> The Project will comply with this prerequisite by:

- Meeting the requirements of Energy Star for Homes, Version 3 and achieving a HERS index of, at most, 55. This will be achieved through strategies that include above code levels of insulation in the cavity as well as continuous exterior of the sheathing, very high efficiency unit-based mechanical systems, LED lighting and controls, Energy Star appliances, and Smart Home systems that reduce unnecessary consumption when a unit is unoccupied. The team also plans to utilize efficient technologies and design to mitigate common area energy and water consumption, including integration of a PV system to offset the common area electric loads.
- Specifying Energy Star certification for all refrigerators, dishwashers, and clothes washers
- Fully ducting all duct runs.

<u>EA Prerequisite – Energy Metering:</u> The Project will sub meter every unit for electrical and gas consumption.

<u>EA Prerequisite – Education of the Homeowner, Tenant or Building Manager:</u> The Project team will provide to the owner an operations and maintenance manual outlining all LEED/sustainability related requirements.

<u>EA Annual Energy Use:</u> The Project will achieve additional energy savings beyond the prerequisite requirements. At this stage of design, it is anticipated that the Project will achieve a HERS score of 55 or less (16 points). The Project achieves an additional 10 points for units smaller than the baseline per the USGBC home size adjustment.

<u>EA Efficient Hot Water Distribution System:</u> The Project will consider insulating all hot water piping to a minimum of R-4.

<u>EA HVAC Start-up Credentialing:</u> The Project team will consider requiring that the HVAC subcontractors have the H-QUITO credential and complete the Energy Star for Homes, Version 3, HVAC system quality installation contractor checklist.

Materials and Resources

<u>MR Prerequisite – Certified Tropical Wood:</u> Every effort will be made to avoid using tropical woods, or if tropical woods are used, FSC Certified woods will be specified.

<u>MR Prerequisite – Durability Management:</u> The Project will promote durability and performance of the building enclosure and its components and systems through appropriate measures as outlined by the USGBC including:

- Use of non-paper faced backer board in specific bath areas;
- Use of water resistant flooring in kitchen and baths; and
- Design and install drain pan and automatic water shutoff valve.

<u>MR Durability Management Verification:</u> Through the process of complying with the Energy Star Version 3 requirements, a third-party verifier will confirm compliance with the water management system builder checklist.

<u>MR Environmentally Preferable Products</u>: The Project will minimize its environmental impact through thoughtful selection of materials. The Proponent will specify local aggregate and recycled content drywall, and will investigate additional options for points in this section during the design process.

<u>MR Construction Waste Management</u>: The Proponent is committed to reducing construction waste at least ten percent below USGBC's baseline, and will strive for a 30% reduction target.

Indoor Environmental Quality

<u>EQ Prerequisite – Ventilation:</u> The unit designs will meet all requirements of ASHRAE Standard 62.2-2010 (with errata). Each unit will have kitchen and bath exhaust as required by the Standard. In addition, fresh air will be mechanically supplied directly to each unit. The team will engage in an integrated design process with the mechanical engineer to analyze the cost/benefit of unit-based heat recovery ventilation systems with smart control capacity to mitigate the energy impact of ventilation. All non-unit spaces will be designed to meet the requirements of ASHRAE 62.1-2010, Sections 4-7.

<u>EQ Prerequisite – Combustion Venting:</u> The Project will only install sealed combustion equipment and will install CO monitors in each unit.

<u>EQ Prerequisite – Garage Pollutant Protection:</u> The Project design will ensure complete separation and air sealing of living spaces from the underground garage. No duct work will run in the garage space, and the garage will be mechanically ventilated to further reduce the potential for CO contamination to the living areas.

<u>EQ Prerequisite – Radon Resistant Construction</u>: The Project site is located in EPA radon zone 2, which does not require a mitigation system. Additionally, the living spaces will be separated by a mechanically ventilated garage, which will further mitigate any potential radon issues.

<u>EQ Prerequisite – Air Filtering:</u> The Project will install MERV 8 filters on the return side of the air handling equipment in each unit. Additionally, the outdoor supply air provided to each unit will be filtered by MERV 6 filters, at minimum. The specifics of the system chosen for outdoor air will dictate whether a higher MERV rating is feasible and appropriate.

<u>EQ Prerequisite - Environmental Tobacco Smoke:</u> The building will be entirely nonsmoking, including individual units. A designated outdoor smoking area will be the only area on site where smoking is permitted, and it will be located at least 25 feet from entries, air intakes and operable windows.

<u>EQ Prerequisite – Compartmentalization:</u> A comprehensive set of air sealing details and specifications will be developed during the design process to set expectations and approaches around unit compartmentalization. A third-party testing agent will be used to verify that the constructed building complies with LEED infiltration requirements.

<u>EQ Enhanced Ventilation:</u> As the mechanical system design progresses, the Project team evaluate the approach for ventilation of the units, and will consider systems that would qualify the Project for these enhanced ventilation points.

<u>EQ Contaminant Control:</u> The Project may include compliant walk-off mats at each primary entrance into the building that meet the 10-foot requirement. For units with direct entry, a shoe removal and storage space that is separated from the living space may be included.

EQ Balancing of Heating and Cooling Distribution Systems: The Project will comply with Option 3. *Per the requirements of Energy Star Version 3, pressure testing of the forced air system will be done to ensure no more than a 3Pa differential between any bedroom and the rest of the unit.*

<u>EQ Enhanced Compartmentalization:</u> The Project team will strive to comply with this credit.

<u>EQ Combustion Venting</u>: The Project will not install fireplaces or wood stoves in any of the units.

<u>EQ Enhanced Garage Pollutant Protection:</u> The Project will strive to follow the requirements of ASHRAE 62.1–2010. The garage will be exhausted sufficiently to create negative pressure with respect to adjacent spaces with the doors to the garage closed. The Project will provide self-closing doors and deck-to-deck partitions or a hard lid ceiling. The pressure differential with the surrounding spaces will be at least 5 Pascal's (Pa) (0.02 inches of water gauge) when all doors are closed.

<u>EQ Low Emitting Products:</u> The Project team will specify paints, coatings, flooring, adhesives, and sealants that comply with California Department of Public Health Standard Method V1.1–2010, using CA Section 01350, Appendix B, New Single-Family Residence Scenario.

Innovation in Design

<u>ID Prerequisite – Preliminary Rating:</u> In preparation for this submission, the Project team met with New Ecology to set greening goals and vet strategies for achieving compliance. From this process, the team developed the preliminary LEED checklist and this narrative.

<u>ID Exemplary Performance</u>: The Project will qualify for exemplary performance points for the Site Selection credit, the Compact Development credit, and the Community Resources credit.

<u>ID LEED Accredited Professional:</u> Paul Eddowes, LEED AP, is coordinating the Article 37 Compliance process and LEED certifiability for this project.

Regional Priority

Regional Priority Credits (RPCs) are established LEED credits designated by the USGBC to have priority for a particular area of the country. When a Project team achieves one of the designated RPCs, an additional credit is awarded to the Project. RPCs applicable to the site include: LT Community Resources, LT Access to Transit, and SS Non-Toxic Pest Control.

5.2 Climate Change Resilience

5.2.1 Introduction

Projects subject to Article 80B, Large Project Review, are required to complete the Climate Change Preparedness Checklist. Climate change conditions considered by the Project team include higher maximum and mean temperatures, more frequent and longer extreme heat events, more frequent and longer droughts, more severe freezing rain and heavy rainfall events, and increased wind gusts.

The expected life of the Project is anticipated to be approximately 50 years. Therefore, the Proponent planned for climate-related conditions projected 50 years into the future. A copy of the Climate Change Checklist is included in Appendix D.

5.2.2 Extreme Heat Events

The *Climate Ready Boston* report predicts that in Boston, there may be between 25 to 90 days over 90 degrees by 2070, compared to an average of 11 days per year over 90 degrees between 1971 to 2000. The Project design will incorporate a number of measures to minimize the impact of high temperature events, including:

- Installing a high-performance building envelope and high-performance HVAC equipment;
- New street trees;
- Significant new landscaped areas;
- Installing operable windows where possible; and
- Installing a vegetated roof to minimize the heat island effect.

5.2.3 Rain Events

As a result of climate change, the Northeast is expected to experience more frequent and intense storms. To mitigate the impacts of these events, the Proponent will take measures to minimize stormwater runoff at the Project site, and protect the Project's mechanical equipment, as necessary. The performance capabilities of the proposed stormwater management system are anticipated to significantly improve the site's infiltration capacity. Stormwater measures will include:

- Decreasing stormwater runoff from the site;
- Water tight utility conduits; and
- Wastewater and stormwater back flow prevention.

5.2.4 Drought Conditions

Although more intense rain storms are predicted, extended periods of drought are also predicted due to climate change. Under the high emissions scenario, the occurrence of droughts lasting one to three months could go up by as much as 75% over existing conditions by the end of the century. To minimize the Project's susceptibility to drought conditions the landscape design is anticipated to incorporate native and adaptive plant materials which require low or no irrigation and are known for their ability to withstand adverse conditions. Plumbing fixtures will be specified to achieve a reduction in water use through low-flow water-closets, low-flow showers, and low-flow sinks.

5.3 Renewable Energy

The Proponent is evaluating the potential for a roof-mounted solar photovoltaic (PV) system, and anticipates installing solar panels on the roof to produce energy to support the common areas of the building. The feasibility of installing a solar PV system will depend on the incentives available at the time of construction, and the ability of the Proponent to take advantage of these benefits.



LEED v4 for Building Design and Construction: Homes

Credit Space Heating & Cooling Equipment

Project Checklist

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6	SCR					Date:				4/4/2017	
Y	?	Ν									
1			Credit	Integrative Process	2						
			-							EA PRESCRIPTIVE PATH (continued)	
15	0	15	Location	and Transportation	15				Credit	Heating & Cooling Distribution Systems	3
Y			Prereq	Floodplain Avoidance	Required				Credit	Efficient Domestic Hot Water Equipment	3
				PERFORMANCE PATH					Credit	Lighting	2
		15	Credit	LEED for Neighborhood Development Location	15				Credit	High Efficiency Appliances	2
			-	PRESCRIPTIVE PATH					Credit	Renewable Energy	4
8			Credit	Site Selection	8				-		
3			Credit	Compact Development	3	1	3.5	5.5	Material	s and Resources	10
2			Credit	Community Resources	2	Y			Prereg	Certified Tropical Wood	Required
2	-		Credit	Access to Transit	2	Y			Prereg	Durability Management	Required
_					-		1		Credit	Durability Management Verification	1
4	4	5	Suctains	ship Sites	7	0.5	1	2	Credit		1
	1	5	Sustaina			0.5	1.5	2	Credit		4
Y			Prereq	Construction Activity Pollution Prevention	Required	0.5	1	1.5	Credit	Construction Waste Management	3
Y	<u> </u>		Prereq	No Invasive Plants	Required			2	Credit	Material Efficient Framing	2
		2	Credit	Heat Island Reduction	2						
		3	Credit	Rainwater Management	3	4.5	6.5	3	Indoor E	nvironmental Quality	16
1	1		Credit	Non-Toxic Pest Control	2	Y			Prereq	Ventilation	Required
						Y			Prereq	Combustion Venting	Required
5	3	2	Water Ef	fficiency	12	Y			Prereq	Garage Pollutant Protection	Required
Y			Prereq	Water Metering	Required	Y			Prereq	Radon-Resistant Construction	Required
	-			PERFORMANCE PATH		Y			Prereq	Air Filtering	Required
			Credit	Total Water Use	12	Y			Prereq	Environmental Tobacco Smoke	Required
			_	PRESCRIPTIVE PATH		Y			Prereq	Compartmentalization	Required
3	3		Credit	Indoor Water Use	6		3		Credit	Enhanced Ventilation	3
2		2	Credit	Outdoor Water Use	4		0.5	1.5	Credit	Contaminant Control	2
						1	1		Credit	Balancing of Heating and Cooling Distribution Systems	3
26	5	7	Energy	and Atmosphere	38		1		Credit	Enhanced Compartmentalization	1
			Prereg	Minimum Energy Performance	Required	2			Credit	Enhanced Computation Venting	2
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			Drorog	Energy Metering	Required	1.5		1 5	Credit		2
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	2	3	Credit	Efficient Hot water Distribution System	5	3			Credit		5
		2	Credit	Advanced Utility I facking	2	1			Credit	LEED AF HOMES	1
		1	Credit	Active Solar Ready Design	1			1.	-		
	1		Credit	HVAC Start-Up Credentialing	1	3	0	0	Regiona	I Priority	4
				PRESCRIPTIVE PATH		1			Credit	Regional Priority: Access to Transit	1
Y		_	Prereq	Home Size	Required	1			Credit	Regional Priority: Community Resources	1
			Credit	Building Orientation for Passive Solar	3	1			Credit	Regional Priority: Nontoxic Pest Control	1
			Credit	Air Infiltration	2				Credit	Regional Priority: Specific Credit	1
			Credit	Envelope Insulation	2						
			Credit	Windows	3	59.5	10	38	TOTALS		Possible Points: 110

4

Certified: 40 to 49 points, Silver: 50 to 59 points, Gold: 60 to 79 points, Platinum: 80 to 110

1120-1132 Washington St.

Chapter 6.0

Urban Design

6.0 URBAN DESIGN

6.1 Architecture and Landscape Design

The proposed Project consists of a four-story residential building with approximately 3,600 sf of commercial space on the ground floor. The mix of land uses surrounding the Project site, located in the Lower Mills neighborhood of Dorchester, include two and three-story residential buildings, the Lower Mills Branch of the Boston Public Library, and a commercial district with restaurants, cafés, and shops. The building footprint has the longest leg of the structure along the southerly property line, adjoining the Dolan Funeral Home parking lot and a small, off site, wooded cluster. This retracts the building back away from the three adjoining residences fronting on Richmond Street to the north.

The building has been designed to complement and respect the existing buildings surrounding the site. The mansard roof on the fourth level not only compliments the characteristics of the neighboring buildings, but also helps reduce the height of the building. The decorative dental moldings under the soffits along with the decorative columns tie the Project in with the rich details incorporated in the surrounding buildings, including the Baker Chocolate Factory Apartments on Adams Street. The red brick that will be used on the first level of the building, as well as the walkways, are similar to materials found in many of the buildings in Lower Mills (see Figure 6-1). The large aluminum glass storefront windows and doors on the first level will bring natural light and ventilation into the spaces to make them welcoming and inviting to both the residents of the building and the local neighborhood.

The Project contains five open space components and three surface parking areas. The proposed planting in each area provides a spatial context for the building. The shrub foundation plantings provide scale transition from the vertical building walls to the horizontal ground plane. The parking for the Project is divided up into a series of bays which are visually separated by building components and proposed natural features. All proposed plantings will be selected to generate seasonal interest and to minimize maintenance.

The first open space area is at the front of the building, along Washington Street, and consists of a lawn apron along the existing sidewalk and paver walkways leading to the building entry points (see Figure 6-3). There will be a blend of deciduous and evergreen shrubs in a foundation planting along the building front to transition from the vertical building to the horizontal ground plane. This design replicates the character of the existing lawn areas currently on the site. There are granite bollards flanking some of the existing walkway entries which will be reused and/or replicated at the walkway entries for the new building. Low level ornamental pole lighting will also be introduced along the



1120-1132 Washington Street Boston, Massachusetts







1120-1132 Washington Street Boston, Massachusetts



existing sidewalk. Appropriate deciduous street tree plantings are proposed in locations that do not conflict with visual access to the two commercial spaces on the ground floor at the front of the building. The combination of bollards, lighting, and street trees will provide a safe and inviting pedestrian environment in this location.

The area on the northerly side of the Project site contains the access drive, parking, and two of the open space components (see Figure 6-4). A small private open space area is proposed in the northwest corner of the site. This open space will consist of a lawn area for small scale informal play and a small play area for toddlers. There will also be a patio area with benches and a trash receptacle, where the residents can sit in the shade of the trees and relax; perhaps while tending to their toddler on the play sculpture. Deciduous and evergreen shrub and tree plantings will be introduced to screen the area from surrounding uses and to provide a natural setting with seasonal interest. This open space will be accessed via a crosswalk across the access drive linked to the building's pedestrian circulation system. This open space will be enclosed by an ornamental fence on the sides abutting adjoining properties and with an ornamental metal fence, with gated access, along the Project access drive. This open space will be for use during the daylight hours and will be secured overnight. The eight commercial parking spaces opposite the drive from the open space are tucked in under the building where they will be less visible.

The third open space component lies along the northerly side of the building where the structure steps back from the property line to provide a separation from the existing residential uses abutting the site. This open space area is configured as linear commons space. Three of the three-bedroom residential units will front onto the commons, and each will have partially enclosed patio space within the commons area. The commons will be enclosed on all open sides with an ornamental metal fence with gated access. A walkway providing pedestrian access for the parking area along the commons will be provided if the site grading permits; otherwise that area will be devoted to open space. The commons will provide a small linear lawn area flanked by deciduous and evergreen trees and shrubs. The trees will provide shade to cool pavement and parked cars, vegetation mass to help break views of the building into a series of smaller scaled segments, and seasonal interest. Low level ornamental pole lighting may either be located along the parking edge of the commons or along the narrow open space strip near the proposed opaque fencing along the property line adjacent the access drive. This segment of fencing will completely screen vehicular movements from the three adjoining houses, which front onto Richmond Street. The residential parking will be separated from the commercial parking by gated access in this location.

The fourth open space area lies along the back of the property, which parallels the existing Lower Mills Branch library. This component will serve primarily as a visual element with the capacity for on-site snow storage. There will be opaque fencing along the property lines coupled with evergreen shrubs on the Project side of the fence along the back property line.


1120-1132 Washington Street Boston, Massachusetts



Deciduous trees will be planted to provide shade and seasonal interest. There will be low level ornamental pole lighting for the parking located in this open space area. The parking here is in a conventional double loaded bay configuration with the access drive continuing on to provide ramp access to the parking in the basement level.

The fifth open space component consists of a lane along the Dolan Funeral Home on the southerly side of the Project site. This lane includes a paver walkway and deciduous trees to break up the views of the building's southern elevation. Some shrubs may also be utilized, where space permits. An opaque ornamental fence will run along the entire property line to visually separate the Project site from the adjoining funeral home. There is currently a large evergreen tree in a planter adjacent to the Project site at the adjoining front corner of the Funeral Home parking lot. The tree does not appear be healthy; if the tree fails, the Proponent will work with the Dolan Funeral Home to provide a replacement tree, at the Proponent's expense, to help maintain the natural setting provided by a tree in this location.

6.2 Evolution of Design

The initial design yielded a more contemporary building, set further back from Washington Street. The vehicular access occurred on the southerly side along the street frontage, adjacent the Dolan Funeral Home. The corresponding parking was located in front, on the street side, of the proposed building. However, the contemporary building design and location was not well received by the Lower Mills community. The community commented that the proposed vehicular access point was in a location where traffic consistently backed up from the traffic light just to the south of the Funeral Home, and that the building should be moved so that it fronts the street.

The present site and building design respond to these concerns expressed by the community. The building has been moved forward to front on Washington Street with a setback that is consistent with existing surrounding buildings. The vehicular access, off Washington Street, has been shifted to the northwesterly side of the site, allowing for more favorable conditions for turning traffic from the site onto Washington Street. Parking has been divided up into a series of smaller scaled lot areas, to the side and rear of the proposed building, leaving the front for open space streetscape amenities.

Chapter 7.0

Historic and Archaeological Resources

7.0 HISTORIC AND ARCHAEOLOGICAL RESOURCES

The Historic and Archaeological Resources section describes the historic and archaeological resources within and in the vicinity of the Project site.

7.1 Project Site

The Project site is located within the Washington Street 1107-1140 Area (MHC # BOS.IA) and the Lower Mills West Area (MHC # BOS.IA) which are both included in the Inventory of Historic and Archaeological Assets of the Commonwealth (Inventory). The Washington Street 1107-1140 Area is a small residential, institutional, and commercial district located at the southerly end of Washington Street near the point where it joins Adams Street and River Street. The area is characterized by Georgian, Federal and Greek Revival residential properties constructed between roughly 1740 and 1870. The properties feature broad proportions, classical forms and classical detailing. The boundaries of the Lower Mills West Area more or less adhere to the inhabited extents of the area shown on the 1850 map of Dorchester. The roughly 45-acre area retains the visual image of an early 19th century industrial village. The majority of the area's historic properties are located southwest of Morton Street, to the west of the Project site.

1126 Washington Street

One building within the Project site is included in the Inventory of Historic and Archaeological Assets of the Commonwealth (Inventory). The building is the George Haynes House (BOS.6382), more commonly known as the John G. Molloy Funeral Home at 1126 Washington Street. Believed to be constructed during the mid-eighteenth to mid-nineteenth century, the building is identified on the inventory form as a five bay Georgian house with a later pedimented gable added during the Greek Revival Period. Boston building permits indicate that the property was altered in 1957 with the introduction of aluminum siding. In 1986, a new roof was installed. In addition, a one-story wing was added to the north side of the residence.

1120 Washington Street

This two-story Greek Revival residence was constructed after 1850. The building features a pedimented front gable roof, and has been altered with the addition of vinyl siding and replacement windows. Boston City Permits indicate that the slate roof of the residence was removed in 1962. In addition, an associated barn was razed in 1947 due to its unsound condition.

1132/1130R Washington Street

This three-story, wood frame, late nineteenth century multi-family residential block located at 1132 Washington Street is capped by a flat roof. The building has been altered by the introduction of vinyl siding and replacement windows. The residential block spans the lot line with a two-story multi-family residential block (1130R Washington Street) to the rear. The rear block features a mansard roof with dormers and two-story bay windows. Like 1132 Washington Street, the rear block has been significantly altered with the introduction of vinyl siding and replacement windows.

7.2 Historic Resources Within the Vicinity of the Project Site

The Project site is located within and in the vicinity of two historic resources listed in the State and National Registers of Historic Places. Table 7-1 identifies the resources within one-quarter mile of the Project site, and corresponds to resources depicted in Figure 7-1.

Historic Resource	Address	Designation*
Dorchester-Milton Lower Mills	Boston: Follows Adams, River and	NRDIS
Industrial District	Medway Streets and Millers Lane	
	Milton: Follows Eliot and Adams	
	Streets	
Dorchester Park	Roughly bounded by Dorchester	NRIND
	Avenue, Richmond, Adams, and	
	Richview Streets.	
Individually listed on the National Re	gister of Historic Places	
National Register of Historic Places h	istoric district	

Table 7-1Historic Resources in the Vicinity of the Project Site

7.3 Archaeological Resources Within the Project Site

A review of Massachusetts Historical Commission's (MHC) online archaeological base maps was conducted on March 9, 2017. It found that the Project site is within the mapped extents of site 19-SU-28. As the proposed Project involves construction on areas of the Project site previously excavated, disturbed and then developed, impacts to archaeological resources are not anticipated. As the Project advances, the Proponent will consult with MHC in accordance with M.G.L., Chapter 9, Sections 26-27C (50 CMR 71.00), as necessary, to assess potential impacts to significant historic and archeological resources. If impacts associated with the Project are unavoidable, the Proponent with work with MHC and interested parties in developing appropriate measures to mitigate Project impacts to those resources.



1120-1132 Washington Street Boston, Massachusetts



7.4 Potential Impacts to Historic Resources

7.4.1 Demolition of Existing Buildings

The proposed Project will require the demolition of the three existing buildings within the Project site. None of the buildings are listed or have been found to be eligible for listing on the National Register of Historic Places. Additionally, all of the buildings have had some level of alteration, such as new roofs, replacement windows, and vinyl siding. The Boston Landmarks Commission (BLC) will be afforded the opportunity to review the proposed demolition through the Article 85 Demolition Delay review process.

7.4.2 Urban Design

The proposed Project consists of a four-story residential building with approximately 3,600 square feet of commercial space on the ground floor. The area surrounding the Project site, located in the Lower Mills neighborhood of Dorchester, contains a mix of uses, including two to three-story residential buildings as well as some commercial uses. The proposed building will have varied elevations with different setbacks and elements that are characteristic of the nearby buildings and neighborhoods.

The proposed building has been designed to complement and respect the existing buildings surrounding the site, but is executed in a manner that clearly reads as new. The mansard roof on the fourth level not only compliments the characteristics of the neighboring buildings, but also helps reduce the height of the building. The decorative dental moldings under the soffits along with the decorative columns tie in with the rich details incorporated in the surrounding buildings, and the red brick that will be used on the first level of the building, as well as the walkways, are similar materials found in many of the buildings in Lower Mills. The large aluminum glass storefront windows and doors on the first level will bring natural light and ventilation into the spaces to make them welcoming and inviting to both the residents of the building as well as the local neighborhood.

7.4.3 Visual Impacts to Historic Resources

While the Project site is located in the vicinity of two historic resources, the Dorchester-Milton Lower Mills Industrial District and Dorchester Park which are listed in the State and National Registers of Historic Places, the proposed four-story Project is not anticipated to have adverse visual impacts to historic resources. The Project is similar in height to other buildings in the area, and the building has been designed to complement and respect the existing buildings surrounding the site. The mansard roof not only compliments the characteristics of the neighboring buildings, but also helps reduce the height of the building. The Project is in keeping with the architectural character of the surrounding neighborhood.

7.5 Consistency with Other Historic Reviews

7.5.1 Boston Landmarks Commission Article 80 Review

The submission of this PNF initiates review of the Project by the BLC under the City's Article 80 Review process.

7.5.2 Boston Landmarks Commission Article 85 Review

The proposed demolition of the existing buildings on the Project site, including 1120 Washington Street, 1126 Washington Street, and 1130R/1132 Washington Street will be subject to review by the BLC under Article 85 of the Boston Zoning Code. An Article 85 Application for each property will be submitted to the BLC.

7.5.3 Massachusetts Historical Commission

The MHC has review authority over projects requiring state funding, licensing, permitting and/or approvals that may have direct or indirect impacts to properties listed in the State Register of Historic Places. As the Project will require an 8(m) permit from the Massachusetts Water Resources Authority (MWRA), an MHC PNF will be filed to initiate the State Register Review process.

Chapter 8.0

Infrastructure

8.0 INFRASTRUCTURE

This Chapter describes the existing sewer, water, and drainage systems surrounding the Project site, and explains how these systems will service the development. The analysis also discusses any anticipated Project-related impacts on the utilities, and identifies mitigation measures to address these potential impacts. The Project is in the early design stages and as the design evolves, the Proponent will coordinate with the various utility companies to ensure full services for the new development.

The construction of the Project is expected to result in the disturbance of an acre or more of earth. A Notice of Intent will be filed under the Environmental Protection Agency's 2017 Construction General Permit. A Stormwater Pollution Prevention Plan (SWPPP) will be prepared, specifying best management practices (BMPs) for protecting the existing stormwater drainage system during construction. A copy of the SWPPP and EPA tracking number will be copied to the Boston Water and Sewer Commission (BWSC).

The Massachusetts Water Resources Authority (MWRA) maintains water distribution lines in Washington Street. An 8(m) permit will be requested from the MWRA to allow construction within their easement.

A Site Plan will be submitted to BWSC requesting abandonment of existing water and sewer services, and construction of the new connections. A Drainage Discharge Permit Application will be submitted to BWSC if construction dewatering is anticipated. The Contractor will file a General Service Application with BWSC to allow the water and sewer work, and file a hydrant meter permit if water is needed during construction.

8.1 Wastewater

8.1.1 Existing Sanitary Sewer System

The BWSC owns and maintains a separated sewer system in the area. There is a 15-inch storm drain and 12-inch sanitary sewer in Washington Street. BWSC's existing sewer system is shown in Figure 8-1.

There are four existing buildings located on the Project site with 1130 and 1132 Washington Street sharing a party wall. The estimated wastewater flow generated by existing uses in these buildings is 2,820 gallons per day (gpd) as shown in Table 8-1. Wastewater flows are based on the wastewater flow estimates provided in 310 CMR 15.00-The State Environmental Code, Title 5.



1120-1132 Washington Street Boston, Massachusetts



Use	Quantity	Wastewater Generation Rate	Total gpd		
1120 Washington	Street				
Two Family	5 bedrooms	110 gpd/bedroom	550		
1126 Washington	Street				
Funeral Home	5,335 sf	75 gpd/1,000 sf ¹	400		
1130 Washington	Street				
Two Family	8 bedrooms	110 gpd/bedroom	880		
1132 Washington	Street				
Three Family	9 bedrooms	110 gpd/bedroom	990		
Total Estimated Ex	kisting Wastewater Flow		2,820 gpd		

Table 8-1 Estimated Existing Wastewater Flows

¹Assumed wastewater generation rate.

8.1.2 Project-Generated Wastewater Generation

The Project will generate an estimated 12,060 gpd, resulting in an estimated net flow increase of 9,240 gpd over existing conditions. Proposed wastewater flows are based on design wastewater flow rates provided in 310 CMR 15-The State Environmental Code, Title 5 as summarized in Table 8-2.

Table 8-2Project Wastewater Generation

Use	Quantity	Wastewater Generation Rate	Total gpd
Multi-Family	108 bedrooms	110 gpd/bedroom	11,880
Retail	3,600 sf	50 gpd/1,000 sf	180
Total Estimated Pr	roject Wastewater Gener	ation	12,060 gpd

8.1.3 Sanitary Sewer Connection

The proposed sanitary sewer line from the new building will connect to the 12-inch sanitary sewer in Washington Street. The garage floor drains will be routed through a gas/oil separator prior to tying into the building's sanitary sewer service.

8.2 Water System

8.2.1 Existing Water Service

BWSC owns and maintains a 16-inch cement-lined, ductile iron water main in Washington Street that is part of the Southern High distribution system. They also maintain an existing hydrant located across the street from the site (H98). The MWRA owns two water distribution pipelines in Washington Street, a 24-inch pit cast iron pipe and a 48-inch cement-lined, cast iron pipe. BWSC's water system map is shown on Figure 8-2.

8.2.2 Proposed Water Service

The proposed building will have separate domestic water and fire protection services. Both will connect to the BWSC's 16-inch water main in Washington Street. Water meters will be of a type approved by BWSC and tied into the BWSC's Automatic Meter Reading (AMR) System. Fixture counts and water meter sizing information will be provided to the BWSC, and services will be designed and coordinated with the BWSC, as part of the Site Plan Review process and General Service Application. The fire protection service will be provided with a backflow prevention device that will be approved though BWSC's Enforcement Section. The location of hydrants and siamese connections will be reviewed by BWSC and the Boston Fire Department (BFD) during the design development phase of the Project.

8.2.3 Anticipated Water Consumption

The Project's estimated water consumption is based on the Project's estimated sewage generation, plus a factor to account for consumption, system losses, and other usages. The total estimated water demand is 13,266 gpd. A more detailed water demand calculation will be submitted to BWSC as part of the Site Plan Review process.

8.2.4 Water Supply Conservation and Mitigation Measures

To help conserve water and reduce the amount of wastewater generated by the Project, the Proponent will investigate the use of water conservation devices such as low-flow toilets and urinals in the residences, flow-restricting faucets in residences and commercial spaces, and sensor operated sinks, toilets, and urinals in commercial spaces consistent with the Proponent's compliance at the LEED Certifiable threshold and in compliance with all pertinent Code requirements.



1120-1132 Washington Street Boston, Massachusetts



8.3 Storm Drainage System

8.3.1 Existing Storm Drainage System

Runoff from a majority of the rooftops and the front third of the site appear to drain towards Washington Street where it is picked up by catch basins in the street, which tie into the 15inch storm drain in Washington Street. The back portion of the site appears to pond within the existing paved surface lot, overflowing to northeasterly properties in large storm events.

8.3.2 Proposed Storm Drainage System

It is anticipated that a large portion of the roof will be vegetated, and the remaining rooftop runoff will be directed to a subsurface infiltration system capable of infiltrating the first inch of runoff from the roof. Runoff from pavement areas will primarily be captured by deepsump catch basins before being routed to either a subsurface infiltration system or water quality unit and detention system. The system will be designed to treat the first inch of runoff, and remove 80% of the total suspended solids. Overflows from larger storm events are expected to be directed to BWSC's 15-inch storm drain in Washington Street. The detailed design of the system will depend on the location of bedrock and groundwater and will be submitted to BWSC as part of the Site Plan Review process.

8.3.3 Water Quality and Construction Stormwater Management

The Project will not impact the water quality of nearby water bodies. The Project proposes a stormwater management program, designed in compliance with MassDEP Stormwater Management Standards for Redevelopment, which will provide pretreatment and infiltration, if feasible, prior to discharging stormwater to the drainage system. An operation and maintenance plan will be developed to support the long-term functionality of the proposed stormwater management system.

A SWPPP will be prepared for the Project. Stormwater pollution prevention measures will include good housekeeping such as properly storing materials, spill prevention and response plans, and proper storage and disposal of solid wastes. Erosion and sediment controls will be used during construction to protect adjacent properties, the storm drain system, and the nearby surface waters. The Contractor will be responsible for controlling dust using street sweeping, watering and other means as necessary.

8.3.4 City of Boston Groundwater Overlay District

The Project site is not located within the City of Boston's Groundwater Conservation Overlay District.

8.4 Electrical Service

Eversource owns and maintains the electrical transmission system in the vicinity of the Project. There are underground conduits in Washington Street, and overhead wires in the back of the site. The electrical power supply design and loads for the building will be coordinated with Eversource during the design phase. The Proponent is investigating energy conservation measures, including solar panels, and energy efficient lighting and heating and cooling systems for the Project.

8.5 Natural Gas

National Grid provides natural gas in the Project area, and owns and maintains a gas main in Washington Street. The building is expected to be provided with a new gas service. The size and location will be coordinated with National Grid during the detailed design phase of the Project.

8.6 Telecommunications Systems

Verizon and Comcast provide cable and telephone services in the Project area. It is anticipated that cable service to the proposed building will be underground from Washington Street.

8.7 Utility Protection During Construction

The Contractor will notify utility companies and call "Dig Safe" prior to excavation. During construction, infrastructure will be protected using sheeting and shoring, temporary relocations, and construction staging as required. The Construction Contractor will be required to coordinate all protection measures, temporary supports, and temporary shutdowns of all utilities with the appropriate utility owners and/or agencies. The Construction Contractor will also be required to provide adequate notification to the utility owner prior to any work commencing on their utility. In addition, in the event a utility cannot be maintained in service during switch over to a temporary or permanent system, the Construction Contractor will be required to coordinate the shutdown with the utility owners and Project abutters to minimize impacts and inconveniences.

Chapter 9.0

Coordination with Other Governmental Agencies

9.0 COORDINATION WITH OTHER GOVERNMENTAL AGENCIES

9.1 Architectural Access Board Requirements

The Project will comply with the requirements of the Massachusetts Architectural Access Board and will be designated to comply with the standards of the Americans with Disabilities Act. See Appendix E for the Accessibility Checklist.

9.2 Massachusetts Environmental Policy Act (MEPA)

The Proponent does not expect that the Project will require review by the Massachusetts Environmental Policy Act (MEPA) Office of the Massachusetts Executive Office of Energy and Environmental Affairs. Current plans do not call for the Project to receive any state permits, state funding or involve any state land transfers.

9.3 Massachusetts Historical Commission

The MHC has review authority over projects requiring state funding, licensing, permitting and/or approvals that may have direct or indirect impacts to properties listed in the State Register of Historic Places. An MHC PNF will be filed to initiate the State Register Review process.

9.4 Boston Civic Design Commission

The Project will comply with the provisions of Article 28 of the Boston Zoning Code. This PNF will be submitted to the Boston Civic Design Commission by the BPDA as part of the Article 80 process.

Appendix A

Site Survey



GENERAL NOTES 1. THE PROPERTY IS SHOWN ON THE CITY OF BOSTON ASSESSORS MAPS AS PARCEL ID'S 1704070000 THRU 1704070005 THEREON. 2. LOCUS TITLE IS RECORDED AT THE SUFFOLK COUNTY REGISTRY OF DEEDS AS OWNERS OF RECORD: CITY POINT CENTER LLC OWNERS REFERENCE: -BOOK 53327 PG. 44 3. PLAN BOOK REFERENCES: -BOOK 6707 PG, 250 AND 541 -BOOK 6657 PG, 250 -BOOK 10275 PG, END -BOCK 10275 PG. END -PLAN OF BOSTON PUBLIC LUBRARY (LAND N/F SCHERER) FILED WITH THE CITY OF BOSTON EVANNEEMING DEPARTMENT -PLAN OF LAND DORCH-STERF, MASS. 10-14-50 BY HAM. FLETCHER -ENG. BOCK 137 PAGE 71-75 (BMSC UTILITY AS-BUILT OF WASHINGTON STREET) NOR THWESTERLY: CITY OF BOSTON FIELD BOOKS -BOOK 834 PG. 1 -BOOK 206 PGS. 130-133 -BOOK 939 PGS. 48-49 BEARING SYSTEM IN USE REFERENCES THE NORTH AMERICAN DATUM OF 1983. 5. OVERALL LOT AREA 48,564 S.F.± (CALC) 48,303 S.F.± (RECORD) 6. DATUM - HORIZONTAL - NAD 83' VERTICAL - CITY OF BOSTON NUMBER OF PARKING SPACES - 52 8. LOCATION OF UNDERGRADING UTUITES IS APPROXIMATE ONLY, AND IS NOT WARANTED TO BE CORRECT. UNDERGRADING UTUITES ARE SHOWN BASED ON A WARANTED TO BE CORRECT. UNDERGRADING UTUITES ARE SHOWN BASED ON A WALL INSPECTION OF SUPPACE OBSERVALE FRATURES ON Y MODIFINI, UTUITI MAY DUST WHICH ARE NOT INDICATED ON THESE PLANS. ALL EXISTING UTUITES SHALL BE VERTIED FOR SERVICE SIZE, INVERT ELEVATION, LOCATIONS, ETC. PRION NEW CONNECTIONS TO OR RELOCATION OF SAME. CONTRACTOR MUST NOTIFY DUG-AT 1-888-344-7233 AT LEAST 72 HOURS FRIGHT TO ANY CONSTRUCTION. NOTIFY THIS FRM IN WRITING OF ANY AND ALL DISCREPANCES PRIOR TO COMMENCING AN WORK. 9. NO INFORMATION ON SERVICE CONNECTIONS FOR WATER OR SEWER COULD BE FOUND IN THE BOSTON WATER AND SEWER COMMISION RECORDS. 10. LOCUS LIES WITHIN FLOOD INSURANCE ZONE X (AREA OF MINIMAL FLOODING) AS SHOWN ON THE FLOOD INSURANCE RATE MAP FOR THE CITY OF BOSTOM, MASSACHUSETTS, COMMUNITY PANEL NO. 25025C 0008 G, DATES SEPTEMBER 25, 11. THE WORD "CERTIFY" IS UNDERSTOOD TO BE AN EXPRESSION OF PROFESSIONAL OPINION BY THE LAND SURVEYOR MINCH IS BASED ON HIS BEST KNOMLEDGE. INFORMATION, AND BELLEF, FORMULATED IN ACCORDANCE WITH COMMONLY ACCEPTED PROCEDURES CONSISTENT WITH APPLICABLE STANDARDS OF PRACTICE, AND AS SUCH TO CONSTITUE'S INTERNA AND ALGURANTEE NOR WARRANTY, EITHER EXPRESS OR IMPLEI THE CERTIFICATIONS SHOWN ARE NOT CERTIFICATIONS TO THE TITLE OR OWNERSHIP O THE PROPERTIES SHOWN. TITLE NOTES - DESCRIPTION OF 10' PASSAGEWAY IS FOUND WITHIN OWNERS REFERENCE DEEDS AND SHOWN ON PLAN REFERENCE 1. - THERE ARE NO APPARENT DEEDED EASEMENTS IN THE RECORDED DEED FOR OVERHEAD UTILITIES CROSSING THE PROPERTY. - SEE DETAIL NOTES 1 THROUGH 6 FOR AREAS OF ABUTTING ENCROACHMENTS ONTO LOCUS - SEE DETAIL NOTES AA THROUGH GG FOR AREAS OF LOCUS ENCROACHMENTS ONTO ABUTTIN - SEE DETAIL NOTES A THROUGH D FOR OBSERVABLE DEBRIS DUMPING AREAS - THE LOCATION OF THE BUILDINGS SHOWN HEREON WAS EITHER IN COMPLIANCE WITH THE LOCAL ZONING BY-LAWS AT THE TIME OF CONSTRUCTION OR IS EXEMPT FROM WOLLATION ENFORCEMENT ACTION PER MASSACHUSETTS GENERAL LAWS CHAPTER 40A, SECTION 7. 1130-1132 Washington Street SOUTHWESTERLY: SURVEYOR'S CERTIFICATION NOR THEASTERLY: TO: CITY POINT CENTER LLC, FIRST AMERICAN TITLE INSURANCE COMPANY, EAST WEST BANK AND RUDOLPH FRIEDMANN LLP; This is to certify that this map or plat and the survey on which it is based were made in accordance with the 2011 minimum standard detail requirements for altraced with one time survey survey as statisticated and address of altra and norms of altra and norms of the survey SOUTHEASTERLY: Containing 2,510 square feet SOUTHWESTERLY: 10/16/14

LENDERS CERTIFICATION

O: CITY POINT CENTER LLC, FIRST AMERICAN TITLE INSURANCE COMPANY, EAST WEST BANK NID RUDOLPH FRIEDMANN LLP;

AND RUDOLPH FREEDMANN LLP: PURSUMIT TO THE ACCUMACT STANDARDS AS ADOPTED BY ALTA AND NSPS AND IN EFFECT ON THE DATE OF THIS CENTRORITON, THE UNDERSIGNED FURTHER CENTRESS THAT IN WY RELATE POSITION. ACCUMACY OF THIS SUM IN THE STATE OF MASSMCHUSETTS, THE RELATE POSITION. ACCUMACY OF THIS SUM IN THE STATE OF MASSMCHUSETS, THE RELATE POSITION. ACCUMACY OF THIS SUM IN THE STATE OF MASSMCHUSETS, THE RELATE POSITION. ACCUMACY OF THIS SUM IN THE STATE OF MASSMCHUSETS, THE RELATE POSITION. ACCUMACY OF THIS SUM IN THE STATE OF MASSMCHUSETS, THE RELATE POSITION. ACCUMACY OF THIS SUM IN THE STATE OF MASSMCHUSETS, THE RELATE POSITION. ACCUMACY OF THIS SUM IN THE STATE OF MASSMCHUSETS, THE RELATE POSITION. ACCUMACY OF THIS SUM IN A DECENT ON THE RELATE POSITION. ACCUMACY OF THIS SUM IN THE FLAM, AND SET BACK FROM THE BOUNDARIES OF THE PROPERTY, CECTOF AS SHOWN ON THE FLAM, AND SET BACK FROM THE ROUNDARIES OF THE REPORT. CLOTTED (3) THE FROMERTY IS CONTROL WITHIN THE ACCESS TO AND FROM WASHINGTON STREET, A PUBLIC WAY. (4) THERE ARE NO KNOWN CASEMENTS OF ENCLUMBANCES (INCLUMD VISIBLE UTILITY LINES) AFTERING THE PROPERTY OTHER THAN AS SHOWN AND DEPICTED ON THIS SUM Y, (5) THERE ARE NO KNOWN THE PLAM, (6) THERE ARE NO ENCRACHMENTS OF ANY IMPROVEMENTS ON THE PROPERTY ONTO ADJOINT PROPERTY, EXCEPT AS SHOWN ON THE PLAM, (7) ALL POTTABLE RECORDED DASEMENTS AND OTHER EXCEPTIONS, AS NOTED ON FIRST MALENCH THE COMMITMENT CATED DENSITY CLASSIFICITIONS ARE SUMMENT ANTER ALTERNAL THE COMMITMENT CATED DENSITY CLASSIFICTIONS ARE SUMMENT ANTER ON THE PROPERTY ONTO ADJOINT PROPERTY CONTROL FORCE THE SUM ON THE RECOMMENTS ON THE PROPERTY ONTO ADJOINT PROPERTY CONTROL FLATE ACCEDING AS AN OTHED DENSITY CLASSIFICTIONS ARE SUMMENT ANTE PATTER DASENDED THE COMMITMENT CATED DENSITY CLASSIFICTIONS ARE SUMMENT ANTEROL. DENSITY CLASSIFICTIONS ARE SUMMENT AND THE COMMITMENT CATED DENSITY CLASSIFICTIONS ARE SUMMENT AND THE PLATE ALTERCOMENTS ON THE ACCORDED DASEMENTS AND OTHER EXCEPTIONS. AS NOTED ON FIRST MALENCIAN THE COMM

Being the some premises conveyed by deed of John G. Molloy and Catherine L. Molloy to John G. Molloy, Trustee of the 1130 Reor Washington Street Realty Trust, dated March 23, 1992 and recorded with soil Deeds in Boar 17370, Page 62.

Containing 759 square feet.

1130R Washington Street, De

LEGAL DESCRIPTION

1120 Washington Street, Dorchester, MA 02124

The land with the buildings thereon numbered 1120 Washington Street in that part of Bosta called Darchester and shown as Lot No. 1 on "Plan of Land, Darchester, Mass., October 14, 1950, H.H. Fletcher, Surveyor" recorded November 30, 1950 and bounded and described as follower:

SOUTHWESTERLY: by Washington Street, eighty-five (85) feet;

NORTHWESTERLY: by land of owners unknown, ninety and 40/100 (90.40) feet;

NORTHEASTERLY: by land of owners unknown, thirty-seven and 20/100 (37.20) feet;

again by land or owners unknown, sixty-three and 70/100 (63.70) feet; NORTHEASTERLY: by Lot 5 as shown on said plan, forty-seven and 67/100 (47.67) feet; and

SOUTHEASTERLY: by Lot 2 as shown on said plan, one hundred fifty-two and 70/100 (152.70) feet.

Containing 10,437 square feet of land.

Being the same premises conveyed by deed of John G. Molloy, Trustee of 1120 Washington Street Really Trust, dated April 18, 2007 and recorded with Suffaik Registry of Deeds in Boo 42399, Page 138.

1126 Washington Street, Dorchester, MA 02124

A certain parcel of land with the buildings thereon now numbered 1126 Washington Street in the Derchester District of Boston, County of Suffak and Commonwealth of Massochusetts, Being shown as Lot 2 on a Plan of Land, Dorchester, Mossochusetts, Moy 26, 1931, H.M. Pietcher Surveyor, recorded with the Suffak Registry of Deeds, Book 6707, Page 541 and being bounded and described as follows:

SOUTHWESTERLY: by Washington Street by two lines, fifty-one and 93/100 (51.93) feet and twelve and 45/100 (12.45) feet;

NORTHWESTERLY: by Lot 1 as shown on said plan, one hundred fifty-two and 74/100 (152.74) feet;

NORTHEASTERLY: by Lot 5 as shown on sold plan, fifty-five and 07/100 (55.07) feet; and

SOUTHEASTERLY: by Lots 3 and 4 as shown on said plan, one hundred fifty-four and 95/100 (154.95) teet. Containing 9,212 square feet of land.

Also another certain parcel of vacant land in the Darchester District of Boston, Suffaik County, Massachusetts, being shown as Lot 5 on "Pian of Land Darchester, Mass." Doted May 26, 1931 by H.M. Ristcher, Surveyor, which pian is recorded with Suffaik Deeds, Book 5707, Page 541, bounded and described as follows:

NORTHWESTERLY: by land of owners unknown one hundred sixty-four and 19/100 (164.19) feet;

NORTHEASTERLY: by land of owners unknown, one hundred thirty-four and 93/100 (134.93) feet;

SOUTHEASTERLY: by land of owners unknown, one hundred forty-six and 18/100 (146.18) feet;

SOUTHWESTERLY: by Lot 5A shown on said plan, thirty-seven and 93/100 feet (37.93) feet;

OUTHEASTERLY: by Lot 5A shown on said plan, twenty (20) feet;

SOUTHWESTERLY: by Lots 1 and 2 as shown on said plan, one hundred two and 74/100 (102.74) feet.

Containing twenty-two thousand (22,000) square feet of land according to said plan. Being the same premises conveyed by deed of Dan G. Molioy, Trustee of the 126 Washington Street Realty Trust, dated October J1, 2000, recorded with the Suffaik Registry of Deeds in Book 25536, Page 285.

The land with the buildings thereon situated in that part of said Bastan called Darchester and numbered 1130-1132 Washington Street being Lot 3 on a plan by M.M. Fletcher surveyor, dated October 14, 1950 and recorder with the Suffak Registry of Deeds in Book 6657, Page 250, bounded and described according to said plan as follows:

by Washington Street, thirty-eight and 67/100 (38.67) feet

NORTHWESTERLY: by lot 2, sixty-six and 17/100 (66.17) feet;

by lot 4, in part through the middle of an eight-inch wall, thirty-eight and 33/100 (38.33) feet; and

by lot 7, sixty-four and 31/100 (64.31) feet.

Also another parcel in soid Dorchester being Lot 5A on a plan by H.M. Fletcher, surveys dated May 26, 1951, recorded with soid Deeds in Book 6707, Page 541, bounded and described as follows.

by lot 4, thirty-seven and 93/100 (37.93) feet;

NORTHWESTERLY: by lot 5, twenty (20) feet; NOR THEASTERLY: by lot 5, thirty-seven and 93/100 (37,93) feet; and

SOUTHEASTERLY: by land of owners unknown, twenty (20) feet.

Being the same premises conveyed by deed of John G. Molloy, Catherine L. O'Meara and Joseph F. Molloy doted December 17, 2004, recorded with Suffak Registry of Deeds in Book 36396, Page 241.

The land with buildings thereon situated in Boston, Suffaik County, Massachusetts, Don District, being 1130 Rear Washington Street, and shown as Lot 4 on "Plan of land, Derchester, Mass., October 14, 1950, A.M. Fletcher, Surveys", recorded with Suffaik Registry of Deeds on November 30, 1950 in Book 6557, Poge 250.

INESTERLY: by Lat 3 as shown on said plan in part through the middle of an 8 inch woll, thirty eight and 33/100 (38.33) feet;

NORTHWESTERLY: by Lot 2 cs shown on sold plan, eighty eight and 78/100 (88.78) feet; ISTERLY: by Lot 5 as shown on said plan, thirty seven and 93/100 (37.93) feet;

SOUTHEASTERLY: by Lot 7 as shown on sold plan, eighty eight and 79/100 (88.79) feet.

Containing 3,385 square feet of land.

ALTA/ACSM LAND TITLE SURVEY PLAN 1120-1132 WASHINGTON STREET DORCHESTER, MASSACHUSETTS DATE: JUNE 11, 2014 SCALE:1"=20' REV DATE: OCTOBER 16, 2014

ZONING LEGEND

ZONING DISTRICT: NEIGHBORHOOD SHOPPING SUBDISTRICT NEIGHBORHOOD DESIGN OVERLAY DISTRICT

	REQUIRED
COUNTY, STATE	SUFFOLK, MA
MINIMUM LOT AREA	NONE
MAXIMUM BUILDING HEIGHT	40'
MINIMUM LOT FRONTAGE	NONE
MINIMUM FRONT SETBACK	NONE
MINIMUM SIDE SETBACK	NONE
MINIMUM REAR SETBACK	20'
MAXIMUM FLOOR AREA RATIO	1.0
MINIMUM OPEN SPACE PER UNIT	50'
MINIMUM LOT WIDTH	NONE

LINE, SYMBOL, AND ABBREVIATION LEGEND

	CE	B CATCH BASIN							
S	SI	MH SEWER MANHOLE							
0	D	MH DRAIN MANHOLE							
1	TE	LEPHONE MANHOLE							
C	C#	BLE MANHOLE							
0	M	WRA MANHOLE							
\$	LIC	GHT POLE							
B	UT	ILITY POLE							
<u>gg</u>	GA	IS GATE							
WG	W/	ATER GATE							
	GA	TE UNKNOWN							
IN	V.	INVERT							
a	F	CHAIN LINT FENCE							
VC	c	VERTICAL CONCRETE CURB							
BC	c	BITUMINOUS CONCRETE CURB							
EH	н	ELECTRIC HAND HOLE							
RE	Т.	RETAINING							
WA	IP	WATER METER PIT							
EL		ELECTRIC							
\$7	Y	STORY							
FF	2	FINISHED FLOOR							
GT		GREASE TRAP							
-0	HE-	- OVERHEAD ELECTRIC LINE							
-	- C -	- GAS LINE							
-	1-	- COMMUNICATIONS LINE							
;	ss -	- SANITARY SERVER LINE							
-	*-	- WATER LINE							
-	50-	- STORM DRAIN							
	55-	CONTOUR LINE							
×	55.2	SPOT GRADE							
u	J	U TREE/HEDGE LINE							

HOYT LAND SURVEYING **1287 WASHINGTON STREET** WEYMOUTH MA. 02189 781-682-9192

Appendix B

Transportation

Appendix B – Transportation

Vehicle, Pedestrian, and Bicycle Counts Trip Generation Synchro Intersection Level of Service Reports

- Existing (2017) Condition
- No-Build (2024) Condition
- Build (2024) Condition

Vehicle, Pedestrian, and Bicycle Counts

Client: Michael Littman Project #: 53 016 HSH Dorchester BTD #: Location 1 Dorchester (Boston), MA Location: Street 1: Washington Street Street 2: River Street Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F

BOSTON BRAFFIC DATA PO BOX 1723, Framingham, MA 01701 Office: 978-746-1259 DataRequest@BostonTrafficData.com www.BostonTrafficData.com

TOTAL (CARS & TRUCKS)

		Washing	ton Street			Washingt	on Street			River	Street					
		Northwe	stbound			South	bound			East	ound			West	bound	
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	52	91	0	0	0	33	20	0	58	0	51	0	0	0	0
7:15 AM	0	50	99	0	0	0	35	21	0	63	0	55	0	0	0	0
7:30 AM	0	43	97	0	0	0	35	32	0	67	0	53	0	0	0	0
7:45 AM	0	46	96	0	0	0	32	40	0	64	0	61	0	0	0	0
8:00 AM	0	44	86	0	0	0	36	41	0	56	0	64	0	0	0	0
8:15 AM	0	45	93	0	0	0	37	39	0	42	0	62	0	0	0	0
8:30 AM	0	42	95	0	0	0	38	38	0	43	0	54	0	0	0	0
8:45 AM	0	38	89	0	0	0	35	33	0 39 0 49				0	0	0	0

		Washingt	ton Street			River Street										
		Northwe	stbound			South	bound			East	bound			West	bound	
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	60	52	0	0	0	42	40	0	39	0	48	0	0	0	0
4:15 PM	0	65	53	0	0	0	47	43	0	37	0	50	0	0	0	0
4:30 PM	0	66	48	0	0	0	48	46	0	38	0	47	0	0	0	0
4:45 PM	0	64	54	0	0	0	47	45	0	36	0	56	0	0	0	0
5:00 PM	0	62	55	0	0	0	49	48	0	39	0	60	0	0	0	0
5:15 PM	0	60	56	0	0	0	43	45	0	40	0	59	0	0	0	0
5:30 PM	0	56	51	0	0	0	41	43	0 39 0 53				0	0	0	0
5:45 PM	0	52	46	0	0	0	38	37	0 35 0 48				0	0	0	0

AM PEAK HOUR		Washing	ton Street			Washing	ton Street			River	Street						
7:15 AM		Northwe	stbound			South	bound			Eastb	ound			West	bound		
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn Left Thru Right				U-Turn	Left	Thru	Right	
8:15 AM	0	183	378	0	0	0	138	134	0	250	0	233	0	0	0	0	
PHF		0.	94			0.	88		0.97				0.00				
HV %	0.0%	1.1%	0.8%	0.0%	0.0% 0.0% 0.7% 0.0%				0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	

PM PEAK HOUR		Washing	ton Street			Washingt	on Street			River	Street						
4:30 PM		Northwe	estbound			South	bound			East	oound			West	bound		
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn Left Thru Right				U-Turn	Left	Thru	Right	
5:30 PM	0	252	213	0	0	0	187	184	0	153	0	222	0	0	0	0	
PHF		0.	99			0.	96		0.95				0.00				
HV %	0.0%	0.4%	0.5%	0.0%	0.0%	0.0%	2.1%	0.0%	0.0%	0.7%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	

Client: Michael Littman Project #: 53 016 HSH_Dorchester BTD #: Location 1 Dorchester (Boston), MA Location: Street 1: Washington Street River Street Street 2: Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F

0.44

PHF



	TRUCKS															
		Washing	ton Street			Washing	ton Street			River	Street					
		Northwe	estbound			South	bound			East	oound			West	bound	
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	1	2	0	0	0	0	0	0	2	0	1	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	1	1	0	0	0	1	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	1	2	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	0
8:30 AM	0	2	2	0	0	0	2	0	0	2	0	1	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	Washington Street Washington Street River Street															
		Northwe	stbound			South	bound			East	oound			West	bound	
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	1	0	0	0	1	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	1	0	0	0	0	1	0	0	1	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	1	0	0	0	2	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
AM PEAK HOUR		Washing	ton Street			Washing	ton Street			River	Street					
7:45 AM		Northwe	stbound	-		South	bound			East	ound	-		West	bound	
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
8:45 AM	0	3	4	0	0	0	3	0	0	3	0	1	0	0	0	0

PM PEAK HOUR		Washing	ton Street			Washing	ton Street			River	Street					
4:30 PM		Northwe	estbound			South	bound			Eastb	bound			West	bound	
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn Left Thru Right				U-Turn	Left	Thru	Right
5:30 PM	0	1	1	0	0	0	4	0	0 1 0 0				0 0 0 0			0
PHF		0.50 0.50							0.25				0.00			

0.33

0.38

3/30/2017, 4:42 PM, 53_016_TMC_Loc 1

0.00

Client: Michael Littman Project #: 53_016_HSH_Dorchester BTD #: Location 1 Location: Dorchester (Boston), MA Street 1: Washington Street Street 2: River Street Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F

BOSTON TRAFFIC DATA PO BOX 1723, Framingham, MA 01701 Office: 978-746-1259 DataRequest@BostonTrafficData.com www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

		Wa	shington St	reet			Wa	ashington St	treet				River Stree	t					
		No	orthwestbou	Ind				Southbound	d				Eastbound				Westbound		
Start Time	Left	Thru	Right	PED		Left	Thru	Right	PED		Left	Thru	Right	PED	Left	Thru	Right	PED	
7:00 AM	0	0	0	1		0	0	0	1		0	0	0	0	0	0	0	0	
7:15 AM	0	0	0	0		0	0	0	0		0	0	0	0	0	0	0	0	
7:30 AM	0	0	0	3		0	0	0	0		0	0	0	1	0	0	0	0	
7:45 AM	0	0	0	2		0	0	0	0		0	0	0	0	0	0	0	0	
8:00 AM	0	0	0	1		0	0	0	0		0	0	0	0	0	0	0	0	
8:15 AM	0	0	0	2		0	0	0	1		0	0	0	0	0	0	0	0	
8:30 AM	0	0	0	2		0	0	0	0		0	0	0	0	0	0	0	0	
8:45 AM	0	0	0	0		0	0	0	0		0	0	0	0	0	0	0	0	

		Wa	shington St	reet		Wa	shington St	treet			River Stree	t					
		No	orthwestbou	ind			Southbound	d			Eastbound				Westbound	1	
Start Time	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
4:00 PM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	
4:15 PM	0	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0	
4:30 PM	0	0	0	3	0	0	0	0	0	0	0	1	0	0	0	0	
4:45 PM	0	0	0	4	0	0	0	0	0	0	0	0	0	0	0	0	
5:00 PM	0	0	0	1	0	0	0	0	0	0	0	2	0	0	0	0	
5:15 PM	0	0	0	2	0	0	0	0	0	0	0	1	0	0	0	0	
5:30 PM	0	0	0	2	0	0	0	0	0	0	0	1	0	0	0	0	
5:45 PM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	

AM PEAK HOUR ¹		Wa	shington St	reet			Wa	shington St	reet				River Stree	t					
7:15 AM		No	orthwestbou	ind				Southbound	ł				Eastbound				Westbound	I.	
to	Left	Thru	Right	PED		Left	Thru	Right	PED		Left	Thru	Right	PED	Left	Thru	Right	PED	
8:15 AM	0	0	0	6		0	0	0	0		0	0	0	1	0	0	0	0	
		-			-					-									

PM PEAK HOUR ¹		Wa	shington St	reet		Wa	shington St	reet			River Stree	t					
4:30 PM		No	orthwestbou	ind			Southbound	1			Eastbound				Westbound	1	
to	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
5:30 PM	0	0	0	10	0	0	0	0	0	0	0	4	0	0	0	0	

¹ Peak hours corresponds to vehicular peak hours.

Client: Michael Littman 53 016 HSH Dorchester Project #: BTD #: Location 2 Dorchester (Boston), MA Location: Street 1: Washington Street Street 2: Morton St/Richmond St Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F

BOSTON BOSTON TRAFFIC DATA PO BOX 1723, Framingham, MA 01701 Office: 978-746-1259 DataRequest@BostonTrafficData.com

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TOTAL (CARS & TRUCKS) Washington Street Washington Street Morton Street **Richmond Street** Northbound Southbound Eastbound Westbound Soft Right Hard Right Start Time U-Turn Left Thru Right U-Turn Left Thru Right U-Turn Hard Left Left Soft Right U-Turn Left 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM Washington Street Washington Street Morton Street **Richmond Street** Northbound Westbound Southbound Eastbound Soft Right Hard Right Start Time U-Turn Left Thru Right U-Turn Left Thru Right U-Turn Hard Left Left Soft Right U-Turn Left 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM

AM PEAK HOUR		Washingt	on Street			Washing	ton Street			Morton	Street			Richmo	nd Street	
7:30 AM		North	bound			South	bound			Eastb	ound			Wes	tbound	
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Hard Left	Left	Soft Right	U-Turn	Left	Soft Right	Hard Right
8:30 AM	0	280	275	61	0	39	137	31	0	37	95	134	0	30	89	33
PHF		0.	94			0.	92			0.9	95			0	.86	
HV %	0.0%	0.0%	1.5%	0.0%	0.0%	2.6%	0.7%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

PM PEAK HOUR		Washingt	on Street			Washingt	on Street			Morton	Street			Richmo	nd Street	
4:30 PM		North	bound			South	bound			Eastb	ound			West	bound	
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Hard Left	Left	Soft Right	U-Turn	Left	Soft Right	Hard Right
5.20 DM	0	445	400	AE	4	20	474	64	0	20	402	470	0	45	400	20
5:50 PM	U	145	190	45		29	171	01	U	20	102	1/8	2	45	109	20
<i>PHF</i>	U	145	96	45	1	29 0.1	94	01	U	20	97	178	2	45 0	109 .88	20

Client: Michael Littman Project #: 53 016 HSH Dorchester BTD #: Location 2 Dorchester (Boston), MA Location: Street 1: Washington Street Street 2: Morton St/Richmond St Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F



Washington Street Washington Street Morton Street **Richmond Street** Northbound Southbound Eastbound Westbound Soft Right Hard Right Start Time U-Turn Left Thru Right U-Turn Left Thru Right U-Turn Hard Left Left Soft Right U-Turn Left 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM **Richmond Street** Washington Street Washington Street Morton Street Northbound Westbound Southbound Eastbound Thru Soft Right Hard Right Start Time U-Turn Left Right U-Turn Left Thru Right U-Turn Hard Left Left Soft Right U-Turn Left 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM AM PEAK HOUR Washington Street Washington Street Morton Street **Richmond Street** 7:45 AM Northbound Southbound Eastbound Westbound U-Turn U-Turn Right Soft Right Soft Right Hard Right to Left Thru Right Left Thru U-Turn Hard Left Left U-Turn Left 8:45 AM PHF 0.50 0.38 0.00 0.00

PM PEAK HOUR		Washing	ton Street			Washing	ton Street			Morton	Street			Richmo	nd Street	
4:00 PM		North	bound			South	bound			Eastb	ound			Wes	tbound	
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Hard Left	Left	Soft Right	U-Turn	Left	Soft Right	Hard Right
5:00 PM	0	0	1	0	0	1	2	0	0	0	0	0	0	0	0	0
PHF		0.	25	-		0.	38	-		0.	00			0	.00	-

TRUCKS

Client: Michael Littman Project #: 53_016_HSH_Dorchester BTD #: Location 2 Dorchester (Boston), MA Location: Street 1: Washington Street Street 2: Morton St/Richmond St Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F

BOSTON TRAFFIC DATA PO BOX 1723, Framingham, MA 01701 Office: 978-746-1259 DataRequest@BostonTrafficData.com www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

		Wa	shington St	reet		Wa	shington St	reet		N	Norton Stree	et		R	ichmond Stre	eet	
			Northbound	1			Southbound	d			Eastbound				Westbound	1	
Start Time	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
7:30 AM	0	0	0	1	0	0	0	1	0	0	0	0	0	0	0	1	
7:45 AM	0	0	0	2	0	0	0	0	0	0	0	2	0	0	0	0	
8:00 AM	0	0	0	4	0	0	0	2	0	0	0	0	0	0	0	0	
8:15 AM	0	0	0	3	0	0	0	0	0	0	0	0	0	0	0	0	
8:30 AM	0	1	0	1	0	0	0	0	0	0	0	1	0	0	0	0	
8.45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

		Wa	shington St Northbound	reet I		Wa	shington St Southbound	treet d		Ν	/lorton Stree Eastbound	et		Ri	chmond Stre Westbound	eet	
Start Time	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
4:15 PM	0	0	0	1	0	0	0	0	0	0	0	1	0	0	0	0	
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	
4:45 PM	0	0	0	2	0	0	0	1	0	0	0	0	0	0	0	0	
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	
5:15 PM	0	0	0	1	0	0	0	2	0	0	0	0	0	0	0	1	
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

AM PEAK HOUR ¹		Wa	shington St	reet		Wa	shington St	reet		Ν	Iorton Stree	et		Ri	chmond Stre	et	
7:30 AM			Northbound				Southbound	d			Eastbound				Westbound		
to	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
8:30 AM	0	0	0	10	0	0	0	3	0	0	0	2	0	0	0	1	
			-				-										

PM PEAK HOUR ¹		Wa	shington St	reet		Wa	shington St	reet		Ν	Norton Stree	et		Ri	chmond Stre	et	
4:30 PM			Northbound				Southbound	ł			Eastbound				Westbound		
to	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
5:30 PM	0	0	0	3	0	0	0	3	0	0	0	1	0	0	0	2	

¹ Peak hours corresponds to vehicular peak hours.

Client: Michael Littman Project #: 53 016 HSH Dorchester BTD #: Location 3 Dorchester (Boston), MA Location: Street 1: Dorchester Avenue Street 2: Richmond Street Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F

HV %

0.0%

0.0%

0.5%

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0.0%

0.0%

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TOTAL (CADE & TOUCKE)

							101	AL (CAR	S & IRUC	JKS)						
		Dorcheste	er Avenue			Dorcheste	er Avenue			Richmor	nd Street			Richmor	nd Street	
		North	bound			South	bound			East	bound			West	bound	
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	7	86	0	0	5	40	8	0	10	8	9	0	1	9	15
7:15 AM	0	12	76	2	0	5	41	9	0	13	12	11	0	1	10	14
7:30 AM	0	16	58	3	0	4	48	10	0	14	14	12	0	3	9	12
7:45 AM	0	14	78	2	0	2	50	10	0	15	13	14	0	5	8	8
8:00 AM	0	10	91	1	0	3	49	9	0	15	12	14	0	4	11	10
8:15 AM	0	9	86	2	0	3	46	8	0	14	12	15	0	3	12	8
8:30 AM	0	8	72	3	0	4	47	8	0	13	11	12	0	3	12	8
8:45 AM	0	8	69	2	0	3	43	7	0	12	12	13	0	2	11	7
		Dorcheste	er Avenue			Dorcheste	er Avenue			Richmor	nd Street			Richmor	nd Street	
		North	bound			South	bound			East	pound			West	bound	
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	9	56	2	0	4	71	5	0	8	9	13	0	11	18	5
4:15 PM	0	10	55	2	0	4	72	5	0	11	11	14	0	10	17	5
4:30 PM	0	9	51	2	0	3	74	7	0	13	11	13	0	11	17	13
4:45 PM	0	13	54	5	0	2	79	8	0	11	12	13	0	11	16	19
5:00 PM	0	12	52	7	0	4	75	9	0	8	14	12	0	13	20	14
5:15 PM	0	12	48	7	0	3	73	7	0	9	13	14	0	13	23	8
5:30 PM	0	10	46	6	0	3	70	7	0	9	10	11	0	12	23	8
5:45 PM	0	11	43	5	0	2	68	6	0	8	11	12	0	10	21	7
							•			D ' 1				D ' 1		
AM PEAK HOUR		Dorcheste	er Avenue			Dorcheste	er Avenue			Richmon	nd Street			Richmon	nd Street	
7:30 AM		North		Dialat		South	bound	Dialat		East		Dialat		West		Dialat
to	0-1um	Leit	242	Right	0-1um	Leit	102		0-1um	Leit E0	1 nru 54	Right	0-Turn	Leit	10	Right
8:30 AM DHE	U	49	01	0	U	12	08	31	U		08	55	U	15	02 02	30
	0.0%	0.0%	0.6%	0.0%	0.0%	0.0%	1 0%	0.0%	0.0%	0.0%	0.0%	1 8%	0.0%	0.0%	0.0%	0.0%
11 V /0	0.0 /0	0.070	0.076	0.076	0.070	0.070	1.0 /0	0.076	0.076	0.0 /0	0.070	1.0 /0	0.076	0.070	0.070	0.076
DM DEAK HOUD		Dorchest				Dorchest				Pichmor	nd Street			Pichmor	nd Street	
4.30 PM		North	bound			South	hound			Fast	ha bireer			West	hound	
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
5:30 PM	0	46	205	21	0	12	301	31	0	41	50	52	0	48	76	54
PHF	-	0.	94		-	0.	97			0.	97		-	0.	95	

0.0%

0.0%

Client: Michael Littman Project #: 53 016 HSH Dorchester BTD #: Location 3 Dorchester (Boston), MA Location: Street 1: Dorchester Avenue Street 2: **Richmond Street** Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F



TRUCKS **Dorchester Avenue Dorchester Avenue** Richmond Street **Richmond Street** Northbound Southbound Eastbound Westbound Start Time U-Turn Left Thru Right U-Turn Left Thru Right U-Turn Left Thru Right U-Turn Left Thru Right 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM Dorchester Avenue **Dorchester Avenue Richmond Street Richmond Street** Northbound Southbound Eastbound Westbound U-Turn Start Time U-Turn Left Thru Right Left Thru Right U-Turn Left Thru Right U-Turn Left Thru Right 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM AM PEAK HOUR **Dorchester Avenue Dorchester Avenue Richmond Street Richmond Street** 7:15 AM Northbound Southbound Eastbound Westbound U-Turn U-Turn Right to Left Thru Right Left Thru U-Turn Left Thru Right U-Turn Left Thru Right 8:15 AM PHF 0.50 0.50 0.25 0.00

PM PEAK HOUR		Dorcheste	er Avenue			Dorcheste	er Avenue			Richmor	nd Street			Richmor	nd Street	
4:00 PM		North	bound			South	bound			Eastb	ound			West	bound	
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
5:00 PM	0	0	0	0	0	0	2	0	0	0	0	1	0	0	0	0
PHF		0.	00			0.	25			0.	25			0.	00	

3/30/2017, 4:49 PM, 53_016_TMC_Loc 3

Client: Michael Littman Project #: 53_016_HSH_Dorchester BTD #: Location 3 Location: Dorchester (Boston), MA Street 1: Dorchester Avenue Street 2: Richmond Street Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F



PEDESTRIANS & BICYCLES

		Dor	chester Ave Northbound	enue I		Dor	rchester Ave Southbound	enue d		Ri	chmond Str Eastbound	eet		Ri	chmond Str Westbound	eet 1	
Start Time	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
7:00 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	
7:45 AM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	1	
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	
8:15 AM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	1	
8:30 AM	0	0	0	3	0	0	0	0	0	0	0	1	0	0	0	1	
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

		Dor	chester Ave Northbound	enue I		Dor	chester Ave Southbound	enue d		Ri	chmond Str Eastbound	eet		Ri	chmond Str Westbound	eet I	
Start Time	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
4:00 PM	0	0	0	1	0	0	0	2	0	0	0	2	0	0	0	6	
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	
4:30 PM	0	0	0	1	0	0	0	7	0	0	0	3	0	0	0	5	
4:45 PM	0	0	0	0	0	0	0	3	0	0	0	1	0	0	0	2	
5:00 PM	0	1	0	2	0	1	0	1	0	0	0	2	0	0	0	4	
5:15 PM	0	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0	
5:30 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	1	
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

AM PEAK HOUR ¹		Dor	chester Ave	enue			Dor	chester Ave	enue		Ri	chmond Str	eet		Ri	chmond Str	eet	
7:30 AM			Northbound					Southbound	ł			Eastbound				Westbound	i i	
to	Left	Thru	Right	PED		Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
8:30 AM	0	0	0	0		0	0	0	2	0	0	0	2	0	0	0	2	
		-			-													-

PM PEAK HOUR ¹		Dor	chester Ave	enue		Dor	chester Ave	enue		Rie	chmond Str	eet		Ri	chmond Str	eet	
4:30 PM			Northbound	1			Southbound	ł			Eastbound				Westbound	1	
to	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
5:30 PM	0	1	0	3	0	1	0	13	0	0	0	6	0	0	0	11	

¹ Peak hours corresponds to vehicular peak hours.

Client: Michael Littman Project #: 53 016 HSH Dorchester BTD #: Location 4 Location: Dorchester (Boston), MA Dorchester Ave/Adams St Street 1: Street 2: Washington Street Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F



TOTAL (CARS & TRUCKS)

HV %	0.0%	0.5%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	2.1%	0.7%	0.5%	0.0%	0.0%	0.5%	0.0%
PHF		0.	96			0.	97			0.	97			0.	92	
5:15 PM	0	213	224	172	0	18	326	69	0	48	152	213	0	158	190	15
to	U-Turn Left Thru Right U-Turn					Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:15 PM		North	bound			South	bound			East	bound			West	bound	
PM PEAK HOUR		Adams	s Street			Dorchest	er Avenue			Washing	ton Street			Adams	Street	
117 /0	0.070	0.070	0.070	0.070	0.070	0.070	0.070	1.2.70	0.070	0.070	1.070	0.070	0.070	0.070	0.170	0.070
HV %	0.0%	0.6%	0.3%	0.0%	0.0%	0.0%	0.6%	1.2%	0.0%	0.0%	1.0%	0.0%	0.0%	0.0%	0.7%	0.0%
0.50 AM		000	97	501	5	 	98	51		<u> </u>	96	100	0	120	92	13
8-30 AM	0	359	286	361	0-1011	6	155	81	0-runi	62	194	153	0-1011	126	150	19
/:30 AM				Pight	LI Turn	South	Thru	Pight	11 Turn	⊑astt Loft	Thru	Pight		vvesti	Thru	Pight
AM PEAK HOUR		Adams	s Street			Dorchest	er Avenue			Washing	ton Street			Adams	s Street	
0.40 FIVI	0	40	1 01	- 39	0	5	10	15	0	3	51	40	0	30	41	5
5:45 DM		49	51	30	0	5	78	13		0 0	37	- 52 - 46	0	30	43	3
5:10 PIVI		23	54	40	0	6	80	14	0	10	41	53	0	30	50	2
5:00 PM		54	56	45	0	6	81	10		10	38	57	0	35	52	4
4:45 PM		55	59	44	0	6	/9	1/	0	11	32	55	0	38	48	4
4:30 PM	0	51	52	39	0	4	84	18	0	13	39	54	0	37	43	3
4:15 PM	0	53	53	44	0	2	82	18	0	13	43	47	0	48	47	4
4:00 PM	0	50	49	44	0	2	83	17	0	12	41	45	0	54	52	4
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
		North	bound			South	bound			East	pound			West	bound	
		Adama	Street			Dorohoot		•	•	Maching	ton Streat			Adama	Street	•
8:45 AM	0	76	73	74	0	2	35	19	0	17	39	35	0	27	31	4
8:30 AM	0	81	76	82	0	3	38	19	0	16	41	37	0	29	32	4
8:15 AM	0	88	77	85	0	3	37	18	0	19	45	40	0	34	38	5
8:00 AM	0	86	82	91	0	2	39	21	0	16	50	40	0	35	41	4
7:45 AM	0	91	72	95	0	0	38	22	0	12	51	37	0	32	36	5
7:10 / M	0	94	55	90	0	1	40	20	0	15	48	36	0	25	35	5
7:15 AM	0	93	63	91	0	2	40	16	0	16	40	32	0	20	38	4
		00	65	83	0-1011	2	38	15		15	38	20		28	40	5
Start Time	LI-Turn	Left	Thru	Right	LI-Turn	Left	Thru	Right	I II-Turn	Lasu		Right	LI-Turn	L eft	Thru	Right
		North	hound			South				Fast				Moetl	hound	
		Adama	Street			Dorohoot			3 & 1700	Washing	ton Street			Adama	Street	
		Adama	Street			Dorohoot		AL (CAR	SAIRU	Machinal	ton Street			Adama	Street	

Client: Michael Littman Project #: 53 016 HSH Dorchester BTD #: Location 4 Dorchester (Boston), MA Location: Dorchester Ave/Adams St Street 1: Street 2: Washington Street Count Date: 3/21/2017 Day of Week: Tuesday Weather: Cloudy, 45°F

0.31



TRUCKS Adams Street Dorchester Avenue Washington Street Adams Street Eastbound Northbound Southbound Westbound U-Turn Start Time U-Turn Left Thru Right U-Turn Left Thru Right Left Thru Right U-Turn Left Thru Right 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM Adams Street **Dorchester Avenue** Washington Street Adams Street Eastbound Northbound Southbound Westbound Start Time U-Turn Left Thru Right U-Turn Left Thru Right U-Turn Left Thru Right U-Turn Left Thru Right 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM AM PEAK HOUR Adams Street **Dorchester Avenue** Washington Street Adams Street 7:45 AM Northbound Southbound Eastbound Westbound U-Turn U-Turn Right U-Turn Right to Left Thru Right Left Thru Left Thru Right U-Turn Left Thru 8:45 AM PHF

PM PEAK HOUR		Adams	Street			Dorchest	er Avenue			Washing	ton Street			Adams	Street	
4:00 PM		North	bound			South	bound			East	oound			West	bound	
to	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
5:00 PM	0	0	0	0	0	0	2	1	0	0	1	1	0	0	2	0
PHF		0.	00			0.	25			0.	50			0.	50	

0.38

0.50

3/30/2017, 4:52 PM, 53_016_TMC_Loc 4

0.25

Client:	Michael Littman
Project #:	53_016_HSH_Dorchester
BTD #:	Location 4
Location:	Dorchester (Boston), MA
Street 1:	Dorchester Ave/Adams St
Street 2:	Washington Street
Count Date:	3/21/2017
Day of Week:	Tuesday
Weather:	Cloudy, 45°F

BOSTON TRAFFIC DATA PO BOX 1723, Framingham, MA 01701 Office: 978-746-1259 DataRequest@BostonTrafficData.com www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

		A	Adams Stree	et		Dor	chester Ave	enue		Wa	shington St	reet		ŀ	Adams Stree	et	
			Northbound	1			Southbound	d			Eastbound				Westbound		
Start Time	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3	
7:30 AM	0	0	0	2	0	0	0	1	0	0	0	1	0	0	0	2	
7:45 AM	0	0	0	1	0	0	0	3	0	0	0	3	0	0	0	4	
8:00 AM	0	0	0	3	0	0	0	5	0	0	0	4	0	0	0	9	
8:15 AM	0	0	0	2	0	0	0	2	0	0	0	2	0	0	0	5	
8:30 AM	0	0	0	1	0	0	0	0	0	0	0	3	0	0	0	7	
8:45 AM	0	0	0	0	0	0	0	1	0	0	0	1	0	0	0	4	

		A	dams Stree	et I		Dor	chester Ave Southbound	enue 1		Wa	shington St Eastbound	reet		A	Adams Stree Westbound	et I	
Start Time	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
4:00 PM	0	0	0	2	0	0	0	4	0	0	0	4	0	0	0	7	
4:15 PM	0	0	0	0	0	0	0	3	0	0	0	1	0	0	0	3	
4:30 PM	0	0	1	1	0	0	0	2	0	0	0	2	0	0	0	4	
4:45 PM	0	0	0	2	0	0	0	3	0	0	0	3	0	0	0	5	
5:00 PM	0	0	0	2	0	0	0	2	0	0	0	2	0	0	0	8	
5:15 PM	0	0	0	0	0	0	0	3	0	0	0	1	0	0	0	4	
5:30 PM	0	0	0	1	0	0	0	4	0	0	0	0	0	0	0	5	
5:45 PM	0	0	0	0	0	0	0	2	0	0	0	0	0	0	0	3	

AM PEAK HOUR ¹		A	Adams Stree	et		Dor	chester Ave	enue		Wa	shington St	treet			A	Adams Stre	ət	
7:30 AM			Northbound	ł			Southbound	d			Eastbound					Westbound	i i	
to	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED		Left	Thru	Right	PED	
8:30 AM	0	0	0	8	0	0	0	11	0	0	0	10		0	0	0	20	
							-	-				-	-					

PM PEAK HOUR ¹		A	dams Stree	et		Dor	chester Ave	enue		Wa	shington St	reet		A	dams Stree	et	
4:15 PM			Northbound				Southbound	1			Eastbound				Westbound		
to	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	
5:15 PM	0	0	1	5	0	0	0	10	0	0	0	8	0	0	0	20	

¹ Peak hours corresponds to vehicular peak hours.

Trip Generation - Proposed Program
1120 Washington Street

Trip Generation Assessment

HOWARD STEIN HUDSON 7-Mar-2017

Land Use	Size	Category	Directional Split	Average Trip Rate	Unadjusted Vehicle Trips	Assumed National Vehicle Occupancy Rate ¹	Unadjusted Person-Trips	Primary Person- Trips	Transit Share ³	Transit Person- Trips	Walk/Bike/ Other Share ³	Walk/ Bike/ Other Trips	Auto Share ³	Auto Person- Trips	Assumed Local Auto Occupancy Rate ⁴	Total Adjusted Auto Trips
Daily Peak Hour																
Apartment⁵	57	Total		6.650	380	1.13	430	430	16%	68	18%	78	66%	284	1.13	252
	units	In	50%	3.325	190	1.13	215	215	16%	34	18%	39	66%	142	1.13	126
		Out	50%	3.325	190	1.13	215	215	16%	34	18%	39	66%	142	1.13	126
Office Building ⁶	3.6	Total		11.030	40	1.13	46	46	15%	6	10%	4	75%	36	1.13	32
	KSF	In	50%	5.515	20	1.13	23	23	15%	3	10%	2	75%	18	1.13	16
		Out	50%	5.515	20	1.13	23	23	15%	3	10%	2	75%	18	1.13	16
Total		Total			420		476	476		74		82		320		284
		In			210		238	238		37		41		160		142
		Out			210		238	238		37		41		160		142
AM Peak Hour																
Apartment ⁵	57	Total		0.51	29	1.13	33	33		9		5		19	1.13	17
	units	In	20%	0.102	6	1.13	7	7	18%	1	28%	2	54%	4	1.13	4
		Out	80%	0.408	23	1.13	26	26	31%	8	13%	3	56%	15	1.13	13
Office Building ⁶	3.6	Total		1.56	6	1.13	7	7		1		1		5	1.13	5
	KSF	In	88%	1.373	5	1.13	6	6	19%	1	17%	1	64%	4	1.13	4
		Out	12%	0.187	1	1.13	1	1	29%	0	8%	0	63%	1	1.13	1
Total		Total			35		40	40		10		6		24		22
		In			11		13	13		2		3		8		8
		Out			24		27	27		8		3		16		14
PM Peak Hour																
Apartment ⁵	57	Total		0.62	35	1.13	40	40		11		7		22	1.13	19
	units	In	65%	0.403	23	1.13	26	26	31%	8	13%	3	56%	15	1.13	13
		Out	35%	0.217	12	1.13	14	14	18%	3	28%	4	54%	7	1.13	6
Office Building ⁶	3.6	Total		1.49	5	1.13	6	6		1		1		4	1.13	4
	KSF	In	17%	0.253	1	1.13	1	1	29%	0	8%	0	63%	1	1.13	1
		Out	83%	1.237	4	1.13	5	5	19%	1	17%	1	64%	3	1.13	3
Total		Total			40		46	46		12		8		26		23
		In			24		27	27		8		3		16		14
		Out			16		19	19		4		5		10		9

1. 2009 National vehicle occupancy rates - 1.13:home to work; 1.84: family/personal business; 1.78: shopping; 2.2 social/recreational

2. Based on ITE Trip Generation Handbook, 3rd Edition method

3. Mode shares based on peak-hour BTD Data for Area 9

4. Local vehicle occupancy rates based on 2009 National vehicle occupancy rates

5. ITE Trip Generation Manual, 9th Edition, LUC 220 (Apartment), average rate

6. ITE Trip Generation Manual, 9th Edition, LUC 710 (General Office Building), average rate

XX

HARD CODED TO BALANCE (Manually change formatting)

Synchro Intersection Level of Service Reports

• Existing (2017) Condition

	۲	→	\mathbf{F}	4	←	•	٠	Ť	۲	6	Ļ	~				
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2			
Lane Configurations		र्भ	1		\$		۳.	î∌		٦	4Î					
Traffic Volume (vph)	37	95	134	30	89	33	280	275	61	39	137	31				
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900				
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00				
Frt			0.850		0.971			0.973			0.972					
Fit Protected	0	0.986	1415	0	0.990	0	0.950	1010	٥	0.950	1022	0				
Salu. Flow (prot) Elt Permitted	U	0.986	1015	U	0.990	U	0.606	1017	U	0.256	1032	U				
Satd. Flow (perm)	0	1873	1615	0	1826	0	1151	1819	0	472	1832	0				
Right Turn on Red			Yes			Yes			Yes			Yes				
Satd. Flow (RTOR)		20	236		9			10			9 20					
Link Distance (ft)		615			710			537			620					
Travel Time (s)		14.0			16.1			12.2			14.1					
Peak Hour Factor	0.95	0.95	0.95	0.86	0.86	0.86	0.94	0.94	0.94	0.92	0.92	0.92				
Heavy Venicles (%) Adi, Flow (vpb)	20	0%	0%	0%	0% 103	0%	208	2%	0%	3%	1/0	0%				
Shared Lane Traffic (%)	57	100	141	55	105	50	270	275	05	72	147	54				
Lane Group Flow (vph)	0	139	141	0	176	0	298	358	0	42	183	0				
Turn Type	Split	NA	Perm	Split	NA		pm+pt	NA		Perm	NA		2			
Protected Phases Permitted Phases	3	3	3	4	4		15	15		1	1		2			
Detector Phase	3	3	3	4	4		5	15		1	1					
Switch Phase																
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0		5.0			10.0	10.0		1.0			
iviinimum split (s) Total Split (s)	16.5	16.5 23.0	16.5 23.0	16.5 19.0	16.5 19.0		14.0			19.5 36.0	19.5 36.0		27.0			
Total Split (%)	19.2%	19.2%	19.2%	15.8%	15.8%		12.5%			30.0%	30.0%		23%			
Maximum Green (s)	16.5	16.5	16.5	12.5	12.5		6.0			26.5	26.5		23.0			
Yellow Time (s)	4.0	4.0	4.0	3.5	3.5		3.0			3.5	3.5		2.0			
All-Red Time (S) Lost Time Adjust (s)	2.5	2.5	2.5	3.0	3.0		6.0			6.0	6.0		2.0			
Total Lost Time (s)		6.5	6.5		6.5		9.0			9.5	9.5					
Lead/Lag	Lead	Lead	Lead	Lag	Lag					Lead	Lead		Lag			
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes		2.0			Yes	Yes		Yes			
Venicle Extension (s) Recall Mode	Z.U Max	2.0 Max	2.0 Max	2.0 Max	2.0 Max		2.0 Max			4.0 C-Max	4.0 C-Max		3.0 None			
Walk Time (s)	Max	Max	Max	Max	Max		Max			O Max	0 Max		7.0			
Flash Dont Walk (s)													16.0			
Pedestrian Calls (#/hr)		22.7	22.7		10 5		22.0	41 F		2/ 5	24 5		16			
Actuated a/C Ratio		32.7	32.7		0.10		33.U 0.28	41.5		26.5	26.5					
v/c Ratio		0.27	0.23		0.89		0.85	0.56		0.40	0.45					
Control Delay		40.9	0.9		91.2		61.8	37.4		53.5	42.4					
Queue Delay		0.0	0.0		0.0		0.0	0.0		0.0	0.0					
LOS		40.9 D	0.9 A		91.2 F		61.8 F	37.4 D		53.5 D	42.4 D					
Approach Delay		20.8	~		91.2		-	48.5		D	44.4					
Approach LOS		С			F			D			D					
90th %ile Green (s)	16.5 May D	16.5	16.5	12.5	12.5		6.0			26.5	26.5 Coord		23.0 Dod			
70th %ile Ferm Code 70th %ile Green (s)	16.5	16.5	16.5	12.5	12.5		MaxR 6.0			26.5	26.5		23.0			
70th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Ped			
50th %ile Green (s)	43.5	43.5	43.5	12.5	12.5		6.0			26.5	26.5		0.0			
50th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip			
30th %ile Green (S)	43.5 MaxR	43.5 MaxR	43.5 MaxR	MaxR	MaxR		0.0 MaxR			20.5 Coord	20.5 Coord		0.0 Skip			
10th %ile Green (s)	43.5	43.5	43.5	12.5	12.5		6.0			26.5	26.5		0.0			
10th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip			
Queue Length 50th (ft)		74	0		130		187	166		28	117					
Internal Link Dist (ft)		535	0		#240		111#299	457		08	540					
Turn Bay Length (ft)		000			000			107			010					
Base Capacity (vph)		510	611		198		349	635		104	411					
Starvation Cap Reductn		0	0		0		0	0		0	0					
Spiliback Cap Reductn Storage Can Reductn		0	0		0		0	0		0	0					
Reduced v/c Ratio		0.27	0.23		0.89		0.85	0.56		0.40	0.45					
Intersection Summary																
Area Type: 0	Other															
Cycle Length: 120																
Actuated Cycle Length: 120	nhoos 1.NI		of Croop													
Natural Cycle: 95	pnase r:Ni	୦୦୯, ୨୧୩୯	or Green													
Control Type: Actuated-Coordin	nated															
Maximum v/c Ratio: 0.89																
Intersection Signal Delay: 47.6	42.00/			In	tersection	LOS: D	2									
Analysis Period (min) 15	102.8%			IC	U Level of	Service	0									
 95th percentile volume exce 	eeds capac	ity, queue	may be lo	nger.												
Queue shown is maximum a	after two cy	cles.														
m Volume for 95th percentile	queue is m	netered by	upstream	signal.												
Splits and Phases: 1: Washi	ngton Stree	t & Mortor	n Street/Ri	chmond S	treet											
1 (D)					1						20			7	≜ tar	
¥1Ø1(K)				_							25			¥ Ø4	105	

2017003::1120 Washington Street

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Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	SBR2	NEL2	NEL	NER	Ø2		
Lane Configurations	٦	R.	۲	1	1		1	۲		1		 	
Future Volume (vph)	250	233	183	378	138	0	134	0	0	0			
Ideal Flow (vnhnl)	1900	233 1900	1900	1900	1900	1900	1900	1900	1900	1900			
Storage Length (ft)	75	0	100	1700	1700	75	7700	. 700	0	0			
Storage Lanes	1	1	1			1			1	1			
Taper Length (ft)	100		100						25				
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
FIL Fit Protected	0.050	0.850	0.050				0.850						
Satd, Flow (prot)	0.950	1615	1787	1900	1900	Ο	1615	1863	0	1863			
Flt Permitted	0.950	1013	0.950	1700	1700	U	1015	1003	U	1003			
Satd. Flow (perm)	1805	1615	1787	1900	1900	0	1615	1863	0	1863			
Right Turn on Red							Yes			Yes			
Satd. Flow (RTOR)							173						
Link Speed (mph)	30			30	30				30				
Link Distance (ft)	464			447	537				214				
Haver Time (S)	10.5	0.07	0.04	10.2	12.2	0.00	0.00	0.00	4.9	0.00			
Heavy Vehicles (%)	0.97	0.97	0.94	0.94	0.88 0%	U.88 1%	0.88 0%	0.92	0.92	0.92			
Adi, Flow (vph)	258	240	195	402	157	0	152	270	270	270			
Shared Lane Traffic (%)	200	2.5				Ū	102	Ŭ	Ŭ	Ŭ			
Lane Group Flow (vph)	258	240	195	402	157	0	152	0	0	0			
Turn Type	Prot	pt+ov	Prot	NA	NA		Prot	Prot		Prot			
Protected Phases	3	13	1	15	5		5	4		4	2		
Permitted Phases				4.5	_		-						
Detector Phase	3	13	1	15	5		5	4		4			
Swiich Phase Minimum Initial (s)	10.0		10.0		10.0		10.0	4.0		10	10		
Minimum Snlit (S)	10.0		10.0		16.5		16.5	4.0		4.0	26.0		
Total Split (s)	27.0		33.0		24.0		24.0	10.0		10.0	26.0		
Total Split (%)	22.5%		27.5%		20.0%		20.0%	8.3%		8.3%	22%		
Maximum Green (s)	20.5		27.5		17.5		17.5	4.0		4.0	22.0		
Yellow Time (s)	4.0		3.0		4.0		4.0	3.5		3.5	2.0		
All-Red Time (s)	2.5		2.5		2.5		2.5	2.5		2.5	2.0		
Lost Time Adjust (s)	0.0		0.0		0.0		0.0	0.0		0.0			
Load/Lag	6.5		5.5		6.5		6.5	6.0		6.0	100		
Lead/Ldy	Lead Voc		Vac					Yos		Yos	Yoc		
Vehicle Extension (s)	2.0		2.0		4.0		4.0	2.0		2.0	3.0		
Recall Mode	None		C-Max		None		None	None		None	None		
Walk Time (s)											7.0		
Flash Dont Walk (s)											15.0		
Pedestrian Calls (#/hr)											7		
Act Effct Green (s)	20.6	82.3	56.2	82.2	19.4		19.4						
Actuated g/C Ratio	0.17	0.69	0.47	0.68	0.16		0.16						
V/C Rall0 Control Delay	0.83	0.22	0.23	0.31	0.51		U.37						
Oueue Delay	0.3	0.0	0.0	2.0	0.0		0.0						
Total Delay	70.3	7.7	10.7	2.9	52.7		15.8						
LOS	E	A	В	A	D		В						
Approach Delay	40.1			5.4	34.5								
Approach LOS	D			А	С								
90th %ile Green (s)	20.5		27.5		27.5		27.5	0.0		0.0	22.0		
90th %ile Term Code	Max		Coord		Max		Max	Skip		Skip	Ped		
70th %ile Green (S)	25.2 Con		53.0 Coord		23.3 Gan		23.3 Gan	0.0 Skin		0.0 Ckin	0.0 Skin		
50th %ile Green (s)	22 A		60.1		18 8		18.8	0.0		0.0	0.0		
50th %ile Term Code	Gan		Coord		Gan		Gan	Skin		Skin	Skin		
30th %ile Green (s)	19.6		66.2		15.7		15.7	0.0		0.0	0.0		
30th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip		
10th %ile Green (s)	15.3		74.4		11.8		11.8	0.0		0.0	0.0		
10th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip		
Queue Length 50th (ft)	191	49	43	4	123		25						
Queue Lerigin 95th (II)	#33/ 201	101	148	113	/11/1		m/U		124				
Turn Bay Length (ff)	75		100	307	437		75		134				
Base Capacity (vph)	328	1123	837	1289	331		424						
Starvation Cap Reductn	0	0	0	405	0		0						
Spillback Cap Reductn	0	0	0	0	0		0						
Storage Cap Reductn	0	0	0	0	0		0						
Reduced v/c Ratio	0.79	0.21	0.23	0.45	0.47		0.36						
Intersection Summary													
Area Type:	Other												
Cycle Length: 120													
Actuated Cycle Length: 120													
Offset: 0 (0%), Referenced to	phase 1:NB	TL, Start o	of Green										
Natural Cycle: 85	dia at 1												
Control Type: Actuated-Coord	ainated												
Intersection Signal Dolay: 24	1			In	torsaction	105-0							
Intersection Signal Delay: 24. Intersection Canacity Litilization	on 47 7%			In		LUS: C	1						
Analysis Period (min) 15	UIT 1.170			IC.		JUNICE I							
 95th percentile volume ex 	ceeds capac	ity, queue	e may be lo	nger.									
Queue shown is maximum	n after two cy	cles.											
m Volume for 95th percentil	le queue is m	netered by	upstream	signal.									
0.11.1.01				0									
Splits and Phases: 2: Drive	eway & Wash	ington Str	reet & Rive	r Street								 1.	1 14
A (R)					Ø2					Ø3		1 04	1 1 as
33 c				26 c	~~				27.	23		10 s	24 s

2017003::1120 Washington Stree

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2
Lane Configurations		Ę	1	۲	¢î		٦	1	1		ሳ ቤ		
Traffic Volume (vph)	62 62	194 194	153	126	150 150	19 19	359	286	361	6	155	81 81	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Storage Length (ft)	0		25	0		50	0		0	0		0	
Taper Length (ft)	25		1	25		1	25		1	25		U	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.95	0.95	0.95	
Frt Elt Protected		0.988	0.850	0.950	0.983		0.950		0.850		0.950		
Satd. Flow (prot)	0	1863	1615	1805	1851	0	1787	1900	1615	0	3393	0	
Fit Permitted	0	0.766	1415	0.396	1051	0	0.599	1000	1415	0	0.944	0	
Right Turn on Red	U	1444	Yes	752	1001	Yes	1127	1900	Yes	0	3200	Yes	
Satd. Flow (RTOR)			77		5				372		63		
Link Speed (mph)		30			30 673			30			30 615		
Travel Time (s)		10.2			15.3			10.1			14.0		
Peak Hour Factor	0.96	0.96	0.96	0.92	0.92	0.92	0.97	0.97	0.97	0.98	0.98	0.98	
Adj. Flow (vph)	65	202	159	137	163	21	370	295	372	0%	158	83	
Shared Lane Traffic (%)													
Lane Group Flow (vph)	0 Porm	267 NA	159	137 Porm	184 NA	0	370 D P+P	295 NA	372 Prot	0 Porm	247 NA	0	
Protected Phases	FCIIII	5	5 6	FCIII	5		D.F +F	16	16	FCIIII	1		2
Permitted Phases	5	_	F (5	_		1			1			
Switch Phase	5	5	56	5	5		6	16	16	1	1		
Minimum Initial (s)	10.0	10.0		10.0	10.0		8.0			10.0	10.0		1.0
Minimum Split (s)	18.0	18.0		18.0	18.0		14.5			17.5	17.5		32.0
Total Split (%)	39.0	39.0		39.0	39.0		18.3%			22.5%	22.5%		27%
Maximum Green (s)	31.0	31.0		31.0	31.0		15.5			19.5	19.5		28.0
Yellow Time (s) All-Red Time (s)	4.5	4.5		4.5	4.5		3.0			4.0	4.0		2.0
Lost Time Adjust (s)	5.5	0.0		0.0	0.0		0.0			5.5	0.0		2.0
Total Lost Time (s)	اممر	0.8		0.8	0.8		6.5			اممر	7.5		100
Lead-Lag Optimize?	Yes	Yes		Yes	Yes		Yes			Yes	Yes		Yes
Vehicle Extension (s)	2.0	2.0		2.0	2.0		4.0			2.0	2.0		3.0
Recall Mode	None	None		None	None		None			C-Max	C-Max		None 7.0
Flash Dont Walk (s)													21.0
Pedestrian Calls (#/hr)		05.4	50.0	05.4	05.4		10.0	50.5	50.5		00 <i>(</i>		49
Act Effect Green (s) Actuated g/C Ratio		25.4	50.3 0.42	25.4 0.21	25.4 0.21		48.0	53.5 0.45	53.5 0.45		28.6		
v/c Ratio		0.87	0.22	0.86	0.46		0.67	0.35	0.40		0.30		
Control Delay		68.6	8.7	87.3	43.0		36.0	27.5	4.2		32.8		
Total Delay		68.6	8.7	87.3	43.0		36.0	27.5	4.2		32.8		
LOS		E	А	F	D		D	С	А		С		
Approach Delay Approach LOS		46.2 D			61.9 E			22.2 C			32.8 C		
90th %ile Green (s)	31.0	31.0		31.0	31.0		15.5			19.5	19.5		28.0
90th %ile Term Code	Max 20.6	Max 20.6		Max 20.6	Max 20.6		Max			Coord	Coord		Ped 28 0
70th %ile Term Code	Gap	Gap		Gap	Gap		Max			Coord	Coord		Ped
50th %ile Green (s)	26.4	26.4		26.4	26.4		20.1			19.5	19.5		28.0
50th %ile Term Code 30th %ile Green (s)	Gap 22.7	Gap 22.7		Gap 22.7	Gap 22.7		Max 23.8			Coord	Coord		Ped 28.0
30th %ile Term Code	Gap	Gap		Gap	Gap		Max			Coord	Coord		Ped
10th %ile Green (s)	16.5 Con	16.5 Con		16.5	16.5 Con		16.5 Con			65.0	65.0		0.0 Skip
Queue Length 50th (ft)	Gap	138	10	102	121		217	165	0	COOLU	67		змр
Queue Length 95th (ft)		298	57	#195	183		#404	259	65		109		
Internal Link Dist (ft) Turn Bay Length (ft)		367	25		593			363			535		
Base Capacity (vph)		373	693	194	481		551	846	925		811		
Starvation Cap Reductn		0	0	0	0		0	0	0		0		
Spiliback Cap Reductin		0	0	0	0		0	0	0		0		
Reduced v/c Ratio		0.72	0.23	0.71	0.38		0.67	0.35	0.40		0.30		
Intersection Summary													
Area Type:	Other												
Actuated Cycle Length: 120													
Offset: 117 (98%), Referenced	to phase 1	NBSB, Sta	art of Gree	n									
Natural Cycle: 85 Control Type: Actuated Coordi	nated												
Maximum v/c Ratio: 0.87	ndieu												
Intersection Signal Delay: 34.8	- 7/ 70/			Int	ersection	OS: C	,						
Analysis Period (min) 15	n 76.7%			IC	U Level of	Service I	J						
 95th percentile volume exc 	eeds capac	ity, queue	may be lo	nger.									
Queue shown is maximum	after two cy	cles.											
Splits and Phases: 3: Adam:	s Street & V	/ashington	Street &	Dorcheste	r Avenue								
1 (R)			Har	,					ŧ	05			Star.
27 s			32 s	-					39 s	20			22 s

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2	
Lane Configurations	50			10	40	20	40	4	0	10	4	27		
Future Volume (vph)	58 58	51	55	15	40	38 38	49	313	8	12	193	37		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		
Flt Protected		0.983			0.945			0.993			0.998			
Satd. Flow (prot)	0	1772	0	0	1781	0	0	1865	0	0	1842	0		
Fit Permitted Satd. Flow (perm)	0	0.848	0	0	0.941	0	0	0.932	0	0	0.977	0		
Right Turn on Red	-		Yes	-		Yes	-		Yes	-		Yes		
Satd. Flow (RTOR)		35			41			2			16			
Link Distance (ft)		710			686			615			708			
Travel Time (s)		16.1			15.6			14.0			16.1			
Peak Hour Factor Heavy Vehicles (%)	0.98	0.98	0.98	0.93	0.93	0.93	0.91	0.91	0.91	0.98	0.98	0.98		
Adj. Flow (vph)	59	52	56	16	43	41	54	344	9	12	197	38		
Shared Lane Traffic (%)	0	1/7	0	0	100	0	0	407	0	0	247	0		
Turn Type	Perm	NA	0	Perm	NA	U	Perm	407 NA	U	Perm	Z47 NA	0		
Protected Phases	_	5			5			1			1		2	
Permitted Phases	5	5		5	Б		1	1		1	1			
Switch Phase	J	J		J	J					1				
Minimum Initial (s)	8.0	8.0		8.0	8.0		8.0	8.0		8.0	8.0		1.0	
Minimum Split (s) Total Split (s)	13.0	13.0		13.0	13.0		13.0 25.0	13.0 25.0		13.0 25.0	13.0 25.0		22.0	
Total Split (%)	21.7%	21.7%		21.7%	21.7%		41.7%	41.7%		41.7%	41.7%		37%	
Maximum Green (s)	8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		18.0	
Yellow Time (s) All-Red Time (s)	3.0	3.0		3.0	3.0		3.0 2.0	3.0		3.0 2.0	3.0		2.0	
Lost Time Adjust (s)	2.0	0.0		2.0	0.0		2.0	0.0		2.0	0.0		2.0	
Total Lost Time (s)		5.0			5.0		Lood	5.0		اممر	5.0		Log	
Lead/Lag Lead-Lag Optimize?							Yes	Yes		Yes	Yes		Yes	
Vehicle Extension (s)	2.0	2.0		2.0	2.0		2.0	2.0		2.0	2.0		3.0	
Recall Mode	None	None		None	None		Max	Max		Max	Max		None	
Flash Dont Walk (s)													8.0	
Pedestrian Calls (#/hr)													6	
Act Effct Green (s)		8.3			8.3			23.4			23.4			
v/c Ratio		0.18			0.18			0.32			0.32			
Control Delay		23.7			14.5			11.8			9.0			
Queue Delay Total Delay		0.0			0.0			0.0			0.0 9.0			
LOS		C			В			В			A			
Approach Delay		23.7			14.5			11.8			9.0			
Approach LOS 90th %ile Green (s)	8.0	8.0		8.0	В 8.0		20.0	В 20.0		20.0	A 20.0		18.0	
90th %ile Term Code	Max	Max		Max	Max		MaxR	MaxR		MaxR	MaxR		Ped	
70th %ile Green (s)	8.0	8.0		8.0 Mox	8.0 Mox		20.0	20.0		20.0	20.0		0.0 Skip	
50th %ile Green (s)	8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		0.0	
50th %ile Term Code	Max	Max		Max	Max		MaxR	MaxR		MaxR	MaxR		Skip	
30th %ile Green (s) 30th %ile Term Code	8.0 Max	8.0 Max		8.0 Max	8.0 Max		20.0 MaxR	20.0 MaxR		20.0 MaxR	20.0 MaxR		0.0 Skip	
10th %ile Green (s)	8.0	8.0		8.0	8.0		35.0	35.0		35.0	35.0		0.0	
10th %ile Term Code	Max	Max		Max	Max		Dwell	Dwell		Dwell	Dwell		Skip	
Queue Length 50th (ft)		24 #131			58			44 #222			117			
Internal Link Dist (ft)		630			606			535			628			
Turn Bay Length (ft) Base Canacity (yph)		200			242			002			025			
Starvation Cap Reductn		0			0			0			733			
Spillback Cap Reductn		0			0			0			0			
Storage Cap Reductn Reduced v/c Ratio		0 54			0 29			0 45			0 26			
Intersection Summary		0.54			0.27			0.45			0.20			
Area Type: C	Other													
Cycle Length: 60														
Actuated Cycle Length: 45.4														
Control Type: Actuated-Uncoor	dinated													
Maximum v/c Ratio: 0.54				la l		00 D								
Intersection Signal Delay: 13.5 Intersection Capacity Utilization	59.2%			In	U Level of	LOS: B Service F	1							
Analysis Period (min) 15				10		L								
90th %ile Actuated Cycle: 60														
50th %ile Actuated Cycle: 38														
30th %ile Actuated Cycle: 38														
10th %ile Actuated Cycle: 53 # 95th percentile volume over	eds capac	tity queue	may he lo	nger										
Queue shown is maximum a	ifter two cy	cles.	may be lu	nger.										
Splits and Phases A. Doreho	stor Avonu	10 & Dichm	and Stree	h.										
	SICI AVEIIU	ις α KICHITI	unu əllee	.1				44						\$
101 25 s							2	n.⊫102 2s						13 s

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2		
Lane Configurations		4	1		\$		1	4Î		٦	4Î				
Traffic Volume (vph)	26	102	178	45	109	20	145	190	45	29	171	61			
Ideal Flow (vph)	1000	102	1000	40	109	1000	140	190	40	1000	1000	1000			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
Frt			0.850		0.984			0.971			0.961				
Fit Protected	0	0.990	1/15	0	0.987	0	0.950	1000	0	0.950	1010	0			
Satd. Flow (prot)	0	1881	1615	0	1845	0	1805	1830	0	1805	1813	0			
Satd. Flow (perm)	0	1881	1615	0	1845	0	840	1830	0	897	1813	0			
Right Turn on Red	0		Yes	Ū	1010	Yes	0.0	1000	Yes	077	1010	Yes			
Satd. Flow (RTOR)			236		4			11			14				
Link Speed (mph)		30			30			30			30				
LINK DISTANCE (IT) Travel Time (s)		14.0			16.1			537 12.2			620 14 1				
Peak Hour Factor	0.97	0.97	0.97	0.88	0.88	0.88	0.96	0.96	0.96	0.94	0.94	0.94			
Heavy Vehicles (%)	0%	0%	0%	0%	0%	0%	0%	1%	0%	0%	1%	0%			
Adj. Flow (vph)	27	105	184	51	124	23	151	198	47	31	182	65			
Lane Group Flow (vph)	0	132	184	0	198	0	151	245	0	31	247	0			
Turn Type	Split	NA	Perm	Split	NA	0	D.P+P	NA	0	Perm	NA	0			
Protected Phases	3	3		4	4		5	15			1		2		
Permitted Phases	0	0	3				1	4.5		1					
Switch Phase	3	3	3	4	4		5	15		1	I				
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0		5.0			10.0	10.0		1.0		
Minimum Split (s)	16.5	16.5	16.5	16.5	16.5		14.0			19.5	19.5		27.0		
Total Split (s)	23.0	23.0	23.0	20.0	20.0		15.0			35.0	35.0		27.0		
Total Split (%) Maximum Groop (c)	19.2%	19.2%	19.2%	16.7%	16./%		12.5%			29.2%	29.2%		23%		
Yellow Time (s)	4.0	4.0	4.0	3.5	3.5		3.0			3.5	3.5		2.0		
All-Red Time (s)	2.5	2.5	2.5	3.0	3.0		6.0			6.0	6.0		2.0		
Lost Time Adjust (s)		0.0	0.0		0.0		0.0			0.0	0.0				
Total Lost Time (s)	Lood	6.5	6.5	Log	6.5		9.0			9.5	9.5		Log		
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes					Yes	Yes		Yes		
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0		2.0			4.0	4.0		3.0		
Recall Mode	Max	Max	Max	Max	Max		Max			C-Max	C-Max		None		
Walk Time (s)													7.0		
Pedestrian Calls (#/hr)													9		
Act Effct Green (s)		38.1	38.1		13.5		32.0	40.5		25.5	25.5				
Actuated g/C Ratio		0.32	0.32		0.11		0.27	0.34		0.21	0.21				
v/c Ratio		0.22	0.27		0.94		0.56	0.39		0.16	0.62				
Queue Delay		0.0	0.0		0.0		0.0	20.4		41.3	40.2				
Total Delay		34.8	3.2		100.0		34.4	26.4		41.3	48.2				
LOS		С	A		F		С	С		D	D				
Approach LOS		16.4 B			100.0 F			29.4			47.5 D				
90th %ile Green (s)	16.5	16.5	16.5	13.5	13.5		6.0	0		25.5	25.5		23.0		
90th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Ped		
70th %ile Green (s)	43.5	43.5	43.5	13.5	13.5 May D		6.0			25.5	25.5		0.0		
50th %ile Green (s)	MaxR 43.5	MaxR 43.5	MaxR 43.5	13 5	13 5		MaxR 6.0			25 5	25 5		ОО		
50th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip		
30th %ile Green (s)	43.5	43.5	43.5	13.5	13.5		6.0			25.5	25.5		0.0		
30th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip		
10th %ile Green (S) 10th %ile Term Code	43.5 MaxR	43.5 MaxR	43.5 MaxR	13.5 MaxR	13.5 MaxR		6.0 MaxR			25.5 Coord	25.5 Coord		0.0 Skin		
Queue Length 50th (ft)	MUAIN	70	0	munt	152		72	163		20	165		Sinh		
Queue Length 95th (ft)		162	27		#290		m110	162		49	255				
Internal Link Dist (ft)		535			630			457			540				
Base Capacity (vph)		596	673		211		272	624		190	396				
Starvation Cap Reductn		0	0		0		0	0		0	0				
Spillback Cap Reductn		0	0		0		0	0		0	0				
Storage Cap Reductn		0 22	0 27		0 04		0 56	0 30		0 16	0 62				
Intersection Commons		0.22	0.27		0.74		0.50	0.37		0.10	0.02				
Area Type:	Other														
Cycle Length: 120	ounor														
Actuated Cycle Length: 120															
Offset: 65 (54%), Referenced t	o phase 1:N	NBSB, Sta	irt of Greer	1											
Control Type: Actuated-Coordi	nated														
Maximum v/c Ratio: 0.94															
Intersection Signal Delay: 41.9	- FO 401			In	tersection	LOS: D									
Intersection Capacity Utilization	n 58.4%			IC	U Level of	Service I	5								
# 95th percentile volume exc	eeds capac	ity, queue	may be lo	onger.											
Queue shown is maximum	after two cy	cles.													
m Volume for 95th percentile	queue is m	letered by	upstream	signal.											
Splits and Phases: 1: Washi	ngton St & I	Morton St	/Richmond	l St	2.0									4	
V 1 (R)					A Bø2				_	÷0	3			¥ Ø4	™ø5

	٨	\mathbf{r}	1	T.	Ŧ	¥	-	•	- ナ	4				
Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	SBR2	NEL2	NEL	NER	Ø2			
Lane Configurations	1	R.	٦	1	•		1	٦	_	1				
Traffic Volume (vph)	153	222	252	213	187	0	184	0	0	0				
ruture volume (vph)	1000	222	252	213	1000	1000	1000	1000	1000	1000				
Storage Length (ft)	75	0041	100	1900	1700	75	1900	1700	1900	1700				
Storage Lanes	1	1	1			1			1	1				
Taper Length (ft)	100		100						25					
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00				
Frt		0.850					0.850							
Flt Protected	0.950		0.950			_								
Satd. Flow (prot)	1/8/	1615	1805	1900	1863	0	1615	1863	0	1863				
Fit Permitted Satd. Flow (norm)	0.950	1615	1905	1000	1062	0	1615	1062	0	1062				
Pight Turn on Pod	1707	1015	1005	1900	1005	0	Vas	1005	0	Vas				
Satd. Flow (RTOR)							155			105				
Link Speed (mph)	30			30	30				30					
Link Distance (ft)	464			447	537				214					
Travel Time (s)	10.5			10.2	12.2				4.9					
Peak Hour Factor	0.95	0.95	0.99	0.99	0.96	0.96	0.96	0.92	0.92	0.92				
Heavy Vehicles (%)	1%	0%	0%	0%	2%	0%	0%	2%	2%	2%				
Adj. FIOW (VPR) Sharod Lano Traffic (%)	101	234	255	215	195	0	192	0	0	0				
ane Group Flow (vnh)	161	234	255	215	195	0	192	0	0	0				
Furn Type	Prot	pt+ov	Prot	NA	NA	U	Prot	Prot	U	Prot				
Protected Phases	3	13	1	15	5		5	4		4	2			
Permitted Phases	3										_			
Detector Phase	3	13	1	15	5		5	4		4				
Switch Phase														
Vinimum Initial (s)	10.0		10.0		10.0		10.0	4.0		4.0	1.0			
Minimum Split (s)	16.5		15.5		16.5		16.5	10.0		10.0	24.0			
rotal Split (S) Total Split (%)	27.0		34.0		29.0		29.0	10.0		10.0	26.0			
Maximum Green (s)	17.5%		20.3%		24.2%		24.2%	0.3% / N		0.3% / N	22%			
Yellow Time (s)	4.0		20.0		4.0		4.0	4.0		4.0	24.0			
All-Red Time (s)	2.5		2.5		2.5		2.5	2.5		2.5	0.0			
ost Time Adjust (s)	0.0		0.0		0.0		0.0	0.0		0.0	2.0			
Fotal Lost Time (s)	6.5		5.5		6.5		6.5	6.0		6.0				
_ead/Lag	Lead		Lead					Lag		Lag	Lag			
_ead-Lag Optimize?	Yes		Yes					Yes		Yes	Yes			
/ehicle Extension (s)	2.0		2.0		4.0		4.0	2.0		2.0	3.0			
Recall Mode	None		C-Max		None		None	None		None	None			
Flash Dont Walk (s)											15.0			
Pedestrian Calls (#/hr)											14			
Act Effct Green (s)	14.4	75.7	57.0	84.0	20.5		20.5							
Actuated g/C Ratio	0.12	0.63	0.48	0.70	0.17		0.17							
//c Ratio	0.75	0.23	0.30	0.16	0.62		0.48							
Control Delay	72.5	8.9	22.6	9.2	50.7		14.3							
Queue Delay	0.0	0.0	0.0	0.0	0.0		0.0							
	72.5 F	δ.9	22.0	9.Z	5U.7		14.3 R							
Approach Delay	34.8	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	Ŭ	16.5	32.7		U							
Approach LOS	С			В	С									
90th %ile Green (s)	16.5		32.3		28.7		28.7	0.0		0.0	22.0			
90th %ile Term Code	Max		Coord		Gap		Gap	Skip		Skip	Ped			
70th %ile Green (s)	16.5		37.3		23.7		23.7	0.0		0.0	22.0			
70th %ile Term Code	Max		Coord		Gap		Gap	Skip		Skip	Ped			
Soth %ile Green (S)	15./ Con		05.4 Coord		20.4		20.4	0.0 Ckin		0.0 Ckin	0.0			
Roth %ile Green (s)	12 2		71.1		0ap 17.1		0dp 17.1	0 U		0 U	0.0			
Both %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip			
10th %ile Green (s)	10.0		79.0		12.5		12.5	0.0		0.0	0.0			
0th %ile Term Code	Min		Coord		Gap		Gap	Skip		Skip	Skip			
Queue Length 50th (ft)	121	50	56	40	153		54							
Queue Length 95th (ft)	#197	102	240	103	m163		m22							
nternal Link Dist (ft)	384		100	367	457		75		134					
uni Bay Length (ft)	/5	1024	100	1210	272		/5							
Starvation Can Poducto	231	1034	000	1318	372		440							
Spillback Can Reductin	0	0	0	0	0		0							
Storage Cap Reductn	0	0	0	0	0		0							
Reduced v/c Ratio	0.70	0.23	0.30	0.16	0.52		0.43							
ntoreaction Summers														
	Other													
Cycle Length: 120	Outor													
Actuated Cycle Length: 120														
Offset: 0 (0%), Referenced to	o phase 1:NB	TL, Start o	of Green											
latural Cycle: 85														
Control Type: Actuated-Coor	dinated													
Aaximum v/c Ratio: 0.75						00.0								
ntersection Signal Delay: 27	.3			In	tersection	LOS: C								
Intersection Capacity Utilizati	1011 47.7%			IC	U Level of	Service A	4							
4 95th percentile volume er	vceeds canac	ity queue	may he lo	naer										
Queue shown is maximun	n after two cv	cles.	andy be lu	goi.										
m Volume for 95th percent	ile queue is m	netered by	upstream	signal.										
		,												
Splits and Phases: 2: Drive	eway & Wash	ington St	& River St	,										
1 (P)				1	602				-	2		1	I ∜Î ₀₅	
34 s				26	22				21	5			29 s	

2017003::1120 Washington Stree

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2
Lane Configurations	40	€	212	150	100	15	5	224	172	10	41	40	
Future Volume (vph)	40	152	213	158	190	15	213	224	172	18	326	69	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Storage Lanes	0		25	1		1	1		1	0		0	
Taper Length (ft)	25	1.00	1.00	25	1.00	1.00	25	1.00	1.00	25	0.05	0.05	
Frt	1.00	1.00	0.850	1.00	0.989	1.00	1.00	1.00	0.850	0.93	0.95	0.95	
Fit Protected	0	0.988	1415	0.950	1070	0	0.950	1000	1415	0	0.998	0	
Flt Permitted	0	0.656	1015	0.515	10/9	U	0.437	1900	1015	U	0.931	U	
Satd. Flow (perm)	0	1231	1615 Voc	978	1879	0	830	1900	1615 Voc	0	3277	0	
Satd. Flow (RTOR)			105		3	res			179		18	162	
Link Speed (mph)		30			30			30			30		
Travel Time (s)		10.2			15.3			10.1			14.0		
Peak Hour Factor	0.97	0.97	0.97	0.92	0.92	0.92	0.96	0.96	0.96	0.97	0.97	0.97	
Adj. Flow (vph)	49	157	220	172	207	16	222	233	179	19	336	71	
Shared Lane Traffic (%)	0	206	220	172	223	0	222	222	170	0	126	0	
Turn Type	Perm	NA	pt+ov	Perm	NA	U	D.P+P	NA	Prot	Perm	NA	U	
Protected Phases	5	5	56	5	5		6	16	16	1	1		2
Detector Phase	5	5	56	5	5		6	16	16	1	1		
Switch Phase Minimum Initial (s)	10.0	10.0		10.0	10.0		8.0			10.0	10.0		10
Minimum Split (s)	18.0	18.0		18.0	18.0		14.5			17.5	17.5		32.0
Total Split (s) Total Split (%)	39.0 32.5%	39.0 32.5%		39.0 32.5%	39.0 32.5%		16.0 13.3%			33.0 27.5%	33.0 27.5%		32.0 27%
Maximum Green (s)	31.0	31.0		31.0	31.0		9.5			25.5	25.5		28.0
Yellow Time (s)	4.5	4.5		4.5	4.5		3.0			4.0	4.0		2.0
Lost Time Adjust (s)	5.5	0.0		0.0	0.0		0.0			0.0	0.0		2.0
Total Lost Time (s)	Lead	8.0 Lead		8.0 Lead	8.0 Lead		6.5 Lag			Lead	7.5 Lead		lan
Lead-Lag Optimize?	Yes	Yes		Yes	Yes		Yes			Yes	Yes		Yes
Vehicle Extension (s) Recall Mode	2.0 None	2.0 None		2.0 None	2.0 None		4.0 None			2.0 C-Max	2.0 C-Max		3.0 None
Walk Time (s)	None	None		None	None		None			0 Max	0 Max		7.0
Flash Dont Walk (s) Pedestrian Calls (#/hr)													21.0 43
Act Effct Green (s)		24.2	43.0	24.2	24.2		49.2	54.7	54.7		35.9		10
Actuated g/C Ratio v/c Ratio		0.20 0.83	0.36 0.34	0.20 0.88	0.20 0.59		0.41 0.50	0.46 0.27	0.46 0.21		0.30		
Control Delay		62.3	6.7	83.9	48.0		30.8	25.8	4.6		38.2		
Total Delay		0.0 62.3	0.0 6.7	0.0 83.9	0.0 48.0		0.0 30.8	0.0 25.8	0.0 4.6		0.0 38.2		
LOS		E	А	F	D		С	C	А		D		
Approach LOS		33.0 C			03.0 E			21.0 C			38.2 D		
90th %ile Green (s)	31.0	31.0		31.0	31.0		9.5			25.5	25.5		28.0 Dod
70th %ile Green (s)	30.3	30.3		30.3	30.3		10.2			25.5	25.5		28.0
70th %ile Term Code	Gap	Gap 25.5		Gap	Gap 25.5		Max 15.0			Coord	Coord		Ped 28.0
50th %ile Term Code	Gap	Gap		Gap	Gap		Max			Coord	Coord		Ped
30th %ile Green (s)	20.5 Gap	20.5 Gap		20.5 Gap	20.5 Gap		17.3 Gap			28.2	28.2 Coord		28.0 Pod
10th %ile Green (s)	13.5	13.5		13.5	13.5		9.8			74.7	74.7		0.0
10th %ile Term Code Oueue Length 50th (ft)	Gap	Gap 162	73	Gap 128	Gap 153		Gap 116	124	0	Coord	Coord 151		Skip
Queue Length 95th (ft)		250	43	#217	222		193	204	49		206		
Internal Link Dist (ft) Turn Bay Length (ft)		367	25		593			363			535		
Base Capacity (vph)		318	624	252	487		441	866	833		992		
Starvation Cap Reductn		0	0	0	0		0	0	0		0		
Storage Cap Reductn		0	0	0	0		0	0	0		0		
Reduced v/c Ratio		0.65	0.35	0.68	0.46		0.50	0.27	0.21		0.43		
Intersection Summary Area Type:	Other												
Cycle Length: 120	o unor												
Actuated Cycle Length: 120 Offset: 25 (21%), Referenced to	to phase 1.1	VBSB, Sta	rt of Greer	1									
Natural Cycle: 85	, i	. <u>_</u> , otu											
Control Type: Actuated-Coordi Maximum v/c Ratio: 0.88	nated												
Intersection Signal Delay: 36.9	70.001			In	tersection	LOS: D	0						
Intersection Capacity Utilizatio Analysis Period (min) 15	n 70.9%			IC	U Level of	Service	L I						
# 95th percentile volume exc	eeds capac	city, queue	may be lo	nger.									
Queue shown is maximum	arter two cy	cies.											
Splits and Phases: 3: Adam	s St & Wasl	hington St	& Dorches	ster Ave									. 1
₩ø1 (R)				÷.	Ø2						Ø5		\$ 706
33 S				32 s						3	9 S		16 s

2017003::1120 Washington Stree

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2		
Lane Configurations		4			4			4			4				
Traffic Volume (vph)	41	50 50	52 52	48	76	54 54	46	205	21	12	301	31			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
Ped Bike Factor Frt		0.951			0.959			1.00			1.00				
Flt Protected		0.986			0.987			0.992			0.998				
Satd. Flow (prot)	0	1782	0	0	1798	0	0	1863	0	0	1870	0			
Fit Permitted Satd, Elow (perm)	0	0.800	0	0	0.847	0	0	0.900	0	0	0.988	0			
Right Turn on Red	0	1440	Yes	0	1040	Yes	0	1070	Yes	0	1051	Yes			
Satd. Flow (RTOR)		38			28			6			8				
Link Speed (mph)		30 710			30 686			30 615			30 708				
Travel Time (s)		16.1			15.6			14.0			16.1				
Confl. Bikes (#/hr)	0.07	0.07	0.07	0.05	0.05	0.05	0.04		1	0.07	0.07	1			
Peak Hour Factor Heavy Vehicles (%)	0.97	0.97	0.97	0.95	0.95	0.95	0.94	0.94	0.94	0.97	0.97	0.97			
Adj. Flow (vph)	42	52	54	51	80	57	49	218	22	12	310	32			
Shared Lane Traffic (%)		4.40		-	400			000	0		05.4				
Lane Group Flow (vpn) Turn Type	Perm	148 NA	0	Perm	188 NA	0	Perm	289 NA	U	Perm	354 NA	0			
Protected Phases	1 Gilli	5		1 01111	5		1 0111	1		1 0111	1		2		
Permitted Phases	5	F		5	-		1	1		1	1				
Switch Phase	5	5		5	5		1	1		1	1				
Minimum Initial (s)	8.0	8.0		8.0	8.0		8.0	8.0		8.0	8.0		1.0		
Minimum Split (s)	13.0	13.0		13.0	13.0		13.0	13.0		13.0	13.0		22.0		
Total Split (s) Total Split (%)	20.0	20.0		20.0	20.0		28.0	28.0		28.0	28.0		22.0		
Maximum Green (s)	15.0	15.0		15.0	15.0		23.0	23.0		23.0	23.0		18.0		
Yellow Time (s)	3.0	3.0		3.0	3.0		3.0	3.0		3.0	3.0		2.0		
All-Red Time (s)	2.0	2.0		2.0	2.0		2.0	2.0		2.0	2.0		2.0		
Total Lost Time (s)		5.0			5.0			5.0			5.0				
Lead/Lag							Lead	Lead		Lead	Lead		Lag		
Lead-Lag Optimize?	2.0	2.0		2.0	2.0		Yes 2.0	Yes 2.0		Yes 2.0	Yes 2.0		Yes 3.0		
Recall Mode	None	None		None	None		C-Max	C-Max		C-Max	C-Max		None		
Walk Time (s)													8.0		
Pedestrian Calls (#/hr)													33		
Act Effct Green (s)		11.4			11.4			39.8			39.8		55		
Actuated g/C Ratio		0.16			0.16			0.57			0.57				
V/C Ratio Control Delay		0.56			0.69			0.30			0.34				
Queue Delay		0.0			0.0			0.0			0.0				
Total Delay		27.6			36.2			13.2			13.3				
LUS Approach Delay		27.6			2 36 2			В 13.2			В 13.3				
Approach LOS		C			D			B			B				
90th %ile Green (s)	15.0	15.0		15.0	15.0		23.0	23.0		23.0	23.0		18.0		
70th %ile Term Code	13.5	13.5		13.5	13.5		24.5	24 5		24.5	24 5		18 0		
70th %ile Term Code	Gap	Gap		Gap	Gap		Coord	Coord		Coord	Coord		Ped		
50th %ile Green (s)	11.3	11.3		11.3	11.3		48.7	48.7 Coord		48.7 Coord	48.7 Coord		0.0 Chin		
30th %ile Green (s)	9.1	9.1		9.1	9.1		50.9	50.9		50.9	50.9		0.0		
30th %ile Term Code	Gap	Gap		Gap	Gap		Coord	Coord		Coord	Coord		Skip		
10th %ile Green (s)	8.0 Min	8.0		8.0	8.0 Mip		52.0	52.0		52.0	52.0		0.0 Skip		
Queue Length 50th (ft)	IVIIII	44		IVIIII	65		COOLO	36		COOLO	45		эмр		
Queue Length 95th (ft)		92			121			167			201				
Internal Link Dist (ft)		630			606			535			628				
Base Capacity (vph)		339			352			963			1056				
Starvation Cap Reductn		0			0			0			0				
Spillback Cap Reductn		0			0			0			0				
Reduced v/c Ratio		0.44			0.53			0.30			0.34				
Intersection Summary															
Area Type: C	Other														
Cycle Length: 70															
Actuated Cycle Length: /0 Offset: 45 (64%) Referenced to	n nhase 1-A	IRSR Stor	t of Green												
Natural Cycle: 60	phase 1.1	JJD, Jtdl	or orcen												
Control Type: Actuated-Coordin	nated														
Intersection Signal Delay: 19.8				Int	ersection I	OS' B									
Intersection Capacity Utilization	1 54.4%			IC	U Level of	Service A	1								
Analysis Period (min) 15															
Splits and Phases: 4. Dorche	ster Ave/D	orchester '	St & Richm	nond St											
							11							<u>.</u>	
₩101(R) 28 c							7.5 22 c	Ø2						<u>₹</u> ¶05	

• No-Build (2024) Condition

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2	
Lane Configurations		د ا	1		4		٦	ţ,		٦	ţ,			
Traffic Volume (vph)	40	102	144	32	95	35	300	295	65	42	147	33		
Ideal Flow (vphpl)	1900	1900	1900	32 1900	95	35 1900	1900	295	00 1900	42	147	33 1900		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		
Frt			0.850		0.971			0.973			0.972			
Fit Protected Sate Flow (prot)	0	0.986	1615	0	0.990	٥	0.950	1010	0	0.950	1022	0		
Flt Permitted	0	0.986	1015	0	0.990	0	0.576	1017	0	0.206	1032	U		
Satd. Flow (perm)	0	1873	1615	0	1826	0	1094	1819	0	380	1832	0		
Right Turn on Red			Yes		0	Yes		10	Yes		0	Yes		
Link Speed (mph)		30	230		30			30			30			
Link Distance (ft)		615			710			537			620			
Travel Time (s)		14.0			16.1			12.2			14.1			
Peak Hour Factor	0.95	0.95	0.95	0.86	0.86	0.86	0.94	0.94	0.94	0.92	0.92	0.92		
Adj. Flow (vph)	42	107	152	37	110	41	319	314	69	46	160	36		
Shared Lane Traffic (%)														
Lane Group Flow (vph)	0 Colit	149	152	0 Calit	188	0	319	383	0	46	196	0		
Protected Phases	Spiit 3	3	Pelm	Spiit 4	4		D.P+P 5	1.5		Perm	1		2	
Permitted Phases	0	U	3				1			1	•		2	
Detector Phase	3	3	3	4	4		5	15		1	1			
Switch Phase Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0		5.0			10.0	10.0		10	
Minimum Split (s)	16.5	16.5	16.5	16.5	16.5		14.0			19.5	19.5		27.0	
Total Split (s)	23.0	23.0	23.0	19.0	19.0		15.0			36.0	36.0		27.0	
Total Split (%)	19.2%	19.2%	19.2%	15.8%	15.8%		12.5%			30.0%	30.0%		23%	
Yellow Time (s)	16.5	16.5	16.5 4 0	12.5	12.5		6.0 3.0			26.5	26.5		23.0	
All-Red Time (s)	2.5	2.5	2.5	3.0	3.0		6.0			6.0	6.0		2.0	
Lost Time Adjust (s)		0.0	0.0		0.0		0.0			0.0	0.0			
Total Lost Time (s)	Load	6.5	6.5	Lag	6.5		9.0			9.5	9.5		lag	
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes					Yes	Yes		Yes	
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0		2.0			4.0	4.0		3.0	
Recall Mode	Max	Max	Max	Max	Max		Max			C-Max	C-Max		lone	
Flash Dont Walk (s)													7.0	
Pedestrian Calls (#/hr)													16	
Act Effct Green (s)		32.7	32.7		12.5		33.0	41.5		26.5	26.5			
Actuated g/C Ratio		0.27	0.27		0.10		0.28	0.35		0.22	0.22			
Control Delay		41.2	1.1		103.3		76.9	37.8		68.7	43.3			
Queue Delay		0.0	0.0		0.0		0.0	0.5		0.0	0.0			
Total Delay		41.2	1.1		103.3		76.9	38.3		68.7 E	43.3			
Approach Delay		21.0	A		103.3		L	55.8		L	48.1			
Approach LOS		С			F			E			D			
90th %ile Green (s)	16.5	16.5	16.5	12.5	12.5		6.0			26.5	26.5		23.0 Dod	
70th %ile Green (s)	16.5	16.5	16.5	12.5	12.5		6.0			26.5	26.5		23.0	
70th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Ped	
50th %ile Green (s)	43.5	43.5	43.5	12.5	12.5		6.0			26.5	26.5		0.0	
Soth %ile Ferm Code	MaxR 43.5	MaxR 43.5	MaxR 43.5	MaxR 12.5	MaxR 12.5		MaxR 6.0			26 5	26 5		0.0	
30th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip	
10th %ile Green (s)	43.5	43.5	43.5	12.5	12.5		6.0			26.5	26.5		0.0	
10th %ile Term Code	MaxR	MaxR 70	MaxR	MaxR	MaxR 140		MaxR 192	170		Coord	Coord		Skip	
Queue Length 95th (ft)		180	1		#267		m#340	m173		#87	203			
Internal Link Dist (ft)		535			630			457			540			
Turn Bay Length (ft)		F10	(11		100		227	(25		02	411			
Starvation Can Reductn		510	0		198		336	635 53		83	411			
Spillback Cap Reductn		0	0		0		0	0		0	0			
Storage Cap Reductn		0	0		0		0	0		0	0			
Reduced v/c Ratio		0.29	0.25		0.95		0.95	0.66		0.55	0.48			
Intersection Summary	01													
Area Type: Cycle Length: 120	Other													
Actuated Cycle Length: 120														
Offset: 11 (9%), Referenced to	o phase 1:N	BSB, Starl	t of Green											
Natural Cycle: 95 Control Type: Actuated Coord	linatod													
Maximum v/c Ratio: 0.95	mated													
Intersection Signal Delay: 53.4	4			In	tersection	LOS: D								
Intersection Capacity Utilizatio	on 64.6%			IC	CU Level of	Service (;							
# 95th percentile volume exe	ceeds capac	ity, queue	may be lo	onger										
Queue shown is maximum	after two cy	cles.												
m Volume for 95th percentile	e queue is m	netered by	upstream	signal.										
Splits and Phases: 1: Wash	nington St &	Morton St.	/Richmond	l St										
	y				11 m						30		7	≜ ar
¥101(K)					202						دھ		▼ 104	601

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Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	SBR2	NEL2	NEL	NER	Ø2
Lane Configurations	۲	R.	٦	1	1		1	٦		1	
Future Volume (vph)	268	250	196	405	148	0	144	0	0	0	
ruture volume (vpn)	1000	250	190	405	148	1000	144	1000	1000	1000	
Storage Length (ff)	75	1700	100	1700	1900	75	1900	1700	1700	1700	
Storage Lanes	1	1	1			1			1	1	
Taper Length (ft)	100		100						25		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Frt		0.850					0.850				
Flt Protected	0.950	1/15	0.950	1000	1000	0	1/15	10/2	0	10/2	
Satd. Flow (prot)	1805	1615	1/8/	1900	1900	0	1615	1863	0	1863	
Satd Flow (norm)	1805	1615	1787	1000	1000	0	1615	1863	0	1863	
Right Turn on Red	1005	1015	1707	1700	1700	0	Yes	1005	0	Yes	
Satd. Flow (RTOR)							173			100	
Link Speed (mph)	30			30	30				30		
Link Distance (ft)	464			447	537				214		
Travel Time (s)	10.5			10.2	12.2				4.9		
Peak Hour Factor	0.97	0.97	0.94	0.94	0.88	0.88	0.88	0.92	0.92	0.92	
Adi Flow (vph)	276	258	200	//31	168	170	164	270	2 %	270	
Shared Lane Traffic (%)	270	200	207	-+51	100	U	104	U	U	U	
Lane Group Flow (vph)	276	258	209	431	168	0	164	0	0	0	
Turn Type	Prot	pt+ov	Prot	NA	NA	-	Prot	Prot		Prot	
Protected Phases	3	13	1	15	5		5	4		4	2
Permitted Phases											
Detector Phase	3	13	1	15	5		5	4		4	
Switch Phase	10.0		10.0		10.0		10.0				4.0
Minimum Initial (s)	10.0		10.0		10.0		10.0	4.0		4.0	1.0
iviiriimum Spiit (S) Total Split (s)	16.5		15.5		16.5		16.5	10.0		10.0	26.0
Total Split (%)	27.0		33.U 27.5%		24.0		24.0	8.3%		8.3%	20.U 22%
Maximum Green (s)	20.5		27.5		17.5		17.5	4.0		4,0	22.0
Yellow Time (s)	4.0		3.0		4.0		4.0	3.5		3.5	2.0
All-Red Time (s)	2.5		2.5		2.5		2.5	2.5		2.5	2.0
Lost Time Adjust (s)	0.0		0.0		0.0		0.0	0.0		0.0	
Total Lost Time (s)	6.5		5.5		6.5		6.5	6.0		6.0	
Lead/Lag	Lead		Lead					Lag		Lag	Lag
Lead-Lag Optimize?	Yes		Yes		4.0		4.0	Yes		Yes	Yes
Pecall Mode	Z.U None		C-Max		4.0 None		4.0 None	Z.U None		Z.U None	3.0 None
Walk Time (s)	NONC		C-IVIGA		NUTC		NUTIC	NOTIC		NONC	7.0
Flash Dont Walk (s)											15.0
Pedestrian Calls (#/hr)											7
Act Effct Green (s)	22.1	81.1	53.6	80.7	20.6		20.6				
Actuated g/C Ratio	0.18	0.68	0.45	0.67	0.17		0.17				
v/c Ratio	0.83	0.24	0.26	0.34	0.52		0.39				
Control Delay	68.2	8.2	11.5	2.7	52.6		16.9				
Queue Delay	0.0	0.0	0.0	0.4	0.0		0.0				
	00.2 F	0.2	B R	Δ	J2.0		10.7 B				
Approach Delay	39.2	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	D	5.8	35.0		U				
Approach LOS	D			А	С						
90th %ile Green (s)	20.5		27.5		27.5		27.5	0.0		0.0	22.0
90th %ile Term Code	Max		Coord		Max		Max	Skip		Skip	Ped
70th %ile Green (s)	26.7		49.9		24.9		24.9	0.0		0.0	0.0
/0th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip
Sout Wile Green (S)	24.6 Con		55./		21.2 Con		21.2	0.0 Skin		0.0 Skip	U.U Skin
30th %ile Green (s)	Gap 21.6		COOLO		Gap 16.6		Gap 16.6	SKIP		SKIP	ол
30th %ile Term Code	Gan		Coord		Gan		Gan	Skin		Skin	Skin
10th %ile Green (s)	17.2		71.7		12.6		12.6	0.0		0.0	0.0
10th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip
Queue Length 50th (ft)	202	58	46	4	131		32	·		·	
Queue Length 95th (ft)	#369	109	m149	120	m181		m77				
Internal Link Dist (ft)	384		100	367	457		75		134		
Length (II) Base Canacity (uph)	/5	1101	100	1061	244		/5				
Starvation Can Reducts	342	1101	198	204	344		434				
Spillback Can Reductin	0	0	0	370	0		0				
Storage Cap Reductn	0	0	0	0	0		0				
Reduced v/c Ratio	0.81	0.23	0.26	0.50	0.49		0.38				
Intersection Summany											
Area Type:	Other										
Cycle Length: 120	Unici										
Actuated Cycle Length: 120											
Offset: 0 (0%), Referenced to	phase 1:NB	TL, Start o	of Green								
Natural Cycle: 85	·										
Control Type: Actuated-Coor	dinated										
Maximum v/c Ratio: 0.83						100 5					
Intersection Signal Delay: 24	.]			In	tersection	LOS: C					
Intersection Capacity Utilizati	ion 49.5%			IC	U Level of	Service A	4				
# 95th percentile volume or	vreeds capac	ity guous	may he le	naer							
Queue shown is maximum	n after two cv	cles.	andy De IC	nger.							
m Volume for 95th percenti	ile queue is m	netered by	upstream	signal.							
				J							
Splits and Phases: 2: Drive	eway & Wash	ington St	& River St							-	
1 (1)				1.1					1	A	
33 s				26.0	202				27.0	د ש	

2017003::1120 Washington Street

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2
Lane Configurations	66	ہ	164	125	161	20	205	207	207	6	41	07	
Future Volume (vph)	66	208	164	135	161	20	385	307	387	6	166	87	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Storage Length (It) Storage Lanes	0		25 1	1		50	1		1	0		0	
Taper Length (ft)	25	1.00	4.00	25	1.00	1.00	25	1.00	1.00	25	0.05	0.05	
Lane Util. Factor Frt	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.95	0.95	0.95	
Flt Protected		0.988	0.000	0.950	0.700		0.950		0.000		0.999		
Satd. Flow (prot) Elt Permitted	0	1863	1615	1805 0 379	1851	0	1787	1900	1615	0	3389	0	
Satd. Flow (perm)	0	1412	1615	720	1851	0	1093	1900	1615	0	3203	0	
Right Turn on Red			Yes		E	Yes			Yes		44	Yes	
Link Speed (mph)		30	11		30			30	399		30		
Link Distance (ft)		447			673			443			615		
Peak Hour Factor	0.96	0.96	0.96	0.92	0.92	0.92	0.97	0.97	0.97	0.98	0.98	0.98	
Heavy Vehicles (%)	0%	1%	0%	0%	1%	0%	1%	0%	0%	0%	1%	1%	
Adj. Flow (vph) Shared Lane Traffic (%)	69	217	1/1	147	1/5	22	397	316	399	6	169	89	
Lane Group Flow (vph)	0	286	171	147	197	0	397	316	399	0	264	0	
Turn Type Protected Phases	Perm	NA 5	pt+ov 5.6	Perm	NA 5		D.P+P	NA 1.6	Prot 1.6	Perm	NA 1		2
Permitted Phases	5	J	50	5	5		1	10	10	1	1		2
Detector Phase	5	5	56	5	5		6	16	16	1	1		
Minimum Initial (s)	10.0	10.0		10.0	10.0		8.0			10.0	10.0		1.0
Minimum Split (s)	18.0	18.0		18.0	18.0		14.5			17.5	17.5		32.0
Total Split (S) Total Split (%)	39.0 32.5%	39.0 32.5%		39.0 32.5%	39.0 32.5%		22.0			27.0	27.0		32.0 27%
Maximum Green (s)	31.0	31.0		31.0	31.0		15.5			19.5	19.5		28.0
Yellow Time (s) All-Red Time (s)	4.5	4.5		4.5	4.5		3.0			4.0	4.0		2.0
Lost Time Adjust (s)	0.0	0.0		0.0	0.0		0.0			0.0	0.0		2.0
Total Lost Time (s)	beol	0.8		0.8 bool	0.8		6.5			bool	7.5		120
Lead-Lag Optimize?	Yes	Yes		Yes	Yes		Yes			Yes	Yes		Yes
Vehicle Extension (s)	2.0	2.0		2.0	2.0		4.0			2.0	2.0		3.0 Name
Walk Time (s)	None	None		None	None		None			C-Max	C-IVIAX		7.0
Flash Dont Walk (s)													21.0
Pedestrian Calls (#/hr) Act Effct Green (s)		27.1	52.0	27.1	27.1		46.3	51.8	51.8		26.9		49
Actuated g/C Ratio		0.23	0.43	0.23	0.23		0.39	0.43	0.43		0.22		
v/c Ratio Control Delay		0.90 71.5	0.23 9.5	0.90 94 1	0.47 42.0		0.75 41.5	0.39 29.0	0.43 4.3		0.34		
Queue Delay		0.0	0.0	0.0	0.0		0.0	0.0	0.0		0.0		
Total Delay		71.5 F	9.5 Δ	94.1 F	42.0 D		41.5 D	29.0 C	4.3 Δ		33.9		
Approach Delay		48.3	~		64.3		D	24.6	~		33.9		
Approach LOS	21.0	D		21.0	21.0		15.5	С		10 5	C 10 5		20.0
90th %ile Term Code	Max	Max		Max	Max		Max			Coord	Coord		Ped
70th %ile Green (s)	31.0 Mox	31.0 Mox		31.0 Mox	31.0 Mov		15.5 Max			19.5 Coord	19.5 Coord		28.0 Dod
50th %ile Green (s)	29.8	29.8		29.8	29.8		16.7			19.5	19.5		28.0
50th %ile Term Code	Gap	Gap		Gap	Gap		Max			Coord	Coord		Ped
30th %ile Term Code	25.2 Gap	25.2 Gap		25.2 Gap	25.2 Gap		ZT.3 Max			Coord	Coord		28.0 Ped
10th %ile Green (s)	18.7	18.7		18.7	18.7		22.6			56.7	56.7		0.0
Oueue Length 50th (ft)	Gap	Gap 147	14	Gap 108	Gap 125		Gap 249	188	0	Coord	Coord 73		Sкip
Queue Length 95th (ft)		#348	66	#221	195		#346	278	67		117		
Internal Link Dist (ft) Turn Bay Length (ft)		367	25		593			363			535		
Base Capacity (vph)		364	720	186	481		527	819	923		769		
Starvation Cap Reductn		0	0	0	0		0	0	0		0		
Storage Cap Reductn		0	0	0	0		0	0	0		0		
Reduced v/c Ratio		0.79	0.24	0.79	0.41		0.75	0.39	0.43		0.34		
Intersection Summary	Othor												
Cycle Length: 120	Outer												
Actuated Cycle Length: 120	to phase 1	NDCD C+-	rt of Cross	n									
Natural Cycle: 95	no priase ra	INBSB, Sla	It of Gree	n									
Control Type: Actuated-Coordi	inated												
Intersection Signal Delay: 37.0)			Int	ersection L	OS: D							
Intersection Capacity Utilization	n 79.8%			IC	U Level of	Service [)						
Analysis Period (min) 15 # 95th percentile volume exc	ceeds capac	ity, queue r	nay be lo	nger.									
Queue shown is maximum	after two cy	cles.		5									
Splits and Phases: 3: Adam	s St & Wash	nington St &	Dorches	ter Ave									
Ø1 (R)			Har	,					\$	05			S 06
27 s			32 s	-					39 s	23			22 s

2017003::1120 Wash	nington Street
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	Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2	
	Lane Configurations		4			4			4			4			
	Future Volume (vph)	62	55 55	59 59	16 16	43	41	53 53	336 336	9	13	207	40 40		
μα μα <thμα< th=""> μα μα μα<</thμα<>	Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900		
n i no se	Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		
Set Ale applice D <thd< th=""> D D D D</thd<>	Fit Protected		0.955			0.944			0.997			0.979			
1 Herminion 0 1 Herminion 0 1 Not 0 <th0< th=""> <th0< td=""><td>Satd. Flow (prot)</td><td>0</td><td>1772</td><td>0</td><td>0</td><td>1779</td><td>0</td><td>0</td><td>1865</td><td>0</td><td>0</td><td>1842</td><td>0</td><td></td><td></td></th0<></th0<>	Satd. Flow (prot)	0	1772	0	0	1779	0	0	1865	0	0	1842	0		
	Fit Permitted Satd. Flow (perm)	0	0.863	0	0	0.938	0	0	0.928	0	0	0.975	0		
sake field field in a second s	Right Turn on Red	_		Yes	-		Yes			Yes	-		Yes		
une clame need to a set of a	Satd. Flow (RTOR)		35			44			2			16 30			
Trave The view of view	Link Distance (ft)		710			686			615			708			
Construction Obs Obs< Obs Obs< Obs Obs< Obs Obs Obs Obs Obs Obs Obs Obs Obs< Obs	Travel Time (s)	0.00	16.1	0.00	0.02	15.6	0.02	0.01	14.0	0.01	0.00	16.1	0.00		
Application Appl	Heavy Vehicles (%)	0.98	0.98	2%	0.93	0.93	0.93	0.91	1%	0.91	0.98	0.98	0.98		
Sand Later (1974) O O No. Vol. Vol. <td>Adj. Flow (vph)</td> <td>63</td> <td>56</td> <td>60</td> <td>17</td> <td>46</td> <td>44</td> <td>58</td> <td>369</td> <td>10</td> <td>13</td> <td>211</td> <td>41</td> <td></td> <td></td>	Adj. Flow (vph)	63	56	60	17	46	44	58	369	10	13	211	41		
Tur Type Perin NA T T T Devolve (free of the set	Shared Lane Traffic (%)	0	179	0	0	107	0	0	437	0	0	265	0		
Name of a point point of the set of t	Turn Type	Perm	NA	-	Perm	NA	-	Perm	NA	-	Perm	NA			
Decision Phase S S S I I I I Mithiam Find(A) 80 80 80 80 80 10 Mithiam Find(A) 100 100 100 100 100 100 Mithiam Find(A) 80 80 80 10 100 Mithiam Find(A) 80 80 80 80 10 Mithiam Find(A) 80 80 80 80 80 Mithiam Find(A) 80 80 80 80 80 Mithiam Find(A) 80 80 80 80 80 Mithiam Find(A) 90 20 20 20 20 20 Mithiam Find(A) 90 20 20 20 20 20 Mithiam Find(A) 90 90 90 90 90 Mithiam Find(A) 90 90 90 90 90 Mithiam Find(A) 90 90 90 90 90 Mithiam Find(A) 90 90 90 90 Mithiam Find(A) 90 90 90 90 Mithiam Find(A) 90 90 90 90 <	Protected Phases Permitted Phases	5	5		5	5		1	1		1	1		2	
Saka Pane Saka Pane	Detector Phase	5	5		5	5		1	1		1	1			
n man man man man man man man man man ma	Switch Phase	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0		10	
Totad Split 0 110 110 110 110 120 250 250 250 250 250 250 Mathematic fields 100 100 100 100 100 100 100 Mathematic fields 100 00 00 00 100 100 Mathematic fields 100 00 00 00 100 Mathematic fields 100 00 00 100 Mathematic fields 100 00 00 100 Mathematic fields 100 100 100 100 <t< td=""><td>Minimum Split (s)</td><td>13.0</td><td>8.0 13.0</td><td></td><td>8.0</td><td>8.0</td><td></td><td>8.0</td><td>8.0</td><td></td><td>8.0</td><td>8.0</td><td></td><td>22.0</td><td></td></t<>	Minimum Split (s)	13.0	8.0 13.0		8.0	8.0		8.0	8.0		8.0	8.0		22.0	
Tools Set (V) 21.75 21.75 21.75 41.75 41.75 41.75 41.75 41.75 41.75 41.75 41.75 41.75 41.75 376 Market Imre(s) 20 20 20 20 20 20 20 20 Market Imre(s) 30 30 30 30 30 30 Total Leaf Imre(s) 30 20 20 20 20 20 Total Leaf Imre(s) 30 50 50 50 50 Total Leaf Imre(s) 30 20 20 20 20 30 Market Imre(s) 30 10 100 100 100 Market Imre(s) 30 10 100 100 100 Market Imre(s) 10 10 10 100 100 Market Imre(s) 10 10 100 100 100 Market Imre(s) 10 10 10 100 100	Total Split (s)	13.0	13.0		13.0	13.0		25.0	25.0		25.0	25.0		22.0	
Yateva Time (a) 10 </td <td>Total Split (%) Maximum Green (s)</td> <td>21.7%</td> <td>21.7%</td> <td></td> <td>21.7%</td> <td>21.7%</td> <td></td> <td>41.7%</td> <td>41.7%</td> <td></td> <td>41.7%</td> <td>41.7%</td> <td></td> <td>37% 18.0</td> <td></td>	Total Split (%) Maximum Green (s)	21.7%	21.7%		21.7%	21.7%		41.7%	41.7%		41.7%	41.7%		37% 18.0	
All Bold Time Agine (a) 20 30 100 <	Yellow Time (s)	3.0	3.0		3.0	3.0		3.0	3.0		3.0	3.0		2.0	
Unit into a bit of	All-Red Time (s)	2.0	2.0		2.0	2.0		2.0	2.0		2.0	2.0		2.0	
Lacella go ne series en entre en entre ent	Total Lost Time (s)		5.0			5.0			5.0			5.0			
Under Lag Unput 20 20	Lead/Lag							Lead	Lead		Lead	Lead		Lag	
None None <t< td=""><td>Lead-Lag Optimize? Vehicle Extension (s)</td><td>2.0</td><td>2.0</td><td></td><td>2.0</td><td>2.0</td><td></td><td>Yes 2.0</td><td>Yes 2.0</td><td></td><td>Yes 2.0</td><td>Yes 2.0</td><td></td><td>Yes 3.0</td><td></td></t<>	Lead-Lag Optimize? Vehicle Extension (s)	2.0	2.0		2.0	2.0		Yes 2.0	Yes 2.0		Yes 2.0	Yes 2.0		Yes 3.0	
Walk Ten: (s) 8.0 Feak-back (Ma) 8.3 8.3 2.4 2.4 0 Tendestion (Sk) (Ma) 8.3 8.3 2.4 2.4 0 Standard (C Ska) (Ma) 0.37 0.31 0.49 0.28 Vic Ratio 0.37 0.31 0.49 0.28 Cardal Dalay 2.4.0 1.4.7 1.28 9.2 Obuse Delay 0.0 0.0 0.0 0.0 USS C 8 8.2 2.4 Mi Ma Corea (S) 8.0 8.0 2.0 2.0 2.0 USS C 8 8.4 9.4 Mi Ma Corea (S) 8.0 8.0 2.00 2.00 2.00 USS C 8 0.0 0.0 0.0 USS Max Max Max Max Reve Nac Reve USS Nac Gorea (S) 8.0 8.0 8.0 2.00 2.00 2.00 2.00 USS Standard Corea (S) 8.0 8.0 8.0 8.0 8.0 8.0 8.0 USS Standard Corea (S) 8.0 8.0 8.0 8.0 8.0 8.0 USS Standard Corea (S) 8.0 8.0 <td>Recall Mode</td> <td>None</td> <td>None</td> <td></td> <td>None</td> <td>None</td> <td></td> <td>Max</td> <td>Max</td> <td></td> <td>Max</td> <td>Max</td> <td></td> <td>lone</td> <td></td>	Recall Mode	None	None		None	None		Max	Max		Max	Max		lone	
near 1.0 min	Walk Time (s)													8.0	
Add 216 Cone (a) 8.3 8.3 23.4 23.4 Add 200 C Factor (a) 0.18 0.18 0.52 0.52 wic Rain 0.57 0.31 0.49 0.28 Control Delay 2.49 14.7 12.8 0.22 Tool Dolay 2.49 14.7 12.8 0.2 Tool Dolay 2.49 14.7 12.8 9.2 Approach Dolay 2.49 14.7 12.8 9.2 Approach Dolay 2.49 14.7 12.8 9.2 Min Sine Coren (c) 8.0 8.0 8.0 200 200 200 200 18.0 Min Sine Coren (c) 8.0 8.0 8.0 200	Pedestrian Calls (#/hr)													6	
Arallane 0, Fall 0, 18 0, 18 0, 12 0, 12 Order Deby 0, 0 0, 0 0, 0 0, 0 0, 0 Order Deby 0, 0 0, 0 0, 0 0, 0 0, 0 Object Deby 2, 49 14, 7 12, 8 9, 2 0 Object Deby 2, 49 14, 7 12, 8 9, 2 0	Act Effct Green (s)		8.3			8.3			23.4			23.4			
Cardial Delay 24.9 14.7 12.8 9.2 Total Delay 24.9 14.7 12.8 9.2 Cols 8 8 A A Approach LOS 0 0.0 0.0 0.0 Total Delay 24.9 11.7 12.8 9.2 Approach LOS 0.0 20.0 20.0 20.0 0.0 900 Misi Como (b) 60.0 80.80 20.0 20.0 20.0 20.0 900 Misi Como (b) 80.80 80.80 20.0 20.0 20.0 20.0 20.0 20.0 900 Misi Como (b) 80.80 80.80 20.	v/c Ratio		0.18			0.18			0.52			0.52			
Ouce beby 0.0 0.0 0.0 0.0 CDB 0.0 0.0 0.0 0.0 CDB 0 0.0 0.0 0.0 CDB 0 0.0 0.0 0.0 CDB 0 0 0 0 State State Conce (s) 8.0 8.0 2.00 2.00 2.00 0.0 State State Conce (s) 8.0 8.0 8.0 2.00 2.00 2.00 0.0 State State Conce (s) 8.0 8.0 8.0 2.00 2.00 2.00 0.0 State State Conce (s) 8.0 8.0 8.0 2.00 2.00 2.00 0.0 State State Conce (s) 8.0 8.0 8.0 2.00 2.00 2.00 0.0 State State Conce (s) 8.0 8.0 3.0 3.0 3.0 0.0 State State Conce (s) 8.0 8.0 3.0 3.0 3.0 0.0 State State Conce (s)	Control Delay		24.9			14.7			12.8			9.2			
Los B Les A Approach Delay 24 9 14 7 17.8 92 Approach Delay 80 80 80 20 92 Marce Term Code Max Max MaxR MaxR MaxR MaxR Ped 107 Msl-Green (6) 80 80 80 200 200 200 0.0 107 Msl-Green (6) 80 80 80 200 200 200 0.0 506 Msl-Green (6) 80 80 80 200 200 200 0.0 506 Msl-Green (6) 80 80 80 200 200 200 0.0 506 Msl-Green (6) 80 80 80 200 200 200 0.0 506 Msl-Green (6) 80 80 80 35.0 35.0 35.0 0.0 506 Msl-Green (6) 80 80 80 50 35.0 0.0 0 506 Msl-Green (6) 80 80 80 80 80 80 80 80 80	Queue Delay Total Delay		0.0			0.0			0.0			0.0			
Approach LOS C B A 900 Mel Ceren (s) 8.0 8.0 8.0 8.0 8.0 8.0 9.0 900 Mel Ceren (s) 8.0 8.0 8.0 8.0 20.0 20.0 20.0 18.0 900 Mel Ceren (s) 8.0 8.0 8.0 20.0 20.0 20.0 0.0 700 Mel Ceren (s) 8.0 8.0 8.0 20.0 20.0 20.0 0.0 700 Mel Ceren (s) 8.0 8.0 8.0 20.0 20.0 20.0 0.0 900 Mel Ceren (s) 8.0 8.0 8.0 20.0 20.0 20.0 0.0 900 Mel Ceren (s) 8.0 8.0 0.0 20.0 20.0 20.0 0.0 300 Mel Ceren (s) 8.0 8.0 0.0 25.0 35.0 35.0 0.0 300 Mel Ceren (s) 8.0 8.0 8.0 8.0 8.0 8.0 20.0 20.0 20.0 300 Mel Ceren (s) 8.0 8.0 8.0 8.0 35.0 35.0 35.0	LOS		C			В			12.0 B			A			
Application LOS (Approach Delay		24.9			14.7			12.8			9.2			
90h Ma Green Code Max	90th %ile Green (s)	8.0	8.0		8.0	в 8.0		20.0	в 20.0		20.0	A 20.0		18.0	
Offm Alle Terren (S) 8.0 8.0 8.0 2.00 2.00 2.00 0.0 Stim Alle Terren (S) 8.0 8.0 8.0 8.0 2.00 2.00 2.00 0.0 Stim Alle Terren (S) 8.0 8.0 8.0 8.0 2.00 2.00 2.00 0.0 Stim Alle Terren (S) 8.0 8.0 8.0 8.0 2.00 2.00 2.00 0.0 Stim Alle Terren (S) 8.0 8.0 8.0 8.0 2.00 2.00 2.00 0.0 Stim Alle Terren (S) 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 Stim Alle Terren (S) 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 Stim Alle Terren (S) 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 Stim Alle Terren (S) 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0	90th %ile Term Code	Max	Max		Max	Max		MaxR	MaxR		MaxR	MaxR		Ped	
Soft Sei Green (s) 8.0 8.0 8.0 8.0 8.0 20.0 20.0 20.0 20.0	70th %ile Green (s) 70th %ile Term Code	8.0 Max	8.0 Max		8.0 Max	8.0 Max		20.0 MaxR	20.0 MaxR		20.0 MaxR	20.0 MaxR		0.0 Skip	
S0n % a Cree (s) 8.0 80 80 80 20 20 20 20 00 00 30n % a Cree (s) 8.0 80 80 80 20 20 20 20 00 00 30n % a Cree (s) 8.0 80 80 80 35 35.0 35.0 0.0 10n % a Cree (s) 8.0 80 80 80 35 35.0 35.0 0.0 10n % a Cree (s) 8.0 80 80 80 80 35 35.0 35.0 0.0 10n % a Cree (s) 8.0 80 80 80 80 35 35 35 25 0 coue Length S0n (n) 74 1 61 77 7 3 a Cree (s) 8.0 60 6 535 62 3 a Cree (s) 8.0 0 0 60 7 3 a Cree (s) 8.0 0 0 60 7 3 a Cree (s) 8.0 0 0 0 0 0 3 a Cree (s) 8.0 0	50th %ile Green (s)	8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		0.0	
3th Sile Term Code Max Max <td>50th %ile Term Code 30th %ile Green (s)</td> <td>Max 8.0</td> <td>Max 8.0</td> <td></td> <td>Max 8.0</td> <td>Max 8.0</td> <td></td> <td>MaxR 20.0</td> <td>MaxR 20.0</td> <td></td> <td>MaxR 20.0</td> <td>MaxR 20.0</td> <td></td> <td>Skip 0.0</td> <td></td>	50th %ile Term Code 30th %ile Green (s)	Max 8.0	Max 8.0		Max 8.0	Max 8.0		MaxR 20.0	MaxR 20.0		MaxR 20.0	MaxR 20.0		Skip 0.0	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	30th %ile Term Code	Max	Max		Max	Max		MaxR	MaxR		MaxR	MaxR		Skip	
tom ner tenn Cube in max	10th %ile Green (s)	8.0 Max	8.0 Max		8.0 Max	8.0 Max		35.0 Dwoll	35.0 Dwoll		35.0 Dwoll	35.0 Dwoll		0.0 Skin	
Outene Lengin 95th (ft) #141 61 #267 126 Itemeral Link 101 630 666 535 628 Turn Bay Length (ft)	Queue Length 50th (ft)	IVIDA	26		IVIDA	11		DWCII	48		Dweii	24		μ	
Initerial Link Usi, (1) 630 600 533 629 Turn Bay Length, (1) 10 0 0 0 Base Capacity, (vph) 313 343 897 933 Sharation Cap, Reductin 0 0 0 0 Splitback Cap, Reductin 0 0 0 0 Storage Cap, Reductin 0 0 0 0 Intersection Summary 0 0 0 0 Area Type: Other 0 0 0 Cycle Length: 60 60 60 60 60 Control Type: Actuated Uncoordinated Intersection LOS: B 1 Maximum V: Ratio: 0.57 Intersection LOS: B 1 Intersection Capacity Utilization 62.6% ICU Level of Service B 1 Analysis Period (min) 15 1 1 90h Sile Actuated Cycle: 60 7 1 1 70h Sile Actuated Cycle: 38 3 3 3 1 30h Sile Actuated Cycle: 38 3 1 1 30h Sile Actuated Cycle: 38 3 1 1 30h Sile Actuated Cycle: 38 3 3 1 1 30h Sile Actuated Cycle: 38 3 1 1	Queue Length 95th (ft)		#141			61			#267			126			
Base Capacity (vph) 313 343 997 933 Starvation Cap Reductn 0 0 0 0 Storage Cap Reductn 0 0 0 0 Storage Cap Reductn 0 0 0 0 Storage Cap Reductn 0 0 0 0 Reduced V (Ralo 0.57 0.31 0.49 0.28 Intersection Summary Tarea Type: Other Cycle Length: 45.4 Natural Cycle: 60 Control Type: Actuated Uncoordinated Maximum VC Ratio: 0.57 Intersection Capacity Litization 62.6% ICU Level of Service B Analysis Period (mh) 15 90th Sile Actuated Cycle: 38 30th Sile Actuated Cycle: 38 30th Sile Actuated Cycle: 38 30th Sile Actuated Cycle: 38 Splits and Phases: 4: Dorchester Ave/Dorchester Si & Richmond SI Splits and Phases: 4: Dorchester Ave/Dorchester Si & Richmond SI Splits and Phases: 4: Dorchester Ave/Dorchester Si & Richmond SI Splits and Phases: 4: Dorchester Si & Richmond SI Splits and Phases: 4: Dorchester Ave/Dorchester Si & Richmond SI Splits and Phases: 4: Dorchester Ave/Dorchester Si & Richmond SI Splits and Phases: 4: Dorchester Si & Richmond SI	Turn Bay Length (ft)		030			000			030			028			
Slavation Cap Keducin 0 0 0 0 0 Slorage Cap Reducin 0 0 0 0 Reduced vic Ratio 0.57 0.31 0.49 0.28 Intersection Summary Area Type: Other Cycle Length: 60 Actuated Cycle: 60 Control Type: Actualed Uncoordinated Maximum vic Ratio: 0.57 Intersection LOS: B Intersection LOS: B Intersection LOS: B Intersection Signal Delay: 14.2 Intersection LOS: B Intersection Capacity Ullization 64.6% ICU Level of Service B Analysis Period (min) 15 90h Side Actuated Cycle: 33 30th Side Actuated Cycle: 33 30th Side Actuated Cycle: 38 30th Side Actuated Cycle: 38 50th Side Actuated Cy	Base Capacity (vph)		313			343			897			933			
Storage Cap Reductin 0 0 0 0 Reduced v/c Ratio 0.57 0.31 0.49 0.28 Intersection Summary Cap Type Other Cap Type Other Cycle Length: 60	Starvation Cap Reductn Spillback Cap Reductn		0			0			0			0			
Reduced v/c Ratio 0.57 0.31 0.49 0.28 Intersection Summary Area Type: Other Cycle Length: 60 Actuated Cycle Length: 45.4 Natural Cycle: 60 Control Type: Actuated-Uncoordinated Intersection LOS: 8 Intersection Capacity Utilization 62.6% Intersection Capacity Utilization 62.6% ICU Level of Service B Intersection Capacity Utilization 62.6% Oth %ile Actuated Cycle: 38 ICU Level of Service B Intersection Capacity Utilization 62.6% Oth %ile Actuated Cycle: 38 ICU Level of Service B Intersection Capacity Utilization 62.6% Oth %ile Actuated Cycle: 38 ICU Level of Service B Intersection Capacity Utilization 62.6% Oth %ile Actuated Cycle: 38 ICU Level of Service B Intersection Capacity Utilization 62.6% Oth %ile Actuated Cycle: 38 ICU Level of Service B ICU Level of Service B Intersection Capacity Utilization 62.6% ICU Level of Service B ICU Level of Service B Intersection Capacity Utilization 62.6% ICU Level of Service B ICU Level of Service B Intersection Capacity Utilization 62.6% ICU Level of Service B ICU Level of Service B Intersection Capacity Utilization 62.6% ICU Level of Service B ICU Level of Service B Intersection Capacity Utilization 62.6% ICU Level of Service B ICU Level Of Service B	Storage Cap Reductn		0			0			0			0			
Intersection Summary Area Type: Other Cycle Length: 60 Actuated Cycle: 60 Control Type: Actuated-Incoordinated Maximum vic Ratio: 0.57 Intersection Signal Delay: 14.2 Intersection Cos: B Intersection Cost Solth & Actuated Cycle: 38 30th % le Actuated Cycle: 38 Solth Actuated Cycle: 38 Solth Actuated Cycle: 38 Solt	Reduced v/c Ratio		0.57			0.31			0.49			0.28			
Area Type: Unter Cycle Length: 60 Actuated Cycle Length: 45.4 Natural Cycle: 60 Control Type: Actuated-Unccordinated Maximum vic Ratio: 0.57 Intersection Capacity Utilization 62.6% ICU Level of Service B Analysis Period (min) 15 90th %ile Actuated Cycle: 60 70th %ile Actuated Cycle: 38 30th %ile	Intersection Summary	41													
Actuated Cycle Length: 45.4 Natural Cycle: 60 Control Type: Actuated Unccordinated Maximum v/c Ratio: 0.57 Intersection Capacity Utilization 62.6% ICU Level of Service B Analysis Period (min) 15 90th %ile Actuated Cycle: 60 70th %ile Actuated Cycle: 38 30th %ile Actuated Cycle	Cycle Length: 60	Iner													
Natural Cycle: 60 Control Type: Actuated Uncoordinated Maximum vC Ratio: 0.57 Intersection Signal Delay: 14.2 Intersection LOS: B Intersection Capacity Utilization 62.6% ICU Level of Service B Analysis Period (min) 15 90th %ile Actuated Cycle: 60 70th %ile Actuated Cycle: 38 30th %ile Actuated Cyc	Actuated Cycle Length: 45.4														
Maximum vic Ratio 0.57 Intersection Signal Delay: 14.2 Intersection LOS: B Intersection Capacity Utilization 62.6% ICU Level of Service B Analysis Period (min) 15 Oth %ile Actuated Cycle: 60 70th %ile Actuated Cycle: 38 30th %ile Actuated Cycle: 38	Natural Cycle: 60 Control Type: Actuated-Uncoord	dinated													
Intersection Signal Delay: 14.2 Intersection LOS: B Intersection Capacity Utilization 62.6% ICU Level of Service B Analysis Period (min) 15 90th %ile Actuated Cycle: 60 70th %ile Actuated Cycle: 38 30th %ile Act	Maximum v/c Ratio: 0.57	amatou													
Analysis Period (min) 15 90th %ile Actuated Cycle: 38 30th %ile Actuated Cycle: 38 30th %ile Actuated Cycle: 38 30th %ile Actuated Cycle: 38 10th %ile Actuated Cycle: 38 10th %ile Actuated Cycle: 38 30th %ile	Intersection Signal Delay: 14.2	62.6%			In	ersection I	LOS: B Sorvico F								
901h %ile Actuated Cycle: 30 501h %ile Actuated Cycle: 38 501h %ile Actuated Cycle: 38 101h %ile Actuated Cycle: 38 101h %ile Actuated Cycle: 38 201h %ile Actuated Cycle: 38 101h %ile Actuated Cycle: 38 101h %ile Actuated Cycle: 38 201h %ile Actuated Cycle: 38 101h %ile Actuated Cycle: 38 101h %ile Actuated Cycle: 38 95 h percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. Splits and Phases: 4: Dorchester Ave/Dorchester St & Richmond St Image: Part Actuated Cycle: 22 s 12 s	Analysis Period (min) 15	02.070			10	U LEVEI UI	JCI VICE L								
7/01 %ile Actuated Cycle: 38 50th %ile Actuated Cycle: 38 10th %ile Actuated Cycle: 38 10th %ile Actuated Cycle: 38 10th %ile Actuated Cycle: 38 0ueue shown is maximum after two cycles. Splits and Phases: 4: Dorchester Ave/Dorchester St & Richmond St Image: Part of the state of	90th %ile Actuated Cycle: 60														
301h %ile Actuated Cycle: 38 101h %ile Actuated Cycle: 53 # 95h percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. Splits and Phases: 4: Dorchester Ave/Dorchester St & Richmond St \$	50th %ile Actuated Cycle: 38														
tuin %ile Actualed Cycle: 53 # 95h percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. Splits and Phases: 4: Dorchester Ave/Dorchester St & Richmond St # 01 # 02 25	30th %ile Actuated Cycle: 38														
Queue shown is maximum after two cycles. Splits and Phases: 4: Dorchester Ave/Dorchester St & Richmond St Image: the system of the system o	# 95th percentile volume exce	eds canac	tity, aueue	may be lo	nger.										
Splits and Phases: 4: Dorchester St & Richmond St 101 25 25 25 25 25 25 25 25 25 25 25 25 25	Queue shown is maximum a	fter two cy	cles.	2,2010	3										
Important in a construction of a transmission of a transmissi	Solits and Phases 4. Dorche	ster Ave/N	Inrchester 9	St & Richr	nond St										
Are/02 Tr/05 225 s 225 s 13 s									1					<u> </u>	
	يور ۽ 25 s							2	≕ø∠ !s					-⊤+05 13 s	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2			
Lane Configurations		د أ	1		4		۲	¢î		۴.	¢î					
Traffic Volume (vph)	28	109	191	48	117	21	155	204	48	31	183	65				
Ideal Flow (vphpl)	28 1900	1900	191	48	1900	1900	1900	1900	48	1900	183	00 1900				
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00				
Frt Elt Protoctod		0.000	0.850		0.985		0.050	0.971		0.050	0.961					
Satd. Flow (prot)	0	1881	1615	0	1847	0	1805	1815	0	1752	1813	0				
Flt Permitted		0.990			0.987		0.401			0.432						
Satd. Flow (perm)	0	1881	1615 Voc	0	1847	0	762	1815	0	797	1813	0				
Satd. Flow (RTOR)			236		4	res		11	res		14	Tes				
Link Speed (mph)		30			30			30			30					
Link Distance (ft)		615			710			537			620					
Peak Hour Factor	0.95	0.95	0.95	0.86	0.86	0.86	0.94	0.94	0.94	0.92	0.92	0.92				
Heavy Vehicles (%)	0%	0%	0%	0%	0%	0%	0%	2%	0%	3%	1%	0%				
Adj. Flow (vph) Sharod Lano Traffic (%)	29	115	201	56	136	24	165	217	51	34	199	71				
Lane Group Flow (vph)	0	144	201	0	216	0	165	268	0	34	270	0				
Turn Type	Split	NA	Perm	Split	NA		D.P+P	NA		Perm	NA					
Protected Phases	3	3	2	4	4		5	15		1	1		2			
Detector Phase	3	3	3	4	4		5	15		1	1					
Switch Phase																
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0		5.0			10.0	10.0		1.0			
Total Split (s)	23.0	23.0	23.0	10.5	10.5		14.0			36.0	36.0		27.0			
Total Split (%)	19.2%	19.2%	19.2%	15.8%	15.8%		12.5%			30.0%	30.0%		23%			
Maximum Green (s)	16.5	16.5	16.5	12.5	12.5		6.0			26.5	26.5		23.0			
Yellow Time (s) All-Red Time (s)	4.0	4.0	4.0	3.5	3.5		3.0			3.5	3.5		2.0			
Lost Time Adjust (s)	2.5	0.0	0.0	5.0	0.0		0.0			0.0	0.0		2.0			
Total Lost Time (s)		6.5	6.5		6.5		9.0			9.5	9.5					
Lead/Lag	Lead	Lead	Lead	Lag	Lag					Lead	Lead		Lag			
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0		2.0			4.0	4.0		3.0			
Recall Mode	Max	Max	Max	Max	Max		Max			C-Max	C-Max		None			
Walk Time (s)													7.0			_
Pedestrian Calls (#/hr)													9			
Act Effct Green (s)		38.1	38.1		12.5		33.0	41.5		26.5	26.5					
Actuated g/C Ratio		0.32	0.32		0.10		0.28	0.35		0.22	0.22					
Control Delay		35.0	4.3		144.6		46.1	34.7		41.5	49.0					
Queue Delay		0.0	0.0		0.0		0.0	0.0		0.0	0.0					
Total Delay		35.0	4.3		144.6 F		46.1 D	34.7		41.5 D	49.0 D					
Approach Delay		17.1	A		144.6		D	39.0		U	48.1					
Approach LOS		В			F			D			D					
90th %ile Green (s) 90th %ile Term Code	16.5 MaxP	16.5 MayP	16.5 MayP	12.5 MaxP	12.5 MaxP		6.0 MayP			26.5 Coord	26.5 Coord		23.0 Pod			
70th %ile Green (s)	43.5	43.5	43.5	12.5	12.5		6.0			26.5	26.5		0.0			
70th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip			
50th %ile Green (s) 50th %ile Term Code	43.5 MaxP	43.5 MaxP	43.5 MayP	12.5 MaxP	12.5 MaxP		6.0 MayP			26.5 Coord	26.5 Coord		0.0 Skin			
30th %ile Green (s)	43.5	43.5	43.5	12.5	12.5		6.0			26.5	26.5		0.0			
30th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip			
10th %ile Green (s) 10th %ile Torm Code	43.5 MaxP	43.5 MaxP	43.5 MaxP	12.5 Max P	12.5 MaxP		6.0 MaxP			26.5	26.5		0.0 Skip			
Queue Length 50th (ft)	IVIDAIX	76	0	WIGAT	~188		97	175		22	182		Эмр			
Queue Length 95th (ft)		175	42		#324		151	244		53	277					
Internal Link Dist (ft)		535			630			457			540					
Base Capacity (vph)		596	673		195		261	634		176	411					
Starvation Cap Reductn		0	0		0		0	0		0	0					
Spillback Cap Reductn		0	0		0		0	0		0	0					
Reduced v/c Ratio		0.24	0.30		1.11		0.63	0.42		0.19	0.66					
Intersection Summary																
Area Type:	Other															
Cycle Length: 120																
Actuated Cycle Length: 120 Offset: 11 (0%) Referenced t	o nhaso 1·N	RSR Start	of Green													
Natural Cycle: 95		555, Start	or oreen													
Control Type: Actuated-Coord	linated															
Maximum v/c Ratio: 1.11	0			In	torsoction											
Intersection Capacity Utilization	7 on 60.0%			IC	U Level of	Service I	3									
Analysis Period (min) 15																
 Volume exceeds capacity Output a shown is maximum 	, queue is th	eoretically	infinite.													
# 95th percentile volume ex	ceeds capac	cies. ity, queue	may be lo	onger.												
Queue shown is maximum	after two cy	cles.	.,	5												
Solits and Phases 1. Mark	nington St º	Morton St	/Pichmon	1 St												
	ແມ່ນເບເປັວເ &	WULUII 31	NUTITIUT	JL	11									+	▲ †	
▼ ¶Ø1 (R)					π 1 Ø2					-	Ø3			♥ Ø4	N Ø5	

Line Gargener Line		٠	\rightarrow	1	T.	Ŧ	¥	-	•	•	4		
Line Configuration N	Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	SBR2	NEL2	NEL	NER	Ø2	
μπ. καταγορία 0.0 0.0 0.0 0.0 0.0 None inform 1 0.0 100	Lane Configurations	1	2000	7	†	†	0	107	<u></u>	0	7		
	Future Volume (vph)	164 164	238	270	228	200	0	197	0	0	0		
Store Let M T <tht< th=""> T T <th< td=""><td>Ideal Flow (vphpl)</td><td>1900</td><td>1900</td><td>1900</td><td>1900</td><td>1900</td><td>1900</td><td>1900</td><td>1900</td><td>1900</td><td>1900</td><td></td><td></td></th<></tht<>	Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900		
	Storage Length (ft)	75	0	100			75			0	0		
Disk Disk Disk Disk Disk Disk Disk Set Person Per	Storage Lanes Taper Length (ft)	100	1	100			I			25	I		
m Deal period Line at Respect of the line is the li	Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		
	Frt		0.850					0.850					
The section 1 The section 2 The s	Fit Protected Satd_Elow (prot)	0.950	1615	0.950	1900	1900	0	1615	1863	0	1863		
Sat P Le gener) 105 185 187 107 100 100 10 10 105 183 0 103 144 Seet Bener 10 145 Seet	Flt Permitted	0.950	1015	0.950	1700	1700	0	1015	1005	0	1005		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Satd. Flow (perm)	1805	1615	1787	1900	1900	0	1615	1863	0	1863		
Lin Speech of A 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Satd Flow (RTOR)							Yes 173			Yes		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Link Speed (mph)	30			30	30		175		30			
Inters Inter	Link Distance (ft)	464			447	537				214			
Heary Vector Dis. Dis. <thdis.< th=""> Dis. Dis.</thdis.<>	Peak Hour Factor	0.97	0.97	0.94	0.94	0.88	0.88	0.88	0.92	4.9	0.92		
Al, Pine (pro) Mo 245 237 243 227 0 244 0 0 0 Tan Type Piot Piot </td <td>Heavy Vehicles (%)</td> <td>0%</td> <td>0%</td> <td>1%</td> <td>0%</td> <td>0%</td> <td>1%</td> <td>0%</td> <td>2%</td> <td>2%</td> <td>2%</td> <td></td> <td></td>	Heavy Vehicles (%)	0%	0%	1%	0%	0%	1%	0%	2%	2%	2%		
Non-Department York Point	Adj. Flow (vph)	169	245	287	243	227	0	224	0	0	0		
Turn Spor Prior Prior Prior Prior Turn Spor 1 1 5 5 4 2 Printing Prior 1 1 5 5 4 2 Printing Prior 100 100 100 100 100 100 Minum Smith 100 100 100 100 100 100 Minum Smith 100 100 100 100 100 100 Minum Smith 100 100 100 100 100 100 100 Minum Smith 000 205 275 175	Lane Group Flow (vph)	169	245	287	243	227	0	224	0	0	0		
Particular Maxes 3 13 1 15 5 4 4 2 Satek Parka 1 1 15 5 5 4 4 Satek Parka 100 100 100 40 4.0 10 4.0 10 Mattern Sigk (2) 100 100 4.0 14.0 100 200 100 200 Mattern Sigk (2) 100 100 4.0 4.0 100 200	Turn Type	Prot	pt+ov	Prot	NA	NA		Prot	Prot	-	Prot		
Direction 3 1 1 5 5 4 4 Minuma Sulta (V) 100 10	Protected Phases	3	13	1	15	5		5	4		4	2	
Sakab Prova Minumu Mini () Minumu Minumu Mini () Minumu Mini () Minumu Minumu Mini () Mi	Detector Phase	3	13	1	15	5		5	4		4		
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	Switch Phase	-	-		-	-		-					
	Minimum Initial (s)	10.0		10.0		10.0		10.0	4.0		4.0	1.0	
Tada Sgim 20, 20, 20, 20, 20, 20, 20, 20, 20, 20,	Total Split (s)	27.0		33.0		24.0		24.0	10.0		10.0	26.0	
$ Volume The Control (s) 285 275 175 175 175 40 40 220 \\ Volume The Control (s) 40 3 3 3 3 40 40 320 Volume The Control (s) 40 40 175 175 175 40 40 220 \\ Volume The Control (s) 40 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0$	Total Split (%)	22.5%		27.5%		20.0%		20.0%	8.3%		8.3%	22%	
Ailest Time (b) 25 25 25 25 25 20 Total cast Time (b) 65 55 65 60 00 Late Lag (printer) Yos Yos Yos Yos Yos Kast More None None None None None Wak Time (c) 15.4 72.6 82.2 22.8 70.7 Festorit Mol (s)	Maximum Green (s)	20.5		27.5		17.5		17.5	4.0		4.0	22.0	
Lind The Adjust (s) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	All-Red Time (s)	2.5		2.5		2.5		2.5	2.5		2.5	2.0	
Link Link Image Log Log Log Link Link Yes Yes Yes Yes Velok Link Link Yes Yes Yes Yes Velok Link None None None None None Velok Link 0.13 0.05 0.43 0.50 0.00	Lost Time Adjust (s)	0.0		0.0		0.0		0.0	0.0		0.0		
Lad-La griphine? Vis	Lead/Lag	Lead		Lead		0.0		0.5	Lag		Lag	Lag	
Vehick Enderson (s) 2.0 2.0 4.0 4.0 2.0 2.0 3.0 Vehick Enderson (s) None None None None None None Veik Enderson (s) 15.4 72.6 72.0 14 Act End Caren (s) 15.4 72.6 14 Act End Caren (s) 15.4 72.6 14 Act End Caren (s) 0.0 0.46 0.19 0.03 0.50 Control Delay 0.78 0.00 0.45 0.0 0.0 0.0 Vic Ratio 0.73 0.25 0.35 0.5 0.0 0.0 Control Delay 0.8 0.4 0.0 0.0 0.0 0.0 Object Halt 8 A 0 C 0.0 2.0 Symbal End Caren (s) 3.6 2.75 2.75 0.0 0.0 2.0 Symbal End Caren (s) 1.6 0.30 2.0 0.0 0.0 2.0 Symbal End Caren (s) 1.6 0.20 2.29 2.39 0.0 0.0 2.0 Symbal End Caren (s) 1.6 0.20 2.29 2.39 0.0 0.0 0.0 Symbal End Caren (s) 1.3	Lead-Lag Optimize?	Yes		Yes					Yes		Yes	Yes	
Name Time (a) Nome	Vehicle Extension (s) Recall Mode	2.0 None		2.0 C-Max		4.0 None		4.0 None	2.0 None		2.0 None	3.0 None	
Flach Dur Wak (s) 15.0 Art Elfet Green (s) 15.4 72.4 52.9 62.2 22.8 22.8 22.8 Art Elfet Green (s) 0.13 6.40 0.43 0.13 0.40 0.41 0.13 0.40 0.41 0.13 0.40 0.41 0.13 0.40 0.41 0.14	Walk Time (s)	10110		o max		110110		Hono	110110		110/10	7.0	
Def Elit Goen (s) 15.4 7.6 5.2 2.2 2.2 2.2 2.2 3.6 Availed of Chain 0.13 0.26 0.46 0.68 0.19 0.01 <	Flash Dont Walk (s)											15.0	
Actualed gC Rafio 0 13 0 6.0 0 73 0 72 0 19 0 19 0 19 0 19 0 19 0 19 0 19 0 19	Act Effct Green (s)	15.4	72.6	52.9	82.2	22.8		22.8				14	
Vic Rain 0.73 0.25 0.35 0.30 Cancer Delay 0.8 100 104 24.5 23.4 21.3 Cancer Delay 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Cancer Delay 67.8 B B A 0.0 0.0 0.0 0.0 Other Delay 67.8 B B A 0.0 0.0 0.0 0.0 0.0 0.0 State Tar Code Max Code Max Max State Tar Code Max State Tar Code Max None State Tar Code Max Max State Tar Code Max Max State Tar Code Max	Actuated g/C Ratio	0.13	0.60	0.44	0.68	0.19		0.19					
One use bey/s 0.0 0.0 0.0 0.0 Clab Deby/s 67.8 10.0 20.0 20.0 20.0 Clab Deby/s 0.0 2.0 2.0 2.0 2.0 2.0 Approach Deby/s 33.8 1.25 37.4 2.0 2.0 2.0 Minit Geren Code Max Corr Max Max Skip Skip Skip Minit Geren Code Max Corr Gap Gap Gap Gap Gap Skip Skip <th< td=""><td>Control Delav</td><td>0.73</td><td>0.25</td><td>0.36</td><td>3.6</td><td>0.63 53.4</td><td></td><td>21.3</td><td></td><td></td><td></td><td></td><td></td></th<>	Control Delav	0.73	0.25	0.36	3.6	0.63 53.4		21.3					
Total Delay 6/78 100 200 3.6 53.4 21.3 Approach Delay 33.6 12.5 37.4 Approach Delay 33.6 12.5 37.4 Approach Delay 33.6 12.5 37.4 Approach Delay 20.5 27.5 27.5 0.0 0.0 22.0 90h 3kie Green (s) 20.5 27.5 27.5 0.0 0.0 22.0 90h 3kie Green (s) 20.5 27.0 2.70 0.0 0.0 22.0 90h 3kie Green (s) 18.0 30.5 27.0 2.70 0.0 0.0 22.0 90h 3kie Green (s) 18.0 30.5 27.0 2.70 0.0 0.0 22.0 90h 3kie Green (s) 18.0 30.5 27.0 2.73 0.0 0.0 0.0 90h 3kie Green (s) 18.0 30.5 27.0 2.73 0.0 0.0 0.0 90h 3kie Green (s) 18.0 8.0 2.0 2.0 90h 3kie Green (s) 18.0 7.0 2.0 5.0 0.0 0.0 0.0 90h 3kie Green (s) 18.0 7.0 7.0 7.0 7.0 0.0 0.0 90h 3kie Green (s) 10.0 7.6 14.0 14.0 0.0 0.0 0.0 10h 3kie Green (s) 10.0 7.6 14.0 14.0 0.0 0.0 0.0 10h 3kie Green (s) 10.0 7.6 14.0 17.0 0.0 0.0 90h 3kie Green (s) 10.0 7.6 14.0 17.0 0.0 0.0 10h 3kie Green (s) 10.0 7.6 14.0 17.0 0.0 0.0 10h 3kie Green (s) 10.0 7.6 14.0 17.0 0.0 0.0 90h 3kie Green (s) 10.0 7.6 14.0 15.0 10.0 7.5 10h 3kie Green (s) 0.0 0 0 0 0 0 80d acea dengh 50h (h) 12.2 60 0.0 0.0 10h 3kie Green (s) 0.0 0 0 0 0 80d acea dengh 50h (h) 13.0 10.0 7.5 134 135 134 135 134 136 134 137 134 136 134 137 134 136 134 137 134 136 134 137 134 136 136 136 136 136 136 136 136	Queue Delay	0.0	0.0	0.6	0.0	0.0		0.0					
Approach Delay 33 6 0 125 37.4 Approach Delay 33 6 0 125 37.4 Shift Sterem (c) 20.5 27.5 27.5 0.0 0.0 22.0 Shift Sterem (c) 18.0 30.5 27.0 27.0 0.0 0.0 22.0 Shift Sterem (c) 18.0 30.5 27.0 27.0 0.0 0.0 22.0 Shift Sterem (c) 18.0 30.5 27.0 27.0 0.0 0.0 22.0 Shift Sterem (c) 18.0 30.5 27.0 23.9 0.0 0.0 0.0 Shift Sterem (c) 15.6 62.0 23.9 23.9 0.0 0.0 0.0 0.0 Shift Sterem (c) 10.6 7.6 62.9 Skip Skip Skip Skip Shift Sterem (c) 10.0 7.6 7.5	Total Delay	67.8 F	10.0 B	20.0 B	3.6 A	53.4 D		21.3 C					
Approach LOS C 2 75 275 275 275 275 00 00 220 90h %ile Green Code Max Coord Max Max Skip Skip Ped 10h %ile Green Code Gap Coord Gap Skip Skip Ped 50h %ile Green Code Gap Coord Gap Skip Skip Ped 50h %ile Green Code Gap Coord Gap Skip Skip Ped 50h %ile Green Code Gap Coord Gap Skip Skip Skip 50h %ile Green Code Gap Coord Gap Skip Skip Skip 50h %ile Green Code Gap Coord Gap Skip Skip Skip 50h %ile Green Code Gap Coord Gap Skip Skip Skip 50h %ile Green Code Gap Coord Gap Gap Skip Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Coord Gap Gap Skip Skip 10h %ile Green Code Min Cod	Approach Delay	33.6	5	5	12.5	37.4		Ű					
9001 Nate Term 27.3 27.3 27.3 27.3 0.0 0.0 22.0 9001 Nate Term 000 0.0	Approach LOS	C 20 5		27 F	В	D		27 F	0.0		0.0	22.0	
20h Skie Green (s) 18.0 30.5 27.0 27.0 0.0 0.0 22.0 20h Skie Green (s) 15.6 62.0 23.9 23.9 0.0 0.0 0.0 50h Skie Green (s) 15.6 62.0 23.9 23.9 0.0 0.0 0.0 50h Skie Green (s) 13.1 67.9 20.5 20.5 0.0 0.0 0.0 30h Skie Green (s) 10.0 7.6 14.9 14.9 0.0 0.0 0.0 10h Skie Green (s) 10.0 7.6 14.9 14.9 0.0 0.0 0.0 10h Skie Green (s) 10.0 7.6 14.9 17.8 72 12.4	90th %ile Term Code	ZU.5 Max		Coord		Z7.5 Max		Max	Skip		Skip	Ped	
VID Nale Lerm Code Gap Coord Gap Gap Skp Ped 50h Nale Creen (s) 15.6 6.20 23.9 23.9 0.0 0.0 0.0 30h Nale Creen (s) 13.1 67.9 20.5 20.5 0.0 0.0 0.0 30h Nale Creen (s) 13.1 67.9 20.5 20.5 0.0 0.0 0.0 10h Nale Term Code Gap Coord Gap Gap Skp Skip Skip 10h Nale Term Code Min Coord Gap Gap Gap Skip Skip 10h Nale Term Code Min Coord Gap Gap Gap Skip Skip 0ueue Length Stih (t) 127 60 94 1 178 72 0.0	70th %ile Green (s)	18.0		30.5		27.0		27.0	0.0		0.0	22.0	
Soft Nate Team Code Gap Coord Gap Gap Skip Skip 30th Nate Team Code Gap Coord Gap Gap Skip Skip 30th Nate Team Code Gap Coord Gap Gap Gap Skip 30th Nate Team Code Gap Coord Gap Gap Gap Skip 10th Nate Team Code Gap Coord Gap Gap Gap Skip 10th Nate Team Code Gap Coord Gap Gap Gap Skip 00ueue Length Solt (ft) 127 60 94 1 178 72 00ueue Length Solt (ft) 134 367 134 107 1mm Bay Length (ft) 75 100 75 Base Capazity (vph) 308 1045 787 1291 368 452 Starvation Cap Reductin 0 0 0 Storage Cap Reductin 0 0 0 0 0 Storage Cap Reductin 0 0 0 0 0 Offset O (WA), Referenced to phase 1:NBTL, Start of Green Natural Cycle Natural Cycle Natural Cycle 120 Kap Intersection LOS: C	70th %ile Term Code	Gap 15.6		62 0		23 9		Cap 23.9	SKIP		SKIP	Ped 0.0	
30h % lie Green (s) 13.1 67.9 20.5 20.5 0.0 0.0 0.0 30h % lie Green (s) 10.0 76.6 14.9 14.9 0.0 0.0 0.0 10h % lie Green (s) 10.0 76.6 14.9 14.9 0.0 0.0 0.0 10h % lie Green (s) 10.0 76.6 14.9 14.9 0.0 0.0 0.0 10h % lie Green (s) 10.7 60 94 1 178 72	50th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip	
Solf here Herrin Code Cap Cap Cap Cap Skp Skp 10h kile Green (s) 100 76.6 14.9 14.9 0.0 0.0 0.0 10h kile Green (s) 100 76.6 14.9 14.9 0.0 0.0 0.0 10h kile Green (s) 100 76.6 14.9 14.9 0.0 0.0 0.0 Cueue Length Solf (t) 197 60 94.1 178 72 Cueue Length Solf (t) 198 103 28.7 112 m231 m104 Internal Link Dist (t) 384 367 457 134 1 Tum Bay Length (t) 75 100 75 134 1 Starvator Cap Reductin 0 0 0 0 0 SpliBack Cap Reductin 0 0 0 0 0 Strange Cap Reductin 0 0 0 0 0 Strade Cap Reductin 0 0 0 <td>30th %ile Green (s)</td> <td>13.1</td> <td></td> <td>67.9</td> <td></td> <td>20.5</td> <td></td> <td>20.5</td> <td>0.0</td> <td></td> <td>0.0</td> <td>0.0</td> <td></td>	30th %ile Green (s)	13.1		67.9		20.5		20.5	0.0		0.0	0.0	
10th Kell Term Code Min Coord Gap Gap Skip Skip Skip Queue Length S0th (t) 127 60 94 1 178 72 Queue Length S0th (t) 195 103 287 112 m231 m104 Internal Link Dist (t) 344 367 457 134 Tum Bay Length (t) 75 100 75 Base Capacity (vph) 308 1045 787 1291 368 452 Starvation Cap Reducin 0 0 0 0 0 0 0 Storage Cap Reducin 0 0 0 0 0 0 0 Reduced v/c Ratio 0.55 0.23 0.51 0.19 0.62 0.50 Intersection Summary Intersection Capacity Length: 120 Intersection Capacity Length: 120 Intersection Capacity Length: 120 Intersection Capacity Link2aich Green Natural Cycle: E5 Control Type: Actuated-Coordinated Intersection LOS: C Intersection LOS: C Intersection Capacity Link2aich S0.0% ICU Level of Service A Analysis Period (min) 15	10th %ile Green (s)	10.0		76.6		14.9		14.9	0.0		0.0	0.0	
Oucle Length Suft (1) 12/ 60 94 1 178 72 Oucle Length Syft (1) 195 103 287 457 134 Tum Bay Length (1) 75 100 75 388 7457 134 Tum Bay Length (1) 75 100 75 388 7457 75 Base Capacity (vph) 308 1045 787 1291 368 452 Starvation Cap Reductn 0 0 221 0 0 0 0 Spillback Cap Reductn 0 0 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 0 0 Retuced vic Ratio 0.55 0.23 0.51 0.19 0.62 0.50 Intersection Summay Intersection Summay Area Type: Other	10th %ile Term Code	Min	(0	Coord		Gap		Gap	Skip		Skip	Skip	
Internal Link Dist (ii) 384 367 457 134 Turn Bay Length (ii) 75 100 75 Base Capacity (iph) 308 1045 787 1291 368 452 Starvation Cap Reductn 0 0 221 0 0 0 Spillback Cap Reductn 0 0 0 0 0 0 0 Reduced vic Ratio 0.55 0.23 0.51 0.19 0.62 0.50 Intersection Summary Area Type: Other Cycle Length: 120 Actuated Cycle Length: 120 Offset: 0 (%), Referenced to phase 1:NBTL, Start of Green Natural Cycle: 85 Control Type: Actuated-Coordinated Maximum vic Ratio: 0.73 Intersection Signal Delay: 26.8 Intersection LOS: C Intersection Signal Delay: 26.8 Intersection LOS: C Intersection Signal Delay: 26.8 Intersection LOS: C Intersection fignal Delay: 26.8 Intersection LOS: C Intersection Signal Delay: 26.8 Intersection Signal Delay: 26.8 Inter	Queue Length 50th (ft)	127	60 103	287	112	178 m231		/2 m104					
Tum Bay Length (ft) 75 100 75 Base Capacity (vph) 308 1045 787 1291 368 452 Starvation Cap Reducth 0 0 221 0 0 0 Spillback Cap Reducth 0 0 221 0 0 0 Spillback Cap Reducth 0 0 0 0 0 0 Reduced vic Ratio 0.55 0.23 0.51 0.19 0.62 0.50 Intersection Summary	Internal Link Dist (ft)	384			367	457				134			
Dase capacity (vpl) 500 1043 700 1271 500 402 Starvation Cap Reductin 0 0 0 2 0 0 0 0 0 Storage Cap Reductin 0 0 0 0 0 0 0 0 0 Storage Cap Reductin 0 0 0 0 0 0 0 0 0 Intersection Summary Area Type: Other Cycle Length: 120 Actuated Cycle Length: 120 Offset: 0 (0%), Referenced to phase 1:NBTL, Start of Green Natural Cycle: 85 Control Type: Actuated-Coordinated Maximum Vc Ratio: 0.73 Intersection LOS: C Intersection Signal Delay: 26.8 Intersection LOS: C Intersection Signal Delay: 26.8 Intersection LOS: C Intersection Gignal Delay: 26.8 Intersection LOS: C Intersection Signal Delay: 26.8 Intersection LOS: C Intersection Community Intersection LOS: C Intersection Community Intersection	Turn Bay Length (ft) Raco Canacity (yph)	209	10/5	100	1201	260		75					
Spillback Cap Reductn 0 0 0 0 0 Storage Cap Reductn 0 0 0 0 0 Reduced vic Ratio 0.55 0.23 0.51 0.19 0.62 0.50 Intersection Summary	Starvation Cap Reductn	0	0	221	0	0		0					
Storage Cap Reducting 0	Spillback Cap Reductn	0	0	0	0	0		0					
Intersection Summary Area Type: Other Cycle Length: 120 Actuated Cycle Length: 120 Actuated Cycle Length: 120 Offset: 0 (0%), Referenced to phase 1:NBTL, Start of Green Natural Cycle: 85 Control Type: Actuated-Coordinated Maximum vic Ratio: 0.73 Intersection LOS: C Intersection Signal Delay: 26.8 Intersection LOS: C Intersection Capacity Utilization 50.0% ICU Level of Service A Analysis Period (min) 15 m m Volume for 95th percentile queue is metered by upstream signal. Splits and Phases: 2: Driveway & Washington St & River St	Reduced v/c Ratio	0.55	0.23	0.51	0.19	0.62		0.50					
Area Type: Other Cycle Length: 120 Actualed Cycle Length: 120 Offset: 0 (%), Referenced to phase 1:NBTL, Start of Green Natural Cycle: 85 Control Type: Actualed-Coordinated Maximum v/c Ratio: 0.73 Intersection Signal Delay: 26.8 Intersection Signal Delay	Intersection Summary												
Cycle Length: 120 Actuated Cycle Length: 120 Natural Cycle: 85 Control Type: Actuated-Coordinated Maximum v/c Ratio: 0.73 Intersection Signal Delay: 26.8 Intersection LOS: C Intersection Capacity Utilization 50.0% ICU Level of Service A Analysis Period (min) 15 m Volume for 95th percentile queue is metered by upstream signal. Splits and Phases: 2: Driveway & Washington St & River St Splits (R)	Area Type:	Other											
Splits and Phases: 2: Driveway & Washington St & River St	Actuated Cycle Length: 120 Offset: 0 (0%), Referenced It Natural Cycle: 85 Control Type: Actuated-Coor Maximum v/c Ratio: 0.73 Intersection Signal Delay: 26 Intersection Capacity Utilizat	o phase 1:NB [*] rdinated 5.8 rion 50.0%	FL, Start o	of Green	In	tersection CU Level of	LOS: C Service F	l.					
	Solits and Phases: 2. Driv	ile queue is m eway & Wash	etered by	upstream & River St	signal.								
	Ø1 (R)		3.5.1.01		÷.	Ø2				1	03		1 04 1 05

Lane Group EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR Ø2	
Lane Configurations	
Traine Volume (vph) 51 163 228 169 204 16 228 240 164 17 350 74	
Idea Flow (vphpl) 1900 1900 1900 1900 1900 1900 1900 190	
Storage Lengin (1) 0 23 0 30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
Taper Length (ft) 25 25 25 25 Land Life Factor 100 <td></td>	
Frt 0.850 0.989 0.850 0.975	
Flt Protected 0.988 0.950 0.950 0.998	
Filt Permitted 0.636 0.492 0.391 0.931	
Satd. Flow (perm) 0 1199 1615 935 1862 0 736 1900 1615 0 3246 0 Bitelt Tura as Bod Vac	
Satd. Flow (RTOR) 115 3 190 17	
Link Speed (mph) 30 30 30 30 30	
Travel Time (s) 10.2 15.3 10.1 14.0	
Peak Hour Factor 0.96 0.96 0.92 0.92 0.92 0.97 0.97 0.97 0.98 0.98 0.98	
Adj. Flow (vph) 53 170 238 184 222 17 235 247 190 19 357 76	
Shared Lane Traffic (%) Lane Group Flow (wh) 0 223 238 184 239 0 235 247 190 0 452 0	
Turn Type Perm NA pt+ov Perm NA D.P+P NA Prot Perm NA	
Protected Phases 5 56 5 6 16 1 2 Permitted Phases 5 5 1 1 1	
Delector Phase 5 5 5 6 5 5 6 16 16 1 1	
Switch Phase Minimum Initial (s) 10.0 10.0 10.0 10.0 8.0 10.0 10.0 10.0	
Minimum Split (s) 18.0 18.0 18.0 18.0 14.5 17.5 32.0	
Total Split (s) 39.0 39.0 39.0 22.0 27.0 32.0 Total Split (%) 32.5% 32.5% 32.5% 18.3% 22.5% 27.6% 27.6%	
Maximum Green (s) 31.0 31.0 31.0 31.0 15.5 19.5 28.0	
Yellow Time (s) 4.5 4.5 4.5 4.5 3.0 4.0 4.0 2.0 All-Red Time (s) 3.5 3.5 3.5 3.5 3.5 3.5 3.5 2.0	
Lost Time Adjust (s) 0.0 0.0 0.0 0.0 0.0 0.0	
Total Lost Time (s) 8.0 8.0 8.0 6.5 7.5 Lead/Lag Lead Lead Lead Lag Lead Lag	
Lead-Lag Optimize? Yes Yes Yes Yes Yes Yes Yes Yes	
Vehicle Extension (s) 2.0 2.0 2.0 4.0 2.0 2.0 3.0 Recall Mode None None C-Max None None	
Walk Time (s) 7.0	
Flash Dont Walk (s) 21.0 Pedestrian Calls (#/hr) 43	
Act Effct Green (s) 25.9 47.8 25.9 25.9 47.5 53.0 53.0 31.1	
Actuated g/C Ratio 0.22 0.40 0.22 0.22 0.40 0.44 0.44 0.26 v/c Ratio 0.86 0.33 0.92 0.59 0.55 0.29 0.23 0.53	
Control Delay 76.8 11.4 89.9 47.1 31.4 27.0 4.6 44.3	
Total Delay 76.8 11.4 89.9 47.1 31.4 27.0 4.6 44.3	
LOS E B F D C C A D	
Approach Delay 43.1 63.7 22.2 44.5 Approach LOS D E C D	
90th %ile Green (s) 31.0 31.0 31.0 31.0 15.5 19.5 28.0	
Your water rein code Max Max Max Max Max Cool of	
Yolk %ile Term Code Max Max Max Max Coord Ped 50th %ile Grage (c) 28.5 28.5 28.5 18.0 19.5 19.5 28.0	
South Allic Credit (s) 20.5 20.5 20.5 10.6 11.5 17.5 20.6 South Allic Term Code Gap Gap Gap Max Coord Ped	
30th %ile Green (s) 23.2 23.2 23.2 23.2 18.1 24.7 24.7 28.0 30th %ile Term Code Gan	
10th %ile Green (s) 15.7 15.7 15.7 15.7 10.1 72.2 72.2 0.0	
10th %ile Term Code Gap Gap Gap Coord Skip Dueue Length 50th (ft) 98 4 136 161 130 138 0 174	
Queue Length 95th (ft) #275 96 #249 238 206 216 50 #256	
Internal Link Dist (ft) 367 593 363 535 Turn Bay Length (ft) 25	
Base Capacity (vph) 309 712 241 483 442 832 814 853	
Starvation Cap Reductin 0	
Storage Cap Reductin 0 0 0 0 0 0 0 0 0	
Reduced v/c Ratio 0.72 0.33 0.76 0.49 0.53 0.30 0.23 0.53	
Intersection Summary Area Type: Other	
Cycle Length: 120	
Offset: 117 (98%), Referenced to phase 1:NBSB, Start of Green	
Natural Cycle: 95	
Maximum v/c Ratio: 0.92	
Intersection Signal Delay: 41.1 Intersection LOS: D Intersection Canacity Utilization 74.2% ICLL evel of Service D	
Analysis Period (min) 15	
# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.	
Splits and Phases: 3: Adams St & Washington St & Dorchester Ave	
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Lano Croun	EDI	EDT	EDD	WDI	W/DT	WDD	NDI	NDT	NDD	CDI	CDT	CDD	an
Lane Configurations	EDL		EDK	VVDL		WDR	INDL		INDIK	JDL	301	SDK	02
Traffic Volume (vph)	44	54	56	51	81	58	49	220	23	13	323	33	
Future Volume (vph)	44	54	56	51	81	58	49	220	23	13	323	33	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Frt		0.951			0.959			0.989			0.988		
Flt Protected		0.986			0.987			0.992			0.998		
Satd. Flow (prot)	0	1769	0	0	1798	0	0	1847	0	0	1854	0	
Fit Permitted	0	0.835	0	0	0.888	0	0	0.890	0	0	0.985	0	
Sald. Flow (perm) Right Turn on Red	0	1498	Ves	0	1018	Ves	0	1657	Ves	0	1830	Ves	
Satd. Flow (RTOR)		39	103		30	103		8	103		9	103	
Link Speed (mph)		30			30			30			30		
Link Distance (ft)		710			686			615			708		
Travel Time (s)		16.1			15.6			14.0	1		16.1	1	
Peak Hour Eactor	0.98	0.98	0.98	0.93	0.93	0.93	0.91	0.91	0.91	0.98	0.98	0.98	
Heavy Vehicles (%)	0%	0%	2%	0%	0%	0%	0%	1%	0%	0%	1%	0%	
Adj. Flow (vph)	45	55	57	55	87	62	54	242	25	13	330	34	
Shared Lane Traffic (%)	0	457	0	0	204	0	0	201	0	•	277	0	
Lane Group Flow (vph)	0 Porm	157 ΝΔ	0	0 Porm	204	0	0 Porm	321 NA	0	0 Porm	3// NA	0	
Protected Phases	r Chill	5		i enn	5		i cilli	1		r citii	1		2
Permitted Phases	5	v		5			1			1			
Detector Phase	5	5		5	5		1	1		1	1		
Switch Phase	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0		10
Minimum Initial (S)	8.0	8.0		8.0	8.0		8.0	8.0		8.0	8.0		22.0
Total Split (s)	13.0	13.0		13.0	13.0		25.0	25.0		25.0	25.0		22.0
Total Split (%)	21.7%	21.7%		21.7%	21.7%		41.7%	41.7%		41.7%	41.7%		37%
Maximum Green (s)	8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		18.0
Yellow Time (s)	3.0	3.0		3.0	3.0		3.0	3.0		3.0	3.0		2.0
All-Red Time (S)	2.0	2.0		2.0	2.0		2.0	2.0		2.0	2.0		2.0
Total Lost Time (s)		5.0			5.0			5.0			5.0		
Lead/Lag							Lead	Lead		Lead	Lead		Lag
Lead-Lag Optimize?	2.0	2.0		2.0	2.0		Yes	Yes		Yes	Yes		Yes
Venicle Extension (s) Recall Mode	Z.U None	Z.U None		Z.0 None	Z.U None		Z.U Max	2.0 Max		2.0 Max	2.0 Max		3.0 None
Walk Time (s)	None	None		NULL	None		WIGA	IVIGA		IVIGA	IVIGA		8.0
Flash Dont Walk (s)													10.0
Pedestrian Calls (#/hr)													33
Act Effect Green (s)		8.4			8.4			21.0			21.0		
v/c Ratio		0.18			0.18			0.43			0.45		
Control Delay		25.7			32.6			14.2			14.2		
Queue Delay		0.0			0.0			0.0			0.0		
Total Delay		25.7			32.6			14.2			14.2		
Approach Delay		25.7			32.6			Б 14.2			Б 14.2		
Approach LOS		C			02.0 C			В			В		
90th %ile Green (s)	8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		18.0
90th %ile Term Code	Max	Max		Max	Max		MaxR	MaxR		MaxR	MaxR		Ped
70th %ile Term Code	8.0 May	0.8 Max		8.0 May	8.0 Max		20.0 MayP	20.0 MayP		20.0 MayP	20.0 MayP		18.0 Ped
50th %ile Green (s)	8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		0.0
50th %ile Term Code	Max	Max		Max	Max		MaxR	MaxR		MaxR	MaxR		Skip
30th %ile Green (s)	8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		0.0
30th %ile Ferm Code	Max	Max		Max	Max		MaxR	MaxR		MaxR	MaxR		Skip
10th %ile Term Code	8.0 Max	8.0 Max		8.0 Max	8.0 Max		∠u.u MaxR	20.0 MaxR		Z0.0 MaxR	Z0.0 MaxR		Skip
Queue Length 50th (ft)	man	21			32			32			38		
Queue Length 95th (ft)		#118			#168			163			188		
Internal Link Dist (ft)		630			606			535			628		
Rase Canacity (unb)		201			215			7/8			827		
Starvation Cap Reductn		0			0			0			027		
Spillback Cap Reductn		0			0			0			0		
Storage Cap Reductn		0			0			0			0		
Reduced v/c Ratio		0.52			0.65			0.43			0.46		
Intersection Summary													
Area Type:	Other												
Cycle Length: 60 Actuated Cycle Longth: 44.9													
Natural Cycle: 60													

Intersection Summary					
Area Type:	Other				
Cycle Length: 60					
Actuated Cycle Length: 46.8					
Natural Cycle: 60					
Control Type: Actuated-Unco	ordinated				
Maximum v/c Ratio: 0.65					
Intersection Signal Delay: 19.	5	Intersection LOS: B			
Intersection Capacity Utilization	on 57.4%	ICU Level of Service B			
Analysis Period (min) 15					
90th %ile Actuated Cycle: 60					
70th %ile Actuated Cycle: 60					
50th %ile Actuated Cycle: 38					
30th %ile Actuated Cycle: 38					
10th %ile Actuated Cycle: 38					
# 95th percentile volume ex	ceeds capacity, queue may be longer.				
Queue shown is maximum	n after two cycles.				
Splits and Phases: 4: Dorc	hester Ave/Dorchester St & Richmond S	t			
₩ø1			AL AD	₩ ø5	
25 e			22 6	12.0	

2017003:: 1200 Washington Street

• Build (2024) Condition

2017003::1120 Washington Stree	et
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2			
Lane Configurations	10	र्भ	1	00		05	7	4		<u></u>	₽	00				
Traffic Volume (vph)	40	102	146 146	32	95 95	35	304 304	302	66 66	42	151	33				
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900				
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00				
Frt Fit Protected		0.986	0.850		0.971		0.950	0.973		0.950	0.973					
Satd. Flow (prot)	0	1873	1615	0	1826	0	1805	1819	0	1752	1834	0				
Flt Permitted		0.986	4/45	0	0.990		0.567	4040		0.191	1001					
Sata. Flow (perm) Right Turn on Red	0	18/3	1615 Yes	0	1826	U Yes	1077	1819	U Yes	352	1834	U Yes				
Satd. Flow (RTOR)			236		9	105		10	100		8	105				
Link Speed (mph)		30			30			30			30					
Link Distance (It) Travel Time (s)		615 14 0			16.1			282			620 14 1					
Peak Hour Factor	0.95	0.95	0.95	0.86	0.86	0.86	0.94	0.94	0.94	0.92	0.92	0.92				
Heavy Vehicles (%)	0%	0%	0%	0%	0%	0%	0%	2%	0%	3%	1%	0%				
Adj. Flow (vpn) Shared Lane Traffic (%)	42	107	154	31	110	41	323	321	/0	40	164	30				
Lane Group Flow (vph)	0	149	154	0	188	0	323	391	0	46	200	0				
Turn Type	Split	NA	Perm	Split	NA		D.P+P	NA		Perm	NA		n			
Protected Phases Permitted Phases	3	3	3	4	4		5	15		1	1		2			
Detector Phase	3	3	3	4	4		5	15		1	1					
Switch Phase	10.0	10.0	10.0	10.0	10.0		5.0			10.0	10.0		1.0			
Minimum Initial (s) Minimum Split (s)	10.0	10.0	16.5	10.0	10.0		5.0			10.0	10.0		27.0			
Total Split (s)	23.0	23.0	23.0	19.0	19.0		15.0			36.0	36.0		27.0			
Total Split (%)	19.2%	19.2%	19.2%	15.8%	15.8%		12.5%			30.0%	30.0%		23%			
Yellow Time (s)	4.0	4.0	4.0	3.5	3.5		6.0 3.0			26.5	26.5		23.0			
All-Red Time (s)	2.5	2.5	2.5	3.0	3.0		6.0			6.0	6.0		2.0			
Lost Time Adjust (s)		0.0	0.0		0.0		0.0			0.0	0.0					
Lead/Lag	Lead	0.5 Lead	0.5 Lead	Laq	6.5 Lag		9.0			9.5 Lead	9.5 Lead		Lag			
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes					Yes	Yes		Yes			
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0		2.0			4.0	4.0		3.0 Nono			
Walk Time (s)	IVIAX	IVIAX	IVIAX	IVIAX	IVIAX		IVIAX			C-IVIAX	C-IVIAX		7.0			
Flash Dont Walk (s)													16.0			
Pedestrian Calls (#/hr)		22.7	22.7		12.5		22.0	11 5		26.5	26 F		16			
Actuated g/C Ratio		0.27	0.27		0.10		0.28	0.35		0.22	0.22					
v/c Ratio		0.29	0.25		0.95		0.97	0.62		0.60	0.49					
Control Delay		41.2	1.3		103.3		82.6	38.2		75.1	43.8					
Total Delay		41.2	1.3		103.3		82.6	38.7		75.1	43.8					
LOS		D	А		F		F	D		E	D					
Approach Delay		20.9			103.3			58.5			49.6					
90th %ile Green (s)	16.5	16.5	16.5	12.5	г 12.5		6.0	E		26.5	26.5		23.0			
90th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Ped			
70th %ile Green (s) 70th %ile Torm Code	16.5 MaxP	16.5 MaxP	16.5 MaxP	12.5 MaxP	12.5 MaxP		6.0 MaxP			26.5	26.5 Coord		23.0 Rod			
50th %ile Green (s)	43.5	43.5	43.5	12.5	12.5		6.0			26.5	26.5		0.0			
50th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip			
30th %ile Green (s) 30th %ile Term Code	43.5 MaxR	43.5 MaxR	43.5 MaxR	12.5 MaxR	12.5 MaxR		6.0 MaxR			26.5 Coord	26.5 Coord		0.0 Skin			
10th %ile Green (s)	43.5	43.5	43.5	12.5	12.5		6.0			26.5	26.5		0.0			
10th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip			
Queue Length 50th (it)		180	2		#267		m#354	238 m324		32 #92	207					
Internal Link Dist (ft)		535			630			202			540					
Turn Bay Length (ft)		E10	411		100		222	40F		77	411					
Starvation Cap Reductn		510	011		198		332	635 52		0	411					
Spillback Cap Reductn		0	0		0		0	0		0	0					
Storage Cap Reductn		0	0		0		0	0		0	0					
		0.29	0.20		0.93		0.97	0.07		0.00	0.49					
Area Type:)ther															
Cycle Length: 120	Milei															
Actuated Cycle Length: 120			(0)													
Uffset: 11 (9%), Referenced to Natural Cycle: 95	phase 1:NE	35B, Start	of Green													
Control Type: Actuated-Coordir	nated															
Maximum v/c Ratio: 0.97				l.e.												
Intersection Signal Delay: 55.0 Intersection Capacity Utilization	65.1%			In	U Level of	Service (2									
Analysis Period (min) 15				10	0.0101											
# 95th percentile volume exce Quoue shown is maximum.	eds capac	ity, queue	may be lo	nger.												
m Volume for 95th percentile	queue is m	netered by	upstream	signal.												
Colline and Pl	·			- han - 1 -												
Spiits and Phases: 1: Washir	igion Stree	a & Mortor	ı Street/Ri	unmond S	ueet									4	4	
♥ Ø1 (R)					₹RØ2						Ø3			∮ Ø4	"N Ø5	

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Lane Group	EBL	EBR	NBL	NBT	SBT	SBR	SBR2	NEL2	NEL	NER	Ø2		
Lane Configurations	٦	N.	٦		1		1	٦		1			
Traffic Volume (vph)	269	250	196	406	149	0	145	0	0	0			
Future volume (vpn)	1000	250	190	406	149	1900	145	1000	1900	1900			
Storage Length (ft)	75	0	100	1700	1700	75	1700	1700	0	0			
Storage Lanes	1	1	1			1			1	1			
Taper Length (ft)	100	1.00	100	1.00	1.00	1.00	1.00	1.00	25	1.00			
Frt	1.00	0.850	1.00	1.00	1.00	1.00	0.850	1.00	1.00	1.00			
Flt Protected	0.950	0.000	0.950				0.000						
Satd. Flow (prot)	1805	1615	1787	1900	1900	0	1615	1863	0	1863			
Fit Permitted Sate Flow (norm)	0.950	1615	0.950	1000	1000	0	1615	1062	0	1062			
Right Turn on Red	1005	1015	1707	1700	1700	U	Yes	1005	0	Yes			
Satd. Flow (RTOR)							173						
Link Speed (mph)	30			30	30				30				
LINK DISTANCE (IT) Travel Time (s)	464			447	255				214				
Peak Hour Factor	0.97	0.97	0.94	0.94	0.88	0.88	0.88	0.92	0.92	0.92			
Heavy Vehicles (%)	0%	0%	1%	0%	0%	1%	0%	2%	2%	2%			
Adj. Flow (vph)	277	258	209	432	169	0	165	0	0	0			
I ane Group Flow (vph)	277	258	209	432	169	0	165	0	0	0			
Turn Type	Prot	pt+ov	Prot	NA	NA	0	Prot	Prot	Ū	Prot			
Protected Phases	3	13	1	15	5		5	4		4	2		
Permitted Phases	2	1.2	1	1.5	-		-						
Switch Phase	3	13	1	15	5		C	4		4			
Minimum Initial (s)	10.0		10.0		10.0		10.0	4.0		4.0	1.0		
Minimum Split (s)	16.5		15.5		16.5		16.5	10.0		10.0	26.0		
Total Split (s)	27.0		33.0		24.0		24.0	10.0		10.0	26.0		
Maximum Green (s)	22.5%		27.5%		20.0%		20.0%	8.3%		8.3%	22%		
Yellow Time (s)	4.0		3.0		4.0		4.0	3.5		3.5	2.0		
All-Red Time (s)	2.5		2.5		2.5		2.5	2.5		2.5	2.0		
Lost Time Adjust (s)	0.0		0.0		0.0		0.0	0.0		0.0			
Lead/Lag	Lead		Lead		0.0		0.0	Lag		Lag	Lag		
Lead-Lag Optimize?	Yes		Yes					Yes		Yes	Yes		
Vehicle Extension (s)	2.0		2.0		4.0		4.0	2.0		2.0	3.0		
Recall Mode Walk Time (s)	None		C-Max		None		None	None		None	None 7.0		
Flash Dont Walk (s)											15.0		
Pedestrian Calls (#/hr)											7		
Act Effct Green (s)	22.2	81.1	53.5	80.6	20.6		20.6						
v/c Ratio	0.18	0.68	0.45	0.67	0.17		0.17						
Control Delay	67.9	8.2	11.6	2.7	52.5		16.8						
Queue Delay	0.0	0.0	0.0	0.4	0.0		0.0						
Total Delay	67.9	8.2	11.6 P	3.1	52.5		16.8 P						
Approach Delay	39.1	A	Б	5.9	34.9		Б						
Approach LOS	D			А	С								
90th %ile Green (s)	20.5		27.5		27.5		27.5	0.0		0.0	22.0		
70th %ile Green (s)	26.8		200rd 49.7		25.0		25.0	SKIP		SKIP	Ped		
70th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip		
50th %ile Green (s)	24.7		55.5		21.3		21.3	0.0		0.0	0.0		
50th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip		
30th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip		
10th %ile Green (s)	17.3		71.6		12.6		12.6	0.0		0.0	0.0		
10th %ile Term Code	Gap	50	Coord		Gap		Gap	Skip		Skip	Skip		
Queue Length 50th (It)	203 #370	58 109	46 m149	4 120	131 m182		33 m78						
Internal Link Dist (ft)	384	107	111147	367	175		mo		134				
Turn Bay Length (ft)	75		100				75						
Base Capacity (vph)	343	1099	796	1258	344		434						
Spillback Cap Reductin	0	0	0	390	0		0						
Storage Cap Reductn	0	0	0	0	0		0						
Reduced v/c Ratio	0.81	0.23	0.26	0.50	0.49		0.38						
Intersection Summary													
Area Type:	Other												
Cycle Length: 120 Actuated Cycle Longth: 120													
Offset: 0 (0%). Referenced to	phase 1:NB	TL. Start o	f Green										
Natural Cycle: 85	,	,											
Control Type: Actuated-Coord	linated												
Intersection Signal Dolay: 24	1			In	ersection	05.0							
Intersection Capacity Utilization	on 49.5%			IC	U Level of	Service A							
Analysis Period (min) 15				.0									
# 95th percentile volume exercise of the second	ceeds capac	ity, queue	may be lo	nger.									
m Volume for 95th percentile	e queue is m	ues. ietered hv	upstream	signal									
			Poulouni										
Splits and Phases: 2: Drive	way & Wash	ington Str	eet & Rive	r Street									
Ø1 (R)				λ i ,	Ø2					Ø3		7 Ø4 1 Ø5	
33 s				26 s					27 s			10 s 24 s	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2		
Lane Configurations		ę	1	٦	ţ,		٦	↑	1		ፋጉ				
Traffic Volume (vph)	66 66	208	165 165	135	161	20	386 386	307 307	387 387	6	166 166	87 87			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900			
Storage Length (ft)	0		25	0		50	0		0	0		0			
Taper Length (ft)	25			25			25			25		U			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.95	0.95	0.95			
Fit Protected		0.988	0.850	0.950	0.983		0.950		0.850		0.949				
Satd. Flow (prot)	0	1863	1615	1805	1851	0	1787	1900	1615	0	3389	0			
Fit Permitted Satd, Flow (perm)	0	0.749	1615	0.379	1851	0	0.581	1900	1615	0	3203	0			
Right Turn on Red	-		Yes			Yes			Yes			Yes			
Satd. Flow (RTOR)		20	77		5			20	399		64				
Link Distance (ft)		447			673			443			615				
Travel Time (s)	0.0/	10.2	0.0/	0.02	15.3	0.02	0.07	10.1	0.07	0.00	14.0	0.00			
Heavy Vehicles (%)	0.96	0.96	0.96	0.92	0.92	0.92	0.97	0.97	0.97	0.98	0.98	0.98			
Adj. Flow (vph)	69	217	172	147	175	22	398	316	399	6	169	89			
Shared Lane Traffic (%) Lane Group Flow (vph)	0	286	172	147	197	0	398	316	399	0	264	0			
Turn Type	Perm	NA	pt+ov	Perm	NA	Ū	D.P+P	NA	Prot	Perm	NA	0			
Protected Phases	5	5	56	5	5		6	16	16	1	1		2		
Detector Phase	5	5	56	5	5		6	16	16	1	1				
Switch Phase	40.0	10.0		10.0	10.0					40.0	40.0		10		
Minimum Initial (s)	10.0	10.0 18.0		10.0 18.0	10.0 18.0		8.0 14.5			10.0 17.5	10.0 17.5		32.0		
Total Split (s)	39.0	39.0		39.0	39.0		22.0			27.0	27.0		32.0		
Total Split (%) Maximum Green (s)	32.5%	32.5%		32.5%	32.5%		18.3%			22.5%	22.5%		27%		
Yellow Time (s)	4.5	4.5		4.5	4.5		3.0			4.0	4.0		2.0		
All-Red Time (s)	3.5	3.5		3.5	3.5		3.5			3.5	3.5		2.0		
Total Lost Time (s)		8.0		8.0	8.0		6.5				7.5				
Lead/Lag	Lead	Lead		Lead	Lead		Lag			Lead	Lead		Lag		
Vehicle Extension (s)	Yes 2.0	Yes 2.0		Yes 2.0	Yes 2.0		Yes 4.0			Yes 2.0	Yes 2.0		Yes 3.0		
Recall Mode	None	None		None	None		None			C-Max	C-Max		None		
Walk Time (s) Flash Dont Walk (s)													7.0		
Pedestrian Calls (#/hr)													49		
Act Effct Green (s)		27.1	52.0	27.1	27.1		46.3	51.8	51.8		26.9				
v/c Ratio		0.23	0.43	0.23	0.23		0.39	0.43	0.43		0.22				
Control Delay		71.6	9.6	94.1	42.0		41.6	29.0	4.3		33.9				
Queue Delay Total Delay		0.0 71.6	0.0 9.6	0.0 94.1	42.0		0.0 41.6	0.0 29.0	0.0 4.3		0.0				
LOS		E	A	F	D		D	С	A		С				
Approach Delay Approach LOS		48.3 D			64.3 F			24.6 C			33.9 C				
90th %ile Green (s)	31.0	31.0		31.0	31.0		15.5			19.5	19.5		28.0		
90th %ile Term Code	Max 21.0	Max 21.0		Max 21.0	Max 21.0		Max 15 5			Coord	Coord		Ped		
70th %ile Term Code	Max	Max		Max	Max		Max			Coord	Coord		Ped		
50th %ile Green (s)	29.8 Con	29.8		29.8 Con	29.8		16.7			19.5 Coord	19.5 Coord		28.0 Ded		
30th %ile Green (s)	25.2	25.2		25.2	25.2		21.3			19.5	19.5		28.0		
30th %ile Term Code	Gap	Gap		Gap	Gap		Max			Coord	Coord		Ped		
10th %ile Green (s)	I8.7 Gap	18.7 Gap		18.7 Gap	Gap		Z3.0 Gap			56.3 Coord	56.3 Coord		0.0 Skip		
Queue Length 50th (ft)	r P	147	14	108	125		250	188	0		73				
Queue Length 95th (ft) Internal Link Dist (ft)		#346 367	66	#221	195 593		#348	278 363	67		117 535				
Turn Bay Length (ft)		507	25		070			000			555				
Base Capacity (vph) Starvation Cap Poducto		364	721	186	481		527	819	923		766				
Spillback Cap Reductn		0	0	0	0		0	0	0		0				
Storage Cap Reductn		0 70	0	0	0 41		0	0	0 42		0				
		0.79	0.24	0.79	0.41		0.76	0.39	0.43		0.34				
Intersection Summary Area Type:	Other													 	
Cycle Length: 120 Actuated Cycle Length: 120	d to phace 1	NDCD Ct	ort of Croc	20											
Natural Cycle: 95	a to pridse T	, שכחווי		а											
Control Type: Actuated-Coord	linated														
Intersection Signal Delay: 37.0	0			In	tersection	LOS: D									
Intersection Capacity Utilization	on 79.8%			IC	U Level of	Service I)								
Analysis Period (min) 15 # 95th percentile volume ex Queue shown is maximum	ceeds capac after two cy	tity, queue cles.	may be lo	nger.											
Solits and Phases: 3. Adam	ns Street & V	Vashingtor	street &	Dorcheste	r Avenue										

Splits and Phases: 3: Adams Street & Washington	Street & Dorchester Avenue		
₩ø1(R)	₩\$ _{Ø2}	★ 05	₩ Ø6
27 s	32 s	39 s	22 s

2017003::1120 Washington Street

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2
Lane Configurations	62	4	50	16	4 2	/1	52	4	0	12	↔ 207	40	
Future Volume (vph)	62	56	59	16	43	41	53	336	9	13	207	40	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Frt	1.00	0.955	1.00	1.00	0.944	1.00	1.00	0.997	1.00	1.00	0.979	1.00	
Flt Protected		0.983			0.992			0.993			0.998		
Satd. Flow (prot)	0	1772	0	0	1779	0	0	1865	0	0	1842	0	
Satd. Flow (perm)	0	1557	0	0	1682	0	0	1743	0	0	1799	0	
Right Turn on Red		05	Yes			Yes		0	Yes			Yes	
Sata. Flow (RTOR) Link Speed (mph)		35 30			44 30			2 30			16 30		
Link Distance (ft)		710			686			615			708		
Travel Time (s)	0.09	16.1	0.00	0.02	15.6	0.02	0.01	14.0	0.01	0.09	16.1	0.00	
Heavy Vehicles (%)	0.98	0.98	2%	0.93	0.93	0.93	0.91	1%	0.91	0.98	1%	0.98	
Adj. Flow (vph)	63	57	60	17	46	44	58	369	10	13	211	41	
Shared Lane Traffic (%) Lane Group Flow (vph)	0	180	0	0	107	0	0	437	0	0	265	0	
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA		
Protected Phases	5	5		5	5		1	1		1	1		2
Detector Phase	5	5		5	5		1	1		1	1		
Switch Phase	~ ~	~ ~		~ ~	0.0		0.0	0.0		0.0	0.0		1.0
winimum initial (s) Minimum Split (s)	8.0 13.0	8.0 13.0		8.0 13.0	8.0 13.0		8.0 13.0	8.0 13.0		8.0 13.0	8.0 13.0		1.0 22.0
Total Split (s)	13.0	13.0		13.0	13.0		25.0	25.0		25.0	25.0		22.0
Total Split (%)	21.7%	21.7%		21.7%	21.7%		41.7%	41.7%		41.7%	41.7%		37%
Viaximum Green (s) Yellow Time (s)	8.0 3.0	8.0		8.0	8.0 3.0		20.0	20.0		20.0	20.0		18.0
All-Red Time (s)	2.0	2.0		2.0	2.0		2.0	2.0		2.0	2.0		2.0
Lost Time Adjust (s)		0.0			0.0			0.0			0.0		
Lead/Lag		5.0			5.0		Lead	5.0 Lead		Lead	5.0 Lead		Lag
Lead-Lag Optimize?	. ·						Yes	Yes		Yes	Yes		Yes
venicle Extension (s) Recall Mode	2.0 None	2.0 None		2.0 None	2.0 None		2.0 Max	2.0 Max		2.0 Max	2.0 Max		3.0 None
Walk Time (s)	None	None					AUGA	MUA		AUGA	MuA		8.0
Flash Dont Walk (s)													10.0
Pedestrian Calls (#/hr) Act Effct Green (s)		8.3			8.3			23.4			23.4		6
Actuated g/C Ratio		0.18			0.18			0.52			0.52		
v/c Ratio		0.58			0.31			0.49			0.28		
Queue Delay		25.0 0.0			0.0			0.0			9.2		
Total Delay		25.0			14.7			12.8			9.2		
LUS Approach Delay		25 O			В 147			В 12.8			9.2		
Approach LOS		C			B			B			A		
90th %ile Green (s)	8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		18.0
70th %ile Green (s)	1VIAX 8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		0.0
70th %ile Term Code	Max	Max		Max	Max		MaxR	MaxR		MaxR	MaxR		Skip
50th %ile Green (s) 50th %ile Term Code	8.0 Max	8.0 Max		8.0 Max	8.0 Max		20.0 MaxP	20.0 MaxP		20.0 MaxP	20.0 MaxP		0.0 Skip
30th %ile Green (s)	8.0	8.0		8.0	8.0		20.0	20.0		20.0	20.0		0.0
30th %ile Term Code	Max	Max		Max	Max		MaxR	MaxR		MaxR	MaxR		Skip
10th %ile Green (s) 10th %ile Term Code	8.0 Max	8.0 Max		8.0 Max	8.0 Max		35.0 Dwell	35.0 Dwell		35.0 Dwell	35.0 Dwell		0.0 Skip
Queue Length 50th (ft)	Max	27		Max	11		Direi	48		DWCI	24		Onip
Queue Length 95th (ft)		#143			61			#267			126		
Turn Bay Length (ft)		030			000			030			028		
Base Capacity (vph)		313			343			897			933		
Starvation Cap Reductn		0			0			0			0		
Storage Cap Reductn		0			0			0			0		
Reduced v/c Ratio		0.58			0.31			0.49			0.28		
Intersection Summary													
Area Type: C	Other												
Actuated Cycle Length: 45.4													
Natural Cycle: 60													
Control Type: Actuated-Uncoor Maximum v/c Patio: 0.59	dinated												
Intersection Signal Delay: 14.2				In	tersection	LOS: B							
Intersection Capacity Utilization	1 62.6%			IC	U Level of	Service E							
Analysis Period (min) 15 90th %ile Actuated Cycle: 60													
70th %ile Actuated Cycle: 38													
50th %ile Actuated Cycle: 38													
10th %ile Actuated Cycle: 53													
# 95th percentile volume exce	eeds capac	tity, queue	may be lo	nger.									
Queue shown is maximum a	arter two cy	cies.											
Splits and Phases: 4: Dorche	ester Avenu	ue & Richm	ond Stree	t									
₩ø1								de la compañía de la comp					
25 s							2	2 s					

Intersection Int Delay, s/veh 0.3 Mayamant N/D

WBL	WBR	NBT	NBR	SBL	SBT	
Y		f.			÷	
2	12	673	2	6	323	
2	12	673	2	6	323	
0	0	0	0	0	0	
Stop	Stop	Free	Free	Free	Free	
-	None	-	None	-	None	
0	-	-	-	-	-	
0	-	0	-	-	0	
0	-	0	-	-	0	
92	92	92	92	92	92	
2	2	2	2	2	2	
2	13	732	2	7	351	
	WBL 2 2 0 Stop - 0 0 0 0 92 2 2 2	WBL WBR Y 12 2 12 0 0 Stop Stop - None 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 92 92 2 2 2 13	WBL WBR NBT Y 12 673 2 12 673 2 12 673 0 0 0 Stop Stop Free - None - 0 - 0 0 - 0 0 - 0 0 - 0 0 - 0 0 - 0 0 - 0 0 - 0 0 - 0 0 - 0 0 - 0 10 - 0 92 92 92 2 13 732	WBL WBR NBT NBR Y 12 673 2 2 12 673 2 2 12 673 2 0 0 0 0 Stop Free Free - None - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 92 92 92 92 2 2 2 2 13 732 2	WBL WBR NBT NBR SBL Y I <tdi< td=""> I</tdi<>	WBL WBR NBT NBR SBL SBT Y I <tdi< td=""> <tdi< td=""> I <td< td=""></td<></tdi<></tdi<>

Major/Minor	Minor1		Major1		Major2		
Conflicting Flow All	1097	733	0	0	734	0	
Stage 1	733	-	-	-	-	-	
Stage 2	364	-	-	-	-	-	
Critical Hdwy	6.42	6.22	-	-	4.12	-	
Critical Hdwy Stg 1	5.42	-	-	-	-	-	
Critical Hdwy Stg 2	5.42	-	-	-	-	-	
Follow-up Hdwy	3.518	3.318	-	-	2.218	-	
Pot Cap-1 Maneuver	236	421	-	-	871	-	
Stage 1	475	-	-	-	-	-	
Stage 2	703	-	-	-	-	-	
Platoon blocked, %			-	-		-	
Mov Cap-1 Maneuver	234	421	-	-	871	-	
Mov Cap-2 Maneuver	234	-	-	-	-	-	
Stage 1	475	-	-	-	-	-	
Stage 2	696	-	-	-	-	-	
Approach	WB		NB		SB		

Approach	VVB	NB	SB	
HCM Control Delay, s	14.9	0	0.2	
HCM LOS	В			

Minor Lane/Major Mvmt	NBT	NBRW	/BLn1	SBL	SBT
Capacity (veh/h)	-	-	378	871	-
HCM Lane V/C Ratio	-	-	0.04	0.007	-
HCM Control Delay (s)	-	-	14.9	9.2	0
HCM Lane LOS	-	-	В	А	А
HCM 95th %tile Q(veh)	-	-	0.1	0	-

Build (2024) Condition, Weekday p.m. Peak H	lou
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2		
Lane Configurations		4	1	10	4	01	150	^	10	1	4	(5			
Future Volume (vph)	28	109	194 194	49 49	117	21	159	212	49	31	190	65 65			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900			
Lane Util. Factor Frt	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
Fit Protected		0.990	0.000		0.987		0.950	0.772		0.950	0.702				
Satd. Flow (prot)	0	1881	1615	0	1847	0	1805	1832	0	1805	1814	0			
Fit Permitted Satd, Flow (perm)	0	0.990	1615	0	0.987	0	0.385	1832	0	0.411	1814	0			
Right Turn on Red	-		Yes			Yes			Yes			Yes			
Satd. Flow (RTOR)		20	236		4			10			13				
Link Distance (ft)		615			710			282			620				
Travel Time (s)		14.0			16.1			6.4			14.1				
Peak Hour Factor Heavy Vehicles (%)	0.97	0.97	0.97	0.88	0.88	0.88	0.96	0.96	0.96	0.94	0.94	0.94			
Adj. Flow (vph)	29	112	200	56	133	24	166	221	51	33	202	69			
Shared Lane Traffic (%)			000		010			070		00	074	0			
Lane Group Flow (vpn) Turn Type	0 Split	141 NA	200 Perm	0 Split	213 NA	0	166 D P+P	272 NA	0	33 Perm	2/1 NA	0			
Protected Phases	3	3	1 cm	4	4		5	15		i ciiii	1		2		
Permitted Phases	0	0	3				1	4.5		1					
Switch Phase	3	3	3	4	4		5	15		1	1				
Minimum Initial (s)	10.0	10.0	10.0	10.0	10.0		5.0			10.0	10.0		1.0		
Minimum Split (s)	16.5	16.5	16.5	16.5	16.5		14.0			19.5	19.5		27.0		
Total Split (S)	23.0 19.2%	23.0	23.0	20.0	20.0		15.0 12.5%			35.0 20.2%	35.0 29.2%		27.0		
Maximum Green (s)	16.5	16.5	16.5	13.5	13.5		6.0			25.5	25.5		23.0		
Yellow Time (s)	4.0	4.0	4.0	3.5	3.5		3.0			3.5	3.5		2.0		
All-Red Time (s)	2.5	2.5	2.5	3.0	3.0		6.0			6.0	6.0		2.0		
Total Lost Time (s)		6.5	6.5		6.5		9.0			9.5	9.5				
Lead/Lag	Lead	Lead	Lead	Lag	Lag					Lead	Lead		Lag		
Lead-Lag Optimize?	Yes	Yes	Yes	Yes	Yes		2.0			Yes	Yes		Yes		
Recall Mode	Max	Max	Max	Max	Max		Max			C-Max	C-Max		None		
Walk Time (s)													7.0		
Flash Dont Walk (s)													16.0		
Act Effct Green (s)		38.1	38.1		13.5		32.0	40.5		25.5	25.5		9		
Actuated g/C Ratio		0.32	0.32		0.11		0.27	0.34		0.21	0.21				
v/c Ratio		0.24	0.30		1.01		0.67	0.44		0.20	0.69				
Queue Delay		0.0	4.2		0.0		40.8	0.0		42.0	0.0				
Total Delay		34.9	4.2		116.6		40.8	27.2		42.6	51.4				
LOS Approach Dolay		16 0	A		F		D	C 22.2		D	D				
Approach LOS		10.9 B			F			52.5 C			50.5 D				
90th %ile Green (s)	16.5	16.5	16.5	13.5	13.5		6.0			25.5	25.5		23.0		
90th %ile Term Code 70th %ile Green (s)	MaxR 43.5	MaxR 43.5	MaxR 43.5	MaxR 13.5	MaxR 13.5		MaxR 6.0			25 5	Coord 25.5		Ped		
70th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip		
50th %ile Green (s)	43.5	43.5	43.5	13.5	13.5		6.0			25.5	25.5		0.0		
30th %ile Ferm Code	MaxR 43.5	MaxR 43.5	MaxR 43.5	13.5	MaxR 13.5		MaxR 6.0			25.5	25 5		SKIP		
30th %ile Term Code	MaxR	MaxR	MaxR	MaxR	MaxR		MaxR			Coord	Coord		Skip		
10th %ile Green (s)	43.5	43.5	43.5	13.5	13.5		6.0			25.5	25.5		0.0		
Oueue Length 50th (ft)	MaxR	MaxR 75	MaxR	MaxR	MaxR ~166		MaxR 82	182		21	Coord 186		Бкір		
Queue Length 95th (ft)		171	41		#318		m117	m176		52	282				
Internal Link Dist (ft)		535			630			202			540				
Furn Bay Length (It) Base Canacity (vph)		596	673		211		248	624		165	395				
Starvation Cap Reductn		0	0		0		0	0		0	0				
Spillback Cap Reductn		0	0		0		0	0		0	0				
Reduced v/c Ratio		0.24	0.30		1 01		0.67	0 44		0 20	0.69				
Intersection Summary		0.21	0.00				0.07	0.111		0.20	0.07				
Area Type:	Other														
Cycle Length: 120															
Actuated Cycle Length: 120 Offset: 65 (54%) Referenced t	to phase 1.1	VRSR Sta	rt of Green	ı											
Natural Cycle: 95	to pridoc 1.1	1000, 010													
Control Type: Actuated-Coord	inated														
Maximum v/c Ratio: 1.01 Intersection Signal Delay: 46.4	1			In	tersection										
Intersection Capacity Utilizatio	n 60.5%			IC	CU Level of	Service I	3								
Analysis Period (min) 15															
 Volume exceeds capacity, Oueue shown is maximum 	queue is th	eoretically	infinite.												
# 95th percentile volume exc	ceeds capac	city, queue	may be lo	onger.											
Queue shown is maximum	after two cy	cles.													
m Volume for 95th percentile	e queue is n	netered by	upstream	signal.											
Splits and Phases: 1: Wash	ington St &	Morton St	/Richmond	l St						.					
Ø1 (R)					A log					40	3			V Ø4	↑ ø₅
35 s				2	7 s					23 s				20 s	15 s

Lane Group Lane Configurations	FBI											
Lane Configurations	LDL	EBR	NBL	NBT	SBT	SBR	SBR2	NEL2	NEL	NER	Ø2	
Troffic Vicking (mil)	1	1	1	4	100	-	100	7	-	1		
Future Volume (vph)	166	238	270	230	202	0	199	0	0	0		
Ideal Flow (vphpl)	1900	∠38 1900	270 1900	230 1900	1900	1900	199	1900	1900	1900		
Storage Length (ft)	75	0	100	.700	.700	75	. 700	.700	0	0		
Storage Lanes	1	1	1			1			1	1		
Taper Length (ft)	100		100						25			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		
FIL FIL Protected	0.050	0.850	0.050				0.850					
Satd. Flow (prot)	1787	1615	1805	1900	1863	0	1615	1863	0	1863		
Flt Permitted	0.950		0.950									
Satd. Flow (perm)	1787	1615	1805	1900	1863	0	1615	1863	0	1863		
Right Turn on Red							Yes			Yes		
Satd. Flow (RTOR)	20			20	20		155		20			
Link Speeu (mpn)	30			30	3U 255				30 214			
Travel Time (s)	10.5			10.2	5.8				4.9			
Peak Hour Factor	0.95	0.95	0.99	0.99	0.96	0.96	0.96	0.92	0.92	0.92		
Heavy Vehicles (%)	1%	0%	0%	0%	2%	0%	0%	2%	2%	2%		
Adj. Flow (vph)	175	251	273	232	210	0	207	0	0	0		
Shared Lane Traffic (%)	175	261	171	121	210	0	207	0	^	0		
сане Group Flow (Vpn) Тигр Туре	175 Prot	251	273 Prot	232 NA	210	U	207 Prot	Prot	U	Prot		
Protected Phases	3	13	1	15	5		5	4		4	2	
Permitted Phases	5	15		10	5		5	-		-	2	
Detector Phase	3	13	1	15	5		5	4		4		
Switch Phase												
Minimum Initial (s)	10.0		10.0		10.0		10.0	4.0		4.0	1.0	
IVIINIMUM Split (s)	16.5		15.5		16.5		16.5	10.0		10.0	24.0	
Total Split (%)	21.0		28.3%		29.0		29.0	8.3%		8.3%	20.0	
Maximum Green (s)	14.5		28.5		22.5		22.5	4.0		4.0	24.0	
Yellow Time (s)	4.0		3.0		4.0		4.0	3.5		3.5	2.0	
All-Red Time (s)	2.5		2.5		2.5		2.5	2.5		2.5	0.0	
Lost Time Adjust (s)	0.0		0.0		0.0		0.0	0.0		0.0		
Load/Log	6.5		5.5		6.5		6.5	6.0		6.0	10-	
Lead/Lag	Lead		Lead					Lag		Lag	Lag	
Vehicle Extension (s)	20		20		4.0		4.0	20		20	3.0	
Recall Mode	None		C-Max		None		None	None		None	None	
Walk Time (s)											7.0	
Flash Dont Walk (s)											15.0	
Pedestrian Calls (#/hr)	45.4	74.0	54.0	00.0	04.0		04.0				14	
Actuated a/C Patio	15.1	74.3	54.9	83.3	21.9		21.9					
v/c Ratio	0.78	0.25	0.33	0.18	0.62		0.49					
Control Delay	73.8	9.7	24.1	9.3	49.2		14.8					
Queue Delay	0.0	0.0	0.0	0.0	0.0		0.0					
Total Delay	73.8	9.7	24.1	9.3	49.2		14.8					
LUS Approach Dolou	24 O	A	C	A	22 1		В					
Approach LOS	30.0 D			17.3 B	32.1 C							
90th %ile Green (s)	16.5		30.4	5	30.6		30.6	0.0		0.0	22.0	
90th %ile Term Code	Max		Coord		Gap		Gap	Skip		Skip	Ped	
70th %ile Green (s)	16.5		35.5		25.5		25.5	0.0		0.0	22.0	
70th %ile Term Code	Max		Coord		Gap		Gap	Skip		Skip	Ped	
50th %ile Green (S)	1/.1 Con		62.2		22.2 Con		22.2 Gon	0.0 Skip		0.0 Skip	0.0 Skin	
30th %ile Green (s)	Gap 14.6		0.00 69.0		Gap 17.9		Gap 17.9	- SKIP		SKIP 0.0	ол	
30th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip	
10th %ile Green (s)	11.0		77.3		13.2		13.2	0.0		0.0	0.0	
10th %ile Term Code	Gap		Coord		Gap		Gap	Skip		Skip	Skip	
Queue Length 50th (ft)	131	58	60	45	153		50					
Queue Length 95th (ft)	#229	116	254	10/	m1/3		m29		124			
Turn Bay Length (ff)	75		100	307	170		75		154			
Base Capacity (vph)	235	1009	825	1298	383		455					
Starvation Cap Reductn	0	0	0	0	0		0					
Spillback Cap Reductn	0	0	0	0	0		0					
Storage Cap Reductn	0	0	0	0	0		0					
Reduced NC Ratio	0.74	0.25	0.33	0.18	0.55		0.45					
Intersection Summary	Oth											
Area Type: Cycle Length: 120	Other											
Actuated Cycle Length: 120												
Offset: 0 (0%), Referenced to	phase 1:NB	TL, Start o	of Green									
Natural Cycle: 85	·											
Control Type: Actuated-Coor	dinated											
Maximum v/c Ratio: 0.78	0					00.0						
Intersection Signal Delay: 27	.8 ion 50.2%			In	tersection	LUS: C						
Analysis Period (min) 15	1011 30.2%			IC	O Level Of	Service A						
 # 95th percentile volume e: 	xceeds capac	ity, queue	may be lo	nger.								
Queue shown is maximun	n after two cy	cles.	<i>,</i>	0								
m Volume for 95th percenti	ile queue is m	netered by	upstream	signal.								
Solits and Phases 2. Drive	oway & Wach	inaton C+	8, Rivor Ct									
	cway & WaSII	แหรเบป อไ	a river 31	¥						*		∔اد ا
SN (31 (0)				1	RØ2				-	🗲 Ø3		↓ Ø4 ↓ Ø5

2017003::1120 Washington Street

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2
Lane Configurations		با	1	٦.	4î		۳.	↑	1		ፋጉ		
Traffic Volume (vph)	51	163	230	169	204	16	230	240	184	19	350	74	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Storage Length (ft)	0		25	0		50	0		0	0		0	
Storage Lanes	0		1	1		1	25		1	0		0	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.95	0.95	0.95	
Frt			0.850		0.989				0.850		0.975		
Fit Protected	0	0.988	1/15	0.950	1070	0	0.950	1000	1/15	0	0.998	0	
Flt Permitted	U	0.634	1015	0.496	18/9	0	0.405	1900	1013	0	0.930	U	
Satd. Flow (perm)	0	1190	1615	942	1879	0	770	1900	1615	0	3273	0	
Right Turn on Red			Yes		2	Yes			Yes		10	Yes	
Link Speed (mph)		30	100		30			30	192		30		
Link Distance (ft)		447			673			443			615		
Travel Time (s)	0.07	10.2	0.07	0.02	15.3	0.02	0.0/	10.1	0.0/	0.07	14.0	0.07	
Heavy Vehicles (%)	2%	1%	0.97	0.92	0.92	0.92	0.96	0.96	0.96	0.97	0.97	0.97	
Adj. Flow (vph)	53	168	237	184	222	17	240	250	192	20	361	76	
Shared Lane Traffic (%)	0	221	227	104	220	0	240	250	102	0	457	0	
Turn Type	Perm	NA	pt+ov	Perm	Z39 NA	0	D.P+P	230 NA	Prot	Perm	437 NA	0	
Protected Phases		5	56		5		6	16	16		1		2
Permitted Phases	5	F	F /	5	-		1	17	1/	1	1		
Switch Phase	5	C	0 C	D	5		0	10	10	1	1		
Minimum Initial (s)	10.0	10.0		10.0	10.0		8.0			10.0	10.0		1.0
Minimum Split (s)	18.0	18.0		18.0	18.0		14.5			17.5	17.5		32.0
Total Split (%)	39.0	39.0		39.0	39.0		13.3%			27.5%	27.5%		32.0 27%
Maximum Green (s)	31.0	31.0		31.0	31.0		9.5			25.5	25.5		28.0
Yellow Time (s)	4.5	4.5		4.5	4.5		3.0			4.0	4.0		2.0
All-Red Time (S)	3.5	3.5		3.5	3.5		3.5			3.5	3.5		2.0
Total Lost Time (s)		8.0		8.0	8.0		6.5				7.5		
Lead/Lag	Lead	Lead		Lead	Lead		Lag			Lead	Lead		Lag
Vehicle Extension (s)	2 0	2 0		Yes 2.0	2 0		Yes 4 0			2 0	2 0		3 0
Recall Mode	None	None		None	None		None			C-Max	C-Max		None
Walk Time (s)													7.0
Pedestrian Calls (#/hr)													43
Act Effct Green (s)		25.8	44.2	25.8	25.8		47.6	53.1	53.1		34.7		10
Actuated g/C Ratio		0.22	0.37	0.22	0.22		0.40	0.44	0.44		0.29		
Control Delav		65.2	7.6	88.8	47.0		34.8	27.0	4.5		0.48 39.6		
Queue Delay		0.0	0.0	0.0	0.0		0.0	0.0	0.0		0.0		
Total Delay		65.2	7.6	88.8	47.0		34.8	27.0	4.5		39.6		
Approach Delay		35.4	A	г	65.2		C	23.4	А		39.6		
Approach LOS		D			E			С			D		
90th %ile Green (s)	31.0 Mox	31.0 Mox		31.0 Max	31.0 Mox		9.5 Mox			25.5 Coord	25.5 Coord		28.0 Dod
70th %ile Green (s)	31.0	31.0		31.0	31.0		9.5			25.5	25.5		28.0
70th %ile Term Code	Max	Max		Max	Max		Max			Coord	Coord		Ped
50th %ile Green (s)	28.3 Gan	28.3 Gan		28.3 Gap	28.3 Gap		12.2 Max			25.5 Coord	25.5 Coord		28.0 Pod
30th %ile Green (s)	23.1	23.1		23.1	23.1		17.4			25.5	25.5		28.0
30th %ile Term Code	Gap	Gap		Gap	Gap		Max			Coord	Coord		Ped
10th %ile Green (s) 10th %ile Term Code	15.6 Gan	15.6 Gan		15.6 Gan	15.6 Gan		11.0 Gan			/1.4 Coord	/1.4 Coord		0.0 Skin
Queue Length 50th (ft)	Oup	173	77	136	161		132	140	0	00010	164		Skp
Queue Length 95th (ft)		#277	53	#247	237		#237	219	50		222		
Internal Link Dist (It) Turn Bay Length (ft)		367	25		593			363			535		
Base Capacity (vph)		307	648	243	487		408	840	821		958		
Starvation Cap Reductn		0	0	0	0		0	0	0		0		
Spiliback Cap Reductin		0	0	0	0		0	0	0		0		
Reduced v/c Ratio		0.72	0.37	0.76	0.49		0.59	0.30	0.23		0.48		
Intersection Summary													
Area Type:	Other												
Cycle Length: 120 Actuated Cycle Length: 120													
Offset: 25 (21%), Referenced	to phase 1:N	IBSB, Star	t of Greer	1									
Natural Cycle: 95	la at a d												
Maximum v/c Ratio: 0.91	mated												
Intersection Signal Delay: 38.5	5			Int	tersection	OS: D							
Intersection Capacity Utilizatio	n 74.3%			IC	U Level of	Service [)						
# 95th percentile volume exc	ceeds canaci	ty, aueue	may be lo	nger.									
Queue shown is maximum	after two cyc	cles.		3									
Splits and Phases: 3: Adam	is St & Wash	ington St	& Dorches	ster Ave									
1 (R)				*	Ø2								\$ 7.05
33 s				32 s						3	9 s		16 s

2017003::1120 Wa	shington Street
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	Ø2			
Lane Configurations		4>			4			⇔			4					
Traffic Volume (vph)	44	55	56	51	82	58	49	220	23	13	323	33				
Future volume (vpn)	44	1000	1000	1000	82 1900	58 1000	1000	1000	23	1000	323	33				
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00				
Ped Bike Factor								1.00			1.00					
Frt Elt Protoctod		0.951			0.959			0.990			0.988					
Satd Flow (prot)	0	1782	0	0	1798	0	0	1863	0	0	1870	0				
Flt Permitted	-	0.784	-	-	0.835		-	0.894		-	0.987	-				
Satd. Flow (perm)	0	1417	0	0	1521	0	0	1679	0	0	1849	0				
Sate Flow (RTOR)		37	Yes		29	Yes		6	Yes		8	Yes				
Link Speed (mph)		30			30			30			30					
Link Distance (ft)		710			686			615			708					
Travel Time (s)		16.1			15.6			14.0	1		16.1	1				
Peak Hour Factor	0.97	0.97	0.97	0.95	0.95	0.95	0.94	0.94	0.94	0.97	0.97	0.97				
Heavy Vehicles (%)	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%				
Adj. Flow (vph)	45	57	58	54	86	61	52	234	24	13	333	34				
Lane Group Flow (vph)	0	160	0	0	201	0	0	310	0	0	380	0				
Turn Type	Perm	NA	Ū	Perm	NA	Ū	Perm	NA	Ū	Perm	NA	0				
Protected Phases		5			5			1			1		2			
Permitted Phases	5	E		5	E		1	1		1	1					
Switch Phase	0	J		5	0		1	1		1	1					
Minimum Initial (s)	8.0	8.0		8.0	8.0		8.0	8.0		8.0	8.0		1.0			
Minimum Split (s)	13.0	13.0		13.0	13.0		13.0	13.0		13.0	13.0		22.0			
Total Split (S) Total Split (%)	20.0	20.0		20.0	20.0		28.0	28.0		28.0	28.0		22.0			
Maximum Green (s)	15.0	15.0		15.0	15.0		23.0	23.0		23.0	23.0		18.0			
Yellow Time (s)	3.0	3.0		3.0	3.0		3.0	3.0		3.0	3.0		2.0			
All-Red Time (s)	2.0	2.0		2.0	2.0		2.0	2.0		2.0	2.0		2.0			
Total Lost Time (s)		5.0			5.0			5.0			5.0					
Lead/Lag							Lead	Lead		Lead	Lead		Lag			
Lead-Lag Optimize?							Yes	Yes		Yes	Yes		Yes			
Venicle Extension (s) Recall Mode	2.0 None	2.0 None		2.0 None	2.0 None		C-Max	2.0 C-Max		2.0 C-Max	2.0 C-Max		3.0 None			
Walk Time (s)	None	None		None	None		O Max	0 Max		O Max	0 Max		8.0			
Flash Dont Walk (s)													10.0			
Pedestrian Calls (#/hr)		11 7			11 7			20 E			20 E		33			
Actuated q/C Ratio		0.17			0.17			0.56			0.56					
v/c Ratio		0.60			0.72			0.33			0.36					
Control Delay		29.6			38.1			13.7			13.8					
Total Delay		29.6			38.1			13.7			13.8					
LOS		С			D			В			В					
Approach Delay		29.6			38.1			13.7			13.8					
Approach LUS 90th %ile Green (s)	15.0	15 O		15.0	15 0		23.0	23.0		23.0	23.0		18.0			
90th %ile Term Code	Max	Max		Max	Max		Coord	Coord		Coord	Coord		Ped			
70th %ile Green (s)	14.2	14.2		14.2	14.2		23.8	23.8		23.8	23.8		18.0			
70th %ile Term Code	Gap	Gap		Gap	Gap		Coord	Coord		Coord	Coord		Ped			
50th %ile Term Code	Gap	Gap		Gap	Gap		Coord	Coord		Coord	Coord		Skip			
30th %ile Green (s)	9.6	9.6		9.6	9.6		50.4	50.4		50.4	50.4		0.0			
30th %ile Term Code	Gap	Gap		Gap	Gap		Coord	Coord		Coord	Coord		Skip			
10th %ile Term Code	8.0 Min	8.0 Min		8.0 Min	8.0 Min		Coord	Coord		52.0 Coord	Coord		Skip			
Queue Length 50th (ft)		49			70			41			52					
Queue Length 95th (ft)		100			130			181			219					
Internal Link Dist (ft) Turn Bay Length (ft)		630			606			535			628					
Base Capacity (vph)		332			348			948			1045					
Starvation Cap Reductn		0			0			0			0					
Spillback Cap Reductn		0			0			0			0					
Reduced v/c Ratio		0.48			0.58			0.33			0.36					
Intersection Summary																
Area Type:	Other															
Cycle Length: 70																
Actuated Cycle Length: /0 Offcot: 45 (64%) Referenced	to phase 1.N	IDCD Star	rt of Groon													
Natural Cycle: 60	to bugge 1:1/	JJJD, Jtdl	n or Green													
Control Type: Actuated-Coord	linated															
Maximum v/c Ratio: 0.72	0			1-1	orcottor	05.0										
Intersection Capacity Utilization	on 57.5%			Ini IC	U Level of	Service F	3									
Analysis Period (min) 15				10		2011100 L										
Solits and Phases: A. Dorch	nester Δινε/Γι	orchester	St & Richn	nond St												
	ISSICI AVG/D	or on o di ci		iona Jt			11							*		
7 ▼1 Ø1 (R) 28 s							π. 72 s	Ø2						20 s		

Intersection

Int Delay, s/veh

Int Delay, s/veh	0.4						
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	¥		et.			÷	
Traffic Vol, veh/h	4	13	392	4	11	422	
Future Vol, veh/h	4	13	392	4	11	422	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	-	None	-	None	-	None	
Storage Length	0	-	-	-	-	-	
Veh in Median Storage, #	# 0	-	0	-	-	0	
Grade, %	0	-	0	-	-	0	
Peak Hour Factor	92	92	92	92	92	92	
Heavy Vehicles, %	2	2	2	2	2	2	
Mvmt Flow	4	14	426	4	12	459	

Major/Minor	Minor1		Major1		Major2		
Conflicting Flow All	911	428	0	0	430	0	
Stage 1	428	-	-	-	-	-	
Stage 2	483	-	-	-	-	-	
Critical Hdwy	6.42	6.22	-	-	4.12	-	
Critical Hdwy Stg 1	5.42	-	-	-	-	-	
Critical Hdwy Stg 2	5.42	-	-	-	-	-	
Follow-up Hdwy	3.518	3.318	-	-	2.218	-	
Pot Cap-1 Maneuver	304	627	-	-	1129	-	
Stage 1	657	-	-	-	-	-	
Stage 2	620	-	-	-	-	-	
Platoon blocked, %			-	-		-	
Mov Cap-1 Maneuver	300	627	-	-	1129	-	
Mov Cap-2 Maneuver	300	-	-	-	-	-	
Stage 1	657	-	-	-	-	-	
Stage 2	611	-	-	-	-	-	

Approach	WB	NB	SB	
HCM Control Delay, s	12.5	0	0.2	
HCM LOS	В			

Minor Lane/Major Mvmt	NBT	NBRW	BLn1	SBL	SBT
Capacity (veh/h)	-	-	499	1129	-
HCM Lane V/C Ratio	-	- (0.037	0.011	-
HCM Control Delay (s)	-	-	12.5	8.2	0
HCM Lane LOS	-	-	В	А	А
HCM 95th %tile Q(veh)	-	-	0.1	0	-

Appendix C

Air Quality

AIR QUALITY APPENDIX

Introduction

This Air Quality Appendix provides modeling assumptions and backup for results presented in Section 4.5 of the report. Included within this documentation is a brief description of the methodology employed along with pertinent calculations and data used in the emissions and dispersion calculations supporting the microscale air quality analysis.

Motor Vehicle Emissions

The EPA MOVES computer program generated motor vehicle emissions used in the garage stationary source analysis along with the mobile source CAL3QHC modeling and mesoscale analysis. The model input parameters were provided by MassDEP. Emission rates were derived for 2017 and 2024 for speed limits of idle, 10, 15, and 25 mph for use in the microscale analyses.

MOVES CO Emission Factor Summary

Carbon Monoxide Only

		2017	2024
Free Flow	25 mph	2.611	1.758
Right Turns	10 mph	4.058	2.693
Left Turns	15 mph	3.508	2.369
Queues	Idle	8.013	3.216

Notes: Winter CO emission factors are higher than Summer and are conservatively used Urban Unrestricted Roadway type used

CAL3QHC

For the intersection studied, the CAL3QHC model was applied to calculate CO concentrations at sensitive receptor locations using emission rates derived in MOVES. The intersection's queue links and free flow links were input to the model along with sensitive receptors at all locations nearby each intersection. The meteorological assumptions input into the model were a 1.0 meter per second wind speed, Pasquill-Gifford Class D stability combined with a mixing height of 1000 meters. For each direction, the full range of wind directions at 10 degree intervals was examined. In addition, a surface roughness (z₀) of 321 cm was used for the intersection. Idle emission rates for queue links were based on 0 mph emission rates derived in MOVES. Emission rates for speeds of 10, 15, and 25 mph were used for right turn, left turn, and free flow links, respectively.

1120-1132 Washington Street, Boston, MA Background Concentrations

POLLUTANT	AVERAGING TIME	Form	2013	2014	2015	Units	ppm/ppb to <i>µg</i> /m³ Conversion Factor	2013-2015 Background Concentration (<i>µg</i> /m³)	Location
	1-Hour (5)	99th %	10.9	12.3	9.4	ppb	2.62	28.5	Harrison Ave., Boston
SO ⁽¹⁾⁽⁶⁾	3-Hour	H2H	9.7	21.5	8.7	ppb	2.62	56.3	Harrison Ave., Boston
302	24-Hour	H2H	5	5.1	4.3	ppb	2.62	13.4	Harrison Ave., Boston
	Annual	Н	1.1	1.1	0.8	ppb	2.62	2.8	Harrison Ave., Boston
PM 10	24-Hour	H2H	34	61	28	μ g/m ³	1	61	Harrison Ave., Boston
PW-10	Annual	Н	15.1	13.9	12.4	µg/m³	1	15.1	Harrison Ave., Boston
DM 2 5	24-Hour (5)	98th %	15.9	12.7	19	μ g/m ³	1	15.9	Harrison Ave., Boston
170-2.5	Annual ⁽⁵⁾	Н	7.3	6.0	8.8	µg/m³	1	7.4	Harrison Ave., Boston
NO ⁽³⁾	1-Hour (5)	98th %	50	51	53	ppb	1.88	96.5	Harrison Ave., Boston
NO ₂	Annual	Н	17.4	15.8	15.0	ppb	1.88	32.8	Harrison Ave., Boston
CO ⁽²⁾	1-Hour	H2H	1.9	1.7	1.4	ppm	1146	2145.3	Harrison Ave., Boston
0.0	8-Hour	H2H	1.2	1.3	0.9	ppm	1146	1489.8	Harrison Ave., Boston
Ozone (4)	8-Hour	H4H	0.059	0.054	0.056	ppm	1963	115.8	Harrison Ave., Boston
Lead	Rolling 3-Month	Н	0.006	0.014	0.016	µg/m³	1	0.016	Harrison Ave., Boston

Notes: From 2013-2015 EPA's AirData Website ¹ SO₂ reported ppb. Converted to $\mu g/m^3$ using factor of 1 ppm – 2.62 $\mu g/m^3$. ² CO reported in ppm. Converted to $\mu g/m^3$ using factor of 1 ppm – 1144 $\mu g/m^3$. ³ NO₂ reported in ppb. Converted to $\mu g/m^3$ using factor of 1 ppm – 1.88 $\mu g/m^3$. ⁴ O₃ reported in ppm. Converted to $\mu g/m^3$ using factor of 1 ppm – 1963 $\mu g/m^3$. ⁵ Background level is the average concentration of the three years. ⁶ The 24-hour and Annual standards were revoked by EPA on June 22, 2010, Federal Register 75-119, p. 35520.

Due to excessive size CAL3QHC, and MOVES input and output files are available on digital media upon request.
Appendix D

Climate Change Preparedness Checklist

AIR QUALITY APPENDIX

Introduction

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PM-2.5	24-Hour (5)	98th %	15.9	12.7	19	μ g/m ³	1	15.9	Harrison Ave., Boston
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NO ⁽³⁾	1-Hour (5)	98th %	50	51	53	ppb	1.88	96.5	Harrison Ave., Boston
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Appendix E

Accessibility Checklist

Article 80 – Accessibility Checklist

A requirement of the Boston Planning & Development Agency (BPDA) Article 80 Development Review Process

The Mayor's Commission for Persons with Disabilities strives to reduce architectural, procedural, attitudinal, and communication barriers that affect persons with disabilities in the City of Boston. In 2009, a Disability Advisory Board was appointed by the Mayor to work alongside the Commission in creating universal access throughout the city's built environment. The Disability Advisory Board is made up of 13 volunteer Boston residents with disabilities who have been tasked with representing the accessibility needs of their neighborhoods and increasing inclusion of people with disabilities.

In conformance with this directive, the BDPA has instituted this Accessibility Checklist as a tool to encourage developers to begin thinking about access and inclusion at the beginning of development projects, and strive to go beyond meeting only minimum MAAB / ADAAG compliance requirements. Instead, our goal is for developers to create ideal design for accessibility which will ensure that the built environment provides equitable experiences for all people, regardless of their abilities. As such, any project subject to Boston Zoning Article 80 Small or Large Project Review, including Institutional Master Plan modifications and updates, must complete this Accessibility Checklist thoroughly to provide specific detail about accessibility and inclusion, including descriptions, diagrams, and data.

For more information on compliance requirements, advancing best practices, and learning about progressive approaches to expand accessibility throughout Boston's built environment. Proponents are highly encouraged to meet with Commission staff, prior to filing.

Accessibility Analysis Information Sources:

- 1. Americans with Disabilities Act 2010 ADA Standards for Accessible Design http://www.ada.gov/2010ADAstandards_index.htm
- 2. Massachusetts Architectural Access Board 521 CMR http://www.mass.gov/eopss/consumer-prot-and-bus-lic/license-type/aab/aab-rules-and-regulations-pdf.html
- 3. Massachusetts State Building Code 780 CMR http://www.mass.gov/eopss/consumer-prot-and-bus-lic/license-type/csl/building-codebbrs.html
- 4. Massachusetts Office of Disability Disabled Parking Regulations http://www.mass.gov/anf/docs/mod/hp-parking-regulations-summary-mod.pdf
- 5. MBTA Fixed Route Accessible Transit Stations <u>http://www.mbta.com/riding_the_t/accessible_services/</u>
- 6. City of Boston Complete Street Guidelines http://bostoncompletestreets.org/
- 7. City of Boston Mayor's Commission for Persons with Disabilities Advisory Board www.boston.gov/disability
- City of Boston Public Works Sidewalk Reconstruction Policy <u>http://www.cityofboston.gov/images_documents/sidewalk%20policy%200114_tcm3-41668.pdf</u>
 Other of Poston – Public Improvement Commission Sidewalk 20ff Policy
- 9. City of Boston Public Improvement Commission Sidewalk Café Policy <u>http://www.cityofboston.gov/images_documents/Sidewalk_cafes_tcm3-1845.pdf</u>

Glossary of Terms:

- 1. *Accessible Route* A continuous and unobstructed path of travel that meets or exceeds the dimensional and inclusionary requirements set forth by MAAB 521 CMR: Section 20
- 2. *Accessible Group 2 Units* Residential units with additional floor space that meet or exceed the dimensional and inclusionary requirements set forth by MAAB 521 CMR: Section 9.4
- 3. *Accessible Guestrooms* Guestrooms with additional floor space, that meet or exceed the dimensional and inclusionary requirements set forth by MAAB 521 CMR: Section 8.4
- 4. *Inclusionary Development Policy (IDP)* Program run by the BPDA that preserves access to affordable housing opportunities, in the City. For more information visit: <u>http://www.bostonplans.org/housing/overview</u>
- 5. *Public Improvement Commission (PIC)* The regulatory body in charge of managing the public right of way. For more information visit: <u>https://www.boston.gov/pic</u>
- 6. *Visitability* A place's ability to be accessed and visited by persons with disabilities that cause functional limitations; where architectural barriers do not inhibit access to entrances/doors and bathrooms.

1. Project Information:

If this is a multi-phased or multi-building project, fill out a separate Checklist for each phase/building.

	Project Name:	1120-1132 Washington Street				
	Primary Project Address:	1120-1132 Washington Street				
	Total Number of Phases/Buildings:	One				
	Primary Contact (Name / Title / Company / Email / Phone):	John Sambucci / City	/ Point Development / john@cityp	pointdev	elopment.com	
	Owner / Developer:	City Point Developme	ent LLC			
	Architect:	RCA, LLC				
	Civil Engineer:	Howard Stein Hudson				
	Landscape Architect:	R. Jon Henson Landscape Architects				
	Permitting:	Epsilon Associates				
	Construction Management:					
L	At what stage is the project at time of this questionnaire? Select below:					
		☑PNF / Expanded PNF Submitted	Draft / Final Project Impact Report Submitted	BPDA	Board Approved	
		BPDA Design Approved	Under Construction	Constr Compl	ruction eted:	
	Do you anticipate filing for any variances with the Massachusetts Architectural Access Board (MAAB)? <i>If yes,</i> identify and explain.	No MAAB variances a	are anticipated.			
2. Building Classification and Description: This section identifies preliminary construction information about the project including size and uses.						
	What are the dimensions of the project?					
	Site Area:	48,303 SF	Building Area:		67,000 GSF	
	Building Height:	40 FT.	Number of Stories:		4 Flrs.	
	First Floor Elevation:	55 BCB	Is there below grade space	-	Yes	

What is the Construction Type? (Select most appropriate type)					
	⊠Wood Frame	Masonry	⊠Steel Frame	⊠Concrete	
What are the principal building uses?	? (IBC definitions are b	elow - select all approp	oriate that apply)		
	Residential – One - Three Unit	☑Residential - Multi-unit, Four +	Institutional	Educational	
	⊠Business	Mercantile	Factory	Hospitality	
	Laboratory / Medical	Storage, Utility and Other		_	
List street-level uses of the building:	Residential, commercial				
3. Assessment of Existing Infrastructure for Accessibility: This section explores the proximity to accessible transit lines and institutions, such as (but not limited to) hospitals, elderly & disabled housing, and general neighborhood resources. Identify how the area surrounding the development is accessible for people with mobility impairments and analyze the existing condition of the accessible routes through sidewalk and pedestrian ramp reports.					
Provide a description of the neighborhood where this development is located and its identifying topographical characteristics:	The Project site is located in the Lower Mills neighborhood at the southeastern edge of Dorchester. Immediately to the west of the site is the Mattapan neighborhood of Boston, and to the south just across the Neponset River is the town of Milton. The area surrounding the Project site contain a mix of uses, including two to three-story residential buildings as well as some commercial uses. The topography in the area is generally flat, sloping gradually downhill as you go south down Dorchester Avenue and Adams Street.				
List the surrounding accessible MBTA transit lines and their proximity to development site: commuter rail / subway stations, bus stops:	MBTA Bus #27 – River Street				
List the surrounding institutions: hospitals, public housing, elderly and disabled housing developments, educational facilities, others:	Within the vicinity of the Project site is the Conservatory Lab Charter School and the Carney Hospital.				
List the surrounding government buildings: libraries, community centers, recreational facilities, and other related facilities:	Within the vicinity of the site is the Boston Public Library – Lower Mills Branch. There are also numerous open spaces in the area.				
4. Surrounding Site Conditions – Existing: This section identifies current condition of the sidewalks and pedestrian ramps at the development site.					

Is the development site within a	The Project site is not within a historic district.
historic district? <i>If yes,</i> identify which	
district:	

Are there sidewalks and pedestrian ramps existing at the development site? <i>If yes</i> , list the existing sidewalk and pedestrian ramp dimensions, slopes, materials, and physical condition at the development site:	Yes, the existing concrete sidewalk at Washington Street is 8' wide. The existing sidewalk does not have a handicap ramp at the Project site.
Are the sidewalks and pedestrian ramps existing-to-remain? <i>If yes,</i> have they been verified as ADA / MAAB compliant (with yellow composite detectable warning surfaces, cast in concrete)? <i>If yes,</i> provide description and photos:	Yes, with modifications for new driveway entrances into the property. No, the existing sidewalks and pedestrian ramps have not been verified as being in compliance at this time, but will be verified during the Project design.
5. Surrounding Site Conditions – Pro This section identifies the propose development site. Sidewalk width sidewalks do not support lively p people to walk in the street. Wide comfortably walking alone, walking	oposed sed condition of the walkways and pedestrian ramps around the h contributes to the degree of comfort walking along a street. Narrow edestrian activity, and may create dangerous conditions that force er sidewalks allow people to walk side by side and pass each other ing in pairs, or using a wheelchair.
Are the proposed sidewalks consistent with the Boston Complete Street Guidelines? <i>If yes</i> , choose which Street Type was applied: Downtown Commercial, Downtown Mixed-use, Neighborhood Main, Connector, Residential, Industrial, Shared Street, Parkway, or Boulevard.	Yes. The residential Street Type was applied.
What are the total dimensions and slopes of the proposed sidewalks? List the widths of the proposed zones: Frontage, Pedestrian and Furnishing Zone:	The sidewalk along Washington Street is approximately 8' wide with minimal slope. The frontage, pedestrian, and furnishing zones will be designed in accordance with Complete Streets Guidelines.
List the proposed materials for each Zone. Will the proposed materials be on private property or will the proposed materials be on the City of Boston pedestrian right-of-way?	Existing materials are concrete with granite curbing along Washington Street – All materials will be on the City of Boston pedestrian right-of-way
Will sidewalk cafes or other furnishings be programmed for the pedestrian right-of-way? <i>If yes,</i> what are the proposed dimensions of the sidewalk café or furnishings and	No

what will the remaining right-of-way clearance be?	
If the pedestrian right-of-way is on private property, will the proponent seek a pedestrian easement with the Public Improvement Commission (PIC)?	N/A
Will any portion of the Project be going through the PIC? <i>If yes,</i> identify PIC actions and provide details.	This will be determined as the Project continues to develop the scope of work in the public way.
6. Accessible Parking: See Massachusetts Architectura regarding accessible parking req Parking Regulations.	l Access Board Rules and Regulations 521 CMR Section 23.00 juirement counts and the Massachusetts Office of Disability – Disabled
What is the total number of parking spaces provided at the development site? Will these be in a parking lot or garage?	94 parking spaces, partially in a below-grade garage and partially at grade.
What is the total number of accessible spaces provided at the development site? How many of these are "Van Accessible" spaces with an 8 foot access aisle?	There will be four accessible spaces. The exterior accessible spaces will have 7 foot wide access aisles.
Will any on-street accessible parking spaces be required? <i>If yes,</i> has the proponent contacted the Commission for Persons with Disabilities regarding this need?	None will be required.
Where is the accessible visitor parking located?	Two spaces are in the retail parking area and the other two spaces are in the basement level parking garage
Has a drop-off area been identified? <i>If yes,</i> will it be accessible?	Yes the drop off and pick up area will be in the retail parking area of the site
7. Circulation and Accessible Routes The primary objective in designir entryways and common spaces, with neighbors.	s: ng smooth and continuous paths of travel is to create universal access to which accommodates persons of all abilities and allows for visitability
Describe accessibility at each entryway: Example: Flush Condition, Stairs, Ramp, Lift or Elevator:	Flush Conditions.
Are the accessible entrances and standard entrance integrated? <i>If yes,</i>	Yes

describe. <i>If no</i> , what is the reason?	
If project is subject to Large Project Review/Institutional Master Plan, describe the accessible routes way- finding / signage package.	Accessible routes diagrams are attached. A way finding/signage package has not yet been developed, but will be developed to meet Building Code and Accessibility Board requirements.
8. Accessible Units (Group 2) and G In order to facilitate access to he units that are proposed for the d	uestrooms: (If applicable) Dusing and hospitality, this section addresses the number of accessible levelopment site that remove barriers to housing and hotel rooms.
What is the total number of proposed housing units or hotel rooms for the development?	Approximately 57 residential units are proposed.
<i>If a residential development,</i> how many units are for sale? How many are for rent? What is the breakdown of market value units vs. IDP (Inclusionary Development Policy) units?	All units will be for sale. Approximately 13% of the 57 units will be IDP units, which results in seven units.
<i>If a residential development,</i> how many accessible Group 2 units are being proposed?	All residential units will all be Group 1 Adaptable and 5% of units will be Group 2
<i>If a residential development,</i> how many accessible Group 2 units will also be IDP units? <i>If none</i> , describe reason.	It is anticipated that one of the accessible units will also be an IDP unit.
<i>If a hospitality development,</i> how many accessible units will feature a wheel-in shower? Will accessible equipment be provided as well? <i>If</i> <i>yes,</i> provide amount and location of equipment.	
Do standard units have architectural barriers that would prevent entry or use of common space for persons with mobility impairments? Example: stairs / thresholds at entry, step to balcony, others. <i>If yes</i> , provide reason.	No.
Are there interior elevators, ramps or lifts located in the development for access around architectural barriers and/or to separate floors? <i>If yes</i> , describe:	

9. Community Impact:

Accessibility and inclusion extend past required compliance with building codes. Providing an overall scheme that allows full and equal participation of persons with disabilities makes the development an asset to the surrounding community.

Is this project providing any funding or improvements to the surrounding neighborhood? Examples: adding extra street trees, building or refurbishing a local park, or supporting other community-based initiatives?	The Proponent has contributed \$2,500 towards improvements for Dorchester Park, which is in the vicinity of the Project site. The Proponent has pledged an additional \$10,000 for civic causes, and the City and neighborhood associations will determine the most appropriate use for this funding. The Project will provide, on site, additional street trees and ornamental pole lighting, to cover the existing street walk, as well as entry walks into the building.
What inclusion elements does this development provide for persons with disabilities in common social and open spaces? Example: Indoor seating and TVs in common rooms; outdoor seating and barbeque grills in yard. Will all of these spaces and features provide accessibility?	Access for persons with disabilities will be provided on all pathways from parking and open spaces to and from the building. A space will be designated for an accessible barbeque grill in the green space being developed on site as a part of the Project. The Condo Association will be responsible for determining the status of the grill.
Are any restrooms planned in common public spaces? <i>If yes,</i> will any be single-stall, ADA compliant and designated as "Family"/ "Companion" restrooms? <i>If no</i> , explain why not.	There are no restrooms planned in the common spaces of the residential portion of the building. The restrooms for the commercial space will be designed once tenants have been finalized.
Has the proponent reviewed the proposed plan with the City of Boston Disability Commissioner or with their Architectural Access staff? <i>If yes,</i> did they approve? <i>If no,</i> what were their comments?	No.
Has the proponent presented the proposed plan to the Disability Advisory Board at one of their monthly meetings? Did the Advisory Board vote to support this project? <i>If</i> <i>no</i> , what recommendations did the Advisory Board give to make this project more accessible?	The Proponent has not presented the plan to the Advisory Board.

10. Attachments

Include a list of all documents you are submitting with this Checklist. This may include drawings, diagrams, photos, or any other material that describes the accessible and inclusive elements of this project.

Provide a diagram of the accessible routes to and from the accessible parking lot/garage and drop-off areas to the development entry locations, including route distances. **See attached.**

Provide a diagram of the accessible route connections through the site, including distances. See attached.

Provide a diagram the accessible route to any roof decks or outdoor courtyard space? (if applicable) See attached.

Provide a plan and diagram of the accessible Group 2 units, including locations and route from accessible entry. **See** attached.

Provide any additional drawings, diagrams, photos, or any other material that describes the inclusive and accessible elements of this project.

- •
- •
- •
- •

This completes the Article 80 Accessibility Checklist required for your project. Prior to and during the review process, Commission staff are able to provide technical assistance and design review, in order to help achieve ideal accessibility and to ensure that all buildings, sidewalks, parks, and open spaces are usable and welcoming to Boston's diverse residents and visitors, including those with physical, sensory, and other disabilities.

For questions or comments about this checklist, or for more information on best practices for improving accessibility and inclusion, visit <u>www.boston.gov/disability</u>, or our office:

The Mayor's Commission for Persons with Disabilities 1 City Hall Square, Room 967, Boston MA 02201.

Architectural Access staff can be reached at:

accessibility@boston.gov | patricia.mendez@boston.gov | sarah.leung@boston.gov | 617-635-3682



1120 Washington Street Boston, Massachusetts





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